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1. Survey Information and Objectives

The Western Trident was contracted to undertake a 3D Marine Seismic Survey for **Apache Energy Limited** in the blocks VIC/P-47 & VIC/P-58, Gippsland Basin, Australia. The SUE survey was located in block VIC/P-58, Client reference GAP04B

The Western Trident will tow an in-sea configuration comprising of eight streamers, each 4800 m long, at a separation of 100 m and a depth of 8m. The energy source will comprise of dual 3000 cubic inch Sleeve airgun, clustered arrays, towed astern of the vessel at a depth of 7m the energy is released from alternate arrays every 18.75 meters along the pre-plotted survey line. The operating pressure of the energy source was 2000 psi.

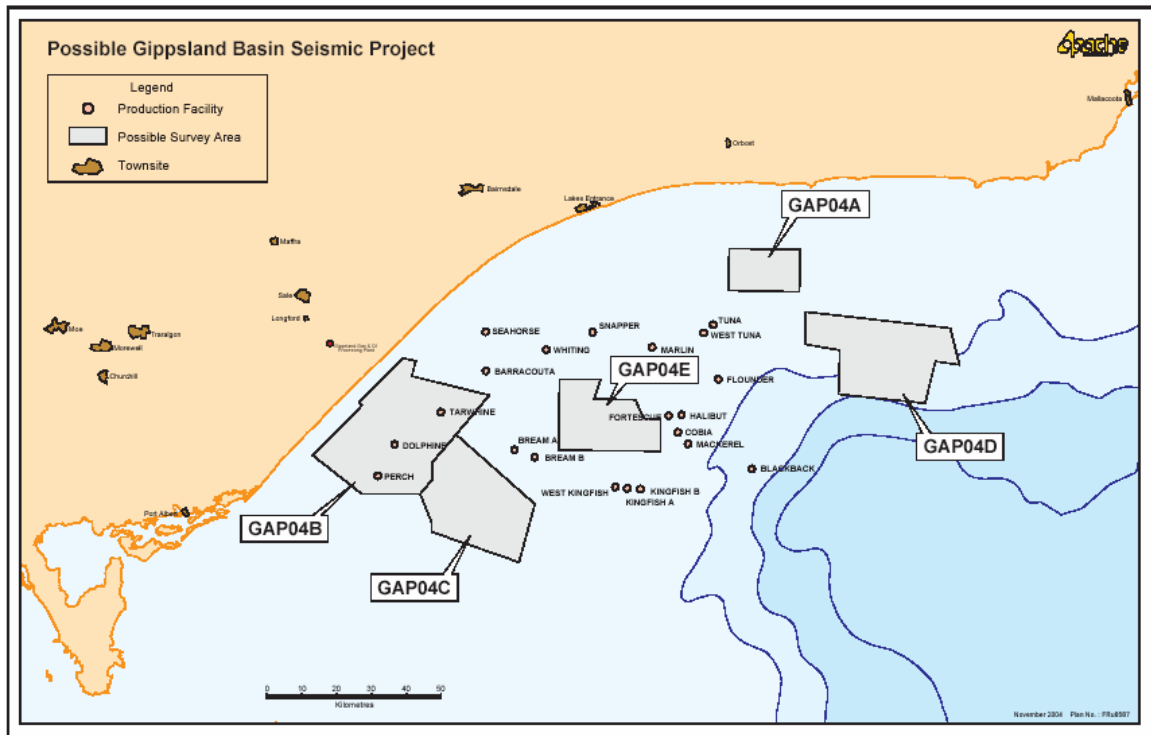
The *M/V Western Trident* is a purpose built vessel for seismic operations and is one of the largest vessels in WesternGeco's fleet. She was delivered in November 1999. The vessel has carried out many complex 3D surveys in various locations worldwide. She is capable of towing 12 x 6,000m TMS Sentry Solid streamers with a maximum separation of 1,200m when using the Monowings.

The vessel is built to DNV+1A1 ICE-1A, EO Helideck classification and to the satisfaction of the rules and regulations of SOLAS 1974. International load line requirements are according to international load line convention of 1966.

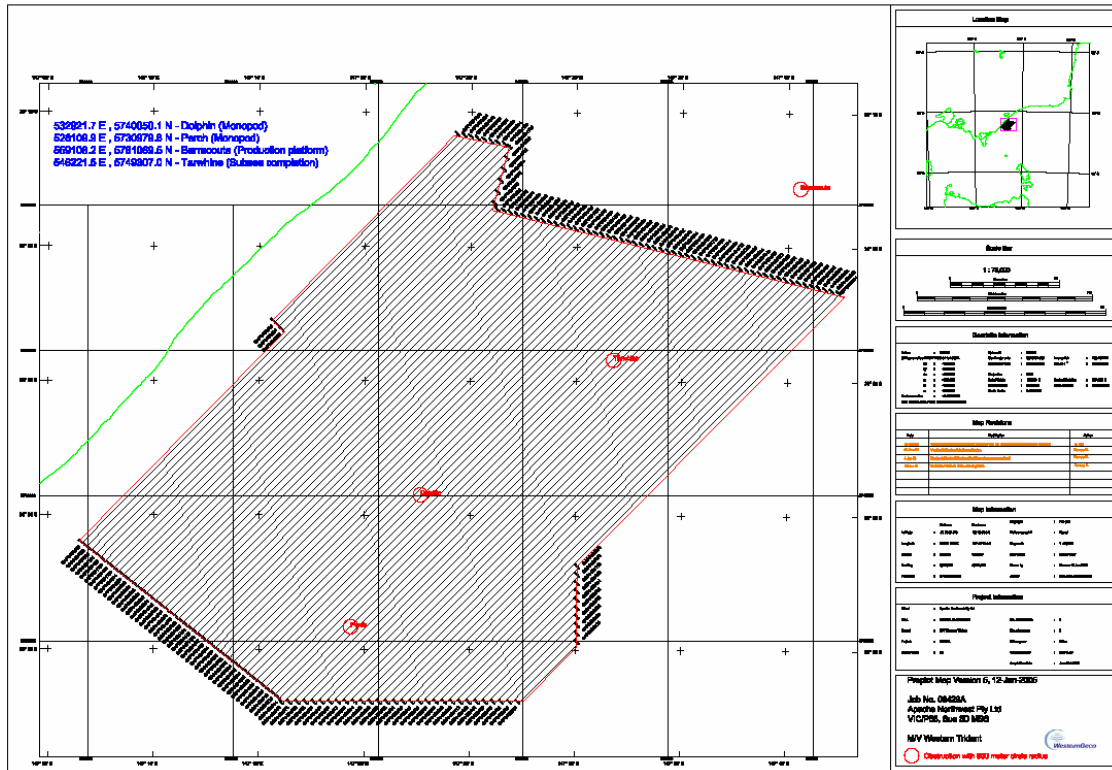
There were 2 obstructions within the VIC/P-58 survey area that required undershoot operations and further details concerning these operations can be found in section 2 of this report.

Apache Energy Pty Ltd chartered the vessel Multiwave seismic survey vessel MV Pacific Titan as the "undershoot source vessel". WesternGeco installed a two boat link communications system on board the Pacific Titan to enable to two vessels to work in tandem.

2. Area Map



3. Program Map



4. Job Book



Seismic Job Book

Version : 12

Job number: 9429	Client: Apache Northwest Pty. Ltd.	Location: AUS / VIC/P58, Sue 3D MSS
Chapter status: Reviewed by vessel	Chapter updated: 17-Jan-05	Chapter updated by: cctee
Project Geo: Tee Chee Cherng (phone : +60 3 2730 8844, email : cctee@slb.com)		

Seismic Acquisition Parameters

General

Client:	Apache Northwest Pty. Ltd.
Vessel(s):	Western Trident
Bid reference:	
Job number:	9429
Contract number:	
Location:	VIC/P58, Sue 3D MSS
Country:	Australia
Corporation code:	Apache_Energy
Client reference:	
Type of survey:	3D marine streamer
Estimated start date:	11-Jan-05
Estimated duration (days):	43
SuperVision required:	No

Project geo:	
name:	Tee Chee Cherng
email:	cctee@slb.com
telephone:	+60 3 2730 8844
Nav supervisor:	
name:	Kumara Krishnasamy
email:	kkrishnasamy@slb.com
telephone:	+60 3 2730 8851
Sales contact:	
name:	Sean Murray
email:	smurray2@perth.westerngeco.slb.com
telephone:	+61 (0)8 9420 4798
Vessel manager:	
name:	Kiran Tuite
email:	tuite1@kuala-lumpur.westerngeco.slb.com
telephone:	+60 3 2730 8861

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Section 1: General Information



Seismic Job Book

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Project Geo: Tee Chee Cherng (phone : +60 3 2730 8844, email : cctee@slb.com)		

Seismic Acquisition Parameters

Survey Area

Area (km2):	1066.711
Average line length (km):	34.829
Number of saillines:	77
Heading (deg):	44.566
Reciprocal heading (deg):	224.566

Streamer Parameters

Cable type:	MSX solid streamer
Module type:	MSX
Number of streamers:	8
Group length (m):	17.75
Number of phones per group:	14
Group interval (m):	12.5
Lo-cut analogue response (Hz-dB/Oct):	2.5-6
Hydrophone sensitivity (V/B):	13.8
Pre-amplifier gains (dB or mB full scale):	6
Streamer length (m):	4800.0
Streamer depth (m):	8.0
Streamer separation (m):	100.0
Number of groups per streamer:	384
Requested source to receiver offset (m):	As Near As Possible/150

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Section 1: General Information



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Seismic Acquisition Parameters

Recording Parameters:

Recording system:	MSX
Recording format:	SegD 8058, Rev 1
Record length (binary sec.):	5.0
Sample rate (ms):	2
Lo-cut recording filter (Hz-dB/Oct):	2-12
Hi-cut recording filter (Hz-dB/Oct):	206-264
Recording system delay (ms):	0
Filter type:	Zero phase

Adjacent trace summation 12.5m to 25m:	No
Record auxiliary channels:	Yes
Offline tape copy required:	No

Dual recording/tape copies (Group formed tapes): Yes

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Section 1: General Information



Seismic Job Book

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Chapter status: Ready for review	Chapter updated: 14-Jan-05	Chapter updated by: kkrishnasamy
Nav Supervisor: Kumara Krishnasamy (phone : +60 3 2730 8851, email : kkrishnasamy@slb.com)		

Positioning Acquisition Parameters

Acquisition Geodetic Parameters

Work datum:

Work datum name: GDA 94

Spheroid name: GRS80

Semi major axis (m): 6378137.0

Inverse flattening (1/f) (m): 298.257222

Datum Transformation From WGS 84 to Local Datum (Bursa Wolf Convention):

dX (m): 0.0

dY (m): 0.0

dZ (m): 0.0

rX (arc secs): 0.0

rY (arc secs): 0.0

rZ (arc secs): 0.0

Scale (ppm): 0.0

Projection type: UTM

Zone: 55S

Central meridian: 147° 0' 0.0" E

Scale factor: 0.9996

False easting (m): 500000

False northing (m): 10000000

Latitude of origin: 0° 0' 0.0" N

Test Point

Latitude in WGS 84: 38° 26' 22.872" S

Longitude in WGS 84: 147° 23' 48.329" E

Northing in WGS 84: 5745324.46

Easting in WGS84: 534625.36

Latitude in local datum: 38° 26' 22.872" S

Longitude in local datum: 147° 23' 48.329" E

Northing in local projection (m): 5745324.46

Easting in local projection (m): 534625.36

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Section 1: General Information



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Positioning Acquisition Parameters

Magnetic Variation and Geoidal Height

Location of prospect centre, latitude: 38° 26' 22.872" S
Location of prospect centre, longitude: 147° 23' 48.329" E
Magnetic variation:
Annual magnetic variation change:
Source of variation data: IGRF2000
Geoidal height data (m):
Source of geoidal height data: EGM96
Date for which values calculated:

Vessel Positioning

Integrated navigation system: TriNav 2.6
Number of independently positioned vessels: 1

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Section 1: General Information



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Nav Supervisor: Kumara Krishnasamy (phone : +60 3 2730 8851, email : kkrishnasamy@slb.com)		

Positioning Acquisition Parameters

Vessel Positioning

Vessel name : Western Trident

Primary navigation system

Vessel position computation system: Cnav
RTCM delivery system: Global Monitoring
Delivery method: Inmarsat
Survey and differential company: C&C Technologies
Contact person: Terry Tay , terry.tay@cctechnol.com
DGPS reference stations:
Via Global network
Contact details (in Singapore):
Terry Tay
Tel: +65 62959738
Mob: +65 91276385
Email: terry.tay@cctechnol.com
(Global 24-hr support):
Tel: +1 (337) 261-0660
email: cnav.support@cctechnol.com

Secondary navigation system

Vessel position computation system: Fugro Multifix 4
RTCM delivery system: Global Monitoring XP
Delivery method: Inmarsat / Spotbeam
Survey and differential company: Fugro Survey
Contact person: Avezac, D Rene, rdavezac@FUGRO.com.sg
DGPS reference stations:
Via Global Monitoring
Skyfix NCC In Singapore
Tel: +65 6863 0604 (24-hr/365 days per year hotline)
Email: skyfix@omnistar.com.sg
Starfix NCC in Perth, Australia
Tel: +61 89 321 0284, +61 89 322 5295 (24-hr/365 days per year hotline)
Email: ncc@fugro.com.au
Tel: +65 6863 0604 (24-hr hotline)
Email: Skyfix Singapore <skyfix@omnistar.com.sg>

Tertiary navigation system

Vessel position computation system: Trinav GPS 2.6

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Positioning Acquisition Parameters

RTCM delivery system: Fugro Skyfix
Delivery method: Inmarsat
Survey and differential company: Fugro Survey
Contact person: Singapore Network Control Centre (24hrs) +65 6863 0604
DGPS reference stations:
Please use all available Reference stations.

Skyfix NCC In Singapore
Tel: +65 6863 0604 (24-hr/365 days per year hotline)
Email: skyfix@omnistar.com.sg

Starfix NCC in Perth, Australia
Tel: +61 89 321 0284, +61 89 322 5295 (24-hr/365 days per year hotline)
Email: ncc@fugro.com.au
Tel: +65 6863 0604 (24-hr hotline)
Email: Skyfix Singapore <skyfix@omnistar.com.sg>

Section 1: General Information



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Positioning Acquisition Parameters

Streamer Parameters

Positioning:

Source surface positioning:	POSNET
Front-net in-sea positioning:	DigiCOURSE
Mid-streamer in-sea positioning:	DigiCOURSE
Tail-net in-sea positioning :	DigiCOURSE
Full streamer IRMA network:	No
Tailbuoy surface positioning:	Posnet
Compass bird type:	DigiCOURSE
Distance between adjacent compasses (m):	300

Section 1: General Information



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Project Geo: Tee Chee Cherng (phone : +60 3 2730 8844, email : cctee@slb.com)		

Source Acquisition Parameters

Source type:	Tuned sleevegun array
Number of source arrays:	2
Alternatively fired sources (flip-flop):	Yes
Source array separation (m):	50.0
Inline stagger required:	No
Shotpoint interval (m):	18.75
Shotpoint interval per source (m):	37.5
Array volume per source (ln3):	3000.0
Operating pressure (psi):	2000
Source depth (m):	7.0
Number of subarrays per source:	4
Subarray separation (m)	6
Number of airguns per subarray:	8
Subarray length (m):	15.1
Gun timing specification (ms):	1.25
Source control system:	SSS
Record nearfields:	Yes
CMS required:	No

Total SCFM required at 4.8 knots: 1420

Timebreak control: Volume

Specification:

https://www.vessel.int.slb.com:181/gpclient/vessels/Western_Trident/9438/Acquisition_Information/Job_Book/v3000d6SS6mDFS_V_FDDrop_Out.pdf

5. Vessel Description

Maritime Specifications / Particulars

Main Particulars

Ships Name	Western Trident
Call Sign	3FE09 (Three, Foxtrot, Echo Zero, Nine)
International Maritime Org. (Imo) No.	9187502
Owner	Seismic Shipping INC
Previous Name	N/A
Flag State & Port Of Registry	Panama, Panama
Panama Official No.	27927-Pext-2
Date Of Build	1-Mar-99
Yard No. And Type Of Vessel	Build 241, Type UT
Yard Built	Ulstein Shipyard, Ulsteinvik, Norway
Date Converted / Power Upgraded	11/2003 Monowing upgrade
Yard Converted	BMV Bergen
Classification Society And Class	DNV, +1A1, EO, HELDK, ICE-C
Class Id No.	20519
Classification Machinery System	PMS, CMS
Class Approved Maintenance System	TM-Master, Windows based
International Safety Management, (Ism) Code Compliance	DNV SMC. Valid until 05-Oct-06
Safe Manning Certificate (Minimum)	No.M3026 (10 crew)

Principal Particulars

Gross Tonnage (Grt)	8369
(Grt) National & International	8369
Gross Tonnage (Grt) Suez Canal	8862.6
Net. Reg.Ton (Nrt) Panama Canal	n/a
(Nrt) National & International	2511
Net. Reg. Ton (Nrt) Suez Canal	6913.12
Lightship Displacement	4667
Dead Weight	4568
Length Over All (Loa)	92.50m
Length Between Perpendiculars	80.10m
Breadth (Moulded)	23.00m
Breadth (Extreme)	25.00m
Depth (Moulded)	9.00m
Draft (Max)	7.30m (Summer)
Draft (Mean)	6.40m (Design)
Air Draft (To Higest Antenna)	32.70m (Summer draft)
Helicopter Deck Rating	Sikorsky S-61 / 9.3t Max
Helicopter Deck Diameter (D-Value)	22.80m
Helicopter Deck Markings Standard	CAA / CAP437 / BHAB

Section 1: General Information

Capacities And Endurance's

Cable / Towpoints / Subarrays	TMS Solid / 16 Tow Points / 10 Sub arrays
Bollard Pull	142t x 100% power
Fresh Water Capacity	440 M ³
Fresh Water Maker Production	2 x 12 tons / 24 Hrs.
Potable Water System	Evaporators, 2 x Alfa Laval De-Salt.
Fuel Capacity, All Tanks Topped	3550 M ³
Fuel, Useful For 100 % Consumption	3250 M ³
Fuel Type	Gas oil
Fuel Tank Heating	N/A
Lub. Oil, Engine Oil (M ³)	30 M ³
CYLINDER OIL, HP COMPRESSORS (M ³)	7 M ³ cylinder oil, 7 M ³ screw compressor oil.
CABLE OIL, KEROSENE (Clean/Dirty)	11 M ³ clean / 7 M ³ dirty
BALLAST, SEA WATER (M ³)	3150 M ³
Speed, Transit, Max. In Calm Sea	15 Knots
Speed, Transit Economy, Ditto	12 Knots
Consumption Of Fuel , Full Speed	36 M ³ / 24 Hrs
Consumption Of Fuel, Economy Speed	26 M ³ / 24 Hrs
Operational Endurance	86 Days (+4 days safety)
Endurance Of Fuel During Survey	85 days, operating with 10 streamers
Consumption Of Fuel In Port	3 M ³ / 24 Hrs
Safety Equipment Certificate	68 Persons

Bridge Navigation Equipment

Radar No 1	FURUNO FAR 2835S (s-band)
Radar No 2	FURUNO FAR 2825 (x-band)
Radar No 3	N/A
Ecdis	SIMRAD SPS COS-100
Gyro Compass	SIMRAD RGC 11
Auto Pilot	SIMRAD AP9 Mk3 / SJS500 Joystick/Autotrack System
Gps Receiver	1 x FURUNO GP80 + 1 x TRIMBLE NT300D
Speed Log	BEN ANTHEA Electro. Mag.
Echo Sounder	SKIPPER GDS 101
Radio's, Vhf, Gmdss*, Type 1	3 x SKANTI VHF 1000 DSC
Radio's, Vhf, Gmdss*, Type 2	3 x NAVICO AXIS 250 (portable)
Radio's, Vhf	6 x MOTOROLA GP340 (portable)
Radio's, Uhf	1 x Motorola GM 300
Radio Direction Finder	N/A
Weather Facsimile	FURUNO DFAX-208 Mk2
Navtex Receiver	ICS ELECTRONIC Nav5
Ups, Power Supply To All Gmdss Radio's	FN Electro Converter/Charger with lead acid battery back up.

Section 1: General Information

Communication Equipment, Compliant With Gmdss Requirements

Radio Station Licence No.	06-11-2003/1 Panama
Class / Corr. Category	A1, A2, A3. GMDSS
Ship / Air Craft Radio	JOTRON TR-6101 (fixed) + Dittel FSG 5
Helicopter Beacon	SAC DS410 (410 KHz. I.D. 'T R I D')
Automatic Identification System (AIS)	
Transmitter / Receiver, Main (Mf)	SKANTI TRP 8251D
Transmitter / Receiver, Reserve (Mf)	N/A
Transmitter / Receiver, Main (Vhf)	3 x SKANTI VHF 1000 DSC
Transmitter / Receiver, Main (Dsc)	SKANTI DSC9000 MF/HF DSC CONTROLLER/RECEIVER
Ais. Automatic Identification System	SKANTI UAIS 2100
Radio, Portable, VHF	6 x MOTOROLA GP340
Booster Unit For Portable Radio (Uhf)	4 x MOTOROLA GP328
Emergency Radio Beacon (Epirb)	N/A
Radar Transponder	JOTRON TRON 40S 406/121.5 MHz
Radar Transponder	2 x JOTRON TRON SART 9 GHz
Radio, Lifeboat, Vhf	3 x NAVICO AXIS 250 (portable)

Satellite Communications

MMSI Number	357 270 000
Inmarsat Type B	NERA SATURN B. Tel:335 726 910 Fax:335 726 911 Data9600: 335 726 912
Inmarsat Type C	2 x SKANTI CAPSAT 435 726 910 and 920
V-Sat Uk	44-207 576 6870
V-Sat Usa	1-713 296 5370
Telefax Machine	SAME AS V-SAT THEN TRANSFERRED
Internal E-Mail & Pc-Network	Eudora, Ethernet
E-Mail Address To Vessel	captain@trident.vessel.int.slb.com

Safety Equipment Crew

Lifeboat Type / Capacity/ No. Of Boats	2 x Norsafe 70 Pers each.
Engine, Lifeboat	Sabb type 4L 186 LB
Liferafts Type /Capacity	Viking, 4 x 25 Pers and 2 x 20 Pers.+ 1 MOB raft x 6 Pax
Number Of Life Rafts	6 rafts total. + 1 MOB
Lifejackets Nos.	142 (Seamaster-1983)
Survival Suits, Thermo Insulated	68 (Koppernaes)
Working Suits, Thermo Insulated	30 x 'Mustang' + 10 'Aqua' Dry suits.
Man Overboard Boat (Mob) Type	Norsafe Magnum, 7.5 mtr.
Engine, Mob And Speed Of Boat	Yanmar 4LH-STE 4 Cyl. Turbo. Appr. 25 knots
Waterjet And Gear Drive, Mob	Hamilton 212 water jet, ZF Hurth gear, HSW 630
Work Boats	CMV AND 25 FOOT NORPOWER WORKBOAT
Engine Work Boat And Speed Of Boat	CMV 2 X Mermaid Turbo-Four II engines 20Kn. Norpower NOGVA/CUMMINS type 6BT5.9M 210HP Speed 15Kn

Section 1: General Information

Fixed Fire Extinguisher System

Engine Room	Inergen, Zenith Electro. 103 pcs. Bottles w/volume 50 ltr Pressure: 300 bar
Separator Room	N/A
Incinerator Room / Galley Ducting	Inc. Room: Inergen. / Galley: CO ²
Tape Store	Inergen, Zenith Electro
Cable Store	N/A
Steamer Winch Room	Streamers covered by fixed water fog system.
Helicopter Deck	AFFF 3%. Two Unitor FJM 80 foam monitors
Paint Store	Fixed water fog system.
Chemical Store	N/A
Main Foam Pump, AFFF Foam Mixture	7.5 M ³ /h, 11 Bar, Grundfoss CR8-100/9. 3% mix.
Main Fire Pump	1xAllweiler NB 40-200/01/194, 50 M ³ /h at 7 Bar.
Water Spray Pumps For Streamers	1x Allweiler NAM 80-250/01/208, 170M ³ /h at 8 Bar
Emergency Fire Pump	2 x Allweiler NAM 125-315/01/326, 240M ³ /h at 5 Bar
Fire Detection Monitoring System	1xAllweiler NB 40-200/01/189, 40 M ³ /h at 7 Bar.
	1 x SERVOTEKNIK BMS-904

Hull Outfitting

Anchor	Maker: ABB Zamech Ltd. Type: SPEC 4320 1 x 4340 Kgs + 1 x 4320 Kgs
Windlass	1 x Ulstein Brattvaag BFM 22U.050, low pressure hydraulic (40 Bar)
Mooring Winches	N/A
Capstan No 1	2 x ODIM Type: 3M3117/OCF801 (Gun deck)
Capstan No 2	N/A
Decks Crane 1, Capacity/Reach/Location	1 x Norlift GPFO 250 0814, D-deck Ps, frame 36. Max. lift 8 tons
Decks Crane 2, Capacity/Reach/Location	1 x Norlift GPFO 250 0814, D-deck Stbd, frame 36. Max. lift 8 tons
Decks Crane 3, Capacity/Reach/Location	HYDRALIFT 1, KMCV 1400-6T (10M) RB600.
Decks Crane 4, Capacity/Reach/Location	N/A
Anti Rolling Damping System	Ulstein Passive Stabilisation System Tk.No.8 Roll Reduction Frd 398 M ³ Tk.No.37 Roll Reduction Aft 312 M ³
Heeling Tanks, Volume And Fuel/Fw/Sw	N/A
BUNKER CONNECTIONS, Locations	1 x forecastledeck centre, frame 117, 2 x main deck Stbd. and port side, frame 57.
BUNKER CONNECTIONS, Type(S)	1 x 4" pipes w. standard flanges on forecastle deck, 2 x 7" with std. flange on main deck. One fitted with 3" camlock female.
BUNKER HOSE Length And Dimension (Loose)	N/A
Crew Accommodation, No Of Bunks	64 bunks
Single Berths Cabins	21
Double Berths Cabins	20
Client Cabins, Single Berths	3
Buisness Conference And Training Rm	A -deck
Sauna And Fitness Room	A-deck

Section 1: General Information

International Oil Pollution Prevention (IOPP) Equipment

Incinerator, Sludge And Waste Oil	Teamtec-Golar, OGS400C, 65 ltr IMO sludge/h. Max 400 ltrs solid waste / charge.
Bilge / Oily Water Separator	World Water Systems, 2500 OCD, 2.5 M³/h, through 15 ppm unit.
Oily Water / Sludge Holding Tanks Cap.	Bilge W.tank:14 M³. Sludge/waste tk's.: 22 M³
Sewage Disposal Plant	Hamworthy Super Trident, ST6A. Macerate, biological plant w. chem. Dosage facility. Max. flow 15 M³/24 Hrs. BOD5 6 Kg's/ 24 Hrs.
Oil Spill Absorbent / Damage Control	1 x Set Oil Spill Kit inc. sorbent booms/pads, granules & dispersant.

Machinery Equipment

Air Source, Hp Compressors	3 x LMF 57/138 - 207 - E60, 1 x LMF off-line compressor, V17/5518-E60, 75 cfm.
Air Capacity, Each And Total (Cfm)	3 x 2000 cfm, total 6000 cfm
Hp Compressor Drive Motors	3 x ABB motors, AMA450 L6L BAFMH, 1 MW, voltage / freq. Controlled.
Main Engine Or Electric Prop. Motors	2 x Bergen Diesel BRM9, 5400 BHP each (3975 Kw Ea)
Auxiliary Engines (Generator Drive)	2 x Caterpillar 3516 STD, 1.4 MW each. 440 V, 60 Hz
Redundancy Propulsion, Az-Thruster	N/A
Vessels Total Brake Hp / Kw For Prop.	10800 BHP, 7900 KW.
Main Engines, Power Supply	N/A
Propeller Type, Main Propulsion	2 x 4 blade CPP in nozzle, diam. 4.2 mtr, 125 rpm
PROPELLER And THRUSTER CONTROL	Ulstein-Liaaen electro / hydraulic control.
Propeller Blade, Spare	N/A
Generators / Alternators	2 x A.van Kaick shaft gen's, DSG 114 M1-6W, 440V, 60 Hz, 3000 KVA each
El. Power, Useful, Out From M.S.Board	> 7000 KW
Ups Power To Instrument Room	1 x Siemens UPS Masterguard S5280, 73 KVA, 15 min. battery back-up.
Power Supply Instr.Room Back -Up	1 x Siemens UPS Masterguard S5280, 73 KVA, 15 min. battery back-up.
Emergency & Harbour Gen. Engine	1 x Caterpillar 3406 DITA, 345 KW
Emergency & Harbour Generator	1 x Caterpillar SR4-3450, 315 KW, 440V, 60 Hz
Fuel Back-Up System For Aux. Eng.	N/A
Cooling System For Aux. Engines	Independent FW cooling. 2 x Sondex FW / SW coolers
Bow Thruster	Ulstein-Liaaen 800 TV, 1.1 MW, 440V, 60 Hz.
Stern Thruster	N/A
Fresh Water Generator (Fwg)	2 x Alfa Laval De-Salt. 12 T/24hrs each
Boiler, Exhaust Gas & Oil Fired	1 x Pyro E 1130, 406 KW
Steering Gear	2 x Ulstein Tenfjord, type SR662

Seismic Specifications

Main Particulars

Streamers	12
Tow Points	16
Sub Arrays	8

Energy Systems

Gun Controller (Type & Manufacturer)	Source Synchronizer System (SSS), Input/Output
Guns (Manufacturer, Type & Capacities)	Input/Output, Sleeve-gun, type I, 40 cu. in. and type IIB, 55 cu. in. to 150 cu. in.
Nominal Source Pressure	2000 psi
Pressure Release	Electro-magnetic solenoid, inertial poppet and seat
Sensor Return	Inductive coil
Timing Resolution	0.1ms
Source	1 x 750 cu. in. compact sleeve gun source per sub-array, 4 sub-arrays per source (3000 cu.in. each) using dual source configuration
Total Compressor Capacity	6600 SCFM
Compressors (Manufacturer & Capacity)	3 x LMF Compressors
Near Field Phone (Manufacturer & Type)	Input/Output 2933008 or AG Geophysical 800-05
Far Field Phone (Manufacturer & Type)	NA
Depth Indicators	AG Geophysical model AG 3303, 3 per sub-array

Streamer Systems

Streamer (Manufacturer & Type)	Thompson Marconi, Sentry Solid Streamer
Streamer Deflector Type	Monowing MKI and MKII
Section Breaking Strength (Typical)	60 kN
Typical Towed-streamer Stress	1000-1818 kg
Streamer Capacity (Max)	
Sentry Solid Streamer	72,000m
Streamers vs. Length (Max)	
Sentry Solid Streamer	12 x 6,000m
Streamer Spread (Max spread Configuration)	1100m using Monowing (Presently capable of 900M)
Streamer Control Device (Manufacturer & Type)	DigiCourse, 5011
Recording System (Manufacturer & Type)	Input/Output MSX 24A

Section 1: General Information

Navigation Systems

Instrument Room Gyrocompass (Manufacturer & Type)	Sperry, MK227
Source Positioning System (Manufacturer & Type)	WesternGeco, Posnet
Global Positioning System (GPS) Receivers (Manufacturer & Type)	1 x Fugro Starfix-Plus, dual frequency 2 x Trimble MS750, dual frequency 2 x Trimble 4000SSE, dual frequency 2 x C-Nav World DGPS.
DGPS QC System (Manufacturer & Type)	TRINAV 2.6
Integrated Navigation System (Manufacturer & Type)	TRINAV 2.6
3-D Quality Control System (Manufacturer & Type)	TRINAV 2.6
3-D Binning System	TRINAV 2.6
Tail Buoy (TB)	
Buoy (Manufacturer & Type)	T98
TB Navigation (Manufacturer & Type)	WesternGeco, Posnet Tailbuoy GPS Unit
Onboard TB Positioning (Manufacturer & Type)	WesternGeco, Posnet
Ultra-short Baseline (USBL) Acoustic Positioning System (Manufacturer & Type)	NA
Acoustic Positioning System (Manufacturer & Type)	Digicourse, System 3
Current Profiler (Manufacturer, Type & Frequency)	RDI, ADCP, 600kHz
Temperature/Salinity Dip Profiler (Manufacturer & Type)	1 x Sippican, Sippican 1 x Valeport, Mk600
Echo Sounder (Manufacturer & Type)	Simrad, EA500
Transducer Frequency & Theoretical Range	1 x 18 kHz to 8100m 1 x 200 kHz to 740m
Transducer Draft	-7.42m

Recording System

Format	4-byte SEG-D, demultiplexed data
Media	IBM 3590 tape
Device	EMASS Robotic tape library with 4 x 3590 IBM tape drives

Other Systems

Other Systems	MSX version 2.1 + PDL CRS Continuous Recording System. Allows acquisition to continue to record data if tape drive(s) fail.
Single & Multi-trace Plotter (Manufacturer & Type)	OYO, GS624

Section 1: General Information

Onboard Seismic Qc

System	SeisView
Software	Omega
Hardware	1 x IBM p Series 640 Model B80 with 4 x processors 8 Gb Ram 54 Gb hard drive

Onboard Seismic Processing

System	Omega
Software	Omega
Hardware	32 x IBM SP-2 UNIX based super computer nodes 2 x IBM p Series 640 Model B80 servers w/ 5.2 Tbyte hard disk space 22 x 3590 IBM tape drives 5.2 Tbyte total hard disk space EMASS Robotic tape library with 26 x 3590 IBM tape drives OYO GS-636 Thermal Plotter

Note: Additional system, equipment, hardware and, software information may be available. Please refer to the appropriate specification sheets and/or manuals for more information.

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6. List of Key Personnel

6.1. Onboard Personnel

POSITION	CREW 1	CREW 2
Party Manager	Michael Martin	Ian Halfpenny
Captain	Rudy Bless	Rudy Bless
Chief Engineer	Kevin Joseph	Gordon Saunders
Chief Officer	Brett Mcphee	Luc Defossez
Acq. Supervisor	Donny Isdaryanto	Victor Lopes
Acq. Shiftleader	Stewart Klincke Essau Leija	J.Q. Chandler Richard Morgan
Pos. Supervisor	Stephen Kilmurray	Paul Melody
Pos. Shiftleader	Joel Pederick	Paul Farrell Mike Gors
Handling Supervisor	Armin Roehl	Paul May
Shiftleader Mechanic	Aldrin Flores Munisvaran Krishan	Colin Robson Paul Hollingsworth
Trilogy QC Leader		
Field Geophysicist	Petr Gorbachev	Jon De Haai

6.2. Office Support Personnel

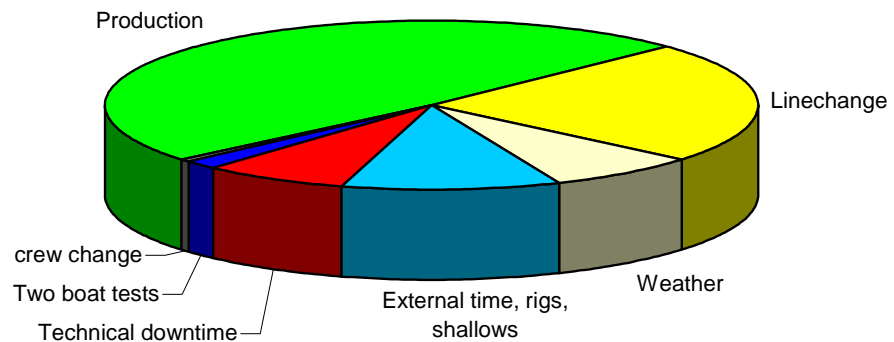
POSITION	NAME	OFFICE
Vessel Manager	Kiran Tuite	Kuala Lumpur
Maritime Superint.	John Hattendorf	Kuala Lumpur
Instrument Support	InTouch Global Operations Support.	Oslo
Navigation Support	InTouch Global Operations Support, Kumara Krishnasamy	Oslo Kuala Lumpur
Mechanical Support	InTouch Global operations Support Darren Parish / Simon Flack	Oslo Kuala Lumpur
Trilogy QC Support	Tee Chee Cherng	Oslo
OBP Supervisor		

7. Field Information and Observations

7.1. Production Statistics

PRODUCTION (Km)		
Prime Traverse Production	3027.56275 Km	
Infill Traverse Production	192.80625 Km	(6.4 %)
Total Traverse	3220.36900 Km	
Prime CMP Production	44055.26250 Km	
Infill Production	2892.90000 Km	
Total CMP Production	46948.16250 Km	

TIME DISTRIBUTION (Hours)		
Production	368.6700 Hours	(48.9 %)
Linechange	176.3200 Hours	(23.4 %)
Weather	55.9830 Hours	(7.4 %)
External time, rigs, shallows	80.5830 Hours	(10.7 %)
Technical downtime	54.6000 Hours	(7.2 %)
Two boat tests	12.1000 Hours	(1.6 %)
crew change	5.2000 Hours	(0.7 %)
Total Survey time	753.4560 Hours	(100 %)



7.2 Daily Summary

Party Managers log in local time UTC + 11

SUE Survey

16th January 2005

Extra floatation was added to the inner streamer lead-ins #4 & #5 in preparation for shallow water operations. The source was deployed and production started on the SUE survey at 05:33 hrs. At the request of Apache the MSX was changed to 5sec records and the run-in to lines has been reduced to 4.8 km. Strong winds and currents have been slowing down the vessel's shooting speed. The wind and sea picked up from the SW during the second sequence and by the end of the line the streamer RMS was >40 m/bar, compass data was also noisy. During the turn to the next line depth control of streamers #6 & #8 was lost and they surfaced. This resulted in tailbuoys crossing, but once the turn was completed we regained control of the streamers and the tailbuoys returned to the correct positions. A noise test taken on the run-in showed the ambient noise to be too high for production to continue. The Trident is continuing the shooting racetrack monitoring the feather and waiting for the weather to improve. The diving operations at Barracouta have not interfered with production and the bridge are following the EAPL procedures contacting the platform and LPCR on entering and leaving restricted zones. V-Sat communications were finally restored today at 11:00 hrs, the Indian Ocean satellite has failed and we have been re routed to the Pacific Ocean satellite.

17th January 2005

The wind and sea conditions improved overnight allowing production to restart at 04:11 hrs. Production was continuous for the rest of the day apart for an extended line change to perform gun maintenance and repair the starboard head float. The planned helicopter operation was delayed for 2 hours to allow the Trident time to clear the Barracouta platform. The helicopter landed at 11:15 hrs and picked up 4 off signers who were taken into Essendon.

18th January 2005

The Trident continued with racetrack production gradually closing in on the Dolphine and Perch platforms. Line changes at the eastern end of the prospect had to be extended to safely transit around the Barracouta platform. The first close pass to the Dolphine platform was successfully completed at 20:00 hrs CPA was tailbuoy #8 at 470m. There were diving operations at Barracouta today but no lines were aborted, good communications with the platform ensured that we did not enter the 8km zone when divers were in the water. Sea conditions were suitable for small boat work and both boats were launched to change the last section on streamer #7 and change acoustic pods on tailbuoys #7, #5, & #2. The CMV ferried the new section out to the workboat then performed a TS-dip and bird changes. The work boat checked the depths of the front end lead-ins, the deepest reading was 16m.

19th January 2005

Good weather conditions continued today. Production was uninterrupted, strong currents of up to 1.4 knots slowed the vessel bottom speed in the afternoon causing an extended line change between sequence 9 & 10. The Barracouta will continue with diving operations for the next two to three weeks, no time delays were incurred today as a result of the diving. A close pass to the Dolphine platform was successfully completed in the morning the closest point of approach was tailbuoy #8 at 391m.

20th January 2005

The wind and sea picked up in the morning then dropped off again in the evening. Production continued all day without interruption, two close passes were performed on the Dolphine platform. The platform is now boxed in with coverage on both sides. The Trident will continue in its present swath racetrack moving the coverage in towards the Perch platform. Diving operations were again in progress on the Barracouta but were timed such that they didn't interfere with our program.

21st January 2005

The sea conditions deteriorated in the morning as the wind strengthened and swung around to the SW. The forecast is for an improvement overnight, the planned supply boat operation was cancel due to unsuitable sea conditions. The final close pass to the Dolphine platform was completed, the next close pass to this platform will be during the undershoot operation. Diving operations on Barracouta are still in progress; good communications with the dive supervisor ensure that both operations can proceed simultaneously.

22nd January 2005

The weather improved enough to launch the CMV in the morning to change two birds on streamer #7 and add some ballast weights to the front of streamer #6. The CMV also transferred passengers from the Lady Roula to the Trident and from the Trident to the Omnes Pioneer. The first 14 km of sequence 19 were scratched due to problems with the MSX recording system and the source separations. During this period the port main engine was also shut down following a spurious alarm from a faulty jacket water temperature sensor. The 225 degree direction swath was swapped to the eastern side of the block so all the central swath lines can be shot in the 45 degree direction into the Barracouta platform. Nominal line change time now increased to 2:15 hours due to survey shape.

23rd January 2005

The Omnes Pioneer left the survey area at 06:00 hrs bound for Melbourne to crew change and pick up supplies and bunkers for the Trident. Whilst she is away we will not be able to perform any close passes to the Perch platform. The CMV was deployed in the morning to change birds on streamers #7 & 8. Adjustments to the ballast of streamer #8 at the front and tail were also performed. A RACU failure in the line change after sequence 23 meant the planned line GAP04B1984 was aborted and the Trident continued heading west to pick up line GAP04B2080.

24th January 2005

Wind and sea conditions picked up slightly but not enough to interfere with production. Completed the last run to the south of the Perch platform 500m zone, to move any close we'll need the Omnes Pioneer to be in attendance. After acquiring line GAP042000 production will switch to the northern block away from the platforms until the Omnes Pioneer returns from Melbourne.

25th January 2005

Continuous production throughout the day. The Trident changed over to the northern swath in the morning to avoid close passes to the Perch platform. The cable-laying vessel Julio Verne is approximately 3.8nm off the end of line GAP04B1136 moving slowly away from the prospect on a heading of 225 degrees. She is not interfering with our turns and is expected to complete her work in the area within the next week. The Omnes Pioneer has been delayed in Melbourne pending an inspection by the Victoria work safe authority and the AIMPE.

26th January 2005

Problems with the MSX during sequence 33 caused two reshoot holes. The MSX locks up for no apparent reason. The MSX memory boards were reseated in the line change after seq 33 in an attempt to isolated the fault. The Julio Verne will remain in the area or another 6 days, line changes today were not effected by the cable laying operation. The Omnes Pioneer is expected to sail from Melbourne Thursday evening and be back on prospect Saturday morning.

27th January 2005

Crew change was completed today by three helicopter flights out of West Sale. Due to the helicopters operators limits on roll and pitch and the prevailing swell conditions Trident was unable to complete the turn onto line after sequence 36 with the first helicopter on deck. After monitoring vessel movement on line direction Trident had to turn to head with seas on the quarter to ensure safe operations. 5.2hrs was therefore logged as crew change time.

The Omnes Pioneer is expected to be back on prospect tomorrow morning. The Julio Verne undertaking cable laying operation is still in position the west of the prospect.

28th January 2005

Production continued in the northern swath C before switching back to swath A in the evening to continue boxing in the Perch platform. A close pass was completed on sequence 41 with Tailbuoy 1 passing 228m off.

False man over board alarms left two holes in production today, one on sequence 38 and one on sequence 39 when the guns automatically shut down on line. The first alarm occurred at 02:13. All crew were contacted and accounted for. On the line change after sequence 39 the fault was traced to a loose connection in the MOB controller patch panel in the gun shack. Total lost time and will depend on re-shoot time. Lines charged full but incomplete.

The Omnes Pioneer arrived back on prospect at 14:00 and was taken alongside at 14:36 whilst the vessel was on line 1440P1039. The fresh provisions were loaded and three reels of cables for repair discharged. She was let go EOL at 17:35. Although alongside for over 3hrs only 179m³ of bunkers was received. Whilst maneuvering alongside ship to ship contact was made between the fenders bending the gun deck door frame.

A planned small boat operation to ballast the head of streamer 2 had to be cancelled at the end of the day due to increased swell and heavy rain and lightning.

The Julio Verne undertaking cable laying operation is still in position the west of the prospect.

29th January 2005

Production continued in swath A, a close pass's of Perch platform on lines heading east.

No new coverage was achieved at the start of line 1744P1043 west of Perch. This was due to a combination of an engine problem on Omnes Pioneer and a northerly feather. After Omnes Pioneer reported problems with the starboard engine on the line change Trident steered north on the run-in to line to clear the platform outside 500m. Omnes Pioneer managed to complete repairs for the close pass to take place but no new coverage was achieved for the first 5km of the line, a northerly feather preventing any new coverage as Trident moved back on to line. Good coverage was archived north of Perch as Trident maneuvered around the platform with the outer stbd paravane passing 160m off.

Linechanges in the east had to be extended for the vessel to turn outside of Barracouta platform. They were longer in the west due to the stagger of the prospect. Shooting speed was reduced due to strong head 1.0kt head currents.

The work boat was deployed in the morning to attempt ballast work at the front of streamer 2. Due to increasing wind the operation was aborted and work boat returned onboard. The job was completed with a second launch late afternoon with streamer 2 bird 3 being replaced and a loose SRD being re-attached on streamer 7.

The Client crew change was completed by helicopter in the morning. Ian Milne and Patric Bonnevier joined.

Support vessel Lady Roula departed at 0530 to call into Lakes Entrance for crew change, supplies and was back on prospect at 23:00.

30th January 2005

Production continued in swath A. Two good close passes of Perch platform on lines heading east successfully acquired, no further coverage is possible without deadhead runs or undershooting.

Linechanges in the east had to be extended for the vessel to turn outside of Barracouta platform. Linechanges were longer in the west due to the stagger of the prospect.

The work boat was deployed in the morning to change bird 11 on streamer 7 which was running light. Sea conditions were too rough for section changing.

Section 2: Operation Summary

The Julio Verne was contacted and Trident was informed that they still have 5 days work outstanding. This will have an impact on completing the run out of line in the NW corner of the prospect.

31st January 2005

After completion of line 2048P1048 production switch back to the centre swathe C. The long linechange (change of swathes and prospect shape) was utilized to deploy the workboats to change section 23A streamer 7.

Strumming noise on streamer 3 increased to level, over 30uB, that action was deemed necessary. After completion of line sequence 49, guns were recovered and streamer 4 stacked to allow recovery of lead-in 3 to investigate. Fairing had been stripped from end of the lead-in and Cumberland grip damaged, probably by catching floating debris or fishing gear.

Whilst undertaking the work to repair the fairing the support paravanes will be adjusted to buoy up the front-ends in preparation for the shallow part of the survey. The support paravanes on lead-in's 3 and 6 will be changed to larger 5000ltr and the support chains shortened. The work boat was deployed prior to the work to check the depth of the lead-ins aft of the support paravanes, 10m was recorded.

The FRC was launched at the end of the day to assist in recovering a gun separation rope and collar which had been lost down lead-in 2 during mobilization. Also the front float T-piece inserted in streamer 3 for the failed front float was removed. The time taken for these tasks was logged as WesternGeco downtime.

In the evening OMS Pioneer spotted and recovered a drifting front buoy which was lost by Trident during mobilization.

OMS Pioneer departed the prospect to head for Port Welshpool to change out an engineer for compassionate leave and a change of Captains.

1st February 2005

Reconfiguration work in preparation for the shallows was completed with streamer 6 support paravane adjusted and all gear redeployed for production to resume at 07:12. (The last long prime line in the east). The first 1.3km of the line was lost due to an air leak. Two re-shoot lines were acquired in the centre swathe. Sea conditions deteriorated in the evening with a southwesterly wind gusting to 45kts. Streamer control was lost with streamers surfacing, streamer 6 remaining on the surface and crossing behind streamer 4. With a poor forecast the decision was taken to head Sw'ly down the coast and recover the guns for safety.

The forecast for the next three days is not too promising; a low-pressure system will develop to the northeast of Bass Strait early Wednesday before deepening and moving over eastern Bass Strait.

The plan to sound the lead-ins in the afternoon had to be canceled as a front crossed the Bass Strait and with wind increasing to 30kts.

OMS Pioneer departed for Port Welshpool 00:00, to change out an engineer for compassionate leave and to change out of Captains, and was back on location at 12:00

2nd February 2005

The weather eased in the morning allowing the vessel to turn back to the prospect, deploy guns and resume production at 12:43. Weather conditions deteriorated on line, wind SE force 7-8 rough seas. The line was completed but further production halted with the vessel continuing east along the coast to wait on weather.

An ENE wind increased to 45kts in the evening and seas 4-5m. Streamer control was lost with streamer 6 crossing streamers 7 and 8 and 2 and 3 surfacing and crossing streamer 1. With the waves forecast to be larger offshore Trident continued down the coast, rolling in a beam sea.

Section 2: Operation Summary

A gale warning is current, Southerly winds 30/40 knots tending northwest to northerly and moderating to 15/25 knots from the east overnight. Seas 4 to 6 metres abating to 2 to 3 metres. Southeasterly swell 2 to 3 metres.

Earlier in the day a yellow egg float was dragged up lead-in 6 by the gun separation rope. During an attempt to recovery the float it was lost from the back deck.

3rd February 2005

As an intense low pressure over the Bass Strait headed west the gale force wind switched to the NW and round to the NE. Streamer control continued to be unstable in seas 4 to 5m and streamers surfacing and crossing. Tailbuoy 8, entangled on tailbuoy 6 late yesterday, parted from the streamer, the two tailbuoys towed from streamer 6. Conditions eased slightly in the morning and cable control was regained allowing Trident to turn back towards the prospect at 05:50. The weather damage has reduced the tail-end positioning redundancy and cable 7 suffers from intermittent coil line leakage. As soon as sea conditions permit the work boats will need to be deployed to repair the damage.

Support paravanes were deployed from the back deck to buoy up lead-ins 4 and 5. In theory all gear should be buoyed up to 12m.

Production resumed at 19:56 on line GAP04B1200P1054, Lady Roula ahead monitoring depths. Wind NE 28Kts, wave height 2.0m.

An Operations and Safety committee meeting was held in the afternoon.

4th February 2005

Production continued in swathe C, heading closer in to the shallows, minimum water depth on line 1184P1056 20.9m.

Weather conditions improved during the afternoon allowing the work boat to be launched on the linechange. The crew first replaced bird 5 on streamer 6 and reattached bird 8 which had come adrift from the front collar. They then successfully untangled tailbuoy 8 from tailbuoy 6 and after replacing the swivel reattached the tailbuoy to streamer 8. The crew then returned to streamer 6 to replace the acoustic unit on tailbuoy 6.

After completing a TS Dip the work boat crew attempted to sound the lead-ins. Sea conditions were not ideal but the deepest point on lead-ins 2 and 3 was found at 8.5m. A possible depth of 15m was observed on lead-in 4 in front of the guns. The support paravane chain will be shortened and lead-in re-sounded in the morning if sea conditions permit,

5th February 2005

Production continued in swathe C, closing in on the coast.

The work boat was deployed on the morning linechange to change bird 4 on streamer 1 and sound the lead-ins. Deepest point was found forward of the gun arrays on lead-in 4 at 10.0m. The wind picked up in the morning to westerly 20kts preventing any further small boat activities.

Lady Roula has requested to call in to Port Welshpool on Monday for crew change.

Latest information is than source vessel Pacific Titon will be on location 12th February for undershoot of the Perch and Dolphin platforms.

6th February 2005

Production continued in swathe C, closing in on the coast. Weather conditions deteriorated late afternoon, west/southwesterly wind increasing to 30 knots and a short 1.5/2m sea building in the evening.

The wind is forecast to back northerly early morning and although 20 to 30 knots may allow production to continue with the short fetch off the coast.

Section 2: Operation Summary

Intermittent coil line leakage evident since the last bad weather period is causing occasional loss of compass and acoustic data on streamer 7.

A fire drill took place in the afternoon, the scenario a fire in the rope locker.

Support vessel OMS Pioneer remains in close attendance for the shallow lines.

Lady Roula will depart the prospect after midnight to head for Port Welshpool for crew change.

7th February 2005

Weather conditions continued to be very variable, light winds in the morning increasing to 25kts late afternoon. With NE'ly wind off the land and wave height of less than 1.5m production was able to continue off the coast but with caution.

A General Safety Meeting was held in the afternoon.

Swathe C border was closed with the acquisition of prime line 1312P1065 leaving no infill coverage outstanding.

Acquisition of the lines along the coast continued. A 14.1m pinnacle in the east prevents the vessel lining up for full coverage on lines north of 1104P1066 inclusive. The vessel successfully passed over 16.3m soundings. At the end of line 1104P1066 the vessel performed a teardrop turn to acquire inshore line 1056P1067. Full coverage could not be achieved at the SOL line due to water depths less than 16m on the run-in. 18m was observed for the first part of the line. A slight deviation of 50m offline was required to ensure the streamers remained outside the marine park. The vessel commenced turning 6km before end of line to ensure safe clearance and sea room from the 14.1m pinnacle. A tear drop turn was then required to turn back onto line 1088P1068 sliding in past the 14.1m point.

The first 11.9km at start of line 1104P1066 was scratched due to failure of an 8/10 pin jumper on array 5. The vessel continued on line whilst the array was recovered, launching the work boat to fault find the streamer 7 intermittent coil line leakage. Section 19A was identified and with good sea condition's the section was change was undertaken on line. With the gun array redeployed production continued with streamer 7 and 8 buried in the coverage and 12CMP recorded. After streamer 7 was repaired production continued with 14 CMP whilst the acoustic unit on tailbuoy 8, damaged in last weeks weather tangle was repaired.

The time for the section change on streamer 7 was accounted as downtime by a factor of 2/16 or 2/8 of the time the vessel was in production in 12 CMP mode. The reduction was subtracted from line change time.

The CMV was deployed to assist the workboat with the section change. The GPS unit was changed but the buoy remains down. An underwater camera inspection was attempted but the water visibility was too poor.

Lady Roula arrive back on prospect at 12:00. OMS Pioneer was on close standby whilst Trident was in water depths of 20m and less.

8th February 2005

Production along the coast continued with completion of the long lines. Teardrop turns were required at each end of the survey. Re-shoot Line 1104A1070 was acquired which include a segment of infill although full coverage could not be obtained at the start of line 1104 because of the 14.1m pinnacle on the run-in. Acquisition continued with the first short line 1040P1071 east of the marine park.

The work boat was deployed midday for bird maintenance.

9th February 2005

Section 2: Operation Summary

The last shallow line was successfully completed at 11:32. Trident then made a long transit around Barracouta to continue production acquiring a re-shoot and infill line 2064J1075 down the eastern edge on route to the short lines in the south.

Multiwave vessel "Pacific Titan" called to report her arrival on a block to the NE of Trident with an intended start time of 06:40GMT, 1740 local. Trident started line 2064J1075 at 16:32. Titan reported seismic interference to be too excessive to live with and time sharing will be required from the end of line 2064J1075 at 21:09.

The long transit was utilised for streamer maintenance, the work boat with the assistance of the CMV was deployed to change active 13A on streamer 4. The work then attempted to repair the acoustic unit on tailbuoy 7 without success.

10th February 2005

Production continued on the short lines in the south-east corner of the survey area. Close communication was maintained with Multiwave vessel "Pacific Titan" and vessels were able to shoot in each other's linechange with little delay to production. After reporting observing Trident at 160uB yesterday evening, today with the vessels at maximum distance apart, Titan reported no interference from Trident and no interference was observed on Trident.

Breezy weather conditions persisted today and there was no opportunity for small boat activity.

An LPT meeting was held in the afternoon.

11th February 2005

Production switched through out the day between the short-line in the south-east and small re-shoot lines in the centre swathes. Communication was maintained with Pacific Titan to avoid interference.

The shooting plan was changed to acquire an extra infill in the east requested by Apache and at the end of the day Trident was in transit around Barracouta to pick up the line.

The work boat was launched midday to change out 3 birds, plans to carry out maintenance on tail buoy 3 and change out tail buoy 5 had to be postponed due to the sea state.

Lady Roula departed the prospect at 01:40 to pick up two-boat engineer from Lakes Entrance. Chidi Offor was successfully transferred to Pacific Titan and Lady Roula was back on location at 15:30.

12th February 2005

Trident acquired full infill line GAP04B1984J1088 to head south. Weather conditions deteriorated but the two outstanding prime lines and an infill line were acquired to complete the short lines in the south-east. With the wind SW 25kts and seas 3.0m a larger turn circle radius was required and streamer control was poor on line with swell noise evident.

With completion of the short southeastern lines at 18:08 Trident turned to rendezvous with Pacific Titan whose ETA at Dolphin was 19:30. Configuration of two boat link commenced at 19:30 with Trident deploying guns.

A medivac drill was carried out in the morning with the maritime crew preparing the helideck.

A first aid training session was held by the medic in the afternoon on the subject of CPR.

13th February 2005

Weather, SW force 6 decreasing to light airs in the afternoon.

The two boat system configuration continued after midnight with a planned test line scheduled to start at 01:30 missed. Time was logged as technical downtime from 06:00, the start of the first scheduled undershoot pass. WesternGeco engineer Chidiebere Offor reported the problem was due to the failure of the truetype receiver installed as part of the (WesternGeco) two boat

Section 2: Operation Summary

equipment on Pacific Titan. The suggested solution was to transfer the salve truetype unit from Trident and to make a TTL from closure as replacement on Trident.

Weather conditions slowly improved in the morning and after Trident turned to create a lee the CMV was launched to transfer the receiver. A line attempt was made past the Dolphin platform in the afternoon with Trinav and spectra systems apparently configured and the line was steered well, but with no closure being received by the MSX no data could be recorded. Chidiebere Offor was transferred across to Trident late afternoon to continue to search for a solution and workaround for the failed true time receiver.

As the swell dropped and the workboat was launched on run-in to line in the afternoon to change out 4 birds.

14th February 2005

Good weather persisted, NE force 3 to light airs.

Tridents two-boat setup was reconfigured to adjust for transfer of the salve Truetype receiver to source vessel Pacific Titan. Initial tests and an attempt to reconfigure back to single vessel mode were complicated by a bad relay in the Spectra relay box. Two-boat production commenced at 11:02 with the first undershoot pass of the Dolphin platform. Production then continued in an anti-clockwise loop around Dolphin and Perch in turn. Turns had to be extended due to strong current up to 1.3kts.

The two-boat FTB is now being issued by a Trinav relay instead of TTL signal so there is a drift between the FTB on two boats. This drift is being logged to file and will be closely checked by QC of the data and will need to be applied in processing. Technical support was contacted for feedback on improvements to the set-up.

The work boat was deployed in the morning, the crew successfully replacing the acoustic coil on tailbuoy 3. The crew again launched in the afternoon line change and successfully replaced tailbuoy 5.

On the first boat launch the Chief Officer was transfer to support vessel Pioneer for an informal inspection and to explain Trident supply boat operations and check lists.

First aid training sessions held continued, today's session on the subject of hemorrhage management.

15th February 2005

Undershoot with Pacific Titan.

The weather deteriorated rapidly today, a strong wind warning was issued west-southwest winds increasing to 25/30 knots during the day and seas 2-3m.

Production continued in an anti-clockwise loop around Dolphin and Perch in turn. Turns had to be extended due to deteriorating weather and strong currents. Good coverage was obtained with close passage of Trident streamers.

Two vessel timing variation resulting from the use of the two Trinav relays in place of the truetype receiver continue to be monitored and recorded. Two boat data was FTP'd to Perth processing data for a review of the ddat quality.

A SIPP's refresher training session was held.

First aid training sessions continued, today's second session on the subject of hemorrhage management.

16th February 2005

Undershoot with Pacific Titan completed.

Section 2: Operation Summary

The weather remained poor today, a strong wind warning was issued west-southwest winds increasing to 25/35 knots during the day and seas 3-4m.

Good coverage was obtained on the final undershoot runs past Dolphin and Perch and the Client accepted the coverage as complete after sequence 98, end of line 08:55

A slight lull in weather and a good lee in the turn allowed the CMV to be launched to collect the failed true time receiver from PacificTitan. A extra undershoot run was made whilst attempts to utilise the truetype receiver as master on Trident were undertaken. The effort was unsuccessful and Pacific Titan was released at 15:00

The time from 08:55 to 15:00 was logged as WesternGeco Time.

Western Trident commenced the Transit to Oscar prospect at 15:00 speed reduced due to the weather, wind southwest 35kts, Sea SW 3-4m.

Efforts continue both on board and ashore to ensure the timing drift in the Undershoot data can be corrected. At a meeting in Perth data processing provided Apache with a before and after display of a single trace gather with the timing shifts removed using a method based on the positioning data and picking of direct arrivals. The LMO corrected data looks promising.

First aid training session on burns was held in the afternoon.

END of Job 9438, Vessel on Transit to next survey.

Field Information and Encountered Problems

7.2.1 Obstructions / Installations on the Field

The survey area approached within 4.2 km of the coastline and came within 0.3 km of Ninety Mile Beach Marine National Park. Seismic acquisition could not be undertaken within the Marine Park boundary, it was treated as an obstruction and the vessel and trailing gear did not traverse the Marine Park. The Marine part restricted the run-in onto the three northern most lines.

Cable ship Guilio Verne, on site to repair the Bass link submarine cable, was a restriction on the run out of lines in the north-west of the survey area at the start of the survey. However her departure was well timed prior to Trident commencing work on the shallow lines and no time was lost.

A detailed bathymetric survey using Laser Airborne Depth Survey (LADS) was completed prior to the seismic survey to fully define the 20 m depth contour. This identified pinnacles with water depths less than 18m in the survey area. To acquire the coastal lines Western Tridents 8 streamer spread was buoyed up to a minimum depth above 12m. Following a hazard analysis (HARC) by the crew the risk was deemed acceptable to take the vessel into a minimum water depth of 18m and traverse over pinnacles with a minimum depth 16m with the vessel on a straight course. This meant a small s of coverage on the north-western boundary could not be acquired due Pinnacles of 15.0m and an area in the extreme north east of the prospect could not be acquired due to the vessel having to turn to clear a pinnacle of 14.1m to the east of lines 1120 and 1104.

There were two fixed obstructions in the survey area, monopods Dolphin and Perch. The Barracouta platform was situated 8km to the east of the prospect area restricting the vessel turning manoeuvres. The survey shooting plan and swathe design was therefore designed to ensure a full run out toward Barracouta but extra line change time was required, logged as "external downtime obstructions", to enable the vessel to turn around the outside of the platform. Diving Operations were in progress on Barracouta and the procedures for "DIVERS in the WATER", drawn up with agreement between Apache and Esso/BHPB were closely followed. Good communication between the vessel and Diving Supervisor resulted in no lost time due to diving operations. WesternGeco and Esso Australia Close Pass Procedure's were closely adhered to and good communication established with the Northern Fields Platforms and Longford Control Room.

At the end of the survey the monopods Dolphin and Perch were undershot with the assistance of Multiwave vessel "Pacific Titan". The undershoot was completed with the minimum eight runs, as Titan towed a single source this consisted of four runs followed by four interleave lines.

7.2.2 Traffic / Shipping Lanes

There were no major shipping lanes through the survey. Occasional fishing vessels and pleasure craft were observed on route to and from the port of Lakes entrance. Support vessels supplying the Northern Field rigs were very co-operative and no conflicts were reported. The bridge was able to contact vessels using channel 16 and ask them to avoid the Western Trident and its towed equipment. The ASI (Automatic Ship Identification system) is now a great help in determining the name and call sign of vessels approaching with-in VHF range.

7.2.3 Fishing Activity

Occasionally fishing vessels from Lakes Entrance passed through the survey area but stayed well clear of the Trident and its towed equipment. Prior to the start of the survey a lot of time had been

invested informing the local fishing fleet of the Western Trident's planned activities. This has clearly paid dividends with no lost time recorded for fishing activities during the survey.

7.2.4 Seismic Interference and Time Share

Multiwave vessel "Pacific Titan" arrived on the 9th February to carry out a small 2D survey on the coast to the northeast of SUE. Trident completed the coastal lines on the same day and was able to transit to continue acquisition on the short lines in the south-east corner of the survey area. Close communication was maintained with Multiwave vessel "Pacific Titan" and vessels were able to shoot in each other's line change with no delay to production. No interference was observed on Trident.

7.2.5 Environmental Obstacles

The climate of the Gippsland Basin can be described as moist cool temperatures having warm summers, with a regular winter-spring rainfall. The region is located on the northern edge of the westerly wind belt known as the roaring forties. Winds often freshen to gale force from the north and north-west, ahead of approaching fronts during all seasons. Once the fronts have passed they then swing abruptly southwest behind the front at similar speeds and abate until they again freshen ahead of the next front. Additionally, low pressure systems can generate wind systems known as the "East Coast Lows", which consist of strong south easterly winds.

An unusual low pressure system which tracked west across Bass Strait on the 2nd and 3rd February resulted in 42hrs of weather downtime.

Regionally, Bass Strait has a unique geometry consisting of a broad shallow region, which descends abruptly to very deep water on each side. The Gippsland Basin is the broad shallow region on the eastern side of Bass Strait. The flux of water through the strait and its variations are key components of many physical and biological processes in the region. The currents within the Gippsland Basin region include components due to tides and wind stress. As a function of this in the open waters, tides generally result in an elliptical movement of the water mass. The East Australian current brings warmer waters into Bass Strait and influences water temperatures. Sea surface temperatures for Bass Strait range from 16 to 18oC in February and 12 to 14oC in August. Wave energy is relatively low, particularly in the broader shelf area in the Gippsland Basin. However, stalled low-pressure systems in the Tasman Sea during the summer can generate higher wave energy at this time. Intermittent upwelling occur along parts of the east Gippsland coast.

Infill was low, 6.4% as the current was parallel to the coast and mainly in line direction resulting in low feather. The strong current often over 1.0kt did reduce the vessels average ground speed.

The water depth range for the survey varied from 18m, with pinnacles below 15m on the coast to 40m in the south.

7.2.6 Operational Observations

The combination of 8m streamer depths and the use of solid streamers allowed production to continue in some very marginal sea conditions. The proximity of the prospect to the coast and the short fetch allowed production to continue with near gale force winds from the NW to the NE. The limiting factor regarding production was not the streamer noise but streamer control and the ability to process the navigation data, as high swell conditions produce noisy compass and acoustic data.

At the end of the survey the monopods Dolphin and Perch were undershot with the assistance of Multiwave vessel "Pacific Titan". Operationally the undershoot was completed efficiently with the minimum eight runs, with Titan towing a single source this consisted of four runs followed by four interleave lines.

Section 2: Operation Summary

The undershoot start was delayed by the failure of WesternGeco's source vessel Truetime receiver that meant that the crew had to strip Trident of one of its units to transfer to Titan and use two TRINAV relays in its place on Trident. The relays introduced erratic timing differences that will be adjusted in processing with static correction files created to adjust the data from a recorded FTB QC file.

Chase boat Performance:

The crew of the supply support vessel "OMS Pioneer" and the fishing support vessel "Lady Roula" performed up to expectations.

Lady Roula's presence ensured good co-operation with the local fishing communities and was also used for personal transfer to Lakes Entrance (tidal dependant) and Welshpool. However due to the variable weather in this area it should be stressed that personnel transfers cannot always be guaranteed and should be restricted to a minimum on future surveys.

During the survey one supply operation with OMS Pioneer was undertaken on line. On approach the port shoulder of the supply vessel Pacific Pioneer made direct contact with Western Trident between the two rigged Yokahama fenders and the framing of the gun deck the door was slightly bent inboard. The incident was reported RIR 20050129002200. A third Yokahama fender will be rigged at the gun deck door to avoid re-occurrence of the incident. This incident is a reminder that future surveys in this area should be planned with a minimum of supply boat operations.

8 HSE Summary

The survey was conducted in a safe and efficient manor with no lost time injuries taking place and no personal injuries.

The crew were encouraged to report all incidents and RIR's, Risk Identification Reports, were reported in QUEST. An action item (or items) was submitted for each report and reviewed before the report could be closed.

Tables below list the following;
RIR's, STOP-cards.
HSE-meetings
Audits & Inspections.

RIR	Description	Date	Category
20050217043035	Bagle virus found on computer	Feb 14, 2005	Near Accident
20050217000759	Found door for Odin control cabinet open.	Feb 16, 2005	Hazardous Sit.
20050216173022	Power lead not put away	Feb 16, 2005	Hazardous Sit.
20050215062959	Potential slip hazard in cabins.	Feb 15, 2005	Hazardous Sit.
20050214073534	Emergency Exit Deficiency	Feb 14, 2005	Hazardous Sit.
20050214052616	Broken tie rod on LMF compressor	Feb 14, 2005	Hazardous Sit.
20050214031914	Fire hazard	Feb 14, 2005	Hazardous Sit.
20050214022428	Obstructed Access to header tanks	Feb 13, 2005	Hazardous Sit.
20050214001148	Bad soldering stand	Feb 14, 2005	Hazardous Sit.
20050213235351	Defective pressureswitch for air vent. system.	Feb 13, 2005	Hazardous Sit.
20050213092710	Tape library door left open.	Feb 10, 2005	Hazardous Sit.
20050213060630	person wearing wrong flotation device	Feb 13, 2005	Hazardous Sit.
20050213041042	Air hose hazard.	Feb 12, 2005	Hazardous Sit.
20050213035842	doorstep loose	Feb 13, 2005	Hazardous Sit.
20050213035152	Lack of PPE in ER	Feb 12, 2005	Hazardous Sit.
20050212231931	Defective battery charger for stb. lifeboat.	Feb 12, 2005	Hazardous Sit.
20050212220943	Houskeeping in Small boat Recesses	Feb 11, 2005	Hazardous Sit.
20050212220258	Unsecured items in the Gym	Feb 03, 2005	Hazardous Sit.
20050212215821	Power tool switch	Feb 08, 2005	Hazardous Sit.
20050212215146	Food provision transfer	Feb 01, 2005	Hazardous Sit.
20050212002930	Norpower Workboat: Found navigation lights broken.	Feb 12, 2005	Hazardous Sit.
20050211165517	Swinging door.	Feb 12, 2005	Hazardous Sit.
20050211002601	Bilge pumps in CMV did not operate.	Feb 10, 2005	Hazardous Sit.
20050210182540	Not Using Safety Equipment While working	Feb 09, 2005	Hazardous Sit.
20050210150404	Seized wheels on fire extinguisher's trolley	Feb 10, 2005	Hazardous Sit.
20050210051221	Observation of tool use, spanners on array.	Feb 10, 2005	Hazardous Sit.
20050209110818	Lost balance on the work boat.	Feb 09, 2005	Near Accident
20050209042943	Skinned knuckles.	Feb 02, 2005	Hazardous Sit.
20050208235724	exhaust fan in store not covered	Feb 09, 2005	Hazardous Sit.
20050208222215	Slip Hazard - Heli-deck	Feb 09, 2005	Hazardous Sit.
20050208194610	Wood Pallet blocking walkway	Feb 09, 2005	Hazardous Sit.
20050208145909	Potential slip hazard	Feb 08, 2005	Hazardous Sit.
20050208000546	Person working in Safety zone without correct PPE	Feb 07, 2005	Hazardous Sit.
20050208000026	Scales in Heli Reception left Unsecured	Feb 07, 2005	Hazardous Sit.
20050207235446	Small oil spill on D Deck under Scrap metal bin	Feb 05, 2005	Hazardous Sit.
20050207234823	Short Preventer(Safety Line) FRC	Feb 04, 2005	Hazardous Sit.

Section 2: Operation Summary

20050207234244	Fire Extinguisher not in place	Feb 01, 2005	Hazardous Sit.
20050207180126	Person positioned himself between cable and reel	Feb 07, 2005	Hazardous Sit.
20050207104653	Doing inappropriate exercise in the gym.	Feb 07, 2005	Hazardous Sit.
20050207053140	Typhoon suit had damage collar neck	Feb 07, 2005	Hazardous Sit.
20050207014456	Lost SRD on tail end of Streamer 6.	Feb 07, 2005	Accident/Failure
20050207012550	Survival suits dripping water around ship	Feb 07, 2005	Hazardous Sit.
20050206160904	Slip hazard	Feb 06, 2005	Hazardous Sit.
20050206140842	Tools left over after work	Feb 05, 2005	Hazardous Sit.
20050206135903	Railing bent near the cable reel	Feb 03, 2005	Hazardous Sit.
20050206135727	Working aloof with no safety harness.	Feb 06, 2005	Hazardous Sit.
20050203160301	GO. Contract worker cleaned up duty mess	Feb 03, 2005	Hazardous Sit.
20050203071050	Moving empty wood reels on deck.	Jan 28, 2005	Hazardous Sit.
20050203065531	No hard hat working near crane block.	Jan 28, 2005	Hazardous Sit.
20050203042858	Helicopter parked too close to personnel baggage	Feb 03, 2005	Hazardous Sit.
20050203041451	Lead-in 7 was rubbing against radar reflector	Feb 03, 2005	Hazardous Sit.
20050203033904	Tail buoy 8 parted and caught on Tail buoy 6.	Feb 03, 2005	Accident/Failure
20050202140638	Lithium Batteries not properly stored.	Jan 30, 2005	Hazardous Sit.
20050202062905	SRD hanging on the cable	Jan 31, 2005	Hazardous Sit.
20050202060754	Workboat chains do not indicate when twisted.	Feb 02, 2005	Hazardous Sit.
20050202040500	Small hatch for cable section left open	Feb 02, 2005	Hazardous Sit.
20050201002751	Lithium battery protection kit not in place	Feb 01, 2005	Hazardous Sit.
20050131130907	laptop and other goods stolen	Jan 27, 2005	Accident/Failure
20050131031435	STOP coffee spill on stairs	Jan 31, 2005	Hazardous Sit.
20050130220115	Loudspeaker on CMV radio not functional	Jan 30, 2005	Hazardous Sit.
20050129002200	Contact with supply vessel (steel to steel)	Jan 28, 2005	Accident/Failure
20050128063637	Lost production due to False man over board alarms	Jan 28, 2005	Accident/Failure
20050125114958	Hydraulic oil leak from cable deck	Jan 24, 2005	Hazardous Sit.
20050124225512	Virus scan definition files not up to date	Jan 25, 2005	Hazardous Sit.
20050124061244	Contents of First Aid Kit Fast Rescue boat	Jan 22, 2005	Hazardous Sit.
20050123102507	VHF radios not put away after use	Jan 23, 2005	Hazardous Sit.
20050123060919	Defective pressure gauge.	Jan 23, 2005	Hazardous Sit.
20050123055422	Faulty pressure gauge.	Jan 23, 2005	Hazardous Sit.
20050123003409	Cup & rubbish on streamer deck.	Jan 23, 2005	Hazardous Sit.
20050120223542	Sludge pump failure.	Jan 20, 2005	Hazardous Sit.
20050119201358	Acoustic unit lost	Jan 20, 2005	Accident/Failure
20050119053701	Broken dipstick.	Jan 19, 2005	Hazardous Sit.
20050118100253	Broken posnet mast	Jan 18, 2005	Hazardous Sit.
20050118054709	Valve spindle damaged.	Jan 18, 2005	Hazardous Sit.
20050118052408	Failed HP fuel pipe on Stbd Eng	Jan 18, 2005	Hazardous Sit.
20050118022207	Broken regulating valve spring.	Jan 18, 2005	Hazardous Sit.
20050118021700	High exh gas deviation	Jan 17, 2005	Hazardous Sit.
20050117003130	Grounding of enclosures	Jan 17, 2005	Hazardous Sit.
20050116201103	Swelling of Right Knee & Lower Leg / Ankle	Jan 16, 2005	Accident/Failure

Section 2: Operation Summary

HSE Meetings

Meeting	Description	Date
20050123173744	LPT	Jan 24, 2005
20050130030157	Catering dept. weekly QHSE meeting w 4	Jan 30, 2005
20050203050941	Operations and Safety Committee Meeting	Feb 03, 2005
20050207231648	Weekly Deck Department Meeting Week 4	Feb 03, 2005
20050208022947	Catering dept weekly QHSE meeting 8 Feb 05	Feb 08, 2005
20050208075323	Engine Dept Safety Meeting	Feb 08, 2005
20050212060720	Safety and ISPS Basic Awareness Level 1	Feb 11, 2005
20050212074731	Seismic Chiefs Meeting 5th February	Feb 05, 2005
20050212074954	Seismic Chiefs Meeting 12th February	Feb 12, 2005
20050213050217	ISPS basic awareness Level 1	Feb 13, 2005
20050213072059	Acq. dept QHSE meeting	Feb 13, 2005

Audits Inspections.

Audit	Description	Date
20050122024850	Vessel feedback report Jan 05	Jan 22, 2005
20050126073819	Western Trident Monthly H&H Report January 2005	Jan 25, 2005
20050126205132	D Deck inspection	Jan 27, 2005
20050203074719	Australasian Jet Audit for WG Trident	Jan 26, 2005
20050212065436	Inspection of Western Tridents gym.	Feb 10, 2005
20050215061428	Internal Cross Audit, of Gun, Mono & Cable decks.	Feb 11, 2005

9 Shipment List

TDT-05018-AD-EXT	SEG D Original Tapes & P190 data	Seq 001-098
TDT-05017-AD-EXT	SEGD Field Tapes& client deliverables	Seq 001-098

10Logs

The final field and copy tape logs are written in PDL (Prospect Data Logger) format. The logs are copied as HTML files and copied onto CD. Copies of the PDL line logs were provided for Apache in the data shipments.

A scanned copy of the Production and Timing Summary is enclosed on the next page.

Section 2: Operation Summary



Vessel M/V Western Trident
Area GAP04B - SUE
Job no. 9429
Client Apache Energy
MMM-YY 17-Feb-05

TIMING & PRODUCTION SUMMARY

DATE	Accountable Time - Hours														Production - kms			
	Transit	WesternGeco Downtime	Undershoot Prod	Undershoot Line change	Undershoot Standby	Other chargeable standby	Production Prime	Prime runout	Linechange Prime	Production Infill	Infill runout	Linechange Infill	Total Day Rate	Total Time	Prime Traverse km	Infill Traverse km	Prime FF CMP km	Infill FF CMP Km
16-Jan						4.033	10.267	0.550	3.600				18.45	18.450	86.43750		1306.20000	
17-Jan		1.050				4.183	13.733	0.767	4.267				22.95	24.000	130.57500		1974.00000	
18-Jan						2.500	13.667	0.833	7.000				24.00	24.000	132.73130		2008.50000	
19-Jan						3.050	14.567	0.883	5.500				24.00	24.000	127.55630		1925.70000	
20-Jan						1.700	16.017	0.783	5.500				24.00	24.000	150.24380		2288.70000	
21-Jan						1.717	15.850	0.933	5.500				24.00	24.000	149.92500		2271.00000	
22-Jan		1.700				2.467	13.150	0.933	5.750				22.30	24.000	117.26250		1744.80000	
23-Jan		2.567				1.933	10.717	0.850	7.933				21.43	24.000	103.08750		1524.60000	
24-Jan						2.367	14.700	0.783	6.150				24.00	24.000	142.95000		2172.00000	
25-Jan						0.867	16.383	0.833	5.917				24.00	24.000	147.95630		2252.10000	
26-Jan		0.233					15.667	1.100	7.000				23.77	24.000	138.80630		2067.30000	
27-Jan		5.200				0.817	11.567	0.833	5.583				18.80	24.000	104.58750		1558.20000	
28-Jan						0.933	16.133	0.883	6.050				24.00	24.000	153.45000		2340.00000	
29-Jan						2.967	9.117	0.567	3.667	5.100	0.333	2.250	24.00	24.000	85.72500	42.52500	1294.80000	642.00000
30-Jan						1.917	9.217	0.750	6.334	4.583	0.267	0.933	24.00	24.000	92.51250	44.86875	1365.00000	679.50000
31-Jan						9.900	8.500	0.617	4.083			0.900	24.00	24.000	82.72500		1246.80000	
1-Feb		3.350				11.550	6.583	0.267	2.250				20.65	24.000	54.99375		841.50000	
2-Feb						17.067	4.783	0.317	1.833				24.00	24.000	40.50000		609.60000	
3-Feb						19.933	4.067						24.00	24.000	35.19375		563.10000	
4-Feb						2.250	13.900	1.083	6.767				24.00	24.000	124.55625		1839.30000	
5-Feb						2.400	14.767	0.767	6.067				24.00	24.000	142.89375		2171.10000	
6-Feb						1.100	14.517	1.050	7.333				24.00	24.000	143.11875		2136.30000	
7-Feb		1.867				3.633	13.150	0.533	4.817				22.13	24.000	122.64375		1791.56250	
8-Feb						4.400	10.750	0.317	5.500	1.200		1.833	24.00	24.000	90.13125	9.93750	1403.70000	159.00000
9-Feb		2.783				7.600	3.683		3.667	4.183	0.250	1.833	21.22	24.000	33.41250	40.53750	534.60000	610.20000
10-Feb						4.567	6.283	1.650	11.500				24.00	24.000	68.73750		869.40000	
11-Feb		11.833				2.767	2.317	0.583	6.500				12.17	24.000	24.91875		321.90000	
12-Feb		0.183				8.617	1.067	0.300	2.250	6.367	0.717	4.500	23.82	24.000	11.45625	54.93750	144.90000	802.20000
13-Feb		18.000			6.000								6.00	24.000				
14-Feb		11.033	5.700	4.500	2.767								12.97	24.000	52.12500		397.80000	
15-Feb			10.283	9.000	4.717								24.00	24.000	93.61875		748.95000	
16-Feb	9.000	6.100	4.800	2.250	1.850								17.90	24.000	42.73125		341.85000	
17-Feb	12.650												12.65	12.650				
Month	21.650	65.900	20.783	15.750	15.333	127.233	305.117	19.766	148.317	21.433	1.567	12.249	709.20	775.10	3027.56275	192.80625	44055.26250	2892.90000
Prev Month																		
Job Total	21.650	65.900	20.783	15.750	15.333	127.233	305.117	19.766	148.317	21.433	1.567	12.249	709.20	775.10	3027.56275	192.80625	44055.26250	2892.90000

Total linechange 176.32
Total Production 368.67
Total Standby 142.57
Total 687.55

Total Traverse 3220.36900

Ian Milne
Client Representative, Apache / Bass Strait Oil

Mike Martin
Party Manager, Western Trident

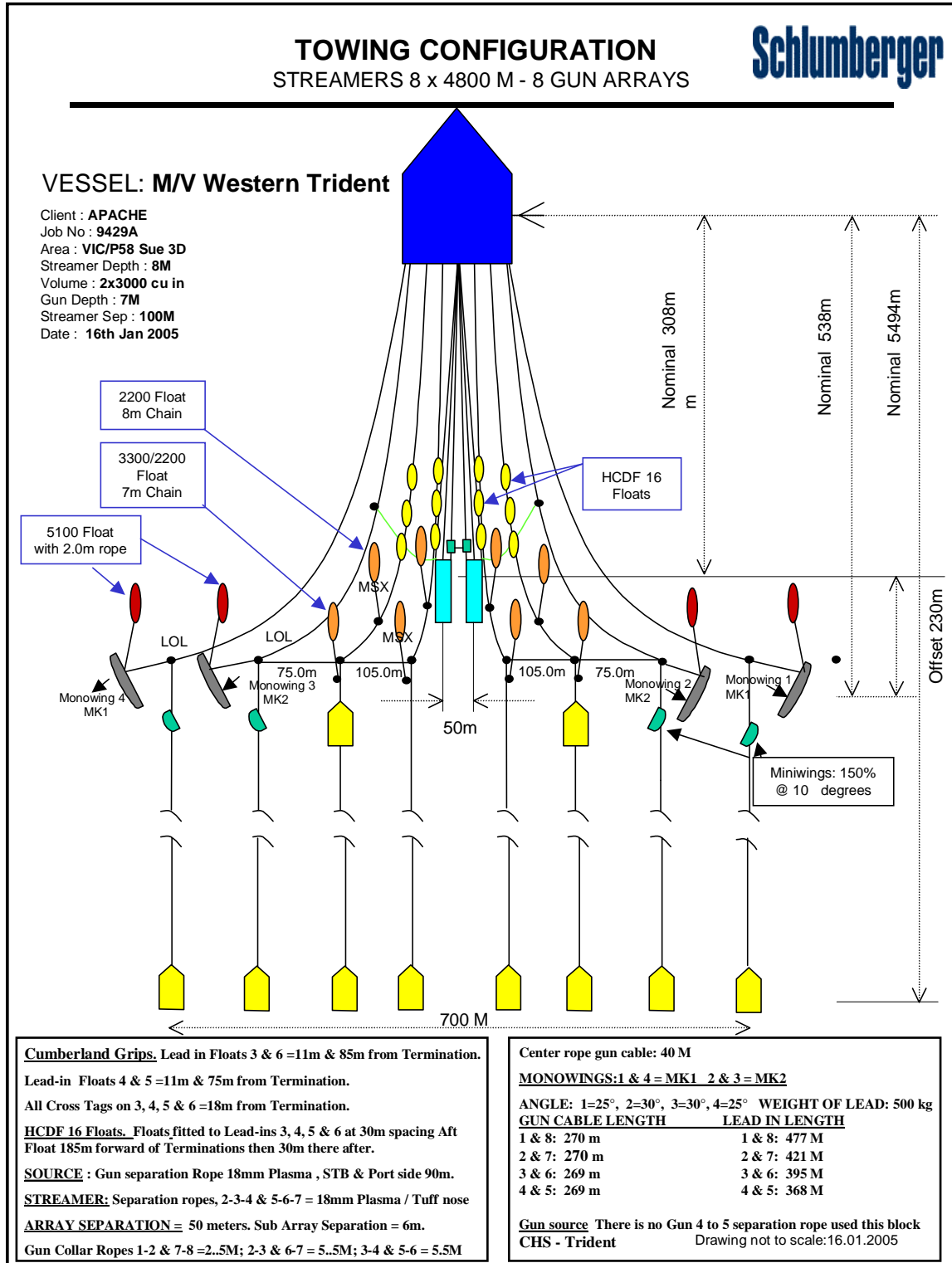
Note: Differences in time logged on the 8th and 9th due to Apache request to split line changes after sequence 70 and 75 . A total 3.6hours day rate time in dispute

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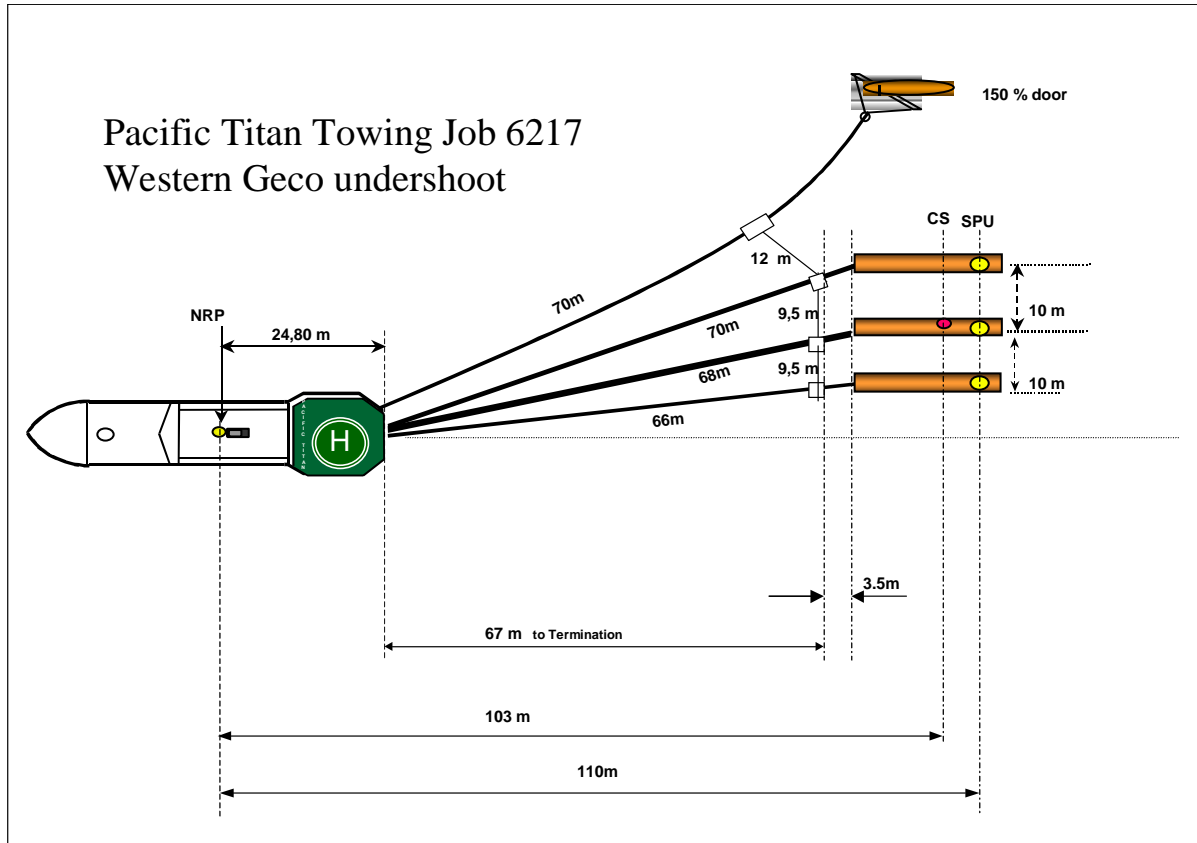
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11. Towing Configuration

11.1. Towing System Layout



11.2. Towing Layout of Source Vessel during Undershoot



12. Streamer Configuration

12.1. Streamer System Description

Streamer System Parameters	
Number of Streamers	8
Type of streamer	Thompson Marconi Sentry Solid, and Guardian Solid
Streamer length	4800
Groups per streamer	384
Group intervals	12.5 m
Outside diameter	64mm
Jacket (type-thickness)	Polyurethane, 3.5 mm
Breaking strength	60kN
Ballast fluid (fluid-quantity)	None
Modules (diameter-length)	Max. Dia 25cm, length 40cm
Channels per module	16
Data transmission link	Fibre Optic
Power	220 – 240 V AC
Active group lengths	17.75 m
Nearest offset available	180 m
Streamer depth	8 m
Streamer separation	100 m
Number of stretch sections	
in front of each streamer	0
end of each streamer	0
No of compasses per streamer	19
No of depth transducers per streamer	19

Section 3: Equipment Configuration

Trace allocation (example for 6 streamers)	Location	Near	Far
Streamer 1	Starboard Outer	1	384
Streamer 2	Starboard Middle Outer	385	768
Streamer 3	Starboard Middle Inner	769	1152
Streamer 4	Starboard Inner	1153	1536
Streamer 5	Port Inner	1537	1920
Streamer 6	Port Middle Inner	1921	2304
Streamer 7	Port Middle Outer	2305	2688
Streamer 8	Port Outer	2689	3072

Hydrophone Parameters	
Detector type	TMS Bender Hydrophone
Group interval	12.5m
Detectors per group	14
Group length	17.75 m
No of groups per section	8
Hydrophones spacing	Centre Weighted
Maximum operating depth	85 Metre
Group sensitivity	13.8 V/bar

12.2. Streamer Layout

STREAMER 1

CABLE 1
REEL 1

Loc	Serial #	Module	Bird	Acoustic	SRD	CHANNEL	Remarks		
LOL	003								
MWA		HSX- 80015							
Dum	6171	CRX00120	AB01-9430						
1A	6080	MSX- 62735		AA01-9430	SRD-	1 8			
1B	6078	CSX-70232	AB02 -9385			9 16			
2A	6025	MSX-60350		AA02-7927	SRD-	17 24			
2B	6036	CSX-71741	AB03 -19554			25 32			
3A	6037	MSX-62512		AA03-8486	SRD-	33 40			
3B	6201	CSX-73184	AB04 -19668			41 48			
4A	6195	MSX-60556			SRD-	49 56			
4B	6167	CSX-73091	AB05-21714			57 64			
5A	6199	MSX-60067			SRD-	65 72			
5B	6197	CSX-73084				73 80			
6A	6028	MSX-60423	AB06- 20375			81 88			
6B	6017	CSX-70831			SRD-	89 96			
7A	6217	MSX-60327				97 104			
7B	6218	CSX-70513	AB07-15550			105 112			
8A	6239	MSX-61844			SRD-	113 120			
8B	6264	CSX-71641				121 128			
9A	6255	MSX-60659	AB08-10464			129 136			
9B	6256	CSX-70594			SRD-	137 144			
10A	6259	MSX-60674				145 152			
10B	6287	CSX-70728*	AB09-12810			153 160			
11A	4122	MSX-60180			SRD-	161 168			
11B	4220	CRX0012		AA04-9048		169 176			
12A	4278	MSX-61362	AB10-7851			177 184			
12B	3379	CSX-70079		AA05-8814	SRD-	185 192			
13A	2720	MSX-60205				193 200			
13B	3861	CSX-71938	AB11-20916			201 208			
14A	3855	MSX- 61870			SRD-	209 216			
14B	3396	CSX-71735				217 224			
15A	3809	MSX -61858	AB12-17165			225 232			
15B	3331	CSX -72091			SRD-	233 240			
16A	3149	MSX -60075				241 248			
16B	2593	CSX -72233	AB13-27737			249 256			
17A	2764	MSX - 60700			SRD-	257 264			
17B	2664	CSX - 70123	26833	SPEED LOG		265 272			
18A	4007	MSX-61718	AB14-20941			273 280			
18B	2369	CSX-70598			SRD-	281 288			
19A	4062	MSX-60678				289 296			
19B	2184	CSX-70553	AB15-18386			297 304			
20A	4184	MSX-60218			SRD-	305 312			
20B	2365	CSX- 70056				313 320			
21A	4256	MSX-60693	AB16-13415			321 328			
21B	3450	CSX-70385			SRD-	329 336			
22A	3826	MSX-62488				337 344			
22B	3872	CSX-70539	AB17-7851			345 352			
23A	2709	MSX-60187			SRD-	353 360			
23B	2277	CSX-70084	AB18-19330			361 368			
24A	4134	MSX-60325		AA06-8987	SRD-	369 376			
24B	3997	CSX -72240	AB19-12203			377 384			
Dum	2446	TSX-90150		AA07-7119	SRD-				
TA	0895-015760-002								
STIC	0897-095470-03								

Section 3: Equipment Configuration

STREAMER 2

**CABLE 2
REEL 2**

LOL	Serial #	Module	Bird	Acoustic	SRD	CHANNEL	Remarks		
LOL	003								
MWA		HSX-80168							
Dum	6173	CRX-001	BB01 -9211						
1A	6203	MSX-60795		BA01-7260	SRD-	1 8			
1B	6187	CSX-71202	BB02 -20036			9 16			
2A	6190	MSX-61953		BA02-9142	SRD-	17 24			
2B	6200	CSX-70279	BB03-19864			25 32			
3A	6204	MSX-61416		BA03-8999	SRD-	33 40			
3B	6208	CSX-71871	BB04-16590			41 48			
4A	6198	MSX-61913			SRD-	49 56			
4B	6206	CSX-70211	BB05-13956			57 64			
5A	6207	MSX-62309			SRD-	65 72			
5B	6205	CSX-70113				73 80			
6A	6164	MSX-60311	BB06-11297			81 88			
6B	6062	CSX-70140			SRD-	89 96			
7A	6291	MSX-?????				97 104			
7B	6290	*CSX-70099	BB07-19702			105 112			
8A	4375	MSX-66267			SRD-	113 120			
8B	4483	CSX-71753				121 128			
9A	2393	MSX-60773	BB08-20323			129 136			
9B	2694	CSX-71670			SRD-	137 144			
10A	4458	MSX-61957				145 152			
10B	2028	CSX-70306	BB09-20235			153 160			
11A	3276	MSX- 61414			SRD-	161 168			
11B	4331	CSX-71264		BA04-8810		169 176			
12A	4421	MSX-60698	BB10-19838			177 184			
12B	4417	CSX-71693		BA05-7322	SRD-	185 192			
13A	4142	MSX-60337				193 200			
13B	2532	CSX-70183	BB11-19658			201 208			
14A	3391	MSX-60729			SRD-	209 216			
14B	3648	CSX- 70067				217 224			
15A	2550	MSX -62006	BB12-17361			225 232			
15B	4363	CSX -71629			SRD-	233 240			
16A	2606	MSX -61950				241 248			
16B	2668	CSX -71102	BB13-10823			249 256			
17A	3258	MSX-61209			SRD-	257 264			
17B	2538	CSX-71426				265 272			
18A	1980	MSX-60378	BB14-16646			273 280			
18B	4248	CSX-71978			SRD-	281 288			
19A	3038	MSX-60375				289 296			
19B	4189	CSX-71374	BB15-17528			297 304			
20A	3834	MSX-62021			SRD-	305 312			
20B	4410	CSX-71308				313 320			
21A	3475	MSX-60451	BB16-8905			321 328			
21B	2813	CSX-71986			SRD-	329 336			
22A	4047	MSX-60103				337 344			
22B	3959	CSX-70579	BB17-12791			345 352			
23A	3489	MSX-61834			SRD-	353 360			
23B	2528	CSX-70283	BB18-19759			361 368			
24A	2121	MSX-63133		BA06-8327	SRD-	369 376			
24B	6019	CSX-70284	BB19-27729			377 384			
Dum	3451	TSX- 90154		BA07-8339	SRD-				
TA	1097100780-02								
STIC	0104143815-01								

Section 3: Equipment Configuration

STREAMER 3

CABLE 3 Reel 3

Loc	Serial #	Module	Bird	Acoustic	SRD	CHANNEL		Remarks	
LI	3								
		HSX-80038 out-in 80019	Tension cell 17000006						
	mini-section	103003	T-Module	006					
Dum	6172	CSX-70050	CB01-10691						
1A	6339	MSX-61379		CA01-8330	SRD-	1	8		
1B	6329	CSX-72520	CB02-10082			9	16		
2A	6337	MSX-60101		CA02-9965	SRD-	17	24		
2B	6333	CSX-70566	CB03 -14196			25	32		
3A	6338	MSX-60155		CA03-8602	SRD-	33	40		
3B	6332	CSX-70146	CB04-13629			41	48		
4A	6325	MSX-62524			SRD-	49	56		
4B	6327	CSX-70730	CB05 -25704			57	64		
5A	6335	MSX-60369			SRD-	65	72		
5B	6348	CSX-70589				73	80		
6A	6237	MSX-60675	CB06-17368			81	88		
6B	6232	CSX-71704			SRD-	89	96		
7A	4366	MSX-62403				97	104		
7B	3126	CSX-70387	CB07 -15203			105	112		
8A	4245	MSX-62273			SRD-	113	120		
8B	4216	CSX-70073				121	128		
9A	4232	MSX-62011	CB08 -14602			129	136		
9B	4233	CSX-70196			SRD-	137	144		
10A	3355	MSX-60619				145	152		
10B	2572	CRX-00019	CB09-29100			153	160		
11A	2567	MSX-60607			SRD-	161	168		
11B	2608	CSX-70536		BA04-9409		169	176		
12A	4198	MSX-63717	CB10-10841			177	184		
12B	4273	CSX-72216		BA05-8607	SRD-	185	192		
13A	1942	MSX-60650				193	200		
13B	2757	CSX-71199	CB11-27769			201	208		
14A	4201	MSX-60755			SRD-	209	216		
14B	4475	CSX-70609				217	224		
15A	3478	MSX-60429	CB12-13773			225	232		
15B	4246	CSX-73856			SRD-	233	240		
16A	3407	MSX-60280				241	248		
16B	4508	CSX-70188	CB13-10497			249	256		
17A	3004	MSX-60111			SRD-	257	264		
17B	3924	CSX-70256				265	272		
18A	2690	MSX- 62726	CB14-17094			273	280		
18B	3784	CSX-71156			SRD-	281	288		
19A	3328	MSX-61865				289	296		
19B	3063	CSX-70089	CB15-27834			297	304		
20A	3708	MSX-61483			SRD-	305	312		
20B	2307	CSX-71990				313	320		
21A	4137	MSX-61747	CB16-10104			321	328		
21B	4252	CSX-73885			SRD-	329	336		
22A	2748	MSX-61387				337	344		
22B	4073	CSX-70362	CB17-15575			345	352		
23A	3330	MSX-60061			SRD-	353	360		
23B	6016	CSX-70732	CB18-19775			361	368		
24A	3647	MSX-61801		BA06-8338	SRD-	369	376		
24B	3657	CSX-72014	CB19-19943			377	384		
Dum	4435	TSX-90013		BA07-9461	SRD-				
TA	0497-094120-001								

STIC xxx

0598138970-4

Section 3: Equipment Configuration

STREAMER 4

CABLE 4 Reel 5

Loc	Serial #	Module	Bird	Acoustic	SRD	CHANNEL		Remarks		
LI	003									
		HSX-80018								
Dum	6135	CSX- 70072	DB01-20476							
1A	6042	MSX-60346		DA01-9499	SRD-	1	8			
1B	6030	CSX-70066	DB02-13172			9	16			
2A	6041	MSX-61902		DA02-9962	SRD-	17	24			
2B	6043	CSX-70548	DB03-17016			25	32			
3A	6038	MSX-60316		DA03-8376	SRD-	33	40			
3B	6058	CSX-70152	DB04-15396			41	48			
4A	6063	MSX-60229			SRD-	49	56			
4B	6084	CSX-70297	DB05-19492			57	64			
5A	6083	MSX- 61827			SRD-	65	72			
5B	6081	CSX-70503				73	80			
6A	6057	MSX-61954	DB06-19005			81	88			
6B	6054	CSX-71708*			SRD-	89	96			
7A	4213	MSX-60225				97	104			
7B	3998	CSX-70027	DB07-15747			105	112			
8A	4251	MSX-60126			SRD-	113	120			
8B	4250	CSX-71685				121	128			
9A	4249	MSX-61391	DB08-14103			129	136			
9B	4413	CSX-72005			SRD-	137	144			
10A	2665	MSX-60136				145	152			
10B	2966	CRX-00005	DB09-13380			153	160			
11A	3152	MSX-61417			SRD-	161	168			
11B	4085	CSX-71991		DA04-8342		169	176			
12A	4017	MSX-62347	DB10-8248			177	184			
12B	3939	CSX- ??		DA05-9437	SRD-	185	192			
13A	1665	MSX-62014				193	200			
13B	2522	CSX-72007	DB11-15668			201	208			
14A	2685	MSX-60863			SRD-	209	216			
14B	1714	CSX-72307				217	224			
15A	2674	MSX-62342	DB12-5624			225	232			
15B	4289	CSX-72229			SRD-	233	240			
16A	3843	MSX-63218				241	248			
16B	4362	CSX-73190	DB13-17803			249	256			
17A	6034	MSX-62721			SRD-	257	264			
17B	4023	CSX-71691				265	272			
18A	4469	MSX-60665	DB14-15422			273	280			
18B	4247	CSX-70257			SRD-	281	288			
19A	4013	MSX-60269				289	296			
19B	1868	CSX-70277	DB15-20020			297	304			
20A	3314	MSX-62005			SRD-	305	312			
20B	1746	CSX-71699				313	320			
21A	2751	MSX-60567	DB16-19403			321	328			
21B	4005	CSX-70301			SRD-	329	336			
22A	3992	MSX-61836				337	344			
22B	2977	CXS-72115	DB17-6374			345	352			
23A	6020	MSX- 60380			SRD-	353	360			
23B	2467	CSX-70568	DB18-13743			361	368			
24A	3847	MSX-62535		DA06-8566	SRD-	369	376			
24B	6039	CSX- 71271	DB19-27459			377	384			
DUM	1655	TSX-90200		DA07-9422	SRD-					
TAD	0297079080-7									
STC	0898157060-5									

Section 3: Equipment Configuration

STREAMER 5

Cable 5 Reel-8									
Loc	Serial #	Module	Bird	Acoustic	SRD	CHANNEL		Remarks	
LI	3								
		HSX-80049							
Dum	6018	CSX-70324	EB01-16858						
1A	6052	MSX-60076		EA01-9426	SRD-	1	8		
1B	6059	CSX-70395	EB02- 15169			9	16		
2A	6060	MSX-60782		EA02-7203	SRD-	17	24		
2B	6069	CSX-70601	EB03-19827			25	32		
3A	6153	MSX-60416		EA03-8333	SRD-	33	40		
3B	6170	CSX-70733	EB04- 22118			41	48		
4A	6168	MSX-62479			SRD-	49	56		
4B	6161	CSX-70302	EB05-14600			57	64		
5A	6186	MSX-61990			SRD-	65	72		
5B	6192	CSX-70391				73	80		
6A	6185	MSX-61940	EB06-14581			81	88		
6B	6184	CSX-71617*			SRD-	89	96		
7A	2832	MSX-60640				97	104		
7B	2924	CSX-70888	EB07-27834			105	112		
8A	3114	MSX-61370			SRD-	113	120		
8B	2604	CSX-72165				121	128		
9A	3996	MSX-60617	EB08-10180			129	136		
9B	4284	CSX-71989			SRD-	137	144		
10A	3107	MSX- 60457				145	152		
10B	4434	CRX-00022	EB09-17919			153	160		
11A	2707	MSX-61872			SRD-	161	168		
11B	3248	CSX- 70511		EA04-7395		169	176		
12A	2745	MSX-62533	EB10-21709			177	184		
12B	2618	CSX-70632		EA05-9444	SRD-	185	192		
13A	3384	MSX-60318				193	200		
13B	3433	CSX-71511	EB11-15478			201	208		
14A	3222	MSX-60358			SRD-	209	216		
14B	1931	CSX-71309				217	224		
15A	2036	MSX-60419	EB12-7059			225	232		
15B	3833	CSX-70407			SRD-	233	240		
16A	2342	MSX-61832				241	248		
16B	2642	CSX-72220	EB13-17421			249	256		
17A	2747	MSX-60090			SRD-	257	264		
17B	2643	CSX-70739				265	272		
18A	4359	MSX-60299	EB14-8519			273	280		
18B	2721	CSX-73448			SRD-	281	288		
19A	4447	MSX-61480				289	296		
19B	2686	CSX-73113	EB15-20227			297	304		
20A	4532	MSX-60314			SRD-	305	312		
20B	3859	CSX-70213				313	320		
21A	4072	MSX-60251	EB16-20368			321	328		
21B	3953	CSX-72126			SRD-	329	336		
22A	2761	MSX-63719				337	344		
22B	2735	CSX-73863	EB17-19214			345	352		
23A	4031	MSX-60768			SRD-	353	360		
23B	3943	CSX-70895	EB18-22609			361	368		
24A	2654	MSX-62417		EA06-9344	SRD-	369	376		
24B	6022	CSX -71254	EB19-20561			377	384		
DUM	2598	TSX-90010		EA07-7617	SRD-				
TAD	0497083840-07								
STC	1298103528-8								

Section 3: Equipment Configuration

STREAMER 6

**CABLE 6
Reel 10**

Loc	Serial #	Module	Bird	Acoustic	SRD	CHANNEL	Remarks		
LI	3								
		HSX- 80202			103002				
dummy	6166	CSX-71997	FB01- 19887						
1A	6336	MSX-60252		FA01-9431	SRD-	1 8			
1B	6341	CSX-73353	FB02-16438			9 16			
2A	6334	MSX-61399		FA02-8527	SRD-	17 24			
2B	6340	CSX-70053	FB03 -20304			25 32			
3A	6347	MSX-61909		FA03-9956	SRD-	33 40			
3B	6370	CSX-70313	FB04 -18036			41 48			
4A	6357	MSX-60324			SRD-	49 56			
4B	6377	CSX-70535	FB05 -19228			57 64			
5A	6378	MSX-61365			SRD-	65 72			
5B	6355	CSX-70538				73 80			
6A	6056	MSX-60361	FB06 -20330			81 88			
6B	6066	CSX-71668*			SRD-	89 96			
7A	2661	MSX-60109				97 104			
7B	3842	CSX-73197	FB07-6458			105 112			
8A	3390	MSX-60201			SRD-	113 120			
8B	2864	CSX-72317				121 128			
9A	2981	MSX-61413	FB08 -19911			129 136			
9B	4043	CSX-72172			SRD-	137 144			
10A	2673	MSX-62495				145 152			
10B	4030	CRX-00016	FB09-13989			153 160			
11A	3865	MSX-60220			SRD-	161 168			
11B	3904	CSX-71726		FA04-8990		169 176			
12A	3468	MSX-61284	FB10-19963			177 184			
12B	4285	CSX-71318		FA05-7290	SRD-	185 192			
13A	3976	MSX-60343				193 200			
13B	2693	CSX-73186	FB11-6911			201 208			
14A	3699	MSX-60110			SRD-	209 216			
14B	2789	CSX-72343				217 224			
15A	2816	MSX-60115	FB12-13988			225 232			
15B	3483	CSX-71196			SRD-	233 240			
16A	6029	MSX-60104				241 248			
16B	2568	CSX-72157	FB13-13786			249 256			
17A	3692	MSX-62346			SRD-	257 264			
17B	4143	CSX-70537				265 272			
18A	2619	MSX-60192	FB14-14008			273 280			
18B	3825	CSX-70010			SRD-	281 288			
19A	2657	MSX-60290				289 296			
19B	2724	CSX-70534	FB15-15501			297 304			
20A	2872	MSX-61831			SRD-	305 312			
20B	2637	CSX-72015				313 320			
21A	2611	MSX- 62453	FB16-7904			321 328			
21B	3254	CSX-71719			SRD-	329 336			
22A	2725	MSX-61378				337 344			
22B	3517	CSX-71201	FB17-8882			345 352			
23A	6011	MSX-60740			SRD-	353 360			
23B	4075	CSX-71931	FB18-15407			361 368			
24A	4078	MSX-60174		FA06-8098	SRD-	369 376			
24B	4077	CSX-70361	FB19-8375			377 384			
DUM	1168	TSX-90152		FA07-8564	SRD-				
TAD	0898152570-05								
STC	0798148730-09								

Section 3: Equipment Configuration

STREAMER 7

CABLE 7 REEL 11									
Loc	Serial #	Module	Bird	Acoustic	SRD	CHANNEL		Remarks	
LI	3								
		HSX-80268							
Dum	6169	CRX-17	GB01-21475						
1A	6070	MSX-61754		GA01-7344	SRD-	1	8		
1B	6073	CSX-71182	GB02-16925			9	16		
2A	6154	MSX-60637		GA02-7393	SRD-	17	24		
2B	6152	CSX-73128	GB03-10250			25	32		
3A	6047	MSX-61851		GA03-8561	SRD-	33	40		
3B	6050	CSX-70934	GB04-26177			41	48		
4A	6086	MSX-61980			SRD-	49	56		
4B	6147	CSX-70562	GB05-18830			57	64		
5A	6145	MSX-63254			SRD-	65	72		
5B	6129	CSX-70575				73	80		
6A	6133	MSX-60273	GB06-6830			81	88		
6B	6146	CSX-71200*			SRD-	89	96		
7A	3263	MSX-62442				97	104		
7B	3801	CSX-73861	GB07-20938			105	112		
8A	2755	MSX-61894			SRD-	113	120		
8B	3832	CSX-71531				121	128		
9A	2601	MSX-61286	GB08-12750			129	136		
9B	4416	CSX-71311			SRD-	137	144		
10A	3486	MSX-61503				145	152		
10B	2722	CRX-00023	GB09-20273			153	160		
11A	3199	MSX-60707			SRD-	161	168		
11B	2786	CSX-71934		GA04-7344		169	176		
12A	4041	MSX-60170	GB10-16916			177	184		
12B	2333	CSX-71633		GA05-8905	SRD-	185	192		
13A	4387	MSX-62337				193	200		
13B	2213	CSX-72322	GB11- 9589			201	208		
14A	3569	MSX-61951			SRD-	209	216		
14B	2655	CSX-70253				217	224		
15A	2744	MSX-63190	GB12-19440			225	232		
15B	4066	CSX-70795			SRD-	233	240		
16A	2716	MSX-62022				241	248		
16B	4026	CSX-70592	GB13-27739			249	256		
17A	1741	MSX-60571,			SRD-	257	264		
17B	4453	CSX-70287				265	272		
18A	2359	MSX-60581	GB14-15592			273	280		
18B	2008	CSX-71872			SRD-	281	288		
19A	3480	MSX-62275				289	296		
19B	4307	CSX-71597	GB15-17784			297	304		
20A	3148	MSX-60389			SRD-	305	312		
20B	4361	CSX-71739				313	320		
21A	3117	MSX-60411	GB16-17162			321	328		
21B	4008	CSX-71210			SRD-	329	336		
22A	4006	MSX-62283				337	344		
22B	6013	CSX- 72112	GB17-21455			345	352		
23A	2905	MSX-61361			SRD-	353	360		
23B	4461	CSX-71626	GB18-6594			361	368		
24A	4356	MSX-61830		GA06-8326	SRD-	369	376		
24B	4478	CSX-71705	GB19-12259			377	384		
DUM	3687	TSX- 90159		GA07 9464	SRD-				
TAD	0698140840-4								
STC	0798148730-3								

Section 3: Equipment Configuration

STREAMER 8

**CABLE 8 Reel
12**

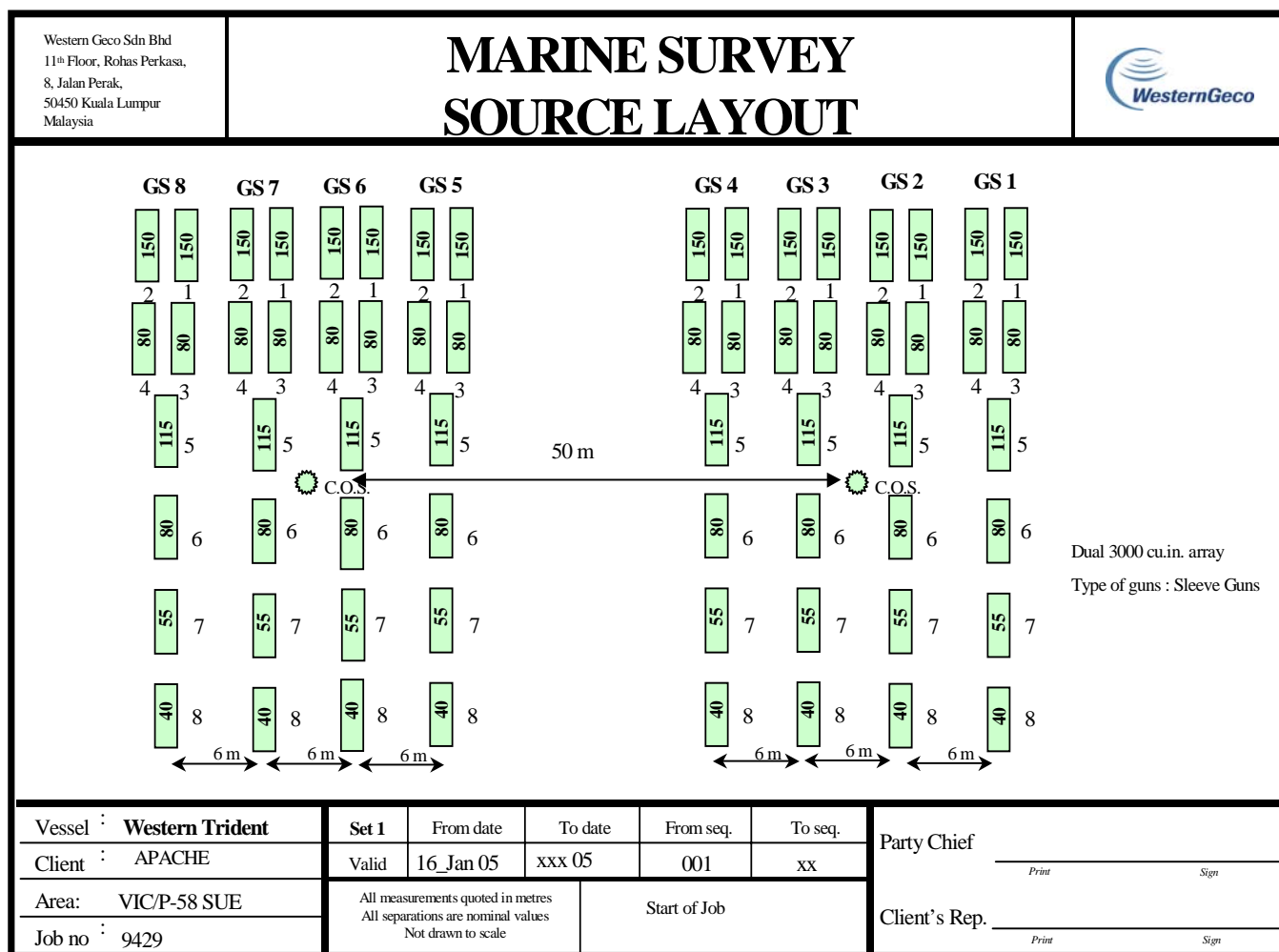
Loc	Serial #	Module	Bird	Acoustic	SRD	CHANNEL	Remarks		
LOL	003								
MWA									
		HSX-80202							
Dum	6027	CRX-	HB01-19965						
1A	6235	MSX-60653		HA01-8504	SRD-	1 8			
1B	6221	CSX-70316	HB02-18032			9 16			
2A	6227	MSX-61394		HA02-7306	SRD-	17 24			
2B	6213	CSX-71314	HB03-14138			25 32			
3A	6209	MSX-60191		HA03-9970	SRD-	33 40			
3B	6211	CSX-70329	HB04-17870			41 48			
4A	6033	MSX-61390			SRD-	49 56			
4B	6074	CSX-71596	HB05-5516			57 64			
5A	6040	MSX-60329			SRD-	65 72			
5B	6046	CSX-70400				73 80			
6A	6076	MSX-60484	HB06-11982			81 88			
6B	6053	CSX-70286			SRD-	89 96			
7A	6032	MSX-60449				97 104			
7B	6026	CSX-71233	HB07-20877			105 112			
8A	6031	MSX-60430			SRD-	113 120			
8B	6035	CSX-70244				121 128			
9A	6021	MSX-61855	HB08-21128			129 136			
9B	6065	*CSX-70521			SRD-	137 144			
10A	2825	MSX-60810				145 152			
10B	3502	CSX-70355	HB09- 20235			153 160			
11A	2545	MSX-62485			SRD-	161 168			
11B	1923	CSX-70184		HA04-8726		169 176			
12A	3218	MSX-62537	HB10-22006			177 184			
12B	3472	CSX-70080		HA05-9958	SRD-	185 192			
13A	4090	MSX-61868				193 200			
13B	2617	CRX-00018	HB11-17239			201 208			
14A	2503	MSX-62591			SRD-	209 216			
14B	2738	CSX-70160				217 224			
15A	2549	MSX-62036	HB12-20282			225 232			
15B	4183	CSX-70136			SRD-	233 240			
16A	3691	MSX-61774				241 248			
16B	3952	CSX-71590	HB13-17706			249 256			
17A	4208	MSX-61792			SRD-	257 264			
17B	3951	CSX-70243	25760	SPEED LOG		265 272			
18A	3950	MSX-60209	HB14-20882			273 280			
18B	3948	CSX-71606			SRD-	281 288			
19A	4403	MSX-61123				289 296			
19B	1367	CSX-71667	HB15-21180			297 304			
20A	4407	MSX-61759			SRD-	305 312			
20B	4304	CSX-70087				313 320			
21A	3973	MSX-62038	HB16-11930			321 328			
21B	4212	CSX-70057			SRD-	329 336			
22A	4211	MSX-63126				337 344			
22B	4382	CSX-73206	HB17-15501			345 352			
23A	4380	MSX- 61380			SRD-	353 360			
23B	4381	CSX-73866	HB18-19848			361 368			
24A	3358	MSX-60847		HA06-7329	SRD-	369 376			
24B	6023	CSX-73870	HB19-18861			377 384			
DUM	6067	TSX- 90078		HA07-8530	SRD-				
TAD	598-129990-02								
STC	1298-103092-04								

13. Source Configuration

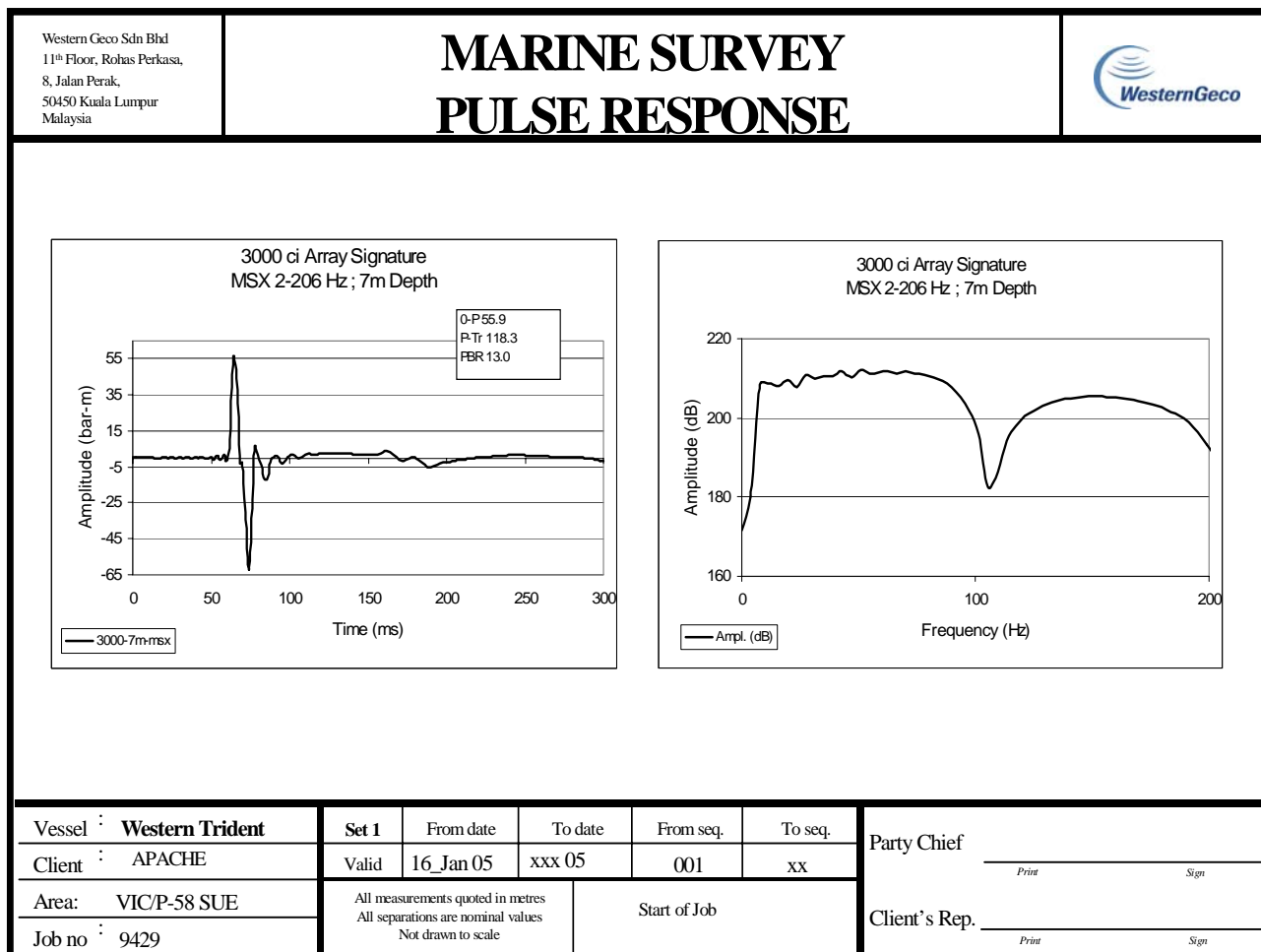
13.1. Source System Description

Source Parameters	
Number of source arrays	2 (Dual source) for Single boat 1 (single source) for Undershoot
Array separation	50 m
Array length	15.1 m
Array width	18 m
Number of strings/array	4
Separation from centre track	25 m
Source volume	3000 cubic inches (Single boat) 3040 cu.in (Under shoot)
Number of hydrophones per array	24
Number of depth transducers per array	12
Number of guns per array	32
Number of clusters per array	8
Airgun type	WesternGeco Sleevegun (single boat) Bolt for Source Vessel (Under shoot)
Operating pressure	2000 psi
Depth of guns	7 m
Peak to Peak amplitude	118.3 Bar-m
Primary to Bubble ratio	13.0

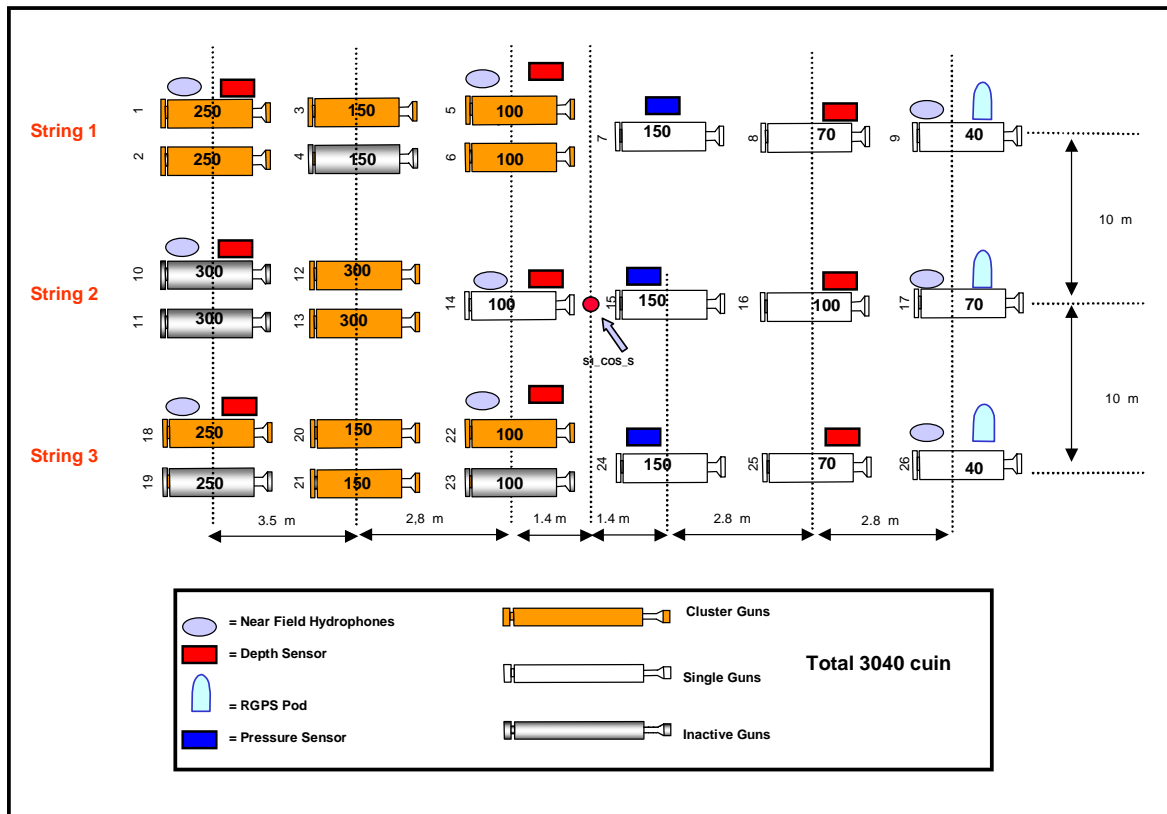
13.2. Source Layout





























13.3. Pulse Response



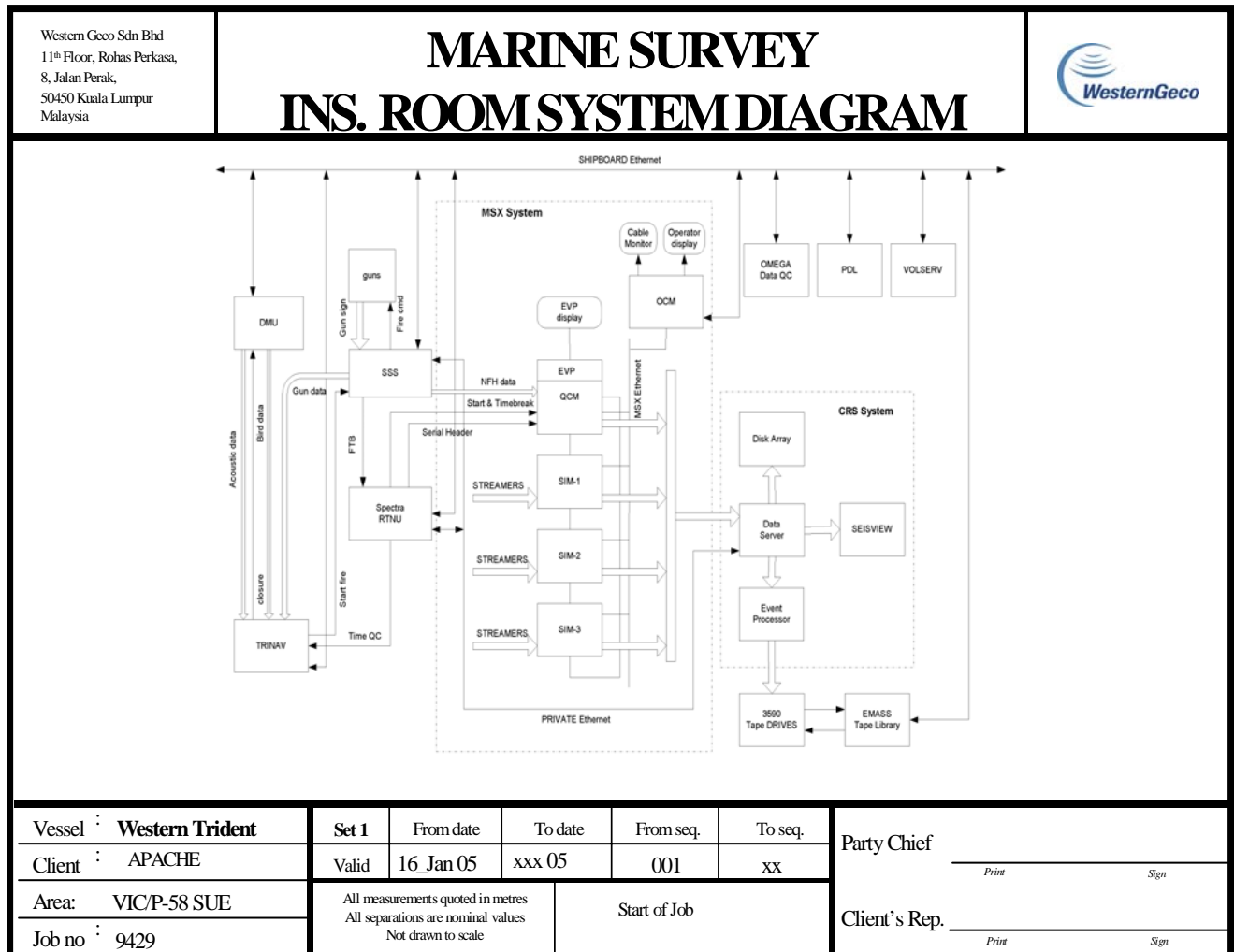
13.4. Source Layout during Undershoot (Pacific Titan)



13.5. Gun Dropout specs on Source vessel (Pacific Titan)

Gun Dropout Specs - 3040 cu.in. Source, 7 m gundepth.									
All two-guns dropouts are allowed, Except these:									
If Gun 1-7 (150cuin) fails, switch off Gun 1-8 (70cuin) - back in spec		1-7 and 1-9	1-7 and 3-9	1-8 and 3-8	2-6 and 3-7	2-8 and 3-8			
If Gun 2-6 (150cuin) fails, switch off Gun 2-7 (100cuin) - back in spec		1-7 and 2-6	1-8 and 2-7	1-9 and 2-6	2-7 and 2-8				
If Gun 2-7 (100cuin) fails, switch off Gun 2-6 (150cuin) - back in spec		1-7 and 2-8	1-8 and 2-8	2-6 and 2-8	2-7 and 3-8				
Cluster guns:									
Cluster 2-2:	If Gun 2-4 or 2-3 (300 cuin) fails, turn of the whole cluster and replace it with Cluster 2-1, Gun 2-2 and 2-1 (300 cuin)								
Cluster 3-1:	If Gun 3-1 (250 cuin) Fails, switch on Gun 3-2 (250 cuin)								
Cluster 1-2:	If 1-3 (150cuin) fails switch on 1-4 (150cuin)								
Cluster 3-3:	If 3-5 (100cuin) fails switch on 3-6 (100cuin)								
If 3-6 (100cuin spare) is enabled and fails, disable 2-6(150cuin) - back in spec									
Cluster 3-2:	If Gun 3-3 (150cuin) fails also switch off 1-1 (250cuin) and 1-5 (100cuin), switch on 1-4 (150cuin), 3-2 (250cuin) and 3-6 (100cuin)								
If Gun 3-4 (150cuin) fails also switch off 1-1 (250cuin) and 1-5 (100cuin), switch on 1-4 (150cuin), 3-2 (250cuin) and 3-6 (100cuin)									
Cluster 1-1:	If Gun 1-1 (250cuin) fails also switch off 1-5 (100cuin) and 3-3 (150cuin), switch on 1-4 (150cuin), 3-2 (250cuin) and 3-6 (100cuin)								
If Gun 1-2 (250cuin) fails also switch off 1-5 (100cuin) and 3-3 (150cuin), switch on 1-4 (150cuin), 3-2 (250cuin) and 3-6 (100cuin)									
Cluster 1-3:	If Gun 1-5 (100cuin) fails also switch off 1-1 (250cuin) and 3-3 (150cuin), switch on 1-4 (150cuin), 3-2 (250cuin) and 3-6 (100cuin)								
If Gun 1-6 (100cuin) fails also switch off 1-1 (250cuin) and 3-3 (150cuin), switch on 1-4 (150cuin), 3-2 (250cuin) and 3-6 (100cuin)									
Array 1									
Spare				Spare					
									
Gun 1-1	Gun 1-2	Gun 1-3	Gun 1-4	Gun 1-5	Gun 1-6	1-7	1-8	1-9	
250 cuin		150 cuin		100 cuin		150 cuin	70 cuin	40 cuin	
Array 2									
Spare		Spare							
									
Gun 2-1	Gun 2-2	Gun 2-3	Gun 2-4	2-5	2-6	2-7	2-8		
300 cuin		300 cuin		100 cuin	150 cuin	100 cuin	70 cuin		
Array 3									
Spare				Spare					
									
Gun 3-1	Gun 3-2	Gun 3-3	Gun 3-4	Gun 3-5	Gun 3-6	3-7	3-8	3-9	
250 cuin		150 cuin		100 cuin		150 cuin	70 cuin	40 cuin	

14. Instrumentation Room System Diagram



Vessel : Western Trident	Set 1	From date	To date	From seq.	To seq.
Client : APACHE	Valid	16_Jan 05	xxx 05	001	xx
Area: VIC/P-58 SUE	All measurements quoted in metres All separations are nominal values Not drawn to scale			Start of Job	
Job no : 9429					

Party Chief

Print Sign

Client's Rep.

Print Sign

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16. Navigation and Positioning System Description

16.1. System Configuration

16.1.1. Navigation Hardware and Software

System	Hardware (Type and Serial No.)	Software Version
TRINAV	WesternGeco TRINAV	TRINAV 2.6.0 patch 27 Sep 2004
Spectra	Concept Systems Spectra	9.8.04
Acoustic System	I/O Digicourse Digirange	System 3 version 4.42
TS-meter	Valeport 604 CTD	
Echo Sounder	Simrad EA 500	
Current Meter	Nortek ADCP at 500Khz.	SeisADCP Version 1.18

16.1.2. System Timing

TRINAV issued closures to the recording/source firing system 604 milliseconds before the predicted time of peak pressure. All TRINAV system positions are at the time of predicted peak pressure. The Spectra Real Time Navigation Unit (RTNU), a VME rack mounted system, performing data acquisition, validation and time stamping for the Spectra system, sends a latched TTL signal to the Source controller (SSS) to determine whether port or starboard source should fire. Spectra also handles the Ethernet communications between the third party MSX, SSS and PDL systems in order that they pass header information between themselves. Timing between the Trinav and Spectra was monitored and logged for each shot point using the two-boat TrueTime receiver to time tag the TRINAV closure and the Spectra CTB1 signal. No anomalies were observed.

Spectra and the MSX recording system utilise the UTC time standard for all time stamping of headers and records, whereas TRINAV utilises GPS time. Consequently there is a difference of 13 seconds (GPS is ahead of UTC) between the records in the TRINAV database and those recorded by Spectra and MSX. This difference was corrected when the P1/90 and P2/94 were generated by TRINAV, thus all field tapes are in the UTC time standard, however, plots and logs etc. from TRINAV that are derived directly from the database remain in GPS time.

A further timing difference lies when the shot time recorded on the shot record in the P2 and P1 is compared with the time stamp recorded on with the seismic field tape: The TRINAV system correctly rounds the decimal seconds whereas the Spectra and MSX truncate the decimal seconds; this means that there is a 1 second difference in timing between the P1 record and the seismic file number for approximately half the shots.

16.1.3. Undershoot Timing

TRINAV issued a closure to the TrueTime master box at 1500ms before shot time. This signal was time stamped and transferred to the TrueTime slave box on the Pacific Titan. The slave TrueTime box was configured to issue a TTL signal out to the gun control system, GunLink, at a specified delay after the time stamp. The GunLink controller then utilised its own internal GPS clock to count down until the shot time at which point the guns would fire and a time break pulse was issued to the slave TrueTime box. This (remote) FTB was time stamped and a message returned to the master TrueTime box with the time of the remote FTB. Both TrueTime boxes were synchronised to GPS time via an onboard GPS clock.

TRINAV used another closure relay to send a signal at shot time to the MSX recording system. This signal was also sent, in parallel, to the master TrueTime box to act as the (local) FTB and was time stamped upon its arrival. The three times (initial closure, local FTB and remote FTB) were output as an ASCII string on each shot and recorded in a file along with any timing difference between the two FTB signals.

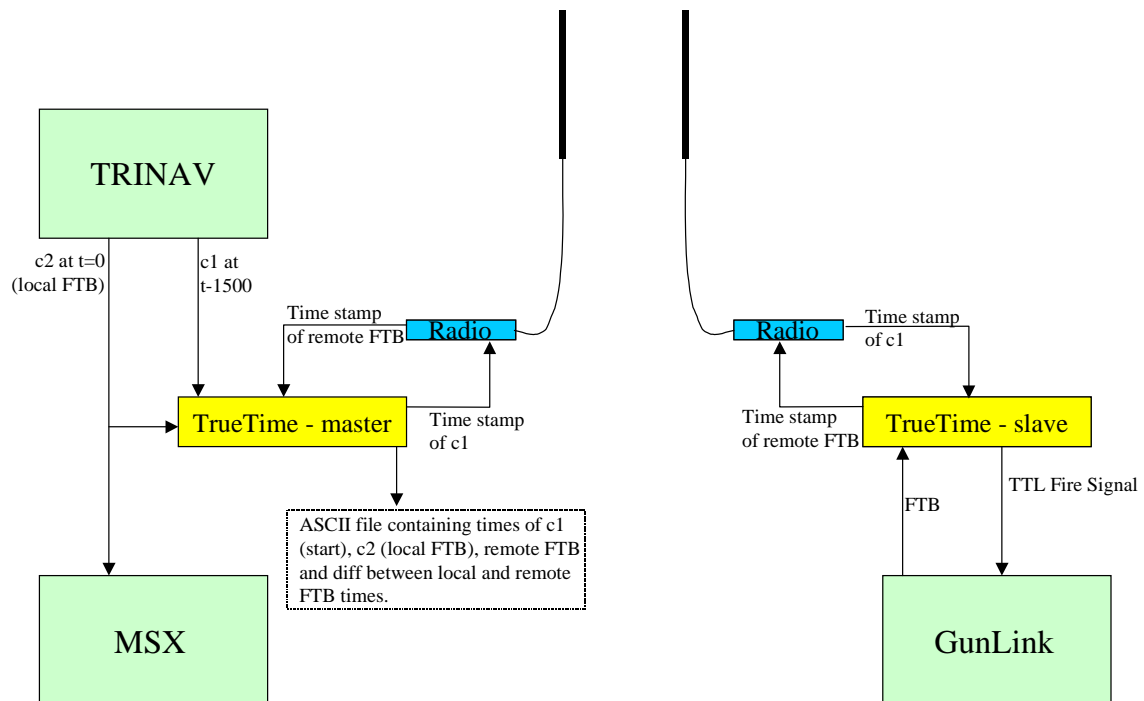


Diagram of timing signals for the undershoot

16.2. Survey Positioning Method Used

This 3D survey was carried out using WesternGeco's standard mode of operation for 8 streamers and dual source surveys.

Positioning of the vessel was by differential GPS, utilizing TRINAV GPS, PosNet, Fugro Multifix DGPS with delivery of Skyfix differential correction data in RTCM SC104 format by Inmarsat B and Optus satellites. Additionally C&C Technologies CNAV DGPS system with a wide area correction not in RTCM format, was received by an integrated receiver.

The centre near group of each streamer and the sources were positioned relative to the vessel using a network consisting of four PosNet rGPS system units mounted on each source and two PosNet rGPS system units mounted on floats towed wide from the vessel, via suspension points on lead-ins 2 and 7. These navigation points were integrated into a network of 116 Digicourse acoustic ranges, 20 baselines and 24 compass azimuths to produce a final position for the centre of source and the centre near groups of all cables.

The centre last group of each streamer was positioned using a network consisting of 8 PosNet rGPS system units, 8 compass azimuths, provided by streamer mounted compass heading units, and a network of 87 Digicourse acoustic ranges.

The mid streamer network consisted of 42 ranges between 16 acoustic transceivers mounted between 2100 and 2300 meters from the centre first group of each streamer.

The streamer shape was modelled by 19 Digicourse series 5000 combined streamer depth control and magnetic compass units per streamer.

Least square condition equations for each streamer assuming circular arcs between compasses and relating the tracking nodes, compasses, tension-corrected distances between compasses, rotation bias and scale were used to compute scale, rotation and individual compass corrections. The streamer shape was then computed by the circular arc method.

16.3. Surface Positioning

16.3.1. Vessel Navigation

<u>System 1:</u>	C&C Technologies CNAV Version 13.3 RTG corrections via integrated receiver.
<u>System 2:</u>	Multifix Version 1.05 Skyfix XP and Skyfix Standard via Inmarsat B and Optus sat
<u>System 3:</u>	TRINAV GPS Skyfix & Starfix corrections via Inmarsat B and Optus sat
<u>System 4:</u>	PosNet 1 Virtual base station corrections from Cnav (in RTG mode)
<u>System 5:</u>	PosNet 2 Virtual base station corrections from Cnav (in RTG mode)

Primary vessel positioning was provided by C-Nav. C-Nav is a different concept in GPS positioning. It is based upon the Real Time Gypsy (RTG) technology developed over a ten-year period by NASA's Jet Propulsion Laboratory (JPL) to provide centimetre-level accuracy for space applications. C&C technology have assimilated this technology to provide worldwide horizontal accuracy of the order of 0.1 meter (1 sigma) so long as the user is within InMarsat and GPS satellite visibility.

C-Nav uses monitoring stations strategically located around the globe. These stations, equipped with dual-frequency geodetic-quality GPS receivers, simultaneously collect RAW GPS observable measurements for the entire GPS constellation and transmit these data to two separate Network Processing Hubs (NPHs) in real-time.

Orbit and clock corrections, resolved by the NPHs for each GPS satellite, are universally valid at any location on Earth. These orbit and clock corrections are transmitted to all C-Nav users within INMARSAT visibility (75° N to 75° S Latitude).

Each C-Nav unit applies the appropriate GPS corrections to the satellites being tracked at that user's location. Local ionospheric and tropospheric effects are eliminated by comparing the L-1 and L-2 frequencies.

Further C-Nav system description and the most current station information can be found at: <http://www.cctechnol.com/site30.php>

Secondary vessel positioning was provided by the third party multi-reference positioning system Multifix XP.

TRINAV GPS is a multiple reference station DGPS system with the capability to be used in dual frequency mode when required, and tailored for the specific needs of seismic surveying. State-of-the-art algorithms combine reference station data and pseudo range measurements into the best position estimates.

By employing an exclusive correlation model for weighting the multiple range corrections in a least squares estimation process, the optimum pseudo-range corrections are obtained. W-testing and F-testing techniques detect and reject correction outliers.

Pseudo-range observations undergo comprehensive checks of validity and consistency before they are used in the fix algorithm. Carrier smoothing reduces the random noise effects on the pseudo ranges, and aids in multipath detection.

Integrity checking is a fundamental part of the processing philosophy: a Fault Detection, Isolation and Correction (FDIC) algorithm checks the consistency of the fix, detects and rejects any outliers, and re-computes the solution. W-testing and F-testing are used to give the best protection against erroneous observations.

Quality control is based upon UKOOA's recommended DGPS quality indicators - the precision and reliability of the fix are displayed as an Error Ellipse and Marginally Detectable Errors (MDE).

The two independent sources of corrections were transmitted to and received onboard the vessel by independent means thereby providing a high degree of redundancy to ensure continuous vessel positioning.

Six different, independent systems utilising two completely independent concepts for correcting the GPS data were used; thereby providing a high degree of redundancy to ensure continuous vessel positioning.

➤ **Further information about these systems is given in Navigation Exhibit 1.**

Although Selective Availability was turned off in May 2000 differential corrections are still required to provide a continuous high quality vessel position. Less frequent updates are required however.

With the current increase in solar activity, users of the Global Positioning System can experience an increased level of instability in computed GPS positions in some geographical areas. For this project, WesternGeco provided a technical solution to this problem through the use of dual frequency receivers and dual frequency reference stations from Fugro.

16.3.2. Float Navigation

Float (tailbuoy, source and wide-towed front floats) surface navigation was provided by PosNet rGPS systems. The in-sea units incorporated a GPS receiver and interfacing for direct data transmission of the raw satellite pseudo-range data through the source cabling or by conventional UHF telemetry radio.

On board the vessel, the raw pseudo-range data from the float unit was matched with simultaneously received data at the vessel's GPS receiver to compute a vector describing the location of the float unit relative to the vessel from which the float position was derived. Relative positioning was better than 2m.

16.4. Streamer and Source Positioning

16.4.1. Acoustics

Acoustic data in the front, mid and tail networks was provided by I/O Digicourse System 3 version 4.42. This system comprises a rack mounted Controller (DMU), Processor and PC based interface which are located in the instrument room. The CTX (Gun Positioning System) transceivers mounted on each source, together with CMX transceivers mounted on the front of each streamer and front float provide a front network from which vessel relative source positioning is computed. CMX transceivers mounted on the streamers and tailbuoys provide vessel and tailbuoy relative streamer positioning.

16.4.2. Streamer Compasses

One hundred and fifty two (152) series 5000 Digibird combined magnetic compass and streamer depth controllers were attached to the eight streamers. They were controlled via the I/O Digicourse System 3 DMU as mentioned above.

Compass Sampling Rate	=	1 second
Averaging constant	=	7 seconds

Compass performance was monitored on a line by line basis throughout the acquisition phase of the survey.

16.4.3. Gyro Compass

The gyrocompasses used during the survey were:

Instrument Room Gyro	- Gyro 1 C Plath SR180 Mk1 Serial No 5029
Ships Gyro	- Gyro 2 C Plath SR180 Mk1 Serial No 5033

The gyro correction values as computed by RTCalib from previous survey were as follows:

Instrument Room Gyro 1	-1.44
Instrument Room Gyro 2	-0.10

16.4.4. Velocity of Sound in Water

The following type of TS-meter has been used to determine the speed of sound in water.

□ Type: Valeport 604 CTD

The model 604 measures Conductivity, Temperature and Pressure parameters and from these measurements Depth, Salinity, Density and Speed of Sound are calculated.

Velocity measurements were taken during the survey on a weekly basis when the weather permitted.

16.4.5. Echo Sounder

The echo sounder speed of sound was set to 1500 m/s. A draught correction of zero was entered in the echo sounder. The speed of sound for the total water column was derived from Temperature Salinity profile measurements taken throughout the survey. The computed speed of sound and draught value were used to produce water depth corrected P190s.

16.5. Auxiliary Navigation Sensors

16.5.1. Current Meter

Data from an Acoustic Doppler Current Profiler (ADCP), or Current Meter, was acquired throughout the survey. This data was used to assist the survey planning throughout the operation and so reduce the infill. The sensor used was a Nortek ADCP operating at a frequency of 500 Hz. Data sets were regularly sent for test and correlation to ensure that the data was consistent and acceptable.

17. Navigation Systems Verification and Monitoring

17.1. Echo Sounder Verification

The verification was carried out to determine the draught of the transducer in use and to compute a correction for the scale error.

- **The dockside verification results are in Navigation Exhibit 2**

17.2. Gyro Monitoring

Continuous monitoring of the vessel gyros was performed using TRINAV's rtCalib utility program and a GPS baseline.

The gyro correction estimates provided by this program have been monitored and compared with previous dockside verification values and previous surveys.

A dockside verification was performed in one direction at Dampier Cargo Wharf, Dampier, Western Australia on the 11th February 2004.

- **The gyro verification results are in Navigation Exhibit 3**

17.3. GPS Monitoring

Continuous monitoring using the Integrity Monitor was carried out offshore to verify that the installation was satisfactorily operational (data reception, transmission, processing and logging were verified) and that the operational settings were correct. Each system to be used, including duplicates, was verified.

rGPS Health Check was carried out with the use of TRINAV GPS's Re-Radiation kit.

- **The TRINAV GPS Integrity Monitor station in use is described in Exhibit 1.**
- **The Health Check results are in Exhibit 3**

Health checks onshore were carried out to verify that the installation was satisfactorily operational (data reception, transmission, processing and logging were verified) and that operational settings were correct. Each system used, including duplicates, was verified.

DGPS Health check onshore using the Integrity Monitor was carried out.

17.4. Current Meter Monitoring

To confirm that the Acoustic Doppler Current Profiler ADCP is operating correctly, with optimum configuration and, in so doing, providing a high quality data set for real-time and post-survey use, a test data set was sent weekly to an external contractor, Fugro GEOS. This process provided the onboard operation with a high level of confidence in the validity of the data being gathered, thereby increasing its value for survey planning.

18. Navigation Processing

18.1. The TRINAV System

TRINAV consists of a network of SUN SPARC workstations, external mass-data storage and hard-copy facilities running WesternGeco proprietary software on the UNIX operating system. Positioning sensors are interfaced to TRINAV through two VME sub systems.

The positions for each vessel/float are passed through a Kalman filter, where they may be integrated with speed and heading inputs. The output of the primary vessel Kalman filter is used for predicting the time when the first CMP position will be at the required distance along the preplot line. Relays are closed a fixed time prior to the estimated time of peak pressure. The raw, decoded data strings, and computed positions are stored to disk/tape.

The raw sensor data and Kalman filtered surface positions are passed from the Real Time acquisition system (TRINAV RT) to a near real time source and receiver positioning system (TRINAV QCPR). TRINAV QCPR computes positions online and provides facilities for any post processing required.

The data received by QCPR is immediately stored in a Techra relational database with directories for raw, filtered and processed data. Front, middle and tail networks are solved by least square adjustment at every shot-point. In-sea measurements are 'clipped' to remove large spikes. Statistical models are used to test the results of the adjustment, by detection of outliers. If the first iteration fails then the adjustment is repeated after the largest outlier has been removed. This routine is repeated until a satisfactory adjustment is achieved.

The quality of the data is then evaluated with the TRINAV application Diagnostics, against a set of standard criteria. WesternGeco's PAC, or **Position Acceptance Criteria**, comprises of a set of tolerances on specified statistics, which allow this objective assessment of the positioning quality to be made.

The resulting node positions are then smoothed using Kalman filters. From the source node, the center of source position is computed. The streamer cable shapes are computed from filtered compass data in order to establish positions for all the receiver groups. Wherever possible, the results of the real-time source and receiver positioning were used to make the final positioning data set. When the results from the online solution exceed the PAC additional processing was carried out on the 'off-line' system.

Final and raw navigation data in UKOOA standard formats was generated directly from the database on the off-line system. Available media are 3590 cartridges.

The technique for these is described in **WesternGeco's Navigation systems – a Technical Introduction**, which is available upon demand.

18.1.1. Shot Editor

The Shot Editor was available for use on all lines as follows:

- Editing of non-production shot-points at the start and end of each line.
- Interpolation of missing shot-points.

18.1.2. Gun Editor

The Gun Editor was available for use on all lines as follows:

- The Gun Editor was used on shot-points interpolated by the Shot Editor to generate the missing gun mask. The gun mask is normally relayed to TRINAV via the External Header.
- The Gun Editor was used to change the status of the sources to non-firing for any NTBP sections of the lines.

18.1.3. Recompute

The vessel system position was computed and the positions saved at one second intervals to disk/tape by TRINAV RT. The positions of all objects at the predicted time of peak pressure were passed to TRINAV QCPR and stored in the database online.

Diagnostics was used on each line to decide if the real time Kalman filtered positions were acceptable. If the positions were not acceptable, the Recompute program was used to select different positions for each object or to merge different DGPS systems for parts of the line.

If new positions were selected in the Recompute these were Kalman filtered in the Smoother program using a forward backward Kalman filter.

The following plots were available for examination and comparison of the positioning systems:

- User selected track plot display of color-coded positions.
- Inline and Crossline time series shot to shot plots for selected positions.
- Inline and Crossline time series difference plot between selected positions and a reference position.
- Time series plots giving stochastic analysis of position quality for selected positions.

18.1.4. Smoother

The Smoother program is used for smoothing of surface positions offline and for smoothing of tracking nodes both online and offline.

When QCPR is acquiring data online the tracking node positions are smoothed using a forward Kalman filter. If the tracking node positions exceeded the PAC tolerances, they were re-smoothed offline using a Forward-Backward Kalman Filter. If new positions were selected in the Recompute program these were smoothed and time adjusted to shot time using the Kalman Forward-Backward filter.

❑ Kalman filter

This filter assumes that between any two shot points there will be zero average acceleration but some oscillation (noise) around the average.

❑ Forward-Backward (FB) Kalman Filter

All smoothing in post processing was performed using a Forward-Backward Kalman filter. This is essentially the weighted average of the raw data and two individual Kalman filters running in opposite directions through the data set.

This filter has the same acceleration parameters as the online Kalman filter but has separate rejection window parameters (for X and Y) thus enabling the user to model the expected motions independently. The FB Kalman filter for surface positions works in the area relative co-ordinate frame, while the FB Kalman and Kalman filters applied to the tracking nodes work in a vessel relative coordinate frame.

The quality of the smoothing was checked using the following difference plots:

- Difference between smoothed and un-smoothed data was checked to see the effect of the filter settings applied.
- Velocity cross-line and in-line plots indicate the amount of noise in the smoothed position.
- Variance Factor plot indicates the fit between the predicted and raw positions.

18.1.5. Filtering

❑ Compass Processing

The compasses were filtered online using two successive Kalman filters to avoid introducing any lag in the data. The difference between the predicted compass reading and the actual compass reading is tested at each shot. If the residual exceeds twice the standard deviation for two successive shots the online compass filtering was flagged as requiring post processing. If the online compass filtering failed, the data was analyzed by viewing time-series plots of raw and filtered data. Filter parameters were chosen to remove spikes and noise from the compasses. In the first instance the Kalman filter parameters were tuned to match the specific data set. If this did not achieve the desired result the following filters were used: -

For front compasses a median filter or a combination of median and mean filters.

Mid streamer and tail filters normally required a longer median depending on noise and movement.

❑ Gyro Filtering

No gyro filtering was carried out.

❑ Acoustic Filtering

The acoustic networks were designed with maximum redundancy to ensure that positioning specifications could be maintained in case of range dropouts due to mechanical or electrical failure, noise or interference. All acoustic data was investigated using time-series plots.

The survey program is designed to identify by means of statistical testing where spikes and reflected ranges are corrupting the data as long as there is sufficient redundancy. On occasions it was necessary to apply clipping filters to remove large spikes which tended to degrade the solution of the tracking nodes. It was necessary to condition the data using some median/mean filters also.

18.1.6. Reprocessing

The source and receiver position computation is divided into a number of discrete steps. These steps are executed automatically online. If post processing is required the operator is able to change parameters and examine the output between steps.

The processes are:

1. Least Squares solution of front and tail networks.
2. Kalman/Kalman FB smoothing of front and tail network tracking nodes
3. Computation of the streamer shape: receiver group lengths and sensor offsets are modified using a streamer tension model. Least squares condition equations are then used to compute corrections to the receiver group intervals and compasses in order to best fit the front and tail tracking nodes. The amount of stretch/compression permissible is user specified. The computation of positions and estimation of variances of the mid streamer network nodes is included in this process.
4. Least squares solution of the mid streamer network
5. Smoothing of the mid streamer tracking nodes
6. Step (3) is repeated using the front, middle and tail tracking nodes.

The least squares solutions include statistical testing and automatic rejection of outliers on a shot by shot basis.

18.2. Quality Control

Navigation post-processing was carried out on-board through to UKOOA P1/90 and P2/94 tape production.

18.2.1. First Line Test Data

After the first line was shot and processed, a test line was sent electronically to an external contractor, ECL. The data sent comprised:

1. All offset diagrams (vessel, streamer, source and float)
2. Offset spreadsheets
3. Velocity Profile Spreadsheet,
4. 100 shot points of P1 and P2 data
5. ASCII file of Diagnostics for this line
6. ASCII file of LAF for this line
7. ASCII files of Surface and Insea Survey Definitions
8. Job Book (as supplied from the supporting office)
9. Minutes from Start-up meeting (if relevant)
10. PFM Magnetic Variation Spreadsheet

A thorough QC of this test line was undertaken. The following checks were carried out:

- Strict compliance with published UKOOA P1 and P2 header and data format and generation of Format Check Reports.
- Graphical display of source and receiver towing geometry and comparison with WesternGeco office and vessel generated diagrams/documentation.
- Full vessel Configuration Report, as defined in the P2 header.
- Check P2 header defined Tow Points, Geodetic Parameters, etc. against WesternGeco Job Book and/or published values.
- List P2 header differences from a prior line sequence (if required).
- Raw data display and analysis
- Automated and manual (if required) data conditioning.
- Data processing to independently resolve vessel, source and receiver co-ordinates.
- Full position comparison report with WesternGeco P1/90 co-ordinates.
- Investigation of unacceptable position comparison results.
- Data Check and Statistics Report for compliance testing with survey contractual standards and specifications.
- Generation of statistics, error reports, test results, displays etc. as deemed necessary to highlight problem areas.
- Generation of QCPro P1/90 file, if desired.
- Check P2 file compliance with WesternGeco standard survey definition naming conventions.
- Check P1/90 and P2 file data compliance with WesternGeco standard numbering conventions.
- Comparison of vessel survey definitions with supplied offset spreadsheet and diagrams.
- Conduct Parameter Confirmation following the Parameter Confirmation Check Lists, MWWD/F012 and MWWD/F013.
- Other Survey Start-Up tests and checks as required and directed by WesternGeco.

When all the checks were performed a feedback report was published on ECL's secure web site. Any corrections required were made by the vessel. The Supporting Office and ECL then received a confirmation from the vessel that all updates had been completed.

18.2.2. Initial QC

The post-processing procedures included the following checks:

- QC checks on all survey parameters.
- Generation of correct survey definitions.
- Completion of shot point edits.
- P2/94 production.
- Completion of gun edits.
- QC of system positions and recomputed positions if required.
- Smoothing of the vessel and buoy positions if required.

- Selective check and filtering if required, of the observations including:
 - Acoustic ranges.
 - Compass bearings.
 - Gyro heading.
- Least squares adjustment of front and tail network if required.
- Smoothing of source/streamer tracking nodes if required.
- Cable shaping to determine final source/receiver positions if required.
- Final QC of all lines
- P1/90 production.

The following documentation was produced for onboard QC:

- Navigation reports detailing information about the survey parameters, calibrations and continuing daily logs.
- A series of statistics and plots from on-line data acquisition:
 - Navigation line logs detailing performance and parameters used for the surface positioning, acoustics and compasses for each line.
 - Seismic observer's logs detailing gun information.
 - Edits list from the seismic observers detailing gun information.

18.2.3. Final QC

The post network solution QC plots and statistical printouts detailed in the previous section were examined and compared to WesternGeco specifications. In addition, trend analysis plots were created and updated after each line. They were analyzed daily to ensure consistency throughout the data set.

18.3. Water Depth Processing

Water depth processing was done on the raw water depth data onboard the vessel.

The water depth data was reduced to Mean Sea Level and then:

- corrected for draught
- filtered to de-spike and interpolate missing data
- corrected for the measured sound velocity in water

The final data was dispatched on 3590 tape direct from the vessel.

19. Observations

19.1. Navigation Summary

All systems performed well, however during acquisition the below systems required further detail.

19.1.1. TRINAV RT/QCPR & Spectra

No major problems were seen in either system except for one line where the TRINAV VME system software crashed whilst online. This resulted in a reshoot.

19.1.2. DGPS

The various DGPS systems all agreed with one another throughout the job. The Multifix XP system developed an electrical problem on its antenna and so stopped working correctly and gave large errors in position. As this was only one of several inputs to the vessel estimator, no loss of positioning accuracy was caused, and, once the antenna had been replaced, the XP system worked well again.

19.1.3. Integrity Monitor

This system performed as specified through the survey. However, there were some gaps in the data received because of problems with the vessel's VSAT system. These problems originated with the VSAT provider and were associated with the shore based equipment. There is no reason to believe that there was any error in the positioning of the vessel during the periods when the Integrity Monitor was not available.

19.1.4. rGPS (Sources, Head and Tail Buoys)

All source and tail buoy floats were operational throughout most of the survey. Marginal weather conditions affected the data quality at times; the gun string rGPS units as waves can swamp the antennas mounted 0.8m above the water line and the tailbuoy GPS shows evidence of the tailbuoy being thrown around by the sea.

There were several instances of the tailbuoy GPS units being non-operational for periods of time. These were usually caused by power problems on the tailbuoy and the units were fixed as weather permitted. The redundancy employed in the tail end network ensured that sufficient positioning accuracy was achieved at all times.

19.1.5. Acoustics

Acoustic performance throughout the survey was generally good. Ranges from the guns were generally poor as were the cross streamer ranges between streamers 4 and 5 as they passed through the gun bubble.

The shallow water created additional problems as reflections were seen in the data acquired. Attempts to gate these reflections out sometimes resulted in data being lost outside the window as the streamers moved relative to one another. At all times, sufficient data was acquired such that the redundancy allowed a high degree of confidence in the final solution.

Several lines were affected by an intermittent coil line leakage problem on streamer 7. The loss of data for a shot or two at a time was such that it was a simple matter to filter through the missed data using a short median/mean filter. Once the leakage on the coil line became bad enough to

affect the data from the acoustic units it was easy to trace and so was repaired. The repair was carried out before the cable positioning was adversely affected.

19.1.6. Compasses

Generally, this was very good data when the weather was clam. The compasses did suffer from the same coil line leakage as the acoustics, but to a lesser degree since they send a much shorter and simpler message. There were several lines that were shot into marginal weather conditions and these caused some problems in processing as the data spiked greater than 10° for large portions of the line. The filters applied smoothed the data to a degree acceptable to the client.

19.1.7. Undershoot

The two boat undershoot went well once the timing issues had been resolved.

A failure of the third TrueTime box meant that it was not possible to start the recording system referenced to this same closure as the initial start signal (t-1500ms). As a result, the TRINAV used another closure relay to send a signal at shot time (t=0) to the MSX recording system. The nature of relays is such that there was a different, and random, small delay on each relay between the time that the relay was signalled and the time that the relay actually closed. This resulted in a variable difference in the two FTB signals of +/-20ms. This difference between the two FTB signals was applied to the recorded seismic data in data processing and resolved this difference.

19.2. Processing and QC Summary

All lines have been processed to pass the Trinav PAC (Position Acceptance Criteria). Data quality in general was good but due to the 8m streamer depth allowing acquisition to continue in moderately rough sea conditions the compass data was noisy on several sequences and heavier filters were required. Online compass calibrations for individual compasses also failed on some of these sequences.

Acoustic data was poor in the cross streamer ranges between cables 4 and 5 – this was a result of a combination of the gun bubbles and the propeller wash. Nevertheless, the acoustic network was very well behaved and the redundancy that is always built in served to provide a very solid network solution on all lines.

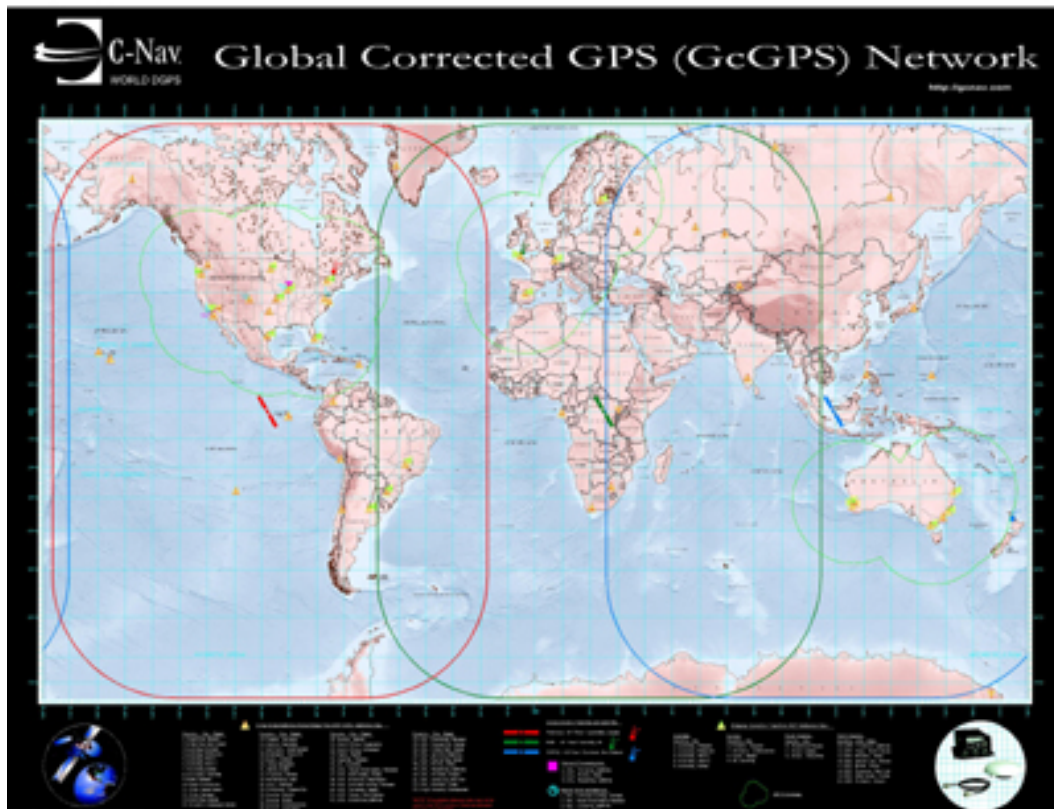
19.3. Conclusions

An acceptable data set was acquired and all the client's requirements were met for the survey.

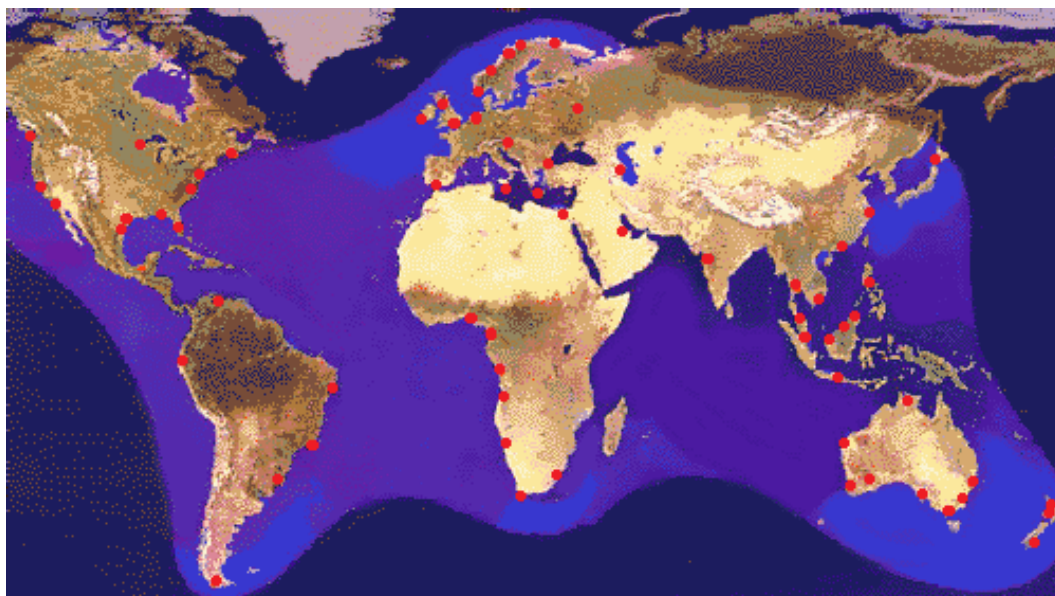
20. Navigation Exhibits

Exhibit 1 : Navigation System

❑ DGPS Coverage Maps for RTCM Sources



❑ OmniStar Reference Stations



❑ **GPS System Installation Notes**

WesternGeco GPS Receivers

TRINAV GPS

Novatel Millennium Receiver

- Serial number CGY00180002
- Hardware revision: 2.03
- Firmware revision: 4.503/2.03
- Receiver connected to the GPS splitter for the forward Trimble antenna

PosNet-1 Trimble

- Model: Trimble SSI
- Serial number: 3839A23949
- Software: Posnet version 1.81
- Firmware: Version 7.29
- Connected to the splitter for the aft Trimble antenna

PosNet-2 Trimble

- Model: Trimble SSI
- Serial number: 3807A21806
- Software: Posnet version 1.81
- Firmware: Version 7.29
- Connected to the splitter for the aft Trimble antenna

rtCalib

- Model: Leica MX9400
- Serial number: 312
- Firmware: version 1.59A
- Connected to the splitter for the aft Trimble antenna

Third Party GPS

Multifix Main

- Model: Ashtech
- Serial number: ZE1200337006
- Software: Multifix 4 version 1.05
- Firmware: Version ZE00
- Connected to the splitter for the aft Trimble antenna

Skyfix Main

- Model: Ashtech
- Serial number: SPM-236
- Software: Starfix HPM vers 4.03
- Connected to the splitter for the aft Trimble antenna

CNAV Main

- Model: 53220-00 Rev X
- Serial number: 250334
- Software: 13.3
- Firmware:
- Connected to the splitter for the aft Trimble antenna

TrueTime Receivers

There are two TrueTime receivers in use. One of them is a standard integrated timing receiver (ITR) being used to provide an IRIG-B timing reference signal for TRINAV. The other is a two-boat timing receiver that is being used as a Timing QC tool to time stamp the TRINAV closure and CTB1 time break signal from the Spectra for comparison purposes.

ITR

- Model: XL-DC-151-601
- Serial number: 9617419
- Software: TrueTime mk III sys ver 020
- Firmware: GPS XL V1.036 182-6111V003
- Connected to the splitter for the aft Trimble antenna.

Timing QC

- Model: 151-602-708
- Serial number: 012117249
- Software: TrueTime XL Ace3 sys ver 029
- Firmware: GPS XL V1.049 182-6483V008
- Connected to the splitter for the aft Trimble antenna.

❑ **TRINAV GPS Integrity Monitor Station Description**


Station Name: SALE
 Location: South East Asia / ASA
 Country: Australia

Latitude	38° 06' 06.273" S
Longitude	147° 05' 21.199" E
Ellipsoid	WGS-84
Semi Major Axis	6378137.0 m
Inverse flattening	1/298.257 223 563
Datum:	WGS-84
Ellipsoid Height	21.44m

Station Description	The Station is located at the Schlumberger OFS Office at Raglan Street, Sale, Victoria AUSTRALIA
Antenna:	The antenna in use is a Model 502 L1/L2 GPS Dual Frequency Antenna from Novatel. The antenna is mounted on a pole on the front of the building, giving a height above ground of approximately 10m. The Receiver is located in the Server Room Racks. Cable run from Antenna to receiver is approx 15m. (LMR-195 cable)
Receiver unit:	The unit in use at the Integrity Monitor is a Novatel Power Pak II dual frequency receiver. Installation was on the 10 May 2002
Observation and Processing method:	The Antenna Position was Surveyed by Kluge Jackson consultants using standard survey methods. Height was derived through measurement on the Australian Height Datum AHD (15.64m) and addition of AUSGEOID98 Model Geoidal Separation value (5.8m).
Date of Survey:	10th May 2002
Comments:	None.

Exhibit 2 : Echo Sounder Calibration

Echo Sounder Check (In Port)



Vessel: Western Trident	Date : 23/12/2004	
Client: Apache	Check started (GMT):	
Job no. 9438	Check ended (GMT):	
Location: Freemantle	E/S draught: 7.65 m	
E/S type: Simrad EA500	Vertical offset keel to E/S: 0.00 m	
Serial no: 4139	Bridge E/S reading N/A	

Observed				
Draught (m)			Lead Line Depth (m)	
Bow	Mid-ships	Stern	Stbd (1)	Port (2)
6.90		7.60	10.65	13.50
Draught at E/S		6.99	LL Depth at E/S	
			12.08	

Echo Sounder Readings	
Freq 1 (m) 18 MHz	Freq 2 (m) 200MHz
4.80	4.90
4.80	4.90
4.80	4.90
4.80	4.90
Average = 4.80	4.90
+ vertical offset keel to E/S transducer	0.00
+ draught (keel to sea surface)	0.00
Total water depth (m)	6.99
11.79	11.89

Observed - Echo Sounder = 0.28 m Freq 1

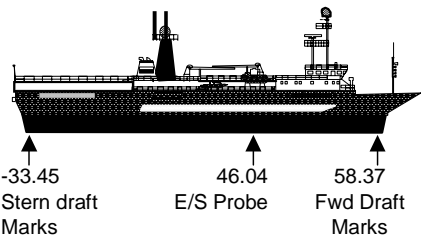
Observed - Echo Sounder = 0.18 m Freq 2

Factory Defaults (from manual)

RangeA	xx.xx	Check <input type="checkbox"/>
Absorption coefficient	3 dB/Km	<input type="checkbox"/>
Transmit power	2000 W	<input type="checkbox"/>
Transducer Depth	0.00	<input type="checkbox"/>
Speed of sound	1500 m/s	<input type="checkbox"/>
two way beam angle	-17 dB	<input type="checkbox"/>
Transducer gain	25 dB	<input type="checkbox"/>
Sample distance	0.25	<input type="checkbox"/>

Sounder Settings Check:

RangeA	xx.xx	Check <input type="checkbox"/>
Absorption coefficient	3 dB/Km	<input type="checkbox"/>
Transmit power	2000 W	<input type="checkbox"/>
Transducer Depth	0.00	<input type="checkbox"/>
Speed of sound	1500 m/s	<input type="checkbox"/>
two way beam angle	-17 dB	<input type="checkbox"/>
Transducer gain	25 dB	<input type="checkbox"/>
Sample distance	0.25	<input type="checkbox"/>

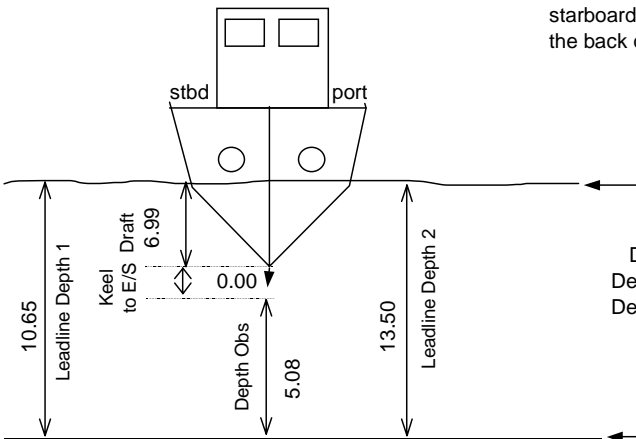


-33.45 46.04 58.37

Stern draft E/S Probe Fwd Draft

Marks Marks

Offsets above are relative to VRP
Echosounder probe is directly below the
starboard liferaft launching davit - just behind
the back of the wheelhouse.



Depth Obs (Draft) = 5.08

Depth Calc (Freq 1) = 4.80

Depth Calc (Freq 2) = 4.90

Exhibit 3 : GPS and Gyro Calibration

❑ Offshore Calibration Report

OFFSHORE CALIBRATION REPORT

Table of Contents

- I. Introduction and Abstract of Results
- II. Differential GPS Verification
- III. RGPS Verification
- IV. Gyro Calibration
- V. Conclusions and Comments on Data Quality
- VI. Secondary and Tertiary GPS System Differences to TRINAV GPS
- VII. Line by Line Results from RT Calib for Gyros and Integrity Monitor

I. Introduction and Abstract of Results

During the seismic survey undertaken by M/V Western Trident for Apache from December 30th 2004 to January 15th, 2005 on the VIC/P47, Moby 3D prospect (WesternGeco job number 9438), the DGPS, rGPS and Gyro positioning systems were monitored continuously throughout acquisition. This allowed C-O values to be computed, monitored and modified, if necessary, whilst offshore. These offshore calibration techniques have been developed by WesternGeco – the principal components comprise:

- The Integrity Monitor, one of several shore reference stations where a GPS receiver and data link are established at a known co-ordinated point allowing comparisons of the vessel GPS receiver performance against the reference receiver.
- The Re-radiation Kit which enables rGPS systems to be fed the same GPS signal as the vessel receiver, thus allowing performance evaluation to be undertaken by means of a zero baseline test.
- The RT Calib system that uses the Primary vessel GPS together with a second GPS installation at a predetermined point on the vessel to determine a heading vector against which the vessels Gyros may be calibrated.

The technique for these is described in **WesternGeco's Navigation systems – a Technical Introduction**, which is available upon demand.

The report presents the observations and results from these offshore calibrations.

Abstract of Results

Value		C-O	SD
Gyro 1 (mean)		-1.47°	0.55°
Gyro 2 (mean)		-0.20°	0.55°
GPS Integrity Monitor Results	Delta Easting	0.36m	0.48m
	Delta Northing	1.00m	0.69m

Navigation System Average Radial Differences

	Diff	SD
TriGPS	0.53m	0.10m
C-Nav	0.38m	0.16m
Posnet 1	0.46m	0.19m
Posnet 2	0.66m	0.16m
Multifix	0.42m	0.32m

II. Differential GPS Verification

M/V Western Trident utilised the following DGPS systems throughout the survey:

Primary vessel positioning was provided by C&C Technologies' CNav with RTG corrections via an integrated receiver.

Secondary vessel positioning was provided by Multifix 4 with direct injection of Skyfix XP and Skyfix Standard RTCM corrections delivered by Inmarsat B and Optus sat.

A Novatel Millennium Dual Frequency GPS receiver provided raw pseudo range data to WesternGeco's TRINAV GPS 2.6 for tertiary vessel positioning with Skyfix RTCM corrections delivered by Inmarsat B and Optus sat and RTCM corrections generated by CNAV.

Data transfer between the vessel and the Integrity Monitor Receiver was achieved using the vessel's VSAT satellite data link.

Method used

Refer to **WesternGeco's Navigation systems – a Technical Introduction**, DGPS Calibrations Integrity Monitor section.

A dual frequency receiver on board combined with a dual frequency Integrity monitor allowed the computation a DF vector between vessel and monitor station which provided positioning integrity irrespective of whether a single or dual frequency solution was used for the vessel positioning.

Results

Chapter VI contains a summary of the statistics taken from the diagnostics files and derived from the data logged by rtDisplay.

Chapter VII contains numerical data from rtcalib for the integrity monitor.

Figure 1 shows an example of the Integrity monitor QC plot created for each sequence. Figures 2 and 3 show the trend analysis for the complete survey.

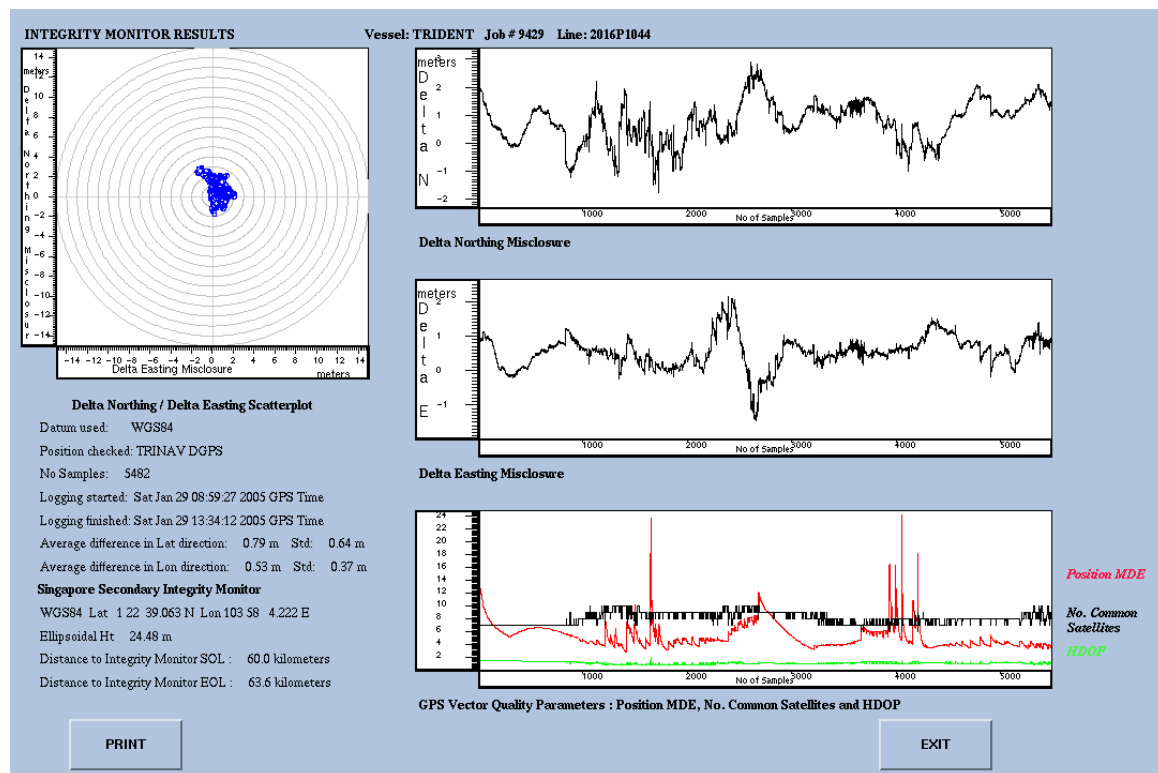


Figure 1: Integrity Monitor Plot to demonstrate GPS quality

Section 4: Navigation

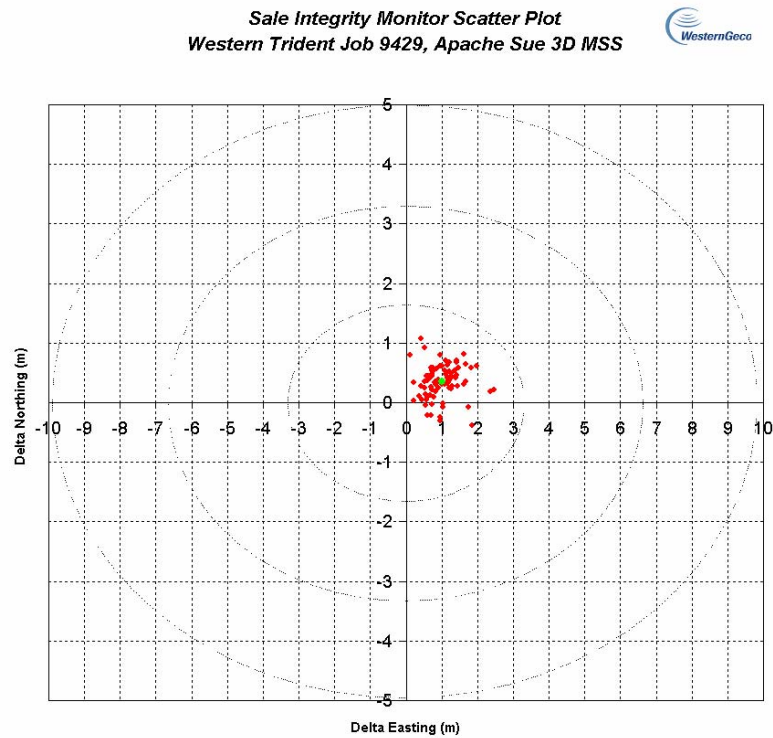


Figure 2: Integrity Monitor Delta Easting - Delta Northing Scatter Plot

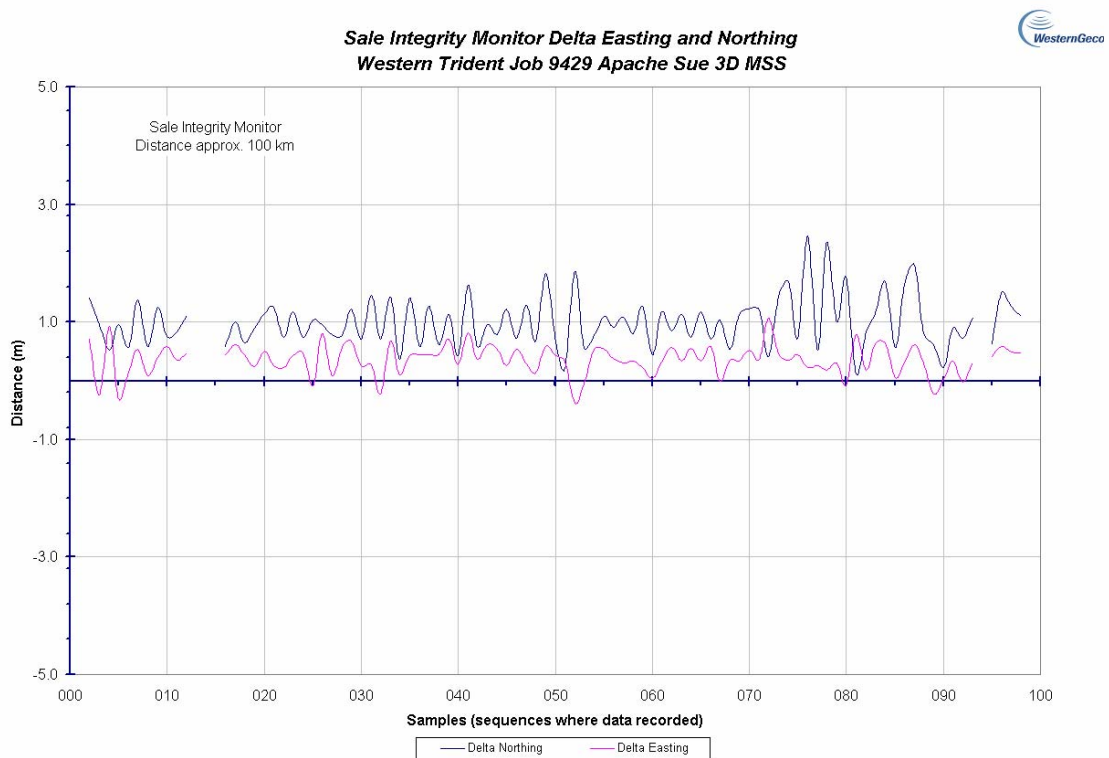


Figure 3: Integrity Monitor Delta Easting – Delta Northing Trend

III. rGPS Verification

M/V Western Trident utilised WesternGeco's TRINAV GPS 2.6 rGPS system throughout this survey for Float and Source positioning. The GPS signal received by the main TRINAV GPS vessel receiver is split using a purpose designed GPS splitter from WR systems inc. It is then used by both the main vessel receiver and transferred to a re-radiating antenna on the back deck, allowing use of a near identical GPS signal by float and vessel receivers simultaneously.

Method used

Refer to **WesternGeco's Navigation systems – a Technical Introduction**, rGPS Calibrations section.

Results

The table below shows a summary of the statistics taken from plots within TRINAV GPS for all float units. This table contains collated data from the re-radiation tests done at the start of the survey.

	Lat	Lon
F001	0.47	-1.02
F002	-0.71	-0.01
F003	-0.10	0.58
F004	-0.50	0.06
F005	0.47	0.67
F006	-0.44	0.20
F007	-0.70	0.11
F008	-0.34	0.24
FG01	0.56	0.36
FG02	0.55	-1.30
FG03	-0.19	-0.64
FG04	0.22	0.52
FG05	0.47	0.67
FG06	-0.13	-0.57
FG07	0.42	-0.56
FG08	0.66	-0.59
FF01	1.10	1.24
FF02	-0.41	-0.88

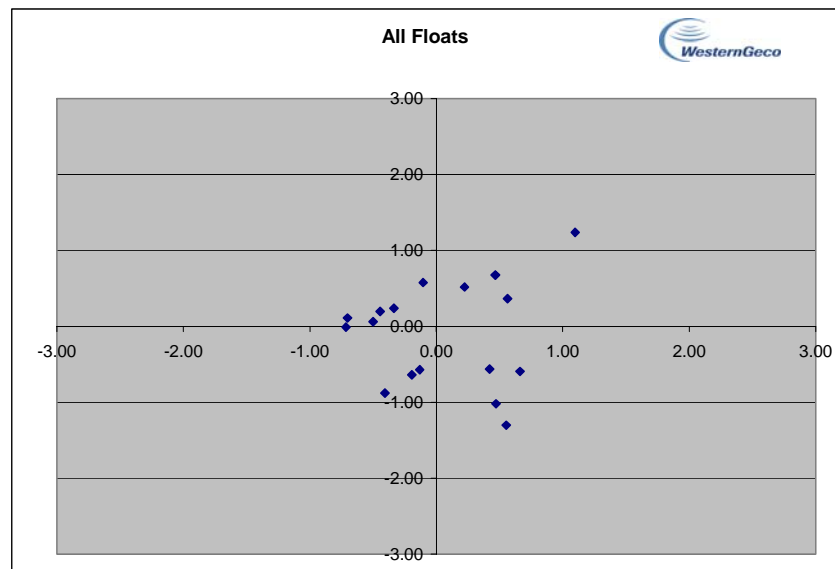


Table 1: rGPS verification test data from re-radiation tests

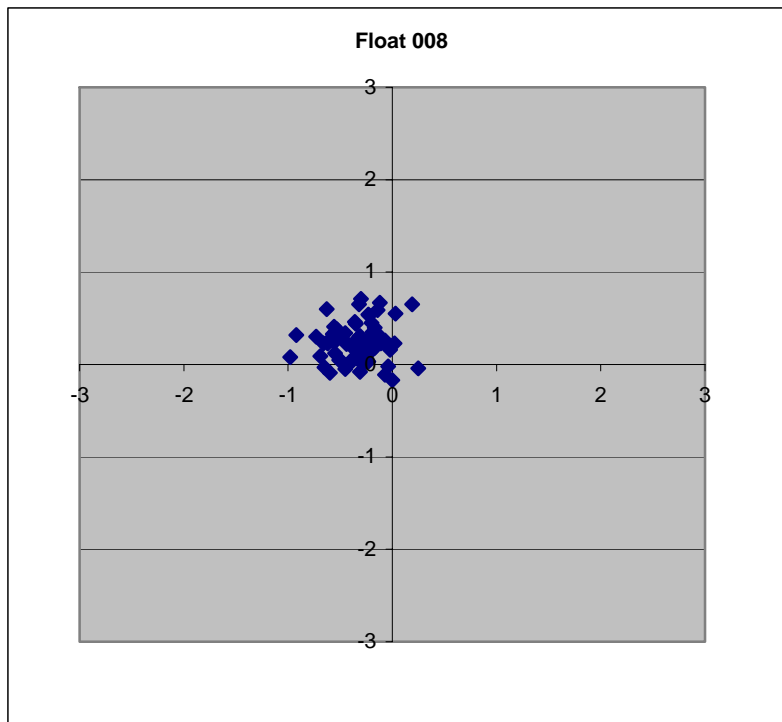


Figure 4: A typical data sample for a unit

IV. Gyro Calibration

M/V Western Trident is fitted with two gyro compasses of type SR-180 MK1, a main survey gyro and a secondary gyro for comparison and backup use. TRINAV GPS is used to determine the heading vector, for comparison with the Gyro headings. This utilises the standard vessel receiver as described above and a second MX 9400 receiver. The second receiver's antenna is mounted 17.3 m ahead of the primary receiver's, with the minimum practicable difference in height. The positions of all antennas used in the Gyro calibration process are determined during a high precision Offset Measurement Survey, performed by an independent contractor, whilst the Vessel is in dock or alongside.

Method used

Refer to **WesternGeco's Navigation systems – a Technical Introduction**, Gyro Calibrations section.

Results

Results from RT Calib are available in several formats, both graphical and tabular. Figure 5 is an example of the QC plot created for each sequence to monitor the Gyro performance. Figure 6 shows the average C-O for each of the gyros in graphical form for all the sequences acquired.

Numerical results for RT Calib are shown in chapter VII.

Section 4: Navigation

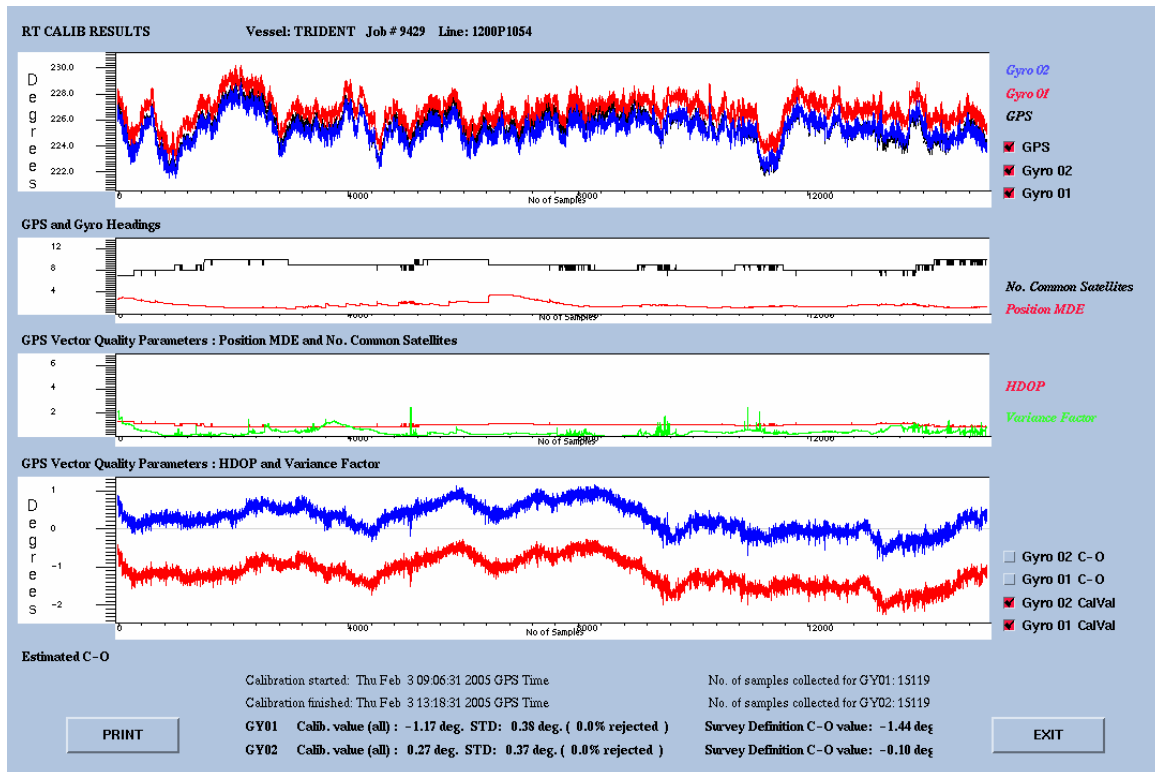


Figure 5: Example of rtcalib plot for a single sequence

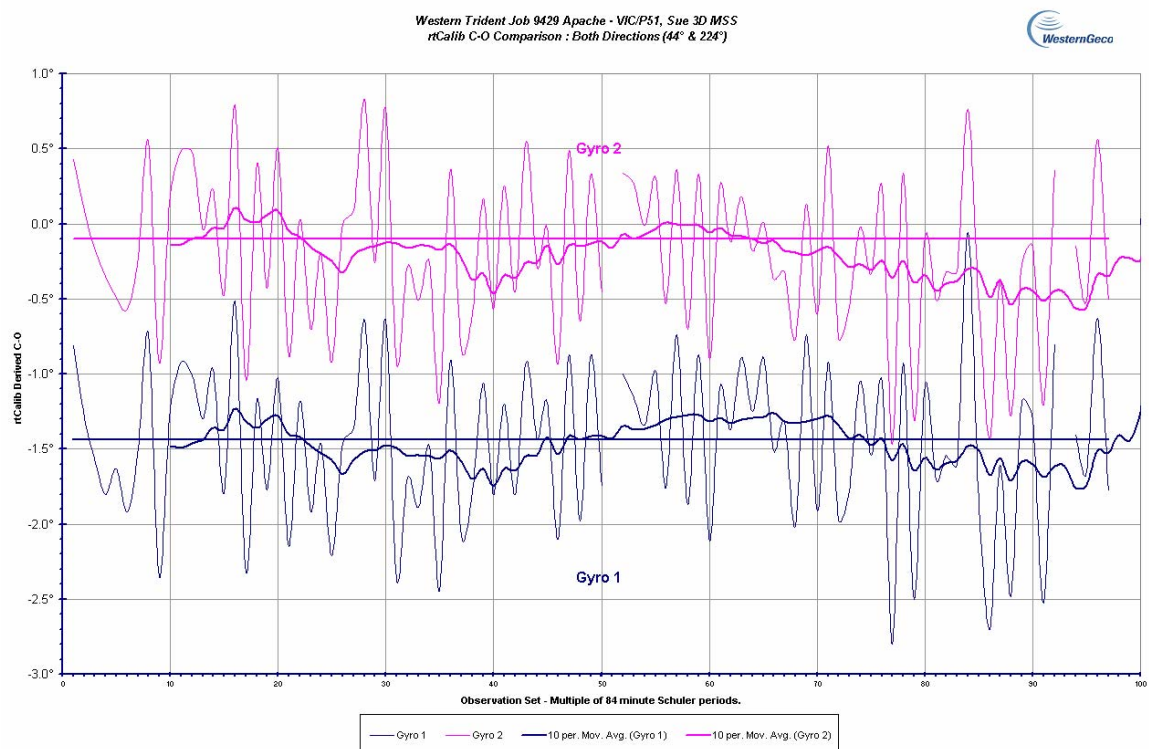


Figure 6: Gyro Calib Trends

V. Conclusions and Comments on Data Quality

The primary gyro calibration value computed from the previous survey and used for this survey agrees well with the offshore calibration results of this survey (as seen in the numerical results in chapter VII).

The re-radiation tests conducted at the start of the job showed no significant deviations thus confirming performance of individual rGPS units.

The GPS positions throughout the survey were reliable and in good agreement with one another (figure 7) with the exception of MultiFix which had intermittent equipment fault during the survey period. MultiFix was not used in the Primary the estimator.

VI. Secondary & Tertiary DGPS System Differences to TRINAV GPS

The following table contains a summary of the statistics taken from the diagnostics files and derived from the data logged by rtDisplay.

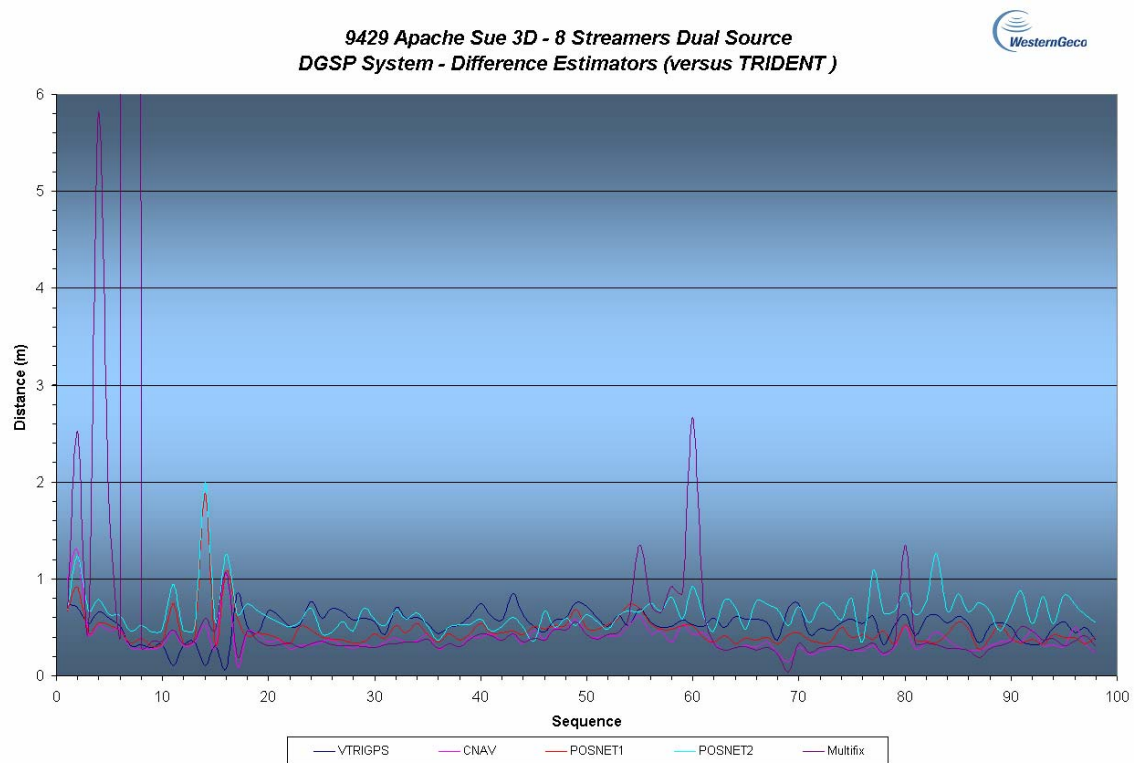


Figure 7: Differences between GPS systems during the survey

VII. Line by Line Results from RT Calib for Gyros and Integrity Monitor

Available Gyros: GY01 Surveydef Corr: -1.44 deg

GY02 Surveydef Corr: -0.10 deg

Gyro Calibration Results:

Western Trident Job 9429 Apache Sue 3D MSS
rtCalib C-O Comparison : Both Directions (44° & 224°)

Line Name		C-O [deg]	Std [deg]	No. samp.		C-O [deg]	Std [deg]	No. samp
1536P1001	GY01	-0.81	1.45	4441	GY02	0.43	1.44	4441
1808P1002	GY01	-1.29	0.57	3979	GY02	0.09	0.7	4194
1824P1003	GY01	-1.56	0.51	5039	GY02	-0.16	0.51	5039
1552P1004	GY01	-1.8	0.59	5035	GY02	-0.35	0.6	5035
1840P1005	GY01	-1.63	0.36	4178	GY02	-0.49	0.49	4590
1568P1006	GY01	-1.92	0.28	5038	GY02	-0.57	0.26	5038
1856P1007	GY01	-1.49	0.13	5034	GY02	-0.21	0.12	5034
1584P1008	GY01	-0.73	0.57	5038	GY02	0.55	0.61	5037
1872P1009	GY01	-2.35	0.27	5038	GY02	-0.93	0.28	5038
1600P1010	GY01	-1.24	0.55	4962	GY02	0.19	0.58	4978
1888P1011	GY01	-0.92	0.49	5039	GY02	0.49	0.49	5039
1616P1012	GY01	-1.01	0.23	5039	GY02	0.48	0.23	5039
1904P1013	GY01	-1.3	0.27	5033	GY02	-0.04	0.27	5033
1632P1014	GY01	-0.97	0.4	5037	GY02	0.23	0.39	5037
1920P1015	GY01	-1.79	0.33	5036	GY02	-0.47	0.34	5036
1648P1016	GY01	-0.52	0.46	5039	GY02	0.79	0.46	5039
1936P1017	GY01	-2.32	0.4	5038	GY02	-1.04	0.43	5038
1664P1018	GY01	-1.17	0.58	5031	GY02	0.4	0.59	5032
1680P1019	GY01	-1.77	0.98	5037	GY02	-0.43	1	5037
1952P1020	GY01	-1.03	0.42	5038	GY02	0.5	0.45	5038
1696P1021	GY01	-2.15	0.69	4781	GY02	-0.88	0.71	5039
1968P1022	GY01	-1.18	0.3	5036	GY02	0.03	0.31	5036
1712P1023	GY01	-1.92	0.25	5038	GY02	-0.7	0.24	5038
2080P1024	GY01	-1.46	0.46	5038	GY02	-0.19	0.45	5038
1792P1025	GY01	-2.21	0.7	5020	GY02	-0.92	0.72	5040
1984P1026	GY01	-1.46	0.3	5038	GY02	0	0.31	5038
1776P1027	GY01	-1.36	0.53	5033	GY02	0.09	0.54	5033
2000P1028	GY01	-0.64	0.56	5039	GY02	0.83	0.56	5039
1520P1029	GY01	-1.71	0.54	5038	GY02	-0.26	0.54	5038
1280P1030	GY01	-0.64	0.33	5041	GY02	0.77	0.32	5041
1504P1031	GY01	-2.37	0.42	5039	GY02	-0.93	0.41	5041
1264P1032	GY01	-1.69	0.24	5041	GY02	-0.28	0.24	5041
1488P1033	GY01	-1.89	0.42	5032	GY02	-0.51	0.43	5032
1248P1034	GY01	-1.48	1.2	5036	GY02	-0.26	1.18	5036
1472P1035	GY01	-2.44	0.35	5038	GY02	-1.19	0.3	5039
1232P1036	GY01	-0.91	0.43	5041	GY02	0.36	0.41	5041
1456P1037	GY01	-2.08	0.68	5038	GY02	-0.84	0.61	5038
1456P1037	GY01	-1.78	0.39	5117	GY02	-0.59	0.41	5117
1296P1038	GY01	-1.06	0.51	4939	GY02	0.17	0.49	4939
1440P1039	GY01	-1.8	0.48	5056	GY02	-0.57	0.49	5056
1216P1040	GY01	-1.2	0.62	3757	GY02	0.25	0.7	4995
1728P1041	GY01	-1.8	0.48	5091	GY02	-0.45	0.48	5116
2000J1042	GY01	-0.92	0.5	5115	GY02	0.55	0.49	5115
1760P1045	GY01	-1.43	0.38	5114	GY02	-0.29	0.38	5114
2032P1046	GY01	-1.19	0.27	5118	GY02	-0.03	0.27	5118
1760J1047	GY01	-2.1	0.48	4890	GY02	-0.93	0.51	5112
2048P1048	GY01	-0.87	0.44	5117	GY02	0.49	0.43	5117
1424P1049	GY01	-1.98	0.8	4982	GY02	-0.65	0.79	5107
2064P1050	GY01	-0.87	0.78	3648	GY02	0.33	0.88	3648

Section 4: Navigation

Line Name		C-O [deg]	Std [deg]	No. samp.		C-O [deg]	Std [deg]	No. samp.
1680A1051	GY01	-1.75	0.67	5947	GY02	-0.46	0.67	5964
1200P1053	GY01	-1	0.53	5117	GY02	0.34	0.5	5117
1200P1054	GY01	-1.16	0.36	5119	GY02	0.27	0.34	5119
1392P1055	GY01	-1.34	0.57	5113	GY02	-0.01	0.58	5113
1184P1056	GY01	-0.98	0.49	5118	GY02	0.31	0.47	5118
1376P1057	GY01	-1.76	0.4	5108	GY02	-0.53	0.41	5108
1168P1058	GY01	-0.74	0.41	5113	GY02	0.36	0.43	5113
1360P1059	GY01	-1.87	0.41	4654	GY02	-0.7	0.43	4654
1152P1060	GY01	-0.87	0.67	5104	GY02	0.33	0.66	5070
1344P1061	GY01	-2.11	0.46	4433	GY02	-0.9	0.45	4506
1136P1062	GY01	-1.09	0.55	4830	GY02	0.25	0.51	4830
1328P1063	GY01	-1.37	0.8	4544	GY02	-0.12	0.78	4544
1120P1064	GY01	-0.89	0.53	5113	GY02	0.18	0.52	5113
1312P1065	GY01	-1.25	0.78	4327	GY02	-0.18	0.82	4365
1104P1066	GY01	-0.89	0.47	5114	GY02	0.01	0.47	5114
1056P1067	GY01	-1.51	0.47	5112	GY02	-0.37	0.47	5112
1088P1068	GY01	-1.32	0.34	5119	GY02	-0.32	0.37	5119
1072P1069	GY01	-2.01	0.39	5109	GY02	-0.77	0.41	5109
1104A1070	GY01	-0.74	0.75	8754	GY02	0.13	0.77	8771
1040P1071	GY01	-1.91	0.44	7373	GY02	-0.6	0.43	7453
1296A1072	GY01	-0.92	0.29	690	GY02	0.52	0.3	690
1024P1073	GY01	-1.96	0.42	7486	GY02	-0.75	0.43	7486
1008P1074	GY01	-1.78	0.6	6407	GY02	-0.55	0.5	6407
2064J1075	GY01	-1.05	0.63	4865	GY02	-0.02	0.62	4866
2224P1076	GY01	-1.54	0.68	2879	GY02	-0.33	0.69	2879
2096P1077	GY01	-1.06	0.4	6396	GY02	0.24	0.42	6396
2208P1078	GY01	-2.8	0.33	3191	GY02	-1.47	0.31	3191
2112P1079	GY01	-0.93	0.34	5032	GY02	0.34	0.31	5032
2192P1080	GY01	-2.5	0.34	3209	GY02	-1.31	0.37	3209
2128P1081	GY01	-1.07	0.22	4342	GY02	-0.08	0.27	4342
1488A1082	GY01	-1.7	0.52	4613	GY02	-0.51	0.51	4613
2064A1083	GY01	-1.54	0.18	1692	GY02	-0.32	0.19	1692
2176P1084	GY01	-1.61	0.35	4016	GY02	-0.32	0.35	4016
2144P1085	GY01	-0.06	1.51	4149	GY02	0.76	1.37	4006
1408A1086	GY01	-1.86	0.5	1305	GY02	-0.54	0.45	1305
1440A1087	GY01	-2.7	0.21	1365	GY02	-1.44	0.21	1365
1984J1088	GY01	-1.61	0.71	5039	GY02	-0.37	0.68	5039
2160P1089	GY01	-2.48	0.49	4319	GY02	-1.28	0.49	4319
2144J1090	GY01	-1.18	0.48	5027	GY02	-0.27	0.48	5027
1632U1091	GY01	-1.3	0.51	5027	GY02	-0.15	0.45	5037
1744U1092	GY01	-2.52	0.64	5039	GY02	-1.2	0.58	5039
1632U2093	GY01	-0.8	0.65	5033	GY02	0.36	0.64	5033
1632U3095	GY01	-1.41	0.27	5031	GY02	-0.15	0.28	5031
1744U3096	GY01	-1.65	0.22	5039	GY02	-0.51	0.22	5039
1632U4097	GY01	-0.63	0.65	5041	GY02	0.56	0.64	5041
1744U4098	GY01	-1.78	0.31	5039	GY02	-0.51	0.32	5039

	C-O	SD	Min	Max
Gyro 1	-1.47°	0.55°	-2.80°	-0.06°
Gyro 2	-0.20°	0.55°	-1.47°	0.83°

	C-O used in survey	Difference
Gyro 1	-1.44°	0.03°
Gyro 2	-0.10°	0.10°

Section 4: Navigation

GPS Integrity Monitor Results:

Job 9429, APACHE Sue 3D MSS

Line Name	No. of Minutes	Start hdg.	End hdg.	C-O Northing	Std [deg]	No. samp.	%Rej	C-O Easting	Std [deg]	No. samp.	%Rej
No Data											
1808P1002	311	47	45	1.41	2.03	6003	3.9	0.71	1.48	6003	7.9
1824P1003	266	44	36	0.95	0.99	5290	5	-0.24	0.95	5290	4
1552P1004	291	226	224	0.52	1.61	5774	4.3	0.92	1.02	5774	6.2
1840P1005	285	43	44	0.96	1.46	5634	2.9	-0.30	1.07	5634	4.3
1568P1006	276	225	225	0.56	1.02	5509	6.9	0.14	1.06	5509	3.4
1856P1007	262	45	53	1.37	0.57	5189	4.2	0.54	0.39	5189	3.3
1584P1008	278	218	228	0.59	0.62	5491	4.4	0.09	0.39	5491	1.9
1872P1009	294	45	49	1.25	0.70	5868	2.5	0.40	0.39	5868	5.3
1600P1010	308	227	227	0.76	0.43	6121	4.3	0.59	0.29	6121	5.7
1888P1011	340	48	45	0.83	0.59	6723	4.4	0.35	0.53	6723	5.7
1616P1012	95	230	228	1.11	0.33	1834	3.1	0.47	0.36	1834	4.4
No Data											
No Data											
No Data											
1648P1016	115	233	228	0.59	0.87	2268	5.7	0.44	0.47	2268	3.5
1936P1017	290	46	50	1.00	0.62	5716	2.9	0.62	0.52	5716	3.3
1664P1018	297	219	234	0.64	0.78	5769	2.0	0.45	0.37	5769	2.1
1680P1019	301	52	47	0.90	0.73	5860	4.9	0.24	0.44	5860	6.8
1952P1020	302	228	223	1.14	1.03	5910	6.3	0.51	0.57	5910	4.3
1696P1021	335	50	40	1.25	0.56	6577	2.3	0.25	0.43	6577	3.2
1968P1022	298	227	222	0.74	0.58	5951	4.9	0.22	0.37	5951	5.7
1712P1023	295	47	48	1.17	0.69	5871	7.2	0.42	0.59	5871	5.0
2080P1024	97	226	227	0.74	0.86	1945	3.0	0.47	0.45	1945	0.1
1792P1025	284	40	44	1.04	0.54	5652	5.4	-0.08	0.38	5652	4.5
1984P1026	269	217	224	0.95	0.91	5362	2.8	0.80	0.47	5362	3.2
1776P1027	307	48	46	0.79	0.64	6105	5.1	0.09	0.56	6105	2.2
2000P1028	280	223	226	0.77	0.77	5606	4.9	0.57	0.57	5606	4.8
1520P1029	282	48	45	1.22	0.62	5635	6.2	0.67	0.50	5635	1.4
1280P1030	262	223	226	0.71	0.98	5243	6.2	0.26	0.33	5243	5.7
1504P1031	323	49	41	1.45	0.50	5822	5.6	0.27	0.38	5822	3.8
1264P1032	291	227	221	0.71	0.97	3937	2.7	-0.22	0.51	3937	1.9
1488P1033	288	50	47	1.43	0.98	4399	7.0	0.67	0.78	4399	4.5
1248P1034	270	223	226	0.37	0.75	5356	3.6	0.10	0.56	5356	3.9
1472P1035	309	48	42	1.40	0.67	6178	7.0	0.42	0.37	6178	2.9
1232P1036	295	226	222	0.58	0.52	5876	8.8	0.44	0.45	5876	1.2
1456P1037	266	45	45	1.27	0.41	5280	4.8	0.45	0.43	5280	3.5
1296P1038	259	225	228	0.61	0.56	5173	4.3	0.44	0.69	5173	3.5
1440P1039	261	46	47	1.12	0.73	5191	1.6	0.70	0.45	5191	4.7
1216P1040	268	221	228	0.43	0.89	5316	5.0	0.27	0.46	5316	4.8
1728P1041	301	44	50	1.62	0.90	5939	2.8	0.81	0.62	5939	7.5
2000J1042	326	226	225	0.59	0.76	6507	4.6	0.37	0.49	6507	3.1
1744P1043	308	56	50	0.95	1.00	6125	1.9	0.61	0.54	6125	3.5
2016P1044	275	221	224	0.79	0.64	5482	5.7	0.53	0.37	5482	5.1
1760P1045	288	44	41	1.22	0.53	5726	5.3	0.25	0.50	5726	5.6
2032P1046	276	216	220	0.72	0.55	5500	5.0	0.53	0.42	5500	2.4
1760J1047	290	46	43	1.29	0.45	5770	4.3	0.28	0.33	5770	3.7
2048P1048	277	229	227	0.67	0.70	5517	4.3	0.13	0.34	5517	6.4
1424P1049	269	45	49	1.82	0.88	5357	6.5	0.58	0.47	5357	4.3
2064P1050	316	228	223	0.67	0.57	6304	5.3	0.42	0.44	6304	4.2
1680A1051	109	48	49	0.21	1.24	2184	4.0	0.33	0.36	2184	10.3
1712A1052	6	46	48	1.86	0.09	122	0.8	-0.38	0.08	122	4.1
1200P1053	270	216	212	0.56	0.53	5391	6.4	-0.05	0.66	5391	4.8
1200P1054	273	228	226	0.77	0.41	5262	3.4	0.54	0.24	5262	3.9
1392P1055	311	44	45	1.09	0.65	5974	3.4	0.54	0.43	5974	3.7
1184P1056	267	229	224	0.91	0.52	5275	3.8	0.38	0.35	5275	4.5
1376P1057	292	45	42	1.08	0.51	5832	5.3	0.30	0.32	5832	5.6
1168P1058	278	228	227	0.80	0.43	5485	3.8	0.34	0.30	5485	7.9
1360P1059	254	44	43	1.27	0.51	5068	6.1	0.23	0.39	5068	2.5
1152P1060	269	225	231	0.44	0.69	5363	3.2	0.04	0.48	5363	4.1

Section 4: Navigation

Job 9429, APACHE Sue 3D MSS

Line Name	No. of Minutes	Start hdg.	End hdg.	C-O Northing	Std [deg]	No. samp.	%Rej	C-O Easting	Std [deg]	No. samp.	%Rej
1344P1061	252	43	42	1.17	0.45	5002	3.2	0.32	0.32	5002	4.0
1136P1062	286	230	231	0.85	0.57	5712	4.0	0.56	0.32	5712	2.9
1328P1063	252	43	48	1.13	0.64	4973	3.9	0.34	0.51	4973	2.2
1120P1064	276	220	226	0.74	0.57	5501	3.1	0.55	0.52	5501	4.3
1312P1065	249	45	45	1.18	0.45	4961	5.2	0.34	0.53	4961	6.0
1104P1066	277	229	226	0.70	0.56	5543	4.3	0.59	0.53	5543	3.3
1056P1067	266	42	80	1.03	0.81	5069	6.3	-0.01	0.57	5069	4.1
1088P1068	302	229	220	0.53	0.38	5997	5.9	0.35	0.30	5997	3.9
1072P1069	263	42	82	1.13	0.83	5003	3.2	0.34	0.47	5003	5.0
1104A1070	158	228	225	1.22	0.85	2975	4.7	0.52	0.51	2975	4.8
1040P1071	136	46	77	1.21	0.54	2633	5.4	0.37	0.51	2633	4.4
1296A1072	21	229	228	0.41	0.35	428	1.2	1.07	0.40	428	0.0
1024P1073	135	45	157	1.42	0.56	2597	3.1	0.46	0.37	2597	5.7
1008P1074	117	45	88	1.68	0.88	2303	5.4	0.35	0.48	2303	4.5
2064J1075	276	224	231	0.73	0.53	5462	4.1	0.45	0.53	5462	7.0
2224P1076	55	43	42	2.47	1.66	635	3.1	0.22	0.97	635	6.6
2096P1077	117	230	228	0.52	0.53	1823	6.6	0.25	0.90	1823	4.3
2208P1078	63	48	51	2.35	0.36	1263	5.9	0.18	0.39	1263	6.0
2112P1079	94	224	228	1.01	0.76	1877	2.8	0.31	0.28	1877	4.7
2192P1080	63	45	49	1.76	1.01	1246	2.6	-0.07	0.45	1246	3.5
2128P1081	82	224	225	0.12	0.59	1459	6.0	0.79	0.35	1459	5.3
1488A1082	87	44	44	0.82	0.67	1443	4.1	0.18	0.56	1443	5.1
2064A1083	38	227	237	1.15	0.20	763	7.7	0.63	0.30	763	0.0
2176P1084	77	47	47	1.68	0.81	1537	4.0	0.64	0.27	1537	5.0
2144P1085	84	229	227	0.57	0.64	1663	7.4	0.05	0.54	1663	2.0
1408A1086	32	50	50	1.63	0.43	622	0.8	0.30	0.25	622	1.0
1440A1087	33	47	46	1.97	0.28	653	8.4	0.62	0.14	653	5.1
1984J1088	330	228	227	0.82	0.67	6546	4.3	0.30	0.45	6546	4.5
2160P1089	82	49	50	0.61	0.67	1620	8.4	-0.22	0.56	1620	7.6
2144J1090	94	225	227	0.22	0.51	1871	3.0	0.03	0.44	1871	6.2
1632U1091	281	227	222	0.89	0.59	5269	5.9	0.33	0.35	5269	4.2
1744U1092	139	42	41	0.73	0.69	2771	2.3	-0.03	0.31	2771	2.1
1632U2093	549	214	56	1.08	0.66	855	3.6	0.30	0.32	855	5.2
1632U3095	176	225	221	0.63	0.69	3524	5.4	0.41	0.32	3524	3.9
1744U3096	157	41	43	1.48	0.30	3135	6.4	0.58	0.36	3135	2.5
1632U4097	185	231	231	1.26	0.66	3678	1.6	0.49	0.52	3678	2.3
1744U4098	120	40	72	1.10	0.47	2391	2.5	0.47	0.27	2391	4.8

Sale Integrity Monitor

Northing				Easting			
Mean		Mean		Mean		Mean	
C-O	SD	Min	Max	C-O	SD	Min	Max
1.00	0.69	0.12	2.5	0.36	0.48	-0.38	1.1

GPS Radial Difference Results

Sequence	Difference Estimators				
	TRIGPS	CNAV	POSNET1	POSNET2	MFIX
1	0.73	0.99	0.67	0.69	
2	0.71	1.29	0.91	1.23	
3	0.54	0.42	0.44	0.68	
4	0.66	0.52	0.55	0.79	
5	0.59	0.47	0.52	0.63	
6	0.51	0.48	0.46	0.62	
7	0.31	0.29	0.34	0.46	
8	0.32	0.27	0.39	0.52	0.29
9	0.29	0.27	0.3	0.45	0.36
10	0.32	0.31	0.34	0.48	0.36
11	0.1	0.46	0.74	0.94	0.47
12	0.31	0.31	0.33	0.47	0.33
13	0.35	0.34	0.37	0.48	0.37
14	0.1	0.53	1.88	2	0.59
15	0.31	0.28	0.32	0.56	0.47
16	0.08	1.05	1.08	1.25	1.06
17	0.85	0.1	0.59	0.64	0.21
18	0.51	0.45	0.41	0.74	0.46
19	0.44	0.42	0.44	0.67	0.36
20	0.67	0.35	0.42	0.6	0.31
21	0.61	0.37	0.38	0.55	0.32
22	0.51	0.27	0.33	0.51	0.34
23	0.53	0.31	0.51	0.56	0.29
24	0.76	0.32	0.47	0.7	0.33
25	0.59	0.35	0.4	0.43	0.36
26	0.7	0.37	0.38	0.45	0.32
27	0.66	0.31	0.37	0.56	0.31
28	0.57	0.28	0.34	0.46	0.31
29	0.59	0.32	0.35	0.7	0.3
30	0.56	0.29	0.43	0.57	0.29
31	0.42	0.35	0.39	0.52	0.32
32	0.71	0.39	0.52	0.68	0.33
33	0.59	0.35	0.44	0.58	0.35
34	0.6	0.36	0.54	0.65	0.35
35	0.54	0.42	0.42	0.51	0.38
36	0.43	0.27	0.35	0.37	0.28
37	0.5	0.33	0.43	0.5	0.33
38	0.53	0.3	0.37	0.53	0.3
39	0.61	0.4	0.43	0.53	0.38
40	0.74	0.4	0.54	0.58	0.43
41	0.62	0.43	0.44	0.46	0.41
42	0.57	0.37	0.44	0.51	0.37
43	0.85	0.43	0.46	0.6	0.43
44	0.63	0.33	0.42	0.51	0.35
45	0.51	0.46	0.51	0.36	0.39
46	0.45	0.38	0.48	0.67	0.37
47	0.57	0.49	0.52	0.5	0.48
48	0.59	0.47	0.52	0.59	0.47
49	0.75	0.58	0.69	0.52	0.56
50	0.72	0.42	0.49	0.63	0.42

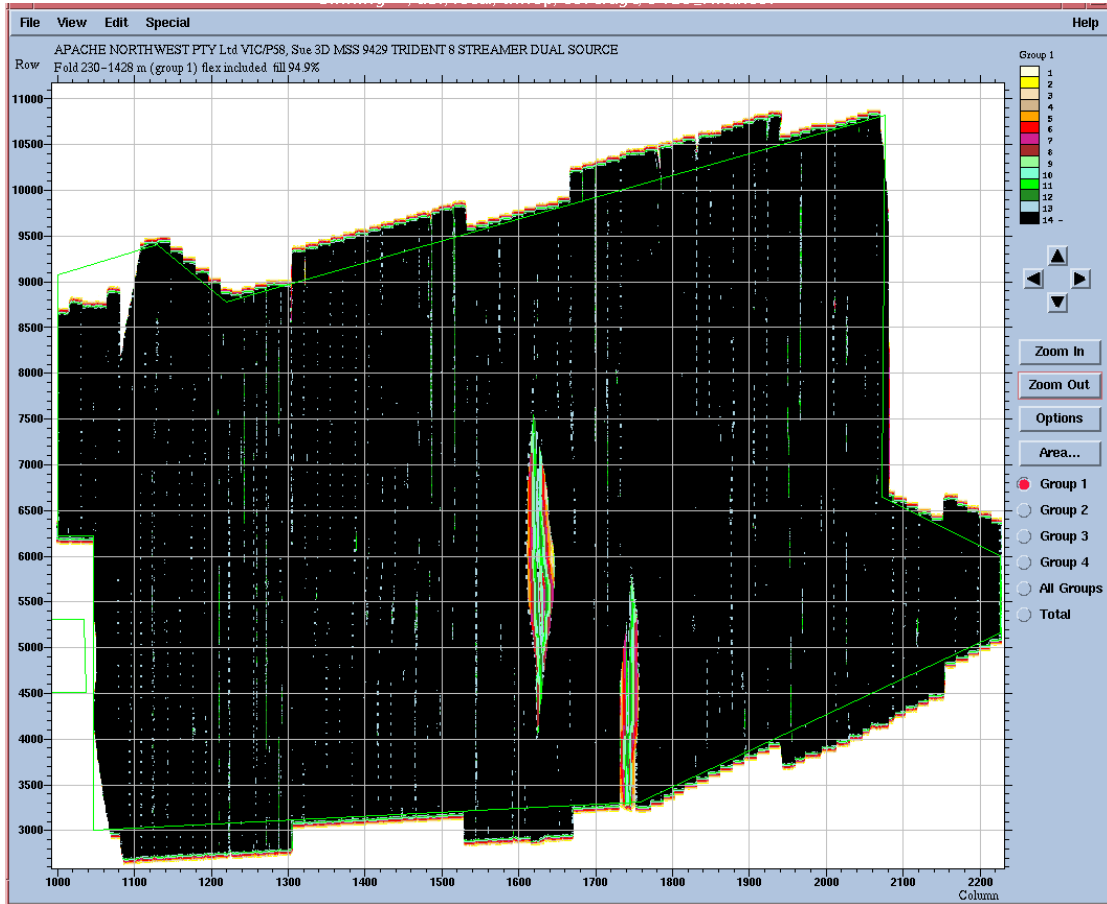
Section 4: Navigation

Difference Estimators					
Sequence	TRIGPS	CNAV	POSNET1	POSNET2	MFIX
51	0.59	0.4	0.48	0.56	0.38
52	0.51	0.41	0.53	0.48	0.42
53	0.62	0.41	0.59	0.62	0.45
54	0.52	0.52	0.73	0.67	0.61
55	0.69	0.61	0.7	0.66	1.35
56	0.56	0.44	0.54	0.74	0.74
57	0.5	0.46	0.48	0.67	0.65
58	0.51	0.35	0.48	0.81	0.92
59	0.57	0.53	0.52	0.58	0.86
60	0.53	0.42	0.52	0.92	2.67
61	0.51	0.44	0.4	0.61	0.7
62	0.59	0.33	0.35	0.46	0.34
63	0.5	0.26	0.41	0.78	0.26
64	0.61	0.29	0.33	0.71	0.29
65	0.58	0.31	0.39	0.48	0.3
66	0.58	0.3	0.37	0.77	0.26
67	0.55	0.35	0.4	0.73	0.29
68	0.37	0.24	0.33	0.69	0.23
69	0.71	0.14	0.42	0.52	0.04
70	0.74	0.29	0.44	0.72	0.33
71	0.42	0.22	0.37	0.55	0.24
72	0.49	0.25	0.34	0.74	0.29
73	0.47	0.28	0.35	0.71	0.3
74	0.55	0.31	0.5	0.57	0.29
75	0.58	0.26	0.4	0.8	0.26
76	0.54	0.25	0.42	0.35	0.29
77	0.61	0.31	0.38	1.09	0.34
78	0.32	0.22	0.46	0.66	0.23
79	0.52	0.29	0.33	0.67	0.33
80	0.63	0.51	0.53	0.86	1.35
81	0.41	0.27	0.37	0.63	0.34
82	0.6	0.36	0.36	0.76	0.34
83	0.63	0.45	0.34	1.26	0.32
84	0.55	0.38	0.43	0.67	0.28
85	0.61	0.29	0.56	0.85	0.28
86	0.55	0.26	0.49	0.66	0.26
87	0.34	0.26	0.27	0.75	0.19
88	0.52	0.31	0.4	0.66	0.28
89	0.55	0.35	0.52	0.46	0.31
90	0.5	0.37	0.39	0.68	0.36
91	0.36	0.35	0.34	0.88	0.51
92	0.32	0.47	0.38	0.54	0.46
93	0.35	0.31	0.32	0.82	0.37
94	0.49	0.32	0.42	0.54	0.39
95	0.56	0.3	0.4	0.83	0.31
96	0.44	0.5	0.4	0.73	0.36
97	0.5	0.33	0.33	0.63	0.41
98	0.37	0.23	0.41	0.55	0.3
Average	0.53	0.38	0.46	0.66	0.42
SD	0.14	0.16	0.19	0.22	0.32

Exhibit 4 : Coverage Maps

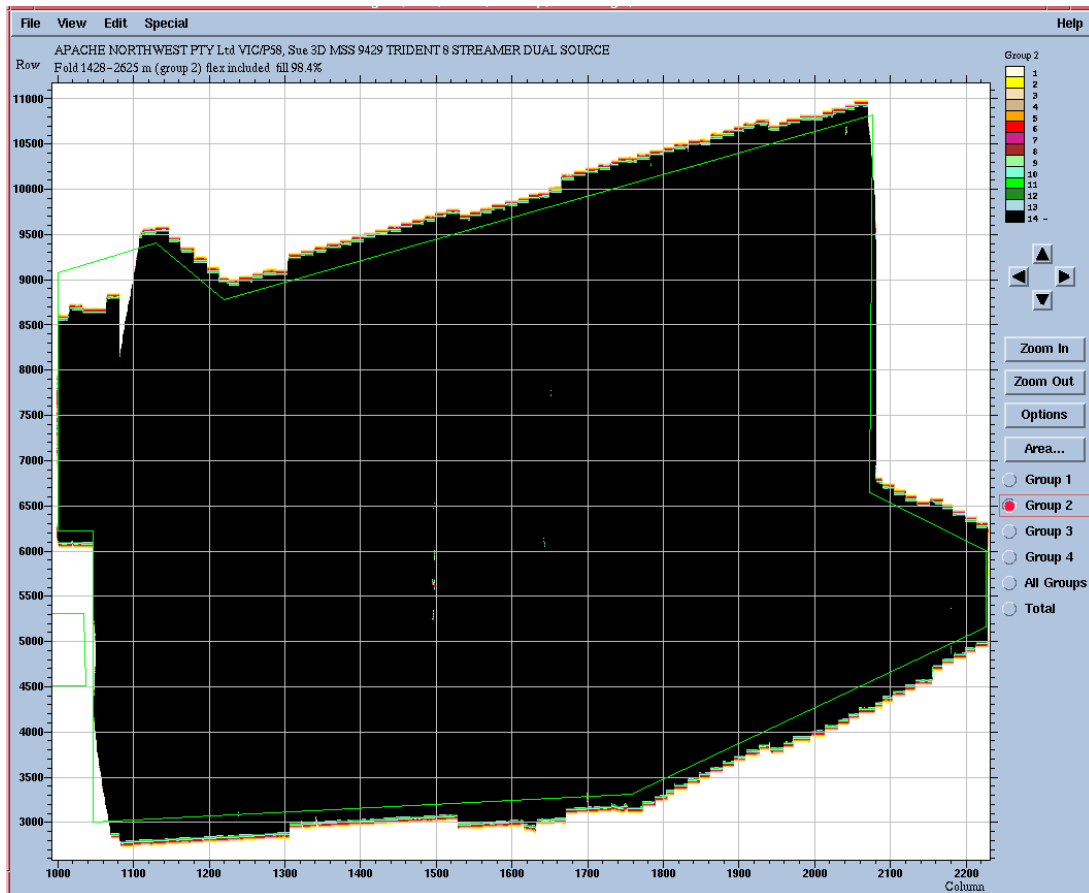
Final flex parameters are a stepped expansion from 100% to 400% bin width i.e. bin width tapering from 50m wide at the head of the cable to 125m wide at the tail:

Group	bin width at head	bin width at tail	per side expansion
1	50.0	62.5	18.75
2	62.5	75.0	25.00
3	75.0	87.5	31.25
4	87.5	125.0	50.00

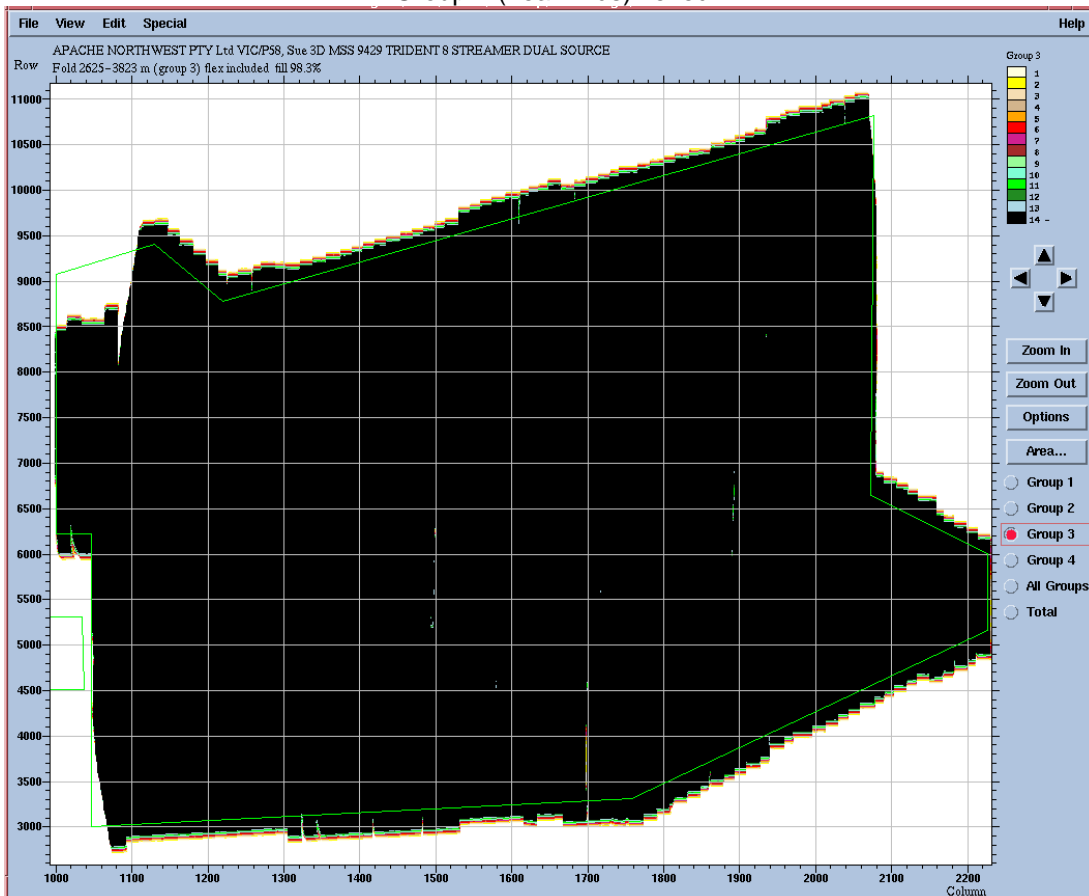


Group 1 (nears) flex included

Section 4: Navigation

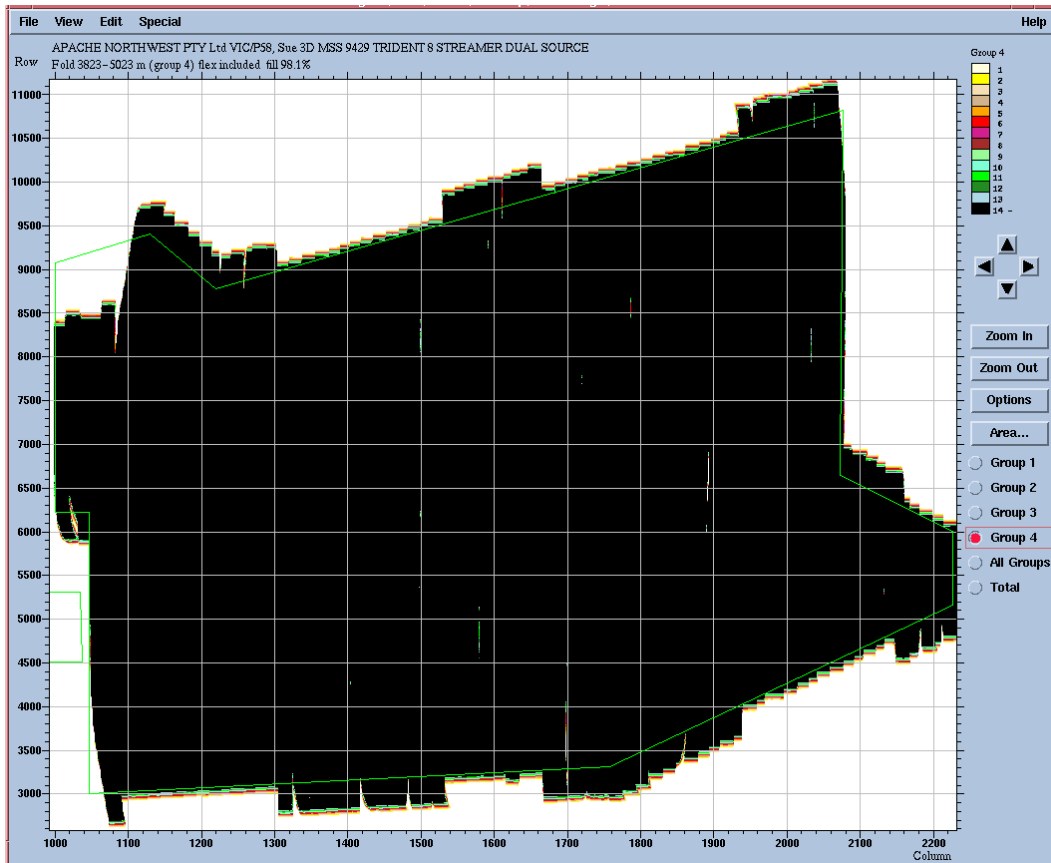


Group 2 (near mids) flexed

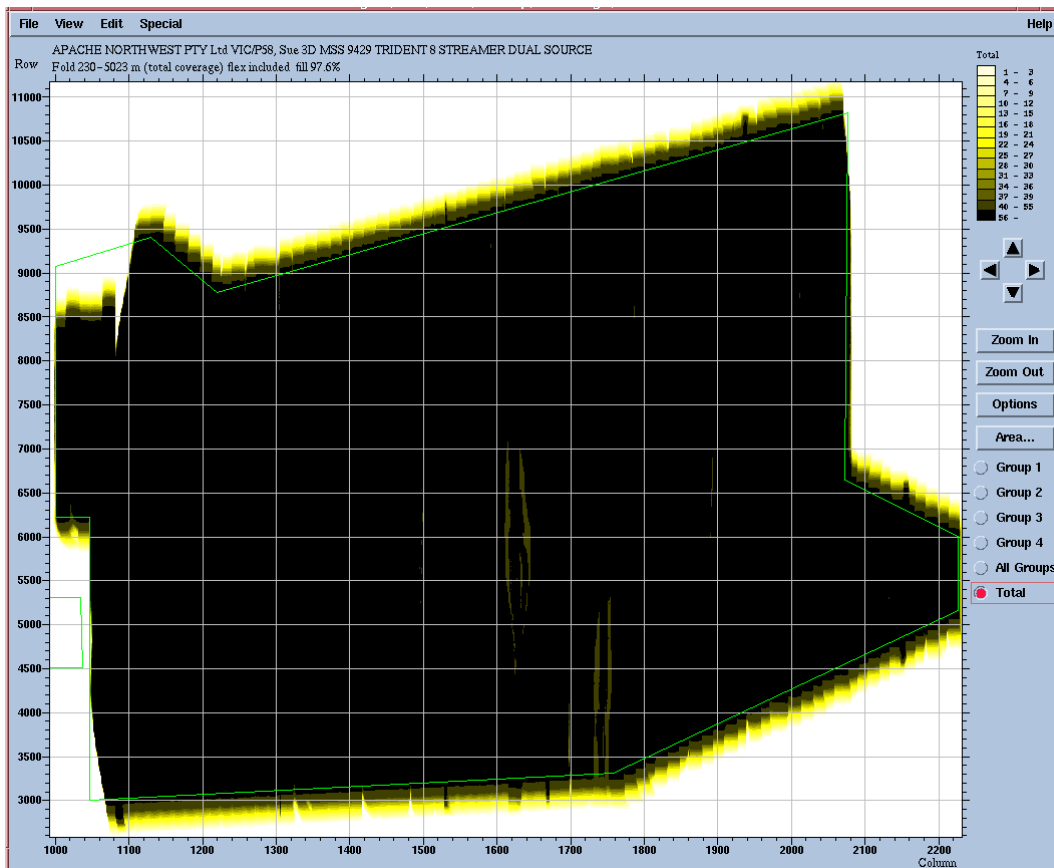


Group 3 (far mids) flexed

Section 4: Navigation

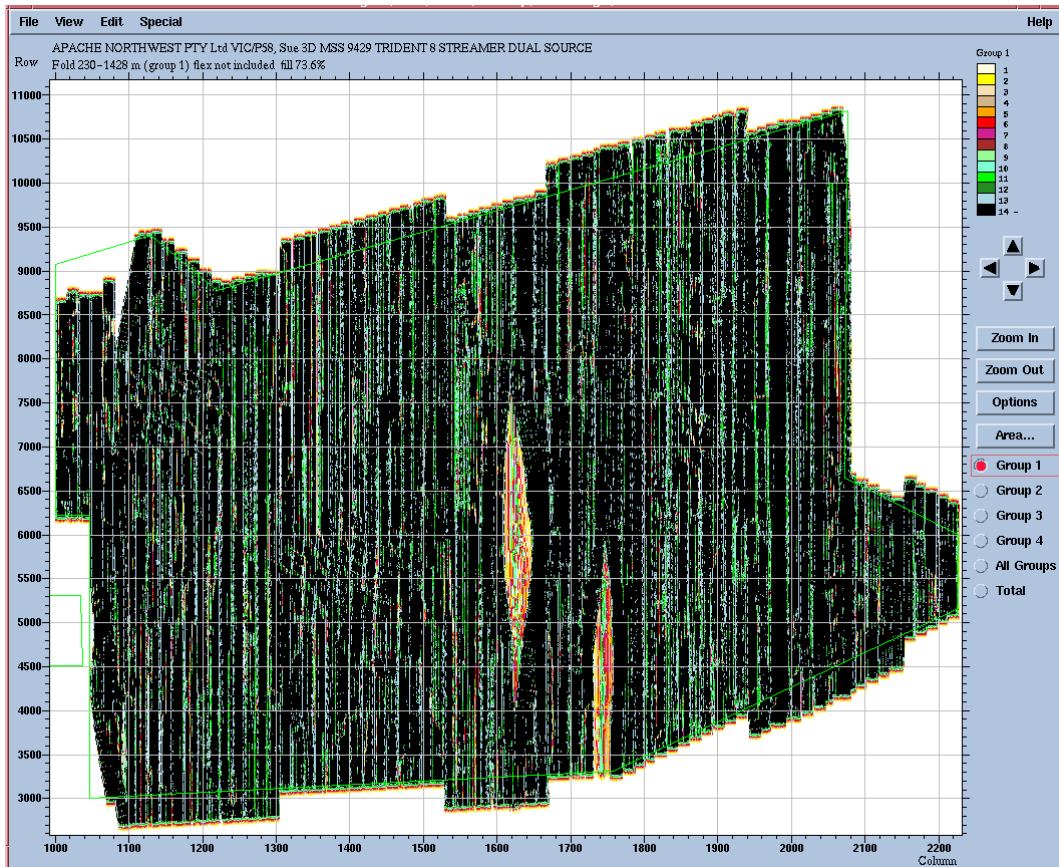


Group 4 (fars) flexed

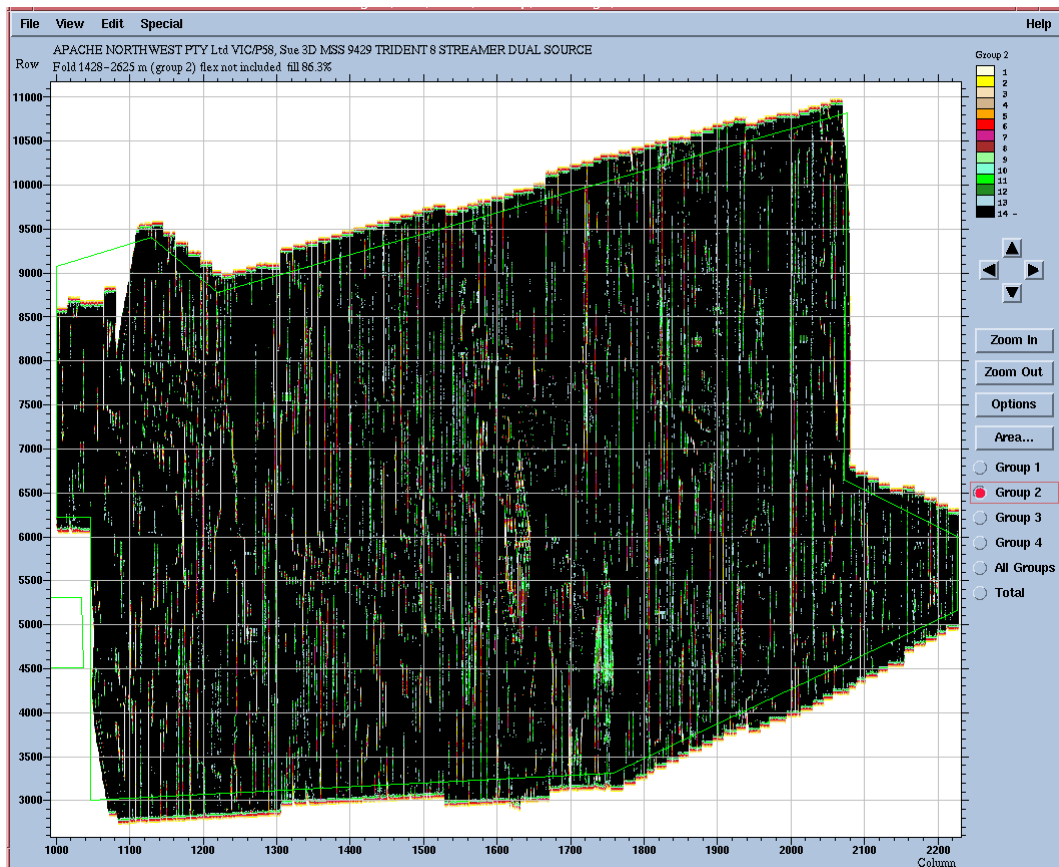


Total cable flexed

Section 4: Navigation

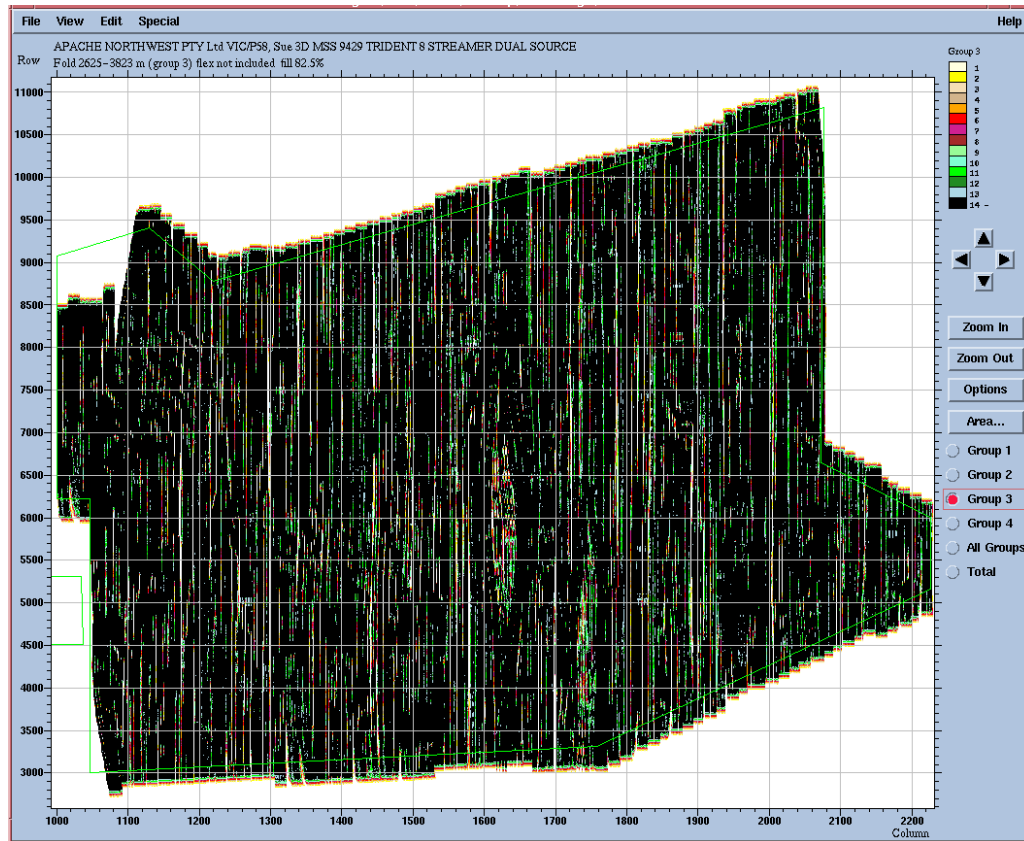


Group 1 (nears) no flex included

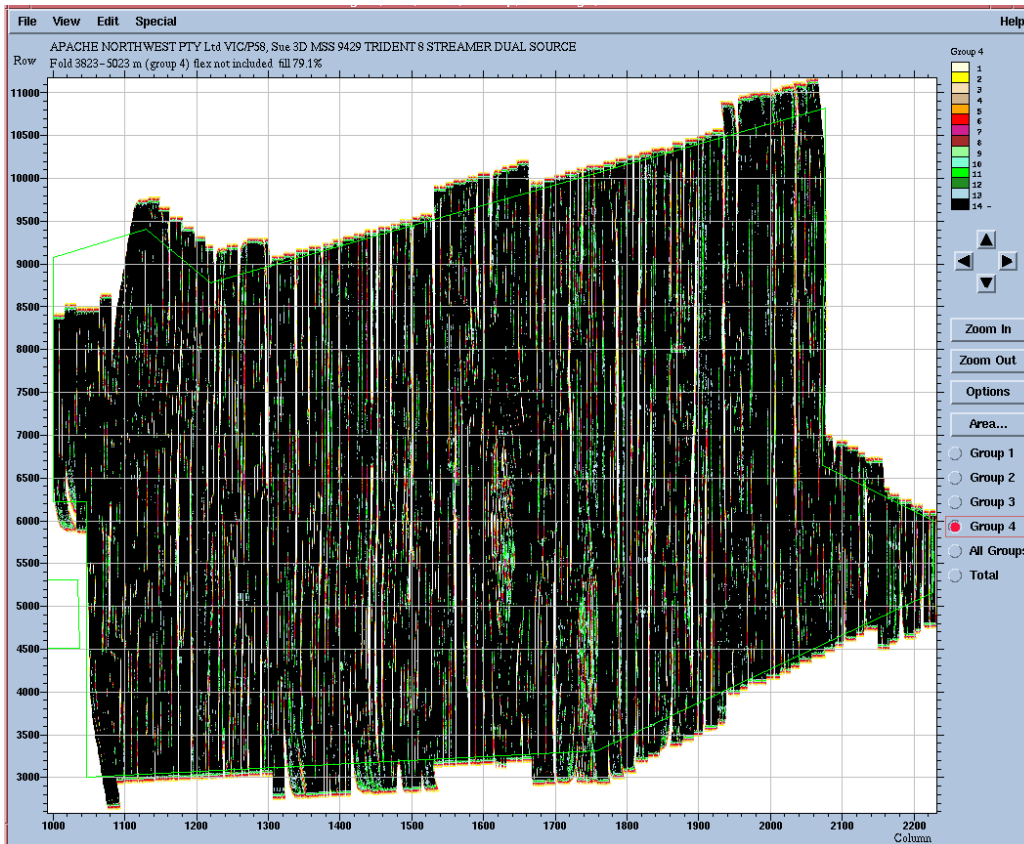


Group 2 (near mids) no flex included

Section 4: Navigation

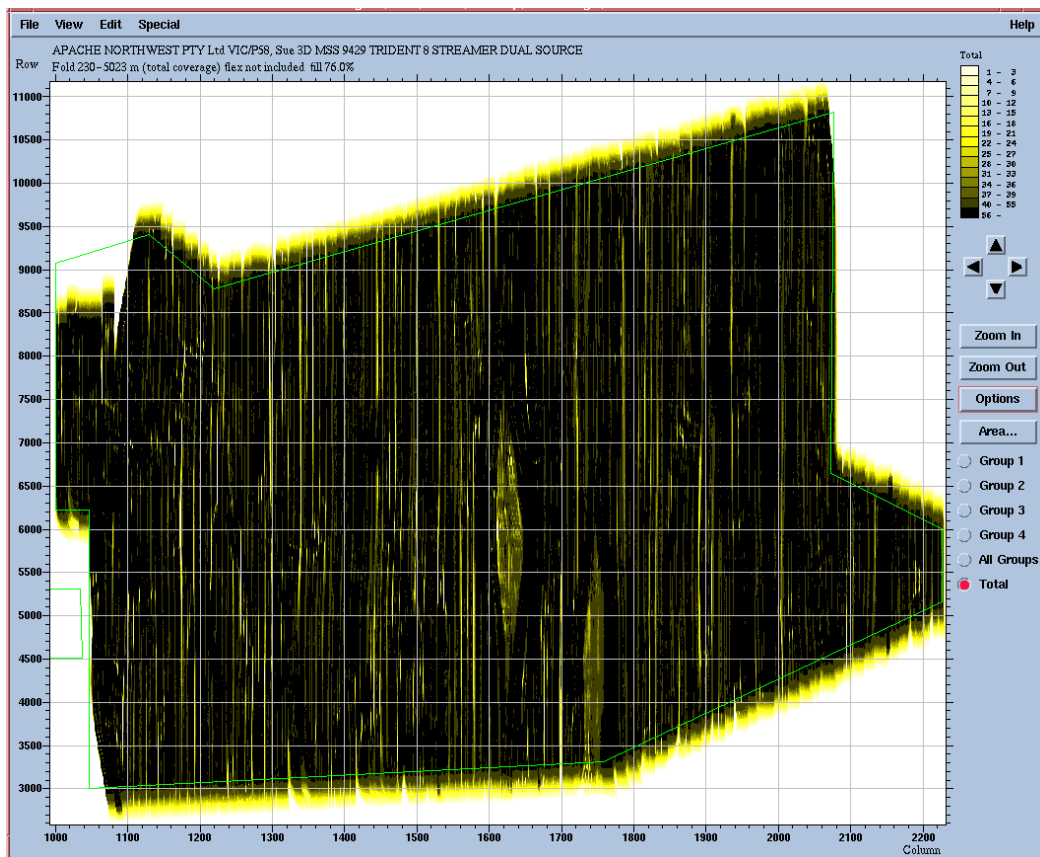


Group 3 (far mids) no flex included



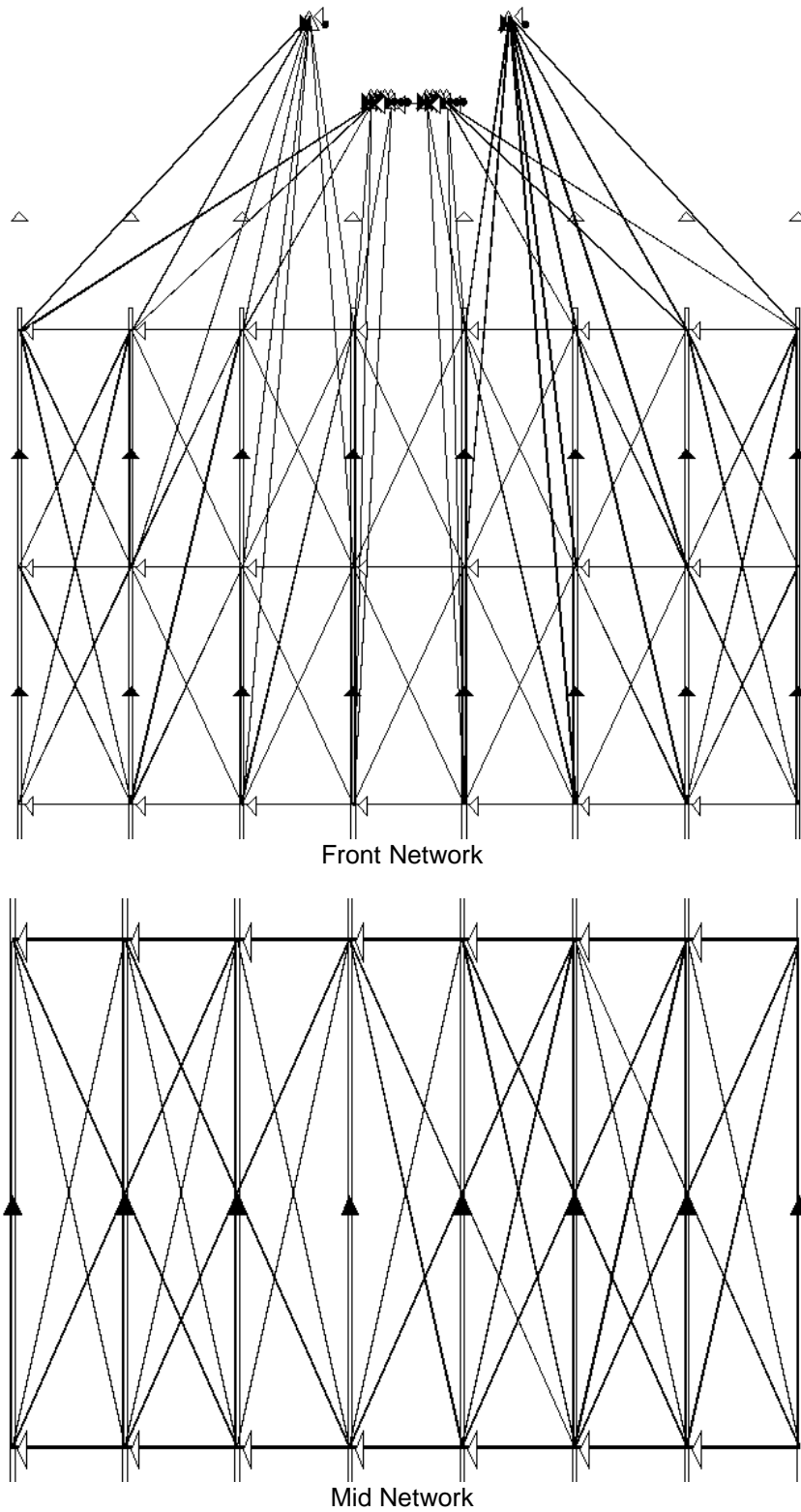
Group 4 (fars) no flex included

Section 4: Navigation



Total cable no flex included

Exhibit 5 : Acoustic Range System



Section 4: Navigation

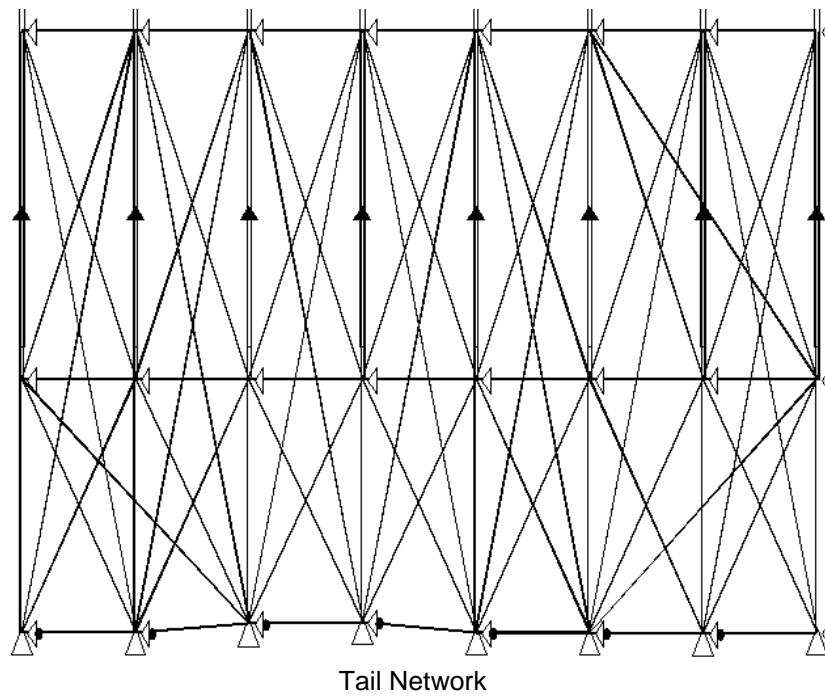


Exhibit 6 : Survey Definition Changes Summary

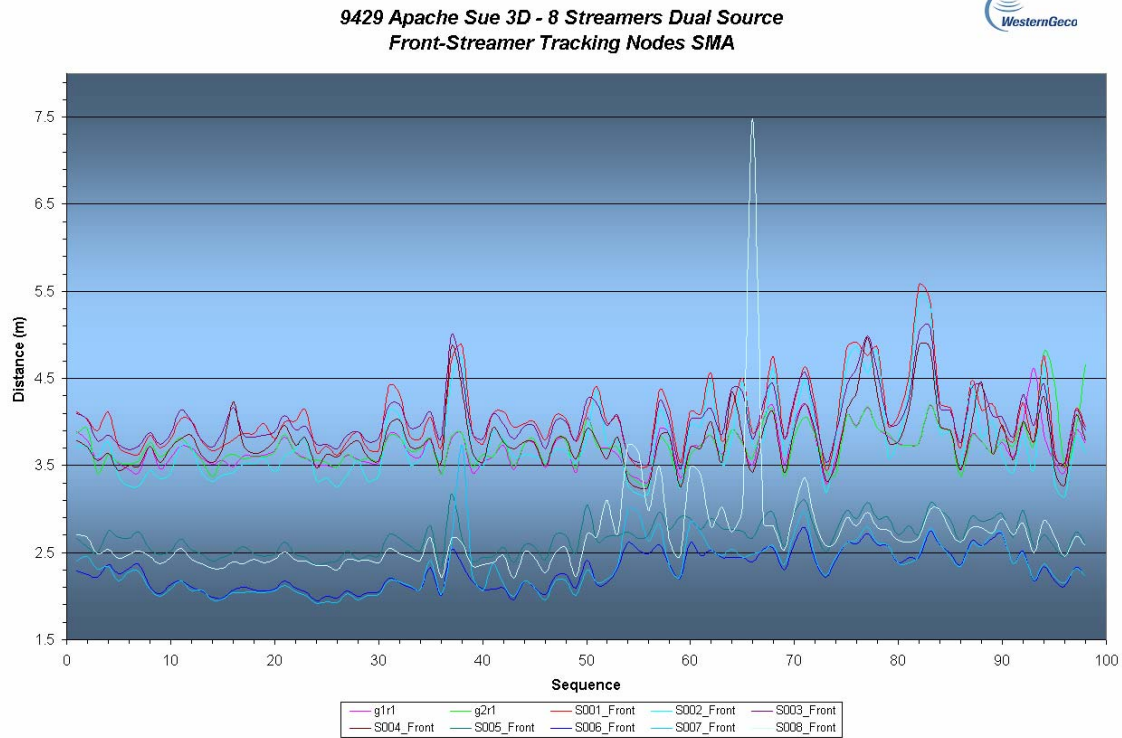
Client Apache Vessel Western Trident

Area Sue Start Date 15th Jan 2005
Job No. 9429 End Date 16th Feb 2005

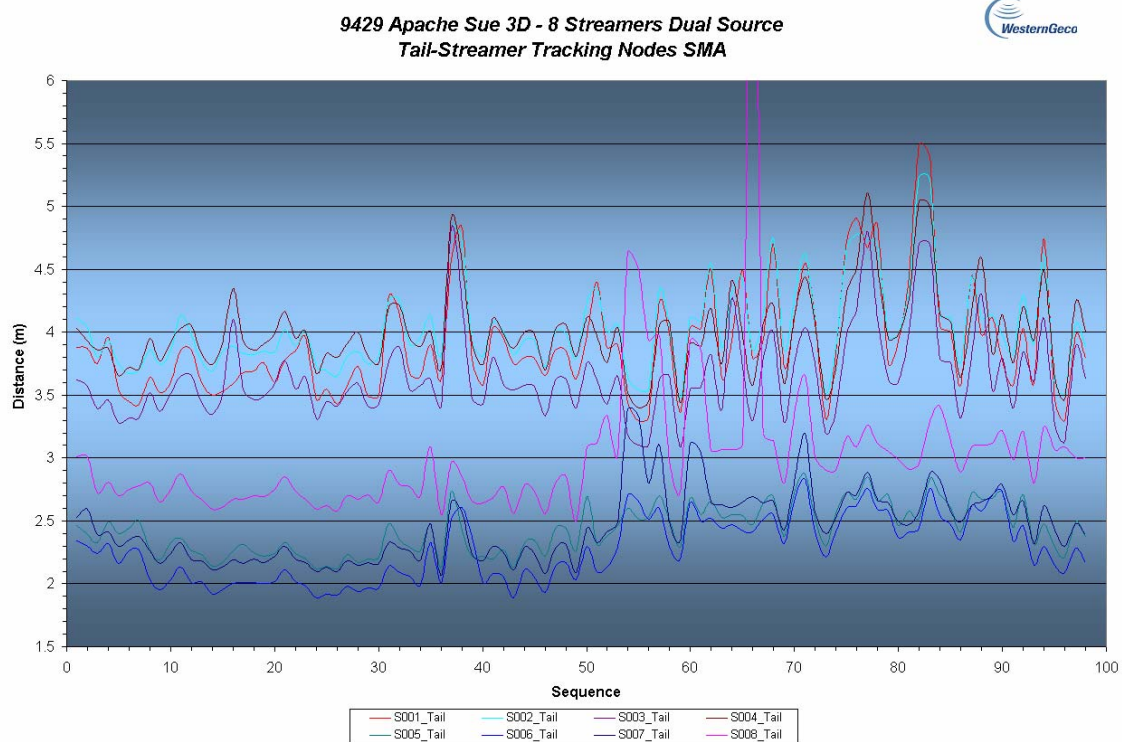
Date	Surdef in use mas9429_	From Seq	To Seq	Offset Database	21. Description
15-Jan-05	01	001	002	01	Start of Survey
16-Jan-05	02	003	007		Recreated Surdef – No Physical Changes
18-Jan-05	03	008	019		New TS-DIP 02 Streamer Depth Was 1516.58 Now 1516.60 Water column Was 1513.55 Now 1516.72 New Bird S3C08 Was 17645 Now 14602
22-Jan-05	04	020	022		New Bird S7C8 was 12750 now 6860 New Bird S7C11 was 9589 now 19997
23-Jan-05	05	023	044		New Bird S7C11 was 19997 now 21073 New Bird S7C10 was 16916 now 17876 New Bird S8C3 was 14138 now 17024
30-Jan-05	06	045	045		New Bird S2C3 was 19864 now 7051
30-Jan-05	07	046	049		New Bird S7C11 was 21073 now 6308
31-Jan-05	08	50	50		Changed order of input for tailbuoys in SSD. FF01 and FF02 now both on Frequency 1. FF01 now coming in on slot 15 rather than slot 4.
1-Feb-05	09	51	52		Adjusted offsets to reflect that the front floats had moved back after the reconfiguration for shallow water and the repair of fairing to correct strumming noise on S003.
2-Feb-05	10	53	56		Changed order of input for tailbuoys in SSD. FF01 and FF02 on separate frequencies, FF01 back on Frequency 2. FF01 now coming in on slot 4 rather than slot 15.
4-Feb-05	11	57	58		New Bird S6C5 14522 (was 19228) and New TS-DIP 03
5-Feb-05	12	59	60		New Bird S1C4 10238 (was 19664)
5-Feb-05	13	61	67		FF02 frequency change, (Reverted to Freq.1)
07-Feb-05	14	66	69		New Bird S9C11 6713 (was 17239)
08-Feb-05	15	70	84		New Bird S1C19 19864 (was 12203) New Bird S8C19 26361 (was 18861)
11-Feb-05	16	85	90		New bird S3C6 14138 (was 17368) New Bird S2C7 6550 (was 19682) New Bird S5C6 19228 (was 14581)
14-Feb-05	17u	91	98		Two boat modifications for undershoot. New Bird S3C2 15337 (was 10082) New Bird S8C3 19668 (was 17024) New Bird S8C2 9589 (was 18032) New Bird S8C7 19702 (was 20877)

Exhibit 7 : Trend Analysis

Tracking Node (Front) Error Ellipse Semi-major Axis (95%)

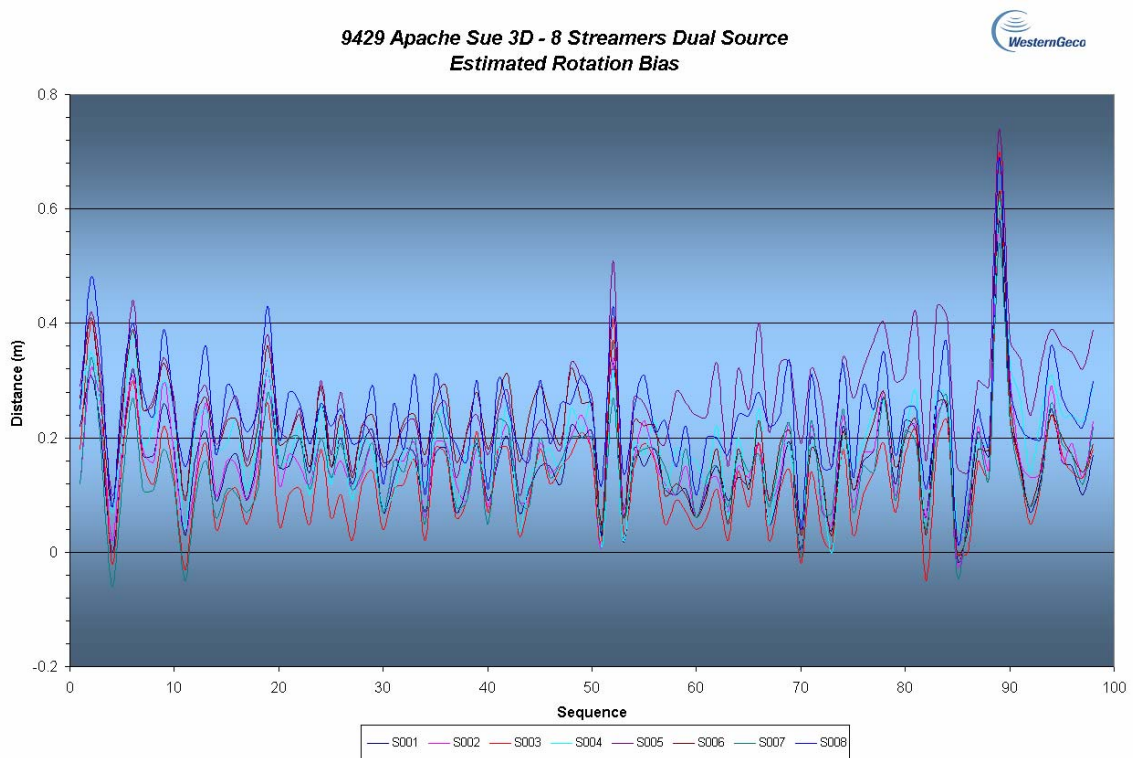


Tracking Node (Tail) Error Ellipse Semi-major Axis (95%)

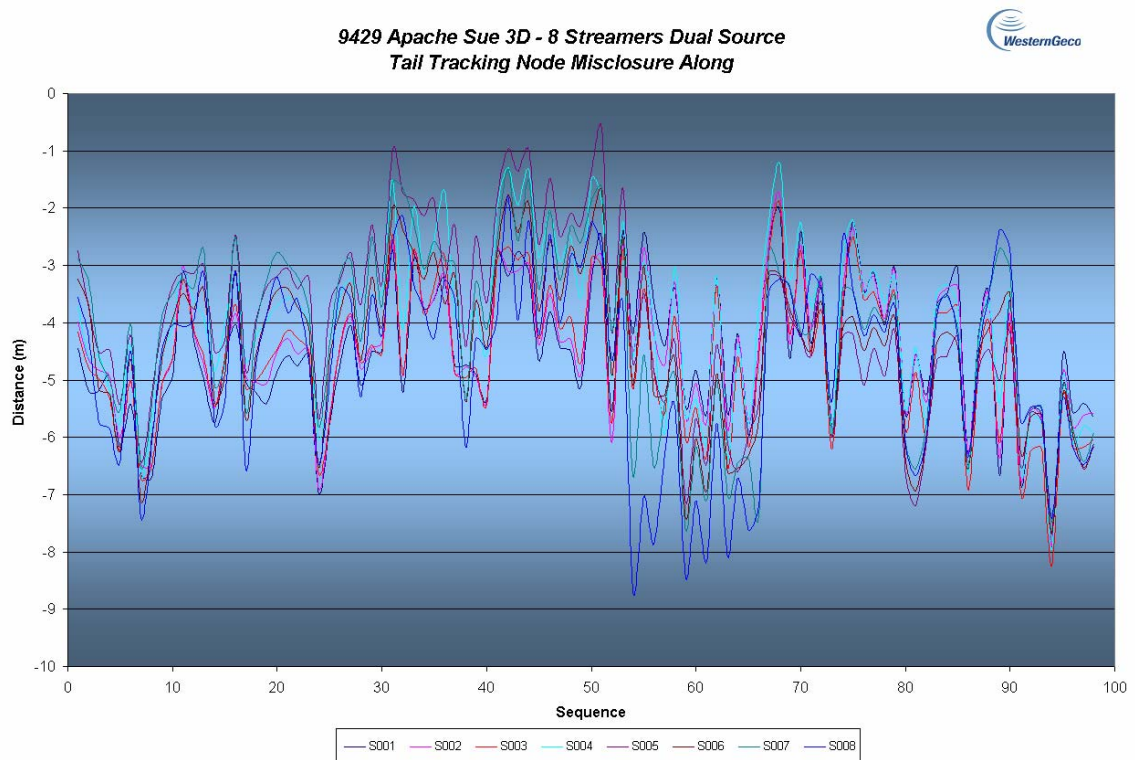


Section 4: Navigation

□ Estimated Rotation Bias

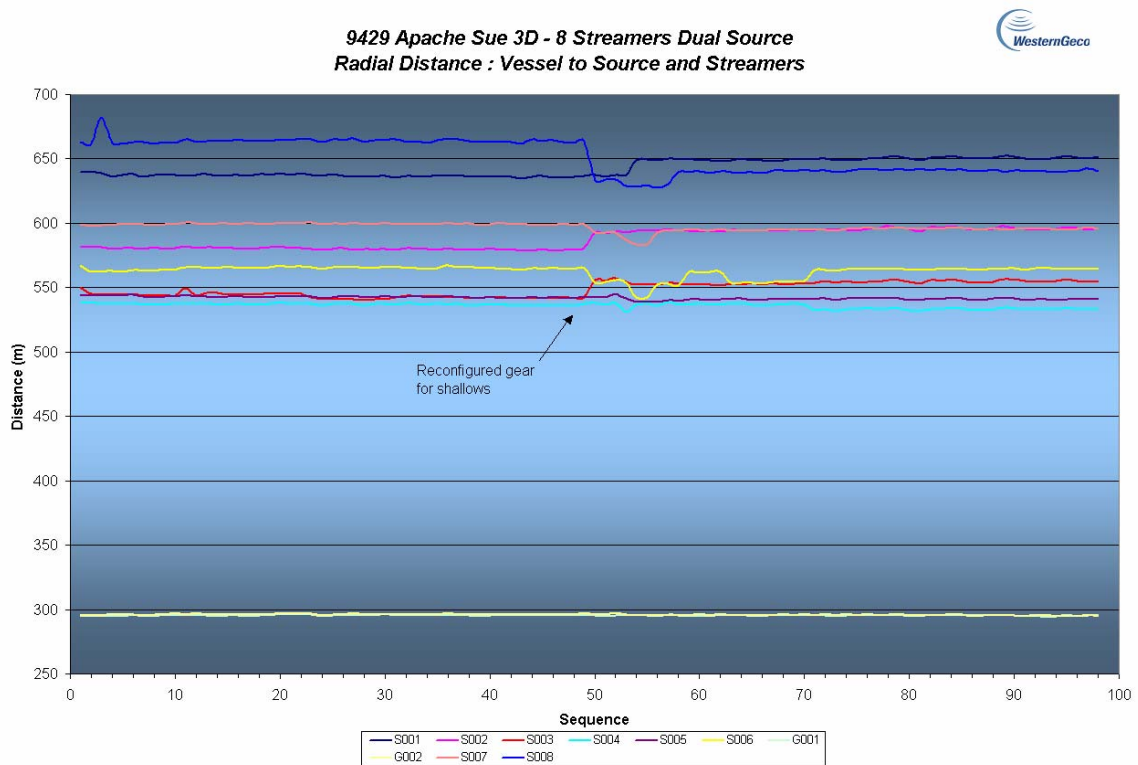


□ Tail Tracking Node Misclosure Along

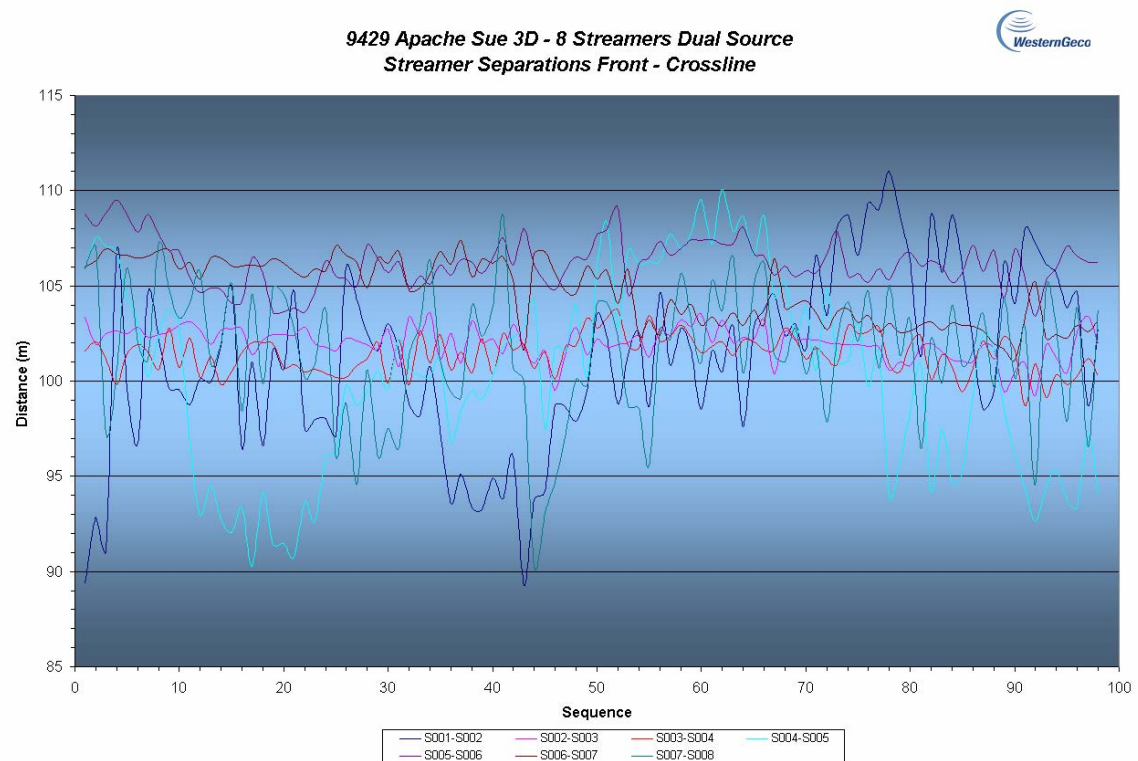


Section 4: Navigation

□ Radial Separation (Vessel to all streamers and sources)

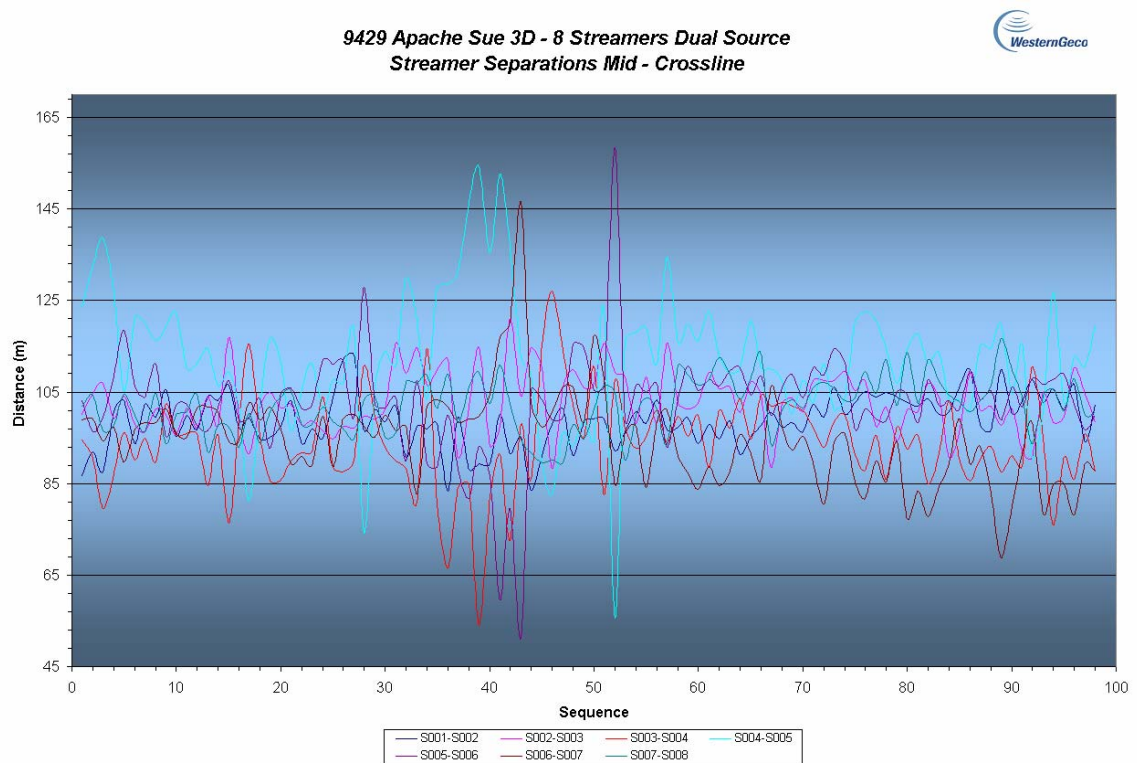


□ Cross Separation (All streamers to front)

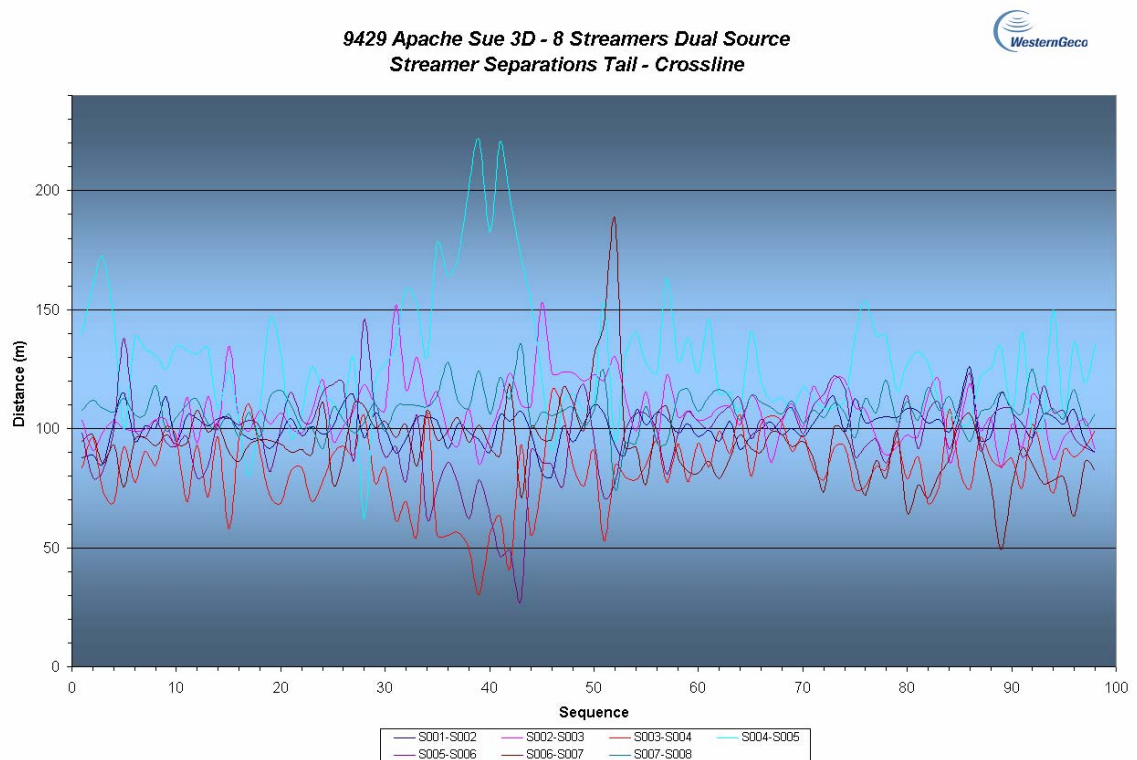


Section 4: Navigation

□ Cross Separation (All streamers to middle)



□ Cross Separation (All streamers to tail)



❑ **Cross Separation (Sources)**

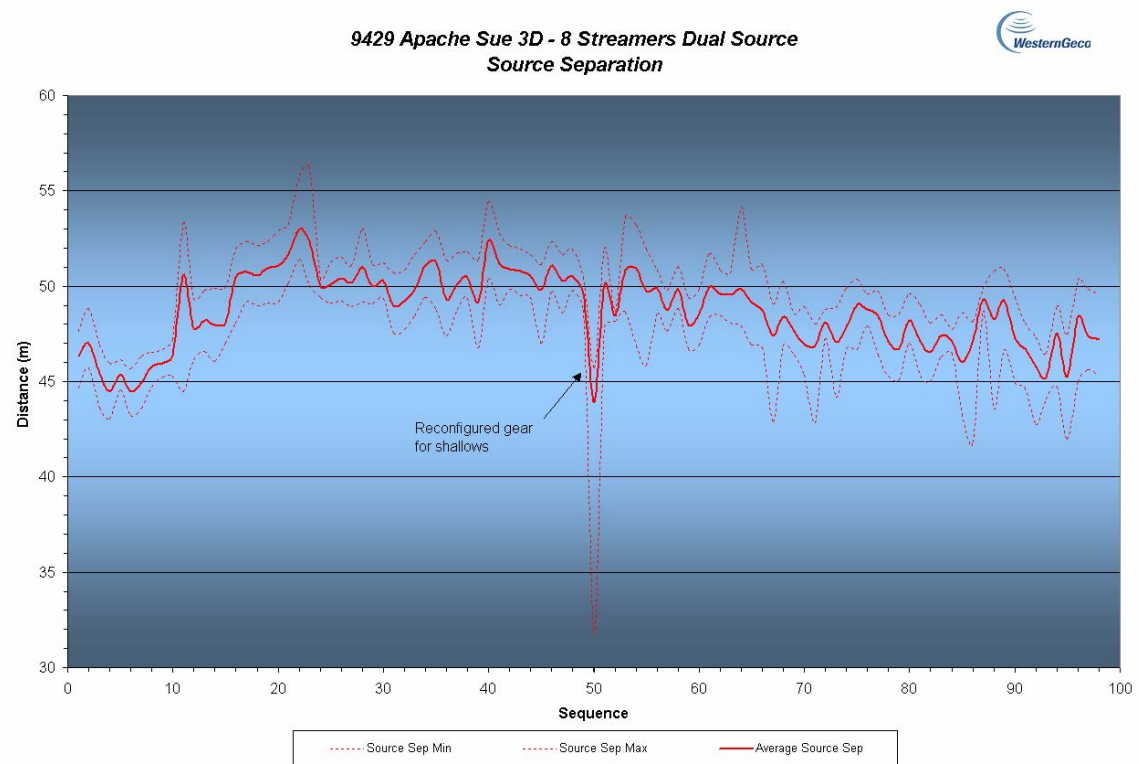
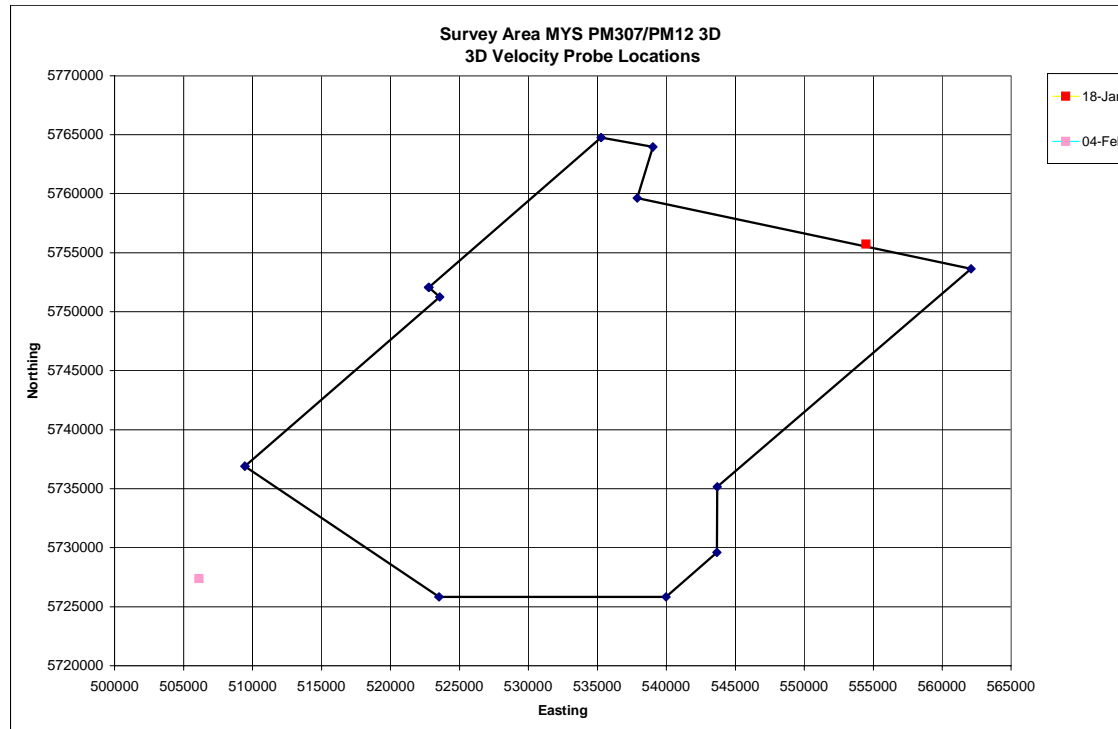


Exhibit 8 : Temperature & Salinity Measurements

❑ Measurement Locations



❑ Measurement Results

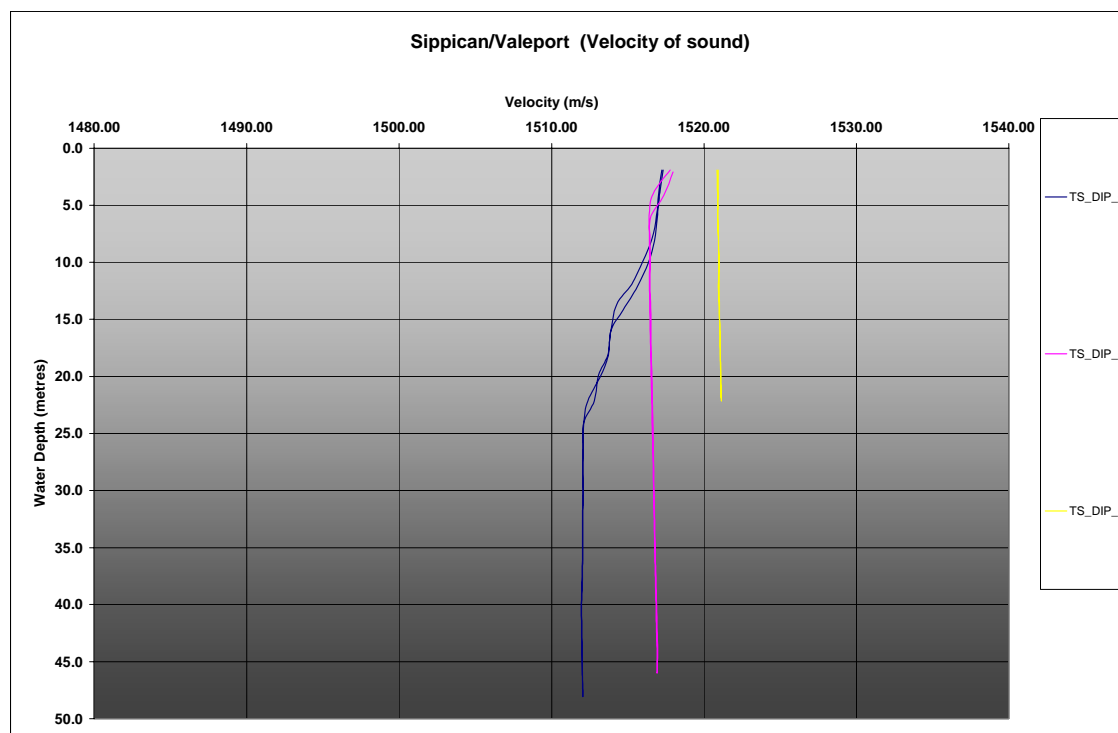


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21. Instrumentation, QC and Processing System

Description

System	Hardware	Software
Recording	Input/Output MSX system IBM RS/6000 B80	Version 2
Tape drives	4 each IBM 3590 cartridge	
Plotter	OYO Geospace: 24 inch	
Onboard QC	Seisview via the CRS	Omega 1.8.1
Source Controller	Input/Output Source Synchronisation System	Version 2.1
Auxiliary Systems	WesternGeco Continuous Recording System	Version 4.2
External Header	SEG-D 8058 Format	
Tension Monitor	WesternGeco CTM	
Bird Controller	Digicourse System 3 DMU	Version 4.31

The onboard data quality control functions are performed both online and offline. Seisview was used for online QC displays such as RMS noise analysis, gun pressures/depths display, shot gathers display and areal rms. On-line QC allowed monitoring of data quality in real time and the ability to make immediate decisions if necessary.

The majority of the QC products, less limited by processing time comparatively to on-line processing, were created offline, using the Omega Processing System configured as a small dedicated processing centre with all necessary facilities.

The processing system was connected to the other onboard departments through the vessel network which also provided an easy access to/from onshore processing centre for all required data transfer as well as for onshore support and/or hardware maintenance works. Below is a description of the onboard quality control and processing system instruments.

Off-Line QC System

System	Hardware	Software
OMEGA SPS Onboard Processing (IBM operating System)	IBM RS/6000 B80s <ul style="list-style-type: none"> 1.00 TBytes data disk 2 × Tektronics work stations 1 × 36" OYO plotter	OMEGA version 1.8.3
EMASS Silo Tape System PC EMASS (OS/2 operating system)	16 × 3590 Tape drives connected to SILO.	

22. Instrumentation and QC Tests

22.1 Semi-Monthly 08 Jan 05

					8th January 2005										APACHE AUSTRALIA									
able					File 1005	File 1006	File 1016	File 1017	File 1018	File 1019	File 1020	File 1021	File 1022	File 1023	File 1025									
Cable	Location	SG	Trace	Channel	T2 @ 0 dB Harmonic Distortion	T2 @ -10 dB Harmonic Distortion	T5 Pre- Amp Noise	T10 Common Mode .7250	T11 Cross- Feed (odd) <2.3 mv	T12 Cross- Feed (even) <2.3mv	T 6 Impulse response 2Hz	T7 Impulse Response 8/18	T7 Step Function 8/18	T4 DRD 8/18	T0 Cable Noise 8/18									
					< 0.0005%	< 0.002%	< .210 uB	<66dB FS	<56dB FS	<56dB FS	+/- 7.0%	+/- 7.0%	+/- 7.0%	+/- 7.0%										
1																								
	6b		91	91				0.7562																
	12b		186	186						54.1														
	15a		225	225									14.9											
	15a		227	227								274.6	40	73.24										
	16b	SG	256	256									29.6	68.12										
2																								
	9b		523	139									29.2	7.15										
	13a	SG	584	200								7.22	24.5											
	13b		589	205						44.8														
	15a		615	231								7.09	7.1	7.89										
	15a	SG	616	232					35.3															
	15b		617	233						29.8														
	15b		622	238						41.8														
	15b		623	239					31.74															
	16a		627	243								248	36.4	72.58										
	18a		661	277								8.08	7.9											
	24a		755	371								9.66	9.5											
3																								
	10a		919	151								7.13	7.1	7.7										
	10b		924	156								8.6	8.6											
	12b		953	185						48.1														
	12b		959	191					33.303															
	13b	SG	976	208					43.87															
	14a		978	210						39.3														
	15a		993	225									20.7	59.7										
	16b		1017	249								9.96	10	7.3										
	16b		1020	252								8.96	8.9											
	16b		1023	255								8.8	8.8											
	19a		1057	289								8.33	8.1											
	22b		1113	345								8.8	8.5											
	22b		1119	351								7.5	7.4											
	23a		1124	356								24.8	30.2	64.1										

4															
	8b		1273	121					53.88		7.29				
	8b	SG	1280	128							7.22	7.2			
	10a		1297	145					36.5				15.4		
	10a		1302	150					40.8						
	11a		1313	161					14.5		11.12	19.7	34.9		
	11a		1314	162					1.5		22.1	31.5	53.3		
	11a		1315	163				0.768			8.7	12.3	30.8		
	11a		1317	165					45						
	13a		1345	193					35.4						
	13a		1349	197					38						
	16b		1407	255				44.4							
	19b		1449	297					34.5						
	20a		1462	310							12.33	12.2	10.07		
	23b		1518	366							8.3	8.1			
	24b		1533	381					52.7						
	24b	SG	1536	384				40.4					8.3		
5															
	7a		1633	97					42.3						
	7a		1634	98					46.44						
	7a		1635	99				54							
	10a		1687	151							9.6	9.65	7.2		
	10b		1692	156							7.8	7.63			
	16a		1783	247							7.8	7.75			
	17b		1806	270							13.7	13.7	11.4		
	18a	SG	1816	280							265.1				
	19a		1826	290					36.1						
6															
	6a	SG	2008	88				48.8			17.1	17.2	17.97		
	8b		2047	127							8.05	8.07			
	24b	SG	2304	384							71.97	34.08	66.34		

7															
	11a	SG	2472	168					55.7						
	11b		2478	174					51.3						
	16a		2546	242					51						
	16a		2548	244				39							
	16a		2549	245					40.4						
	16a		2550	246					23.2						
	16a		2551	247				18.4							
	16b		2553	249					49.5						
	18b		2588	284				46.8			60.33	60.8	62		
	23a		2658	354					37.6						
	23b		2667	363				55.5							
	23b		2671	367				39.6							
	24a	SG	2680	376				49.4							
	24b		2681	377					20.4			7.3	16.1		
	24b		2682	378					0.396		56.27	69.11	64.9		
	24b		2683	379				16.52			21.95	40.6	54.4		
	24b		2684	380				6.4				10.1	22		
	24b		2685	381					28.4		8.55	18.22	33.4		
	24b		2686	382					16.7		8.48	15.76	37.5		
	24b		2687	383				5.2				10.55			
	24b	SG	2688	384				24.2			966.4	9.8			
8															
	10a		2837	149								7.9	14.9		
	10b		2842	154								15.8	7.7		
	11a	SG	2856	168				44.9							
	11b		2860	172				52.8							
	11b		2861	173					25.1						
	19a		2978	290					50.1						

22.2 Daily Tests

	Apache 9429				Reel #: V30380		seq 43		January 29, 2005	
Cable	Location	SG	Trace	Channel	T2 @ 0 dB	T2 @ -60 dB	T5 Noise	T6 Impulse	T4 DRD	T7 Impulse
					+/- 0.0005%	+/- 0.5%			+/- 10.0 %	+/- 10.0 %
1										
	16a		243	243					72.780	273.29
	18a		274	274						
	18a		275	275						
2										
	2b		413	29						
	5a		452	68						
	9a	SG	520	136					22.199	
	10b		543	159						10.51
	16a		627	243						28.24
3										
	16b		1017	249						10.38
	16b		1023	255						10.46
	19a		1057	289						10.11
	23a		1124	356					24.934	
4										
	10a		1297	145					10.233	
	12b	SG	1344	192						
	13a		1345	193						
	13a		1346	194					14.516	
	13a		1349	197					10.109	
	20a		1462	310						11.82
5										
	17b		1806	270					11.686	14.98
6										
	6a	SG	2008	88					18.084	17.3
	10a		2065	145					15.100	
	24b	SG	2304	384					22.871	
7										
	18b		2588	284					62.145	60.96
	23b		2665	361						
	23b		2667	363						
	23b		2669	365						
	23b		2670	366						11.94
8										

Cable	Apache 9429				Reel #: V30546		seq 67		February 7, 2005	
	Location	SG	Trace	Channel	T2 @ 0 dB +/- 0.0005%	T2 @ -60 dB +/- 0.5%	T5 Noise	T6 Impulse +/- 7.0 %	T4 DRD +/- 10.0 %	T7 Impulse +/- 10.0 %
1										
	16a		243	243					72.780	272.92
	18a		274	274						
	18a		275	275						
2										
	2b		413	29						
	5a		452	68						
	9a	SG	520	136					22.199	
	10b		543	159						10.60
	11b		554	170					29.400	
	11b		555	171					66.900	80.40
	16a		627	243						39.40
3										
	4a		822	54						
	12b		959	191						
4										
	5a		1220	68						
	7b		1257	105					12.200	
	10a		1297	145					31.200	
	10a		1298	146					24.200	
	12b	SG	1344	192						
	13a		1345	193					24.500	
	13a		1346	194					10.100	
	20a		1462	310					15.600	11.70
5										
	17b		1806	270					11.686	14.98
6										
	6a	SG	2008	88					18.084	18.08
	24b	SG	2304	384					23.480	
7										
	12b		2490	186					15.600	
	18b		2588	284					15.600	61.45
8										

22.3 Semi-Monthly 1 Feb 05

					1-Feb-05				APACHE 9249								
					File 1005	File 1006	File 1014	File 1015	File 1016	File 1017	File 1018	File 1019	File 1020	File 1021	File 1022	File 1023	File 1025
Cable	Location	SG	Trace	Channel	T2 @ 0 dB Harmonic Distortion	T2 @ -10 dB Harmonic Distortion	T2 @ -90 dB DRD 4%	T2 @ -100 dB DRD 4%	T5 Pre- Amp Noise	T10 Common Mode .7250	T11 Cross- Feed (odd) <2.3 mv	T12 Cross- Feed (even) <2.3mv	T 6 Impulse response 2Hz	T7 Impulse Response 8/18	T7 Step Function 8/18	T4 DRD 8/18	T0 Cable Noise 8/18
					< 0.0005%	< 0.002%	+/- 4.0%	+/- 4.0%	< .210 uB	<66dB FS	<56dB FS	<56dB FS	+/- 7.0%	+/- 7.0%	+/- 7.0%	+/- 7.0%	
1																	
	11a	SG	168	168							43.440						
	16a		243	243										272.92	39.07	72.111	
2																	
	9a	SG	520	136											14.63	29.584	
	10b		543	159										10.07			
	11b		553	169								19.632					
	11b		554	170								973.564					
	11b		555	171							985.063						
	15a	SG	616	232							13.066						
	16a		627	243											20.66	61.942	
3																	
	1b		780	12	0.000504												
	12b		953	185								60.577					
	12b		959	191							81.620						
	14a		978	210								10.664					
	23a		1124	356											18.98	57.173	

4																	
	9b	SG	1296	144							112.631						
	10a		1297	145								122.403				12.861	
	10a		1302	150								12.391					
	12b		1338	186								132.612					
	12b		1340	188							126.704						
	13a		1345	193								30.472				15.165	
	13a		1346	194												12.928	
	13a		1348	196							72.999						
	13a		1349	197								69.576				11.839	
	13a	SG	1352	200							22.722						
	16b		1407	255							13.130						
	20a		1462	310									11.70	11.61			
	24b	SG	1536	384							13.138						
5																	
	17b		1806	270									14.90	14.89	11.838		
	19a		1826	290								23.221					
6																	
	6a	SG	2008	88									17.20	17.22	18.170		
	10a		2065	145								28.708					
	24b	SG	2304	384										18.15	26.383		
7																	
	16a		2546	242								11.262					
	16a		2550	246								59.456					
	16a		2551	247							83.726						
	18b		2588	284									61.00	61.00	62.260		
8																	
	11b		2860	172							19.515						
	11b		2861	173								28.647					

22.4 QC Tests

22.4.1 Gain Correction Test.

The Gain parameters, determined by tests conducted at the beginning of Moby survey, were checked and accepted.

The single velocity function, used for Geospread Compensation and NMO correction is presented below.

Single Velocity Function used for Geospread Compensation and Normal Move Out Correction:

TIME(ms)	Velocities (m/s)
0	1500
75	1500
100	1530
400	1900
700	2312
800	2372
1270	2600
2000	3200
3300	4400
5000	5400

23.QC Products and Processing Sequence

For on-line QC analysis seismic data was re-sampled to 4 ms.

Seismic data for off-line QC analysis had 2 ms sample rate.

Water Bottom Cube also was produced with 2 ms sample rate.

23.1 Shots and FK Analysis

Shot records were displayed **online** by rotating cable/source combinations. Paper plots were also produced for every 113th shot during the line to check noisy and spiking channels, swell noise, seismic interference and other types of noise encountered.

This helped to identify noise sources and QC data outside the windows used for Attributes analysis.

Shot records were also displayed offline within the Omega Processing System. Every 105th shot, all cables were written to a QCViewer file that could be displayed on screen for identifying noisy traces and interference.

For the same shots FK analysis was performed. FK displays were used as an extra tool helping to identify the different kind of noise that could affect seismic records.

For every line Shot and FK displays of the first good shot point were saved in gif format.

23.2 RMS Analysis

23.2.1 Deep and Ambient RMS Windows

Deep window RMS values were calculated in a time window from 4500 – 5000 ms of the records. RMS values were calculated for every trace, each shot.

Ambient window RMS values were calculated in a time window from 500 – 1000 ms.

The calculation was performed for the last 100 filed channels of each streamer.

Processing Sequence

1. Data Input: Deep RMS: All shots, all channels, window 4500 - 5000 ms.
Ambient RMS: All shots, field channels 285 - 384, window 500 - 1000 ms.
2. Scaling: By 71.428571 to convert amplitudes to microbars.
3. Raw RMS Analysis: One trace is output for each shot containing the RMS amplitude over the window for each selected channel:
Deep RMS analysis: field channels 1 – 384;
Ambient RMS analysis: field channels 285 – 384;
4. Low Frequency RMS Analysis: Minimum phase low pass filter at 8 Hz 18 dB/Oct was applied. One trace is output for each shot containing the RMS amplitude over the window for each channel.
5. Mid Frequency RMS Analysis: Minimum phase low pass filter at 8 Hz 18 dB/Oct was applied. One trace is output for each shot containing the RMS amplitude over the window for each channel.
Minimum phase band pass filter was applied:
Low cut 8 Hz 18 dB/Oct;
High cut 70 Hz 72 dB/Oct.
6. High Frequency RMS Analysis: One trace is output for each shot containing the RMS amplitude over the window for each channel.
Minimum phase low cut filter at 70 Hz 72 dB/Oct was applied.

23.2.2 RMS Displays

The output analysis generated various displays, allowing analysing the level of noise for each channel for entire sail line in different frequency bands, to identify noise source (sometimes with combination of information from Shot display and/or BSTK), to detect bad channels and detect or confirm shots, affected by external or electrical noise.

The first three displays, described below, are based on the same Raw Deep RMS data.

The reason to produce all of them is that each of them better highlight some of the events, that may be difficult to be spotted or measured on other plots.

The fourth display combines data, measured in different time windows and in different frequency diapasons.

Arial RMS display. Represents channel numbers versus shotpoints with colour-coded RMS values; shows signal amplitude in microbars.

This display gives a general overview of noise level through the sail line and allows determination of noisy or dead channels, as well as noisy shots.

The display was produced both **on-line** with Raw RMS data (2 Hz / 12 dB/Oct LCF) and **off-line** with both Raw RMS data (2 Hz / 12 dB/Oct LCF) and Mid-High Frequency data (8 Hz 18 dB/Oct LCF).

Average RMS values of each trace for the entire line. The Display helps to identify noisy, weak, and dead traces. The display was produced **off-line** for the Deep Analysis window for Raw RMS data (2 Hz / 12 dB/oct LCF).

Average RMS values of each cable versus Shotpoint. The Display was generated in order to identify noisy areas throughout the sail line; to detect shots, affected by electrical noise (example: telemetry error), direction of any interfering external noise. The display was produced both **on-line** and **off-line** with Raw RMS data (2 Hz / 12 dB/Oct LCF).

Bandpass Average Deep and Ambient RMS values versus Shotpoint. For each shot RMS values were averaged and plotted versus Shotpoint. Correspondingly to 23.2.1, five graphs were presented on display: Raw Deep, Low frequency, Mid frequency and High frequency Deep RMS, Raw Ambient (consisting of the last 100 traces of each cable over a window of 500-1000ms).

A possibility to observe and analyse together the RMS, registered in different time and frequencies windows, helps to identify the cause of noise and separate the real noise, particularly swell noise, from noise, caused by geological events (strong seismic signal at deep times). This display was produced **off-line**.

An **on-line** modification produced only a pair of Raw Deep RMS and Raw Ambient RMS as a main identifier of the level of swell noise.

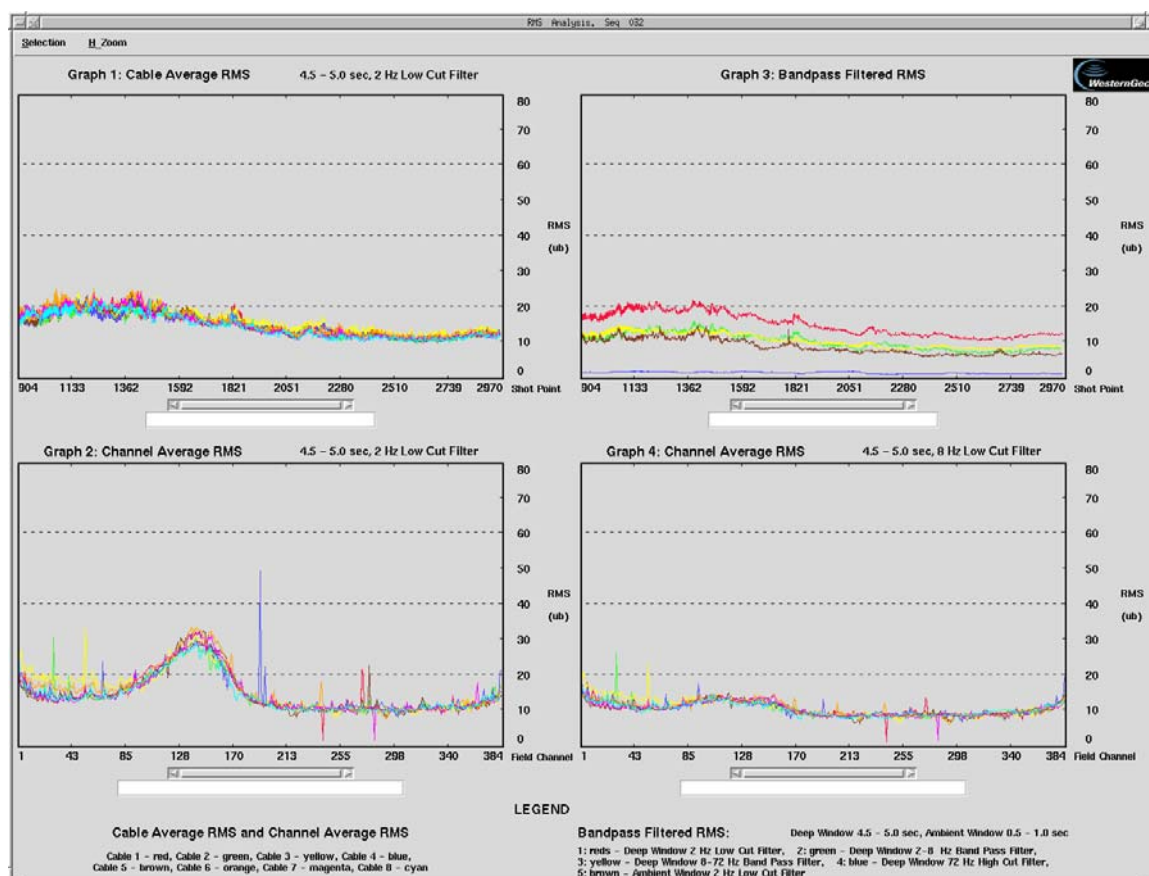


Figure 1. RMS Attributes Display.

GIF files were created for this off-line RMS display and delivered to a client's representative on-board. These were also uploaded to the Supervision server in Oslo to allow for client viewing from ashore.

23.3 Bad Traces Editing

Analysis of Shots and RMS data allowed us to identify bad traces to write into two different Edits Files.

Zeroed, distorted, noisy and weak traces were identified as bad and included in the acquisition log as edits.

Any shots with parity or Telemetry errors were identified and noted in the acquisition log as a shot edit for that streamer.

All shots affected by misfires, low or high pressure, or shots where synchronisation error exceeded 1.25 ms for any gun, also were added to the Edits File.

In addition, extra traces that fell out of depth specification were detected from P1/90 and output into a text file in a form “Shotpoint” – “Trace”.

These depth edits also were added to a “bad traces” file.

To be able to visualize the depth edits text file and final edits file for better inspection a plot Traces vs Shotpoints with colour-coded depth were produced for each line (figure 2).

Finally, all edits from “bad traces” file also were produced as a plot Traces vs Shotpoints (figure3). These plots were presented to client’s representatives on board.

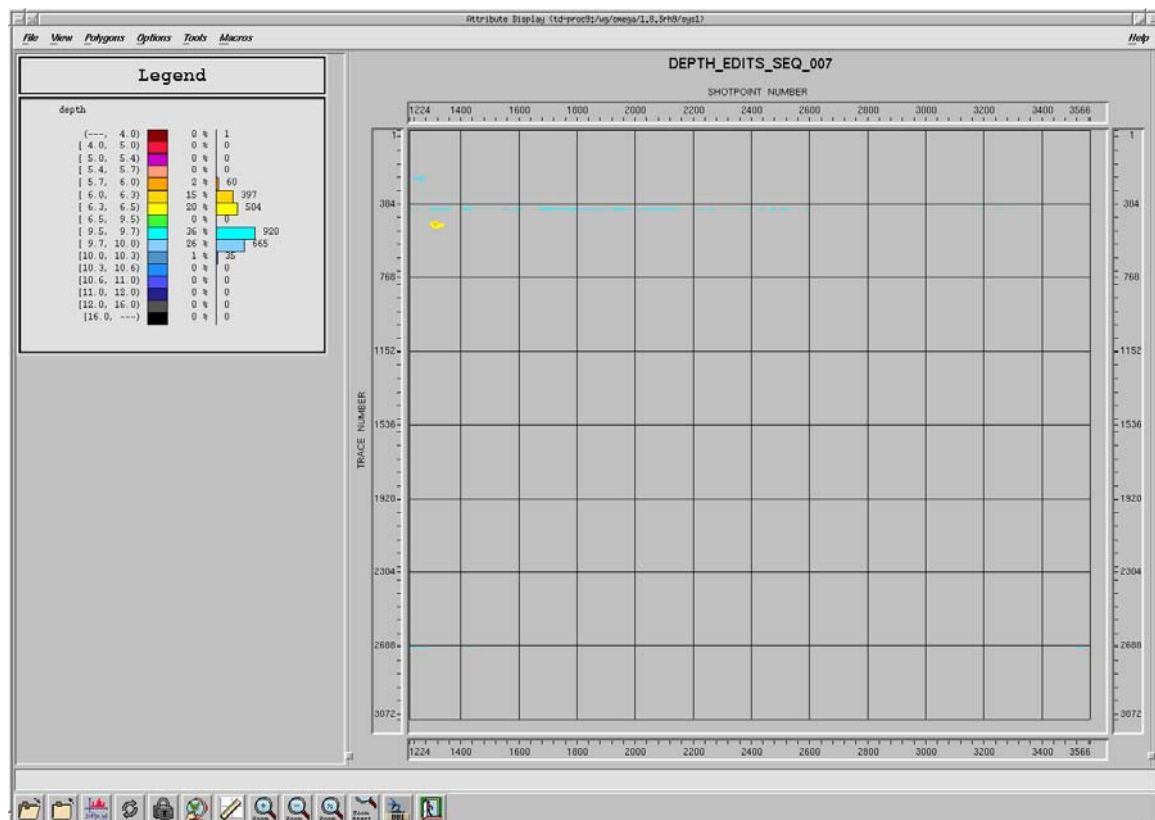


Figure 2. Depth Edits Display (Sequence 007).

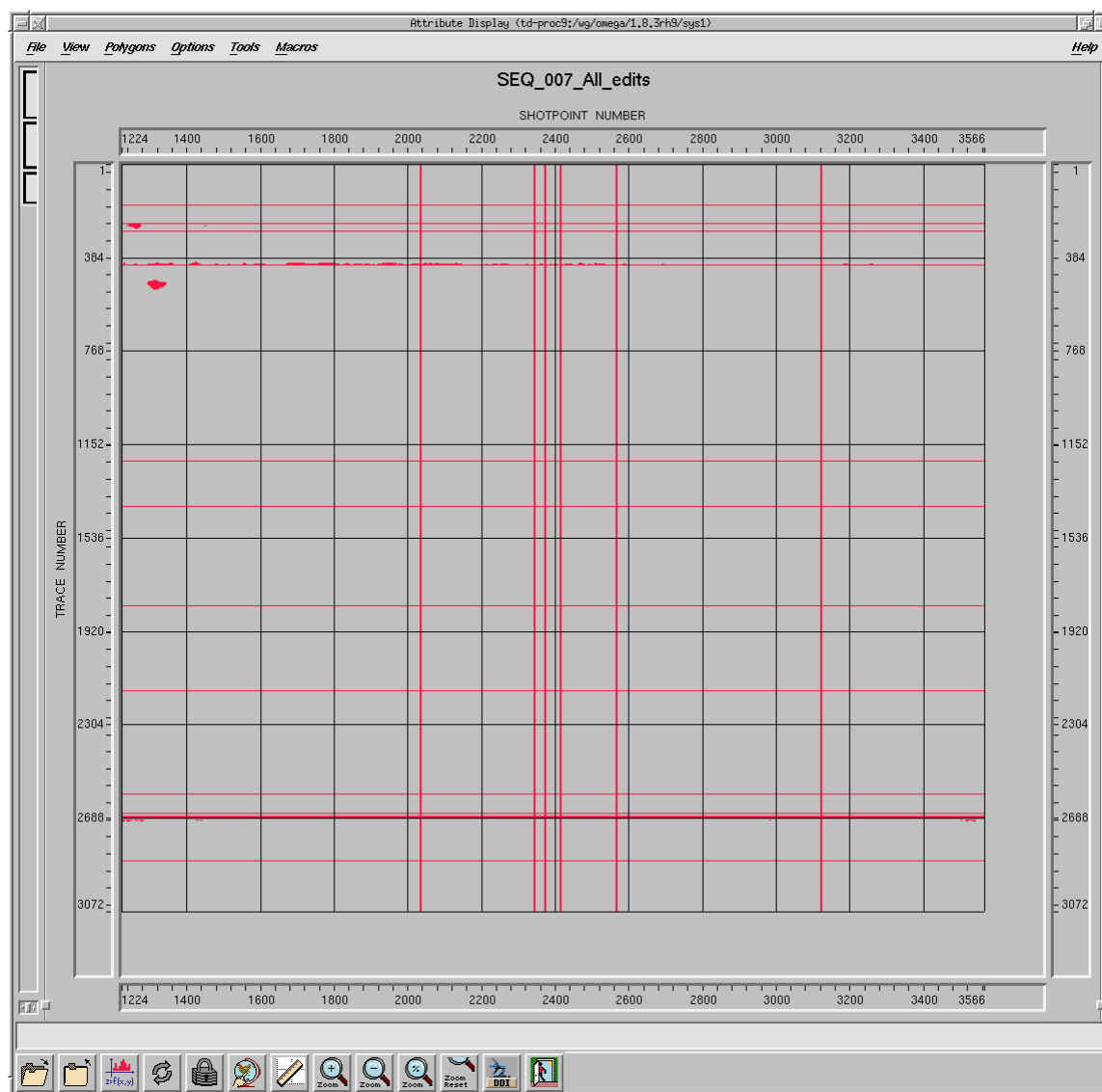


Figure3. All Edits Display (Sequence 007).

23.4 Near Trace Display

As part of the quality control process, near trace data with streamer rotation per sail line were selected for every sail line acquired. The first second of data was displayed to allow for detection of autofires. These were displayed using QCViewer and gif files were delivered to the onboard client and uploaded to the Supervision server in Oslo.

Processing sequence:

1. Collect near traces :	Field channel 9, selected source (Port or Starboard) and streamer combination.
2. Bandpass frequency filter	Low cut filter 2 Hz. 12dB/oct
3. Gain recovery: - Geospread compensation; - Exponential Gain Correction	Geospread compensation using the single velocity function (for velocity function see 22.4.1) ----- Exponential gain correction: 4 dB/sec, window length 2000 ms, start time 2000 ms
4. Output to QCV Display :	Scale: horizontal = 35 traces/cm: vertical=23 cm/sec.

23.5 Source Attributes

Source analysis of each substring was performed for every line to determine possible air leakages and any drop in source energy, detect the sources depth and guns firing time.

Header information was read from a single trace to detect the required information.

Correspondingly, three attribute displays were produced on-line and off-line:

- guns pressure vs shotpoint for each bundle (one sensor per substring);
- guns depth vs shotpoint for each bundle (three sensors per substring);
- guns firing time vs shotpoint for each gun.

Additionally, an attribute display with sources comparison information was produced off-line.

For comparison, 50 near traces from two inner streamers (streamers 4 and 5) were extracted.

For these traces for every shot RMS was calculated in the time window from

Water Bottom Time + 500 ms to Water Bottom Time + 3000 ms. The values, represented averaged values for Port and Starboard sources and their difference, were produced for every shotpoint (figure 4).

For undershoot lines as guns related information was not written into SEG-D headers and a single source was used, no Source attribute displays were produced. The guns related information was recorded separately by undershooting vessel RV Titan.

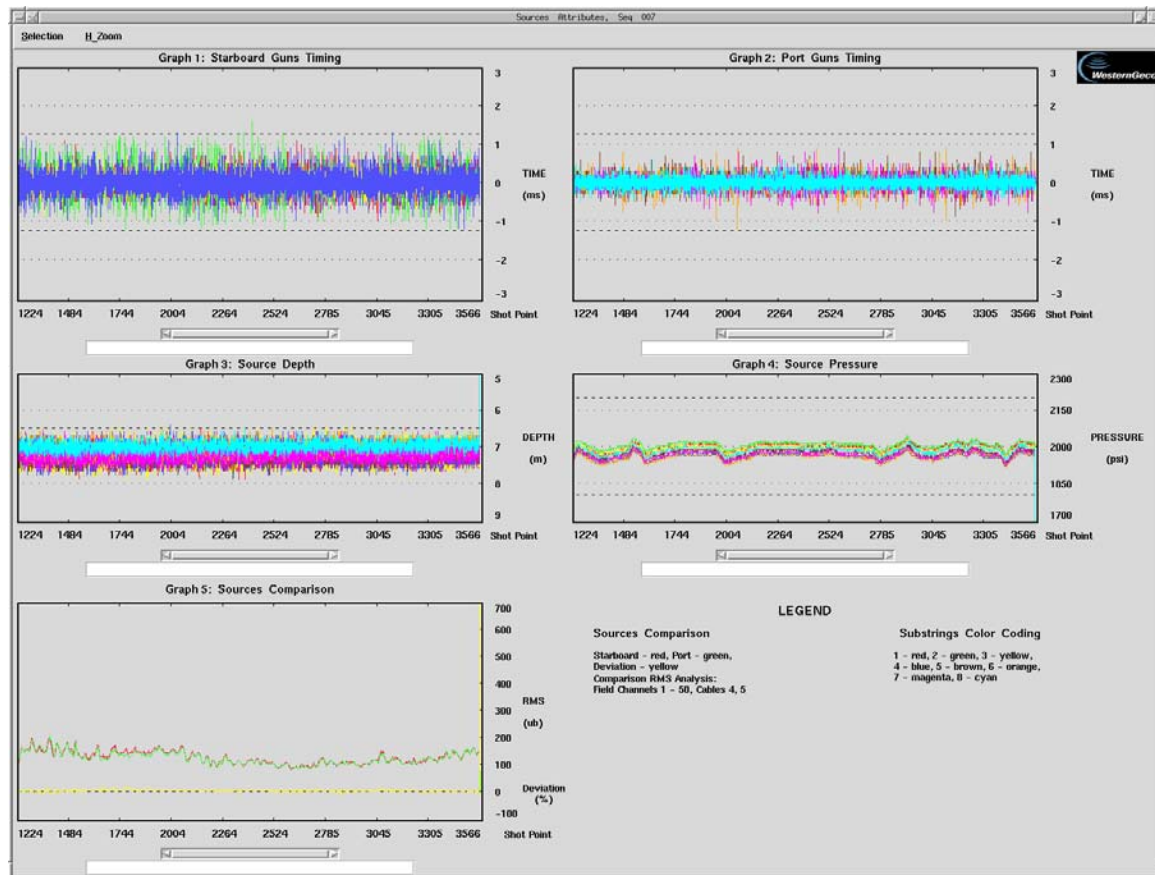


Figure 4. Sources Attribute (Sequence 007).

23.6 Brute Stack

For each sail line a different source / streamer combination was used to generate a brute stack for one subsurface CMP line.

On-line Brute Stack. A real time Terminal display was generated for every line. It involved selection of every second trace. At the end of the line acquisition, the QC group was able to generate paper plot with brute stack if required. This intended to give a much faster guide in identifying the extent of external noise in the data acquired until a full off-line brute stack was produced later.

Off-line Brute Stack was generated after bad shots and traces, derived from shots / RMS analysis, were removed from processing sequence.

A GIF file of Brute Stack was created for every line and placed in Supervision.

A paper plot also was generated for every line for QC purpose.

Processing sequence:

	OFF-LINE	ON-LINE
Input 1 CMP line per sail line	384 channels	128 channels (3:1 traces decimation).
Line edits applied	Delete bad shots/traces derived from Observers Log file and from shots / RMS analysis	Delete spiky / noisy traces, determined from previous lines

Gain Recovery	Geospread Compensation	Single Velocity Function
Low Cut Minimum Phase Frequency Filter	3 Hz 18 dB/Oct	3 Hz 12 dB/Oct
Nominal Marine Geometry	2D geometry using nominal offsets	
	Group Interval 12.5 m	Group Interval 37.5 m
Adjacent Traces Summation (2:1) with Differential Move Out Correction	Single Velocity Function	Not Applied
Nominal Marine Geometry	2D geometry using nominal offsets. Group Interval 25 m	
Predictive Deconvolution.	Operator length 300 ms; Gap 36 ms. (Not applied for undershoot lines)	Not Applied
Normal Move Out Correction	Single Velocity Function	
Pre-stack Outside Mute with offset/time pairs:	Distance(m)	Time(ms)
	200	4
	500	220
	700	629
	1560	1580
	5000	3620
Stack Root N scaling	64 fold for single boat operation (dual source) 128 for undershoot lines (single source)	
Output	To disk file in OMEGA format	
Output	To disk file in SEG Y format	Not Applied
Trace scaling	Window length 1000 ms 50% overlap. (applied only to a screen output)	Window length 5000 ms
Screen Output	Output to QCV file for QCViewer	Output to a Terminal Display
Output to Paper Plot	36" OYO Plotter 20 traces/cm 10 cm/sec	Not required for this project

23.5 First Break QC (P190 QC) Display

The main purpose of this QC tool is to confirm the positioning of the source and near trace of each cable within the P190. This is done by calculating the distances between the source and the near trace of each cable using the x-y coordinates in the P190. Using this distance and a water velocity of 1500 m/s, a calculated time is derived from the equation distance = velocity x time. This calculated time, or navigation spike, was superimposed onto the seismic trace and shifted 70ms earlier so that it could be compared from SP to SP. An incorrect source position in the P190 would be represented by a shift of roughly 10-30ms or 80-100ms depending on which streamer was being viewed. If this occurred, it was obvious by the way the traces were displayed for QC purposes and that SP was edited. The other purpose of this QC tool is to check the consistency of the navigation network from shot to shot. Any slight movements in the navigation spikes could represent a weak network solution if proportional movements are not seen with the first breaks of the seismic trace.

Field channel number 3 from each streamer was selected. As soon as the final navigation data (P190) was available, the near traces were merged with the processed navigation data. The x / y source and receiver positions were written to the trace headers and analysed.

1. Collect near traces :	Select field channel 3 from each cable
2. Geometry update	Merge selected traces with final P190 headers. A shift of 70 ms was used to offset seismic and navigation data prior to display.
3. Truncate data	Truncate data below 350 ms.
4. Display	Display seismic and navigation data for each subsurface line. Data was output to disk in CGM format, and also viewed via QCviewer interactive display.

23.7 Water Bottom Cube

The main purpose of this QC tool is to check for erroneous positioning during the acquisition by analysis of in-line, cross-line, and time-slices plots.

The seismic and navigation data were merged after final navigation P190 data was available. The x / y source and receiver positions were written to the trace headers. This information was then used to assign true offsets, select traces with offset between 430 and 490 m., and grid the selected near traces.

The processing flow included:

- Input selected traces,
- Bad traces/shot edited,
- Progressive stack file created,
- Geospread compensation using Single Velocity Function
- NMO (normal moveout) corrected using the same velocity function.
- Writing into OmegaVu cube for visual inspection on screen and on paper plots.

Cube Parameters:

Inlines	: 931 - 2459	Increment:	1
Crosslines	: 851 - 3753	Increment:	1
Cell Size	: 18.75 m x 25.00 m		
Rotation	: 44.566 degrees		
Corners Coordinates			
931 / 851	: X = 505414.53 Y = 5736932.37		
931 / 3753	: X = 543597.44 Y = 5775698.15		
2459 / 851	: X = 532629.84 Y = 5710126.27		
2459 / 3753	: X = 570812.73 Y = 5748892.05		
Data Length	: 1000 ms.		
Sample Rate	: 2 ms.		

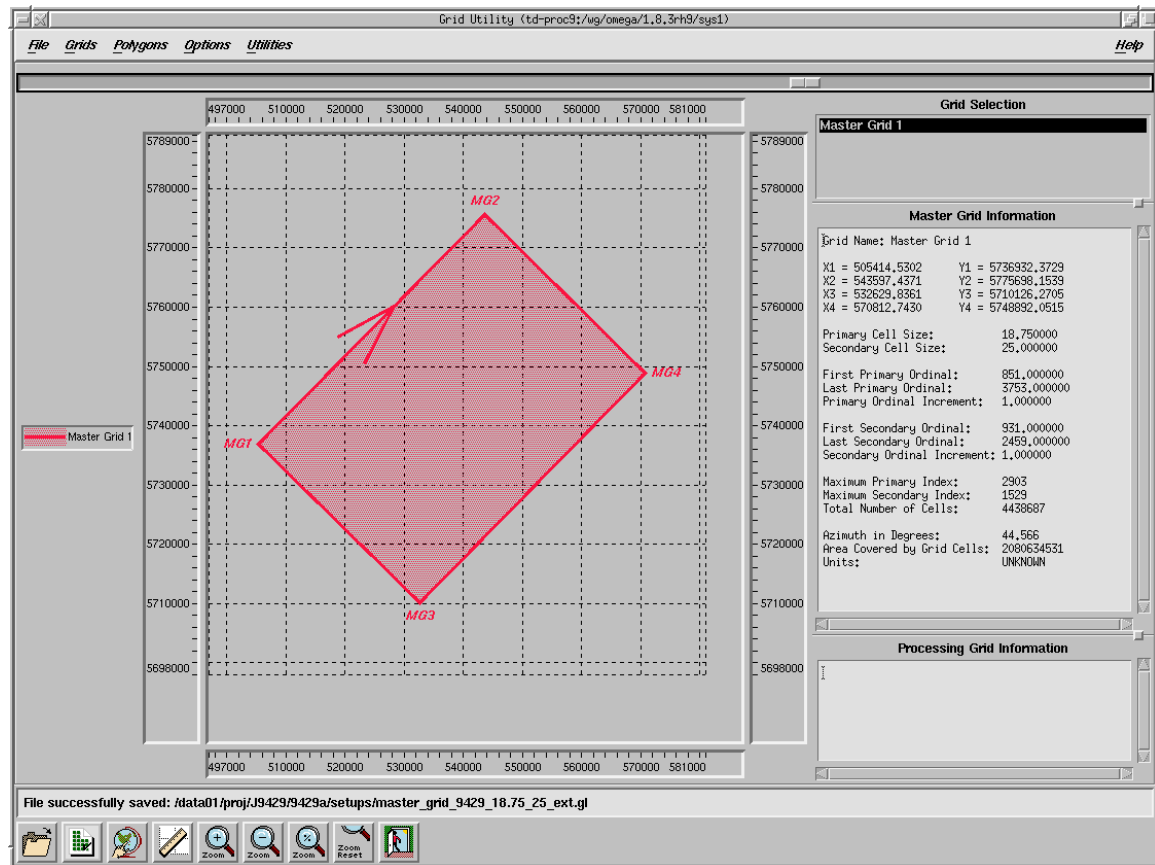


Figure 5. The Grid used for Water Bottom Cube.

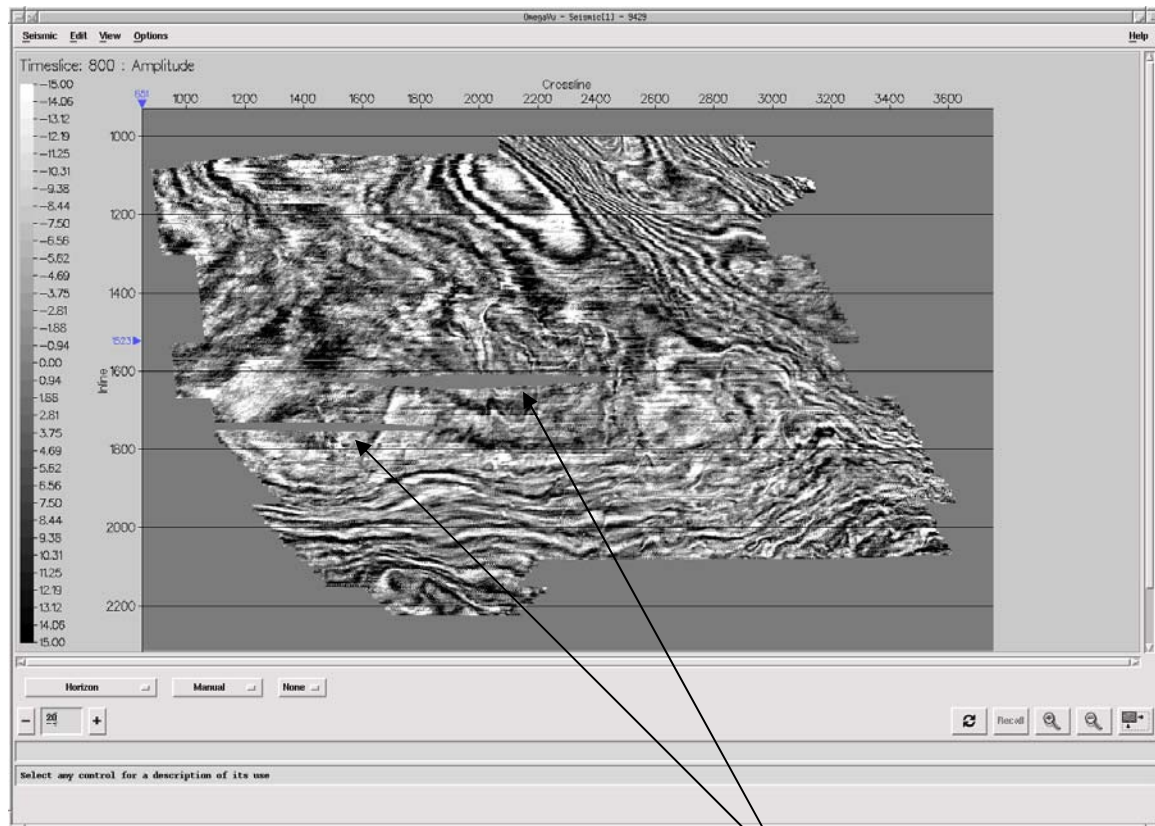


Figure 6. Water Bottom Cube. Time Slice at 800 ms. Not filled blocks in the middle of survey correspond to undershoot areas.

24. Data Quality / Observations

24.1 Quality Control Summary

24.1.1 QC Outputs

A significant number of plots and displays were produced for quality control of each sequence, allowing rapid and accurate delineation of noise types and their associated effects on data quality. A dedicated local disk directory was provided so that gif files of these displays were provided regularly after end of each acquisition line for the onboard client to evaluate. Most of the products were created offline, but a chosen number of displays were generated online in order to provide a much quicker appraisal of the data quality, using Shot display, Brute Stack display, attributes such as RMS noise level, source pressure, depth for each string. Also a gun timing display presenting firing time versus Shotpoint for each gun was produced in real time and off-line. RMS analysis on deep and ambient windows provided very useful information for the client and crew in determining the amount of swell noise, ship's noise and other types of noise present in the data.

Analysis of RMS level for each channel, averaged for the entire line, helped to identify noisy or weak channels.

Shot gathers were plotted on the OYO plotter with an interval of 2118 metres (every 113th shot, for different cable/source combination), which were being checked by the acquisition group.

In addition, shot records were output offline every 105th shot which were viewed through Omega QCviewer to identify noisy channels and electrical spikes. FK analysis was performed on these shots. A RMS source comparison was performed on every sequence to identify any serious problems with the source output.

As an extra quality control, allowed to visualise depth edited traces, (8m target streamers depth, +/- 1.5 m allowed depth variations), two Attribute Displays were produced:

- Depth edited traces versus Shotpoint with colour-coded depth;
- All edits versus Shotpoint.

The visualisation of text files allowed to observe and analyse the edited areas much more easier.

The monitoring of quality of navigation data was performed by producing First Break QC plot and by analysis of cross-lines, in-lines, time-slices of Water Bottom Cube.

24.1.2 Noise encountered

❑ **Swell Noise**

Seq 002 at end of line was affected by swell noise

This kind of noise slightly affected most of lines, though Raw Ambient RMS level never exceeded 15 uB and for most of the lines was around 5 – 6 uB.

❑ **Ship Noise**

No ship noise was encountered during this project.

❑ **Strumming Noise**

The towing noise sometimes slightly affected the front of streamers 4, 5 and 6 throughout the entire survey.

At sequences 048 and 049 strumming noise affected streamer 4 due to fairing damage.

The gear was picked up and fairing was fixed.

❑ **Seismic Interference**

None encountered, however the unidentified noise affected data of sequence 6, causing several blocks editing.

❑ **Rig noise**

None encountered

❑ **Source problems, autofires**

Occasional misfires or timing synchronization errors resulted in shot edits for some sequences.

The First Break QC and guns timing displays were used to confirm which guns fired at the time, and both the P1/90 and observers log updated to reflect this problem.

❑ **Parities Problems**

Any shots with parity or Telemetry errors were identified and noted in the acquisition log as a shot edit for that streamer.

❑ **Mud Rolls**

Due to shallow soft water bottom strong surface waves (mud rolls) are visible on most of shot plots. However, this kind of wave has a slow propagation velocity (approximately 1200 – 1300 m/s) and not visible on brute stack plots.

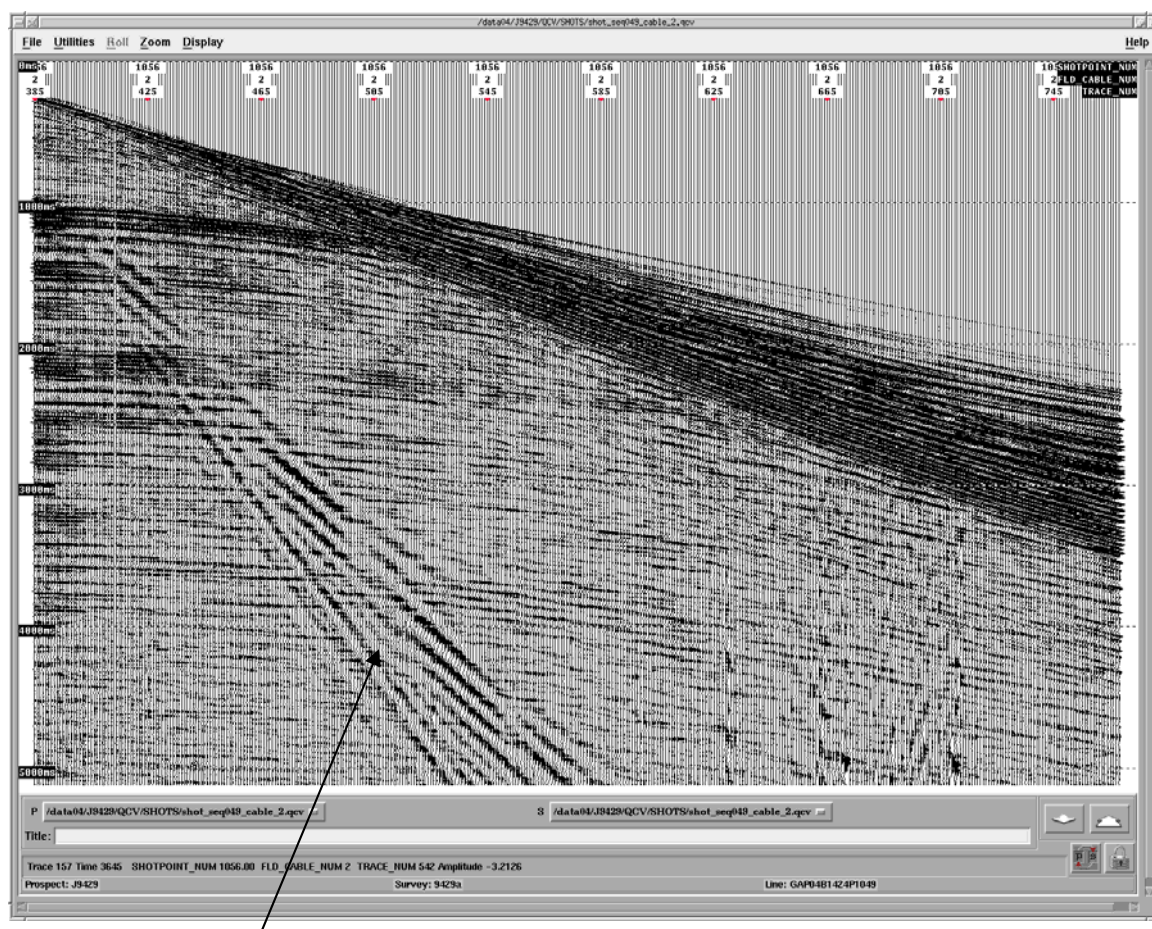


Figure 7. Strong mud roll is visible on a shot plot.

24.2 Instrument Summary

Slight strumming noise observed at the beginning of survey and affected streamer-3. The noise was getting stronger on sequence 049. We then decided to recover streamers for rectifying the problem. On sequence 50 onward the problem was fixed.

Occasionally telemetry error occurred on streamer-8 at the beginning of survey, and the affected data had been edited out from the coverage. The occurrences were noted down on the observer logs.

All noisy traces were noted down on the observer logs and some of them were edited out from the coverage.

The undershoot lines were acquired on sequences 91 to 98; the Pacific Titan was the source vessel during that operation. She used bolt guns with 3040cu.in gun volume, single source. The time difference between recording start time and shooting time was recorded as a text file for every undershooting line.

These files allow calculating on a shot-by-shot basis the time difference, which must be applied at an early stage of seismic processing. Original time difference files and recalculated files (these recalculated text files has a format DHMS DIFFERENCE ms) are written on CD-ROM together with observer's logs.