

DEPT. NAT. RES & ENV



PE902056

H1563

WELL COMPLETION REPORT

13 MAY 1992

PETROLEUM DIVISION

LINDON NO. 2

PEP 105

VICTORIA

TAIPAN PETROLEUM PTY LTD

**PREPARED BY
GEOWESTE PTY LTD**

TABLE OF CONTENTS

	page
1. SUMMARY	3
1.1 Geological	3
2.2 Drilling	3
2. INTRODUCTION	6
3. LOGISTICS AND ENVIRONMENTAL CONSIDERATIONS	7
3.1 Logistics	7
3.2 Landholder	7
3.3 Environment	7
4. SUPERVISION AND REPORTING	8
4.1 Company	8
4.2 Contractor	8
4.3 Reporting	8
5. DRILLING DATA	9
5.1 Well Design	9
5.2 Pressure Control	10
5.3 General Data	10
5.4 Rig and Equipment Specifications	12
5.5 Casing and Cementing	15
5.6 Completion	16
5.7 Drilling Fluids	16
5.8 Water Supply	19
5.9 ROP and Drilling Bits	19
5.10 Deviation Record	19
5.11 Time Distribution	20
6. GEOLOGICAL DATA	21
6.1 Objectives	21
6.2 Stratigraphy	22
6.3 Hydrocarbons	25
6.4 Sampling and Sample Examination	26
6.5 Wireline Logging	27
7. CONTRACTORS AND SERVICES	28
APPENDIX 1 WELL HISTORY	
APPENDIX 2 DRILL STEM TEST DATA	
APPENDIX 3 PRODUCTIVITY TEST DATA	
ENCLOSURE 1 COMPOSITE WELL LOG	
ENCLOSURE 2 WIRELINE LOGS	
ENCLOSURE 3 LITHOLOGICAL LOGS (added by DNRE)	

WELL SUMMARY SHEET

COMPANY : TAIPAN PETROLEUM PTY LTD
 SPUDDED : 12-5-91
 COMPLETED : 25-5-91
 T.D. : 970.0m

WELL : LINDON NO. 2
 BASIN : OTWAY BASIN, VICTORIA
 TENEMENT : PEP 105
 LAT. 38° 04' 6.8" LONG. 141° 30' 54.7"

ELEVATION: GL=63.3m ASML, kB = 68.3m ASL SEISMIC DATUM = 0m ASL

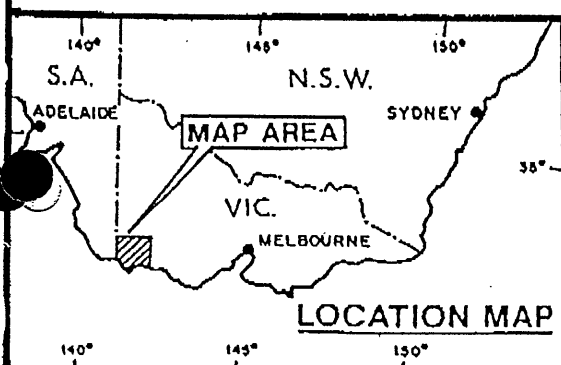
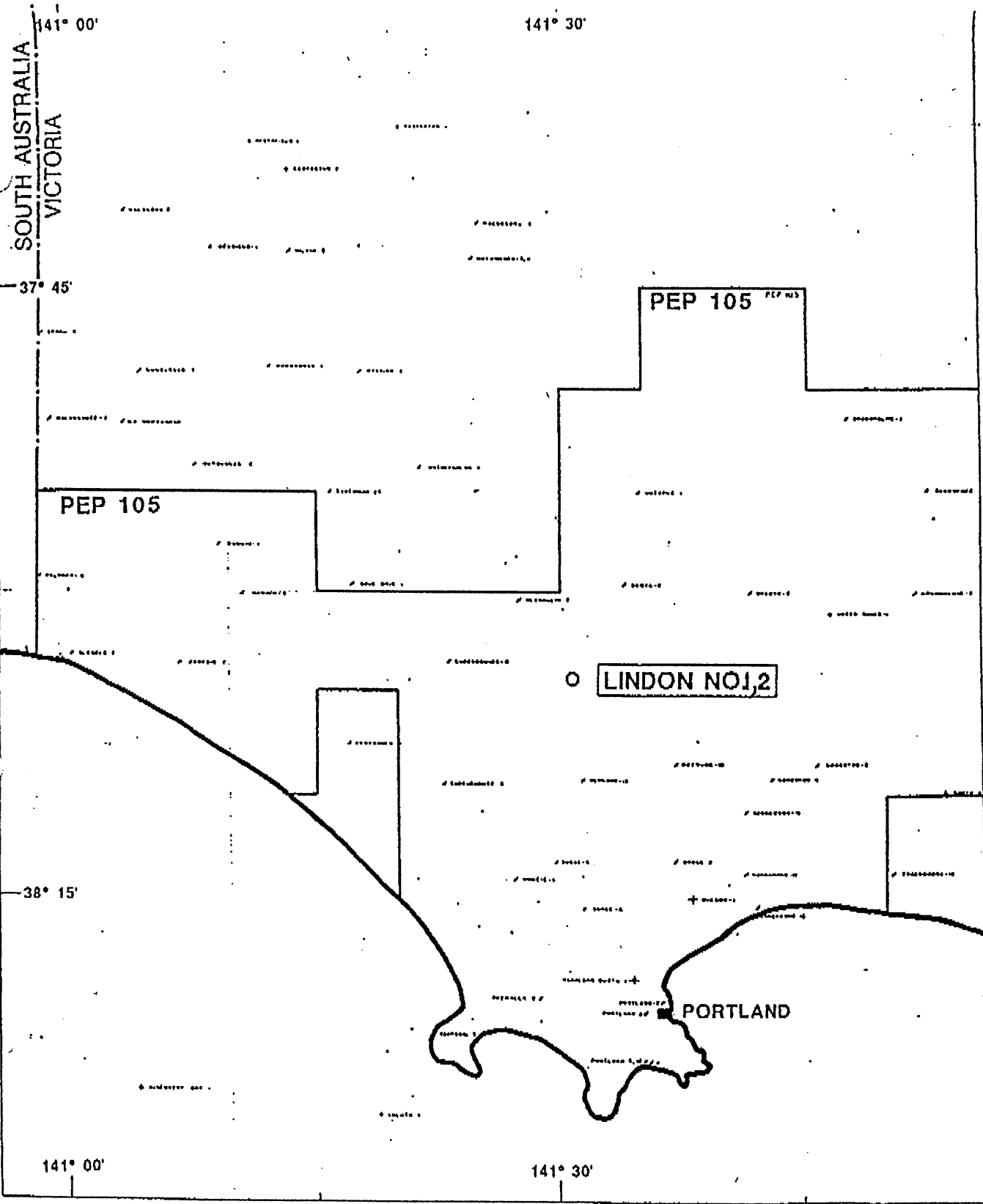
FORMATION	TOPS (m)		LITHOLOGY	REMARKS / SHOWS
	DRILL	SUBSEA		
HEYTSBURY GROUP				
Port Campbell Limestone	GL.50m	63.3] calcarenite, marl calcarenite calclatite	
Gellibrand Marl	187	-119		
Clifton Formation	244	-176		
NIRRANDA SUBGROUP				
Narraturk Formation	270	-202	Marl	
Mepunga Formation	349	-281	calcarenite, marl	
WANGERRIP GROUP				
Dilwyn Formation	407	-339	sandstone, minor claystone, minor basalt / dolerite	908.0 - 915.0m SST : 45% - 50% fluorescence 10-15% vis. oil stain TG 28.6 units BG 0.5 units 915.0 - 919m 20% - 5% fluorescence
Pember Mudstone	660	-592	siltstone, minor clay stone, slightly carbonaceous.	
Pebble Point Formation	908	-840	sandstone-clayey, silty.	
SHERBROOK GROUP				
Paaratte Formation	947	-879	sandstone	
TOTAL DEPTH	970.0	-902		

H O L E	surface - 115m : 12 1/4"	C A S I N G	9 Jts 9 5/8" 43lb/ft JAP K55 set at 111.74m cmtd to surface
	115 - 970 m : 8 1/2"		80 Jts 7" 26lb/ft Sumitomo J55 LTC R3 set at 962.3m
CORES	NIL		93 Jts 2 7/8" 6.5lb/ft J55 EUE set at 894.5m

L O G S	1 suite only 966-100m : Dual laterolog, Microlog, Microlaterolog, sonic, gamma ray, caliper 963-750m : Photo - Density, Neutron, caliper, gamma ray 941-200m : CBL, VDL, GR 988-888m : GRS, CCL
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T E S T	DST 1 : 904.3 - 912.85 mkB : test aborted - test head valve problem DST 2 : 902.7 - 914.1 mkB : test aborted - packer failed to seat
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C O M P L E T I O N	COMPLETION COMPLETED AND SHUT-IN ON THE PEBBLE POINT FORMATION AS A POTENTIAL HEAVY OIL PRODUCER. INTERVAL PERFORATED 908.1-911.1m SURFACE COMPLETION : CANADAWERKS 7 1/8" 3000psi CHRISTMAS TREE
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TAIPAN PETROLEUM PTY LTD
PEP 105
LINDON NO. 2
REGIONAL LOCATION MAP

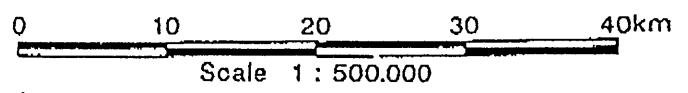


FIGURE 1

recovered 29 deg API, 30 deg C poor point oil and completion brine without any formation water. The inferred influx rate was 4.5 BOPD.

1.2 DRILLING

Following 5 days rigging up, Lindon No 2 was spudded at 0130hrs on May 12, 1991. The well was drilled to a total depth of 970mKB in 10 days and was completed for production testing on May 25, 1991 (day 14).

Lindon No 2 was drilled using Gearhart Drilling Services Rig No 2, a Superior Model 700E with a nominal depth capacity of 3350m, 4 1/2" drill pipe, 3000 psi annular B.O.P., 5000 psi double gate B.O.P. and SCR electric drive. Mud tank capacity was 400 bbls. Drilling depths were measured in metric units from the kelly bushing 4.8m above ground level. Two 5 man drill crews each worked 12 hr shifts, 7 days per week, supported by a toolpusher, fitter and dayman.

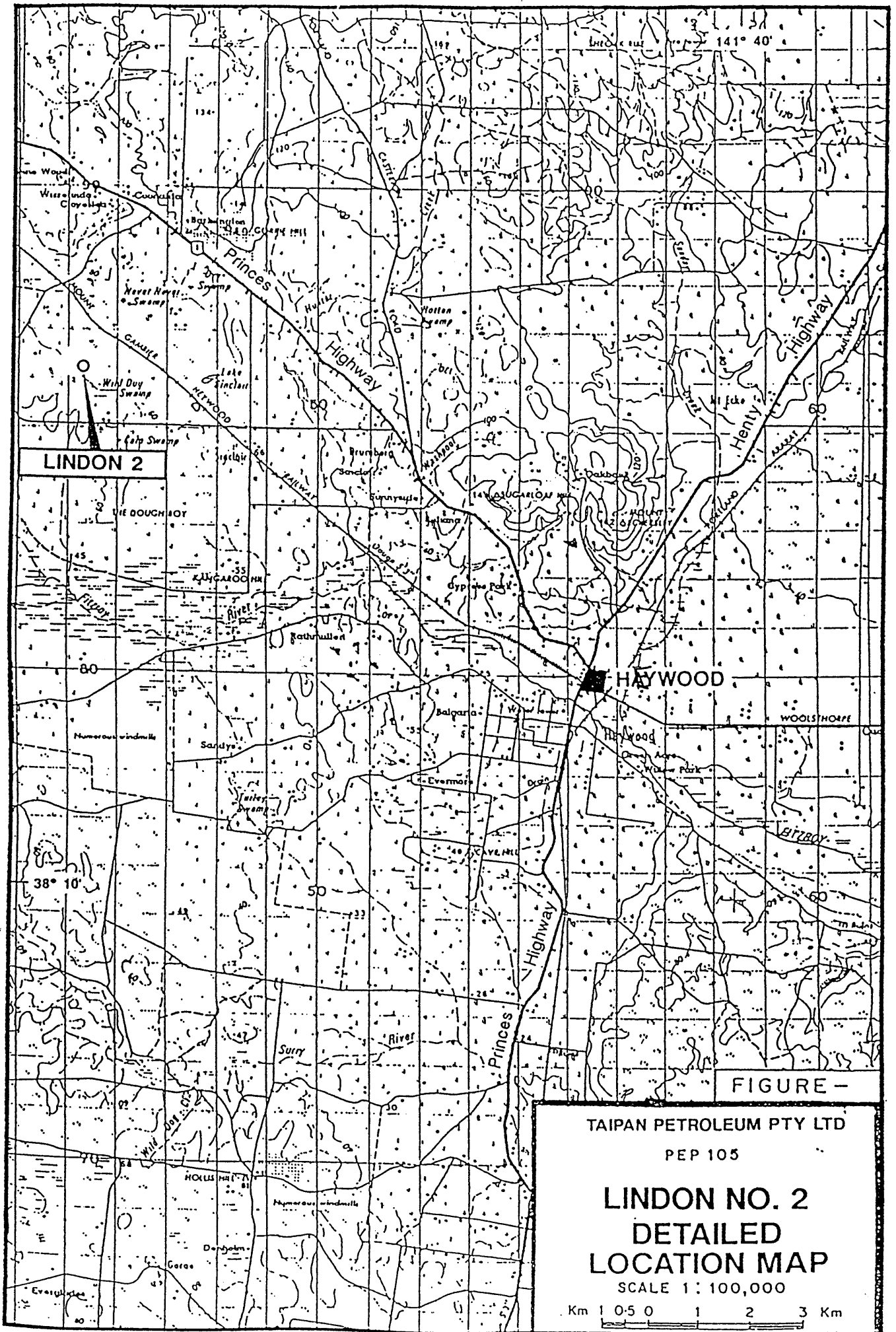
12 1/4" hole was drilled to 115m with ROPs of 20m per hr and 9 5/8" casing run to 111.7m and cemented to surface. B.O.P.s were nipped up and tested. An 8 1/2" bit was run in hole to drill out cement, float collar, casing shoe and 3m of new formation. A formation integrity test leaked off at an equivalent mud weight of 16.2 ppg. 8 1/2" hole was drilled to 891m using two bits. All mud tanks were then dumped and new polymer mud mixed and circulated. 8 1/2" hole was then drilled to 911.8m and the drill string tripped out for DST No 1.

DST No 1 was attempted over the interval 904.3-912.85m. The test head valve was not opened at the commencement of the test resulting in the status of the tool and the test being not determinable. The test was therefore aborted. 8 1/2" hole was then drilled to 914.1m and the drill string tripped out for DST No 2. DST No 2 was attempted over the interval 92.7-914.1m but the test packer failed to seat and the test was aborted. 8 1/2" hole was then drilled to the total well depth of 970m.

Following a 15 stand wiper trip wireline logs were run. Run 1, 966-100m, comprised dual laterolog, microlog, microlaterolog, compensated sonic, gamma ray and caliper. Run 2, 961-750m, comprised photo-density, compensated neutron, gamma ray and caliper.

Following a wiper trip, 7" production casing was run to 962.3m and cemented. The B.O.P.s were re nipped-up and 2 7/8" EUE tubing run in hole with 6" bit and casing scraper to tag plug at 945m. The casing was filled with a 6% KCl brine, the tubing pulled out and CBL log run from 940-200m. The log located the 7" casing radioactive pip tag at 882m and showed a continuous cement bond to 25.5m.

The bottom hole completion made provision for rod pumping, the rod pump to be landed in top profile of opened sliding sleeve. The packer, BHA and 2 7/8" tubing was strapped in hole under tension to position top gun at 908.8m to perforate interval 908.1-911.1m. A 180m brine cushion was used. The GR/CCL positioning log was run



LINDON 2

HAYWOOD

FIGURE -

TAIPAN PETROLEUM PTY LTD
 PEP 105
LINDON NO. 2
DETAILED
LOCATION MAP
 SCALE 1:100,000
 Km 1 0.5 0 1 2 3 Km

Figure 2

2 INTRODUCTION

The Lindon Prospect is located in the onshore Otway Basin, 30kms northwest of Portland in PEP 105 in the southwest corner of Victoria. Wildcat well Lindon No 1, drilled in 1983 by Beach Petroleum N.L. porous Tertiary Pebble Point Formation sandstone with significant oil shows. Although a drill stem test recovered heavily oil cut and gas cut mud, Lindon No 1 was plugged and abandoned. Taipan petroleum Pty Ltd re-evaluated the Lindon No 1 data and approached the PEP 105 permittees with a proposal to retest the Pebble Point Formation by drilling a well close to Lindon No 1. In December 1990 Taipan petroleum reached agreement for a 'Drilling Option' for the 'Lindon Prospect' with the PEP permittees (Gas and Fuel Exploration N.L. - operator, Beach Petroleum N.L., Victoria Exploration Inc., Crusader Resources N.L., Australian Hydrocarbons N.L. and Mosaic Oil N.L.).

Lindon No 2, was located as close as possible to Lindon No 1 (30m to the south), and was drilled during May, 1991. The well was completed for production testing and was tested with a swabbing unit.

3 LOGISTICS, LANDHOLDERS AND ENVIRONMENTAL CONSIDERATIONS

3.1 LOGISTICS

Lindon No 1 is located in a well developed rural area of southwest Victoria. The region is well serviced with a large vessel deep water port, a major rail terminal and an airline serviced airport, located at Portland, 30 km from the well site (see Figure 1). A properly maintained and utilised railway line passes within 1km of the well site and power lines and telephone lines pass immediately adjacent to the site. A sealed road passes within 1km of the site. A small township, Haywood, with motel and hotel accommodation and shops, is located 12km southeast of the well site (see Figure 2). The Lindon No 1 well site required only very minimal preparation. The pre existing Lindon No 1 site had not been fully reclaimed, the pad being still intact. Access, requiring only minor extension to the south. The pre existing sump was reopened. Access to the well site was via sealed roads to 1 km from the site. The final 1 km utilised the access road constructed for Lindon No 1 which required only minor upgrading. All site work was completed by the landholder who also operated a gravel quarrying business on the property. No problems were encountered with rig Mobilisation and demobilisation and only minor rainfall occurred during operations. Drilling water was obtained from a bore on the property. No camp was established at the site and crews were accommodated at the hotel and motel in Haywood. The hotel supplied all food. A telecom line was run 1 km from the nearest existing cable and separate telephone and facsimile communications lines established at Taipan Petroleum's site office. Taipan established two caravans at the well site, one to accommodate Taipan site representatives and the other as a site office.

3.2 LANDHOLDER

The well site is located on a cattle property owned by Mr. B. Price who lives on the property. Agreement was reached with the landholder for the drilling operations. A satisfactory Compensation Agreement was reached between B. Price and Taipan Petroleum Pty Ltd. The landholder was engaged to construct the well site and to provide drilling water to the rig.

3.3 ENVIRONMENT

Lindon No 2 is located on very gently undulating cleared grazing land normally stocked with cattle. Approximately 2 hectares were utilised during drilling operations and this area has no trees or shrubs. Because the site for Lindon No 1 was still usable, very little construction was required for Lindon No 2 and the environmental impact was minimal. Good weather conditions during drilling operations, a well gravelled access road and lateric soils at the well site, resulted in no disruption of the soil surface by vehicle movements around the drill pad. Following completion the wellsite was fenced and safety drains around the site were checked to ensure that any spillages that may occur would be contained on the site.

4 SUPERVISION AND REPORTING

4.1 COMPANY

Taipan Exploration was represented at the site by Mr. Griff Weste and by Taipan director Mr. Wayne Dimech, who were accommodated at the well site for the duration of the drilling program. Gas and Fuel Exploration, operator for PEP 105, was represented by their observor. Drill stem testing and production testing was supervised by Mr. Bill Waterhouse of Petroleum Engineering Services Pty Ltd.

4.2 CONTRACTOR

Gearhardt Drilling Services provided an experienced toolpusher. Logistical support was provided from Gearhart Drilling Services Brisbane base.

4.3 REPORTING

Approved IADC-API Daily Drilling Reports were completed by each drilling shift and were signed by the Gearhart Drilling Services toolpusher and by the Taipan Petroleum representative. A daily drilling and geological report was faxed daily to Taipan Petroleums Perth Office, to Gas and Fuel Explorations Melbourne office, to each of the other PEP 105 permittees, and to the Petroleum Division, Department of Manufacturing and Industry Development. Daily costs were faxed to Taipan Petroleum Perth office.

5. DRILLING DATA

5.1 WELL DESIGN

Lindon No 2 was designed as a redrill of the uppermost 1000m of Lindon No 1. The well was located as close as possible to Lindon No 1, but at a safe distance (40m) to ensure that the Lindon No 1 hole and its zone of invasion was not intersected.

Well design was kept as simple as possible to keep drilling costs to a minimum. The relatively shallow prognosed total depth (940m), and the known drilling conditions required only a simple casing program. Stable surface conditions and the shallow prognosed depth for the 9 5/8" casing point (circa 110m) allowed design of the 12 1/4" hole without running a conductor. The use of a cellar jet was considered sufficient to maintain the surface hole.

Thin section studies of core samples taken from the Pebble Point Formation reservoir in Lindon No 1 indicated the presence of smectite clays and possible formation damage. This may have resulted in a substantial loss of permeability resulting in only limited volumes of oil being recovered by DST. Lindon No 2 was designed to minimise the possibility of damage to the Pebble Point. At approximately 889m (15m above the top Pebble Point), the bentonite mud would be dumped and displaced with a polymer - 6% KCl "drill-in" mud. This would allow the reservoir to be drilled with a clean mud of minimal weight and with a thin tough polymer mud cake. 6% KCl was considered to provide sufficient inhibition.

The Pebble point was to be drilled slowly (500 lb WOB), at minimal pump rate (55 SPM, 160 gpm), to minimise hydraulic damage to the formation and to maintain an in-gauge hole to provide a good DST packer seat.

PEBBLE POINT FORMATION HYDRAULICS

Jet size	12-11-11
SPM	55
GPM	160
Annular velocity past drill pipe	75 FPM
Annular velocity past drill collars	118 FPM
KCl mud weight	8.7 ppg
Surface pressure	450 psi
Bit pressure loss	234 psi
Nozzle velocity	173
Impact force	124
Bit H.P.	21

Surface H.P.	42
% H.P. at bit	52

In order to ensure that test intervals did not include the oil/water contact, a 3m interval was planned for the first DST, assuming continuous oil shows. The drilling program was to drill 3m into the Pebble Point, conduct DST No 1, then drill metre by metre in an attempt to pick the oil/water contact, conducting further DSTs until the oil/water contact was intersected.

7" casing and 2 7/8" tubing sufficient to complete the well for production testing of the Pebble Point Formation was brought to the well site prior to the completion of testing. Other completion equipment (Christmas tree, etc.), was sourced and held on standby.

5.2 PRESSURE CONTROL

Lindon No 1 intersected no reservoirs or hydrocarbons in the uppermost 110m and therefore no pressure control was considered necessary for the 12 1/4" hole. The BOP stack was to be nipped up on the 9 5/8" casing to provide pressure control for potential reservoirs to be intersected in the 8 1/2" hole. Gearhart drilling Services Rig 2 was equipped with a 13 5/8" 3000 psi spherical annular BOP, a 13 5/8" 5000 psi double gate BOP, a 160 gal accumulator, and 3000 psi choke manifold. The driller on each shift held current well control certificates. Drilling procedures followed guidelines set out in the approved Drilling Operations Manual and in the Emergency Procedures Manual.

Following cementing of the 9 5/8" casing (returns to surface observed), the BOP stack was nipped up and tested. A leak-off test was carried out when 3m of new formation had been drilled in the 8 1/2" hole. Leak-off occurred at an Equivalent Mud Weight of 16.2 ppg, which was more than sufficient for the prognosed total depth of the well, considering that no abnormal pressures were encountered in Lindon No 1.

Lindon No 2 was completed with a Canadawerks 11" 3000 psi X 7", 3000 psi "C" Tubing Spool, pressure tested to 3000 psi. The BOP stack was nipped up on the "C" tubing spool and tested to 1500 psi prior to running tubing. Prior to perforating, the whole Canadawerks Christmas tree and eah valve separately, were tested to 2000 psi against the two way check valve in the tube hanger. The lines to the wing valve on the "C" tubing spool were tested against the valve to 3000 psi.

5.3 GENERAL DATA

Well Name:	Lindon No 2
Status:	Completed as possible production well
Type of Hole:	Appraisal

Operator for tenement: Gas and Fuel Exploration N.L.

Operator for well: Taipan Exploration Pty Ltd

Tenement: PEP 105

PEP 105 permittees:
(at time of drilling) Gas and Fuel Exploration N.L.
Beach Petroleum N.L.
Victoria Exploration Inc.
Crusader Resources N.L.
Australian Hydrocarbons N.L.
Mosaic Oil N.L.

Location: Otway Basin
Southwest Victoria
30km northwest of Portland
30m south of Lindon No 1
Latitude 38 04 6.8
Longitude 141 30 54.7

Nearest well: Lindon No 1
Beach Petroleum, PEP 105, 1983/1984
30m north of Lindon No 2

Elevations: ground level 63.3m AMSL
Kelly Bushing 68.3m AMSL
Drill Floor 68.0m AMSL
Drill depths measured from kelly bushing

Total well depth: 970.0m (strapped drillers depth)
962m (loggers-unable to reach T.D.)

Spud date: 12th May, 1991 @ 0130hrs

Total depth date: 20th May, 1991 @ 2130hrs

Well completed: 25th May, 1991 @ 1345hrs

Rig released: 25th May, 1991 @ 2000hrs

Drilling Contractor: Gearhart Drilling Services Pty Ltd

Drilling Rig: G.D.S. Rig 2, Superior Model 700E SCR

Hole data: GL to KB = 4.98m
GL - 115m 12 1/4" tricone. cellar jet
115 - 970m 8 1/2" tricone

Drilling fluids: supplied by Australian Mud Company Ltd
GL - 892m bentonite (Ausgel)
892 - 970m KCl-polymer

Drill Stem tests: Halliburton Reservoir Services/Expertest
DST No 1 904.3 - 912.85m
DST No 2 902.7 - 914.1m

Wireline logging: BPB Wireline Services
 one suite only, at T.D.
 966 - 100m Dual Laterolog
 Microlog
 Microlaterolog
 Compensated Sonic
 Gamma Ray
 Caliper
 963 - 750m Photo Density
 Compensated Neutron
 Caliper
 Gamma Ray
 941 - 200m Cement Bond Log
 Variable Density Log
 Gamma Ray
 988 - 888m Gamma Ray Spec.
 CCL

Casing: 5.2 - 111.74m
 115m (9 jts) 9 5/8" JAP 43 lb/ft K55
 set @ 111.74m, cmtd to surface

Production casing: 4.9 - 962.3m
 962m (80 jts) 7" Sumitomo 26 lb/ft J55
 set at 962.3m, cmtd to 255m (by CBL log)

Production tubing: 4.8 - 894.5m
 899m (91 jts) 2 7/8" 6.5 lb/ft EUE J55
 hung above PSTD of 945m

Perforations: interval 908.1 - 911.1m
 Vann Systems 5" TCP guns

Surface completion: Canadawerks type C, 11", 3000 psi X 7 1/16"
 with "S" secondary seal and pressure
 tested to 2000 psi. Fitted with 2 1/16"
 3000 psi flanged gate valve and 2 9/16"
 and 2 1/16" 3000 psi companion flange.

5.4 RIG AND EQUIPMENT SPECIFICATIONS

5.4.1 Drilling Rig

Make/model

Superior Model 700E SCR\

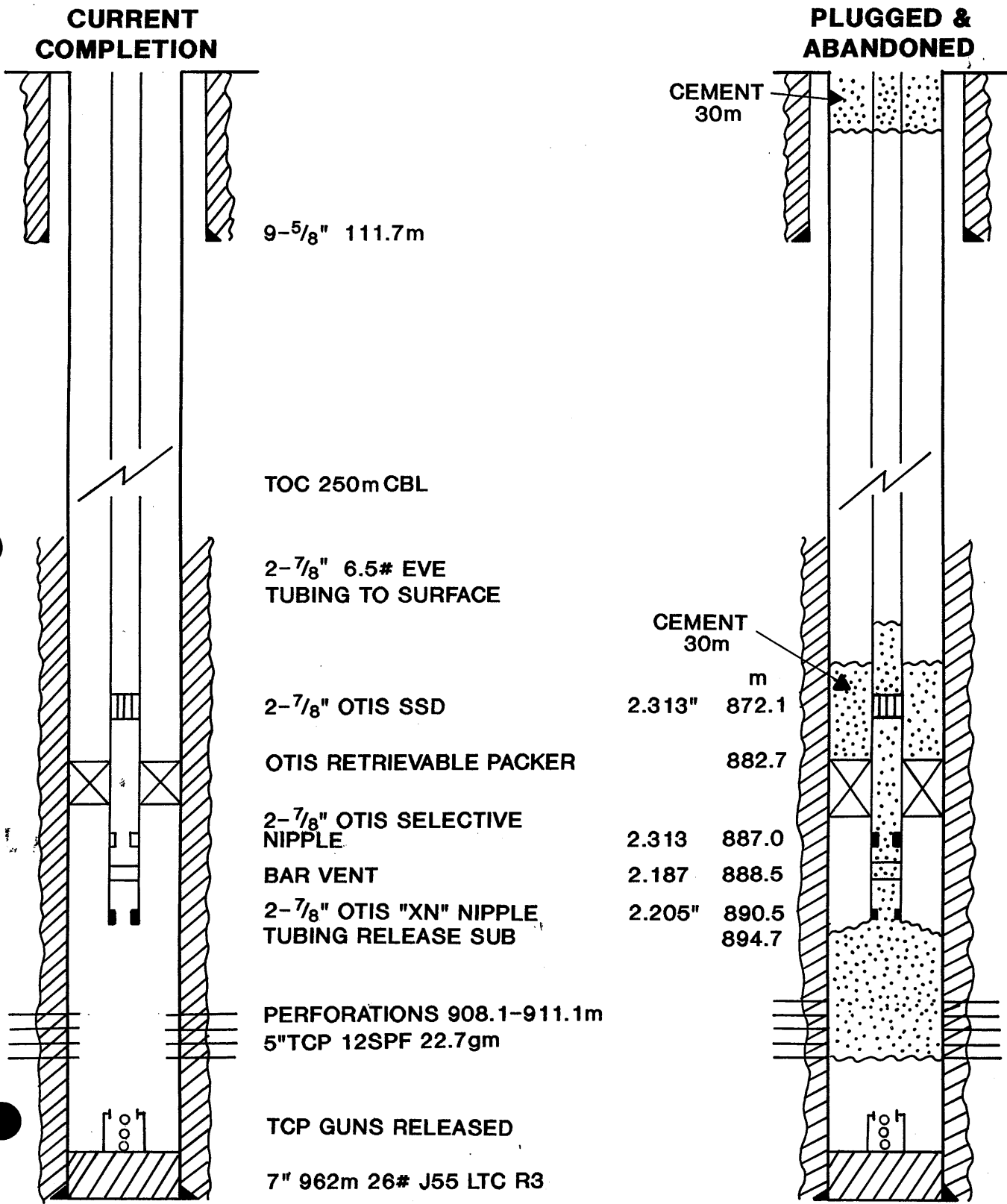
Depth capacity

11,000 ft (3350m) with 4 1/2" DP

Drawworks

SCR electric driven, complete with auxillary brake and sandreel.
 Maximum input H.P. 1000, driven by EMD motor.
 One Foster Model 37 make-up spinning cathead.
 One Foster Model 24 break-out cathead.
 Transmission-2 speed with high chain 1 1/4' triple 26t to 24t twin

PEP 105 LINDON No.2 WELLBORE SCHEMATIC



TOTAL DEPTH 970m

NOT TO SCALE
ALL DEPTHS IN mKB

disc PO218 air clutch
 -low chain 1 1/4' triple 20t to 39t twin disc PO218 air
 clutch

Engines

four Caterpillar Model 3412 PCTA diesel

Mast

Floor mounted cantilever mast Dreco - model No M1273-510 designed
 in accordance with A.P.I Specification 4E 'Drilling and Well
 Servicing Structures'.

Clear working height - 127 ft

Base width - 13 ft 6 ins

Hook load - gross nominal capacity 510,000 lbs

- capacity with 10 lines = 410,000 lbs

with 8 lines = 365,000 lbs

with 6 lines = 340,000 lbs

with 4 lines = 306,000 lbs

Maximum wind load 100 mph - no setback

Maximum wind load 84 mph - rated setback

Adjustable racking board with capacity for 108 stands of 4 1/2" DP,
 10 stands of 6 1/2" DC. 3 stands 8" DC

Crown block

215 ton with 5 X 36" sheaves and one fastline sheave grooved 1 1/8"

Substructure

One piece, 14 ft H X 13 ft 6" W X 50 ft L. 12 ft BOP clearance

Set-back 200,000 lbs, casing 210,000 lbs.

Rig lighting

explosion proof fluorescent.

Travelling block

One 667 Crosby McKissock 250 tne combination block hook

Webb Wilson 250 ton Hydra-hook unit 5 - 36" sheaves

Kelly drive

one 250 HDP Varco kelly drive bushing.

Kelly

One square kelly drive 4 1/4" X 40 ft complete with scabbard.

Swivel

One Oilwell PC-300 ton.

Rotary table

One Oilwell A 20 1/2" rotary table torque tube driven from
 drawworks.

Air compressors and receivers

Two Leroi Dresser Model 660A air ompressor packages with 10 H.P.
 motors rated at 600 V, 60 HZ, 3 phase.

Receivers each 120 gal, fitted with relief valves.

Instrumentation

One 6 pen Drill Sentry recorder to record:

weight - Martin Decker Sealtite, plus Cameron deadline type

penetration
 pump pressure
 electric rotary torque
 rotary speed
 pump SPM

One drillers console with:

Martin Decker weight indicator electric rotary torque guage
 pit scan
 SPM guage (2 per console)
 rotary RPM guage
 one set of Double Shot
 one Baroid mud kit

Drilling line

5000 ft 1 1/8" Tiger brand

Generator

Four Brown Boveri 600 V, 3 phase 60 HZ AC generators, powered by 4 Cat 3412 PCTA diesel engines.

Fuel tanks

One 140 bbl
 One 6000 gals

5.4.2 Pressure Control System

BOP's and accumulator

One Hydril 13 5/8" 3000 psi spherical annular BOP.
 One Hydril 13 5/8" 5000 psi flanged double gate BOP.
 One Galaxie 13 5/8" 5000 psi 3000 double studed daptor flanges.
 One cup tester.
 One Wagner model 130-160 3 BND 160 gal accumulator with 16 11 gal bladder bottles, 1.5gal/min auxillary air pump, hydraulic control panel with hydraulic readout guages for annukar pressure, accumulator pressure, manifold pressure.
 One Wagner model GMSB-5A 5 station remote drillers control.

Kelly cocks

One Griffith lower kelly cock
 One Griffith upper kelly cock

Drill pipe safety valve

One Griffith 6 1/2" inside blowout preventers (4 1/2" H)
 One Griffith 6 1/2" stabbing valve (4 1/2")

Choke manifold

One McEvoy choke and kill manifold 2", 3000 psi

5.4.3 Mud System

Mud tanks

One 25 bbl pill tank
 Two 108 bbls mix tanks
 One 120 bbl reserve tank
 One 120 bbl desilt tank
 One 120 bbl desand tank

LINDON No 2 : CASING SCHEMATIC

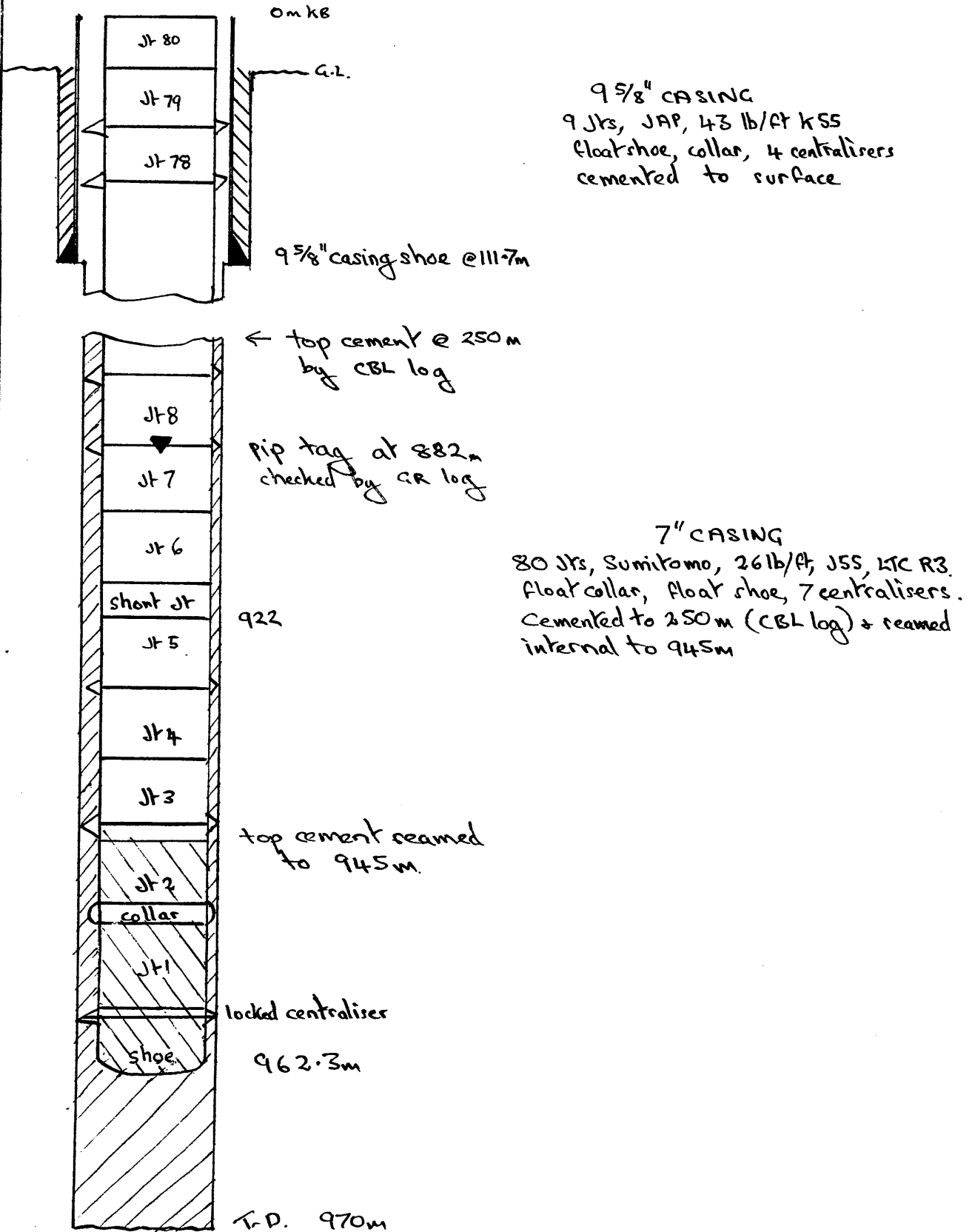


FIGURE 3

One 130 bbl shaker tank
 One 15 bbl sand trap

Water tanks

One 400 bbl

Mud pumps

One Gardner Denver model PZHVE 750 driven by 800 HP EMD motor.
 One National KSH-280 6" X 12" Duplex powered by 2 GM 6-71 engines.

Mixing pumps

Five Mission Magnum 5" X 14" centrifugal pumps complete with 50 HP
 600 V 3 phase explosion proof electric motors.

Trip tank pump

One Mission Magnum 2" X 3" centrifugal with 20 HP expl. proof motor

Mud agitators

Six Geograph/Pioneer 40 TD - 15" "Pitbull" agitators with 15 HP
 electric motors.

Shale shakers

One Brandt dual tandem shale shaker.

Desander

One Pioneer T8-6 Sandmaster desander.

Desilter

One Pioneer T12-4 Siltmaster desilter.

5.4.4 Drill Pipe and Collars

Drill pipe

1000 ft (326 jts) 4 1/2' grade E 16.60 lb/ft hard banded drill pipe

Drill collars

25 X 6 1/2" OD drill collars
 3 X 8" OD drill collars
 9 jts 4 1/2" Hevi-wate drill pipe

5.5 CASING AND CEMENTING

5.5.1 Surface Casing

See Figure 3

9 joints (115m) 9 5/8" JAP 43 lb/ft K55 with float collar, float
 shoe and 4 centralisers.

RT-casing head: 5.2m, set at 111.72m.

Cemented to surface (cement returns observed)

150 sx class A cement in 19 bbls water at 2% CaCl₂ (40% excess),
 displaced with 25 bbls water, 1000 psi

Cement tagged at 91m, float at 99.7m, shoe at 111.7m

Formation integrity test achieved 16.2 ppg equivalent mud weight

5.5.2 Production Casing

See Figure 3
 80 joints (962m) 7" Sumitomo 26 lb/ft J55 LTC R3 with float collar,
 float shoe, 7 centralisers.
 Top float collar at 947m
 Pip tags at 882.7m-driller, 882m-CBL/gamma
 RT-casing spool 4.9m to casing shoe at 962.3m
 Cemented to 255m (from CBL log)
 Internal cement reamed to 945m
 Lead slurry (750-255m) 12 lb/gal
 Tail slurry (970-750m) 15.7 lb/gal

5.5.3 Production Tubing

See Figure 4
 91 joints (899m) 2 7/8" 6.5 lb/ft EUE J55
 Pip tag at 882.7m on top of packer (882.8m by GR/CCL log)
 Hung above PBT of 945m
 Mechanical tubing release at 894.7m
 Top shot at 908.1m

5.6 COMPLETION

5.6.1 Bottom Hole Completion

See Figure 4
 Completion interval 908.1 - 911.1m - top 3m of Pebble Point Fm.
 Single packer, single string (2 7/8"EUE)
 Provision for rod pumping - rod pump to be landed in top profile of
 opened sliding sleeve.
 Perforations carried out under drawdown.
 5" TCP guns run on dry tubing and loaded at 12 spf with 22.7 gm RDX
 charges.

5.6.2 Surface Completion

See Figure 5
 Canadawerks Type "C" 7 1/16" 3000 psi X 11" with Type "S" secondary
 seal, Barton 2 1/16" 3000 psi gate valve at 9 5/8" casing head,
 Barton 2 1/16" 3000 psi flanged gate valve at tubing spool, Barton
 2 9/16" 3000 psi flanged gate master valve to Cameron 2 9/16" 3000
 psi wing valve and 2 1/16" 3000 psi RX24 companion flange and 2
 9/16" 3000 psi well cap.

5.7 DRILLING FLUIDS

5.7.1 Supply and Control

All drilling fluids were supplied by Australian Mud Company
 Limited, which company also provided a recommended mud program.
 Australian Mud Company also provided an experienced mud engineer
 who supervised preparation and maintenance of all drilling muds
 during the drilling operations and prepared a daily mud report.
 Mud tests were carried out on a routine basis. Full tests were
 carried out by the mud engineer three times per day and basic
 parameters checked by the drillers 3 times per drilling shift.
 Drilling fluids were supplied from Adelaide.

Company: TAIPAN PETROLEUM LINDBON # 2 Well Name: Field: Type L/OS: BOTTOM HOLE COMPLETION
 Country: STG Perforations: Temp: PBTD

AUSTRALIA 12 SPF

Completion Comp Test Single Fluid Type + #
 Workover DST Dual RAM at TOP Shot

Tubing	Size	Weight	Grade	Thread	Depth
	2 7/8	6.5	J-55		
Casing					
Liner					
Workstring					

No.	Description	Depth	Length	O.D.	I.D.
	2 7/8 EUE TUBING TO SURFACE				
	OTIS SLIDING SLEEVE	872.06	0.975		
	1 JOINT 2 7/8 EUE	873.04	9.663		
	RADIO ACTIVE MARKER	882.70	-	-	-
	OTIS RETRIEVABLE PACKER	882.70	1.155		2.50
	10' 2 7/8 EUE PUP JOINT	883.86	3.085		
	OTIS SELECTIVE LANDING NIPPLE	886.95	0.37		2.313
	4' 2 7/8 EUE PUP JOINT	887.32	1.17		
	MAXIMUM DIFFERENTIAL BAR VENT	888.49	0.735	3.875	2.187
	4' 2 7/8 EUE PUP JOINT	889.22	1.245		
	OTIS XN NIPPLE	890.47	0.395		2.205
	10' 2 7/8 EUE PUP JOINT	890.86	3.85		
	MECHANICAL TUBING RELEASE	894.71	0.51	3.375	2.25
	LATCH 2.25				
	4' 2 7/8 EUE PUP JOINT	895.22	1.185		
	X-OVER 2 7/8 EUE BOX X 2 3/8 EUE PIN	896.41	0.16		1.99
	1 JOINT 2 3/8 EUE TUBING	896.57	9.665		1.99
	2 3/8 MECHANICAL FIRING HEAD	906.23	1.515	3.375	1.56
	SAFETY SPACER	907.75	0.25	5.00	-
	TOP SHOT	908.1	-	-	-
	INTERVAL, 5m 12 SPF, 22.7GM		3.00	5.00	-
	BOTTOM SHOT	911.1	-	-	-
	BLANK SECTION		0.23	5.00	-
	BULL PLUG		0.05	5.00	-

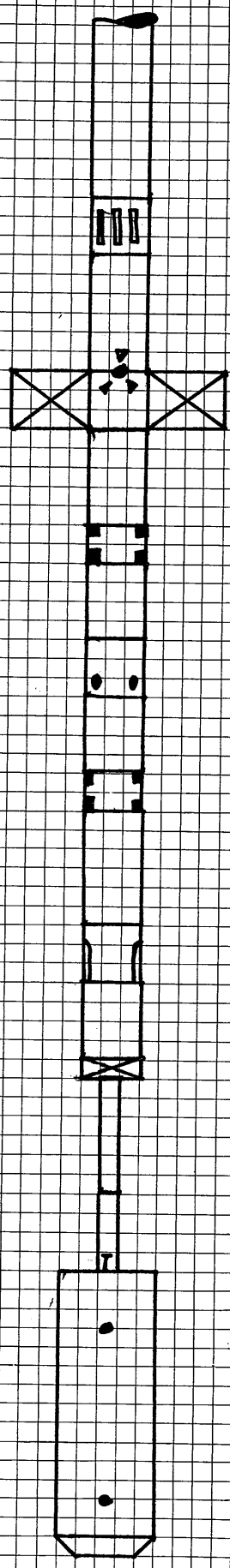


FIGURE 4

LINDON NO. 2 - WELLHEAD SKETCH

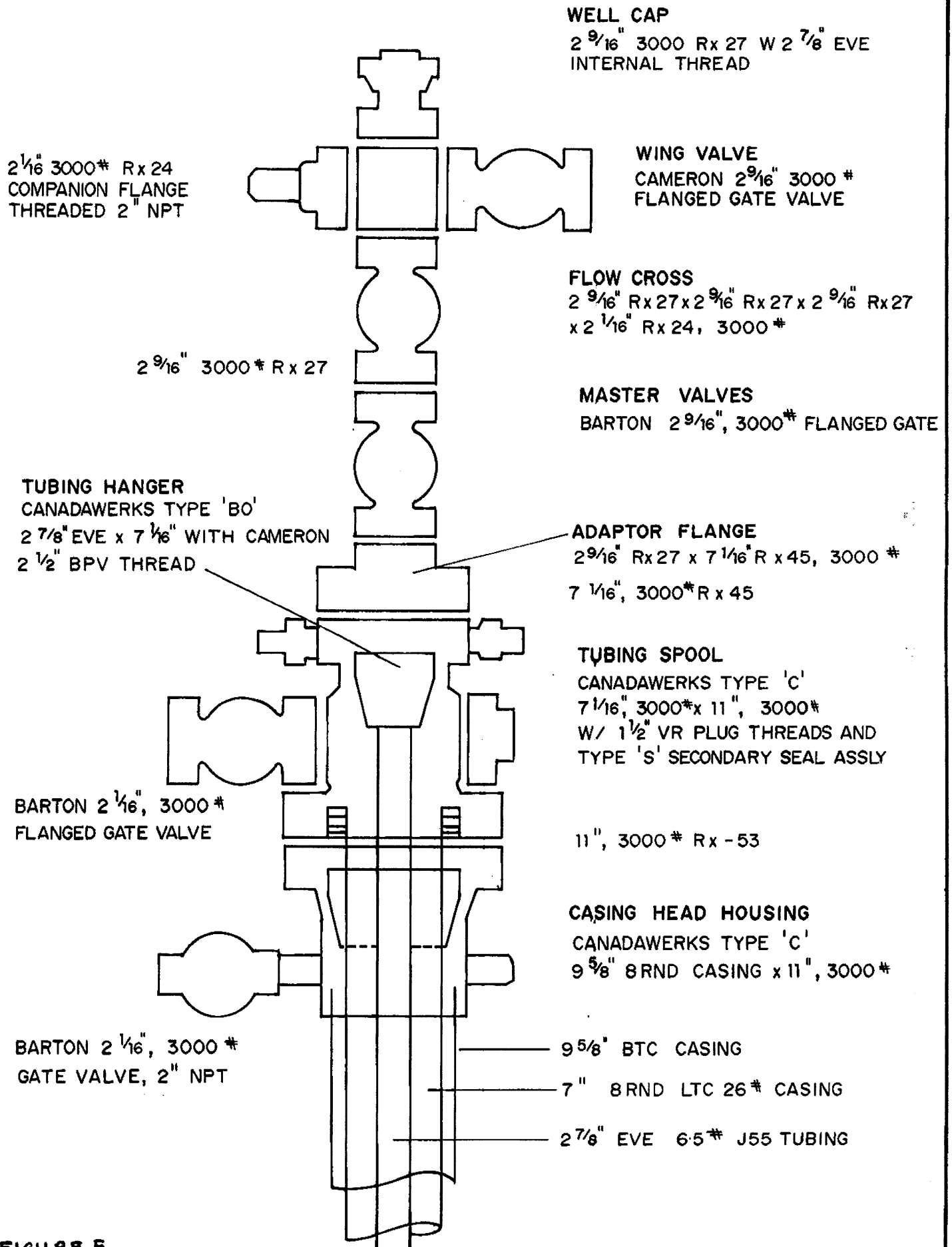


FIGURE 5

5.7.2 Hole Above Target Reservoir (surface to 891m)

No hole problems were anticipated for the formations overlying the Pebble Point and a simple, cheap mud was considered adequate. The 12 1/4" hole and 8 1/2" hole to 891m were drilled using a simple bentonite mud system. A full volume of mud (400+ bbls) was used comprising Ausgel with minor soda ash and caustic soda for control of pH and hardness. The high clay content of the formations drilled necessitated heavy dilution to maintain the required mud weight and viscosity. Little control of filtrate loss was possible. From 719m CMC-EHV was added to reduce the filtrate loss. Solids control was limited by breakdown of the desander and desilter and this necessitated some dumping and make up of additional new mud.

5.7.3 Drilling From 891m to T.D.

Evaluation of Lindon No 1 well core from the Pebble Point indicated the presence of smectite clays and that these clays suffered significant swelling by contact with the drilling fluid. The mud program for Lindon No 2 was designed to minimise possible swelling by using a completely fresh KCl-polymer mud to drill the target zone, maintaining strict control of the fluid loss and pH. KOH was used instead of NaCl to reduce dispersive effects.

At 891m the hole was circulated clean, a high viscosity pill pumped and the drill bit pulled to the casing shoe. All mud was dumped, the mud tanks cleaned and a complete new polymer mud comprising KCl, Drill-Pac, Aus-Dex, and KOH. This mud was conditioned and used to drill through the Pebble Point Formation target reservoir with API filtrate at 6.0 cc and 6% KCl. The filter cake was tough and thin. High viscosity pills were pumped prior to both DSTs.

DRILLING FLUID PARAMETERS

PARAMETER	PREFERRED RANGE	ACHIEVED RANGE
<u>TOP HOLE</u> (surface to 891m)		
mud weight (ppg)	8.7 - 9.2	8.5 - 9.2
viscosity (sec/qt)	38 - 48	38 - 48
pH	9.0 - 9.5	9.5
API filtrate (ml/30 min)	below 15cc	12 - 22
yield point (lb/100 sq ft)	8 - 10	10 - 16
sand (%)	0.5	tr - 1
<u>RESERVOIR</u> (891m to TD)		
mud weight (ppg)	8.9 - 9.1	8.7 - 8.9
viscosity sec/qt)	45 - 48	45 - 49
pH	9.0	9.5 - 9.6
API filtrate (ml/30 min)	below 8cc	4.2 - 6.0
yield point (lb/100 sq ft)	6 - 8	15 - 20

5.7.4 Drilling Fluid Consumption

ITEM	PROGNOSED CONSUMPTION	ACTUAL CONSUMPTION
<u>Surface - 891m</u>		
Aus-Gel	250 X 25 kg	236 X 25 kg
CMC-EHV	5 X 25 kg	9 X 25 kg
Soda ash	3 X 25 kg	3 X 25 kg
Caustic soda	5 X 25 kg	2 X 25 kg
<u>891m - TD</u>		
DrillPac	20 X 50 lb	20 X 50 lb
Aus-Dex	48 X 25 kg	60 X 25 kg
KOH	9 X 25 kg	6 X 25 kg
KCl	240 X 25 kg	280 X 25 kg
Aus-Gel	nil	

5.8 WATER SUPPLY

Drilling water was supplied from a water bore located approximately 700m from the well site and on the same property. water was carted on request by the landholder using a 10,000 gal tank on a tip truck. analysis data of fthe bore water showed normal salinities and that the water was suitable for drilling and cementing.

5.9 ROP AND DRILLING BITS

High rates of penetration (up to 0.5 min/m) were achieved in the predominantly very soft, unconsolidated Tertiary sediments except where bit balling occurred. ROP slowed dramatically in hard basalt/dolerite bands where the stabilisers tended to hang up. ROP was deliberately slowed whilst drilling the target reservoir.

The 12 1/4" hole was drilled with one Reed HP 12J bit. Three bits were used for the 8 1/2" hole, two R.B.I. HP 2 and one used Varel L116. Excessive bit wear in the 8 1/2" hole resulted from bit balling caused by the very sticky nature of the Teriary marls and by damage drilling very hard basalt/dolerite horizons. Bit details are given in the Bit Record.

5.10 DEVIATION RECORD

Hole deviation was measured using a Totco "Godevil". Surveys were conducted at 50m intervals in the 12 1/4" hole and at 100m intervals in the 8 1/2" hole. Maximum measured hole deviation was 1 deg. at total depth.

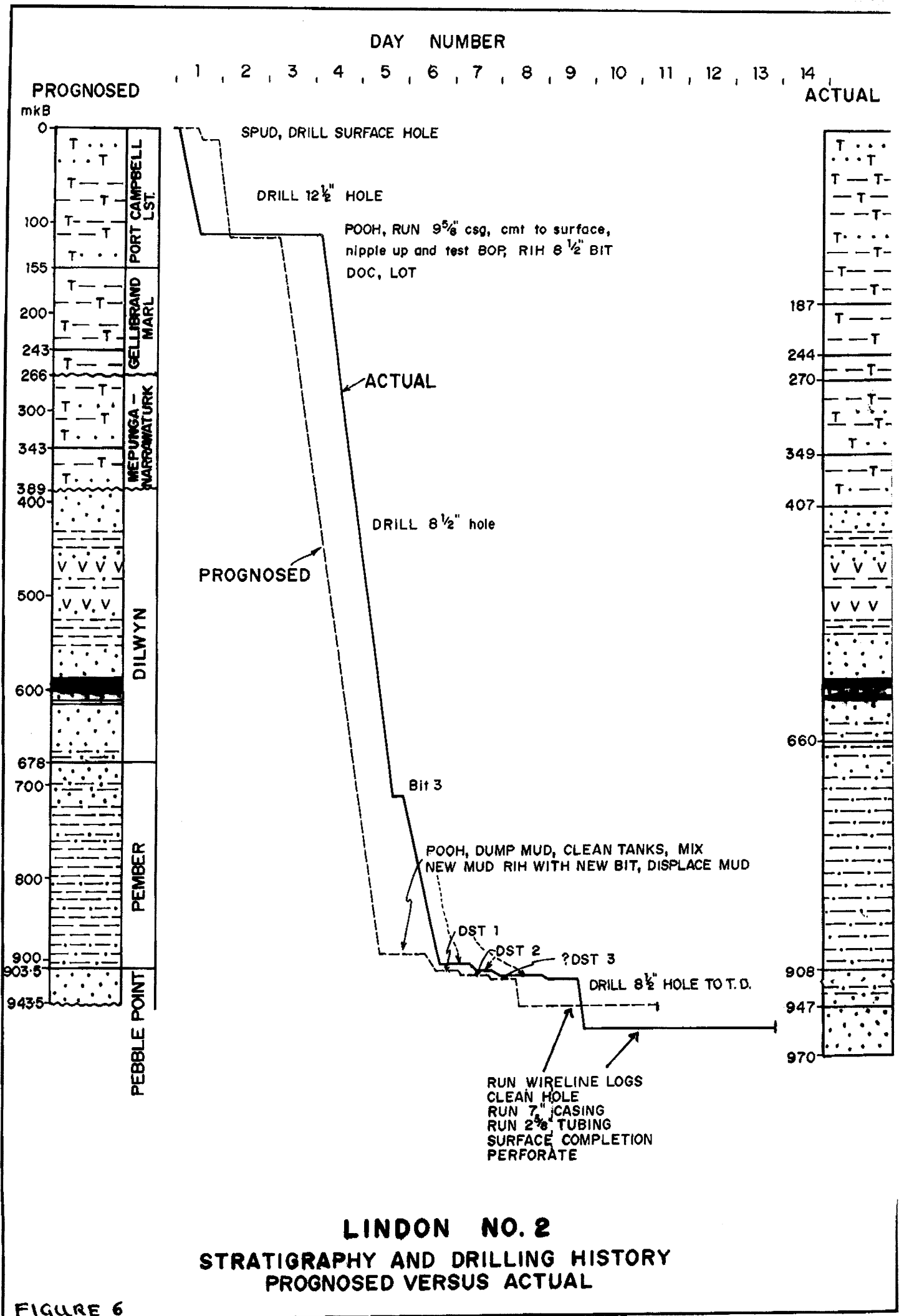
DEVIATION RECORD	
DEPTH (m)	DEVIATION (deg.)
24	0.75
58	0.75
103	0.25
216	0.25
311	1.0
548	1.0
879	0.75
970	1.0

5.11 TIME DISTRIBUTION

Lindon No 2 was completed in 14 days from spud-in, 3 days behind schedule. The most significant delays were caused by delays during drilling. The prognosed time to drill to 891m was 4 days. Actual time was 6.7 days. The main causes of drilling delays were repairs to the rigs BOPs and choke manifold valves (23 hrs), which were seized following 18 months rig stacked time close to the ocean, and problems with the rigs SCR (silicon controlled rectifier) power system. Time distribution is summarised in the table below and in Figure 6.

DRILLING TIME DISTRIBUTION

ITEM	PROGNOSSED TIME (hours)	ACTUAL TIME (hours)
drill 12 1/4" hole	8	14
drill 8 1/2" hole	64	85
run, cmt casing, etc	72	117
new mud	24	15.5
drill stem tests	36 for 3 DSTs	26.5 2 DSTs
downtime	8	28.5
spud-in to rig-down	10 days	14 days



LINDON NO. 2
STRATIGRAPHY AND DRILLING HISTORY
PROGNOSED VERSUS ACTUAL

FIGURE 6

GEOLOGICAL DATA

6.1 OBJECTIVES

6.1.1 Outline of Play

Lindon No 2 was drilled to re-test the hydrocarbon occurrence intersected in the Pebble Point Formation by Lindon No 1 drilled in 1983/1984 by Beach Petroleum N.L.

Petrographic studies of a core obtained from the upper portion of the Pebble Point Formation in Lindon No 1 (912.5 - 917.0m) identified a matrix of kaolin, smectite and chlorite. The studies indicate that Smectite is a major component in the upper portion of the reservoir. The Pebble Point Formation in Lindon No 1 was drilled using drilling parameters and mud condition which were not well suited to a reservoir containing hygroscopic clays. High pump pressures and rates, together with a high water loss (17.5 cc/30 min), appear to have caused significant reservoir damage. Although cuttings and core from the Pebble Point in Lindon No 1 indicate that the uppermost 6 metres has good porosity and 40% fluorescence was observed, two Drill Stem Tests produced very poor results, recovering only oil and gas cut mud.

The Lindon No 2 test was designed around the premise that formation damage resulted in the Pebble point Formation reservoir failing to flow in Lindon No 1. Lindon No 2 was therefore designed to retest the uppermost Pebble Point Formation using drilling and mud parameters which would minimise hydraulic impact and water loss to the reservoir, significantly reducing the possibility of smectite swelling and other formation damage.

6.1.2 Structure

No additional seismic has been carried out to re-evaluate the Lindon Prospect since the drilling of Lindon No 1. The Lindon Prospect is defined by 4 seismic lines of the Beach petroleum 1983 Denhelm survey and by reprocessed data from 2 1972 Shell lines. The seismic data was re-interpreted by Taipan Petroleum to more accurately locate Lindon No 2 over the crest of the local subclosure at Pebble Point level.

Lindon No 1 was located close to the crest of a closed NW-SE anticlinal structure at base Tertiary level (see Figures 7, 9). Seismic mapping of the Pebble Point/ base Tertiary horizon shows broad horst-block like structuring in the Lindon Prospect area. Taipan Petroleum mapped subtle NW-SE rollover at Pebble Point level independent of faulting (see Figure 8). Fault independent aerial closure was estimated at approximately 5 sq km with 94m vertical relief.

The seismic data indicates thickening of the Pember Mudstone and Sherbrook Group on the downthrown side of the northern fault indicating development during the Upper Cretaceous and during Pember Mudstone deposition.

Lindon No 2 was located 40m to the south of Lindon No 1 to test the

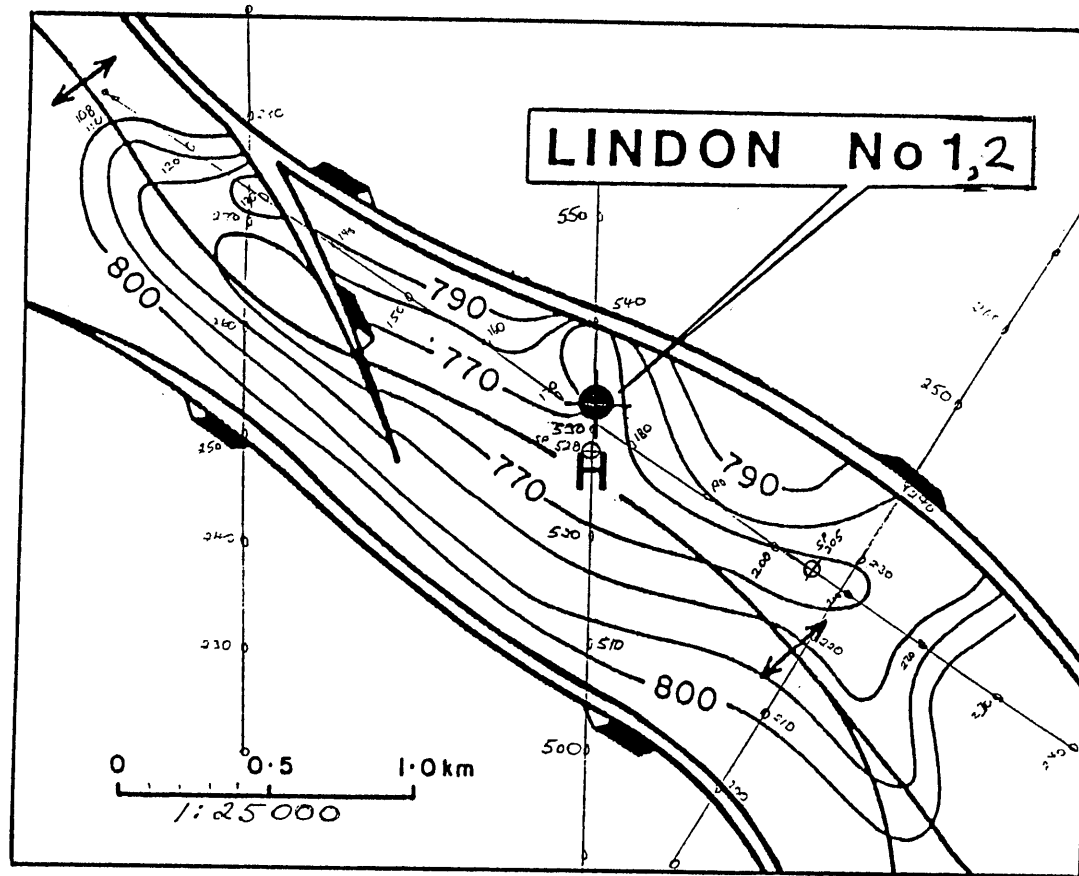


Figure 7: Time structure map on top of the Pebble Point Formation (contour interval: 10 milliseconds).

TWT STRUCTURE AT PEBBLE POINT FORMATION

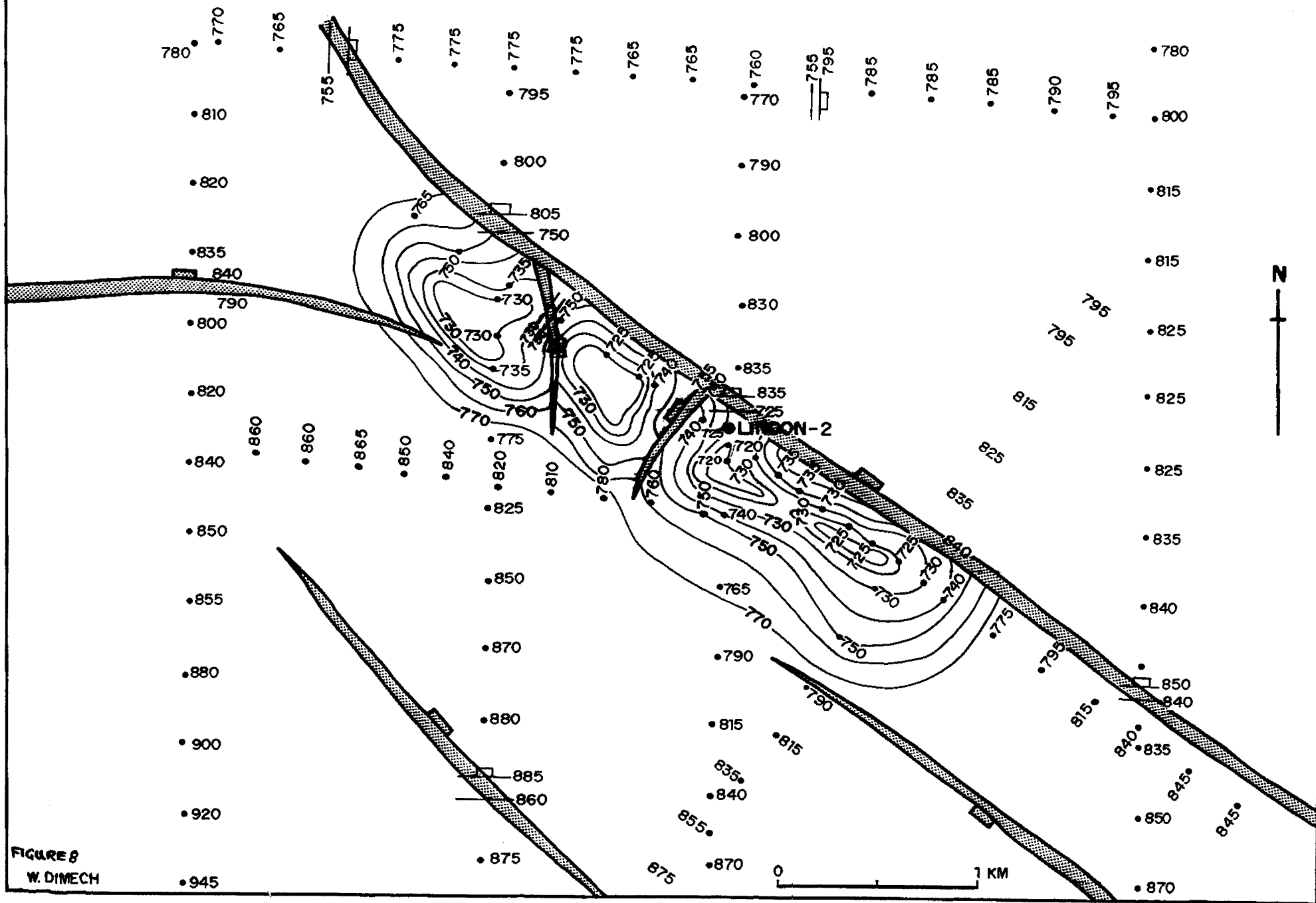


FIGURE 8
W. DIMECH

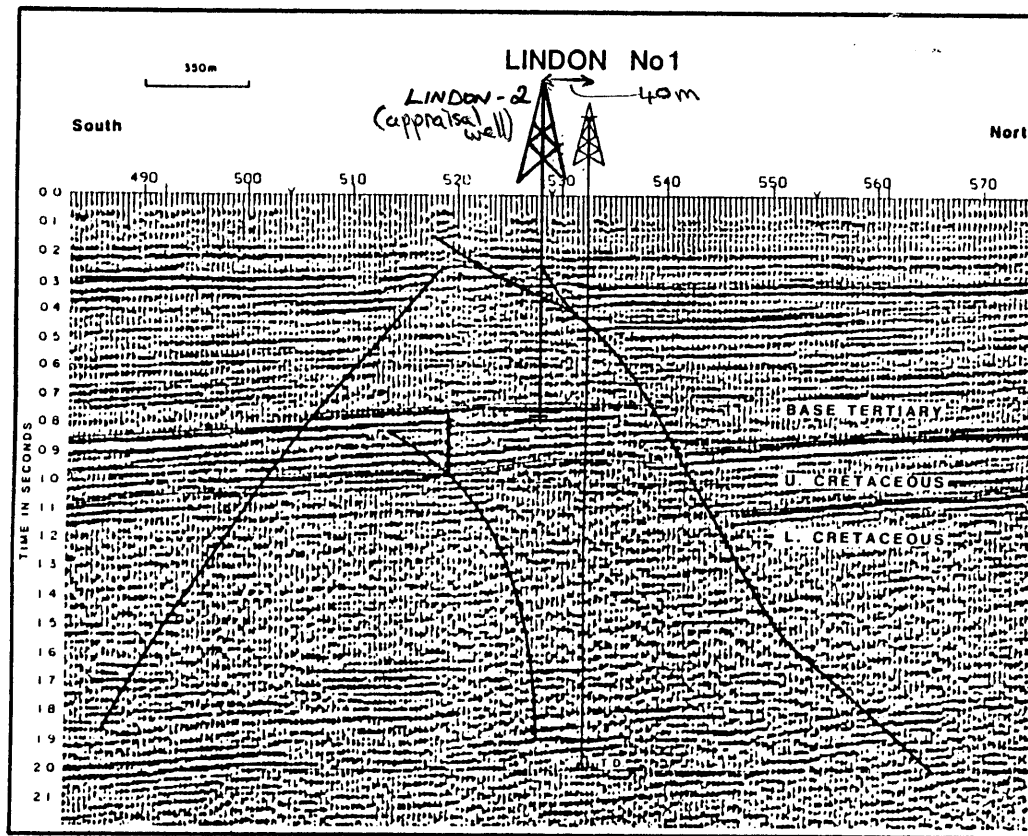


Figure 9: Seismic line over the Lindon structure.

same hydrocarbon occurrence at a re-interpreted crest of the structure at Pebble Point level.

6.2 STRATIGRAPHY

6.2.1 Introduction

The stratigraphy of Lindon No 2 is the same as that intersected to 970m in Lindon No 1 located 40m to the north. Stratigraphic tops and thicknesses are shown in the Stratigraphic Table and the prognosed Stratigraphy is shown as Figure 10. Lithological descriptions and wireline log data for the formations intersected are shown at 1:1000 scale on the Composite Well Log (Enclosure 1).

No palaeontological examination has been made of Lindon No 2 cuttings and the stratigraphy described here is based on comparison of the cuttings descriptions and wireline logs with those from Lindon No 1 where palaeontology was completed. There are discrepancies between the prognosed and actual stratigraphic tops because the prognosis was based on the Lindon No 1 well summary sheet which gives depths for tops which significantly vary from those determinable from the wireline logs and palaeontology.

6.2.2 Upper Cretaceous Sherbrook Group

Paaratte Formation (947m - 970mTD: 23+m thick)

Lindon No 2 was terminated 23m into the Paaratte Formation to gain sufficient depth to enable a completion in the Pebble Point Formation. The lithology is all sandstone; clear to translucent, generally loose, medium to coarse grained, subround to occasionally subangular and moderately well sorted. There is a trace of argillaceous matrix and minor calcite cement. Pyrite/marcasite nodules are common. During drilling the top of the formation was observed as an abrupt change from siltstone of the overlying Pebble Point to a clean sandstone with an accompanying drilling break.

6.2.3 Tertiary Wangerrip Group

Pebble Point Formation (908m - 947m: 39m thick)

The lowermost 12m of the formation is a dark greyish brown argillaceous and slightly carbonaceous siltstone which occasionally grades to light grey - greyish brown claystone. The upper 27m is sandstone: clear to white, loose to friable, occasionally hard, fine to coarse grained, subangular to subround, poorly to moderately well sorted. There is a minor silt matrix and minor silica and calcite cements. The distribution of cement is very variable. The uppermost 4m which is probably the best reservoir with the best oil show was described as being clear to frosty, very light grey to light brown in part, loose, occasionally friable to firm, fine to very coarse grained, occasionally granular, dominantly medium to very coarse grained, subangular to subround, poorly sorted quartz, trace to common light greyish brown and occasionally light grey argillaceous matrix, rare siliceous and calcareous cements, rare pyrite. The contacts with the overlying and underlying units, the Paaratte Formation and Pember Mudstone Member are sharp and distinct indicating disconformable or unconformable relationships. During drilling the top of the Pebble

Point was observed as an abrupt change from claystone of the overlying Pember Mudstone to sandstone accompanied by a marked drilling break.

Pember Mudstone Member (660m - 908m: 248m thick)

This is a fine grained unit. Brownish grey to olive grey dispersive claystone, commonly grading to arenaceous siltstone is dominant. The claystone and siltstone are finely carbonaceous, micaceous and there are common fossil fragments. There is a patchy calcite cement. Minor sandstone is light grey, predominantly fine grained, subangular to subround, moderately well sorted, with an argillaceous matrix. The top of the Pember Mudstone was observed during drilling as a change from sandstone of the Dilwyn Formation to a clayey siltstone with a decrease in ROP.

Dilwyn Formation (407m - 660m: 253m thick)

The Dilwyn Formation is predominantly quartz sandstones with minor volcanics and minor siltstone. The sandstones are generally clear, loose, medium to very coarse grained, mostly coarse grained, subangular to subround, moderately to poorly sorted. There is trace to minor argillaceous matrix, minor argillaceous flakes and minor pyrite. Thin volcanic layers of basaltic composition are probably extrusive basalts but may be dolerite sills or dykes. The volcanics are mostly dark greenish grey to black mottled dark greyish brown, very hard, subvitreous, cryptocrystalline to finely crystalline. Dark mafic minerals are abundant with minor possible pyroxene and white feldspar. Pyrite is common. The volcanic layers are very distinctive on the wireline logs and on the Masterlog ROP plot (see Enclosure 1). The siltstone is dark greyish brown, soft to firm, carbonaceous, clayey and arenaceous. The top of the formation was identified during drilling by an abrupt change from the firm to moderately hard calcarenite of the overlying Mepunga Formation to uncemented sandstone with an associated moderate drilling break.

6.2.4 Tertiary Nirranda Subgroup and Heytsbury Group

Mepunga Formation (349m - 407m: 58m thick)

This formation is interbedded calcarenite/limestone and marl. The calcarenite grades to sandy limestone and is orange to light brown and firm to moderately hard with clear, very fine to fine grained, subangular to subround, quartz grains, minor glauconite, fossil fragments and pyrite. The marl is a medium grey to greenish grey very soft claystone. The top of the Mepunga Formation was observed during drilling as a change from the marl of the overlying Narrawaturk Formation to a harder carbonate cemented unit (calcarenite and limestone).

Narrawaturk Formation (270m - 349m: 79m thick)

In Lindon No 2 the Narrawaturk Formation is marl with minor calcarenite. The marl is a light grey to greenish grey, very soft, sticky, calcareous claystone and siltstone. The calcarenite is light grey to pale orange, firm, limonitic, and has common fossil fragments. The formation top was difficult to pick during drilling. It is discernable on the wireline logs as the marl underlying the Clifton Formation calcarenite.

Clifton Formation (244m - 270m: 26m thick)

This formation is a limestone/calcarenite. It is light grey to greyish orange, hard, finely crystalline with abundant quartz sand grains and abundant fossils.

Gellibrand Formation (187m- 244m: 57m thick)

The Gellibrand Formation is very soft marl with minor interbedded calcarenite. The lithologies are very similar to those of the underlying and overlying units.

Port Campbell Formation (surface - 187m: 187m thick)

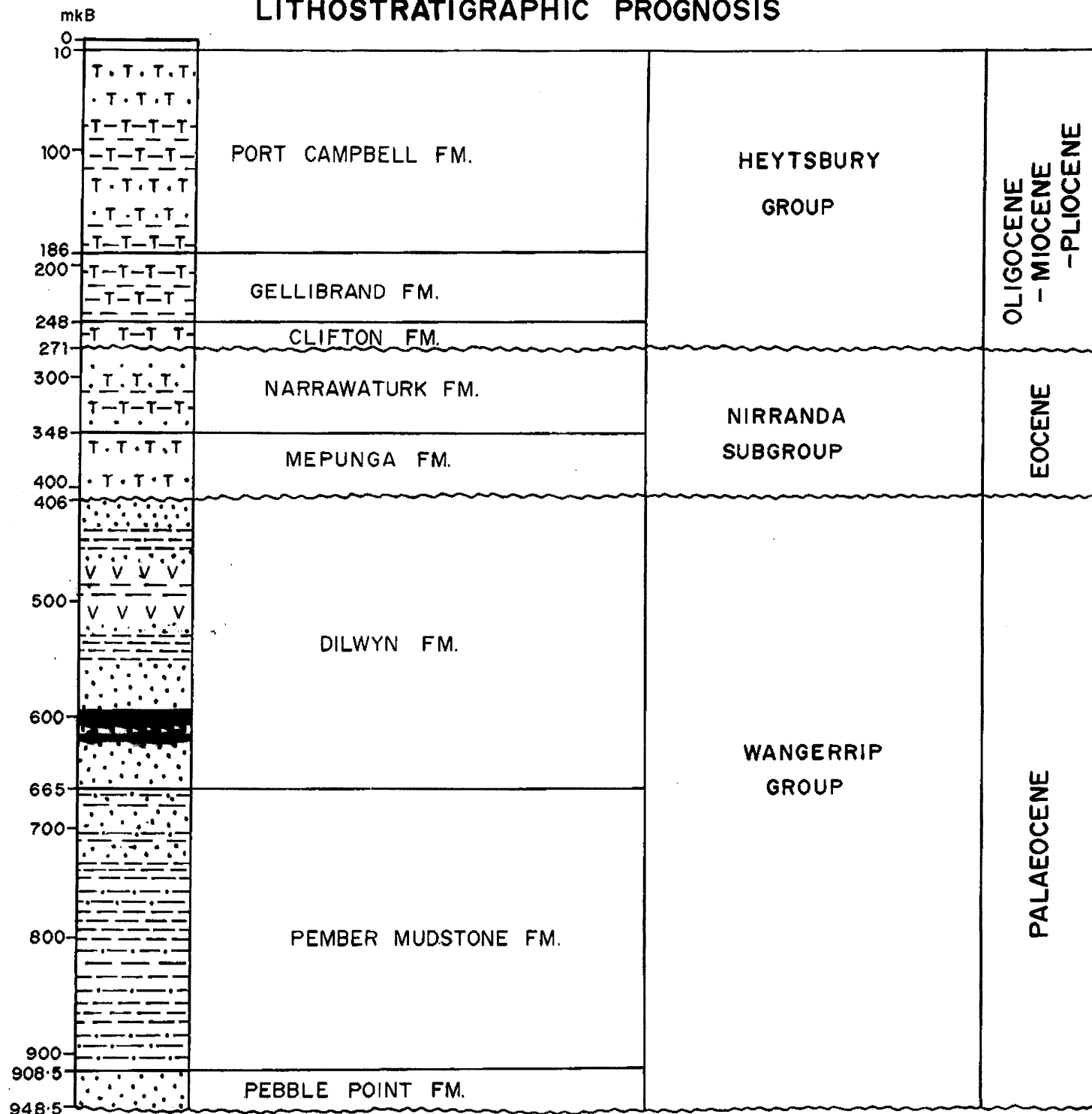
This formation is dominantly firm calcarenite and minor very soft marl. The lithologies are very similar to those of the underlying units.

LINDON No 2 STRATIGRAPHIC THICKNESSES

AGE	FORMATION	TOPS		THICKNESS (m)
		DRILL (mKB)	SUBSEA (m)	
HEYTSBURY GROUP				
Pliocene)	Port Campbell Fm.	5m	63	182
Miocene)	Gellibrand Fm.	187	-119	57
Oligocene)	Clifton Fm.	244	-176	26
NIRRANDA SUB-GROUP				
Eocene	Narrawaturk Fm.	270	-202	79
	Mepunga Fm.	349	-281	58
WANGERRIP GROUP				
Palaeocene	Dilwyn Fm.	407	-339	253
	Pember Mudstone Mbr.	660	-592	248
	Pebble Point Fm.	908	-840	39
SHERBROOK GROUP				
Cretaceous	Paaratte Fm.	947	-879	23+
	TOTAL DEPTH	970	-902	-

note: M.S.L. = seismic datum
 KB = 68.3m
 G.L. = 63.3m
 drilling depths measured from kelly bushing (KB)
 maximum well deviation = 1 deg.
 thicknesses uncorrected for deviation

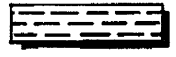
LINDON NO. 2 LITHOSTRATIGRAPHIC PROGNOSIS



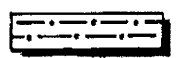
TD ≈ 950m
(base of Pebble Point)



MARL



CLAYSTONE



SILTSTONE



SANDSTONE



COAL



BASALT / DOLERITE

FIG. 10 LINDON NO. 2
TAIPAN PETROLEUM

6.3 HYDROCARBONS

6.3.1 Reservoir Potential

The reservoir potential, based on visible porosity observed from cuttings and logs and on seal relationships are described below by formation.

Paaratte Formation: 23m intersection of generally loose, coarse grained, well sorted quartz sand with only a trace of argillaceous matrix and very minor, patchy, calcite cement. Very good to excellent inferred porosity. Neutron porosity curve indicates approximately 25% porosity (limestone units). The Paaratte could be sealed by the 12m siltstone and claystone interval at the base of the Pebble Point, but local faulting may violate the seal. The Paaratte intersected has good reservoir potential.

Pebble Point Formation: uppermost 27m is loose to friable and occasionally hard quartz sandstone. Loose sand grains in cuttings, particularly from 908.0 - 911.0m and 911.3 - 919m, infer a good porosity. Friable to hard silica cemented cuttings fragments, from 911.0 - 911.3m and below 919m, were observed to have a poor porosity. The bimodal grainsize distribution (fine and coarse), poor to moderate sorting, and presence of hygroscopic clay matrix minerals, indicate a variable, but overall moderate reservoir potential for the 27m interval and a good reservoir potential for the interval 908.0 - 911.0 and 911.3 - 915m. The neutron porosity log shows variable porosity values of between 25% and 35% limestone porosity units for this interval. The 248m thick marl of the overlying Pember Mudstone forms an excellent seal to the sands of the Pebble Point.

Dilwyn Formation: Intervals of up 55m thick consisting of loose, mostly coarse grains of quartz with only traces of matrix and cement. Inferred porosity is very good. The 400m of marls and calcarenites of the overlying Nirranda Subgroup and Heytsbury Group form an effective seal. The Dilwyn Formation has good reservoir potential.

6.3.2 Hydrocarbon Shows

The anticipated oil show was observed in the Pebble Point Formation. Oil stained cuttings were observed over the interval 908 - 919m. Visible hydrocarbon in the cuttings occurred as a pale yellowish brown stain on sand grains. 50% natural fluorescence occurred over the interval 980 - 915m, decreasing below 915m to 5% at 919m. The fluorescence was moderately bright yellowish gold. The crush cut was instantly diffusing to streaming, moderately bright pale yellowish white to pale bluish yellow. From 908 - 916m there was a gas show of 28.6 units against a background of 0.5 units with corresponding high values of C1 to C5 on the chromatograph. The wireline log data (see Enclosure 2), shows no definite indication of the presence of hydrocarbons.

6.3.3 Testing and Completion

Drill Stem Test data is included as Appendix 2. Drill stem tests No 1 and No 2 failed to test the capability of the Pebble Point reservoir to flow hydrocarbons. Data gained from the drilling of Lindon No 1 and Lindon No 2 indicate a variable quality reservoir containing a high poor point, waxy oil, with an oil/water contact at Lindon No 1, inferred from DST data and core, at 917.5m. Hydrocarbons and an oil/water contact are not evident in the wireline log data for either well. In Lindon No 2, cuttings fluorescence indicated oil only to at least 915m, decreasing fluorescence to 919m and patchy good visible porosity from 908 to 919m with a hard cemented horizon between 911.0 and 911.3m. The decision was made to complete Lindon No 2 over the 3m interval 908.1 to 911.1m to ensure exclusion of the oil/water contact. Following completion over this interval the well did not flow. Swabbing and static gradient surveys indicated a very slow rate of influx.

6.4 SAMPLING AND SAMPLE EXAMINATION

6.4.1 Well Monitoring

The well was monitored by a standard pressurised mudlogging unit manned by one mudlogger per shift. The unit monitored hydrocarbon gases by continuous sampling at the possum belly located between the flowline and shale shakers. Analysis was by hot wire detector and by Carlo Erba 4200 automatic gas chromatograph which was regularly calibrated. A kelly bottle system was used to monitor ROP. Alarm activating pit volume indicators measured mud levels in the return and active pits and counters monitored pump strokes on pumps 1 and 2. Chromatograph, total gas, active mud pit level, ROP, and pump stroke data were continuously recorded on chart paper by multipen plotter.

6.4.2 Sampling

Shaker samples were taken at 10m intervals to 400m and at 5m intervals from 400m to total depth. A small portion of each sample was washed for examination. The remainder of each sample was split into 2 portions and placed in properly labelled calico sample bags and dried. On completion of the well, one set of samples was submitted to the Petroleum Group, Victorian Department of Manufacturing and Industrial Development and another set to Gas and Fuel Exploration N.L.

No cores were taken. DST No 1 and No 2 failed and no fluids suitable for sampling were recovered.

6.4.3 Sample Examination

Cuttings samples were examined under ultra-violet light for fluorescence and then described following examination under low powered binocular microscope. The description was entered on the mudlog at 1:500 scale and is included at reduced scale (1:1000) as part of the Composite Log (Enclosure 1).

6.5 WIRELINE LOGGING

Because Lindon No 2 was drilled only 40m from Lindon No 1 only limited wireline logging, sufficient to meet the wells objective, was carried out. At total depth 2 conventional oil-field logging runs were completed. The data from these runs is included as Appendix 2. The loggers were able to reach 966m, 4m short of total depth. Run 1 recorded dual laterolog, microlaterolog, sonic, gamma ray and caliper from 966 to 100m. Run 2 recorded density, neutron, caliper and gamma ray across the Pebble Point reservoir from 963 to 750m. The general characteristics of the log curves agree with those from Lindon No 1. Formation tops appear 2m shallower than shown on the Lindon No 1 Composite Log which gives a different kelly bushing elevation than the well summary sheet. The Lindon No 2 deep and shallow laterolog curves show little separation and actually overlay each other through the Pebble Point where drilling hydraulics were optimised to reduce formation damage and to produce an in-gauge hole.

Wireline logging was also used to assist completion of the well. The cementing of the 7" casing and location of radioactive pip tags were checked using the cement bond log, variable density log, and gamma ray. The position of the tubing conveyed perforating guns was checked using the GRS and CCl logs. Following perforating the loggers wireline was used to detect the fluid level in the tubing and to detect if the fluid was oil or water.

7

CONTRACTORS & SERVICES

DRILLING	Gearhart Drilling Services Pty Ltd 72 Dowd Street WELSHPOOL WA 6106
CEMENTING	Halliburton Cementing Services Halliburton Australia Pty Ltd 44 Churchill Road DRY CREEK SA 5094
MUDLOGGING	Halliburton Geodata 17 Musgrave Avenue WELLAND SA
DRILLING FLUIDS MUD ENGINEERING	Australian Mud Company Limited 15 Spencer Street JANDAKOT WA 6104
DRILL STEM TESTS	Halliburton Reservoir Services Halliburton Australia Pty Ltd 44 Churchill Road DRY CREEK SA 5094 Expertest Pty Ltd 138 Richmond Road MARLESTON SA 5033
WIRELINE LOGGING	BPB Wireline Services P.O. Box 465 STRATHPINE QLD 4500
COMPLETION	Vann Systems Halliburton Australia Pty Ltd 44 Churchill Road DRY CREEK SA 5094
PRODUCTION TESTS	Expertest Pty Ltd 138 Richmond Road MARLESTON SA 5033
TESTING SUPERVISION ENGINEERING DESIGN	Petroleum Engineering Services (Aust.) Pty Ltd P.O. Box 122 UNLEY SA 5061
WELL SUPERVISION	Geoweste Pty Ltd 8 Cumberland Avenue ALDGATE SA 5154
STRATIGRAPHER	Tabassi & Associates Pty Ltd 28 Sunline Avenue NOBLE PARK NORTH VIC 3171

APPENDIX 1

DRILLING HISTORY

APPENDIX 1 DRILLING HISTORY

(taken from daily report data)

24 HOURS TO 0800HRS 12 MAY, 1991

0800-0130 rig up
0130-0230 drill 12 1/4" hole to 14m
0230-0630 rig up and drill mouse hole
0630-0800 drill 12 1/4" hole to 23m

24 HOURS TO 0800HRS 13 MAY, 1991

0800-0830 run deviation survey
0830-1000 drill 12 1/4" hole to 32m
1000-1100 repair SCR control system
1100-1200 drill 12 1/4" hole to 71m
1200-1230 run deviation survey
1230-1500 drill 12 1/4" hole to 115m
1500-1530 circ bottoms up
1530-1600 run deviation survey
1600-1630 wiper trip, strap out of hole
1630-1800 RIH. circ, POOH
1800-1930 rig up for 9 5/8" casing
1930-2300 run 9 5/8" casing to 111.74m
2300-2330 circ through casing
2330-0030 cement casing
0030-0800 WOC

24 HOURS TO 0800HRS 14 MAY, 1991

0800-0900 WOC
0900-2100 nipple up BOPs
2100-0200 test blind rams, choke manifold,
choke valves malfunction
accumultor switching coil failed
0200-0800 repair BOPs

24 HOURS TO 0800HRS 15 MAY, 1991

0800-1900 repair hydraulic choke, repair manual choke
1900-2200 test BOP, chokes, pipe rams, Hydril,
kelly cocks to 1000 psi
2200-2300 make up bit and BHA. RIH
2300-0230 tag cement at 91m. drill out float collar + casing shoe +
float, drill 8 1/4" hole to 117m
0230-0300 leak off test
0300-0400 drill 8 1/2" hole to 136m
0400-0600 repair No 1 pump
0600-0800 drill to 179m

24 HOURS TO 0800HRS 16 MAY, 1991

0800-1000 drill to 228m
1000-1030 run deviation survey
1030-1430 drill to 323m
1430-1500 run deviation survey
1500-2330 drill to 427m
2330-2400 run deviation survey
2400-0800 drill to 542m

24 HOURS TO 0800HRS 17 MAY, 1991

0800-0930 drill to 560m
0930-1000 run deviation survey
1000-1830 drill to 719m
1830-1900 circulate
1900-2000 POOH
2000-2030 service rig
2030-2230 make up bit No 3, RIH
2230-2300 ream 18m to 719m
2300-0800 drill to 825m

24 HOURS TO 0800HRS 18 MAY, 1991

0800-1130 drill to 844m
1130-1200 repair rig SCR system
1200-1900 drill to 891m
1900-1930 circulate hole clean
1930-2000 run deviation survey
2000-2130 pump high vis pill. POOH to casing shoe,
working tight hole from 891-800m
2130-0700 dump and clean mud tanks, mix new polymer mud
0700-08000 RIH

24 HOURS TO 0800HRS 19 MAY, 1991

0930-1030 circulate to condition hole and mud
1030-1300 drill to 904m
1300-1330 circulate
1330-1400 trip 10 stands
1400-1930 circulate at 620m
1930-2000 RIH and wash 9m to bottom
2000-0230 drill to 908.1m - drilling break
0230-0300 flow check - no flow, circulate, pull back 1 stand,
circulate bottoms up
0300-0400 drill to 912.85m
0400-0500 flow check - no flow, circulate, pull back 1 stand,
circulate bottoms up
0500-0700 strap out of hole
0700-0800 make up DST tool

24 HOURS TO 0800HRS 20 MAY, 1991

0800-0930 make up for DST No 1

0930-1200 RIH
 1200-1230 rig up to test
 1230-1500 run DST No 1 - misrun, surface valve not opened
 1500-1700 POOH
 1700-1830 lay out DST tools
 1830-2130 make up BHA, RIH, tag fill at 901m
 2130-2200 wash to bottom
 2200-2230 drill to 914.10m
 2230-2300 flow check, circulate out sample, lay out 3 singles
 2300-0100 RIH to bottom, sweep hole with 5bbl high vis pill at
 100stks, spot 10bbl high vis pill on bottom
 0100-0130 pull back 2 stands, pick up kelly, pump slug
 0130-0300 POOH, lay out BHA
 0300-0715 make op for DST No 2
 0715-0800 RIH for DST No 2

24 HOURS TO 0800HRS 21 MAY, 1991

0800-0930 RIH DST No 2
 0930-1030 test packer failed to seat
 1030-1230 POOH
 1230-1430 lay out DST tools, clean
 1430-1500 make up BHA, RIH to shoe
 1500-1530 slip 40ft drill line
 1530-1700 RIH
 1700-1830 drill to 922m at 75 stks and 5001b WOB
 1830-2130 drill to 970m at 100 stks and 20001g WOB
 2130-2200 circulate prior to wiper trip
 2200-2300 wiper trip 15 stands
 2300-0030 circulate hole clean
 0030-0230 drop survey tool, strap out of hole
 0230-0745 run wireline logs Run 1 966-100m
 0745-0800 run wireline tools in hole for Run 2

24 HOURS TO 0800HRS 22 MAY, 1991

0800-1200 record wireline logs Run 2 963-750m
 1200-1400 RIH
 1400-1500 ream 956-970m, circulate
 1500-1930 lay out 4 1/2" DP and DC
 1930-0030 change pipe rams to 7", rig up to run 7" casing
 0030-0800 run 80 joints 26 ppf J55 LTC R3 7" casing to top fill at
 950m, circulate, run to 962.3m

24 HOURS TO 0800HRS 23 MAY, 1991

0800-0900 circulate
 0900-1000 run cement-test line to 3000psi, pump 10bbls 4% KCl
 brine, release bottom plug, mix and pump lead slurry of
 130 sx class A cement with 48bbls water and 4% bentonite
 and 4% KCl and 1% CFR-3 (15.5 US gal/SK); immediately
 followed by tail slurry of 110 sx class A cement with
 13.6bbls water and 4% KCl and 25 US gal/10bbls Halad 322L
 (5.2) US gal/SK), drop top plug, displace with 119bbls

water, land plug at 1500 psi, land casing and set slips
 in ime 13 mins
 1000-1800 WOC, open Halliburton valve to casing, no returns
 1800-1930 dress 7" stub, lay down cross over and spacer tool
 1930-0500 install tubing spool, nipple up BOP
 0500-0800 rig up flow line, etc

24 HOURS TO 0800HRS 24 MAY, 1991

0800-0900 circulate
 0900-0830 test BOPs to 1000 psi
 0830-0930 rig up to run 2 3/8" tubing
 0930-1330 run 2 7/8" tubing with 6" bit and casing scraper,
 tag plug at 945m
 1330-1430 circulate fresh water, displace with 6% KCl brine
 1430-1630 POOH
 1630-2100 run CBL log 940-200m
 2100-0300 lay out 6 singles, make up packer BHA, strap in under
 tension filling lowermost 170m tubing with KCl brine
 0300-0600 run GR/CCL positioning log,
 correlate pip tags-casing and tubing
 0600-0800 test packer to 1000 psi, nipple down BOPs

24 HOURS TO 0800HRS 25 MAY, 1991

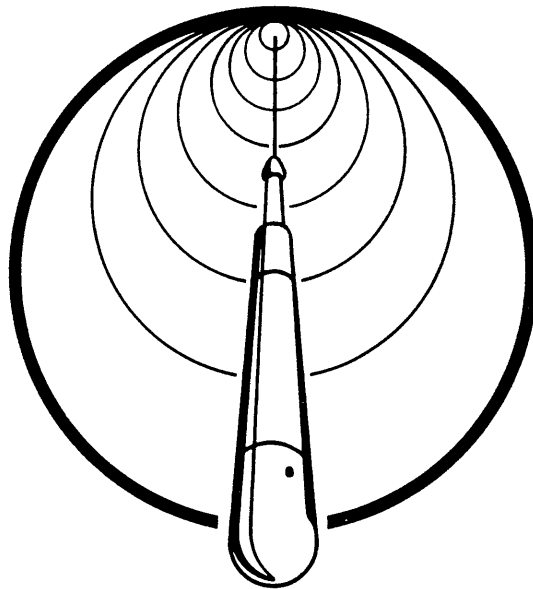
0800-0930 nipple down BOPs
 0930-1200 nipple up 2 9/16" 3000 psi Canadawerks christmas tree
 1200-1300 test christmas tree and each valve to 2000 psi
 1300-1345 hook up flare line and kill line, put 2000 psi on annulus
 1345-1430 drop TCP gun detonating bar, replace well cap, detonation
 in 37 secs, observe annulus for pressure change, bleed
 off annular pressure, close tubing spool side valve,
 1430-1630 observe for flow, no initial flow
 1630-1800 run BPB wireline to determine top of fluid in tubing
 - water only at 605m
 1800-2000 rig down BPB
 2000- rig down rig, rig released at 2000hrs

APPENDIX 2

DRILL STEM TEST DATA

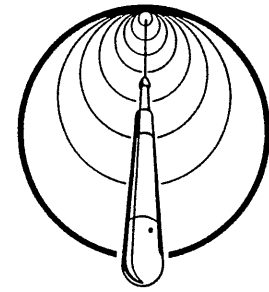
EXPERTEST

ELECTRIC WIRELINE
SERVICE



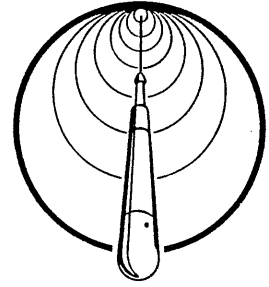
Electronic BHP/BHT Survey

Customer: Taipan Petroleum
Location: Lindon #2
Formation: Pebble Point
Date: 19th to 20th May, 1991



CUSTOMER: Taipan Petroleum
 LOCATION: Lindon #2
 FORMATION: Pebble Point
 DATE: 19th to 20th May, 1991

TIME	DESCRIPTION OF EVENTS
16-05-91	Mobilization of Equipment to Location
17-05-91	Bench Test of CCDST Package Standing by for test
18-05-91	Bench Test & Fine Tuning of CCDST Package Preparation of Pre-Test Planning Report
19-05-91	
0510	Arrive on Location and rig in CCDST Package
0630	Standing by for test
	DST #1
1250	Tool Opened No response observed on surface instrumentation
1300	Tool Closed
1312	Test Head Valve found to be closed
1315	Test Head Valve Opened - Still no response on surface instrumentation - Some bubbles evident in bucket
1323	Tool Opened for second flow period
1324	Tool skidded 6' downhole
1331	Tool Closed for second Build-up
1400	Chamber Pressure bled down - No response observed on SRO gauge - Some bubbles observed in bucket
1407	Tested SRO gauge with Rig Air System - OK



CUSTOMER: Taipan Petroleum
 LOCATION: Lindon #2
 FORMATION: Pebble Point
 DATE: 19th to 20th May, 1991

TIME	DESCRIPTION OF EVENTS
1410	Attempt made to open Hydraspring
	Not possible to determine tool status at surface
1440	Release Packer & Rig Down
20/05/91	DST #2
0520	Arrive on location
	Checked that SRO Pressure lines were clear
	Checked calibration of SRO Gauge up to 50 psi
0940	Manifold was filled with water and pressured up with Rig Air
	to test all surface equipment - all OK
0954	Tool Opened - Annulus dropped 40 to 50 feet
0957	An attempt was made to re-seat the packer
1003	Tool re-opened. Annulus dropped again
1004	Picked up to close the tool
	End of test
	Rigged out CCDST Package
	Returned to Adelaide

CLOSED CHAMBER DST PRE-TEST PLANNING

LOCATION: Lindon #2

INTERVAL: 2962-3002 'KB

DATE: 10/5/91

WELL DATA:

Expected Bottom Hole Pressure : 1255 psia
Expected Bottom Hole Temperature: 109 °F

Well-head Pressure : 0 psig
Well-head Temperature: 48 °F

Choke Diameter : 0.500 inches
Choke Coefficient: 4.38800

Gas Deviation Factor: 0.950
Gas Specific Gravity: 0.700

Chamber Volume: 37.971 bbls

Internal Diameter of Drill Collars: 2.812 inches
Total Footage of Drill Collars: 547 feet

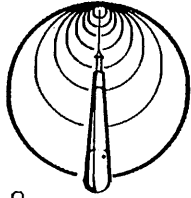
Internal Diameter of Drill Pipe: 3.826 inches

Depth to Top Packer : 2956 feet
Length of tools between
packer and valve: 34 feet

CALCULATED VALUES:

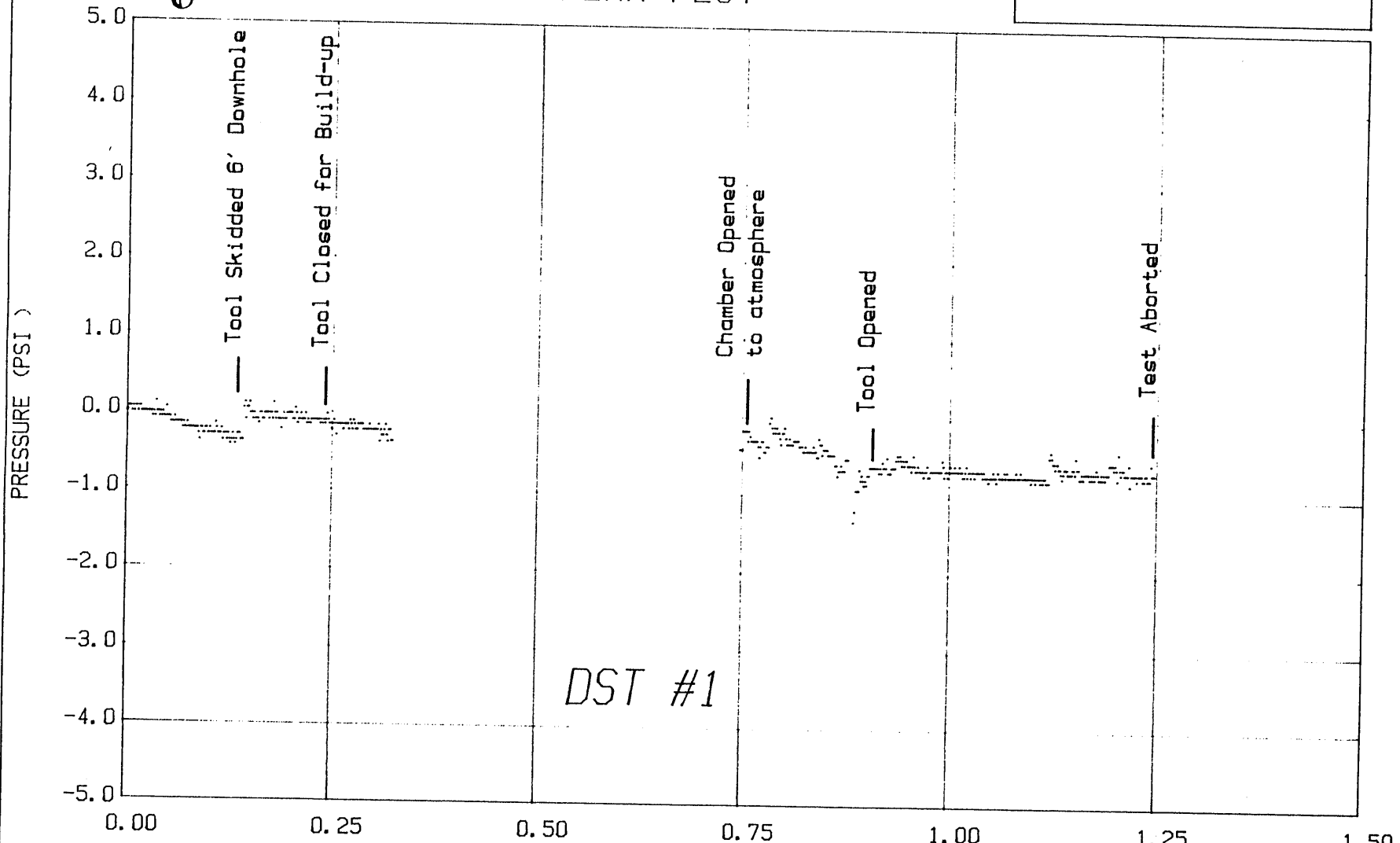
	MAX POSSIBLE RATE	MAX SURFACE PRESSURE CHANGE
PURE GAS	6.458 mmscf/d	304.02 psi/min
PURE WATER	4437.544 b/d	1.24 psi/min
GAS SATURATED WATER	4437.544 b/d + 45 mscf/d	3.38 psi/min

Average Chamber Temperature: 538.17 °R
Average Chamber Pressure : 15.27 psia
Gas - Water Ratio (GWR) : 1.82



EXPERTEST PTY. LTD.
ELECTRIC WIRELINE SERVICE
LINEAR PLOT

Taipan Petroleum
WELL: Lindon #2
ZONE: Pebble Point
Closed Chamber DST



DST #1

PLOT REFERENCE TIME IS
13:15 HRS. on 19/05/91

DELTA TIME (HOURS)

PLOT FINISHES AT
14:30 HRS. 19/05/91

CLOSED CHAMBER DST PRE-TEST PLANNING

LOCATION: Lindon #2

INTERVAL: 2962-3002 'KB

DATE: 20/5/91

WELL DATA:

Expected Bottom Hole Pressure : 1255 psia
Expected Bottom Hole Temperature: 109 °F

Well-head Pressure : 0 psig
Well-head Temperature: 42 °F

Choke Diameter : 0.500 inches
Choke Coefficient: 4.38800

Gas Deviation Factor: 0.950
Gas Specific Gravity: 0.700

Chamber Volume: 38.284 bbls

Internal Diameter of Drill Collars: 2.812 inches
Total Footage of Drill Collars: 547 feet

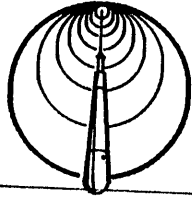
Internal Diameter of Drill Pipe: 3.826 inches

Depth to Top Packer : 2972 feet
Length of tools between
packer and valve: 28 feet

CALCULATED VALUES:

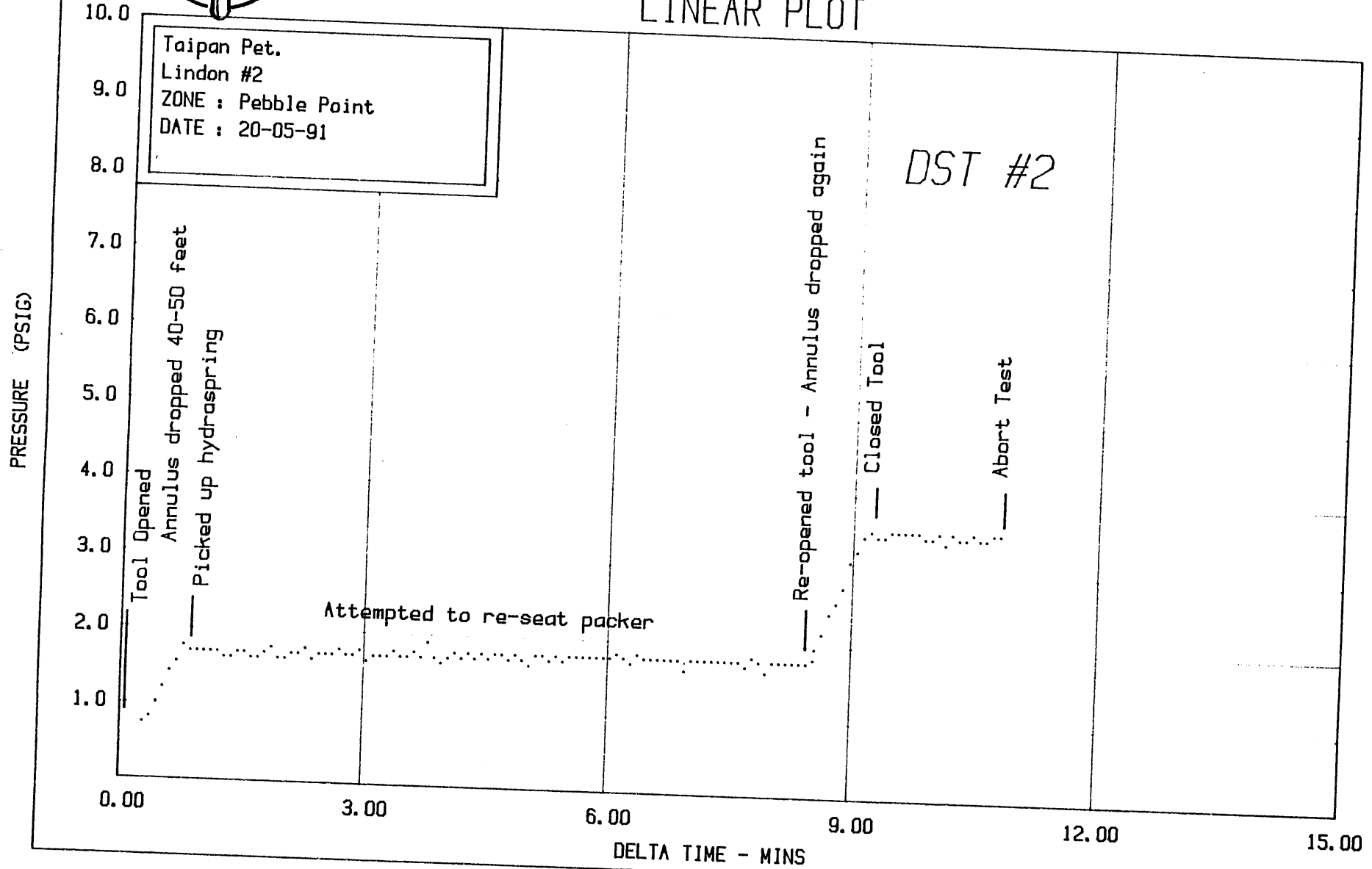
	MAX POSSIBLE RATE	MAX SURFACE PRESSURE CHANGE
PURE GAS	6.458 mmscf/d	299.85 psi/min
PURE WATER	4437.544 b/d	1.23 psi/min
GAS SATURATED WATER	4437.544 b/d + 45 mscf/d	3.34 psi/min

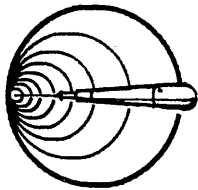
Average Chamber Temperature: 535.17 °R
Average Chamber Pressure : 15.27 psia
Gas - Water Ratio (GWR) : 1.82



EXPERTEST PTY LTD - CLOSED CHAMBER DST LINEAR PLOT

Taipan Pet.
Lindon #2
ZONE : Pebble Point
DATE : 20-05-91

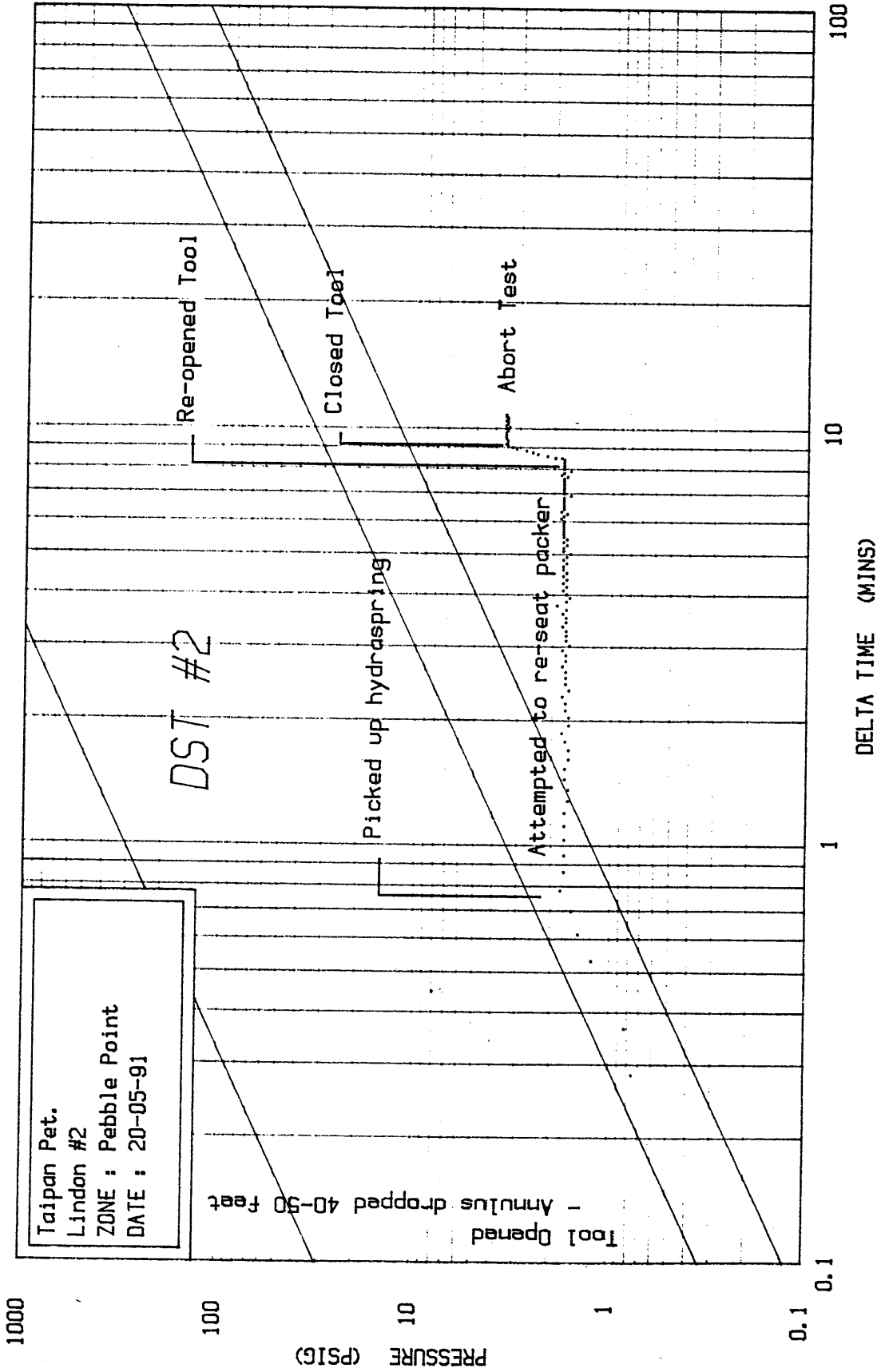




EXPERTEST PTY LTD - CLOSED CHAMBER DST LOG-LOG PLOT

Taipan Pet.
Lindon #2
ZONE : Pebble Point
DATE : 20-05-91

DST #2



FORMATION TEST REPORT



HALLIBURTON RESERVOIR SERVICES



A Halliburton Company

Customer: TAIPAN PETROLEUM P/L
Well Description: LINDON #2
Field Name: OTWAY BASIN

TEST NO: DST #1
TEST DATE: 19-MAY-91
TICKET NO: 001101

HALLIBURTON
RESERVOIR
SERVICES

REPORT TICKET NO: 001101
BT-GAUGE TICKET NO: 101101
MEMORY GAUGE TICKET NO: 001101
DATE: 19/5/91
HALLIBURTON CAMP: MOOMBA
TESTER: T.Stephens D.Schneider
WITNESS: G.Weste

DRILLING CONTRACTOR: GDS Rig #2
LEGAL LOCATION: see remarks

OPERATOR: TAIPAN PET. P/L
LEASE NAME: LINDON
WELL NO: 2
TEST NO: 1
TESTED INTERVAL: 905.43 - 912.85 m

FIELD AREA: OTWAY BASIN
COUNTY/LSD:
STATE/PROVINCE: VICTORIA
COUNTRY: AUSTRALIA

NOTE: THIS REPORT IS BASED ON SOUND ENGINEERING PRACTICES, BUT
DUE TO THE CAUSE OF VARIABLE WELL CONDITIONS AND OTHER INFORMATION WHICH MUST
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OUT OF OR IN CONNECTION WITH SUCH DATA, CALCULATIONS OR OPINIONS.

TABLE OF CONTENTS

SECTION 1: TEST SUMMARY & INFORMATION

Summary of Test Results	1.1
Test Period Summary	1.2
Pressure vs. Time Plot	1.3
Test and Formation Data	1.4
Rate History Table	1.5
Tool String Configuration	1.6
Operator Job Log	1.7

SECTION 2: ANALYSIS

Plots	2.1
-------	-----

SECTION 3: MECHANICAL GAUGE DATA

Gauge No. 2171	3.1
----------------	-----

SECTION 4: MEMORY GAUGE DATA

Gauge No. 76997	4.1
Gauge No. 72825	4.2

Date: 19/5/91

Ticket No: 001101

Page No: 1.1

SUMMARY OF TEST

Lease Owner: TAIPAN PET. P/L

Lease Name: LINDON

Well No.: 2

Test No.: 1

County/LSD:

State/Province: VICTORIA

Country: AUSTRALIA

Location Tested: PEBBLE POINT

Surface Temp: 103.50 F

Well Depth: 912.85 m

Pay: 7.42 m

Tested Interval: 905.43 - 912.85 m

Perforated Interval (m):

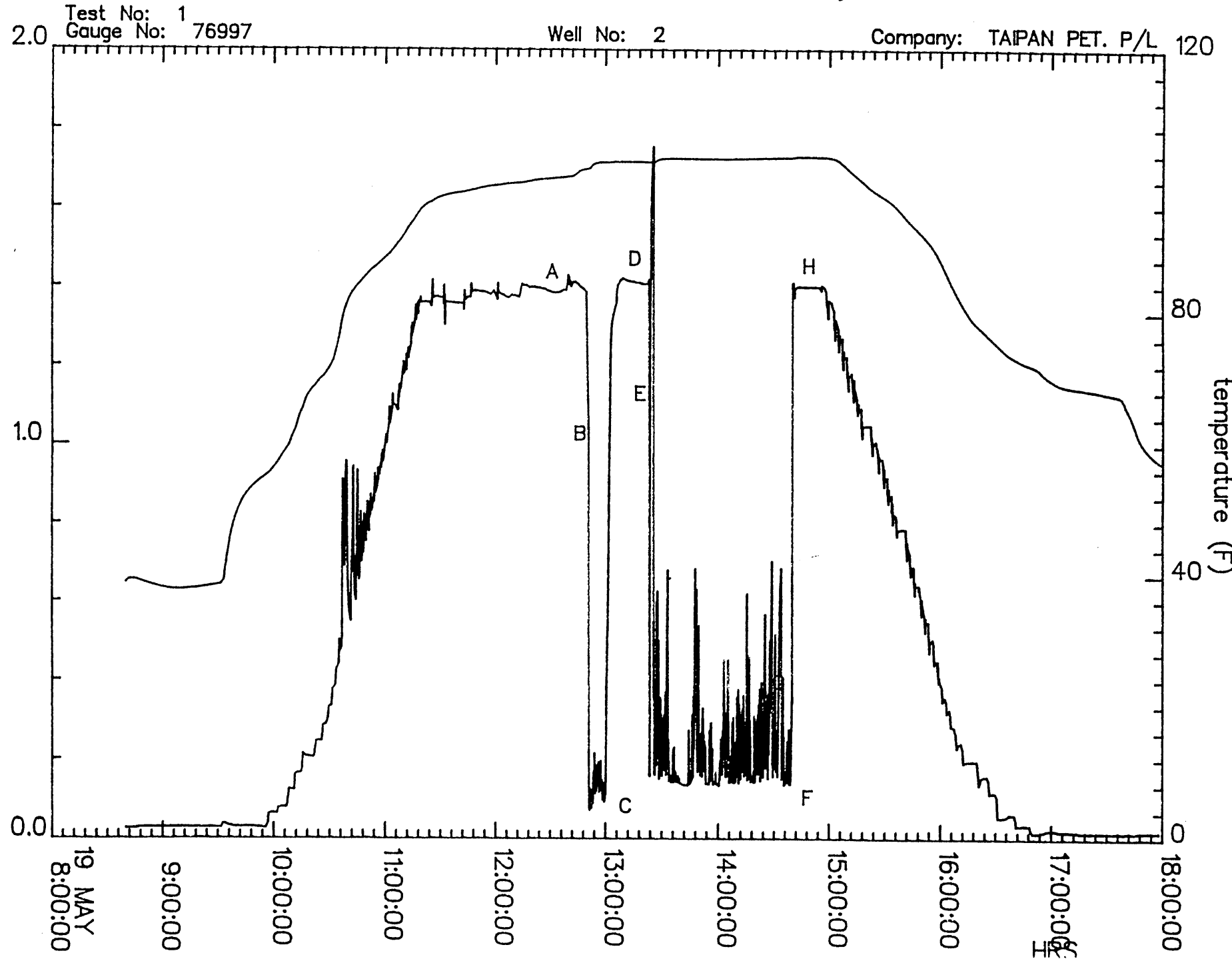
NOTES:

APPROXIMATELY 18mtr. OF FILTERCAKE ABOVE D.C.I.P. VALVE
TRACES OF HEAVY CRUDE OIL IN LOWER TEST TOOL

REMARKS:

ALL DOWNHOLE PRESSURES ARE IN ABSOLUTE PSIA.
SEVERE PLUGGING OF TEST TOOL IS EVIDENT BY PRESSURES RECORDED
IN DIFFERENT LOCATIONS IN TEST STRING
LEGAL LOCATION: - LAT - 38 04' 06.8" S
- LONG- 141 30' 54.7" E

Pressure/Temperature History








Date: 19/5/91
Ticket No: 001101
Page No: 1.3

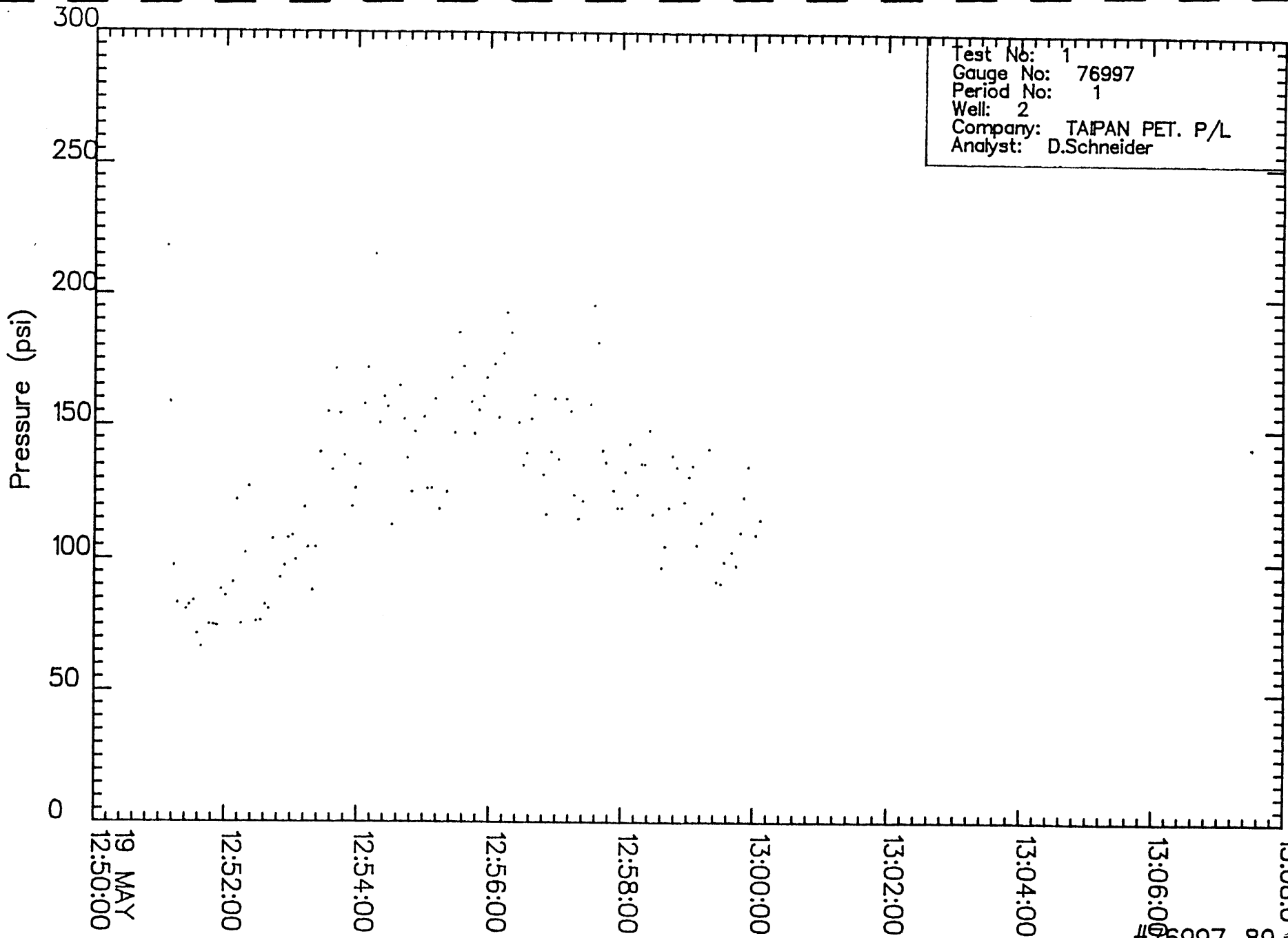
RATE HISTORY TABLE

Period No	Test Type	j	Prod Rate q(j) (bbl/D)	Duration (hrs)	Cum. Time t(j) (hrs)
		0	0.0	0.00	0.00
1	DD	1	0.0	0.15	0.15
2	BU	2	0.0	0.39	0.54
3	DD	3	0.0	1.25	1.79
4	BU	4	0.0	0.03	1.81

TEST STRING CONFIGURATION

	O.D. (in)	I.D. (in)	LENGTH (m)	DEPTH (m)
 DISTRIBUTOR VALVE	5.000	1.680	0.610	
 OPEN HOLE PACKER	7.500	1.530	1.771	905.430
 ANCHOR PIPE SAFETY JOINT ..	5.000	1.500	1.311	
 FLUSH JOINT ANCHOR	5.000	2.370	4.572	
 BLANKED-OFF RUNNING CASE ..	5.000	2.440	1.237	911.308
TOTAL DEPTH				912.85

HRS



Test No: 1
 Gauge No: 76997
 Period No: 1
 Well: 2
 Company: TAIPAN PET. P/L
 Analyst: D.Schneider

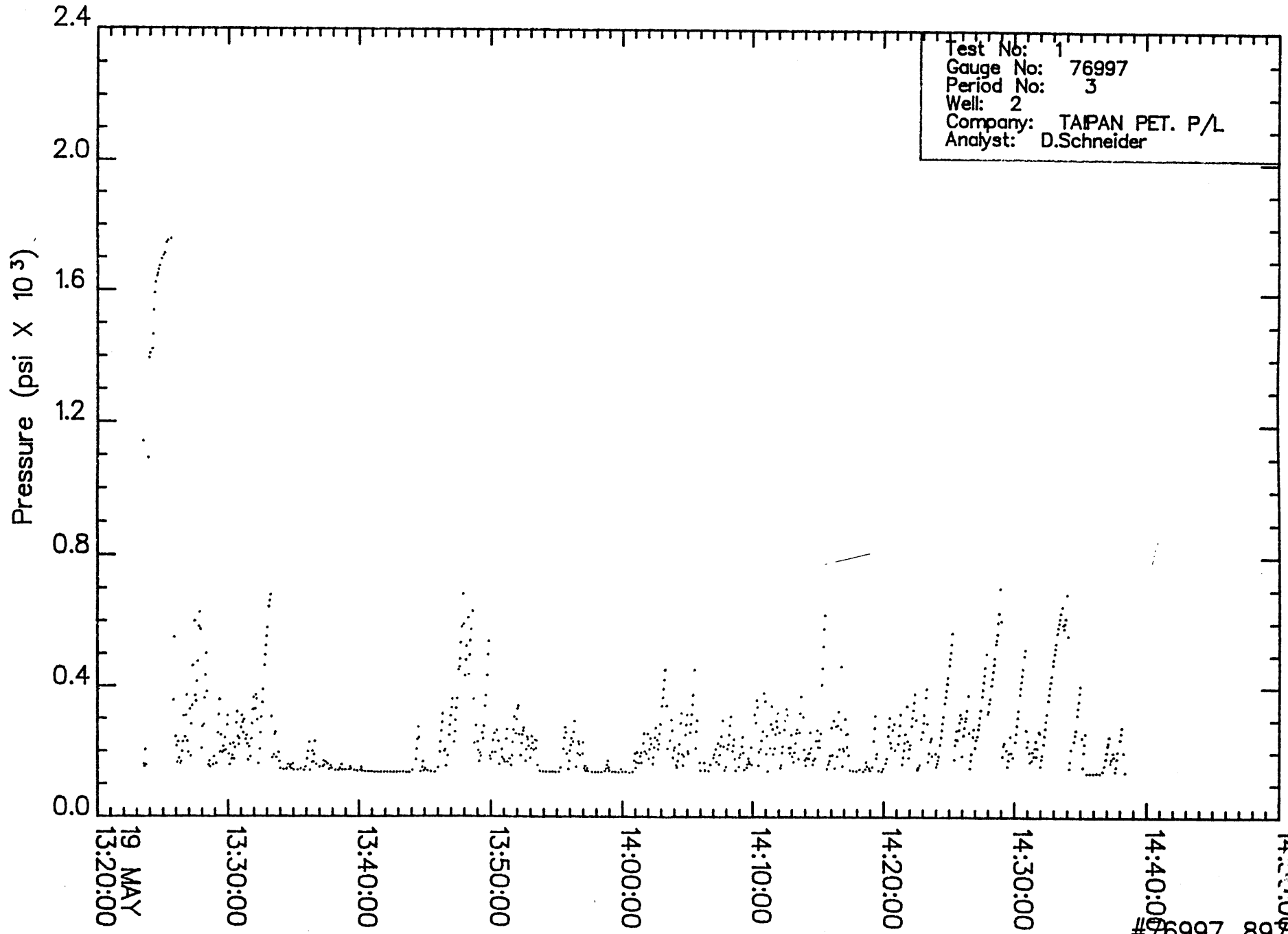
Date: 19/5/91

Ticket No: 001101

Page No: 2.2.1

#76997 89 / mt

Pressure Vs Time

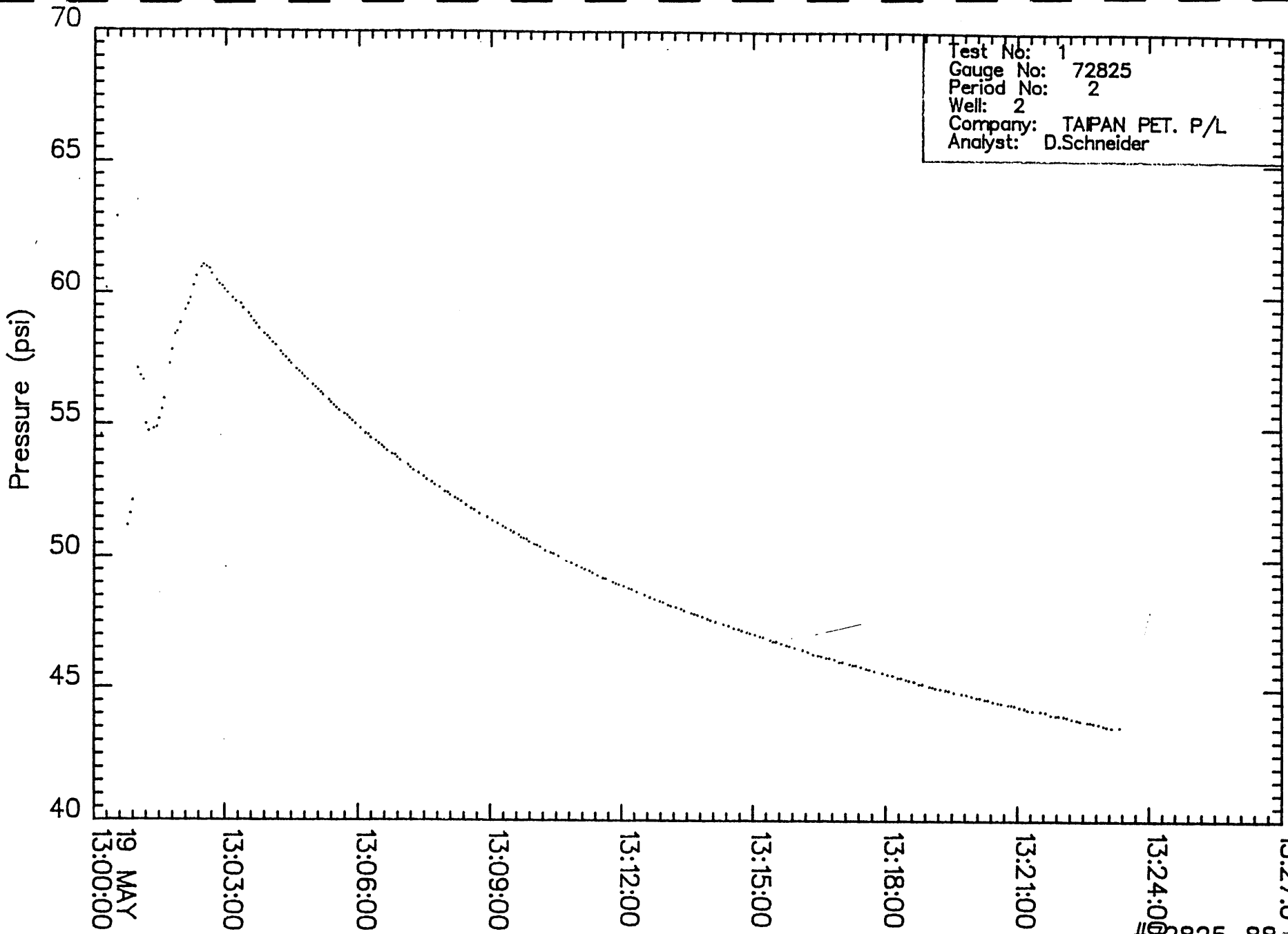


Date: 19/5/91

Ticket No: 001101

Page No: 2.2.3

#76997 897mt



Test No: 1
 Gauge No: 72825
 Period No: 2
 Well: 2
 Company: TAPAN PET. P/L
 Analyst: D.Schneider

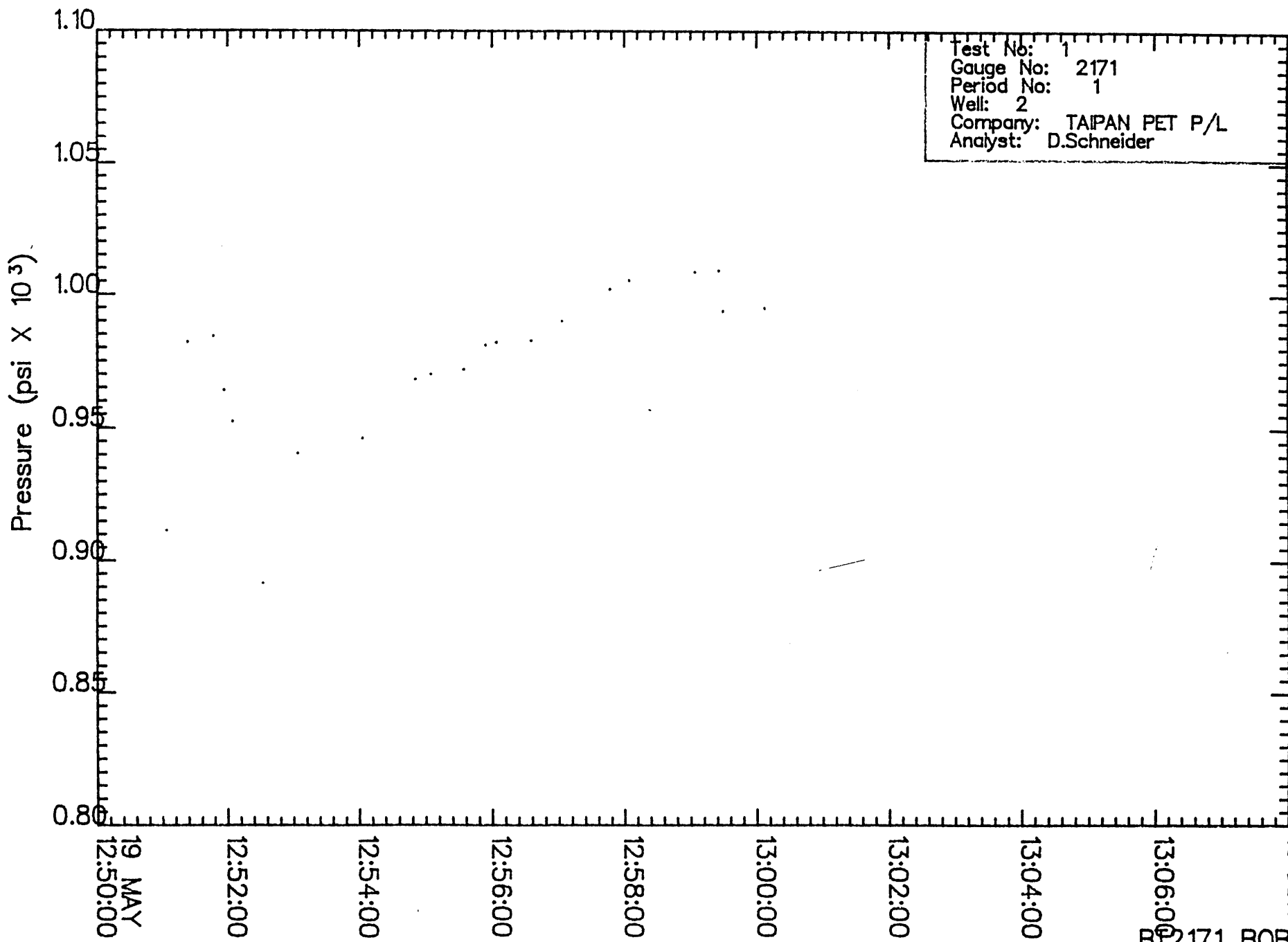
Date: 19/5/91

Ticket No: 001101

Page No: 2.2.5

#72825 88 0mi

Pressure Vs Time



Test No: 1
Gauge No: 2171
Period No: 1
Well: 2
Company: TAIPAN PET P/L
Analyst: D.Schneider

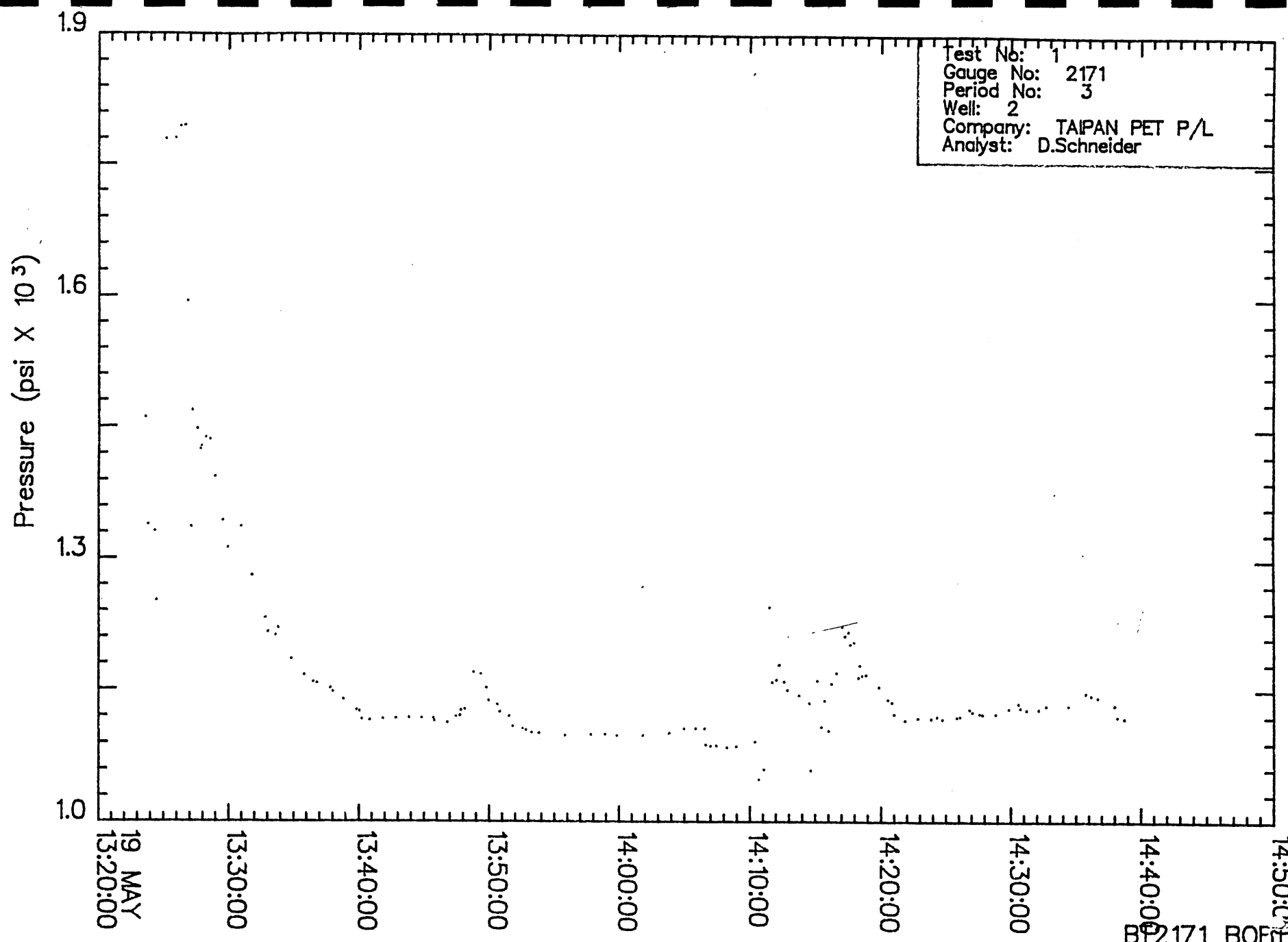
Date: 19/5/91

Ticket No: 101101

Page No: 2.2.7

BT2171 BOBT

Test No: 1
Gauge No: 2171
Period No: 3
Well: 2
Company: TAIPAN PET P/L
Analyst: D.Schneider



19 MAY
13:20:00

13:30:00

13:40:00

13:50:00

14:00:00

14:10:00

14:20:00

14:30:00

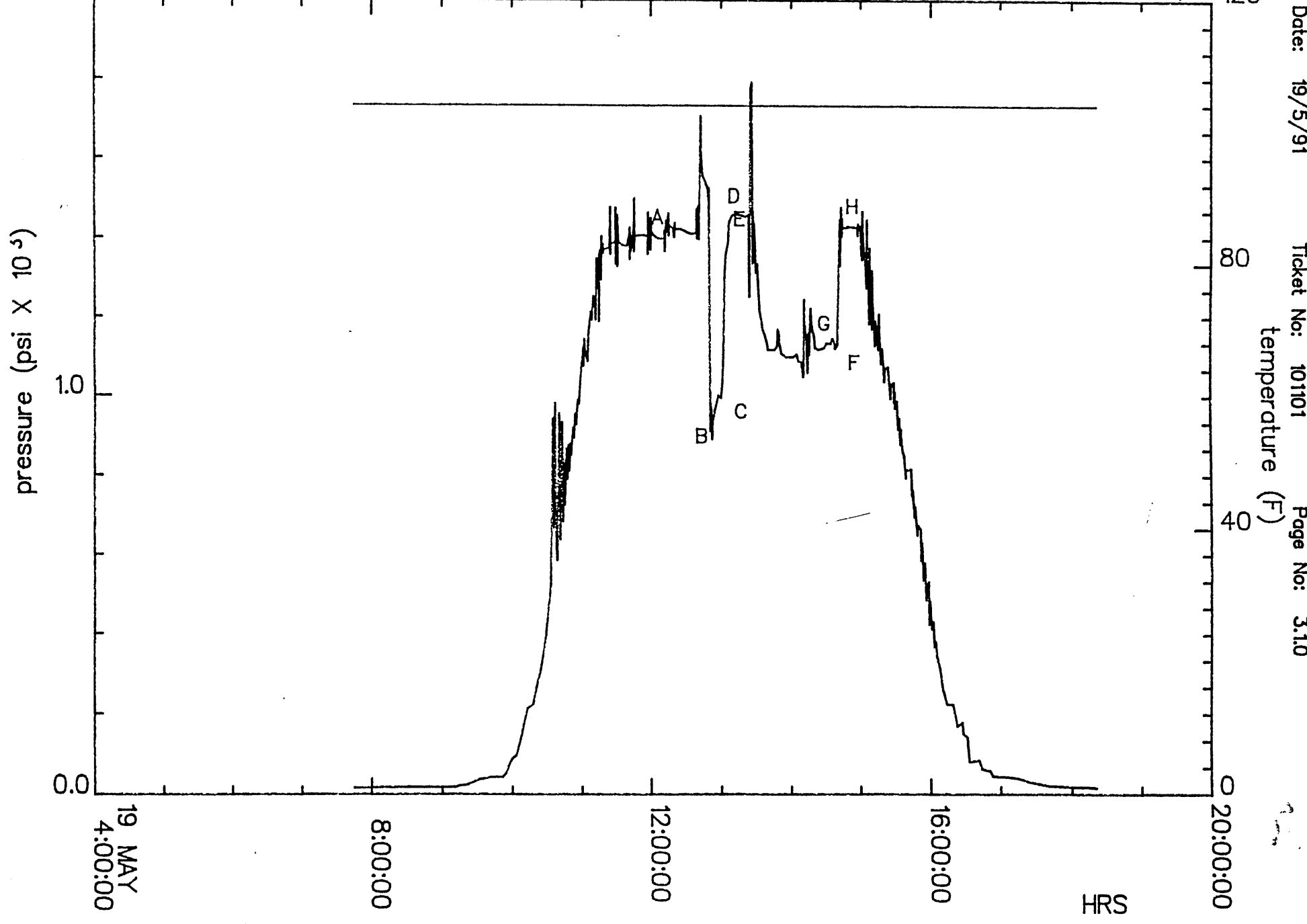
14:40:00

14:50:00

BP2171 BOE

Pressure/Temperature History

Test No: 1
Gauge No: 2171
Well No: 2
Company: TAIPAN PET P/L 120



Date: 19/5/91

Ticket No: 101101

Page No: 3.1.0

temperature (F)

19 MAY
4:00:00

8:00:00

12:00:00

16:00:00

HRS

20:00:00

Gauge No: 72825

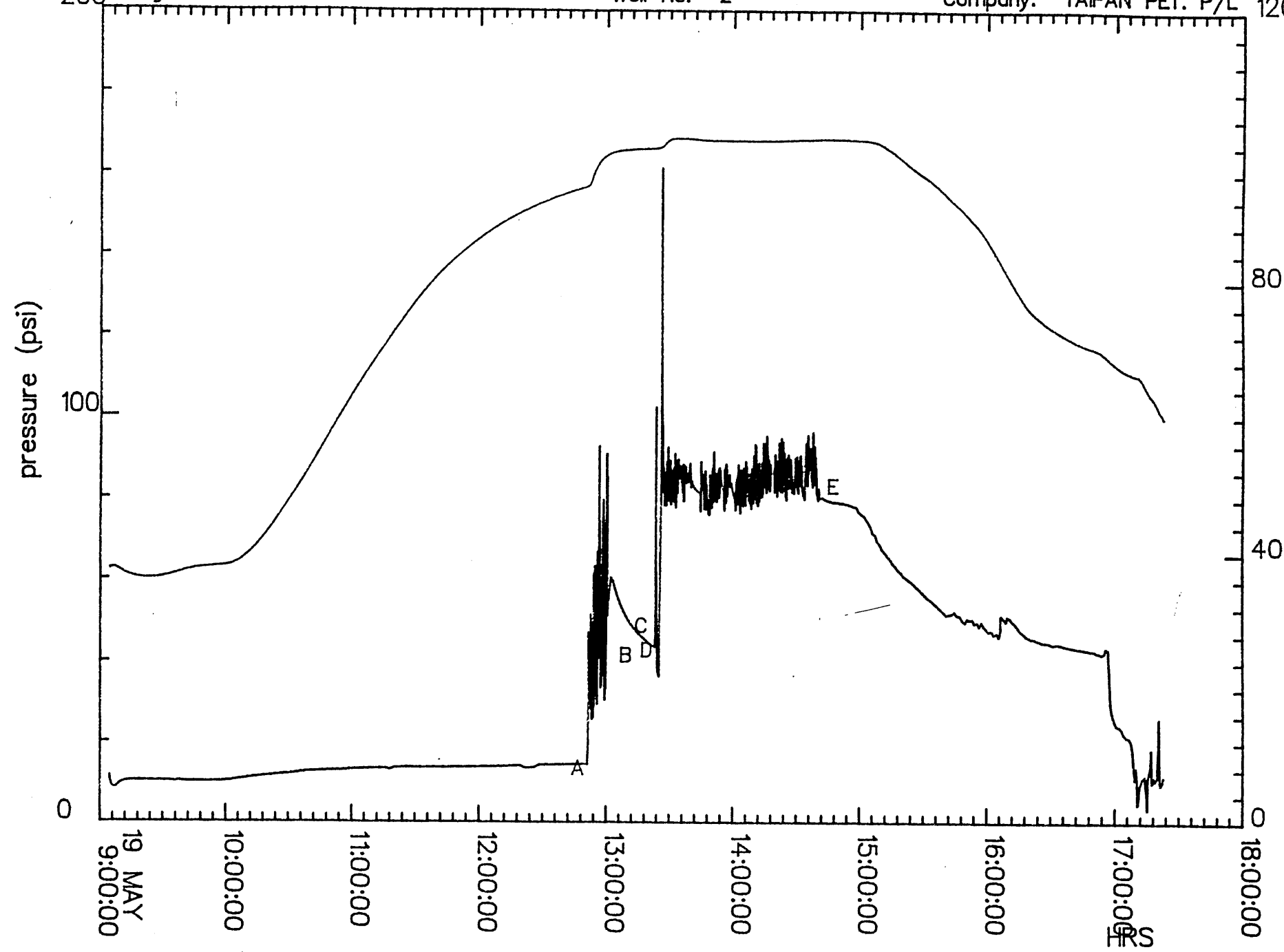
Well No: 2

Company: TAIPAN PET. P/L

Date: 19/5/91

Ticket No: 001101

Page No: 4.2.0



FORMATION TEST REPORT



HALLIBURTON RESERVOIR SERVICES



A Halliburton Company

Customer: TAIPAN PETROLEUM P/L
Well Description: LINDON #2
Field Name: OTWAY BASIN

TEST NO: DST #2
TEST DATE: 20--MAY--91
TICKET NO: 001102

HALLIBURTON
RESERVOIR
SERVICES

REPORT TICKET NO: 001102
MEMORY GAUGE TICKET NO: 001102
DATE: 20/5/91
HALLIBURTON CAMP: MOOMBA
TESTER: T.Stephens D.Schneider
WITNESS: G.Weste

DRILLING CONTRACTOR: GDS Rig #2
LEGAL LOCATION: see remarks

OPERATOR: TAIPAN PET
LEASE NAME: LINDON
WELL NO: 2
TEST NO: 2
TESTED INTERVAL: 902.68 - 914.10 m

FIELD AREA: OTWAY BASIN
COUNTY/LSD:
STATE/PROVINCE: VICTORIA
COUNTRY: AUSTRALIA

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TABLE OF CONTENTS

SECTION 1: TEST SUMMARY & INFORMATION

Summary of Test Results	1.1
Test Period Summary	1.2
Pressure vs. Time Plot	1.3
Test and Formation Data	1.4
Rate History Table	1.5
Tool String Configuration	1.6
Operator Job Log	1.7

SECTION 2: ANALYSIS

Plots	2.1
-------	-----

SECTION 3: MEMORY GAUGE DATA

Gauge No. 76997	3.1
Gauge No. 72825	3.2

Date: 20/5/91

Ticket No: 001102

Page No: 1.1

SUMMARY OF TEST

Lease Owner: TAIPAN PET

Lease Name: LINDON

Well No.: 2

Test No.: 2

County/LSD:

State/Province: VICTORIA

Country: AUSTRALIA

Formation Tested: PEBBLE POINT

Hole Temp: 106.00 F

Total Depth: 914.10 m

Net Pay: 11.42 m

Gross Tested Interval: 902.68 - 914.10 m

Perforated Interval (m):

RECOVERY:

REMARKS:

ALL DOWNHOLE PRESSURES ARE IN ABSOLUTE PSIA.
DST WAS ABORTED WHEN PACKER SEAT WAS NOT ACHIEVED.

LEGAL LOCATION: - LAT - 38 04' 20" S
- LONG- 141 30' 08" E

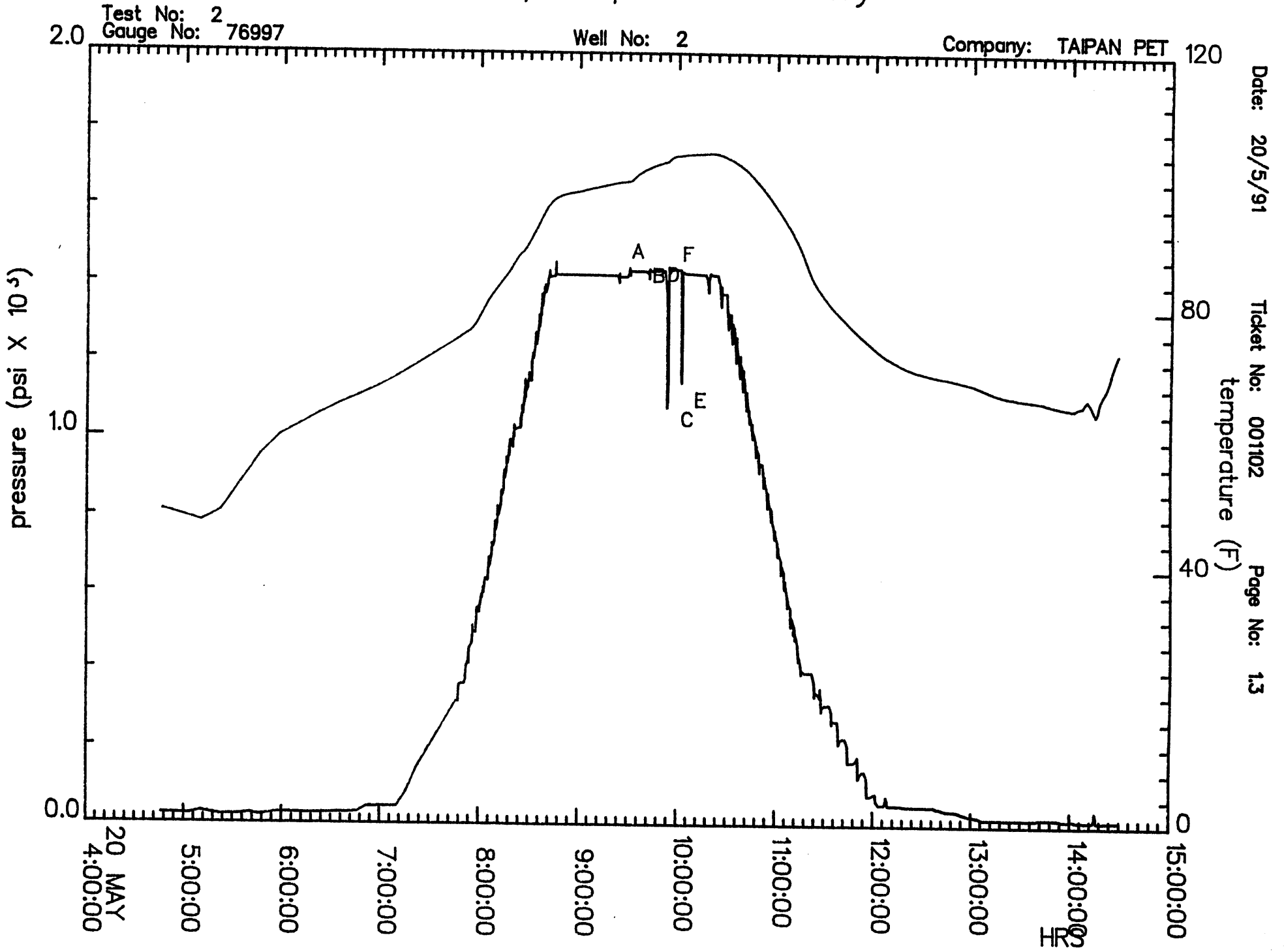
TEST PERIOD SUMMARY

Gauge No.: 76997 Depth: 907.65 m Blanked off: Yes

ID	PERIOD	DESCRIPTION	PRESSURE (psi)	DURATION (min)
A		Initial Hydrostatic	1430.35	
B	1	Start Draw-down	1432.92	
C		End Draw-down	1082.90	0.73
D	2	Start Draw-down	1435.61	
E		End Draw-down	1132.19	0.65
F		Final Hydrostatic	1424.67	

NOTE: for Pressure vs. Time Plot, see next page.

Pressure/Temperature History



TEST AND FORMATION DATA

Formation Tested: PEBBLE POINT
 All Depths Measured From: KELLY BUSHINGS
 Elevation: 68.76 m
 Total Depth: 914.10 m
 Net Pay: 11.42 m
 Hole or Casing Size: 8.500 in
 Gross Tested Interval: 902.68 - 914.10 m
 Perforated Interval (m):

HOLE FLUID

HOLE TEMPERATURE

Type: KCL
 Weight: 9.10 lbm/gal
 Viscosity: cp
 Depth: 907.65 m
 Estimated: 105.00 F
 Actual: 106.00 F

HYDROCARBON PROPERTIES

CUSHION DATA

	@ 60 F	TYPE	AMOUNT	WEIGHT
Oil Gravity (API):				
Gas/Oil ratio (ScF/STB):		NIL		
Gas Gravity (SG):	0.75			

FLUID PROPERTIES FOR RECOVERED MUD AND WATER

SOURCE	RESISTIVITY	CHLORIDES	SG	PH
	@	F		
	@	F		
	@	F		
	@	F		
	@	F		
	@	F		

SAMPLER DATA























Surface Pressure: psi
 Volume of Gas: ft3
 Volume of Oil: cc
 Volume of Water: cc
 Volume of Mud: cc
 Total Liquids: cc

REMARKS:

ALL DOWNHOLE PRESSURES ARE IN ABSOLUTE PSIA.
 DST WAS ABORTED WHEN PACKER SEAT WAS NOT ACHEIVED.

LEGAL LOCATION: - LAT - 38 04' 20" S
 - LONG- 141 30' 08" E








TEST STRING CONFIGURATION

	O.D. (in)	I.D. (in)	LENGTH (m)	DEPTH (m)
 DRILL PIPE.....	4.500	3.826	726.040	
 FLEX WEIGHT	4.500	2.812	55.769	
 DRILL COLLARS	6.250	2.812	83.360	
 PUMP OUT REVERSING SUB ...	6.000	3.000	0.305	857.528
 DRILL COLLARS	6.250	2.812	9.280	
 IMPACT REVERSING SUB	6.000	3.000	0.305	867.113
 DRILL COLLARS	6.250	2.812	18.420	
 BAR CATCHER SUB	5.750	1.000	0.305	
 AP RUNNING CASE.....	5.000	2.250	1.262	886.340
 CROSSOVER.....	5.000	2.250	0.305	
 ELECTRONIC GAUGE RUNNING CASE	5.500	2.250	2.370	889.660
 CROSSOVER.....	5.000	2.250	0.305	
 CROSSOVER.....	5.000	2.200	0.305	
 DUAL CIP VALVE	5.000	0.870	1.484	891.760
 SAMPLE CHAMBER	5.000	2.500	1.484	
 DRAIN VALVE	5.000	2.200	0.262	
 HYDROSPRING TESTER	5.000	0.750	1.618	895.080
 AP RUNNING CASE.....	5.000	2.250	1.262	895.790
 JAR.....	5.000	1.750	1.524	
 VR SAFETY JOINT	5.000	1.000	0.847	
 OPEN HOLE PACKER.....	7.500	1.530	1.771	900.490
 DISTRIBUTOR VALVE.....	5.000	1.680	0.610	
OPEN HOLE PACKER.....	7.500	1.530	1.771	902.680

CONTINUED

HRS

TEST STRING CONFIGURATION

	O.D. (in)	I.D. (in)	LENGTH (m)	DEPTH (m)
 ANCHOR PIPE SAFETY JOINT ..	5.000	1.500	1.311	
 FLUSH JOINT ANCHOR	5.000	2.370	4.572	
 EMR GAUGE HANGER	5.000	2.370	0.465	907.650
 BLANK ANCHOR	5.000	2.370	1.518	
 BLANK ANCHOR	5.000	2.370	1.518	
 FLUSH JOINT ANCHOR	5.000	2.370	0.305	
 BLANKED-OFF RUNNING CASE ..	5.000	2.440	1.237	912.560
TOTAL DEPTH				914.10

HRS

Date: 20/5/91
Test No: 2

Ticket No: 001102

Page No: 1.7.1

OPERATOR JOB LOG

Type of Flow Measuring Device: 6"CERAMIC CHOKE

TIME HH:MM:SS	CHOKE SIZE (in)	SURFACE PRESSURE (psi)	GAS RATE (Mscf/D)	LIQUID RATE (bbl/D)	REMARKS
------------------	-----------------------	------------------------------	-------------------------	---------------------------	---------

20-May-91

04:40:00					MAKE UP TOOLS
07:10:00					TOOLS MADE UP, RUN IN HOLE
08:45:00					RIG UP SURFACE EQUIPMENT
08:55:00					PRESSURE TEST SURFACE EQUIP.
09:35:00					HEAD UP
09:47:00					SET WEIGHT ON TOOL
09:53:22					TOOL OPEN
09:53:50					LOST PACKER SEAT
09:54:06					PICK UP ON TOOL
09:56:30					SET WEIGHT ON TOOL
10:02:00					TOOL OPEN
10:02:30					LOST PACKER SEAT
10:02:40					PICK UP ON TOOL
10:02:40					TEST TOOL 1.5mtr. OFF BOTTOM
10:05:00					RIG DOWN SURFACE EQUIPMENT
10:10:00					LAY OUT TEST HEAD
10:25:00					PULL OUT OF HOLE
12:10:00					TOOLS AT FLOOR
14:30:00					TOOLS LAID OUT

TEST PERIOD SUMMARY

Gauge No.: 76997 Depth: 907.65 m Blanked off: Yes

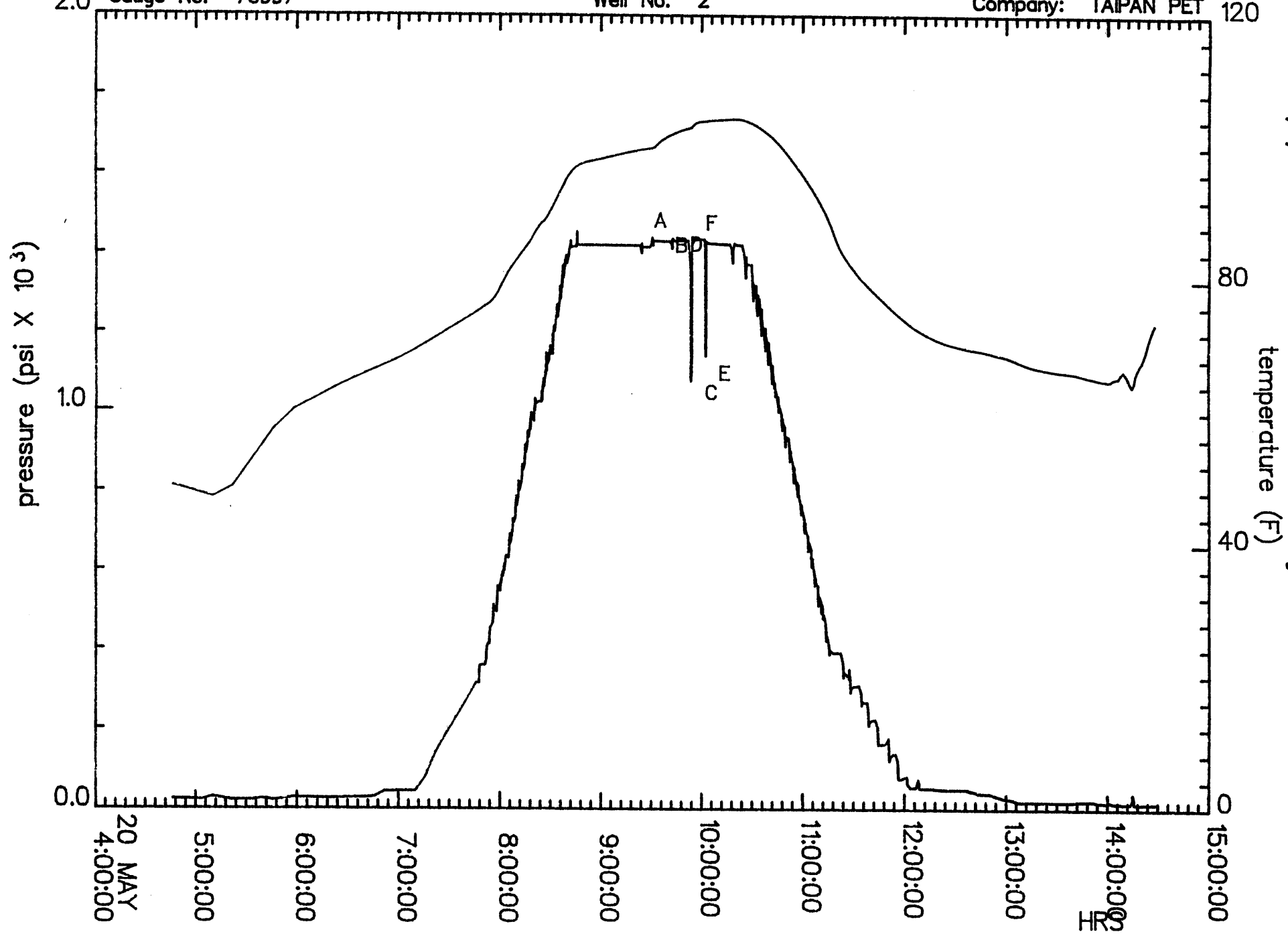
ID	PERIOD	DESCRIPTION	PRESSURE (psi)	DURATION (min)
A		Initial Hydrostatic	1430.35	
B	1	Start Draw-down	1432.92	
C		End Draw-down	1082.90	0.73
D	2	Start Draw-down	1435.61	
E		End Draw-down	1132.19	0.65
F		Final Hydrostatic	1424.67	

NOTE: for Pressure vs. Time Plot, see next page.

Pressure/Temperature History

Test No: 2
Gauge No: 76997
Well No: 2
Company: TAIWAN PET

Date: 20/5/91
Ticket No: 001102
Page No: 3.10



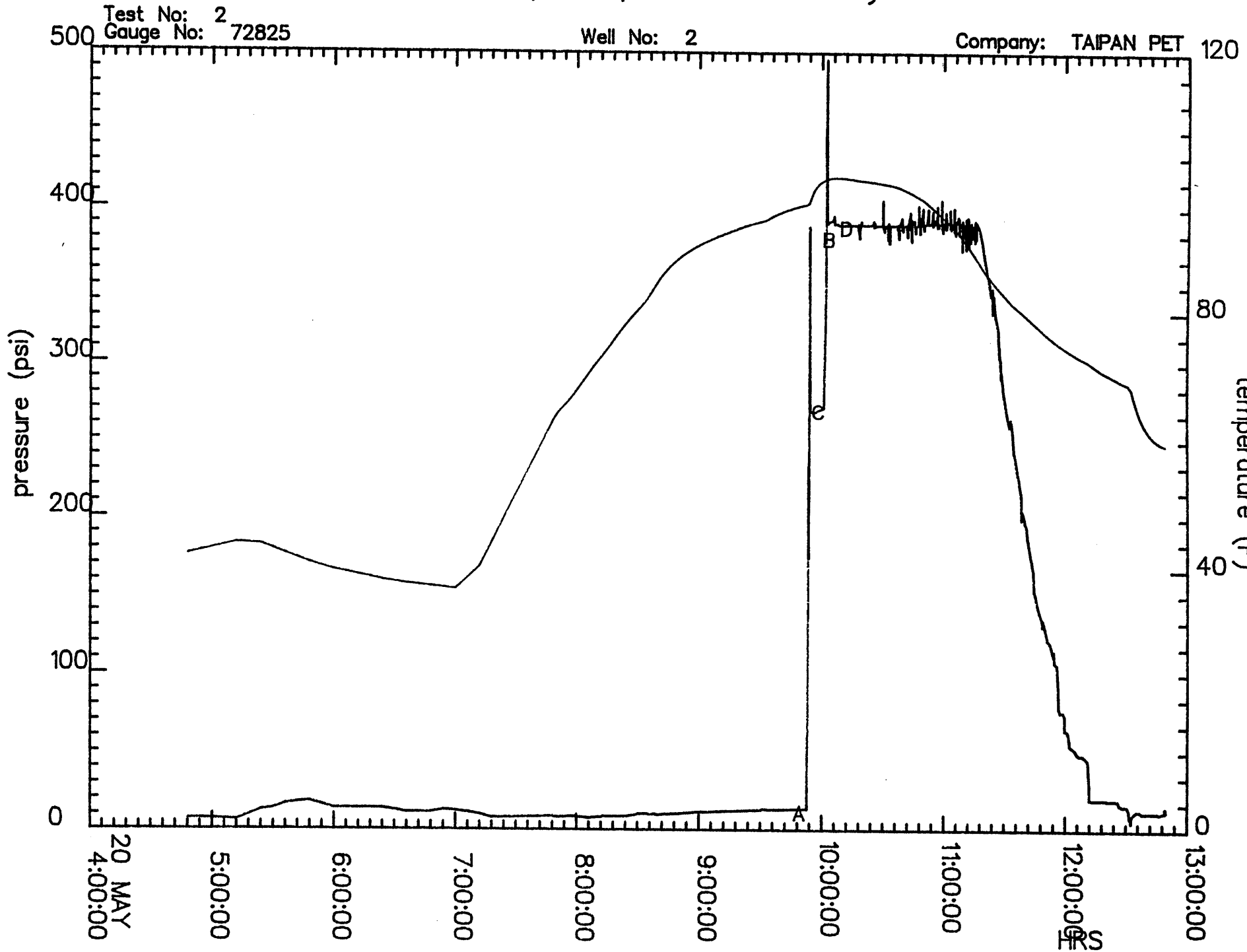
TEST PERIOD SUMMARY

Gauge No.: 72825 Depth: 889.66 m Blanked off: No

ID	PERIOD	DESCRIPTION	PRESSURE (psi)	DURATION (min)
A	1	Start Draw-down	13.81	
B		End Draw-down	388.54	0.72
C	2	Start Draw-down	271.52	
D		End Draw-down	395.71	0.78

NOTE: for Pressure vs. Time Plot, see next page.

Pressure/Temperature History

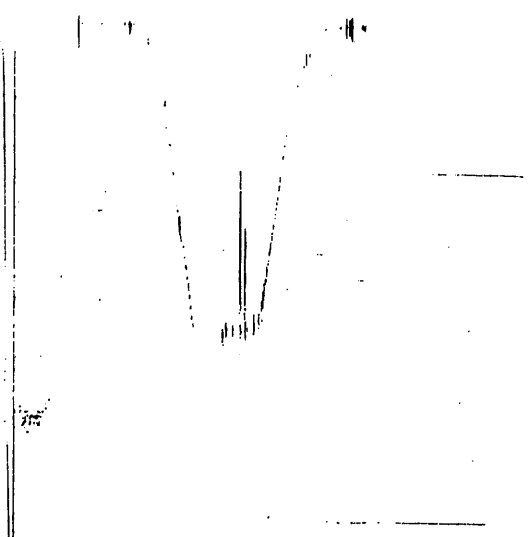
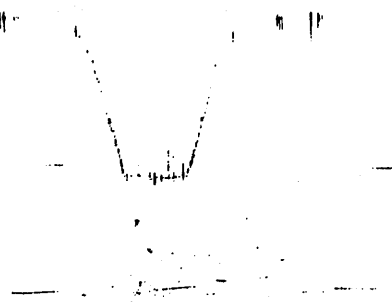


Date: 20/5/91

Ticket No: 001102

Page No: 3.2.0

Flow 2270



DST #2
7.2171 BoBT (Blanked off)
6000 PSI GAUGE 24HR Clock 912.56 mtk.

DST #2 Flow
BT 2270 24HR Clock 3000 PSI 895.79 mtk.

DST #2
3933 REC. 24HR Clock 3000 PSI GAUGE 886.34 mtk.

APPENDIX 3

PRODUCTIVITY TEST DATA

TAIPAN PETROLEUM PTY. LTD.
LINDON No.2

OPERATIONS REPORT: 1

Covering Daily Operations on: Saturday 8 June, 1991.

- 14.30 hrs. Wireline/Test Supervisor on location.
Unloaded Expertest flow equipment and released truck.
- 21.00 hrs. Expertest wireline truck and mast arrived in Heywood
after delayed departure from Adelaide

TAIPAN PETROLEUM PTY. LTD.
LINDON No.2

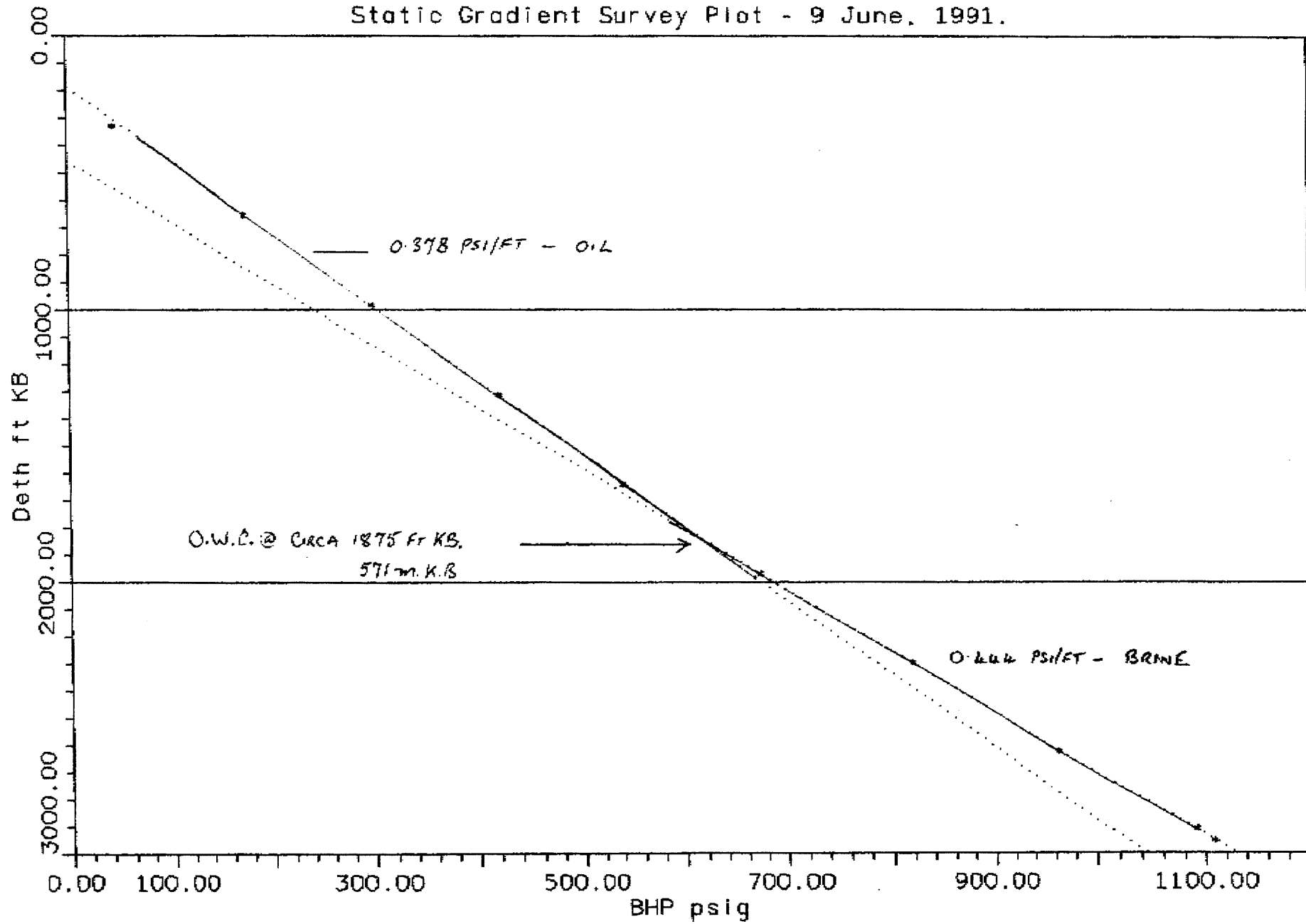
OPERATIONS REPORT: 2

Covering Daily Operations on: Sunday 9 June, 1991.

- 07.45 hrs. Spot equipment and commence rigging up.
- 09.45 Shut in tubing head pressure (SITHP); 634.34 kPa.
(92 psig).
Shut in annulus pressure (CIAP); 0.
- 10.30 RIH with 2.2 inch blind box and tagged fluid at 62 m.
(203 ft.) K.B.
Attempted to work through waxy oil.
- 11.15 POH and changed blind box for 1.9 inch guage cutter.
- 11.45 Tagged fluid level at same depth and attempted to
work through fluid, POH.
- 12.30 RIH with 1.9 inch guage cutter and additional sinker
bars.
Tagged fluid at 58 m. (190 ft.) K.B. and worked
through heavy crude until the tool string ran free at
122 m. (400 ft.) K.B.
Tagged TCP gun firing bar at 900.6 m. (2955 ft.) K.B.
POH.
- 15.00 Ran Static Gradient survey without difficulty.
Plotted results indicate on oil column of gradient
0.378 psi/ft to circa 571 m. (1875 ft.) K.B., below
which is completion brine of gradient 0.444 psi/ft.
- 17.30 Secure well and shut down for the night.

APPX TOP OIL COLUMN 190 FT KB.
APPX VOL OIL COLUMN 9.76 BBL.
VOL BRINE IN TUBING 6.25 BBL.

LINDON No. 2
Static Gradient Survey Plot - 9 June, 1991.



TAIPAN PETROLEUM PTY. LTD.
LINDON No.2

OPERATIONS REPORT: 3

Covering Daily Operations on: Monday 10 June, 1991.

- 07.45 Hrs Rig up Braided line equipment for swabbing.
- 10.00 Make 1.9 inch gauge ring run to 152 m. (500 ft.) K.B. and tagged fluid top at 55 m. (180 ft.) K.D.
- 10.45 Rigged up flowlines from wellhead to tank and pit.
- 12.00 RIH with swab mandrel and 2.5 inch swab cups, worked through fluid top at 55 m. K.B.
- 12.30 - Made 13 swab runs, from 142 m. (465 ft.) to 858 m. (2815 ft.), recovering an estimated 10.7 Bbls of oil and 7.9 Bbls of completion brine.

Note 1. Calculated tubing volumes from static gradient survey were 9.76 Bbls oil and 6.25 Bbls brine.

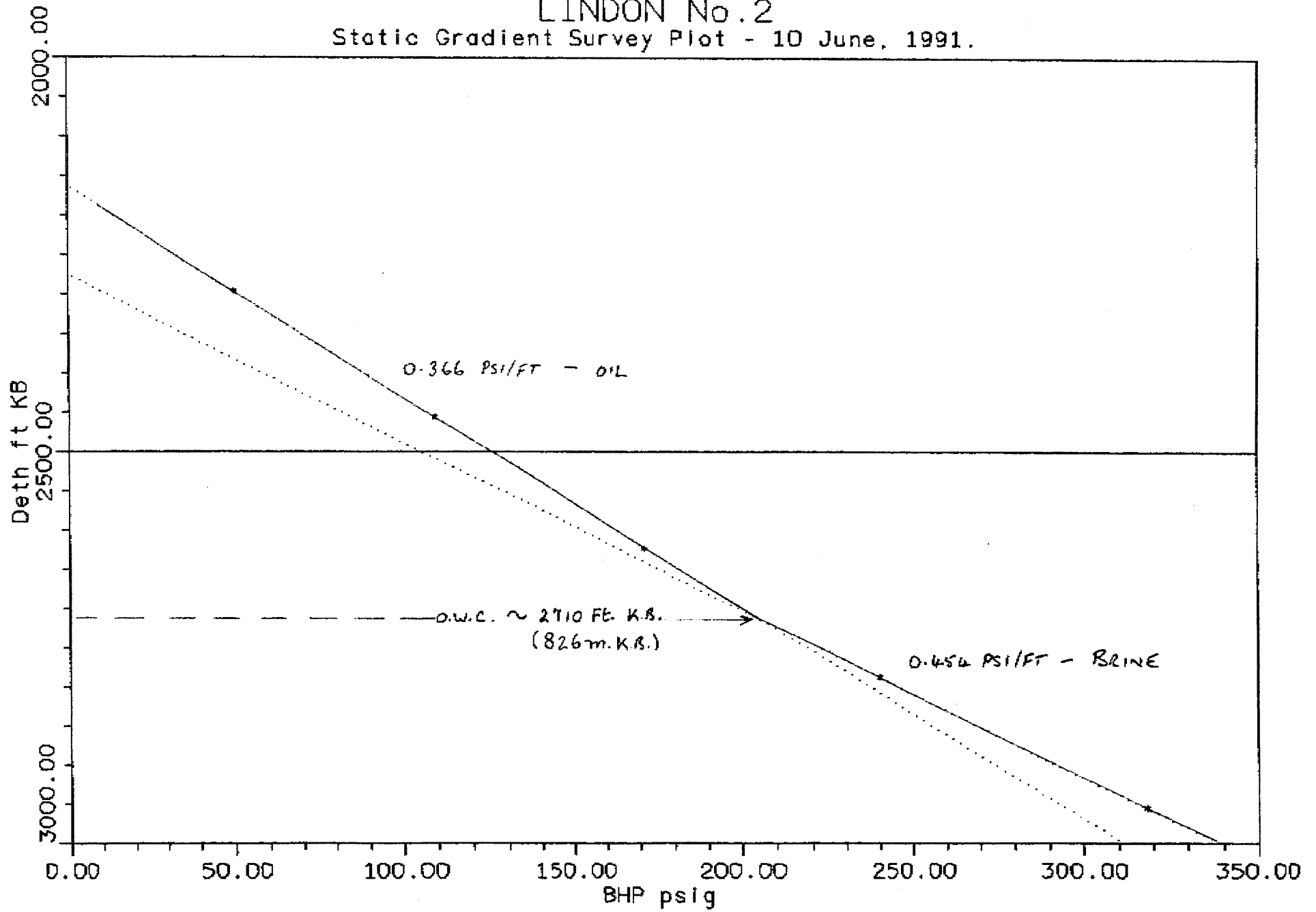
Note 2. That swabbed fluid was directed to the pit as the thickness of the oil made it impossible to carry out gauge dipping in the tank.

Refer to attached swab report for details.

The last swab before nightfall pulled approximately 0.4 Bbls of newly influxed oil in addition to brine.

- 17.00 Secured well and shut down for the night.

LINDON No. 2
Static Gradient Survey Plot - 10 June, 1991.



TAIPAN PETROLEUM PTY. LTD.
LINDON No.2

OPERATIONS REPORT: 4
Covering Daily Operations on: Tuesday 11 June, 1991.

- 07.45 hrs Ran Static Gradient survey #2; top of fluid column at 661 m. (2170 ft.) K.B.
OWC at approx. 826 m. (2710 ft.) K.B.
BHP 318.6 psig at 901 m. (2955 ft.) K.B.
- 12.30 - Made 5 swab runs from 721 m. (2365 ft.) to 858 m. (2815 ft.) K.B., recovering an estimated 3.3 Bbls of oil and 0.7 Bbls of completion brine, with apparent minimal influx.
- Note Swabbed fluid volumes measured in a small calibrated dip tank.
- 15.30 RIH with 2.5 inch 'B' shifting tool, shifted release sub at 894 m. (2934 ft.) K.B. and dropped TCP guns. Ran tools down to 926 m. (3038 ft.) K.B. to check wellbore clear to 15 m. below perforations.
- 16.30 - Made 2 further swab runs from 858 m. (2815 ft.) K.B., recovering a further 0.25 Bbls each of oil and brine.
- 17.15 Ran in with swab mandrel and tagged top of fluid at 852 m. (2795 ft.) K.B.
POH.
- 17.30 Secured well and shut down for the night.

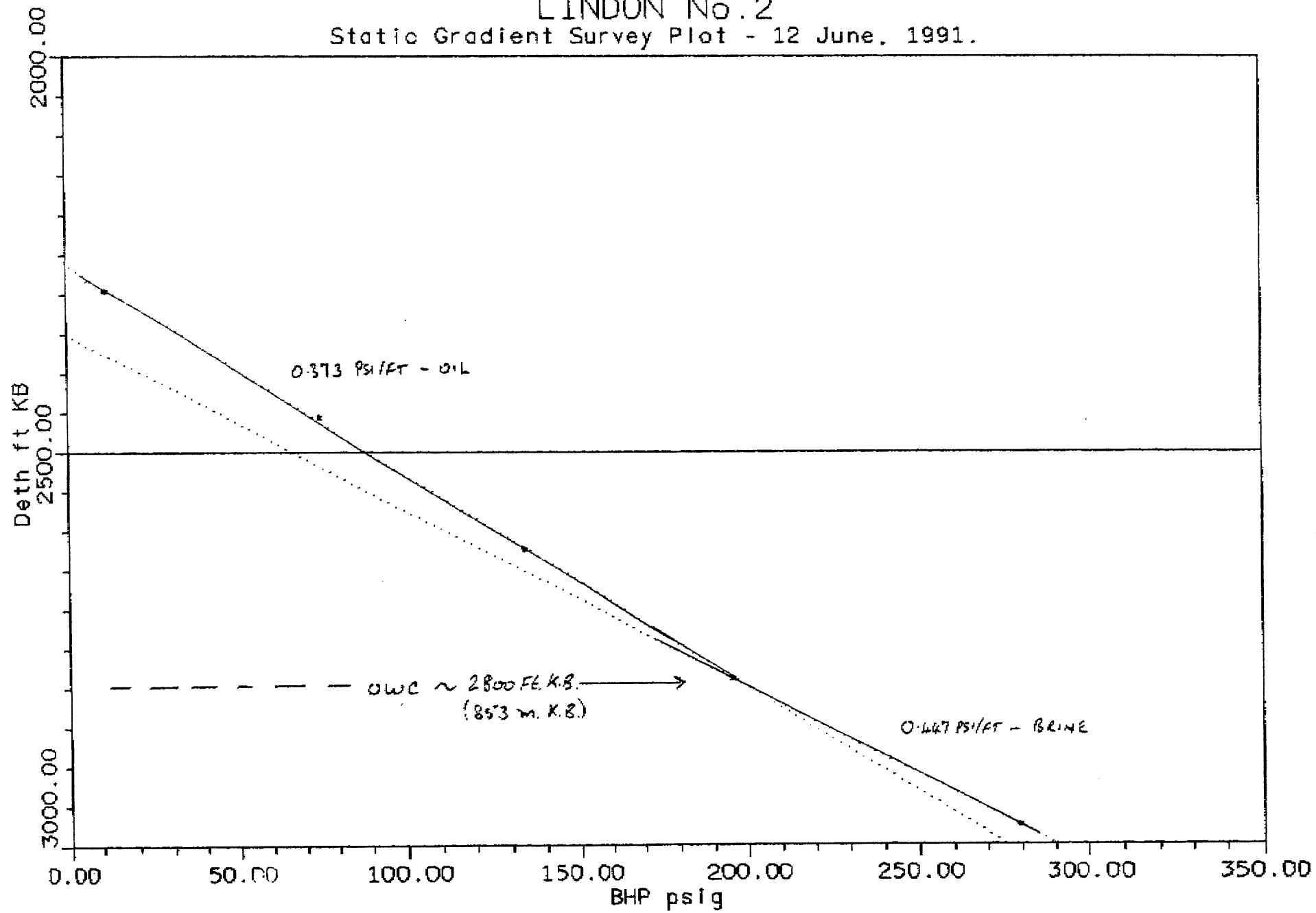
TAIPAN PETROLEUM PTY. LTD.
LINDON No.2

OPERATIONS REPORT: 5

Covering Daily Operations on: Wednesday 12 June, 1991.

- 08.00 hrs Ran Static Gradient survey #3; top of fluid column at
 692 m. (2269 ft.) K.B.
 OWC at approx. 853 m. (2800 ft.) K.B.
 BHP 279 psig at 907 m. (2975 ft.) K.B.
- Influx in 15³/₄ hrs overnight was 526 ft of 2⁷/₈ inch
 6.5# tubing, approximately 3.05 Bbls, of oil.
- 12.00 Suspend well test operations.
 Rig down all equipment ready for transport.
- 18.00 Secure well.

LINDON No. 2
Static Gradient Survey Plot - 12 June, 1991.



SOUTH AUSTRALIA
VICTORIA

141° 00'

141° 30'

37° 45'

PEP 105

PEP 105

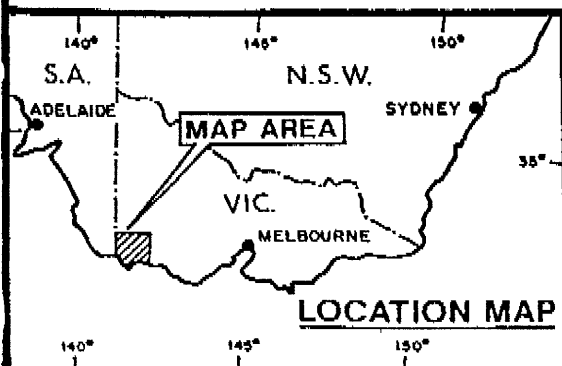
LINDON NO.2

38° 15'

141° 00'

141° 30'

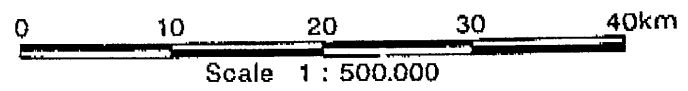
PORTLAND



LOCATION MAP

FIGURE 1

TAIPAN PETROLEUM PTY LTD
PEP 105
LINDON NO. 2
REGIONAL LOCATION MAP



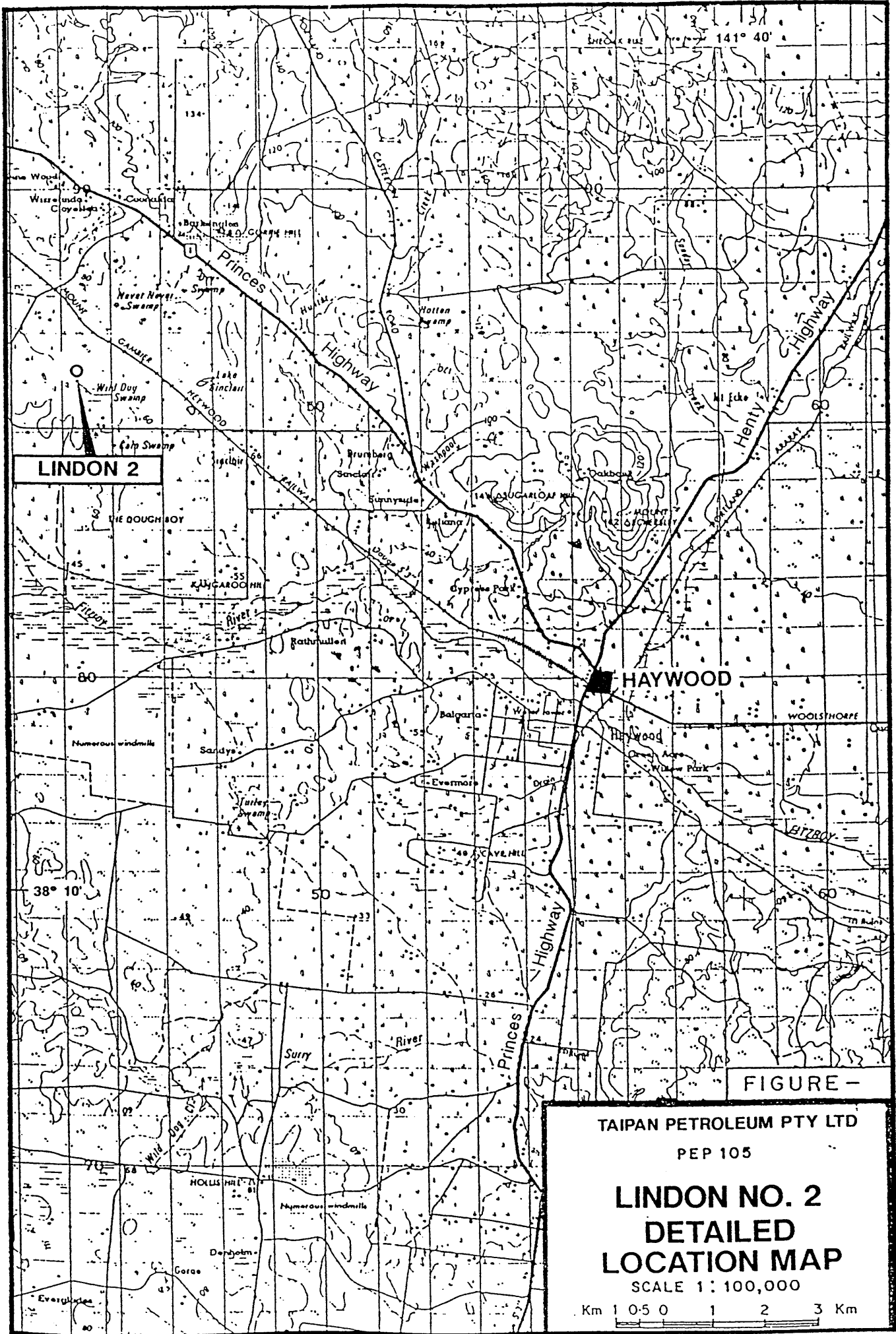


FIGURE -

TAIPAN PETROLEUM PTY LTD
 PEP 105

**LINDON NO. 2
 DETAILED
 LOCATION MAP**

SCALE 1 : 100,000

Km 1 0.5 0 1 2 3 Km

Figure 2

PE600852

This is an enclosure indicator page.
The enclosure PE600852 is enclosed within the
container PE902056 at this location in this
document.

The enclosure PE600852 has the following characteristics:

- ITEM_BARCODE = PE600852
- CONTAINER_BARCODE = PE902056
- NAME = Composite well log
- BASIN = OTWAY
- PERMIT =
- TYPE = WELL
- SUBTYPE = COMPOSITE_LOG
- DESCRIPTION = Composite well log for Lindon-2
- REMARKS =
- DATE_CREATED = 25/05/1991
- DATE_RECEIVED = 13/05/1992
- W_NO = W1045
- WELL_NAME = Lindon-2
- CONTRACTOR = H Geodata
- CLIENT_OP_CO = Taipan Petroleum

(Inserted by DNRE - Vic Govt Mines Dept)

PE600849

This is an enclosure indicator page.
The enclosure PE600849 is enclosed within the
container PE902056 at this location in this
document.

The enclosure PE600849 has the following characteristics:

ITEM_BARCODE = PE600849
CONTAINER_BARCODE = PE902056
NAME = Photodensity neutron caliper & gamma
ray log
BASIN = OTWAY
PERMIT =
TYPE = WELL
SUBTYPE = WELL_LOG
DESCRIPTION = Photodensity neutron caliper & gamma
ray log (1:200) for Lindon-2
REMARKS =
DATE_CREATED = 21/05/1991
DATE_RECEIVED = 13/05/1992
W_NO = W1045
WELL_NAME = Lindon-2
CONTRACTOR = BPB
CLIENT_OP_CO = Taipan Petroleum

(Inserted by DNRE - Vic Govt Mines Dept)

PE600851

This is an enclosure indicator page.
The enclosure PE600851 is enclosed within the
container PE902056 at this location in this
document.

The enclosure PE600851 has the following characteristics:

- ITEM_BARCODE = PE600851
- CONTAINER_BARCODE = PE902056
- NAME = Photodensity neutron caliper & gamma
ray log
- BASIN = OTWAY
- PERMIT =
- TYPE = WELL
- SUBTYPE = WELL_LOG
- DESCRIPTION = Photodensity neutron caliper & gamma
ray log (1:500) for Lindon-2
- REMARKS =
- DATE_CREATED = 21/05/1991
- DATE_RECEIVED = 13/05/1992
- W_NO = W1045
- WELL_NAME = Lindon-2
- CONTRACTOR = BPB
- CLIENT_OP_CO = Taipan Petroleum

(Inserted by DNRE - Vic Govt Mines Dept)

PE600853

This is an enclosure indicator page.
The enclosure PE600853 is enclosed within the
container PE902056 at this location in this
document.

The enclosure PE600853 has the following characteristics:

- ITEM_BARCODE = PE600853
- CONTAINER_BARCODE = PE902056
- NAME = Dual Laterolog, MRS, SP, Sonic Caliper
& Gamma ray
- BASIN = OTWAY
- PERMIT =
- TYPE = WELL
- SUBTYPE = WELL_LOG
- DESCRIPTION = Dual Laterolog, MRS, SP, Sonic Caliper
& Gamma ray for (1:500) Lindon-2
- REMARKS =
- DATE_CREATED = 21/05/1991
- DATE_RECEIVED = 13/05/1992
- W_NO = W1045
- WELL_NAME = Lindon-2
- CONTRACTOR = BPB
- CLIENT_OP_CO = Taipan Petroleum

(Inserted by DNRE - Vic Govt Mines Dept)

PE600850

This is an enclosure indicator page.
The enclosure PE600850 is enclosed within the
container PE902056 at this location in this
document.

The enclosure PE600850 has the following characteristics:

ITEM_BARCODE = PE600850
CONTAINER_BARCODE = PE902056
NAME = Computer Generated Log
BASIN = OTWAY
PERMIT =
TYPE = WELL
SUBTYPE = WELL_LOG
DESCRIPTION = Computer Generated Log (enclosure from
WCR) for Lindon-2
REMARKS =
DATE_CREATED = 21/05/1991
DATE_RECEIVED = 13/05/1992
W_NO = W1045
WELL_NAME = Lindon-2
CONTRACTOR = Crocker Data processing
CLIENT_OP_CO = Taipan Petroleum

(Inserted by DNRE - Vic Govt Mines Dept)