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WELL COMPLETION REPORT

PPL2 OTWAY BASIN VICTORIA IONA-2

K. LANIGAN / V. AKBARI / D. GRANT SEPTEMBER, 1994

TEXT AND APPENDICES VOLUME 1

KL/aj:lona-2wcrcover

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GFE RESOURCES LTD

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KL/aj:iona-2/wer

PETROLEUM DIVISION

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VOLUME 2

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SUMMARY

WELL DATA SUMMARY

Permit:

PPL2 Otway Basin, Victoria

Lat./Long.:

Surface 38° 34' 30.989"S 143° 02' 01.585"E

38° 34' 36.135"S 143° 02' 05.982"E TD

AMG:

Surface 677165.0mE

5728378mN

Seismic:

677267.9mE TD

5728217mN

Iona 93-01 Line

VP 248.2

Elevation:

Ground Level 128.5m AHD

Kelly Bushing (well datum) 134.2m AHD

Total Depth:

Drilled

1650.0mKB (driller) 1650.0mKB (logger)

True Vertical TD

1626.4mKB (-1492.2mSS)

Pre-drill Status: Development well Post-drill Status: Gas Producer

GFE Resources Ltd 100%

(Operator)

Rig:

Century Rig 11

Spud Date:

Participants:

1200 hrs 14/2/94

TD Reached: Rig Released: 1915 hrs 24/2/94 1000 hrs 06/3/94

Engineering

Hole Size

121/4" to 640m 81/2 " to 1650m Casing

16" Conductor to 16m (pre-spud) 95/8" 36lb/ft BTC K55 R3 to 636m

7" 26lb/ft L80 NEWVAM-RS to 1448.24m

Plugs

1. 1650-1471m (not tested)

Group	Formation/Unit		Depth	Thick	mess (m)	High/Low to		
		Drilled (mKB)	TVD (mKB)	TVD (mSS)	Drilled	TrueVertical	Prognosis	
Heytesbury	Port Campbell Limestone	5.7	5.7	128.5	-	-	-	
	Gellibrand Marl	not diffe	rentiated	-		-	-	
Nirranda	Narrawaturk Marl	not diffe	rentiated	-	-	-	-	
	Mepunga Formation	.284.5	284.5	-150.3	52.2	52.2	3.8m Low	
Wangerrip	Dilwyn Formation	336.7	336.7	-202.5	211.1	206.4	1.0 m Low	
	Pember Mudstone	547.8	543.1	-408.9	71.8	67.9	1.4 m Low	
	Pebble Point Formation	619.6	611.0	-476.8	52.4	49.8	0.3 m Low	
Sherbrook	Paaratte Formation	672.0	660.8	-526.6	360.7	349.1	1.1 m Low	
	Skull Creek Mudstone	1032.7	1009.9	-875.7	130.3	129.7	5.2 m Low	
	Nullawarre Greensand	1163.0	1139.6	-1005.4	95.0	94.9	3.1 m Low	
	Belfast Mudstone	1258.0	1234.5	-1100.3	39.0	38.9	2.2 m High	
	Waarre Formation Unit D	1297.0	1273.4	-1139.2	19.5	19.5	1.3 m High	
	Unit C	1316.5	1292.9	-1158.7	31.5	31.5	6.8 m High	
	Unit B	1348.0	1324.4	-1190.2	24.0	24.0	_	
	Unit A	1372.0	1348.4	-1214.2	29.5	29.5	_	
Otway	Eumeralla Formation	1401.5	1377.9	-1243.7	248.5	248.5	2.8 m High	
	TD	1650.0	1626.4	-1492.2				

Key Hydrocarbon Indications

Nullawarre Greensand:

3 - 32.4 units Total Gas

Waarre Formation Unit D: Waarre Formation Unit C: 6 - 8 units, with 32 unit peak at 1305 m 21.5 - 255 units, mostly above 100 units

Waarre Formation Unit B:

9 - 13.5 units, with broad 35 unit peak 1356 - 1362 m

Waarre Formation Unit A:

159 units at top, dropping quickly towards base

Eumeralla Formation:

1405 - 1435 m, 9.5 - 390 units, with trace -2% moderately bright yellow-orange pinpoint-patchy fluorescence.

1435 - TD, 4 - 46 units with peak 60 - 175 units at 1468 - 1470 m

	Logging	Cori	ng
DLL-MSFL-GR-SP-Cal	1645.5 - 5.5	No cores w	ere cut
LDL-CNL-GR-Cal	1649 - 1000		
AS/BHC-GR-Cal	1645.5 - 625	Completion	Logging
WSS (Checkshots)	20 levels	CBL-VDL-CCL-GR	1435 - 850
RFT-GR	26 pressure points, 1 fluid sample	Perforating & Packer Setting Record	1340.5 - 1334.5
CST-GR	Shot 30, Recovered 29		

Formation Tests

No formation tests were conducted

		Log /	Analysis (Pay Zor	ies)		
Interval	Thickness (m)	Net Sand (m)	Net Pay (m)	Av. Eff. Ø (%)	<u>S_w (%)</u>	V _{cl} (%)
1316.43 - 1347.98	31.55	27.9	27.58	23.81	16.71	5.29
1347.98 - 1371.91	23.93	5.60	5.03	23.08	17.94	8.81

INTRODUCTION

1. INTRODUCTION

The Iona structure was initially delineated by Beach Petroleum NL from the 1981 Curdie Seismic Survey and the 1986 Sherbrook Seismic Survey. Discovery of the gas accumulation within it occurred with the drilling of Iona-1 in March, 1988 in what was then part of PEP108. Beach Petroleum NL were the permit operators and Iona-1 was the final farmin commitment for Bridge Oil Limited to earn a 50% equity. The well encountered a 26-metre gross gas column within sandstone in the top half of the Late Cretaceous Waarre Formation which flowed at 8.1 MMCFD prior to being cased and suspended.

An area containing the Iona field was then acquired by the Gas and Fuel Corporation of Victoria (GFCV) in July, 1989 and this excised acreage became Petroleum Production Licence Two (PPL2) in December, 1990.

Iona-1 was brought on-stream in December, 1992 via a pipeline to the North Paaratte production facility in the adjacent PPL1, and since then has produced around 1.2 BCF per year to supply markets in Warrnambool and other local towns.

Ownership of PPL2 was transferred to GFE Resources Ltd on 1 July, 1993.

Further development of the Iona field was considered beneficial for a variety of reasons, mainly;

- to maintain security of supply to the existing gas market;
- to provide deliverability of the gas for the projected peak level;
- to ensure efficient reservoir management and optimum field drainage; and
- to investigate the hydrocarbon potential and reservoir characteristics of the Eumeralla Formation in this area.

Additional seismic was acquired in 1993 (the Iona Seismic Survey) and from the subsequent mapping a location for the Iona-2 development well was selected to penetrate the apex of the structure at the Top Waarre Formation level.

WELL HISTORY

2. WELL HISTORY

2.1 LOCATION (see Figures 1 and 2)

Surface Location:

Latitude:

38° 34' 30.989"S

Longitude:

143° 02' 01.585"E

AMG:

677165.0mE

5728378.0mN

Bottom Hole Location:

Latitude:

38° 34' 36.135"S

Longitude:

143° 02' 05.982"E

AMG:

677267.9mE

5728217.0mN

Seismic:

Line:

Iona 93-01

Vibe Point:

248.2

Property Title:

County:

Heytesbury

Parish:

Paaratte

Section:

2.

Allotment:

12A

Property Owner:

J. & G.J. Bognar

S. Meek

2.2. GENERAL DATA

Well Name:

Iona-2

Permit:

PPL2 Otway Basin, Victoria

Operator:

GFE Resources Ltd

Level 6, 6 Riverside Quay

South Melbourne Victoria 3205

Participants:

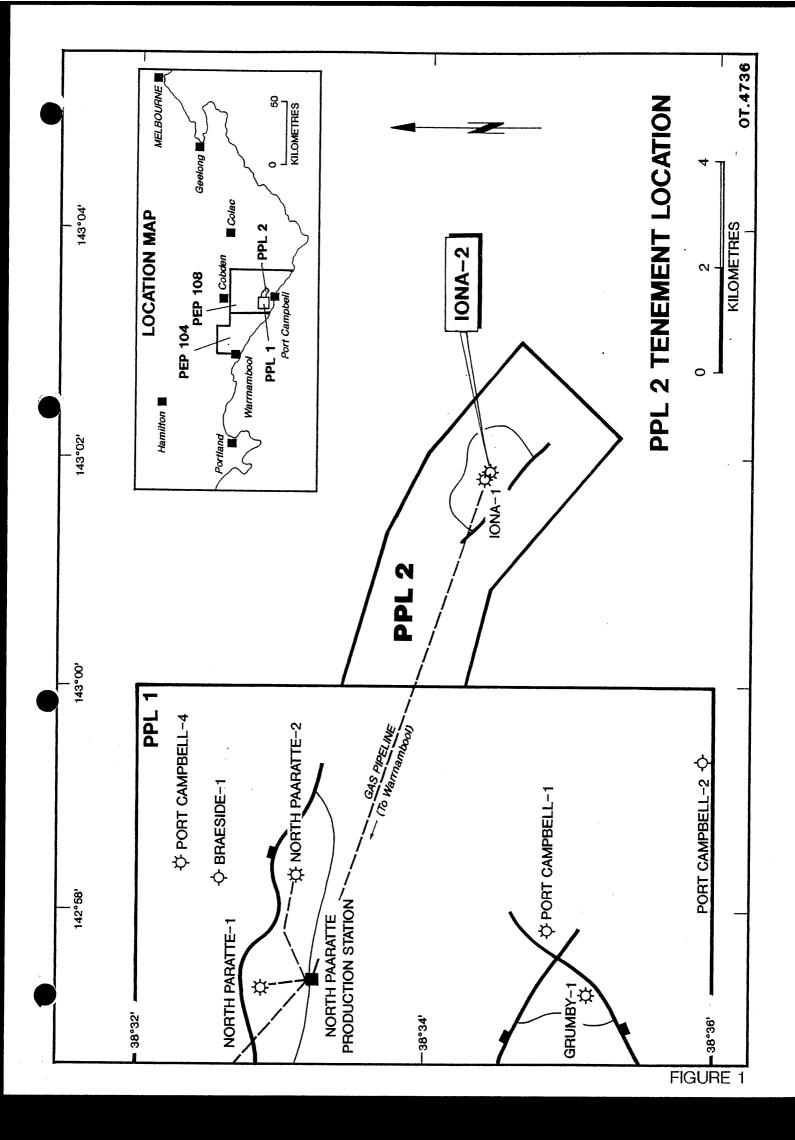
GFE Resources Ltd 100%

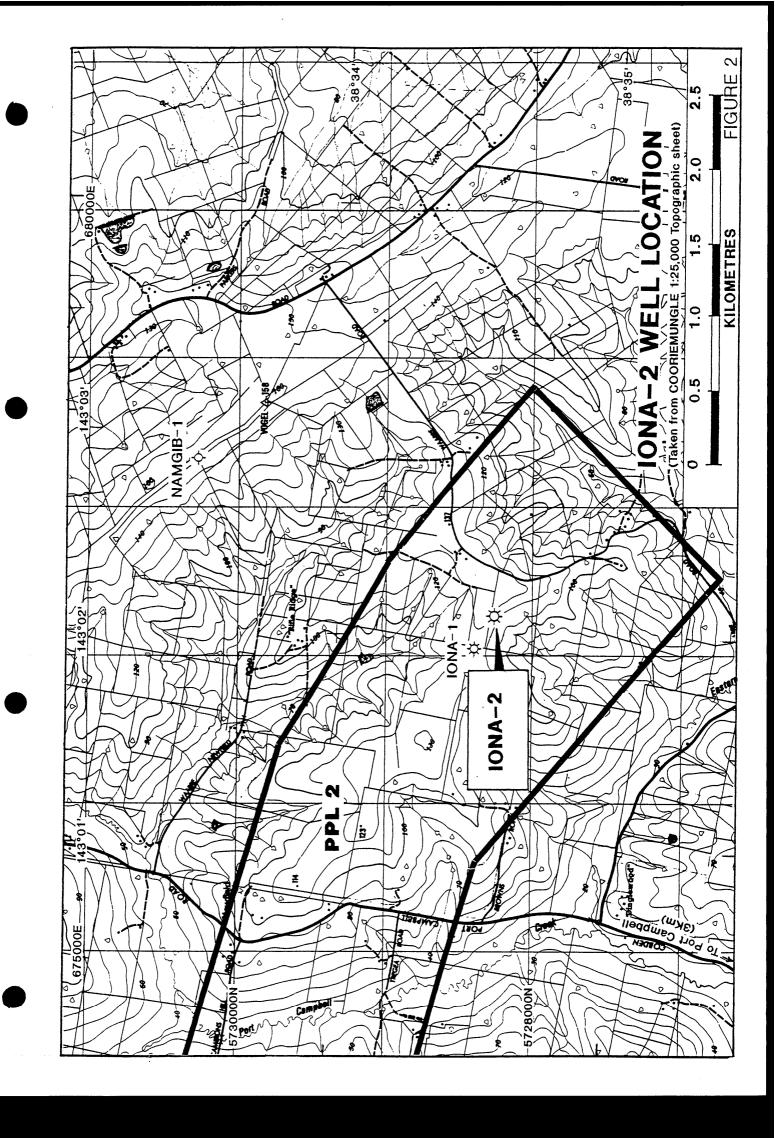
Elevation:

Ground Level (GL): 128.5m AHD

Kelly Bushing (KB): 134.2m AHD (datum)

(All depths are Drilled/Measured Depths relative to KB unless otherwise stated)





Total Depth (Measured/Drilled): Driller: 1650.0mKB

Logger:

1650.0mKB

Total Depth (True Vertical): 1626.4mKB (1492.2mSS)

Drilling Commenced: 1200 hours, 14 February, 1994

Total Depth Reached: 1915 hours, 24 February, 1994

Rig Released: 1000 hours, 6 March, 1994

Well Status: Gas producer

2.3. DRILLING DATA

2.3.1 Drilling Contractor

Century Drilling Limited

2.3.2 Drilling Rig

Century Rig 11 (see Appendix 1)

2.3.3 Casing and Cementing Details

A 16" Conductor pipe was cemented at 16m prior to rig up

Surface Casing

Size: 9⁵/₈"

Weight & Grade: 36 lb/ft BTC K55 R3

(54 Joints)

Centralizers: 634m, 612m, 589m,

565m, 519m, 473m, 426m,

339m, 333m and 287m

Float Collar: 624.4m

Shoe: 636m (logger depth)

Cement: 644 sacks Class "A"

cement mixed with 140bbls

2% prehydrated gel followed by 162 sacks Class "A" cement mixed

with 20bbls water with 0.15% HR4

Method: Single plug displacement

(top plug only)

Equipment: Halliburton Services

Production Casing

Size:

Weight and Grade: 26lb/ft L80 NEWVAM-RS (120 Joints)

7"

Centralizers: 1442m, 1399m, 1363m,

1345m, 1330m, 1315m, 1291m, 1255m, 1219m, 1184m, 1143m, 1112m,

1040m, 1004m, 960m, 933m,

897m and 861m

Float Collar: 1436.26m (driller depth)

Shoe: 1448.24m (driller depth)

Cement: 170 sacks Class "G" cement mixed

with 100 bbls 4% prehydrated gel

followed by 200 sacks Class "G" cement

mixed with 40 bbls water with 3%

Halad 322

Method: Single plug displacement

(top plug only)

Equipment: Halliburton Services

Cement plugs

<u>Plug No.1</u> Interval: 1650-1471m

Cement: 60 sacks class "A" cement

neat mixed with 3% HR4

Method: Balanced

Tested: No

2.3.4 Drilling Fluid

The drilling fluid program used was that designed and recommended by Baroid. Details of the mud system used and assessment of its performance is contained in the Drilling Fluid Recap (Appendix 2).

2.3.5 Drilling Bits

Four drilling bits were used during the drilling of Iona-2, and a record of their pertinent details is shown in Table 1.

2.3.6 Water Supply

Drilling water was obtained from an existing dam down hill from the lease and stored in a pit dug near the wellsite.

2.3.7 Drilling History

A summary of wellsite operations can be found in Appendix 3A, and a compilation of the operations summaries from daily reports issued during the drilling and completion of the well is provided in Appendix 3B.

2.4 FORMATION SAMPLING AND TESTING

2.4.1 Cuttings

No cutting samples were collected from surface to 150 metres. Cutting samples were then collected at ten-metre intervals from 150 to 640 metres $(9^{5}/_{8}"$ casing depth) and at 2.5-metre intervals down to total depth. Each sample was washed and air dried and divided into four splits, three of which were stored in labelled plastic bags and the fourth in "Samplex" trays.

Additionally, one set of 500 gram unwashed samples were collected at tenmetre intervals from 640 metres to total depth and stored in labelled cloth bags. All samples were retained by the operator.

Lithological descriptions of cuttings by the wellsite geologist during the drilling of Iona-2 are compiled in Appendix 4A, along with a compilation of the lithological descriptions from daily reports issued during the drilling of the well in Appendix 4B.

2.4.2 Cores

2.4.2.1 Conventional Core

No conventional cores were cut in Iona-2.

TABLE 1

BIT RECORD

Contractor:

Century Drilling

State:

Victoria

Spud: 14/2/94

GFE Representative:

Ken Smith

Permit: PPL2

Reached T.D.: 24/2/94

Rig:

#11

Well:

Iona-2

No.	Size	Make	Type	IADC Code	Serial	Depth Out	Metres Drilled	Hours	Av. Rate	Accum Drlg	Wt.	RPM	Vert Dev.	Pump Press.	Jets	GPM		Mud			ull. ond.	Remarks
						(m)			(m/hr)	Hours	000 lbs		(°)	(psi)			WT	VIS	WL	Т	B	- -
1RR	121⁄4"	Varel	L-114	1.1.4	26776	320	304	12½	24.3	12.5	5/20	120	0	550	1x18 2x20	450	8.9	41	N/C	1	3 1	POOH to kick off
2	12¼"	Sec	S33SF	1.1.6	629176	640	320	20	16	32.5	15/20	down hole motor	18.5	1400	3x16	508	9.3	47	11.8	2	1 1	12¼ T.D.
2RR	121/4"	Sec	S33SF	1.1.6	629176	640	(178)	5	36	<u>-</u>	0	40	18.5	1100	3x20	508	9.0	43	N/C	2	1 1	Reaming
3	81/2"	Varel	ETD417	4.1.7	88736	781	141	5	28	37.5	5/8	130	20.0	1400	2x10	305	8.9	38	13.9	1	1 1	BHA Change
3RR	81/2"	Varel	ETD417	4.1.7	88736	1052	271	13½	20	57.5	10/20	down hole motor	8.0	1425	2×12	305	8.9	42	11.3	1	1 1	BHA Change
3RR	8½"	Varel	ETD417	4.1.7	88736	1268	216	32	6.75	89.5	20	110	1.5	1225	2×12	305	9.4	44	6.8	1	1 1	Bit Change
							648*	50½*	12.8*													
	Not rea	ally a goo	d enough r	un to proj	pe rl y evalu	ate poten	tial. Slight	tly under	gauge bu	t would sti	ll be drilli	ng full go	auge hol	е.		<u></u>	I	1	1	LL		
4	81/2"	Varel	ETD417	4.1.7	88735	1650	382	31½	12.1	12.1	25	90	3/4	1225	3x12	305	9.4	40	6.4	1	1 1	T.D.
	Hole a	verage pe	enetration 1	3.6. A re	latively sh	ort and ea	sy run for	this type o	of bit.													<u> </u>

^{*} Totals for Bit No.3

2.4.2.2 Sidewall Cores

A total of 30 sidewall cores were attempted (Enclosure 9), of which 29 were recovered.

All recovered sidewall core samples were checked for lithology and hydrocarbon shows and then stored in sealed plastic jars. Sidewall core jars 1 through 19 subsequently had their head-space checked for hydrocarbons (see Section 3.3.2). Descriptions of the sidewall cores are contained in Appendix 5 and a summary of subsequent analyses is given in Section 2.4.4.

2.4.3 Testing

2.4.3.1 Drill Stem Testing

No Drill Stem Tests were carried out on Iona-2.

2.4.3.2 Wireline Formation Testing

Repeat Formation Test (RFT) pressure readings were carried out at 26 points spanning the Nullawarre, Waarre and Eumeralla Formations (Enclosure 7).

A summary of the RFT results is presented in Table 2 and the pressure points in the Waarre Formation are plotted in Figure 3, along with similar data from Iona-1.

While the Iona-1 data indicates a gas column in Unit C with a Gas/Water Contact (GWC) at around -1195.0mSS, the Iona-2 data is less straightforward, indicating one gas column in Unit C and a separate gas column in Unit B. Pressure points from beneath the gas column in Unit B and from Unit A are thought to be from water wet zones, but some points appear to be affected by supercharging, so GWC's could not be confidently identified.

A sample was taken in the Waarre Formation at 1361.8m (below the inferred GWC) to obtain a water sample on which $R_{\rm w}$ and salinity measurements could be made for possible use in log analysis. The resulting analysis is shown in Table 3, but the sample is unlikely to be pristine and thus not truly representative of $R_{\rm w}$.

TABLE 2

SUMMARY OF RFT RESULTS

Test No.	Depth (mKB)	Depth (mTVD)	Depth (mSS)	Pressure (psia)	Comment
1	1171.5	1147.5	1013.3	1501.1	Good Test
2	1175.0	1151.0	1016.8	1504.0	Good Test
3	1173.0	1149.0	1014.8	1501.1	Good Test
4	1318.0	1294.4	1160.2	1718.6	Good Test
5	1324.5	1300.9	1166.7	1719.0	Good Test
-6	1329.5	1305.9	1171.7	1719.8	Good Test
7	1336.0	1312.4	1178.2	1720.5	Good Test
8	1340.0	1316.4	1182.2	1721.1	Dry Test
9	1346.0	1322.4	1188.2	1721.9	Good Test
10	1355.0	1331.4	1197.2	1738.0	Good Test
11	1358.0	1334.4	1200.2	1738.9	Good Test
12	1361.5	1337.9	1203.7	1747.5	Super charged
13	1361.8	1338.2	1204.0	1742.8	Good Test
14	1381.0	1357.4	1223.2	1776.9	Good Test
15	1386.5	1362.9	1228.7	1781.6	Good Test
16	1388.5	1364.9	1230.7	1784.4	Good Test
17	1395.0	1371.4	1237.2	1793.5	Good Test
18	1407.5	1383.9	1249.7	-	Dry Test
10	1412.5	1388.9	1254.7		Dry Test
20	1404.5	1380.9	1246.7	-	Dry Test
21	1418.0	1394.4	1260.2	-	Dry Test
22	1423.5	1399.9	1265.7	-	Dry Test
23	1468.5	1444.9	1310.7	-	Lost Seal
24	1414.5	1390.9	1256.7	-	Lost Seal
25	1414.5	1390.9	1255.8	-	Dry Test
26	1361.8	1338.2	1204.0	-	Sample
27	1347.5	1323.9	1189.7	1722.0	Good Test

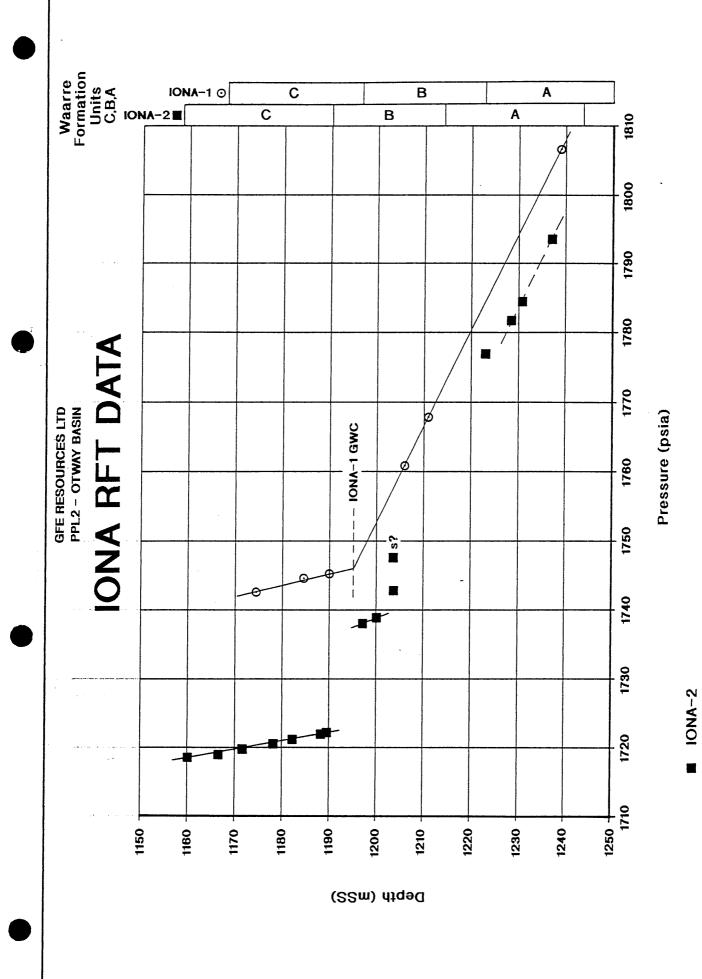


FIGURE 3

IONA-1

0

TABLE 3

WATER ANALYSIS OF RFT SAMPLE

Ph Conductivity (Resistivity (oh: Density @ 25°(Total Dissolve	6.05 29400 0.34 1.012 18815		
		(mg/l)	(me/l)
Sodium	Na	3180	138.26
Potassium	K	3350	85.90
Calcium	Ca	100	5.00
Magnesium	Mg	35.5	2.96
Soluble Iron	Fe(s)	5.0	-
Chloride	Cl	7300	205.63
Carbonate	CO_3	Nil	-
Bicarbonate	HCO_3	1205	19.75
Sulphate	SO_4	42	0.88
Nitrate	NO ₃	4.9	0.08
Sum of Ions		15217	

2.4.4 Sample Analysis

Analysis of selected cuttings and sidewall core samples from Iona-2 comprised organic geochemistry, palynology and petrography. Table 4 lists the analyses performed on each sample, details of which can be found in the appropriate Section/Appendix.

Palynology	see Section 3.6	and Appendix 6
Petrography	see Section 3.2.4.1	and Appendix 7
Geochemistry	see Section 3.4	and Appendix 8

2.5 LOGGING AND SURVEYS

2.5.1 Mud Logging

A standard skid-mounted unit equipped for continuous recording of depth, penetration rate, mud gas, pump rate and mud volume data, as well as intermittent mud and cuttings gas (blender) analysis was operative from 150m hole depth until the well was completed. The Formation Evaluation Log ("Mud Log") comprises Enclosure 2a, and a Gas Ratio Analysis Log comprises Enclosure 2b.

2.5.2 Wireline Logging

Wireline logging was performed by the Schlumberger Seaco using a standard truck-mounted unit. The logging suite carried out at total depth consisted of the following logs:-

Log	Interval (mKB)	Enclosure Number	
Dual Laterolog - Micro-Spherically Focussed Log - Gamma Ray - Spontane Potential - Caliper (DLL-MSFL-GR-SP-Cal)	1645.5 - 5.5 eous	3	
Lithodensity Log - Compensated Neutron Log - Gamma Ray - Caliper (LDL-CNL-GR-Cal)	1649 - 1000	4	
Sonic - Gamma Ray - Caliper (AS-GR-Cal) *	1645.5 - 625 1645.5 -1000	5	

TABLE 4

SIDEWALL CORES AND CUTTINGS ANALYSES

Sample	Depth (mKB)	SWC Recovery (cm)	Palynology	Geochemistry	Petrography
SWC#30	1034.5	5.0	/		
SWC#29	1090.5	4.0	✓		
SWC#28	1129.0	4.0	✓		
SWC#27	1161.0	4.0	<		
SWC#26	1260.0	3.0	✓		
SWC#25	1281.0	3.5	✓		
SWC#24	1290.0	4.0	✓		
SWC#23	1303.5	5.0	~		
SWC#22	1315.0	2.0	✓		
SWC#21	1353.0	3.0	✓		
SWC#20	1358.0	2.0		✓	
SWC#19	1362.0	2.5		✓	
SWC#18	1371.0	3.0	✓		
SWC#17	1374.0	3.0			
SWC#16	1381.0	4.5		✓	
SWC#15	1386.0	4.5			
SWC#14	1392.0	3.5		✓	
SWC#13	1402.0	2.5	~		
SWC#12	1408.5	3.5		✓	Y
SWC#11	1412.0	5.0	✓		✓
SWC#10	1418.0	3.5			✓
SWC#9	1426.0	3.5		✓	V.
SWC#8	1437.5	2.5	✓		
SWC#7	1457.5	5.0	√		
SWC#6	1469.0	3.5		✓	V
SWC#5	1516.5	6.5	✓		✓
SWC#4	1537.0	no recovery			
SWC#3	1550.5	3.0		\checkmark	\checkmark
SWC#2	1590.0	1.5	✓		
SWC#1	1599.0	1.5	Y		
Cuttings	1365 - 1370			✓	
Cuttings	1385 - 1390				
Cuttings	1410 - 1415				
Cuttings	1347 - 1350		✓		
Cuttings	1332 - 1335		✓		
Cuttings	1312 - 1315		√		
Cuttings	1292 - 1295		√		

(BHC-GR)	1000 - 625	
Well Seismic Survey (WSS Checkshot)	1570 - 530	8
Repeat Formation Tester - Gamma Ray (RFT-GR)	1650 - 1171.5	7
Cement Bond Log - Variable Density Log - Casing Collar Locator - Gamma Ray (CBL-VDL-CCL-GR)	1435 - 850	6
Perforation and Packer Setting Record	1340.5 - 1334.5	10
Sidewall Core Sampler (CST-GR)	1599 - 1034.5	9

^{*} An array sonic was requested but, due to operator error, the full waveform was not recorded, and this was not noticed until after the hole was cased. Schlumberger subsequently ran the array sonic through casing in an attempt to obtain some meaningful data, but this was not successful.

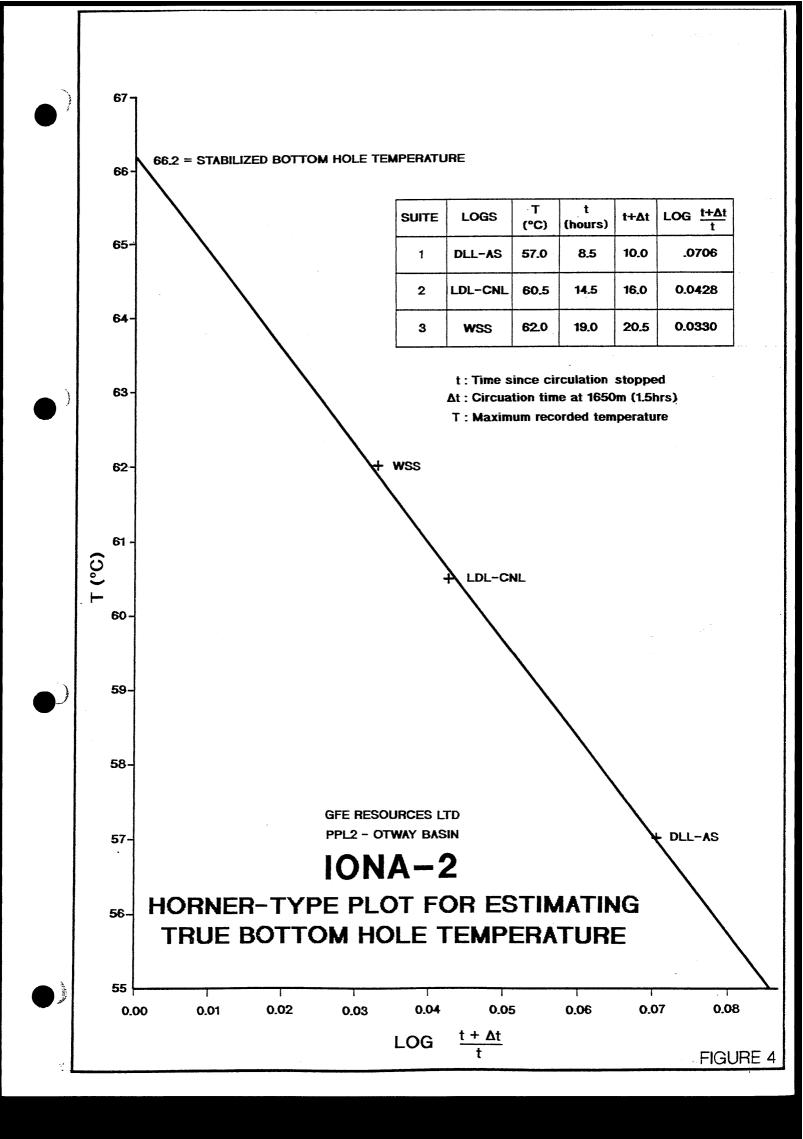
2.5.3 Bottom Hole Temperature

Maximum temperatures recorded during wireline logging were as follows:

Log	(mKB) Depth	(mTVD)	Temperature (°C)	
DLL-MSFL-AS-GR	1645.5	1624.9	57.0	
LDL-CNL-GR	1649.0	1625.4	60.5	
WSS	1649.5	1625.9	62.0	
RFT	1468.5	-	56.1	

The first three of these were plotted on a modified Horner plot and, using a straight line best-fit extrapolated back to the Temperature axis, a stabilised bottom hole temperature of 66.2°C was obtained (Figure 4). The RFT maximum recorded temperature was not used because the depth it was recorded at was well above T.D., and thus not valid for this purpose.

Assuming a mean surface temperature of 18°C, the stabilised bottom hole temperature of 66.2°C at 1625mTVD yields a temperature gradient of 3.0°C per 100 metres.



2.5.4 Deviation Surveys

Totco deviation surveys were carried out while drilling straight hole to 320m, with results as shown in Table 5.



Totco Deviation Surveys

Depth (mKB)	Deviation (°)		
48.70	3/4		
84.70	1/2		
119.50	1/2		
155.80	1/2		
229.00	1/4		
257.00	1/4		

From 320m the hole was directionally drilled with deviation angles being continually monitored by means of Measurement While Drilling (MWD) equipment, to a maximum of 20° (reached at 774m). Below 774m the drift angle was gradually decreased, falling to less than 2° below 1300m and less then 1° below 1530m. During drilling this was monitored with single-shot surveys, and at total depth, a multi-shot survey was performed. Results of these surveys are included in the Directional Drilling Report (Appendix 9).

The calculated true vertical depth (TVD) and horizontal departure (HD) at total depth are as follows:

TVD: 1626.4mKB (1492.2mSS)

HD: 191metres towards 148° from the surface location.

2.5.5 Velocity Surveys

A Velocity Survey (WSS-Checkshot) was carried out by Schlumberger Seaco, and the raw data (Enclosure 8) was corrected to obtain time versus depth values below the seismic reference datum. The procedure used in this correction and the resulting values are presented in Appendix 10 and the resulting time-depth velocity-depth curves and synthetic seismogram are shown with the Iona 93-01 seismic line in Figure 5.

PE906674

This is an enclosure indicator page. The enclosure PE906674 is enclosed within the container PE900963 at this location in this document.

The enclosure PE906674 has the following characteristics:

ITEM_BARCODE = PE906674
CONTAINER_BARCODE = PE900963

NAME = Time-Depth Curve

BASIN = OTWAY

PERMIT = PPL2

TYPE = WELL

SUBTYPE = VELOCITY_CHART

DESCRIPTION = Time-Depth Curve for Iona-2

REMARKS =

DATE_CREATED =

DATE_RECEIVED = 19/01/95

 $W_NO = W1095$

WELL_NAME = IONA-2

CONTRACTOR =

CLIENT_OP_CO = GFE RESOURCES LTD

(Inserted by DNRE - Vic Govt Mines Dept)

PE906675

This is an enclosure indicator page. The enclosure PE906675 is enclosed within the container PE900963 at this location in this document.

The enclosure PE906675 has the following characteristics:

ITEM_BARCODE = PE906675
CONTAINER_BARCODE = PE900963

NAME = Seismic Section and Synthetic

Seismogram

BASIN = OTWAY PERMIT = PPL2

TYPE = WELL

SUBTYPE = MONTAGE

DESCRIPTION = Interpreted Seismic Section with

Synthetic Seismogram and Time-Depth

Curve for Iona-2

REMARKS =

DATE_CREATED = 30/09/94 DATE_RECEIVED = 19/01/95

 $W_NO = W1095$

WELL_NAME = IONA-2

CONTRACTOR =

CLIENT_OP_CO = GFE RESOURCES LTD

(Inserted by DNRE - Vic Govt Mines Dept)

GEOLOGY

3. GEOLOGY

3.1 STRATIGRAPHY

The section penetrated in Iona-2 is interpreted to have formation tops as shown in Table 6 based on consideration of rate of penetration, cuttings descriptions, palynology and wireline logs (primarily the latter).

Iona-2 was drilled as a deviated hole below 320 metres, so Table 6 shows both Drilled (or Measured) and True Vertical Depths and Thicknesses. The True Vertical Depths have been calculated from the Measured Depths via interpolation of the Directional Drilling data (Appendix 9). Unless stated otherwise, depths mentioned in this report will be the Measured Depth (MD) below the well datum, the kelly bushing (KB). True Vertical Depths are used where correlation away from the well bore is required, i.e. to other wells or to integrate into seismic data.

Comparison with a selection of nearby wells was undertaken, particularly Iona-1, which was drilled only a few hundreds metres away. Due to a lack of cuttings samples above 150 metres and a lack of distinguishing gamma ray character, tops for the Gellibrand Marl and Narrawaturk Marl could not be satisfactorily identified in Iona-2, but are thought likely to be at similar depths to those picked in Iona-1. A correlation between the two Iona field wells is shown in Figure 6, and it is important to note that the Iona-2 log shown there has been variably compressed in proportion to the degree of hole deviation so that it is a True Vertical Depth (TVD) profile.

It should also be noted that some minor changes have been made to the Iona-1 picks given in the Well Completion Report (Buffin, 1989), most notably the shift of the top of the Waarre Formation Unit A from 1366 metres to 1354 metres, which is currently thought to be a more appropriate position based on the Iona-2 logs.

PE906676

This is an enclosure indicator page.

The enclosure PE906676 is enclosed within the container PE900963 at this location in this document.

The enclosure PE906676 has the following characteristics:

ITEM_BARCODE = PE906676
CONTAINER_BARCODE = PE900963

NAME = Stratigraphic Correlation

BASIN = OTWAY

PERMIT = PPL2

TYPE = WELL

SUBTYPE = STRAT_COLUMN

DESCRIPTION = Stratigraphic Correlation of Iona-1 and

Iona-2

REMARKS =

DATE_CREATED = 31/08/94

DATE_RECEIVED = 19/01/95

 $W_NO = W1095$

WELL_NAME = IONA-2

CONTRACTOR =

CLIENT_OP_CO = GFE RESOURCES LTD

(Inserted by DNRE - Vic Govt Mines Dept)

TABLE 6

Stratigraphic Unit	Drilled * Depth	Drilled Thickness	True Vertical Depth [TVD]		True Vertical Thickness [TVT]
	(mKB)	(m)	(mKB)	(mSS)	(m)
Heytesbury Group	5.7	-	5.7	128.5	-
Port Campbell Limestone	5.7	_	5.7	128.5	-
Gellibrand Marl	not differentiated	-	-	-	-
Nirranda Group	not differentiated	_	_	_	-
Narrawaturk Marl	not differentiated	_	-		
Mepunga Formation	284.5	52.2	284.5	-150.3	52.2
Wangerrip Group	336.7	335.3	336.7	-202.5	324.1
Dilwyn Formation	336.7	211.1	336.7	-202.5	206.4
Pember Mudstone	547.8	71.8	543.1	-408.9	67.9
Pebble Point Formation	619.6	52.4	611.0	-476.8	49.8
Sherbrook Group	672.0	729.5	660.8	-526.6	717.1
Paaratte Formation	672.0	360.7	660.8	-526.6	349.1
Skull Creek Mudstone	1032.7	130.3	1009.9	-875.7	129.7
Nullawarre Greensand	1163.0	95.0	1139.6	-1005.4	94.9
Belfast Mudstone	1258.0	39.0	1234.5	-1100.3	38.9
Waarre Formation	1297.0	104.4	1273.4	-1139.2	104.4
Unit D †	1297.0	19.5	1273.4	-1139.2	19.5
Unit C	1316.5	31.5	1292.9	-1158.7	31.5
Unit B	1348.0	24.0	1324.4	-1190.2	24.0
Unit A	1372.0	29.5	1348.4	-1214.2	29.5
Otway Group	1401.5	248.5	1377.9	-1243.7	248.5
Eumeralla Formation	1401.5	248.5	1377.9	-1243.7	248.5
Total Depth (Driller) Total Depth (Logger)	1650.0 1650.0		1626.4 1626.4	-1492.2 -1492.2	

^{*} Also referred to as Measured Depth (MD)

[†] Also known as the Flaxman Formation

3.2 LITHOLOGY

The following is a summary of the lithological units observed in Iona-2. More detailed descriptions are included in Appendix 4, as well as on the Mud Log (Enclosure 2a). Additional lithological information can be found in the Sidewall Core Description (Appendix 5) and the associated petrography report (Appendix 7).

3.2.1 Heytesbury and Nirranda Groups (Surface - 336.7m)

3.2.1.1 Port Campbell Limestone

Due to no cuttings samples being collected above 150 metres and a lack of gamma ray character this unit could not be identified in Iona-2. It is recorded as occurring from surface to 39 metres in Iona-1.

3.2.1.2 Gellibrand/Narrawaturk Marls (undifferentiated)

From the start of sampling (150m) down to about 280 metres the observed lithology was;

Marl: medium greenish grey to brownish grey, very soft, sticky, occasionally silty, common to abundant fossil fragments (including bryozoa, gastropods and sponge spicules), massive, with trace pyrite and coaly fragments below about 200 metres and trace to occasionally common glauconite towards the base.

The Gellibrand/Narrawaturk contact may be around 200 metres in Iona-2 (it was picked at 202m in Iona-1), but could not be positively identified from the available data.

3.2.1.3 Mepunga Formation (284.5 - 336.7m)

Sandstone; medium to dark brownish-grey; fine to coarse, dominantly coarse; poorly sorted; subangular to subrounded, dominantly subrounded quartz; common iron oxide; rare glauconite; trace pyrite, trace mica; moderate calcareous cement; fair visual porosity.

3.2.2 Wangerrip Group (336.7 - 672.0m)

3.2.2.1 Dilwyn Formation (336.7 - 547.8m)

Sandstone; off white; translucent; fine to coarse, dominantly coarse; poorly to moderately sorted; subangular to subrounded, dominantly subrounded quartz; common brown and orange iron oxide stain, occasional pyrite; occasional glauconite; trace mica; good intergranular porosity, interbedded with

Claystone: dark greyish to brown; very silty; micromicaceous; massive; soft; dispersive.

3.2.2.2 Pember Mudstone (547.8 - 619-6m)

Claystone; medium to dark brownish to grey; moderately silty; trace to common glauconite; trace pyrite; micromicaceous; massive; soft; dispersive.

3.2.2.3 Pebble Point Formation (619.6 - 672.0m)

Sandstone; medium to dark brown; very fine to very coarse, occasionally pebbly, dominantly coarse; poorly sorted; subangular to subrounded, dominantly subrounded quartz; common iron oxide; moderate iron oxide cement; common to abundant argillaceous matrix; soft; poor visual porosity, interbedded with

Claystone; dark brownish-grey, occasionally light to medium brown; trace volcanic lithics; trace pyrite; trace fossil fragments; massive; moderately firm.

3.2.3 Sherbrook Group (672.0 - 1401.5m)

3.2.3.1 Paaratte Formation (672.0 - 1032.7m)

Sandstone: white to light grey, translucent; very fine to coarse, occasionally pebbly, dominantly coarse; poorly sorted; subangular to subrounded, dominantly subrounded; quartz; trace multi-colour lithics; trace mica; trace pyrite; weak brownish-grey silty matrix; poor visual porosity, soft, interbedded with

Claystone; light to medium grey; silty; micromicaceous; carbonaceous; soft; dispersive and minor *Coal*; dark brown to black, soft.

3.2.3.2 Skull Creek Mudstone (1032.7 - 1163.0m)

Claystone; medium to dark grey-brownish; very silty, occasionally grading into argillaceous siltstone; micromicaceous; carbonaceous; very soft; dispersive, interbedded with thin

Sandstone: light grey, translucent; fine to medium, dominantly fine; moderately sorted; subangular to subrounded, dominantly subrounded quartz; common multi-colour lithics; rare mica; rare pyrite; rare to common argillaceous matrix; poor visual porosity; soft.

3.2.3.3 Nullawarre Greensand (1163.0 - 1258.0m)

Sandstone; very light green, translucent; very fine to medium, dominantly fine; moderately sorted; subangular to subrounded, dominantly subrounded quartz; rare to common dark green glauconite; rare coloured lithics; no apparent matrix; good intergranular porosity; loose.

3.2.3.4 Belfast Mudstone (1258.0 - 1297.0m)

Claystone: dark grey-greenish; silty; common to abundant glauconite nodules increasing with depth; common carbonaceous detritus; rare pyrite; soft.

3.2.3.5 Waarre Formation (1297.0 - 1401.5m)

3.2.4.5.1 Unit D (1297.0 - 1316.5m)

Claystone; dark grey; silty; carbonaceous; rare to common glauconite; rare pyrite; soft; dispersive, interbedded with thin Sandstone; light grey to tan; fine to medium, dominantly medium; poorly to moderately sorted; subangular to subrounded, dominantly subrounded quartz; rare to common glauconite; common pyrite; weak calcareous cement; poor visual porosity; soft to moderately hard.

3.2.3.5.2 Unit C (1316.5 - 1348.0m)

Sandstone; light brownish-grey, translucent; very fine to coarse, dominantly medium; poorly to moderately sorted;

subangular to subrounded, dominantly subrounded quartz; trace pyrite; trace glauconite; trace to common multi-colour lithics; weak silica cement; weak calcareous cement; good intergranular porosity; soft to moderately firm, interbedded with minor

Claystone; dark grey; silty; carbonaceous; rare glauconite and pyrite, soft.

3.2.3.5.3 Unit B (1348.0 - 1372.0m)

Claystone; dark grey; silty; carbonaceous; rare glauconite, rare pyrite; soft; dispersive, interbedded with thin Sandstone; light brownish-grey; very fine to coarse, dominantly medium; poorly sorted; subangular to subrounded, dominantly subrounded quartz; trace pyrite; trace glauconite; common lithics; weak silica cement; good intergranular porosity; soft.

3.2.3.5.4 Unit A (1372.0 - 1401.5m)

Sandstone: white to light grey, translucent; very fine to coarse; dominantly fine; moderately sorted; subangular to subrounded, dominantly subrounded quartz; common to rare multi-colour lithics; common carbonaceous detritus; rare mica; moderate calcareous cement; poor to fair visible porosity; moderately hard.

3.2.4 Otway Group (1401.5 - 1650.0m)

3.2.4.1 Eumeralla Formation (1401.5 - 1650.0m)

<u>Sandstone</u>; White to very light grey; very fine to medium, dominantly fine; moderately sorted; subangular to subrounded, dominantly subrounded quartz; common multi-colour lithics; rare to common altered feldspars; common carbonaceous detritus; moderate silica cement poor to fair visual porosity; moderately hard, interbedded with <u>Claystone</u>; light to medium grey, brownish; silty; common multi-colour lithics; micromicaceous; carbonaceous; soft and sticky.

3.3 HYDROCARBON INDICATIONS

3.3.1 Mud Gas Readings

The mud gas detection equipment was operational from a hole depth of 150 metres until the 7" casing was run. The levels of gas detected during drilling are plotted on the Mud Log (Enclosure 2a) and can be summarised as follows:

- > Down to 540 metres no gas was detected.
- ➤ Over the interval 540 641 metres (which encompasses the Pember Mudstone and upper Pebble Point Formation) mud gas readings ranged;

Total Gas : 0.1 - 1.6 units C_1 : 1 - 180 ppm C_2 : BDL* - 35 ppm C_3 : BDL* - 22 ppm

with the maximum encountered at 575 metres.

- From 641 metres down to 740 metres (the middle and lower Pebble Point Formation and the uppermost Paaratte Formation) no gas was detected.
- From 740 metres down to about 1085 metres (covering most of the Paaratte Formation and the top half of the Skull Creek Mudstone) mud gas readings were low and stayed relatively flat, ranging;

Total Gas: BDL - 0.1 units

 C_1 : 1 - 6 ppm

Through the lower half of the Skull Creek Mudstone (1085 - 1159 metres) gas readings began to increase fairly steadily, ranging;

Total Gas : 0.1 - 6.5 units C_1 : 9 - 1240 ppm C_2 : 1 - 38 ppm C_3 : BDL - 22 ppm

C₄ : BDL - 3 ppm (only in lowest 5 metres)

^{*} Note: BDL denotes Below Detection Limit.

and over the interval 1160 - 1238 metres (broadly corresponding to the Nullawarre Greensand) ranged;

Total Gas : 3 - 32.4 units (mostly above 5 units) C_1 : 600 - 6000 ppm (mostly above 1200ppm) C_2 : 1 - 38 ppm (mostly above 20ppm) C_3 : 2 - 45 ppm (mostly above 5ppm) C_4 : 1 - 20 ppm

From 1240 metres down to 1317 metres (broadly corresponding to the Belfast Mudstone and the Waarre Formation Unit D) mud gas readings dropped off, ranging;

 Total Gas
 : 1 - 8.8 units

 C_1 : 208 - 1540 ppm

 C_2 : 2 - 59 ppm

 C_3 : BDL - 32 ppm

 C_4 : BDL - 4 ppm

except for a peak (within the Unit D interval) centred on 1305 metres which ranged up to;

 $\begin{array}{cccc} \text{Total Gas} & : & 32 \text{ units} \\ \text{C}_1 & : & 5073 \text{ ppm} \\ \text{C}_2 & : & 425 \text{ ppm} \\ \text{C}_3 & : & 126 \text{ ppm} \\ \text{C}_4 & : & 28 \text{ ppm} \end{array}$

Formation Unit C - the main reservoir unit) gas readings ranged;

Total Gas: 21.5 - 255 units (mostly above 100 units) C_1 3680 - 43200 ppm (mostly above 18000ppm) C_2 147 - 2478 ppm (mostly above 800ppm) C_3 57 - 945 ppm (mostly above 300ppm) C_4 30 - 332 ppm (mostly above 100ppm) C_5 1 - 66 ppm (mostly above 10ppm)

notably including the first detection of C₅.

> Throughout the interval 1350 - 1373 metres (corresponding to Waarre Formation Unit B) gas readings dropped markedly to a background of;

Total Gas : 9 - 13.5 units C_1 : 1468 - 2200 ppm C_2 : 60 - 118 ppm C_3 : 41 - 65 ppm C_4 : 8 - 25 ppm C_5 : BDL - 2 ppm

with a broad peak at 1356 - 1362 metres ranging;

Total Gas : 35 - 36.5 units C_1 : 6000 - 6240 ppm C_2 : 250 - 263 ppm C_3 : 110 - 120 ppm C_4 : 35 - 40 ppm

Gas readings rose sharply again at 1375 metres (corresponding to the top of Waarre Formation Unit A);

Total Gas : 159 units C_1 : 31000 ppm C_2 : 310 ppm C_3 : 57 ppm C_4 : 33 ppm

but then dropped quickly towards the base, falling to 3.2 units of Total Gas at 1400 metres.

Within the Eumeralla Formation gas readings divide readily into two intervals. The uppermost, 1405 - 1434 metres, corresponds to a dominantly sandy interval where values ranged:;

Total Gas: 9.5 - 390 units (mostly above 50 units) C_1 1720 - 61000 ppm (mostly above 7000 ppm) C_2 44 - 3150 ppm (mostly above 400 ppm) C_3 40 - 2150 ppm (mostly above 260 ppm) C_4 7 - 960 ppm (mostly above 60 ppm) (mostly above 7 ppm) C_5 1 - 70 ppm

> Below 1434 metres mud gas readings through the rest of the Eumeralla Formation ranged;

Total Gas : 4 - 46 units C_1 : 720 - 8000 ppm C_2 : 19 - 398 ppm C_3 : 13 - 200 ppm

 C_4 : 1 - 75 ppm

 C_5 : BDL - 15 ppm (mostly BDL)

except for one notable peak at 1468 - 1470 metres (corresponding to the top of a thick sandstone unit) which ranged:

Total Gas: 60 - 175 units

 C_1 : 7200 - 21600 ppm C_2 : 730 - 2190 ppm C_3 : 530 - 1630 ppm C_4 : 280 - 860 ppm

 C_5 : 50 - 150 ppm

3.3.2 Sidewall Core Gas Reading

Shortly after recovering the sidewall cores, each was placed in a sealed container and subsequently the air within each container was sampled via syringe and analysed in the Baker-Hughes Inteq chromatograph. Results of these analyses are included with the sidewall core descriptions in Appendix 5.

3.3.3 Fluorescence

Cuttings samples and sidewall cores were routinely inspected for shows with the following results;

3.3.3.1 Cuttings

No significant fluorescence or oil staining was observed down to 1360 metres (the middle of Waarre Formation Unit B).

Within sandstones from 1360 to 1400 metres, 10 - 30% moderately bright, medium yellow pin-point fluorescence with instant bright yellow to milky white cut was observed.

In the Eumeralla Formation down to 1435 metres, trace to 20% moderately bright, pin-point to patchy, medium to light yellow fluorescence with slow streaming, light-medium yellow cut was observed.

Cuttings samples from 1365, 1385 and 1410 metres were submitted during drilling for a "quick look" evaluation of hydrocarbons and the results are included in the Geochemistry section.

No fluorescence or staining were observed from 1435 metres to Total Depth.

3.3.3.2 Sidewall Cores

Fluorescence was observed in six sidewall cores, two each from the Waarre Formation Units A and B and the upper Eumeralla Formation. Descriptions of the fluorescence and cut for each are included in Appendix 5. Five of these were submitted for geochemical analysis via extraction, liquid chromatography and gas chromatography of the saturates fraction, and two were then selected for GC-MS. In addition to these, three sandstone sidewall cores which did not exhibit fluorescence were analysed by whole extract gas chromatography. Results from all these analyses are included in the Geochemistry section.

3.3.4 Clean-up Flow Gas Sample

No sampling of gas was attempted during the drilling of Iona-2. Subsequent to the completion of the well a clean-up flow was conducted prior to connection to the North Paaratte production facility. Analysis of a gas sample taken during this flow is shown in Table 7 and, as expected, it closely resembles analyses of the Waarre Formation gas sampled in Iona-1.

TABLE 7

Iona-2 Gas Analysis

Component	Mole Percent Concentration
Methane	84.300
Ethane	3.070
Propane	1.260
Iso-Butane	0.293
Normal-Butane	0.324
Neo-Pentane	0.005
Iso-Pentane	0.122
Normal-Pentane	0.094
Hexanes	0.190
Heptanes+	0.280
Carbon Dioxide	6.490
Oxygen+Argon	0.025
Nitrogen	3.470
Helium	0.059

Calculated Properties f	for the dry gas at M.S.C
Gross Heating Value	37.1 MJ/m ³
Wobbe Index	44.8 MJ/ m ³
Relative Density	0.685

Analyst: I. Strudwick	
	Fuel Corporation of Victoria, Services Division
Report Reference Num	ber: 94/0608
Procedure References:	
	ISO 6976

3.4 GEOCHEMISTRY

3.4.1 Analyses

A total of 11 samples (8 sidewall cores and 3 cuttings) from Waarre Formation Units A and B and the Eumeralla Formation were analysed to identify and characterise their hydrocarbon content. No source rock studies were undertaken due to a perceived lack of source potential throughout the penetrated section.

The three cuttings samples from intervals exhibiting fluorescence were submitted for thermal extract gas chromatography (GC_{therm}) using Geotech's Geo-Fina Hydrocarbon Meter (GHM). All of the eight sidewall cores were sandstone; but three did not show any fluorescence, and so were only analysed by whole-extract gas chromatography (GC_{whole}). Extracts from the remaining five underwent liquid chromatographic separation followed by gas chromatography of the saturates fraction (GC_{sats}) and two of these were then selected for gas chromatography-mass spectrometry (GC-MS) work. One was also run in the GHM to attempt to provide a comparison with (and thereby integration of) the cuttings GHM data.

Also for comparison, extraction of SWC 7 (1391.5m) from Iona-1 was undertaken followed by liquid chromatographic separation and gas chromatography of the saturates fraction.

Data from all these analyses, as well as interpretation by Geotech, are collated into a report included here as Appendix 8.

3.4.2 Results

 GC_{therm} was performed on cuttings from the Waarre and Eumeralla Formations (1365m, 1385m an 1410m) during drilling to characterize the nature of the shows, notably oberved fluorescence. The chromatograms of the three samples indicate the presence of a hydrocarbon rich in n-alkanes above C_{17} and also in the gasoline fraction. The n-alkane content below C_{17} is severely depleted. All three chromatograms also show a baseline hump peaking at approximately C_{25} .

The baseline hump has a strong signature indicative of pipe dope. This renders interpretation of the chromatograms somewhat speculative. Ignoring this hump, these samples have similar characteristics and are most likely the same oil. The moderate odd-over-even preference around C_{23}/C_{25} is indicative of a strong terrestrial origin. This is in agreement with both the high pristane/n- C_{17} and pristane/phytane ratios, 3.3 and 4.9, respectively (Table 8).

Sidewall core 20 (1358m) was also thermally extracted to verify the probable pipe contamination in the cuttings samples and its GC_{therm} profile is similar to those of the three cutting samples, but without the baseline hump, indicating that the contaminant is absent. Also missing is much of the gasoline fraction, which may be attributable to flushing from mud in the well bore.

Solvent extraction was performed on eight sidewall cores primarily to obtain more reliable results and secondly to enable biomarker studies to be performed if later required.

Of the four solvent extracted sidewall cores from the Waarre Formation (1358m, 1362m, 1381m and 1392m) the shallowest three yielded excellent quantities of free hydrocarbons from 10, 700 to 5,600ppm (Table 8), while the deepest sidewall core yielded only a small amount of hydrocarbon (69ppm).

The saturate chromatograms from the top three sidewall cores characterize the same oil which is depleted in n-alkanes below C_{17} with a unimodal distribution centred at approximately C_{23} . (Note: due to having been extracted with solvent these saturate chromatograms will not display the light ends below approximately C_{12} like the thermally extracted chromatograms do). The odd-over-even preference indicates a terrestrial origin, as do the pristane/phytane ratios (4.81-5.39). The pristane/n- C_{17} ratio also indicates a coaly origin, however, this parameter may be unreliable due to the possible depletion of the n- C_{17} . These chromatograms also indicate the possibility of biodegradation. The low yield from the SWC 14 (1392m) probably indicates that there is a negligible quantity of oil present in the lower part of the Waarre Formation Unit A.

TABLE 8

SUMMARY OF EXTRACTION AND CHROMATOGRAPHY

SWC No.	DEPTH (M)	FORMATION	TOTAL EXTRACT (PPM)	PRIS/PHYT	PRIS/n-C17	PHYT/n-C18	MPI-1	VR
20	1358.0	Waarre	10724.0	5.37	2.86	0.37	1.06	1.04
19	1362.0	Waarre	6849.4	5.39	3.02	0.38	Q.	1
16	1381.0	Waarre	5636.4	4.81	1.17	0.15	QN.	ı
14	1392.0	Waarre	69.4	N ON	QN.	Ð	Q.	ı
12	1408.5	Eumeralla	1414.5	5.12	0.37	0.07	1.17	1.10
6	1426.0	Eumeralla	143.3	4.73	0.34	0.07	Q.	1
9	1469.0	Eumeralla	41.2	QN	QN.	QN	S	1
3	1550.5	Eumeralla	31.3	ND	QV	QN.	QN	1
7*	1391.5	Eumeralla	2452.2	2.80	0.53	80.0	ND	

* Iona-I

Of the four sidewall cores from the Eumeralla Formation which were solvent extracted (1408.5m, 1426m, 1469m and 1550.5m) the two shallowest yielded moderate quantities of free hydrocarbons (1414ppm and 143 ppm), while the deepest two yielded negligible amounts of free hydrocarbons (41ppm and 31ppm).

Saturate chromatograms for the 1408.5m and 1426m samples characterize an early to peak mature oil with n-alkanes from at least C_9 to C_{31} . It has a bimodal distribution with maxima at approximately C_{18} and C_{23} , similar to Tuna-4 oil (Burns *et al.*, 1987*) which has an API of 39°. A slight odd-over-even preference not only indicates input from higher plant waxes, but also that the oil is not late mature. The pristane/phytane ratios (5.12 and 4.73) also suggest oxic conditions.

Hydrocarbon yields from the 1461m and 1550.5m sidewall cores indicate that there is neglible oil present in this zone of the Eumeralla Formation. The whole oil chromatograms characterize an oil with only a small proportion of nalkanes.

Biomarker distributions were determined for the branched/cyclic and aromatic fractions for sidewall cores 20 and 12 (1358m and 1408.5m). A detailed interpretation and the mass fragmentograms are included in Appendix 8 and indicate that the degraded (biodegraded?) oil is genetically related to the deeper undegraded oil and that they probably have a common source. The oil was sourced from terrestrial, coaly organic matter. This was indicated by the presence of codalene and retene, a predominance of C_{29} over C_{27} diasteranes and steranes together with the presence of bi-, tri- and tetra-diterpenoids, markers for resinous matter in higher plants.

The methylphenanthrene index (MPI) was measured for both samples for the purposes of calculation of the maturity at which the oil was generated. MPI values of 1.06 and 1.17 indicate vitrinite equivalent values of approximately 1.0 to 1.1% using the Radke and Welte (1983†) method. Although this typically would be considered very late mature, the work of Burns *et. al.* (1987) on Gippsland crudes (also of a coaly origin) would indicate the Iona oil is early to peak mature. Again, this is consistent with the odd-over-even preference, and the n-alkane distribution.

^{*} APEA J., v.27, p.63-72.

[†] see references list Appendix 8

3.4.3 Discussion

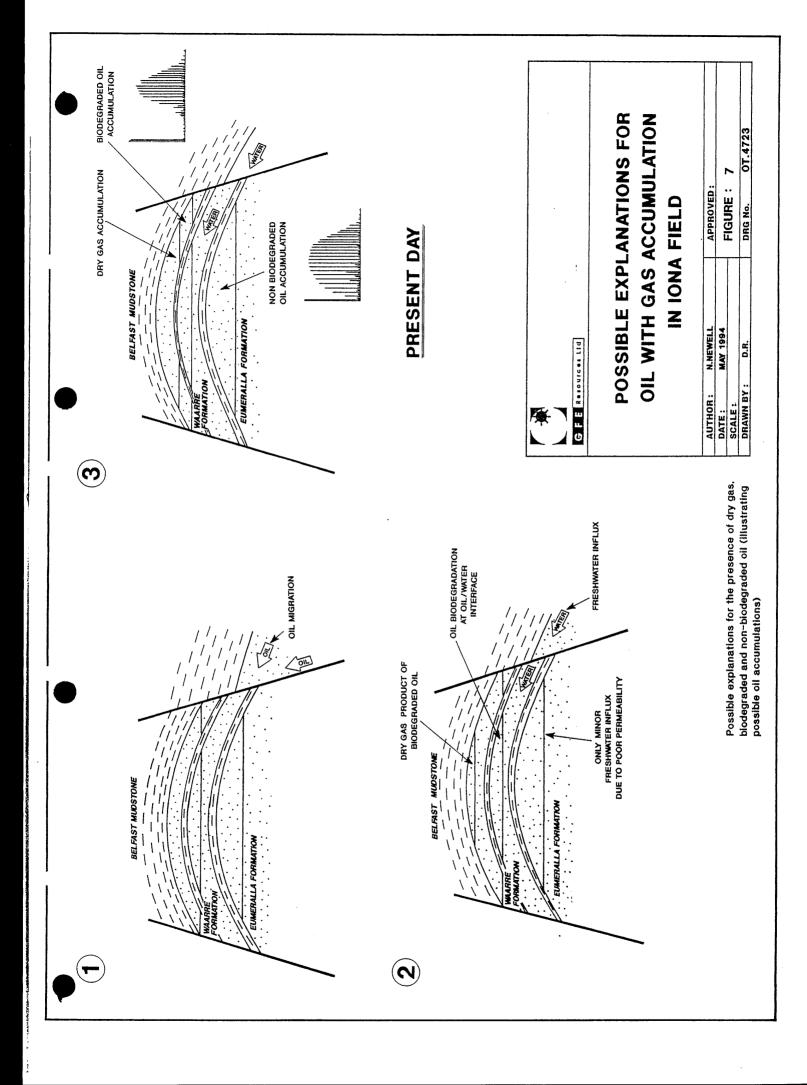
3.4.3.1 Waarre Formation

Extraction of samples from the Waarre Formation in Iona-2 has clearly shown the presence of a degraded oil in at least Units A and B. Similar studies of a sample from Unit C in Iona-1 have also indicated the presence of a degraded oil. (Note: the chromatograms for the Iona-1 samples display neglible hydrocarbons below C₁₇ probably due to poor storage). It is likely that degraded oil is present across the Iona field within the Waarre Formation. The base of this zone occurs approximately midway through Unit A in Iona-2, which is below the lowest known gas.

At least three explanations (Figure 7), or a combination thereof, are possible in relation to the presence and origin of this degraded oil;

- 1. Subsequent to the trap being filled with oil fault reactivation resulted in leakage of most of the oil with a heavy residual component remaining. The structure was then later filled by gas.
- 2. The original oil column was displaced by gas, leaving only a heavy residual component. This scenario does not adequately explain the presence of the degraded oil below the gas water contact.
- 3. The original oil column was biodegraded leaving a relatively dry gas (with C₁ being 85% of total gas or 93% of hydrocarbon gas) and a residual oil. This phenomenon has been proposed for many of the dry gas/biodegraded oil fields on the Northwest Shelf with examples at West Muiron, Wandoo, Roller, Skate, Leatherback and many others.

Whichever is the case, the extent of this degraded oil highlights the oil potential of this region. It also raises the possibility of the presence of a degraded oil column (rather than residual) being present within Unit A. This unit has not been tested in either Iona wells except for RFT pressure measurement in Iona-2. This pressure, if valid, does not conflict with the possibility of oil being present. Gas readings while drilling through this interval show reasonable increases in both C_1 and



C₂. No C₅ was recorded over this interval, however, this could be expected with a degraded oil depleted in short chain alkanes. Fluorescence is also recorded through this interval, consisting of 10-30% bright yellow pinpoint fluorescence with instant blooming cut. The fluorescence was strongest between 1375 to 1385 within Unit A of the Waarre Formation.

3.4.3.2 Eumeralla Formation

Extraction of samples from the Eumeralla Formation in Iona-2 has shown the presence of a whole oil (non-degraded) in the sandstone unit immediately below the unconformity. The deepest of these samples is at 1426m, indicating the possibility of an at least 23m oil column. The fact that the hydrocarbon yields are not high (1414.5ppm and 143.3ppm) may suggest that oil saturation is low.

Biomarker studies indicate that the Eumeralla Formation oil is genetically related to the Waarre Formation oil, while gas chromatograms of both indicate they have had different histories since generation. The most obvious explanation for the difference in physical properties is that the Waarre Formation oil has undergone biodegradation while the Eumeralla Formation oil has not. This can be further explained by the low permeability of the Eumeralla Formation relative to the Waarre Formation and a lack of freshwater influx into the former. The low permeability of the Eumeralla Formation below the unconformity was further indicated by the inability to sample with the RFT.

A sidewall core from Iona-1 from the equivalent Eumeralla Formation section was thermally extracted to ascertain the lateral extent of this non-degraded oil. The GC_{sats} trace of this sample from 1391.3 metres characterizes a degraded oil almost completely lacking in n-alkanes below C_{17} , which is unlike the degraded samples from Iona-2, where residual components below C_{17} are present. However, the lack of components below C_{17} in the Iona-1 sample may be all or partly due to six years of storage at ambient conditions, thus making the validity of the comparison questionable.

The presence of oil in the Eumeralla Formation is also indicated by both fluorescence and the gas chromatogram while drilling. Between 1400 and 1435 metres the sandstone had approximately 2% bright yellow pinpoint fluorescence with a slow streaming cut. Total gas reached 390 units at 1423 metres, with up to 2180ppm of C₃ and 960ppm of C₄. The gas levels in this interval were actually higher than while drilling through the gas zone in the Waarre Formation.

Within Iona-2 two possible oil columns have been identified by geochemical analysis and other supportive drilling data (ie. fluorescence, gas and pressure data). A degraded oil column may present within Unit A of the Waarre Formation between 1372m and 1385m, and a non-degraded oil column may be present within the Eumeralla Formation between 1403m and 1434m.

Due to uncertainty about the Waarre Formation accumulation and the poor permeability of the Eumeralla Formation another well would be difficult to justify to test these zones alone. However, if another well is to be drilled for future gas drainage, the well should be engineered such that these zones can be fully evaluated. These tests might also be considered in either Iona-1 or Iona-2 after the completion of gas production.

3.5 LOG ANALYSIS

Log analysis was performed on the wireline logs using Crocker Data Processing's PETROLOG software. The interval 1160.1 - 1627.9m was subdivided into eight zones covering stratigraphic units from the Nullawarre Greensand to the Eumeralla Formation and each zone was analysed independently with the input parameters and cut-offs as shown in Appendix 6. A three-metre interval at the base of the Waare Formation was excluded from analysis due to anomalous log responses (thought to be due to carbonate bands), and the top 37m of the Eumeralla Formation was treated separately from the remainder due to the better shows observed during drilling.

Only zones 4 and 5 (covering the Waarre Formation Units C and B, respectively) indicated any net pay, and a complete listing of the calculated results for these two zones is given in Appendix 6. An interpretive log spanning all eight zones is provided as Enclosure 11, and summary of results is shown in Table 9.

TABLE 9

IONA-2 LOG ANALYSIS RESULTS SUMMARY

IONA-1	Waarre Unit C	1299.21	28.80	23.0	23.3	0.05	0.50	0.30	20.27	23.87	(19.69)	4.04	4.84	3.87
8	Eumeralla	1438.50 1627.94	189.43	6.9	16.9	0.05	0.50	0.30	0.00	n/a	n/a	n/a	n/a	n/a
7	Eumeralla	1401.47 1438.50	37.03	4.9	10.9	0.05	0.50	0.30	0.00	n/a	n/a	n/a	n/a	n/a
9	Waarre Unit A	1371.91 1398.58	26.67	3.7	23.3	0.05	0.50	0.30	0.00	n/a	n/a	n/a	n/a	n/a
2	Waarre Unit B	1347.98 1371.91	23.93	5.6	22.8	0.05	0.50	0.30	5.03	23.08	17.94	8.81	1.16	96.0
7	Waarre Unit C	1316.43 1347.98	31.55	27.9	23.7	0.05	0.50	0.30	27.58	23.81	16.71	5.29	6.57	5.48
3	Waarre Unit D	1296.92 1316.43	19.51	0.5	18.2	0.05	0.50	0.30	0.00	n/a	n/a	n/a	n/a	n/a
7	Belfast	1260.04 1296.92	36.88	0.0	0.0	0.05	0.50	0.30	0.00	n/a	n/a	n/a	n/a	n/a
-	Nullawarre	1160.07 1260.04	76.99	74.9	23.1	0.05	0.50	0.30	0.00	n/a	n/a	n/a	n/a	n/a
ZONE#	FORMATION Nullawarre	From (m) To (m)	Interval (m)	Net Sand [†] (m)	Sand Average $\emptyset_{\text{eff.}}^{+}$ (%)	Average \varnothing eff. Cut off	S _w Cut off	V _{clay} Cut off	Net Pay (m)	Pay Average $\varnothing_{ m eff.}$ (%)	Pay Average S _w (%)	Pay Average V _{clay} (%)	Integrated \varnothing (m)	$Sum \varnothing^*(1-S_w)(m)$

 $^{^{\}dagger}$ Obtained by doing analysis with $S_{\rm w} = 100\%$ n/a denotes not applicable due to not pay being zero

For comparison, Table 9 also includes results from the Waarre Formation Unit C in Iona-1, which shows that this formation in Iona-2 is almost three metres thicker, has about five metres more net sand and about seven metres more net pay. The average effective porosity for the Unit C pay sand in both wells is almost 24 per cent, which closely compares with the average overburden porosities measured in core plugs from Iona-1.

The pay zones in Units C and B are readily apparent in Enclosure 11, but the significance of the smaller indications of gas shown in the other zones is less certain. During drilling, increases in mud gas were observed in some of the non-pay zones shown in Enclosure 11, as well as some fluorescence in the lower Waarre Formation and the upper Eumeralla Formation. However, it is thought likely that most of the apparent "hydrocarbon" response displayed is an artefact of clay content, mineralogy and inappropriate estimates of some key input parameters (such as R_w).

3.6 PALYNOLOGY

Eighteen sidewall cores and four cuttings samples were submitted for palynological analysis and the resulting report comprises Appendix 6.

The samples ranged from 1034.5 metres (near top Skull Creek Mudstone) down to 1599 metres (Eumeralla Formation) and spanned from basal Campanian to Lake Albian in age.

As in Iona-1, it appears that the A. Distocarinatus zone (and thus the Cenomanian) is not present in Iona-2, its absence comprising part of the mid-Cretaceous unconformity.

Around the base Belfast Mudstone/top Waarre Formation contact the Iona-2 palynological data compliments Iona-1 in that; (i) whereas the *O. Porifera* dinoflagellate zone was not seen in Iona-1 (due to lack of sampling in the basal Belfast Formation?) it is present at this same stratigraphic level in Iona-2, and (ii) conversely, the *C. Striatoconus* zone was observed in the top of Waarre Unit D in Iona-1, but was not observed in Iona-2, either due to insufficient sampling and/or because the uppermost part of Unit D in Iona-1 may be absent in Iona-2.

All of the Sherbrook Group samples are considered to be marine but, in the Waarre Formation, not necessarily the restricted marine units proposed by Buffin (1989*), whilst all Eumeralla Formation samples are attributed to non-marine lacustrine environments.

^{*} Iona-1 Well Completion Report

3.7 STRUCTURE

The Iona structure was first identified by Beach Petroleum NL from the 1981 Curdie Seismic Survey, and subsequently better constrained by the 1986 Sherbrook Seismic Survey. In March, 1988 Iona-1 was drilled and discovered the gas accumulation in the Waarre Formation Unit C. Iona-1 was drilled slightly off structure (at Shot Point 235 on line OB81A-C62) due to surface topography and the structure was originally mapped as a four-way dip closure with only 0.44km² closure at Waarre Formation level. The thickness of the gas column in Iona-1 demonstrated that the bounding faults sealed, providing closure down to about 1195mSS and thereby indicating a larger areal extent of closure (approximately 3km²).

A small amount of additional seismic was obtained over the Iona structure as part of the 1988 Vogel Seismic Survey and a re-interpretation of the feature indicated a rotated fault block bounded to the northeast and southwest by northwest-trending faults.

From this mapping the apex of the structure was interpreted to be about 250 metres east-southeast of Iona-1. The Iona 93-01 seismic line was acquired to confirm the location of this crest and, having done so, the location of Iona-2 updip from Iona-1 was assured.

The formation top depths encountered in Iona-2 were well within the error limits of the prognosed depths (Figure 8), with the biggest discrepancy being the top of the Waarre Formation Unit C coming in 6.8 metres high. Thus, the pre-drill structural interpretation remains unchanged (Figures 9 and 10).

ERA	PERIOD	GROUP		PREDICTED		ACTUAL (TV	
	T	- ₹	5.5		PORT CAMPBELL LIMESTONE		5.7 Difference
		I HEYTESBURY		39.7	GELLIBRAND MARL	Undiffer- entiated	
)SC	}	_¥-		202.7	NARRAWATURK MARL		0.0-1
Ž	₹		A	280.7	MEPUNGA FORMATION	284.5	3.8m Low (+1.4%)
CAINOZOIC	TERTIARY	WANGERRIP	NIRRANDA	335.7	DILWYN FORMATION	336.7	1.0m Low (+0.3%)
		WAN		541.7	PEMBER MUDSTONE	543.1	1.4m Low (+0.3%)
				610.7	PEBBLE POINT FORMATION	611.0	0.3m Low (+0.05%)
		~~~		659.7	PAARATTE FORMATION	660.8	1.1m Low (+0.2%)
MESOZOIC	LATE CRETACEOUS	SHERBROOK		1004.7	SKULL CREEK MUDSTONE	1009.9	5.2m Low (+0.5%)
MESC	LATE	0,		1136.7	NULLAWARRE GREENSAND	1139.6	3.1m Low (+0.3%)
-							2.2m High (-0.2%)
	]			1236.7	BELFAST MUDSTONE	1234.5	1.3m High (-0.1%)
1				1274.7 1299.7	WAARRE FORMATION Unit D	1273.4	6.8m High (-0.5%)
				1233.1	WAARRE FORMATION Units C,B,A,	1292.9	
	EARLY RETACEOUS	OTWAY		1380.7	EUMERALLA FORMATION	1377.9	2.8m High (-0.2%)
L	<u>Г</u> О		. !	TD 1630.7		TVTD 1626.4	

Note: Predicted KB-GL distance was 5.5m.
Actual was 5.7m, so all prognosed tops have 0.2m added to them in this comparision.

GFE RESOURCES LTD PPL2 OTWAY BASIN

IONA-2

PREDICTED vs ACTUAL FORMATION TOPS

OT.4740 FIGURE 8

# TOP WAARRE UNIT C TIME MAP (msTWT) (DATUM 150mSS)

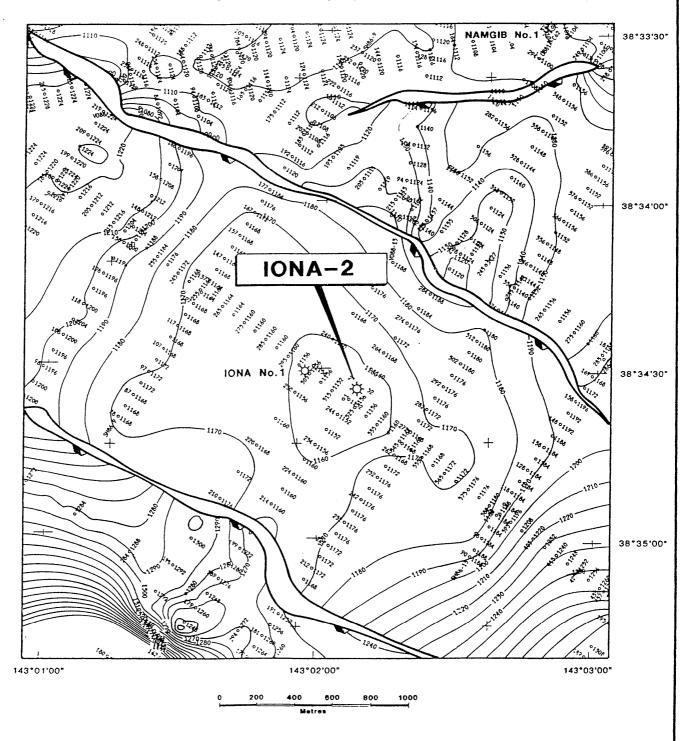
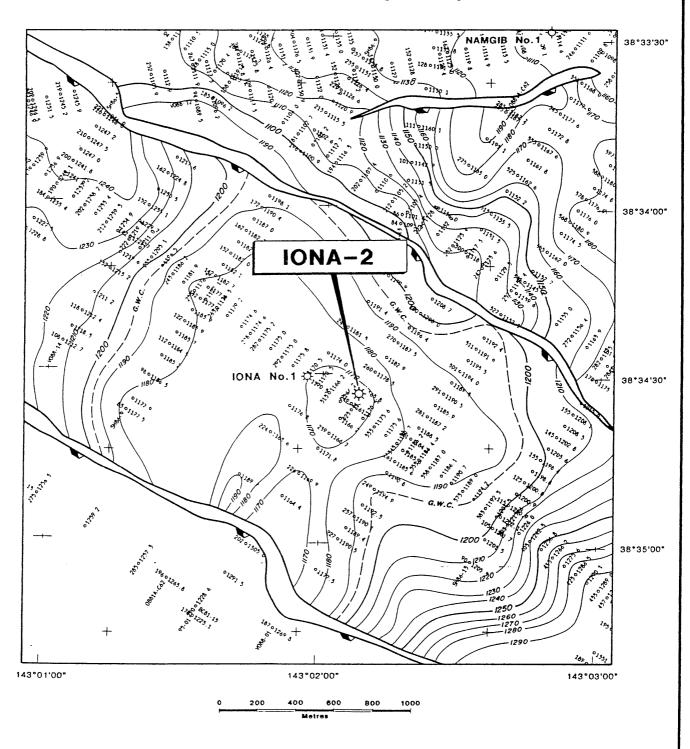


FIGURE 9

OT.4721

# TOP WAARRE UNIT C DEPTH MAP (mSS)



OT.4722

FIGURE 10

# CONCLUSIONS

# 4. CONCLUSIONS

### 4.1 OBJECTIVES VERSUS PERFORMANCE

From an engineering perspective the drilling and completion of Iona-2 fully met the set objectives. As shown on the Drilling Progress Chart (Figure 11), the well was completed in the anticipated time, after having reached the prognosed depth about two days early, but then taking almost that same time longer to be completed.

Also, (as shown in Figure 12) the directional drilling was successful in steering the hole towards the desired subsurface location, with the actual bottom hole location being only 11.3 metres southeast of the proposed location. More importantly, the actual top of the Waarre Formation Unit C primary target was only 5.2 metres southeast of the proposed location.

As outlined in Section 3.7 and Figure 8, the prediction of formation tops was very successful, with all but one horizon coming in  $\leq \pm 0.5\%$  of the prognosis. In terms of metres, the largest discrepancy was the top Waarre Formation Unit C being 6.8 metres high, which was a favourable outcome that contributed to the gas column being larger than expected.

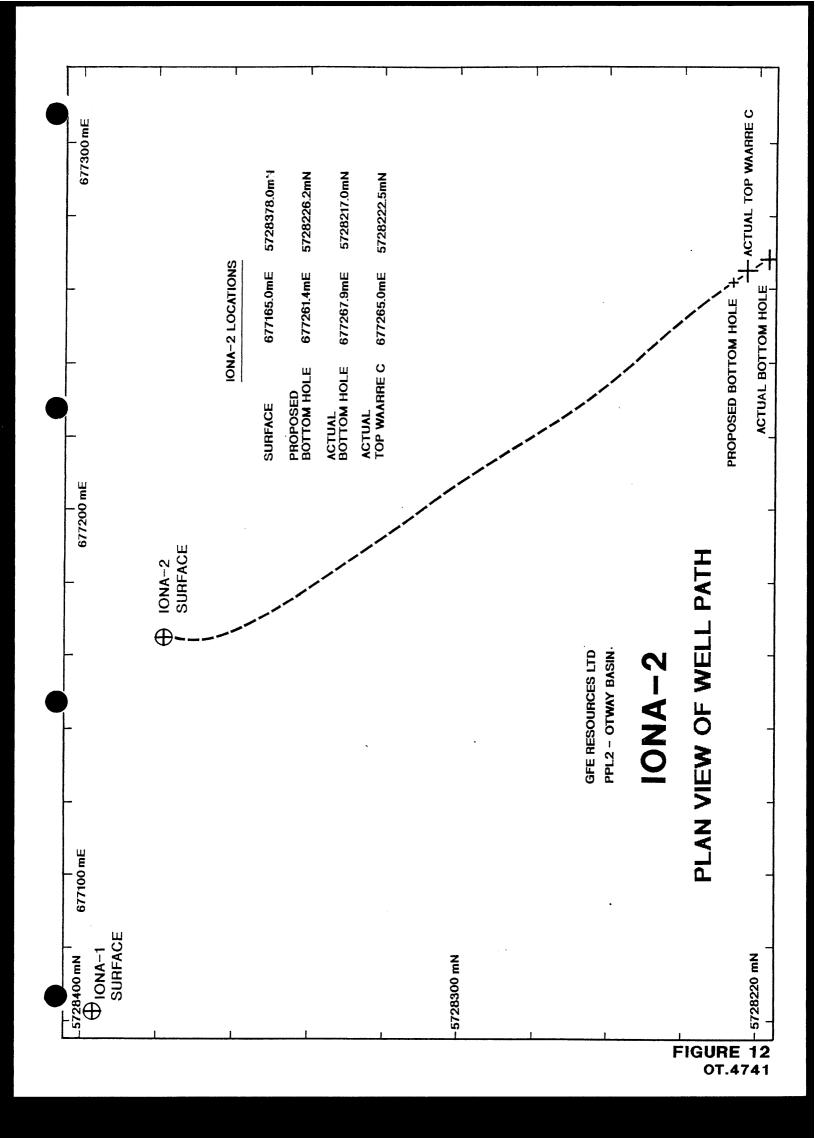
The Waarre Formation Unit C primary reservoir target was not expected to differ greatly from the section drilled in Iona-1 (only 270 metres away). However, there were some significant differences, which provided a more beneficial outcome than had been anticipated;

- (i) Unit C is 2.7 metres thicker in Iona-2; and
- (ii) Unit C contains more clean sand, resulting in 27.6 metres of net pay and an average effective porosity of 23.8% (cf. 20.3 metres and 23.9% in Iona-1).

Also unexpected, logs and RFT pressures indicate that in the Waarre Unit B sand there is an additional (and separate) gas column with 5.0 metres of net pay and an average effective porosity of 23.1%.

Thus, Iona-2 has been found to contain significantly more gas-filled reservoir than was predicted based on Iona-1, and has therefore surpassed its main technical and commercial objectives.

FIGURE 11



One objective which could be regarded as not being completely fulfilled was the investigation of the Eumeralla Formation. Mud gas readings and fluorescence observed in sands at the top of the drilled Eumeralla Formation section were of considerable interest. However, in not wanting to jeopardise the main objective of Iona-2 (to be completed as a Waarre Formation gas producer) no Drill Stem Test (DST) was conducted. Although a DST would have been the most definitive means of evaluating the Eumeralla Formation's prospectivity at this location, the inability to obtain any indication of significant permeability with the RFT (despite eight attempts) and the conclusion from log analysis that the zone was water wet and has generally low effective porosity (also supported by SWC petrography) suggests that a DST may not have been worthwhile. However, if another well is drilled on the Iona structure, a DST should be considered for the Eumeralla Formation.

# 4.2 CONTRIBUTION TO GEOLOGICAL KNOWLEDGE AND HYDROCARBON PROSPECTIVITY

Having been drilled as a development well, there was no great expectation that Iona-2 would significantly alter or add to the knowledge gained from the Iona-1 discovery well. It has instead mainly supported (and provided additional information for) the results from Iona-1.

Some aspects which have gained greater emphasis from Iona-2 are:

- facies variation within the Waarre Formation. While lateral variation in thickness and sand content of units in the Waarre Formation is clearly evident in many wells, it is interesting to note the small but significant differences between the Iona-1 and Iona-2 sections (which are only 270 metres apart), especially the thicker sand in Unit C in Iona-2, which yields a much thicker net pay than Iona-1.
- the gas column in the Unit B sand. This sand is below the Gas/Water Contact and Lowest Known Gas determined in Iona-1, and thus was not expected to contain gas in Iona-2. As well as adding 5.0 metres to the total net pay, it is noteworthy because the RFT data suggests it is not in direct communication with the main pay interval, and therefore is an example of isolated, stacked reservoirs in the Waarre Formation.
- hydrocarbon shows in the Eumeralla Formation. Mud gas and fluorescence were both observed more commonly and at higher levels in Iona-2 than in Iona-1.

Although not fully tested in Iona-2, these shows suggest the Eumeralla Formation in this area is prospective.

- more detailed organic geochemistry. In addition to gas chromatography of extracted hydrocarbons (as was done in Iona-1) one Waarre and one Eumeralla sample were analysed by GC-MS. The results indicated the samples were virtually identical, fully mature oil sourced from terrestrial (coaly) organic matter.
- palynological work suggests that all Sherbrook Group samples are from marine environments, while all Eumeralla Formation samples are from non-marine environments.
- a water sample obtained by RFT from the Waarre Formation Unit B has provided a R_w of 0.34 ohm.m at 25°C, but this is thought to be at least partially diluted with filtrate.

# APPENDIX 1

### **GFE RESOURCES LTD**

# **APPENDIX 1**

# **RIG SPECIFICATIONS**

IONA-2

### **INVENTORY - RIG #11**

CARRIER Cooper LTO 750 Carrier with triple front and rear axles

54000lb front and 70000lb rear. All necessary highway equipment. Unit levelled with hydraulic jacks when

stationery.

SUBSTRUCTURE 17' floor height - 14' below table beams with plates in base.

**DRAWWORKS** Cooper 750 H.P. Drawworks.

42" x 12" main drum with Fawick 28VC 1000 clutch and 3000 metres  $^9/_{16}$ " sandline. Driven by 2 each Cat D3406TA

Diesel Engines.

**ROTARY TABLE** National Rotary Table Model C-175

**DERRICK** Cooper Derrick Model 118-365. Ground height 118'.

Maximum rated static hook load 350000 lbs with 10 lines.

Mast raised, lowered and telescoped hydraulically.

CROWN BLOCK Cooper Crown Block with 4 working sheaves. Fast line

sheave and dead line sheave. All grooved for  $1-\frac{1}{8}$ " line.

Sandline sheave grooved for ⁹/₁₆" line.

**HOOK BLOCK** National Hook Block Model 435 G-175. 175 ton capacity.

4-35" sheaves grooved for  $1-\frac{1}{8}$ " line.

SWIVEL P-200 National.

**KELLY SPINNER** Foster Model K-77

SLUSH PUMPS No. 1:

National 8-P-80 Slush Pump.  $6^{1}/_{4}$ " x  $8^{1}/_{2}$ " Triplex single

acting driven by Cat. D398TA Diesel Engine.

No. 2:

National 7-P-50 Slush Pump driven by Cat D379TA Diesel

Engine.

**PULSATION DAMPENER** 1 each Hydril Pulsation Dampener type K20-3000.

MUD SYSTEM 2 x 300 bbl tanks incorporating 80 bbl pill tank and 40 bbl

trip tank.

SHAKERS Triton NNF Screening Machine (Linear Motion).

**DEGASSER** Drilco Atmosheric Degasser Standard Pit. 7¹/₂ H.P. 60 Hz

230v.

**DESANDER** Demco Model 122. Two, 12" cone with Warman 6" x 4"

Centrifugal pump driven by 50 H.P. Electric Motor.

DESILTER

Pioneer Economaster Model T12-E4. 12 x 4" cones with Warman 6" x 4" Centrifugal pump, driven by a 50 H.P.

Electric Motor.

**MUD MIXING PUMP** 

Warman 6" x 4" Centrifugal pump driven by a 50 H.P.

Electric Motor.

**MUD AGITATORS** 

4 only Brandt Mud Agitator Model MA 7.5.

**B.O.P'S &** 

**ACCUMULATOR** 

10" x 3000 P.S.I. Shaffer Double Gate B.O.P. with  $2^{3}/_{8}$ ",

 $2^{7}/_{8}$ ",  $3^{1}/_{2}$ ",  $4^{1}/_{2}$ ",  $5^{1}/_{2}$ ", 7" and Blind.

10" x 3000 P.S.I. Hydril GK Annular B.O.P. Koomey B.O.P. Control Unit. Accumulator Unit Model 100-11S.

**CHOKE MANIFOLD** 

Cameron 5000 psi.

**SPOOL** 

10" x 3000 x 10" x 3000 Flanged Drilling Spool with 3" x 3000 flanged choke and kill outlets.

**INSTRUMENTATION** 

Martin-Decker 6 pen Rcord-O-Graph

Martin-Decker Weight Indicator Type F.S.

Martin-Decker Mud Pressure Gauge Martin-Decker Rotary R.P.M. Indicator Martin-Decker Stroke Indicator (2 off) Martin-Decker Rota Torque Indicator Martin-Decker Tong Torque Indicator Martin-Decker Mud Flow Sensor

Martin-Decker Mud Flow Fill System

Martin-Decker Mud Volume Totaliser (M.V.T.)

**AUTOMATIC DRILLER** 

Satellite Automatic Driller Model SA100-50-1500.

WIRELINE STRIPPER

Guiberson Oil Saver Type H-4.

**SURVEY UNIT** 

Totco 8 Deg Recorder.

**MUD LAB** 

Baroid Rig Laboratory Model 821.

**KELLY** 

 $5^{1}/_{4}$ " HEX Kelly.  $2^{13}/_{16}$ " I.D. x 40' long with  $6^{5}/_{8}$ " API Reg.

L.H. Box up 4" I.F. Pin down.

**UPPER KELLY VALVE** 

Upper Kelly Cock. 10000 test 6⁵/₈" API Reg. L.H.

Connections.

LOWER KELLY VALVE

Hydril Kelly Guard.  $4^{1}/_{4}$ " - 10000 P.S.I. 4" I.F. Pin and Box.

KELLY DRIVE BUSHING

Varco Type 4 KRS Kelly Drive Bushing.

DRILL PIPE

7000' Drill Pipe  $4^1/2''$  O.D. 16.60 lb. Grade E Range 2 with

4" I.F. x 18 degree taper tool joints.

DRILL COLLARS

20 each Drill Collars 6¹/₄" O.D. slick 2¹³/₁₆" I.D. x 30' long

with  $4^{1}/_{2}$ " XH pin and box connections.

**FISHING TOOLS** 

To suit pipe, collars and tubing.

**SUBSTITUTES** 

To suit drill string.

**HANDLING TOOLS** 

Farr Hydraulic Power Tongs, 13³/₈" Varco SSW-10

spinning wrench.

Manual tongs, elevators and slips to handle pipe, collars,

casing and tubing.

WELDING EQUIPMENT

Lincoln Electric Welder Model 400AS.

AIR COMPRESSORS

Sullair compressor Package Model 10-30.

**AC GENERATOR** 

2 each Caterpillar 3408TA AC Generator model SR-4. 1800

rpm 60 hz 275 kw.

**FUEL TANKS** 

2 each 10,000 litre - Skid Mounted.

WATER TANK

400 bbl tank with two Warman 3 x 2 pumps driven by 24 hp

electric motors

PIPE RACKS

5 sets 30" in length

**CATWALKS** 

2 piece Catwalk drill pipe construction 42" height.

**RADIO** 

Codan Mobile Transceiver.

TRANSPORTATION

International 530 Payloader.

Toyota 4 x 4 Pickup.

Toyota 4 x 4 Crew Vehicle.

**RIG ACCOMMODATION** 

2 Skid Mounted Toolpusher/Company Man Units.

### **CAMP**

1- Camp Generator House 31' long x 10' wide skid mounted complete with 2 -3304 T 80 Kw, 50 Hz, 200 - 400 volt generators, camp distribution panel. 6,794 litres fuel storage, 12,000 litres fresh water storage and 24,000 litres shower water storage.

1 Kitchen/Dining Room	40' x 10' x 10'
1 Recreation Room	40' x 10' x 10'
1 Ablution/Laundry	40' x 10' x 10'
3 12 Man Bunkhouses	40' x 10' x 10'
1 Cooler/Freezer	20' x 8' x 8'

# APPENDIX 2

### **GFE RESOURCES LTD**

# **APPENDIX 2**

# DRILLING FLUID RECAP

IONA-2

G.F.E. RESOURCES LTD DRILLING FLUID RECAP IONA-2 PPL 2, OTWAY BASIN VICTORIA



Prepared by

Date

A. Searle / M. Olejniczak

March 1994

"All information, recommendations and suggestions herein concerning our products are based on tests and data believed to be reliable. However, it is the user's responsibility to determine the safety, toxicity and suitability for their own use of the products described herein."

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#### **WELL SUMMARY**

G.F.E. Resources Ltd Operator

lona-2 Well Name

Deviated to 19°, then dropped to vertical Average Angle

PPL 2, Otway Basin, Victoria Location

Century Drilling Contractor

Rig 11 Rig

13 Febuary 1994 Rig On Location

14 Febuary 1994 Start Date

5.2 m **RKB Elevation** 

1650 m MD Total Depth

24 Febuary 1994 Date Reached T.D

11 Days Total Days Drilling

5 March 1994 Rig Release

21 Days Total Days On Well

Drilling Fluid Type	Interval	Hole Size	,	Cost (A\$)
AQUAGEL/CMC AQUAGEL/CMC to KCL/Polymer	16 - 640 m 640 - 1650 m	12- 1/4" 8-1/2"	\$ \$	2,992.18 22,369.17
Mud Materials Charged To Drilling	тот	AL	\$	25,361.35
Engineer On Location From : Drilling Fluid Engineering :	14/2/94 To 3/3/94 18 Days @ \$ 530/Da	ау	\$	9,540.00
Total Cost Of Drilling Materials & E	ngineering		\$	34,901.35
Mud Materials Not Charged To Dril	ling		\$	5,171.40

16 m 20 " Conductor @ **Casing Program** 631.1 m 9-5/8"

1443.5 m 7" Production

Ken Smith **Drilling Supervisors** 

Alan Searle, Manfred Olejniczak **Baroid Mud Engineers** 

#### INTRODUCTION

lona-2 was spudded in on 14 Febuary using Century rig 11, drilling 12 -1/4" hole out of the surface conductor set at 16 m.

Water was used initially, with 1% KCI added at 125 m to inhibit dispersion through the Gellibrand Marl and reduce water consumption. From 320 m the system was converted to an AQUAGEL/CMC mud to provide hole stability through the sands of the Dilwyn Formation. The hole was also deviated from the vertical to a maximum of 19 degrees from this point. After reaching 640 m the 9-5/8" casing was run and cemented to 631.1 m.

This same AQUAGEL/CMC system was then continued in the 8-1/2" hole through the sands of the Paraate Formation down to 1000 m. The hole angle was allowed to gradually drop back towards the vertical from about 800 m reaching 8 degrees by 1000 m and 0.75 degrees by TD.

From 1000 m the mud was converted to a 3%KCI/CMC/DEXTRID system to provide increased inhibition and improved log separation through the lower part of the Sherbrook Group and into the Eumeralla Formation.

After reaching the 1650 m TD on 24 Febuary, the hole was successfully logged and completed with a 7" production string set at 1443.5 m.

The final cost of \$25,361.35 for materials used for drilling, (not including cementing and completion) was 18% higher than programmed. The additional costs came from a higher polymer consumption than estimated in the 12-1/4" section. The actual dilution rates were close to that estimated.

#### DISCUSSION BY INTERVAL

12 1/4" Hole

16 m to 640 m

(624 m drilled - 4 Days)

Port Campbell Limestone to Pebble Point Formations

Mud System

Native Clay converting to AQUAGEL/CMC from 320 m

#### 1. DRILLING FLUID

lona-2 was spudded using water, with native clays relied upon to provide viscosity while drilling ahead. The clays of the Gellibrand Marl formation were expected to be highly dispersive, requiring heavy dilution to control solids build up and viscosity increase. In fact, cuttings remained relatively firm and discrete down to 125 m.

Despite a low funnel viscosity of 30 secs/qt, and a yield point of 8 lb/100 ft², there was sufficient carrying capacity to lift cuttings in excess of 2" diameter and good hole cleaning was achieved. It was considered unnecessary to add Lime to flocculate the system, other than for one sack used just after drilling into the Gellibrand Marl.

As the depth increased, the marl cuttings became softer. At 125 m 1% KCl (by weight) was added to the system to minimise dispersion and reduce dilution requirements. This also flocculated the mud system, resulting in a funnel viscosity in the range of 40 secs/qt with a PV/YP ratio of 4/39. As drilling continued the KCl content was allowed to deplete to 0.4% by the time casing point was reached.

At the 320 m kick-off point a trip was made to pick up the directional drilling assembly. AQUAGEL/CMC-EHV premix was added to the system gradually reducing the filtrate through the sands of the Dilwyn Formation to 11.8 ml/30 mins by casing point. The addition of the CMC-EHV also deflocculated the system, reducing the Yield Point to the 10-14 lb/100 ft², and the funnel viscosity to 38 to 43 secs/qt.

Dilution was generally required for volume maintenance only. Solids build up resulted in the mud weight increasing to 9.0 ppg, where it stabilised while drilling the sands. While making wiper trips and reaming prior to running casing, the mud weight increased to a maximum of 9.3 ppg. No downhole losses were recorded at any time.

#### 2. TYPICAL PROPERTIES

Depth	:	216	640	m
Mud weight	:	8.85	9.0	ppg
Viscosity	:	31	43	secs/qt
Plastic Viscosity	:	4	9	cPs
Yield point	:	39	12	lbs/100 ft ²
API Filtrate	:	N.C.	11.8	ml/30 min
Solids	:	3.5	4.3	%
M.B.C.	:	13	15	ppb equiv.
Chlorides	:	5400	740	mg/L
KCI	:	1.0	0.4	% wt soln

#### 3. HOLE CONDITIONS

No hole problems were experienced down to 125 m. Hole cleaning was good and cuttings load in the annulus was not a problem. From 125 to 151m, in the Gellibrand Marl, three singles were drilled particularly quickly. This resulted in the annulus becoming overloaded with clay solids. The flowline became blocked and a mud ring had to be circulated out, resulting in lost time. When drilling resumed the weight on bit was reduced to control the drilling rate and no further problems were encountered with the clays.

At 320 m a trip was made to pick up a directional drilling assembly. The trip out was trouble free, however, when running back in a bridge was reamed from 293 to 305 m. Drilling continued using the downhole motor without rotating pipe, while building and then maintaining hole angle at 18.5°.

At the 640 m casing point the hole was circulated clean, and a wiper run to surface. The hole was tight at 475 m and it was necessary to pump out one single. Continued pulling all the way out of the hole, with tight hole experienced over the interval 456 - 379 m.

The directional tools were laid out before running back in. The bit would not pass through the kick-off point at 320 m and tight hole had to be reamed from 320 - 351 m (Dilwyn Formation). Further tight sections were reamed from 408 -529 m (Dilwyn) and 609 -640 m (Pebble Point). There was only 3 m of fill on bottom.

After circulating out another wiper trip was made. This time only minimal drag was recorded, with 2 m of fill on bottom. The hole was again circulated and conditioned before pulling out to run casing.

The 9 5/8" casing was then run and cemented to 631.12 m, without problems. A 644 sx 2% bentonite lead slurry and a 162 sx 0.15% HR4 tail slurry were used. The cement was displaced with 159 bbls of water. Good cement returns were observed at surface.

#### 4. SOLIDS CONTROL

The Triton shale shaker was run throughout the interval with 50 mesh screens. Heavy cuttings loads, particularly through the Dilwyn, dictated this screen mesh size. Fitting finer screens would have resulted in mud losses over the shaker.

Both the desander and desilter were run continuously while drilling. The sand content in the suction was successfully controlled to less than 0.25% while drilling, increasing to 1% while reaming tight hole at TD.

The addition of 1% KCl at 125 m reduced clay dispersion, so that the cuttings remained quite firm and discrete and were easily removed by the solids control equipment.

The sands of the Dilwyn Formation were coarse and, again, solids equipment was able to remove these without difficulty. Dilution was required for volume maintenance rather than solids control.

#### 5. CONCLUSIONS AND RECOMMENDATIONS

- Very high penetration rates can be achieved through the Gellibrand Marl. However, the time lost cleaning out mud rings and flowline blockages tends to negate any advantage gained. Controlled drilling of the Gellibrand Marl prevents the occurrence of these problems and minimises any risk of packing off the hole.
- The one-off addition of 1% KCl by weight assisted in maintaining firm discrete cuttings through the Gellibrand Marl. Dilution requirements were reduced, with mud weight and solids content easier to control. This practice is recommended for future wells.
- The tight hole problems wiper tripping were most likely due to key-seating over the angle building interval.
- The mud used in this interval produced a reasonable quality hole at minimal cost. It is recommended if drilling other wells in the area.

to drilling into the Waare formation. This mud weight was then maintained to TD.

#### 2. TYPICAL PROPERTIES

		GEL/CMC	KCI/Polymer	
Mud weight	:	8.8	8-9 to 9.4	ppg
Viscosity	:	35 to 38	37 to 42	sec/qt
Plastic Vis	:	5 to 6	11 to 15	cP
Yield point	:	9 to10	8 to 12	lb/100 ft ²
API Filtrate	:	25 to14	6.8 to 6.2	ml/30 min
Solids	:	3.4	3.6 to 6.2	% Vol
M.B.C.	:	11to 8	10 to 15	ppb equiv.
pH	:	11 to 9	9.0 to 10	
Chlorides	:	1200	13,500 to 16,200	mg/l
KCI	•		2.7 to 3.1	% wt soln

#### 2. HOLE CONDITIONS

After drilling out from casing, 5 m of new hole was drilled and a leak-off test performed, giving an equivalent mud weight of 10.1 ppg.

A conventional drilling assembly had been used to drill out from casing, however, this would not drop angle as required while drilling ahead. At 781m a trip was made to pick up the downhole motor and MWD to achieve better directional control.

Drilled through the Paaratte and into the Skull Creek Mudstone with no hole problems. At 1052 m, while making a connection at 1039 m, the drill collars became differentially stuck above the jars. Initial attempts to work the pipe free were unsuccessful, including spotting 40 bbl of water above the jars. To further reduce hydrostatic pressure the entire annulus was displaced to water and the pipe came free. After displacing back to mud the hole was circulated before pulling out to lay out the directional tools.

While running back in with a new assembly, a bridge was encountered at 1034 m. While reaming the interval 1024 - 1043 m the kelly hose blew out and it was necessary to pull back to the casing shoe for repairs. The bit was then run back in with no problems other than 8 m of fill on bottom.

Drilling continued with the mud weight allowed to increase naturally in preparation for drilling the Waare Formation. While taking a survey at 1162 m, in the Nullawaare Greensand, the pipe became differentially stuck again, but was pulled free with 137,000 lbs overpull. The mud weight at this time was 9.1 ppg.

Hole conditions were good for the remainder of the well, with the mud weight increased to the 9.3 to 9.4 ppg range. Trips run at 1286 m and at the 1650 m TD encountered only slight tight hole coming out and no problems going back to bottom. Schlumberger logs and RFT's were run without significant problems. The 7" production casing was run without problems but

became differentially stuck while reciprocating at its setting depth, indicating differential sticking was still a problem.

#### 3. SOLIDS CONTROL

Initially the shaker was fitted with 3x110 mesh screens. As sand blinding occurred through the Paaratte, the screens were changed to 2x110,1x50 and later to 110,84,50 mesh. This combination eliminated mud losses from the shakers and was retained for the remainder of the 8 1/2" interval.

The desander and desilter were run while drilling down to approximately 1150 m. The desilter was then shut off to allow the drill solids content to increase, raising the mud weight to 9.3+ ppg prior to the top of the Waare Formation.

After a trip at 1268 m, the mud weight rose to 9.4 ppg. The desilter was then run intermittently through the Waare, to maintain the mud weight at 9.3+ to 9.4 ppg. After drilling into the Eumeralla the mud weight began to increase and it became necessary to run the desilter continuously. The dilution rate was also increased to control the mud weight at 9.3 to 9.4 ppg.

#### 4. CONCLUSIONS AND RECOMMENDATIONS

The mud program recommended that AQUAGEL and CMC-EHV be added in a 15:1 ratio through the Paraate Formation. These two products work together well at this ratio to provide good viscosity and yield point with moderate filtration control. During the drilling of this section insufficient AQUAGEL was actually added. This resulted in the viscosity and yield point being a little less than programmed through the Paraate Formation. This may have been a contributing factor in the calliper log through this section being slightly worse than on the lona-1 well. The need to maintain the AQUAGEL content will need to be stressed more for the next well.

The drill pipe was differentially stuck at 1039 m, again temporarily stuck at 1181 m, and the 7" production casing also became stuck just prior to cementing. This showed that the hole was prone to differential sticking, most likely in the Paraate formation. Possible means of reducing this tendency would be to:

(i) Ensure a higher AQUAGEL content is maintained while drilling through the Paraate to provide better wall sealing.

(ii) Consider adding BARACARB 110 and BARACARB 35 (Crushed Limestone) as additional plugging agents through the Paraate.

As mentioned above the large increase in viscosity and filtration that occurred when KCI additions began at 1000 m, may have been a factor in the pipe becoming differentially stuck at 1039 m. Extra care needs to be taken by the engineer to reduce the mud clay content and begin adding polymers to act as deflocullants before beginning the KCI additions. The KCI additions also need to start slowly so that the effects on the system are minimised. This approach will most likely result in a lower

viscosity for some time, but this is preferable to an excessively flocculated system.

- During logging at TD the mud began to show some signs of bacterial degradation with a significant smell, a slowly worsening API Filtrate, and reducing viscosity. The DEXTRID used for filtration control is prone to bacterial attack. One can of BARACIDE bactericide was added at TD, but this was probably too late. I would recommend that BARACIDE additions begin as soon as DEXTRID is added.
- Mud costs for the interval were about 18% higher than programmed. The estimate may actually have been just a little too low for the interval, but programs are meant to give the engineer a target to aim for.

Completion

7" Production String to 1443.5 m (4 Days)

9.1 ppg NaCl Inhibited Brine

After Schlumberger logging was successfully completed a 60 sx cement plug was set at 1520 m. The top of the cement was tagged at 1471 m, and the 7" production string then run and cemented to 1443.5 m. Mud was used to displace the cement.

The mud tanks were then all dumped and cleaned. 320 bbls of 9.1 ppg NaCl brine inhibited with BARACOR-100 was mixed up for the completion fluid. In addition 40 bbls of high viscosity, low solids fluid was mixed in the pill tank using two sxs of XCD Polymer, for use as sweeps.

The casing was displaced to the 9.1 ppg inhibited brine after the first casing scraper run. Water was initially pumped to displace the mud until clean returns were observed at the shakers. A 15 bbl high viscosity sweep was then pumped chased with the completion brine, with the returning sweep dumped at surface.

After perforating the casing, a second casing scraper was run with a second 15 bbl high viscosity sweep pumped and dumped when returned to surface. At this stage the mud engineer was released. The rest of the completion was then run without any further circulation. As the formation was taking about 1 bbl/hr through the perforations, additional 9.1 ppg NaCl brine was mixed by the rig crew following instructions left behind by the Baroid engineer to maintain the casing volume.

**APPENDIX 1.** 

## FORMATION TOPS (From Schlumberger Logs)

FORMATION	DEPTH m	PROGNOSED DEPTH m
Paaratte	672	659.5
Skull Creek Mudstone	1032	1004.5
Nullawaare Greensand	1163	1136.5
Belfast Mudstone	1258	1236.5
Waare Sandstone	1297	1274.5
Eumeralla	1400	1380.5
T.D.	1650	1625

#### APPENDIX 2.

### 8-1/2" HOLE CALLIPER DATA (Averaged every 25 m)

### IONA-2 COMPARED WITH IONA-1

	IONA-2	IONA-1 HOLE SIZE ins
DEPTH	HOLE SIZE ins	8-3/4
650	9-1/4 10-1/2	8-3/4
675	10-1/2	8-1/2
700	10-1/4	8-1/2
725 750	12	8-1/2
730 775	15	8-1/2
800	11	8-1/2
825	9-1/4	8-1/2
850	9-1/4	8-1/2
875	9-1/4	8-1/2
900	9-1/4	8-1/2
925	8-3/4	8-1/2
950	8-1/2	8-1/2
975	8-1/2	8-1/2
1000	8-3/4	8-1/2
1025	8-3/4	8-1/2
1050	8-1/2	8-1/2
1075	8-3/4	8-1/2
1100	9	8-1/2
1125	9-3/4	8-3/4
1150	9-1/2	8-1/2
1175	9-1/4	8-1/2 8-1/2
1200	8-3/4	9
1225	9-1/4	9 10
1250	9-1/2	8-1/2
1275	9-3/4	8-3/4
1300	9 8-1/2	8-1/2
1325	8-1/2 8-1/2	8-1/2
1350	8-1/2	8-1/2
1375	8-1/2	8-1/2
1400 1425	8-1/2	8-1/2
1450	9	8-1/2
1475	9	8-3/4
1500	8-3/4	
1525	8-3/4	
1575	8-1/2	
1600	8-1/2	
1625	8-3/4	
1650	8-1/2	



#### Baroid Australia Pty Ltd COMPANY G.F.E. RESOURCES LTD.

DAILY ACTIVITY SUMMARY

WELL IONA - 2

LOCATION OTWAY BASIN, VICTORIA CONT/RIG CENTURY DRILLING / RIG - 11 PAGE-1

#### 1994 ACTIVITY

- 14 Feb Complete rigging up. Rig inspection by Mines Dept. Spud in at 12:00 hours. Drilled 12 1/4" hole from 16 - 232m, taking surveys approx every 35m. High ROP through Gelibrand Marl caused annulus to load up with cuttings, resulted in mud rings and blocked flowline at 151m; circulated hole clean, reduced weight on bit to lower ROP from
- Drilled to kick off point at 320m, taking surveys every 35m. Circulated bottoms up. 15 – Feb POOH. Changed bit and made up kick – off assembly with downhole motor and MWD tool; 1.15 deg bent angle in motor. RIH, hit bridge at 293m. Reamed to 305m, ran to bottom. Criculated and oriented motor. Drilled to 500m building angle; no rotation.
- 16—Feb Drilled 12 1/4" hole from 500 —640m, buiilding angle and then maint— aining at 18.5 deg. Reached casing point at 640m, circulated bottoms up. POOH, tight spot at 475m, pick up kelly and pumped out 1 single. Continued pulling out with tight hole from 456 - 379m. Service down— hole assembly, laid out directional tools. Made up BHA for clean out trip. RIH, unable to get through kickoff point. Reamed from 320 - 351, 408 - 524 and 609 -640m; recorded 3m of fill. Circulate hole clean.
- Wiper trip to top of 8" drill collars; slight drag, 2m of fill, washed 2m to bottom. Circulated 17 – Feb hole clean. POOH, cut drill line, laid out 8" drill collars, stabilisers and directional tools. Rigged up and ran 9 5/8" casing. Rigged up Howco surface equipment. Circulated casing. Cemented 9 5/8" casing; 10 bbls water, 644 sx 2% gel lead slurry, 162 sx 0.15% HR4 tail slurry. Released plug and displaced with 159 bbls water. Wait on cement.
- Wait on cement. Install Braden head and nipple up BOP's. Pressure test BOP's with 18 – Feb HOWCO. Made up bit and BHA, RIH to drill out.
- Continue RIH, tagged cement at 623.8m. Pressure test kelly cocks, stabbing valve and 19 – Feb flare line. Drilled float and shoe, made 5m of new hole. Circulate to condition mud and clean hole. Ran F.I.T. Circulated, repeat F.I.T. Drilled 8 1/2" hole from 645 - 781 m, taking single shot surveys every 38m. Building angle, circulated hole clean. POOH, no tight hole recorded. Pick up downhole motor and MWD. RIH, no fill. Orientated motor and then drilled 8 1/2" hole from 781 - 823m.
- Drilled 8 1/2" directional hole from 823 1052m, surveys run with MWD tool. Became 20 – Feb differentially stuck while making connection at 1039m; collars stuck above jars. Worked stuck pipe, spotted 40 bbls water above jars, unsuccessfully. Displaced annulus to water to reduce hydrostatic, pulled free. Displaced hole back to mud while working pipe. POOH, laid out downhole motor and MWD. Made up new BHA and RIH.
- 21—Feb Continued RIH. Hit bridge at 1034m, ream/wash 1024 1043m, one jet partially blocked. Blew kelly hose while reaming. POOH to casing shoe. Replaced kelly hose. RIH, washed 8m to bottom, no fill. Drilled 8 1/2" hole from 1080 - 1133m; survey at 1096m.
- 22 Feb Drilled 8 1/2" hole from 1133 1181m. Circulate and survey at 1165m. Pipe became stuck while taking survey. Worked differentially stuck pipe, pulling 137000 lbs over, before rotating free. Worked pipe and circulated hole clean. Continued drilling from 1165 — 1268m. Circ- ulated bottoms up. Short trip from 1268 - 900m, no fill. Circulated bottoms up. Survey, pump pill and circulate. Survey again. POOH.
- 23 Feb POOH for bit and BHA change. Laid out 6 x 6 1/4" drill collars. Made up new BHA. RIH to 1245m, wash/ream to 1268m, no fill. Drilled 8 1/2" hole from 1268 — 1404m. Survey at 1345 m.

#### Baroid Australia Pty Ltd COMPANY G.F.E. RESOURCES LTD.

DAILY ACTIVITY SUMMARY

PAGE-2

WELL IONA - 2
LOCATION OTWAY BASIN, VICTORIA
CONT/RIG CENTURY DRILLING / RIG - 11

#### 1994 ACTIVITY

- 24 Feb Drilled to 1650 m TD. Circulated bottoms up. Began running wiper trip back to casing shoe.
- 25 Feb Continued wiper trip. Hole only slightly tight coming out at 1050 m. Ran back to bottom, precautionary washing and reaming last 5 m. Circulated out, pumped slug and strapped out with multi-shot survey. Ran Schlumberger logs.
- 26 Feb Continued logging. Rigged down Schlumberger. RIH with BHA. Slipped line at shoe.

  Continued RIH. Precautionary washed and reamed last 21 m to bottom. Circulated and conditioned mud for 2 hrs. POH and continued logging with Schlumbereger.
- 27 Feb Completed Logging. Rigged down Schlumberger. Ran BOP test. RIH open ended to 1520 m and set 60 sx cement plug. Pulled back 5 stands and flushed pipe. POH, picked up bit and BHA. RIH and tagged cement plug at 1471 m. Pulled back to 1457 m and began circulating hole clean.
- 28 Feb Continued circulating hole clean till 01:00 hrs. POH, laying out pipe. Rigged up and ran 7" production casing to 1449 m. Rigged up cement head and began circulating casing.
- 01 Mar Cemented 7" casing displacing with mud. After waiting on cement, lifted BOP off and cut casing. Replaced BOP and pressure tested. Unable to test seal assembly. Lifted BOP and removed "B" section. Wait on casing spear to reset casing slips.
- 02—Mar Ran casing scraper. Displaced mud from casing with water. Pumped 15 bbl hi-vis XCD Polymer sweep. Displaced hole to inhibited 9.1 ppg NaCl brine.
- 03 Mar POH with casing scraper. Rigged up Schlumberger. Ran cement bond log. Perforated casing. Rigged down Schlumberger. Ran in casing scraper, Pumped 15 bbl hi vis sweep and circulated casing clean with brine.

04 – Mar

# RECAP TABLES

MATERIAL RECAP

Page 1.

COMPANY G.F.E. RESOURCES LTD.
WELL IONA - 2
LOCATION OTWAY BASIN, VICTORIA

BAROID

HOLE SIZE 12 1/4"

CONTRACTOR/RIG CENTURY DRILLING / RIG - 11

MUD TYPE AQUAGEL/CMC

A\$748.05 COST/DAY **DRILLING DAYS** 640 INTERVAL TO (m) A\$4.80 COST/m 16 **ROTATING HRS** 16 FROM (m) COST/bbl A\$2.45 DRILLED (m) 624 1.96 CONSUMPTION FACTOR (bbl/m) 17-Feb-94 DATE

MATERIAL	UNIT SIZE	UNIT	QUAN EST	ACT	CONC	(lb/bbl) ACT	TOTAL C ESTIMATE	OSTS ACTUAL
AOUACEL av	25 kg	14.33	226	52	9.8	2.3	3,238.58	745.16
AQUAGEL,sx Caustic Soda	25 kg 25 kg	32.43	11	10	0.5	0.5	356.73	324.30
CMC-EHV	25 kg	106.61	14	12	0.6	0.5	1,492.54	1,279.32
KCL,Tech(sx)	25 kg	14.44		10		0.5		144.40
KCL, Tech(sx)	50 kg	28.88		17		1.5		490.96
Lime	25 kg	8.04	7	1	0.3	0.0	56.28	8.04

 VOLUMES
 COST LESS BARITE : A\$5,144.13 A\$2,992.18

 Sea W.
 bbl

 1250
 1213

Sea W. 1250 Drill W. bbl other bbl bbl other 9 bbl 16.9 Chemical bbl Salvaged Mud 1222 1267 TOTAL MUD USED bbl

COMMENTS

Commenced drilling from 16m with water, relying on native clay from Gellibrand Marl to build viscosity.

Lime was added as required to flocculate the system and increase viscosity. At approximately 125m,

KCI was addded to give 1% by weight and improve cuttings quality, this was allowed to deplete as drilling progressed.

Premix additions were commenced from 320m and the mud system converted to AQUAGEL/CMC-EHV while building angle

The actual mud cost was approximately 60% of that programmed, due to lower dilution requirements and a significantly

lower AQUAGEL useage.

MATERIAL RECAP

Page 2.

COMPANY G.F.E. RESOURCES LTD. WELL IONA - 2 LOCATION OTWAY BASIN, VICTORIA

HOLE SIZE 8 1/2" CONTRACTOR/RIG CENTURY DRILLING / RIG - 11 MUD TYPE AQUAGEL/CMC to 3% KCI/Polymer

A\$2,033.56 COST/DAY 11 **DRILLING DAYS** 1650 INTERVAL TO (m) A\$22.15 COST/m 82 **ROTATING HRS** 640 FROM (m) COST/bbl A\$10.51 DRILLED (m) 1010 2.11 CONSUMPTION FACTOR (bbl/m) 28-Feb-94 DATE

		UNIT	OHAI	VIIIY	CONC	(lb/bbl)	TOTAL	COSTS
MATERIAL	UNIT SIZE	COST	EST.	ACT	EST	ACT	ESTIMATE	ACTUAL
B - 11	50 kg	15.96		36		1.9		574.56
Barite,sx	25 kg	7.98	248	82	5.9	2.1	1,979.04	654.36
Barite,sx	_	14.33	142	232	3.4	6.0	2,034.86	3,324.56
AQUAGEL.sx	25 kg	549.92	1-12-	1	0.0	0.0	549.92	549.92
BARACIDE	25 kg		18	21	0.4	0.5	583.74	681.03
Caustic Soda	25 kg	32.43			0.9	1.5	3.731.35	6,289,99
CMC-EHV	25 kg	106.61	35	59			4.251.48	4,790,40
DEXTRID LT	50 lb	59.88	71	80	1.5	1.9		3,884.36
KCL, Tech(sx)	25 kg	14.44	213	269	5.1	7.0	3,075.72	- / -
Lime	25 kg	8.04	4	2	0.1	0.1	32.16	16.08
oda Ash	25 kg	16.15	7	2	0.2	0.1	113.05	32.30
BARACOR 129	25 kg	64.96		2		0.1		129.92
	208 lt	417.25		1		0.2		417.25
CONDET PAC-R	50 lb	170.74		6		0.1		1,024.44

VOLUMES			COST LESS BARITE : COST WITH BARITE :	A\$14,372.28 A\$16,351.32	A\$21,140.25 A\$22,369.17
Sea W.	bbl				
Drill W.	bbl	1922	1700		
other	bbi				
other	bbl				
Chemical	bbl	47.3	59		
Salvaged Mud	bbl	350	370		
TOTAL MUDUSED	bbl	2319	2129		

COMMENTS

370 bbl of AQUAGEL/CMC mud carried over from previous 12-1/4" interval.

MATERIAL RECAP

NON-DRILLING

COMPANY G.F.E. RESOURCES LTD. WELL IONA - 2 LOCATION OTWAY BASIN, VICTORIA **HOLE SIZE** 

CONTRACTOR/RIG CENTURY DRILLING / RIG - 11 USED FOR Cementing & Completion

MATERIAL	UNIT	UNIT	QUA	NTITY	CONC (IB/BBI) TOTAL C	
MATERIAL	SIZE	COST	EST	ACT	EST ACT ESTIMATE	ACTUAL
AQUACEL SH	25 kg	14.33	40	20	573.20	286.60
AQUAGEL,sx	208 lt	583.35	1	1	583.35	583.35
BARACOR-100		7.71	240	387	1,850.40	2,983.77
SALT	25 kg		2-10	20,	499.14	998.28
XCD Polymer	25 kg	499.14	,	2		319.40
BARAFILM 415	25 lt	159.7		2		

VOLUMES			COST LESS BARITE : COST WITH BARITE :	A\$3,506.09 A\$3,506.09	A\$5,171.40 A\$5,171.40
Sea W.	bbl bbl	320	523		
Drill W.	bbl	020			
other	bbl	04.0	24		
Chemical	bbl bbl	21.3	31		
Salvaged Mud	bbl	341	554		

COMMENTS

20 sxs AQUAGEL used in cement mix water for 9-5/8" casing.

2 sxs XCD Polymer used to mix Hi – Vis sweeps used to clean 7" production casing after casing scraper runs.

387 sxs salt and 1 drum of BARACOR-100 mixed in 523 bbls water to make up completion brine.

2 cans of BARAFILM 415 used to coat drill pipe as anti-corrosion measure, while laying out pipe.



MATERIAL SUMMARY

COMPANY G.F.E. RESOURCES LTD. WELL IONA - 2

LOCATION OTWAY BASIN, VICTORIA CONTRACTOR/RIG CENTURY DRILLING / RIG - 11

**WELL DURATION HOURS** DAYS SIZE m INTERVAL MUD TYPES 14-Feb-94 FROM: 16 624 4 12 1/4" AQUAGEL/CMC 04-Mar-94 TO: 82 AQUAGEL/CMC to 3% KCI/Polyme8 1/2" 1010 11

> A\$1,690.76 COST/DAY A\$15.52 COST/m A\$8.51 COST/bbl 98 1634 15

		TOTALS	1634 13			4 00
DECAR BY	A. Searle, M. Ole		CON	SUMPTION FAC	TOR (bbl/m)	1.82
		UNIT	QUAN	FITY	TOTAL	XOSTS
MATERIAL	UNIT		ESTIMATE	ACTUAL	ESTIMATE	ACTUAL
	SIZE	COST		36		574.56
Barite,sx	50 kg	15.96	0.49	82	1.979.04	654.36
Barite,sx	25 kg	7.98	248		5.273.44	4,069.72
AQUAGEL,sx	25 kg	14.33	368	284	549.92	549.92
BARACIDE	25 kg	549.92	1	1		1,005.33
Caustic Soda	25 kg	32.43	29	31	940.47	
	25 kg	106.61	49	71	5,223.89	7,569.31
CMC-EHV	50 lb	59.88	71	80	4,251.48	4,790.40
DEXTRID LT	= =	14.44	213	279	3,075.72	4,028.76
(CL,Tech(sx)	25 kg		2,0	17		490.96
KCL,Tech(sx)	50 kg	28.88	11	3	88.44	24.12
Lime	25 kg	8.04	11	2	113.05	32.30
Soda Ash	25 kg	16.15	/	2	, 10.00	129.92
BARACOR 129	25 kg	64.96		4		417.25
CONDET	208 It	417.25		1		1,024.44
PAC-R	50 lb	170.74		6		1,024.44
FAC=H	00 15					

VOLUMES			ESS BARITE : ITH BARITE :	A\$19,516.41 A\$21,495.45	A\$24,132.43 A\$25,361.35
Sea W. Drill W.	bbl bbl bbl	3172	2913		
other other Chemical	bbl bbl	64.2	68		
Salvaged Mud TOTAL MUD USED	bbl bbl	3236	2981		

COMMENTS

Above materials are those used only for drilling.



# Baroid Australia Pty Ltd company G.F.E. RESOURCES LTD.

WEEKLY INVENTORY

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# Baroid Australia Pty Ltd company G.F.E. RESOURCES LTD.

WEEKLY INVENTORY

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# Baroid Australia Pty Ltd company G.F.E. RESOURCES LTD.

WEEKLY INVENTORY

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	COMPANY		ш.	RES LTI	ا ا															YEAR	1994
	MELL	<u>₹</u>	28/02			01/03	-		02/03		0	03/03	-	04	04/03						1 1
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Barite.sx	25 kg			320			320			320			88			320					
AQUAGEL.sx	25 kg	27		217			217	-		216	+		216	+		216					
BARACIDE	25 kg										+	+	1		1						
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KCL, Tech(sx)	50 kg											+	+			1					
Lime	25 kg			17			17			17			17		+	17					
Soda Ash	25 kg			20			ଅ			8			ล	2		98					
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COMPANY G.F.E. RESOURCES LTD.

LOCATION OTWAY BASIN, VICTORIA
CONT/RIG CENTURY DRILLING / RIG - 11

MATERIAL RECONCILIAT

DATES: FROM

14-Feb-94

WELL	IONA – 2						T/RIG			<u>ING / R</u>	G - 11				,	TO 04 - Mar - 9
		START		TOTAL			INTERV	AL USE	AGE			(8)	VAR-	TOTAL		
MATERIAL	UNIT	втоск			(1)	(2)	(3)	(4)	(5)	(6)	(7)	NON		USED		
	SIZE			+DEL.	12 1/4"	8 1/2"						DRLG			TORY	COMMENTS
Barite,sx	50 kg	236		236		36						ļ		36	200	
Barite,sx	25 kg	402		402		82						-		82	320	
QUAGEL,sx	25 kg	520		520	52	232						20	ļ	304	216	
BARACIDE	25 kg	1		1		1_								1		
Caustic Soda	25 kg	40		40	10	21							<b> </b>	31	9	
CMC-EHV	25 kg	80		80	12	59								71	9	
DEXTRID LT	50 lb	80		80		80						<del> </del>		80		
(CL,Tech(sx)	25 kg	119	240	359		269							<u> </u>	279		
(CL,Tech(sx)	50 kg	17		17	17		<u> </u>							17		
ime	25 kg	20		20		2							<b> </b>	3		
Soda Ash	25 kg	20		20		2	ļ	<u> </u>					<b> </b> -	2		
Z SPOT	208 lt		5	5			ļ						<b>-</b>	1		3 of the EZ SPOT were not
BARACOR-100	208 lt		1	1			ļ					1 1	·	1		Baroid stock, but from Nelso
SALT	25 kg		600	600	<u> </u>						<u> </u>	387		387		warehouse.
CD Polymer	25 kg		10	10	<u> </u>			ļ				2		2		
BARACOR 129	25 kg		10	10		2	ļ	ļ						2		
BARAFILM 415	25 lt		2	2					ļ			2	<u> </u>	2		
CONDET	208 lt		1			1			ļ		ļ		-	11		
PAC-R	50 lb		20			6		1		ļ	ļ			6		
BARACARB 110	25 kg		48						-		ļ				48	·
BARACARB 600	25 kg		48	48	<u> </u>			ļ			ļ			-	48	
					ļ					<u> </u>	ļ					
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SOLIDS CONTROL and MUD **VOLUME ANALYSIS** 

PAGE 1

COMPANY G.F.E. RESOURCES LTD. WELL IONA - 2

LOCATION OTWAY BASIN, VICTORIA

1994

•	CONT/RIG	PERMITTE	JUITETHIAG /	nia – n				1	04 6-6	oo Esh	23 - Fah
SOLIDS CON		14-Feb	15-Feb	16-Feb	17 – Feb	18Feb	19-Feb	20-Feb	21-Feb	22-Feb	110/84/50
Shaker 1	Screens	3 x 50	3 x 50	3 x 50	3 x 50	3 x 110		110/84/50	110/84/50	21	14
TRITON	Hrs	12	14.5	16	3.5		10	12	15		
Shaker 2	Screens						i				
	Hrs										
Shaker 3	Screens						Ì				
	Hrs										
Shaker 4	Screens	ĺ							į		
	Hrs						40.0	10.0	11.7	12.7	10.9
Desander	U/F ppg	9.4	14.3	12.1			13.8	12.9 6.5	2.5	1.5	2
2 x 12"	bbi/hr	6	7.5	7.5	į		7.45	12	15	20	14.5
	Hrs	12	13.5	10			8.5	78	38	30	29
	bbl	72	101	75			63	10.9	11.4	10.2	10.9
Desilter 1.	U/F ppg	10.7	14.6	12.6			10.7	5	3	6	5
12 x 4"	bbl/hr	3.5	3.5	3.5	1		5.75	12	3	4.5	8.5
	Hrs	12	14	10			8.5 49	60	9	27	43
	bbl	42	49	35	i		49	- 60			
Desilter 2.	U/F ppg										
1	bbl/hr		İ				ļ				
	Hrs										
	bbl										
Centrifuge 1	Feed ppg										
	O/F ppg										
	U/F ppg										
	bbl/hr	İ									
	Hrs										
	bbl										
Centrifuge 2	Feed ppg										
	O/F ppg										
	U/F ppg										
	bbl/hr										
		1	1	i			1	i i			
	Hrs	i .									
	bbl								I	20 F-b	00 Fab
VOLUMES I	bbl	14-Feb	15-Feb	16-Feb	17-Feb	18-Feb	19-Feb	20-Feb	21 – Feb	22-Feb	23-Feb
VOLUMES I	bbl bbl	14-Feb 91	15-Feb 207	271	17-Feb 164	131	170	219	21-Feb 236	265	298
	bbl bbl lume				164			219 41			
Downhole Vo	bbl b <b>bl</b> lume			271		131	170	219		265	298
Downhole Vo Initial Reserve	bbl bbl lume		207	271 27	164	131 101	170 33	219 41	236	265 71	298 37
Downhole Vo Initial Reserve	bbl bbl lume Act Mud			271	164	131	170	219 41		265	298
Downhole Vo Initial Reserve	bbl bbl lume Act Mud Seawater		207	271 27	164	131 101	170 33	219 41	236	265 71	298 37
Downhole Vo Initial Reserve	bbl lume Act Mud Seawater Drill-Water other		207	271 27 130	164	131 101	170 33 250	219 41 ,	330	265 71 100	298 37 250
Downhole Vo Initial Reserve	bbl lume Act Mud Seawater Drill-Water other		207	271 27	164	131 101 33	170 33 250	219 41	236 330	265 71 100	298 37 250
Downhole Vo Initial Reserve	bbl lume Act Mud Seawater Drill-Water other other Chemical		207 203 3.5 27	271 27 130	101	131 101 33	170 33 250 4 41	219 41 , 125	236 330 12 71	265 71 100 3 37	298 37 250 6 37
Downhole Vo Initial Reserve Added:	bbl lume Act Mud Seawater Drill-Water other other Chemical		207 203 3.5 27 465	271 27 130 2 360	164	131 101 33 33 322	170 33 250 4 41 407	219 41 , 125 9	236 330 12 71 330	265 71 100 3 37 386	298 37 250 6 37 338
Downhole Vo Initial Reserve Added:  Final Reserve Initial Active	bbl lume Act Mud Seawater Drill-Water other other Chemical		207 203 3.5 27	271 27 130	101	131 101 33	170 33 250 4 41	219 41 , 125	236 330 12 71	265 71 100 3 37	298 37 250 6 37
Downhole Vo Initial Reserve Added:	bbl lume Act Mud Seawater Drill—Water other other Chemical		207 203 3.5 27 465	271 27 130 2 360 159	101	33 322 101	170 33 250 4 41 407 246	219 41 , 125 9	236 330 12 71 330	265 71 100 3 37 386	298 37 250 6 37 338
Downhole Vo Initial Reserve Added:  Final Reserve Initial Active	bbl lume Act Mud Seawater Drill—Water other Chemical		207 203 3.5 27 465	271 27 130 2 360	101	131 101 33 33 322	170 33 250 4 41 407	219 41 , 125 9	236 330 12 71 330	265 71 100 3 37 386	298 37 250 6 37 338
Downhole Vo Initial Reserve Added:  Final Reserve Initial Active	bbl lume Act Mud Seawater Drill-Water other Chemical Res Mud Seawater Drill-Water	91	203 3.5 27 465 180	271 27 130 2 360 159	101	33 322 101	170 33 250 4 41 407 246	219 41 , 125 9	236 330 12 71 330	265 71 100 3 37 386	298 37 250 6 37 338
Downhole Vo Initial Reserve Added:  Final Reserve Initial Active	bbl lume Act Mud Seawater Drill-Water other Chemical Res Mud Seawater Drill-Water other	91	203 3.5 27 465 180	271 27 130 2 360 159	164 101 101 322	33 322 101	170 33 250 4 41 407 246	219 41 , 125 9	236 330 12 71 330	265 71 100 3 37 386 137	298 37 250 6 37 338 256
Downhole Vo Initial Reserve Added:  Final Reserve Initial Active	bbl lume Act Mud Seawater Drill-Water other Chemical Res Mud Seawater Drill-Water other other other other	91	203 3.5 27 465 180	271 27 130 2 360 159	101	33 322 101	170 33 250 4 41 407 246 115	219 41 , 125 9 355 175	236 330 12 71 330 271	265 71 100 3 37 386 137	298 37 250 6 37 338 256
Downhole Vo Initial Reserve Added: Final Reserve Initial Active Added:	bbl lume Act Mud Seawater Drill-Water other Chemical Res Mud Seawater Drill-Water other Chemical Chemical	800	203 3.5 27 465 180 45	271 27 130 2 360 159	164 101 101 322	33 322 101	170 33 250 4 41 407 246 115	219 41 , 125 9 355 175	236 330 12 71 330 271	265 71 100 3 37 386 137	298 37 250 6 37 338 256
Downhole Vo Initial Reserve Added:  Final Reserve Initial Active Added:	bbl lume Act Mud Seawater Drill—Water other Chemical Res Mud Seawater Drill—Water other other Chemical Seawater Orill—Water other other other	800	203 3.5 27 465 180 45	271 27 130 2 360 159 35	164 101 101 322	33 322 101	170 33 250 4 41 407 246 115	219 41 , 125 9 355 175	236 330 12 71 330 271	265 71 100 3 37 386 137	298 37 250 6 37 338 256
Downhole Vo Initial Reserve Added:  Final Reserve Initial Active Added:	bbl lume Act Mud Seawater Drill—Water other Chemical Res Mud Seawater Drill—Water other Chemical Seawater Orill—Water other	800 4 114	203 3.5 27 465 180 45 0.5	271 27 130 2 360 159 35	101 101 322 2 172	33 322 101 115	170 33 250 4 41 407 246 115	219 41 , 125 9 355 175	236 330 12 71 330 271	265 71 100 3 37 386 137	298 37 250 6 37 338 256
Downhole Vo Initial Reserve Added:  Final Reserve Initial Active Added:	bbl lume Act Mud Seawater Drill—Water other Chemical Res Mud Seawater Drill—Water other other Chemical Seawater Orill—Water other other other	800 4 114	203 3.5 27 465 180 45 0.5	271 27 130 2 360 159 35	101 101 322 2 172 322	33 322 101 115	170 33 250 4 41 407 246 115	219 41 , 125 9 355 175	236 330 12 71 330 271 47 151 386	265 71 100 3 37 386 137 5 57 104 338	298 37 250 6 37 338 256
Final Reserve Initial Active Added:  Losses: S Final Active	bbl bbl lume Act Mud Seawater Drill—Water other Chemical Res Mud Seawater Drill—Water other chemical Solids Control ost/Dumped DownHole	800 4 114 134	203 3.5 27 465 180 45 0.5 150 65	271 27 130 2 360 159 35	101 101 322 2 172	33 322 101 115	170 33 250 4 41 407 246 115	219 41 , 125 9 355 175	236 330 12 71 330 271	265 71 100 3 37 386 137	298 37 250 6 37 338 256
Final Reserve Initial Active Added:  Losses: S Final Active Total Final Vo	bbl bbl lume Act Mud Seawater Drill—Water other Chemical Res Mud Seawater Drill—Water other chemical Solids Control ost/Dumped DownHole	800 4 114 134 465	203 3.5 27 465 180 45 0.5 150 65 360 387	271 27 130 2 360 159 35 110 58 322 322	164 101 101 322 2 172 322 423	131 101 33 322 101 115	170 33 250 4 41 407 246 115	219 41 , 125 9 355 175 138 13 330 330	236 330 12 71 330 271 47 151 386 457	265 71 100 3 37 386 137 5 57 104 338 375	298 37 250 6 37 338 256 1 72 136 354 391
Final Reserve Initial Active Added:  Losses: S Final Active Total Final Vo	bbl bbl lume Act Mud Seawater Drill—Water other Chemical Res Mud Seawater Drill—Water other Chemical Solids Control Lost/Dumped DownHole	800 4 114 134 465	203 3.5 27 465 180 45 0.5 150 65	271 27 130 2 360 159 35 110 58 322 322	164 101 101 322 2 172 322 423 SYS1	131 101 33 322 101 115 407 440	170 33 250 4 41 407 246 115	219 41 , 125 9 355 175 138 13 330 330	236 330 12 71 330 271 47 151 386 457	265 71 100 3 37 386 137 5 57 104 338 375	298 37 250 6 37 338 256 1 72 136 354 391
Final Reserve Initial Active Added:  Losses: S Final Active Total Final Vo DILUTION Interval Type	bbl bbl lume Act Mud Seawater Drill—Water other Chemical Res Mud Seawater Drill—Water other Chemical Solids Control Lost/Dumped DownHole	800 4 114 134 465 465	203 3.5 27 465 180 45 0.5 150 65 360 387	271 27 130 2 360 159 35 110 58 322 322 SYS1 640	164 101 101 322 2 172 322 423	131 101 33 322 101 115	170 33 250 4 41 407 246 115 112 262 355 396 SYS-2 823	219 41 , 125 9 355 175 138 13 330 330 330	236 330 12 71 330 271 47 151 386 457 SYS-2 1133	265 71 100 3 37 386 137 57 104 338 375	298 37 250 6 37 338 256 1 72 136 354 391 SYS-2 1404
Final Reserve Initial Active Added:  Losses: S Final Active Total Final Vo DILUTION Interval Type Depth m	bbl lume Act Mud Seawater Drill—Water other Chemical Res Mud Seawater Drill—Water other Chemical Solids Control Lost/Dumped DownHole	800 4 114 134 465 465 SYS1	203 3.5 27 465 180 45 0.5 150 65 360 387	271 27 130 2 360 159 35 110 58 322 322	164 101 101 322 2 172 322 423 SYS1	131 101 33 322 101 115 407 440	170 33 250 4 41 407 246 115 112 262 355 396 SYS-2 823 183	219 41 , 125 9 355 175 138 13 330 330 330	236 330 12 71 330 271 47 151 386 457 SYS-2 1133 81	265 71 100 3 37 386 137 57 104 338 375 SYS-2 1268 135	298 37 250 6 37 338 256 1 72 136 354 391 SYS-2 1404 136
Final Reserve Initial Active Added:  Losses: S Final Active Total Final Vo DILUTION Interval Type Depth m Daily drilled in the serve Initial Active Initial Active Initial Active Initial Active Initial Active Initial Initial Vo DILUTION Interval Type Depth m Daily drilled in Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Initial Ini	bbl bbl lume Act Mud Seawater Drill—Water other Chemical Res Mud Seawater Drill—Water other chemical Solids Control Lost/Dumped DownHole	800 4 114 134 465 465 SYS1 232	203 3.5 27 465 180 45 0.5 150 65 360 387 SYS1 500	271 27 130 2 360 159 35 110 58 322 322 SYS1 640 140 168	164 101 101 322 2 172 322 423 SYS1	131 101 33 322 101 115 407 440 SYS-2 640	170 33 250 4 41 407 246 115 112 262 355 396 SYS-2 823 183 374	219 41 , 125 9 355 175 138 13 330 330 330 SYS-2 1052 229 151	236 330 12 71 330 271 47 151 386 457 SYS-2 1133 81 198	265 71 100 3 37 386 137 5 57 104 338 375 SYS-2 1268 135 161	298 37 250 6 37 338 256 1 72 136 354 391 SYS-2 1404 136 208
Final Reserve Initial Active Added:  Losses: S Final Active Total Final Vo DILUTION Interval Type Depth m Daily drilled in Daily Dilution	bbl bbl lume Act Mud Seawater Drill—Water other Chemical Seawater Drill—Water other Chemical Solids Control Lost/Dumped DownHole Dlume	91 800 4 114 134 465 465 SYS1 232 216 248	203 3.5 27 465 180 45 0.5 150 65 360 387 SYS1 500 268	271 27 130 2 360 159 35 110 58 322 322 SYS1 640 140	164 101 101 322 2 172 322 423 SYS1 640	131 101 33 322 101 115 407 440	170 33 250 4 41 407 246 115 112 262 355 396 SYS-2 823 183 374 369	219 41 , 125 9 355 175 138 13 330 330 330 151 134	236 330 12 71 330 271 47 151 386 457 SYS-2 1133 81 198 342	265 71 100 3 37 386 137 57 104 338 375 SYS-2 1268 135 161 108	298 37 250 6 37 338 256 1 72 136 354 391 SYS-2 1404 136 208 257
Final Reserve Initial Active Added:  Losses: S Final Active Total Final Vo DILUTION Interval Type Depth m Daily drilled in Daily Consur	bbl bbl lume Act Mud Seawater Drill—Water other Chemical Seawater Drill—Water other	800 4 114 134 465 465 465 SYS1 232 216 248 804	203  3.5 27 465 180 45 0.5 150 65 360 387  SYS1 500 268 215 252	271 27 130 2 360 159 35 110 58 322 322 SYS1 640 140 168	164 101 101 322 2 172 322 423 SYS1 640 172	131 101 33 322 101 115 407 440 SYS-2 640	170 33 250 4 41 407 246 115 112 262 355 396 SYS-2 823 183 374 369 183	219 41 , 125 9 355 175 138 13 330 330 330 330 1052 229 151 134 412	236 330 12 71 330 271 47 151 386 457 SYS-2 1133 81 198 342 493	265 71 100 3 37 386 137 5 57 104 338 375 SYS-2 1268 135 161 108 628	298 37 250 6 37 338 256 1 72 136 354 391 SYS-2 1404 136 208 257 764
Final Reserve Initial Active Added:  Losses: S Final Active Added:  Losses: S Final Active Total Final Vo DILUTION Interval Type Depth m Daily drilled in Daily Consur Interval Drille	bbl lume Act Mud Seawater Drill—Water other Chemical Res Mud Seawater Drill—Water other Chemical Solids Control Lost/Dumped DownHole Dlume  m h bbl mption bbl ad m	91 800 4 114 134 465 465 SYS1 232 216 248 804 216	203  3.5 27 465 180 45 0.5 150 65 360 387  SYS1 500 268 215 252 484	271 27 130 2 360 159 35 110 58 322 322 SYS1 640 140 168 167	164 101 101 322 2 172 322 423 SYS1 640 172 2	131 101 33 322 101 115 407 440 SYS-2 640	170 33 250 4 41 407 246 115 112 262 355 396 SYS-2 823 183 374 369	219 41 , 125 9 355 175 138 13 330 330 330 151 134 412 525	236 330 12 71 330 271 47 151 386 457 SYS-2 1133 81 198 342 493 723	265 71 100 3 37 386 137 5 57 104 338 375 SYS-2 1268 135 161 108 628 884	298 37 250 6 37 338 256 1 72 136 354 391 SYS-2 1404 136 208 257 764 1092
Final Reserve Initial Active Added:  Losses: S Final Active Added:  Losses: S Final Active Total Final Vo DILUTION Interval Type Depth m Daily drilled in Daily Consur Interval Drille Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Daily Consur Interval Dilution Dilution Daily Consur Interval Dilution Dilution Dilution Dilution Dilution Daily Consur Interval Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dilution Dil	bbl lume Act Mud Seawater Drill—Water other Chemical Res Mud Seawater Drill—Water other Chemical Solids Control Lost/Dumped DownHole Dlume  m h bbl mption bbl ad m	800 4 114 134 465 465 232 216 248 804 216 248	203  3.5 27 465 180 45 0.5 150 65 360 387  SYS1 500 268 215 252 484 463	271 27 130 2 360 159 35 110 58 322 322 SYS1 640 140 168 167 624 631	164 101 101 322 2 172 322 423 SYS1 640 172 2 624 803	131 101 33 322 101 115 407 440 SYS-2 640	170 33 250 4 41 407 246 115 112 262 355 396 SYS-2 823 183 374 369 183 374 2.04	219 41 , 125 9 355 175 138 13 330 330 330 151 134 412 525 1.27	236 330 12 71 330 271 47 151 386 457 SYS-2 1133 81 198 342 493 723 1.47	265 71 100 3 37 386 137 5 57 104 338 375 SYS-2 1268 135 161 108 628 884 1.41	298 37 250 6 37 338 256 1 72 136 354 391 SYS-2 1404 136 208 257 764 1092 1.43
Final Reserve Initial Active Added:  Final Reserve Initial Active Added:  Losses: S Final Active Total Final Vo DILUTION Interval Type Depth m Daily drilled in Daily Consur Interval Drille Interval Diluting Rate bbl/m	bbl lume Act Mud Seawater Drill—Water other Chemical Res Mud Seawater Drill—Water other Chemical Solids Control Lost/Dumped DownHole Dlume  m h bbl mption bbl ad m	91 800 4 114 134 465 465 SYS1 232 216 248 804 216	203  3.5 27 465 180 45 0.5 150 65 360 387  SYS1 500 268 215 252 484	271 27 130 2 360 159 35 110 58 322 322 SYS1 640 140 168 167 624	164 101 101 322 2 172 322 423 SYS1 640 172 2 624	131 101 33 322 101 115 407 440 SYS-2 640	170 33 250 4 41 407 246 115 112 262 355 396 SYS-2 823 183 374 369 183 374 2.04	219 41 , 125 9 355 175 138 13 330 330 330 151 134 412 525 1.27	236 330 12 71 330 271 47 151 386 457 SYS-2 1133 81 198 342 493 723	265 71 100 3 37 386 137 5 57 104 338 375 SYS-2 1268 135 161 108 628 884 1.41 1101	298 37 250 6 37 338 256 1 72 136 354 391 SYS-2 1404 136 208 257 764 1092 1.43 1358

BAROID

## Baroid Australia Pty Ltd

COMPANY G.F.E. RESOURCES LTD.

SOLIDS CONTROL and MUD **VOLUME ANALYSIS** 

	COMPANY			LID.						F	PAGE 2
		IONA - 2	OIN MOTO							'	AGE 2
	OCATION	OTWAY BA	SIN, VICTO	JRIA / BIC 11							1994
	CONT/RIG	CENTURY	OF Eab	76-Feb	27_Feb	28-Feb	01 – Mar	02-Mar	03-Mar	04-Mar	
SOLIDS COI		110/84/50	25-1 eb	20-1 eb	21 100	00 1 00	O, IVICI.				
Shaker 1	Screens	19					į				
TRITON	Hrs Screens	19									
Shaker 2	Hrs			İ							
Shaker 3	Screens										
Snaker S	Hrs										
Shaker 4	Screens										
Silakei 4	Hrs	1		į							
Desander	U/F ppg	11.3									
2 x 12"	bbl/hr	1.5					}				
2 X 1 2	Hrs	18									
	bbl	27									
Desilter 1.	U/F ppg	11.3			į						
12 x 4"	bbl/hr	4			i						
	Hrs	18	ĺ	j							
	bbl	72									
Desilter 2.	U/F ppg										
	bbl/hr										
	Hrs										
	bbl										
Centrifuge 1	Feed ppg			•		-					
	O/F ppg		İ								
	U/F ppg										
	bbl/hr										
	Hrs										
	bbl										
Centrifuge 2	Feed ppg										
	O/F ppg										
	U/F ppg										
	bbl/hr										
VOLU <b>M</b> ES	bbl/hr Hrs bbl	24-Feb	25-Feb	26-Feb	27-Feb	28-Feb	01 – Mar	02-Mar	03-Mar	04-Mar	
	bbl/hr Hrs bbl bbl	24-Feb 351	25-Feb 395	26-Feb 395	365	395	239	239	239	239	
Downhole Vo	bbl/hr Hrs bbl blume							239 23	239 37		
Downhole Vo Initial Reserv	bbl/hr Hrs bbl blume	351	395	395	365	395	239	239	239	239	
VOLUMES Downhole Volutial Reserv Added:	bbl/hr Hrs bbl  bul  blume	351	395	395	365 27	395	239	239 23 14	239 37	239	
Downhole Vo Initial Reserv	bbl/hr Hrs bbl bbl blume e Act Mud	351	395	395	365 27	395	239	239 23	239 37	239	
Downhole Vo Initial Reserv	bbl/hr Hrs bbl bbl blume e Act Mud Seawater	351 37	395 34	395	365 27	395	239	239 23 14	239 37	239	
Downhole Vo Initial Reserv	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill—Water	351 37	395 34	395	365 27	395	239	239 23 14	239 37	239	
Downhole Vo Initial Reserv	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill-Water other	351 37	395 34 110	395 87 4	365 27 16	395 44	239 23	239 23 14 40	239 37 10	239 47	
Downhole Vo Initial Reserv	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill-Water other other Chemical	351 37 200	395 34 110 4 87	395 87 4 27	365 27 16	395 44 23	239 23 23 23	239 23 14 40	239 37 10	239 47 47	
Downhole Vo Initial Reserv Added:	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill-Water other other Chemical	351 37 200	395 34 110	395 87 4 27 254	365 27 16	395 44 23 238	239 23	239 23 14 40 37 324	239 37 10	239 47	
Downhole Vol Initial Reserv Added: Final Reserve Initial Active	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill-Water other other Chemical	351 37 200 10 34	395 34 110 4 87	395 87 4 27	365 27 16	395 44 23	239 23 23 23	239 23 14 40	239 37 10	239 47 47	
Downhole Vol Initial Reserv Added: Final Reserve Initial Active	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill-Water other other Chemical	351 37 200 10 34 354	395 34 110 4 87 342	395 87 4 27 254	365 27 16 1 44 254	395 44 23 238 21	239 23 23 23 256	239 23 14 40 37 324 40	239 37 10 47 119	239 47 47 120	
Downhole Vol Initial Reserv Added: Final Reserve Initial Active	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill—Water other Chemical e Res Mud	351 37 200 10 34 354	395 34 110 4 87 342	395 87 4 27 254	365 27 16	395 44 23 238	239 23 23 23	239 23 14 40 37 324	239 37 10	239 47 47	
Downhole Vo Initial Reserv Added: Final Reserve	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill-Water other Chemical e Res Mud Seawater	351 37 200 10 34 354	395 34 110 4 87 342	395 87 4 27 254	365 27 16 1 44 254	395 44 23 238 21	239 23 23 23 256	239 23 14 40 37 324 40	239 37 10 47 119	239 47 47 120	
Downhole Vollatial Reserve Added:  Final Reserve Initial Active	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill-Water other Chemical e Res Mud Seawater Drill-Water	351 37 200 10 34 354	395 34 110 4 87 342	395 87 4 27 254	365 27 16 1 44 254	395 44 23 238 21	239 23 23 23 256 347	239 23 14 40 37 324 40 43	239 37 10 47 119	239 47 47 120 70	
Downhole Vo Initial Reserv Added: Final Reserve Initial Active	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill-Water other Chemical e Res Mud Seawater Drill-Water other other other other	351 37 200 10 34 354 213	395 34 110 4 87 342	395 87 4 27 254	365 27 16 1 44 254	395 44 23 238 21	239 23 23 23 256	239 23 14 40 37 324 40	239 37 10 47 119	239 47 47 120	
Downhole Vo Initial Reserv Added: Final Reserve Initial Active Added:	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill-Water other Chemical e Res Mud Seawater Drill-Water other other other other other other	351 37 200 10 34 354 213	395 34 110 4 87 342 61	395 87 4 27 254 64	365 27 16 1 44 254	23 238 21 40	239 23 23 256 347	239 23 14 40 37 324 40 43	239 37 10 47 119 50	239 47 47 120 70	
Downhole Volinitial Reserve Added:  Final Reserve Initial Active Added:  Losses:	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill—Water other Chemical Seawater Drill—Water other Chemical Chemical Solids Control Lost/Dumped	351 37 200 10 34 354 213	395 34 110 4 87 342 61	395 87 4 27 254 64	365 27 16 1 44 254	395 44 23 238 21	239 23 23 23 256 347	239 23 14 40 37 324 40 43	239 37 10 47 119	239 47 47 120 70	
Downhole Vollatial Reserve Added:  Final Reserve Initial Active Added:  Losses:	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill-Water other Chemical e Res Mud Seawater Drill-Water other Chemical cother Chemical cother other other	351 37 200 10 34 354 213	395 34 110 4 87 342 61	395 87 4 27 254 64	365 27 16 1 44 254 5	23 238 21 40	239 23 23 256 347 18 692	239 23 14 40 37 324 40 43 5	239 37 10 47 119 50 6 45	239 47 47 120 70 2	
Downhole Volinitial Reserve Added:  Final Reserve Initial Active Added:  Losses: S	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill—Water other Chemical e Res Mud Seawater Drill—Water other Chemical Solids Control Lost/Dumped DownHole	351 37 200 10 34 354 213	395 34 110 4 87 342 61 55 50 254	395 87 4 27 254 64 39 25 254	365 27 16 1 44 254 5 15 20 238	23 238 238 21 40	239 23 23 256 347 18 692 324	239 23 14 40 37 324 40 43 5 40	239 37 10 47 119 50 6 45	239 47 47 120 70 2 72 120	
Downhole Vollatial Reserve Added:  Final Reserve Initial Active Added:  Losses:  Final Active Total Final V	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill—Water other Chemical e Res Mud Seawater Drill—Water other Chemical Solids Control Lost/Dumped DownHole	351 37 200 10 34 354 213	395 34 110 4 87 342 61	395 87 4 27 254 64	365 27 16 1 44 254 5	23 238 21 40	239 23 23 256 347 18 692	239 23 14 40 37 324 40 43 5	239 37 10 47 119 50 6 45	239 47 47 120 70 2	
Downhole Volatial Reserve Added:  Final Reserve Initial Active Added:  Losses:  Final Active Total Final V	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill-Water other Chemical e Res Mud Seawater Drill-Water other Chemical Solids Control Lost/Dumped DownHole	351 37 200 10 34 354 213 99 73 342 376	395 34 110 4 87 342 61 55 50 254 341	395 87 4 27 254 64 39 25 254 281	365 27 16 1 44 254 5 15 20 238 282	23 238 21 40 13 256 279	239 23 23 256 347 18 692 324 347	239 23 14 40 37 324 40 43 5 40 119 156	239 37 10 47 119 50 6 45 120 167	239 47 47 120 70 2 72 120 167	
Downhole Volential Reserve Added:  Final Reserve Initial Active Added:  Losses:  Final Active Total Final Volential Type Interval Type	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill-Water other Chemical e Res Mud Seawater Drill-Water other Chemical Solids Control Lost/Dumped DownHole	351 37 200 10 34 354 213 99 73 342 376	395 34 110 4 87 342 61 55 50 254 341 SYS-2	395 87 4 27 254 64 39 25 254 281	365 27 16 1 44 254 5 15 20 238 282	395 44 23 238 21 40 13 256 279	239 23 23 256 347 18 692 324 347	239 23 14 40 37 324 40 43 5 40 119 156	239 37 10 47 119 50 6 45 120 167	239 47 47 120 70 2 72 120 167	
Downhole Volential Reserve Added:  Final Reserve Initial Active Added:  Losses: S  Final Active Total Final Volential Type Depth m	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill-Water other Chemical Seawater Drill-Water other Chemical Solids Control Lost/Dumped DownHole	351 37 200 10 34 354 213 99 73 342 376 SYS-2 1650	395 34 110 4 87 342 61 55 50 254 341	395 87 4 27 254 64 39 25 254 281	365 27 16 1 44 254 5 15 20 238 282	23 238 21 40 13 256 279	239 23 23 256 347 18 692 324 347	239 23 14 40 37 324 40 43 5 40 119 156	239 37 10 47 119 50 6 45 120 167	239 47 47 120 70 2 72 120 167	
Downhole Volential Reserve Added:  Final Reserve Initial Active Added:  Losses:  Final Active Total Final Volential Type Depth m Daily drilled	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill-Water other Chemical Seawater Drill-Water other Chemical Solids Control Lost/Dumped DownHole	351 37 200 10 34 354 213 99 73 342 376 SYS-2 1650 246	395 34 110 4 87 342 61 55 50 254 341 SYS-2 1650	395 87 4 27 254 64 39 25 254 281 SYS-2 1650	365 27 16 1 44 254 5 15 20 238 282 SYS-2 1650	395 44 23 238 21 40 13 256 279 SYS-2 1650	239 23 23 256 347 18 692 324 347 Complet 1650	239 23 14 40 37 324 40 43 5 40 119 156  Complet 1650	239 37 10 47 119 50 6 45 120 167 Complet 1650	239 47 47 120 70 2 72 120 167 Complet 1650	
Downhole Volential Reserve Added:  Final Reserve Initial Active Added:  Losses: S  Final Active Total Final Volential Type Depth m	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill-Water other Chemical Seawater Drill-Water other Chemical Solids Control Lost/Dumped DownHole	351 37 200 10 34 354 213 99 73 342 376 SYS-2 1650 246 172	395 34 110 4 87 342 61 55 50 254 341 SYS-2 1650 105	395 87 4 27 254 64 39 25 254 281 SYS-2 1650 64	365 27 16 1 44 254 5 15 20 238 282 SYS-2 1650 35	395 44 23 238 21 40 13 256 279 SYS-2 1650	239 23 23 256 347 18 692 324 347 Complet 1650 692	239 23 14 40 37 324 40 43 5 40 119 156 Complet 1650 40	239 37 10 47 119 50 6 45 120 167 Complet 1650	239 47 47 120 70 2 72 120 167 Complet 1650 72	
Downhole Volinitial Reserve Added:  Final Reserve Initial Active Added:  Losses: S  Final Active Total Final V  DILUTION Interval Type Depth m  Daily drilled	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill-Water other Chemical e Res Mud Seawater Drill-Water other Chemical Solids Control Lost/Dumped DownHole	351 37 200 10 34 354 213 99 73 342 376 SYS-2 1650 246	395 34 110 4 87 342 61 55 50 254 341 SYS-2 1650 105 114	395 87 4 27 254 64 39 25 254 281 SYS-2 1650 64 4	365 27 16 1 44 254 5 15 20 238 282 SYS-2 1650 35 6	395 44 23 238 21 40 13 256 279 SYS-2 1650 13 40	239 23 23 256 347 18 692 324 347 Complet 1650	239 23 14 40 37 324 40 43 5 40 119 156  Complet 1650	239 37 10 47 119 50 6 45 120 167 Complet 1650	239 47 47 120 70 2 72 120 167 Complet 1650	
Downhole Volinitial Reserve Added:  Final Reserve Initial Active Added:  Losses:  Final Active Total Final V DILUTION Interval Type Depth m Daily drilled Daily Dilution Daily Consul	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill-Water other Chemical e Res Mud Seawater Drill-Water other Chemical Solids Control Lost/Dumped DownHole olume	351 37 200 10 34 354 213 99 73 342 376 SYS-2 1650 246 172	395 34 110 4 87 342 61 55 50 254 341 SYS-2 1650 105	395 87 4 27 254 64 39 25 254 281 SYS-2 1650 64	365 27 16 1 1 44 254 5 15 20 238 282 8YS-2 1650 35 6 1010	395 44 23 238 21 40 13 256 279 SYS-2 1650 13 40 1010	239 23 23 256 347 18 692 324 347 Complet 1650 692 365	239 23 14 40 37 324 40 43 5 40 119 156  Complet 1650 40 88	239 37 10 47 119 50 6 45 120 167 Complet 1650 45 56	239 47 47 120 70 2 72 120 167 Complet 1650 72 72	
Downhole Volinitial Reserve Added:  Final Reserve Initial Active Added:  Losses:  Final Active Total Final V DILUTION Interval Type Depth m Daily drilled Daily Dilution Daily Consulnterval Drille	bbl/hr Hrs bbl bbl blume e Act Mud Seawater Drill-Water other Chemical e Res Mud Seawater Drill-Water other other Chemical Solids Control Lost/Dumped DownHole olume  m bbl mption bbl ed m	351 37 200 10 34 354 213 99 73 342 376 SYS-2 1650 246 172 210	395 34 110 4 87 342 61 55 50 254 341 SYS-2 1650 105 114	395 87 4 27 254 64 39 25 254 281 SYS-2 1650 64 4 1010 1433	365 27 16 1 1 44 254 5 5 15 20 238 282 87S-2 1650 35 6 1010 1468	395 44 23 238 21 40 13 256 279 SYS-2 1650 13 40 1010 1481	239 23 23 256 347 18 692 324 347 Complet 1650 692	239 23 14 40 37 324 40 43 5 40 119 156 Complet 1650 40	239 37 10 47 119 50 6 45 120 167 Complet 1650 45 56	239 47 47 120 70 2 72 120 167 Complet 1650 72	
Downhole Volinitial Reserve Added:  Final Reserve Initial Active Added:  Losses:  Final Active Total Final V DILUTION Interval Type Depth m Daily drilled Daily Dilution Daily Consulnterval Drille Interval Dilutinterval Dilutin	bbl/hr Hrs bbl bbl  Dlume e Act Mud Seawater Drill—Water other Chemical Seawater Drill—Water other Chemical Solids Control Lost/Dumped DownHole olume  m h bbl mption bbl ed m ion bbl	351 37 200 10 34 354 213 99 73 342 376 SYS-2 1650 246 172 210 1010	395 34 110 4 87 342 61 55 50 254 341 SYS-2 1650 105 114 1010	395 87 4 27 254 64 64 281 SYS-2 1650 64 4 1010 1433 1.42	365 27 16 1 44 254 5 5 15 20 238 282 87S-2 1650 35 6 1010 1468 1.45	395 44 23 238 21 40 13 256 279 SYS-2 1650 13 40 1010 1481 1.47	239 23 23 256 347 18 692 324 347 Complet 1650 692 365	239 23 14 40 37 324 40 43 5 40 119 156  Complet 1650 40 88 732	239 37 10 47 119 50 6 45 120 167 Complet 1650 45 56	239 47 47 120 70 2 72 120 167 Complet 1650 72 72 849	
Downhole Volinitial Reserve Added:  Final Reserve Initial Active Added:  Losses:  Final Active Total Final V DILUTION Interval Type Depth m Daily drilled Daily Dilution Daily Consulaterval Drille Interval Dilut Rate bbl/m	bbl/hr Hrs bbl bbl  Dlume e Act Mud Seawater Drill—Water other Chemical Seawater Drill—Water other Chemical Solids Control Lost/Dumped DownHole olume  m h bbl mption bbl ed m ion bbl	351 37 200 10 34 354 213 99 73 342 376 SYS-2 1650 246 172 210 1010 1264	395 34 110 4 87 342 61 55 50 254 341 SYS-2 1650 105 114 1010 1369	395 87 4 27 254 64 39 25 254 281 SYS-2 1650 64 4 1010 1433	365 27 16 1 1 44 254 5 5 15 20 238 282 87S-2 1650 35 6 1010 1468 1.45 1692	395 44 23 238 21 40 13 256 279 SYS-2 1650 13 40 1010 1481	239 23 23 256 347 18 692 324 347 Complet 1650 692 365	239 23 14 40 37 324 40 43 5 40 119 156  Complet 1650 40 88	239 37 10 47 119 50 6 45 120 167 Complet 1650 45 56	239 47 47 120 70 2 72 120 167 Complet 1650 72 72	



# Baroid Australia Pty Ltd COMPANY G.F.E. RESOURCES LTD. WELL IONA - 2

## WATER BASE MUD PROPERTIES

Page 1 YEAR 1994

	WELL	IONA -	2		п									20/02		21/02		22/02		23/02		24/02		25/02	1001
		14/02		15/02		16/02		17/02		18/02	·	19/02		_			IN	22/02 IN	IN	23/02 IN	IN	1N	IN	IN	
Sample Location	IN or OUT	IN	IN	IN	IN	_IN_	IN	IN			IN	IN	IN	IN	PIT	IN							24:00	24:00	
Time Sample Taken	hrs	17:45	24:00	15:00	23:00		23:40			ļ	04:30		24:00	11:15		12:45		11:40	19:30		24:00			1650	
Depth	m	125	216	344	482	640	640	640			645	762	823	1045	1052		1133	1215		1297	1404	1520		8.5	
Hole Size	ins	12.2	12.2	12.2	12.2	12.2	12.2	12.2			8.5	8.5	8.5	8.5	8.5	8.5	8.5	8.5	8.5	8.5	8.5	8.5	8.5 40	8.5	
Flowline Temp	°C	29.4	31.1	34.4	38.9	42.8	38.3			ļ	33	33.3	34	37.2		34.4	42.8	42.8	43.9	37.8	42.2	42		- 1	
Weight	ppg	8.7	8.85	8.9	8.9	9	9.3	9.3			8.8	8.85	8.8	8.9	8.9	8.95	9.1	9.2	9.3	9.4	9.35	9.4	9.4	9.4	<del> </del>
Funnel Viscosity	sec/qt	30	41	39	37	43	47	47		ļ	35	35	38	51	38	37	38	39	39	39	39	38	40	40	
600 rpm	1b/100 ft ²	12	47	27	22	30	38	38			21	20	21	48	35	29	30	32	35	40	32	31	36	36	<del> </del>
300 rpm	lb/100 ft ²	10	43	18	16	21	26	26		ļ	16	15	15	38	23	18	19	20	22	25	20	20	24	24	
200 rpm	lb/100 ft ²									<b></b>										<b> </b>				ļ	
100 rpm	lb/100 ft ²									<b> </b>											ļ	<b> </b>	ļ		
6 rpm	lb/100 ft ²									ļ										<b></b>	ļ	<b> </b>			
3 rpm	lb/100 ft ²			<b></b>						<b> </b>									<del></del>	<del> </del>	<del> </del>	ļ		10	-
Plastic Viscosity	сР	2	4	9	6	9	12	12		<u> </u>	5	5	6	10	12	11	11	12	13	1		1	12	12	
Yield Point	lb/100 ft ²	8	39	9		12	14	14		-	11	10	9	28	11	7	8	8	9			9		12	
Gel – 10 sec	lb/100 ft ²	4	25	4	8	7	9	9		ļ	9	10	4	8	2	1	1	1	2			2		6	
Gel – 10 min	lb/100 ft ²	7	31	7	22	25	37	37		-	21	25	14	16	5	2	3	5	7	8	5	8		12	
Gel - 30 min	lb/100 ft ²						ļ			<b> </b>					ļ					ļ	ļ	<b> </b>	21	21	
API Filtrate	ml/30min	N.C.	N.C.	N.C.	20	12.8	11.8	11.8		<u> </u>	N.C.	25	13.9	21	11.3	9.6	8.2	7.5	6.8	6.2	6.1	6.6		6.7	<del> </del>
API Filter Cake	32nd ins			<u> </u>	3	2	2	2		ļ		3	2	3	2	1	1	<u>  1</u>	1	1	1	1 1	1 1	1-1	┼
HPHT Filtrate	ml/30min		ļ	<u> </u>			<u> </u>	<u> </u>				ļ		<u> </u>	ļ	<u> </u>		<u> </u>	<u> </u>	-	-	<b>]</b>		<b> </b>	
HPHT Filter Cake	32nd ins			<u> </u>				<b></b>		_		ļ		<b> </b>	-	ļ		ļ	-	<b> </b>		<b> </b>		<b> </b>	<del> </del>
HPHT Temp	°F				ļ	ļ	ļ	<u> </u>	ļ		<u> </u>	ļ		ļ		<u> </u>	ļ	<b>_</b>	<del> </del>	ļ		<del> </del>		ļ- <u>-</u>	
Solids	% Vol	2.5	3.5	3.7	3.7	4.3	6.8	6.8		<u> </u>	3.4	3.9	3.4	3.6	3.6	3.3	4.5	5.3	6	6.5	6.1	6.2	6.2	6.2	+
Oil 0	.84% Vol			<u> </u>	<u> </u>	ļ		ļ		_		ļ		ļ	-	<u> </u>		ļ		<del> </del>	<del> </del>			<b> </b>	+
Water	% Vol	97.5	96	96	96	95.5	93	93		<b>_</b>	96.5	96					94.2	-	+						+
Sand	% Vol	Tr	Tr	0.25	Tr	Trace	1	1 1			0.1	Trace	0.25	0.15		0.25								Tr	+
Methylene Blue cap	ppb		13	15	15	15		-		<u> </u>	11	11	8				12								
рН	meter	8.1		4		<del></del>	9				11.5	1	9			-	9.5								
Alk. Mud Pm	ml	0.28	0.34	0.5			0.69	0.69		_	1.98	-													
Alk. Filtrate Pf	ml	0.02	2	0.01	0.03	0.03	0.02	0.02	<u> </u>	_	0.43	-				0.06				~				0.1	
Alk. Mf	ml	0.12	0.1	0.06	0.08	0.1	0.12	0.12			0.52		0.16	-						-			_		
Chlorides	mg/Lx10 ³	0.5		_	3,35					_	1.5					41		_		_					
Total Hardness	mg/L	20	370	160	40	10	15	15	1		80		<del> </del>					1							+
Calcium	mg/L		150	100	30	1					70	-						-							
KCL	% Wt Soln		1	0.75	5 0.€	0.5					0.2			1.5						_		<b></b>	3 3		
K+ Ion Conc	mg/Lx10 ³			4.3	3 3.4	2.9	2.3	2.3	4	_	1.1	0.6	1	8.6	9.5	15.2	16.6	15.8	17.8	16.6	6 17.8				
Sulphite Residual	mg/L									<b>_</b>			<del> </del>	┨——	-	-	<u> </u>	<b> </b>			-	5	0 40	40	4
				_		-	<u> </u>	<b>_</b>				J				-								<b> </b>	+
						1				_		<b></b>	<del> </del>					<del> </del>	ļ						+-
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# Baroid Australia Pty Ltd COMPANY G.F.E. RESOURCES LTD.

WATER BASE MUD PROPERTIES

Page 2 YEAR 1**994** 

	WELL	IONA -	- 2	7/02		28/02		01/03		02/03		03/03	I	03/03	- 1										
		26/02						01/03		02/03		00/00		00,00				1							
Sample Location	IN or OUT	IN				IN																			
Time Sample Taken	hrs	09:00			24:00																				
Depth	m	1650			1650									-											
Hole Size	ins	8.5		8.5	8.5	8.5								-											
Flowline Temp	<u>.</u> €																								
Weight	ppg	9.35		9.3	9.3	9.3																			<del>                                     </del>
Funnel Viscosity	sec/qt	38		36	34	34																			<del> </del>
600 rpm	lb/100 ft ²	30		27	25	25																			<del> </del>
300 rpm	lb/100 ft ²	20		17	16	16																			
200 rpm	lb/100 ft ²											ļ		ļ											
100 rpm	lb/100 ft ²																								<del> </del>
6 rpm	lb/100 ft ²																								├─
3 rpm	lb/100 ft ²													ļ											
Plastic Viscosity	cР	10		10	9	9				<u></u>				1											<b>├</b> ─
Yield Point	lb/100 ft ²	10		7	7	7								ļ											—
Gel - 10 sec	lb/100 ft ²	2		2	1	1				ļ				<u> </u>											—
Gel - 10 min	lb/100 ft ²	8		6	5	4								<u> </u>									i		<u> </u>
Gel - 30 min	lb/100 ft ²	12		9	8																				<u> </u>
API Filtrate	ml/30min	6.8		6.8	6.8	6.9																			1
API Filter Cake	32nd ins	1	1 1	1	1	1																			<u> </u>
HPHT Filtrate	ml/30min	╁			<u> </u>																			L	<u> </u>
HPHT Filter Cake	32nd ins	<b>-</b>																							<u> </u>
HPHT Temp	%F	1			ļ																				
Solids	% Vol	5.8	1	5.9	5.9	5.9															<u> </u>				
	.84% Vol	J.0		0.0	J	1																			<u></u>
	% Vol	93		93	93	93		1		1															
Water Sand	% Vol	0.1		0.1					1	1															
		10	-	10						1		1	T												T
Methylene Blue cap		9.7		9				<b> </b>	<b> </b>	1	<b> </b>	1		1											T
pH	meter ml	0.4		0.2			<u> </u>	-	-	<b></b>	1														T
Alk. Mud Pm		0.4		0.1			<u> </u>	1	<b>†</b>				1		1				1						
Alk. Filtrate Pf	ml	0.6		0.1				1	<del>                                     </del>	<b> </b>	1		1	1	<b>†</b>	1									
Alk. Mf	ml							-	-	╁┈┈	-	1	<b>-</b>	-			<b></b>	1	1		1	1			
Chlorides	mg/Lx10 ³	14		13.5					+	╢	_	1	+	1		-	<b>†</b>	1		1			1		1
Total Hardness	mg/L	20		20			+	<b> </b>	+	1-		1	+	$\dagger$	+	1	t				1				1
Calcium	mg/L	20		20		_		-	+		-	╂	+	1	1	1	1	#	-	1		1	1	1	1
KCL	% Wt Soln	2.8		2.7		_		╂	+	-	+	╢	+	-	+	╂	1	1	1	1	1	1	1		T
K+ Ion Conc	mg/Lx10 ³	16.1		15.5	15.5	15.5		╂	+		-	╢	+	-	1	<b> </b> -		1	<del> </del>	1		1			1
Sulphite Residual	mg/L	40	)	<b> </b>	-		+		-	╂		1	+	-	-	<b> </b>	-	-	-	1	+	<b> </b>	<b> </b>	1	+
			-	<b> </b>	-		ļ	╂	-	-		-	-	<b></b>		<b> </b>	<del>                                     </del>	1-	+	1	+	1-	+	1	+
				<u> </u>		_{	1	4		_		┦		4		1		╢	+	┨——		╢	+	╢	+



COMPANY G.F.E. RESOURCES LTD.

WELL IONA - 2

LOCATION OTWAY BASIN, VICTORIA

CONT/RIG CENTURY DRILLING / RIG - 11

BIT RECORD

DATES:

FROM 14-Feb-94

TO 04-Mar-94

BIT NO.	BIT SIZE ins	MAKE	ТҮРЕ	JETS	DPUEL LIN	DPTH OUT m	DRLD m	HRS ON BIT	RATE m/hr	AGG DRLG HRS	WOB x1000		VERT DEV. deg.		PUMP RATE bbl/min	MUD WT ppg	VIS	CONDITION & REMARKS
1	12.25	Varel	L114	1 x 18, 2 x 20	16	320	304	12	25.3	12	15/20	120	0.25	550	9.89	8.8	40	1–3–In (RR bit) Kick–off pt. Change bit and BHA.
2	12.25	Security	S33SF	3 x 16	320	640	320	20	16	32	15/20		18.5	1575	11.58	9	43	1-2-1/8 Casing point.
2RR	12.25	Security	S33SF	3 x 20	640	640								1100	12.1	9.3	47	1-2-1/8 Clean out trip. Ream tight hole. Set 9 5/8"
3	8.5	Varel	ETD 417	2 x 10, 1 x 11	640	781	141	5	28.2	37	5/8	130	19.2	1400	7.19	8.8	35	1 – 1 – In Change BHA. P/up motor and MWD.
3RR	8.5	Varel	ETD 417	1 x 10, 2 x 12	781	1052	271	13.5	20.1	50.5	0/20	40		1425	7.26	8.9	38	
3RR	8.5	Varel	ETD 417	1 x 10, 2 x 12	1052	1268	216	32	6.8	82.5	0/15	110	2.5	1325	7.4	9.3	39	1-1-In Change bit and BHA to drill Waare.
4	8.5	Varel	ETD 417	3x12	1268	1650	382	31.5	12.1	114	25	90	0.75	1225	7.4	9.4	39	1-1-1 T.D.



COMPANY G.F.E. RESOURCES LTD.

WELL IONA - 2

LOCATION OTWAY BASIN, VICTORIA

CONT/RIG CENTURY DRILLING / RIG - 11

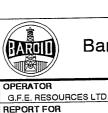
DIRECTIONAL SURVEYS

PAGE-1

M'	Dm	TVD m	INCL°	DIR °	DISP m
	48.7		0.75		
•	84.7		0.5		
1	19.5		0.5		
. 1	55.8		0.5		
1:	91.9		0.5		
	229		0.25		
	257		0.25		
	286		Zero		
	393	392.8	6.7	188.9	
	422	421.5	10.1	179.8	
	461	459.6	14.8	159.9	
	499	496.2	15.8	148.6	
	538	533.6	17.6	145.9	
	586	579.1	18.7	145.2	
	622	613.3	18.5	143.1	
	660		17.75	142.5	
	698		18.25	142.5	
	736		19.25	145.4	
	813	795	18.5	148.4	
8	51.4	833	15.5	144.5	
	89.7	872	12.4	139.1	
	18.3	900	11.1	137.5	
Ū	965	947	10	138.7	
	986	9.2	9.2	140.1	
	1042	1024	8.2	143.1	
	1096		5.5	140	
	1165		3.25	136	
	1250		2.5	143	
	1345		1.5	153	
	1450		1	151	
	1632		0.75	136	

**GRAPHS** 

# **DAILY MUD REPORTS**



KEN SMITH

Impact lb f

Depth

Weight

Sample Location

Flowline Temp

Funnel Viscosity

Plastic Viscosity

Yield Point

API Filtrate

Solids

Sand

рΗ

KCL

HPHT Filtrate

Dissolved Salts

Alk. Mud Pm

Chlorides

Rheometer lb/100 ft2

Oil/Water Content

Methylene Blue cap

Alk. Filtrate, Pf/Mf

Total Hardness/Calcium

ALAN SEARLE

API/HPHT Filter Cake

Time Sample Taken

WELL NAME AND NO.

Current

IN or OUT

hrs

m

°C

cF

Gels 10 sec/10min/30 min lb/100 ft²

ppg

sec/qt

lb/100 ft²

ml/30min

ml/30min

32nd ins

% Vol

% Vol

% Vol

% Vol

ppb meter

ml

mi

mg/L

mg/Lx10

% Wt Solr

IN

125

29

30

8

4/7/-

N.C

2.5

Tr

-/97.5

8.1

0.28

0.02/0.12

12/10

MELBOURNE

0.5

20/-

8.70

#### Baroid Australia Pty Ltd

up to 24:00 hrs, 14/2/94 MUD REPORT NO. TVD 232 DEPTH-m MD 232 DATE 15/2/94

ACTIVITY START DATE Drilling 12 1/4" hole 14-Feb-94

CONTRACTOR / RIG COUNTRY **AUSTRALIA** CENTURY DRILLING / RIG - 11 TOWNSHIP REPORT FOR PORT CAMPBELL RICK GIDDENS

LOCATION

spm_bbl/min

0-25 lb/100 ft2

0.75 %

4.812

5.076

92

OTWAY BASIN, VICTORIA **PUMP DATA** CASINGS DRILLING STRING BIT DATA Eff % bbl/stk ins x ins Length m Size ins Pump Make OD ins ID ins Size 12.250 ins 95 0.0523 National 7-P 7.75 5.5 12.9 Riser Set @ 3.826 Type Varel L114 4.5 Pipe 1 95 0.0705 National 8-P 6 8.5 Set @ 55.4 Nozzles 32nds Pipe 2 4.5 2.75 Set @ Pipe 3 20 18

FIELD OR BLOCK NO.

232

216

31

8.85

41

4

39

25/31/-

N.C.

3.5

0.5

-/96.0

13

8.0

0.34

-/0.10

5.4

370/150

47/43

1.0

Tr

TOTAL bbl/min 9.888 Pump Press 550 ps Set @ 163.7 6.25 2.25 CIRCULATING DATA Set @ MUD VOL bbl Col 2 m/min Total circ 56 mins Downhole 91 Set @ Noz Area 0.86 ins² **OPEN HOLE SECTIONS** 23.9 Active Bottoms up 9 mins DP 465 Set @ Sect 1 TFA insa Surface-bit - mins Set @ Total Circ 556 Line Sect 2 47.0 NV m/sec ECD ppg Rise

> MUD PROPERTIES VIS WEIGHT <9.2 ppg IN API Filt N.C. HTHP 17:45 24:00

Top @

BY AUTHORITY REMARKS Commenced drilling with water, relying on native clays for viscosity. Cuttings remained relatively firm and discrete through Gellibrand Marl down to 125m, delayed addition of KCI to this depth.

MUD PROPERTY SPECIFICATIONS

40-50 sec

ml

YP

KCL

High ROP between 125 and 151m resulted in cuttings overload in annulus - flowline blocked, mud rings forming. Lowered ROP by reducing weight on bit, no further problems.

KCI caused clays to flocculate, no need to add lime other than one sack used higher up hole. pH low due to minimal lime use, will add caustic soda to increase pH to 9+.

Ran desander and desilter while circulating, dumping and diluting as necessary. Clay and solids content gradually increasing. Cuttings quality improved after addition of KCI.

Complete rigging up. Rig inspection by Mines Dept. Spud in at 12:00 hours. Drilled 12 1/4" hole from 16 - 232m, taking surveys approx every 35m. High ROP through Gelibrand Marl caused annulus to load up with cuttings, resulted in mud rings and blocked flowline at 151m; circulated hole clean, reduced weight on bit to lower ROP from 151m.

600 rpm/300 rpm 200 rpm/100 rpm 6 rpm/3 rpm

INVENTORY AND CONSUMPTION CONSUMPTION COST MUD TYPE Native Clav REC USED PRODUCT DESCRIPTION Additions bbi SOLIDS CONTROL EQUIPMENT 236 Barite,sx 50 kg Sea W screen size Make 402 25 kg Barite,sx 800 12 Drill W Shaker 1 TRITON 3 x 50 109 25 kg 10 KCL, Tech(sx) other 490.96 Shaker 2 50 kg 17 KCL, Tech(sx) other 8.04 Shaker 3 19 Lime Barite Shaker 4 Chemicals ppg bbl/hr hrs bbi bbl 72 Losses 9.4 6 Desander 114 42 Sol. Con. 10.7 3.5 12 Desilter 1 134 Lost/Dumped Desilter 2. Down Hole Centrifuge 103 Newhole Centrifuge 2 556 **NET GAIN** 248 Discharged Solids Control Effic

**CUMULATIVE COST** DAILY COST WAREHOUSE OFFICE **BAROID Engineer** 643.40 A\$ A\$ 643.40

THE RECOMMENDATIONS MADE HEREON SHALL NOT BE CONSTRUED AS AUTHORIZING THE INFRINGEMENT OF ANY VALID PATENT, AND ARE MADE WITHOUT ASSUMPTION OF ANY LIABILITY BY BAROID DRILLING FLUIDS, INC OR IT'S AGENTS, AND ARE STATEMENTS OF OPINION ONLY.

2505	DIE DIE			SURVE	Y DATA			SOLIDS AN	ALYSIS		TIME BREAKDO	WN	hrs
	RVE PITS	1-1-1	MD m	TVD m	INCL°	DIR °	DISP m	Low Grav. Solids	% Vol	3.5	Drilling		9
NO	TYPE	bbl	48.7	IVUIII	0.75			Low Grav. Solids	ppb	31.8	Circulating		0.5
6	Pill Tank		84.7		0.5			High Grav. Solids	% Vol	0.3	Reaming In		
7	Trip Tank		119.5	<del> </del>	0.5			High Grav. Solids	ppb	4.4	Reaming out		
<b> </b>			155.8		0,5			ASG of Solids	g/cc	2.60	Tripping		
-	ļ		191.9		0.5			Cuttings Volume	bbl	103.0	Survey		2.5
			191.9	<del> </del>	0.5			Interval Dilution	bbl/m	1.2	Rig up		9
<u> </u>			<b></b>				+	Interval Consumption	bbl/m	3.7	Other		3
	1		ļ								AVE ROP 1	m/hr	24

						<del></del>						4.00 6		15/2/94	
<b>1</b>				_			MUD REP	ORT NO	-T		p to 2				
RAROIII	Baroid	d Au	ıstrali	ia Pt\	/ Ltd		DATE 1	6/2/94	C	DEPTH	-m N	MD 500	)	TVD 497	7
	<b>D</b> 01. 01.			•			START DA	ATE		ACTIVI					
							14-Feb-9	94			_	hole, t	ouilding a	angle.	
PERATOR				CONTRAC	CTOR / RIG	ì				COUNT					
G.F.E. RESOURCE	S LTD.			CENTUR	Y DRILLING	/ RIG - 1	1			AUSTE					
EPORT FOR			F	REPORT	FOR				i '	TOWNS		2011			
KEN SMITH				RICK GIE						OCAT	CAMPE	DELL			
VELL NAME AND	NO.		1	FIELD OR	BLOCK N	0.			1		Y BASI	N VIC	TORIA		
IONA - 2				PPL - 2							UMP E		TOTAL		
BIT DATA	DF	RILLING	STRING	<del></del>		ASINGS	James m	Pump M	lake	ins x			bbl/stk	spm b	obl/mir
Size 12.250 ins	OD	ins			Size ins		Depth m	Nationa		5.5	7.75	95	0.0523	100	5.2
ype Sec S33SF	Pipe 1	4.5	3.826	254.7	Riser	Set @		Nationa		6	8.5	95	0.0705	90	6.34
Nozzles 32nds	Pipe 2	4.5	2.75	55.4		Set @		INALIONA	10-1		- 0.0				
16 16 16	Pipe 3					Set @		Pump P	ress 1	475 psi		TOT	AL bbl/m	in	11.57
	Col 1	6.25	2.25	125.3		Set @ Set @		MUD V		bbl	CIRCI	ULATI	NG DAT	A	
	Col 2	8	2.25	64.6		Set @		Downho			Total ci			AV m	n/min
Noz Area 0.59 ins²		EN HOL	E SECTIO	NS		Set @		Active			Bottom	s up 1	6 mins	DP	2
rFA ins²	Sect 1				Liner	Set @		Total Ci	rc 5	67	Surface	-bit 1	mins	DC	42.
VV m/sec 80.5	Sect 2			500	Liner	Top @		Reserve		i	ECD pr	og	8.92	Riser	
mpact lb f 591	Current		12.25	500 AUD PRO	DEDTIES	rup w		N					ATIONS	3	
				MUD PHO	IN		WEIGHT	<9.2 p			0-50 s		YP	0-25	b/100
Sample Location		r OUT	IN		23:00		API Filt	<15 m		HTHP	r	nl	KCL	.75 9	%
Time Sample Taker			15:00	<del> </del>	482		BY AUTHO			/lud pro	gram				
Depth	m		344		39		REMARK	S							
Flowline Temp	<u>°C</u>		34		8.90		Ralied on	native cl	lays for	viscos	ity prior	to trip	ping. Aft	er trip be	egan
Weight	ppg		8.90		37		adding pr	emix with	h AQUA	AGEL a	nd CM	C-EH	V to mair	ntain visc	cosity
Funnel Viscosity	sec/	/qt	39		6		and reduc	e filtrate	throug	h Dilwy	n sand	is.			
Plastic Viscosity	cP_	20.00	9		10		Caustics	oda adde	ed to ra	ise pH	to 9.				
Yield Point		00 ft²	9 4/7/-		8/22/-		Hydraulic	paramet	ters det	termine	d by di	rection	nal driller	s require	ements
Gels 10 sec/10min/		00 ft²			20.0		3 x 16/32	nozzles.	550 gr	m circi	ulating	rate. A	ctual gpi	n lower	due to
API Filtrate		30min	N.C.		20.0		pressure	limtation	s.						
HPHT Filtrate		30min			3/-		Bunning (	desnder .	and de	silter w	hile circ	culating	g. Sand	content o	only a
API/HPHT Filter Ca		id ins			3.7		trace, des	nite qua	ntity of	sand r	emove	d from	hole. So	me losse	es ove
Solids	% V		3.7		0.3		shaker so	reens du	ue to he	eavv sa	nd load	i.			
Dissolved Salts	% V		0.3		-/96.0		101101101			•					
Oil/Water Content	% V		-/96.0		_/90.0 Tr		1								
Sand	% V		0.3		1		1								
Methylene Blue ca			15		15		1								
pH	met	ter	8.1		9.0 0.86		ACTIVIT	Y							
Alk. Mud Pm	<u>ml</u>		0.50		0.03/0.08		Drilled to	kick-off	f point a	at 320m	n, taking	g surve	eys every	35m. C	irculate
Alk. Filtrate, Pf/Mf	<u>mi</u>		0.01/0.06		3.4		hottoms	un. POO	H. Cha	naed b	it and r	nade u	ıp kick-	off assen	nbly w
Chlorides		/Lx10 ³	3.9 160/100		40/30		downhole	motor a	and MV	VD tool:	; 1.15 d	leg ber	nt angle i	n motor.	RIH, ì
Total Hardness/Ca		/∟ Wt Soln	0.8		0.6		bridge at	293m. R	Reamed	to 305	m, ran	to bott	om. Cric	ulated a	ınd
KCL		/Lx10 ³	4.3		3.4		oriented	motor. D	rilled to	500m	buildin	g angl	e; no rot	ation.	
K+ Ion Conc	mg,	/LX10°	4.5		1		1								
					<del> </del>		1								
							1								
							1				,				
	600 mm/2	00 mm	27/18		22/16		1								
Rheometer	600 rpm/3 200 rpm/1		21,10				1								
lb/100 ft ²	6 rpm/3 rp			<del> </del>			1								
	o rpm/3 rp	RYAND	CONSU	MPTION			1								
PRODUCT DESC		ALL AIN	USED	REC	BAL	COST	MUD TY		AQUAG					UMPTIC	
	50 kg				236		SOLIDS	CONTR					Additi		bbl
Barite,sx	25 kg				402		<u></u>	Mak			size		Sea W		1
Barite,sx	25 kg 25 kg		32		488	458.56	Shaker 1	TRITON	١	3 x 50		14.5	Drill W	<u> </u>	2
AQUAGEL,sx	25 kg 25 kg		7		33	227.01						<u> </u>	other		<del> </del>
CAUSTIC Soda	25 kg 25 kg		10		70	1066.1		3				ļ	other		
CMC-EHV	ZJ NY		1				Shaker 4			L			Barite		-
				<u> </u>					ppg	bbl/hr		bbi	Chemi		
			<del> </del>		+		Desande		14.3	7.5					bbl
							Desilter	1	14.6	3.5	14	49			1
			1			T	Desilter :	2.						umped	<u> </u>
						1	Centrifuç	ge 1				ļ	Down		
						1	Centrifuç	ge 2				ل	Newho		1
			<del> </del>										NET		<del>  _</del>
			T				Solids C					%	Disch		1 2
PAROID F	ngineer		OFFICE		WAREHO	USE			LYCO	ST		CUM	ULATIVE	COST	
BAROID E	ignicei		J. 1 104				1	A &	17F4	67		A\$	2395	.07	
ALAN SEAF	RLE		MELBOUR	RNE			1	A\$	1751	.07		ДΨ	2030		
1			03 - 621	3311											
Tel. 03 - 787 1: THE RECOMMEND		E HEREC	NI CHALL N	OT BE COM	ISTRUED AS	AUTHORIZ	ING THE IN	FRINGEN	MENT OF	ANY V	ALID PA	TENT,	AND ARE	MADE	
THE RECOMMEND.	TION OF ANY	יובתבע	LA BA BABU	ID DRILLIN	G FLUIDS. IN	C OR IT'S	AGENTS, AN	ID ARE S	TATEME	NTS OF	OPINIO	ON ONL	.Y		
	TION OF ANY	UMBILI I	טוואטוטו												_
WITHOUT ASSUMP								SOLI	OS ANA	ALYSIS	;	TIME	BREAK	DOWN	hr
			SHEV	EA DVIV				O O LLIC				_			
RESERVE PITS	bbi Is.	4D m	_	INCL°		DISP m	Low Gra	v. Solids		% Vol		Drilli	ng		
RESERVE PITS NO TYPE		MD m	TVD m	INCL°	DIR °	DISP m			3	% Vol ppb	3.5 31.8	Circu	ng ulating		
RESERVE PITS  NO TYPE  6 Pill Tank	bbi M 27	229	TVD m		DIR °	DISP m	Low Gra	v. Solids	3	% Vol	3.5 31.8 0.2	Circu Rear	ng ulating ming In		1
RESERVE PITS NO TYPE			TVD m	INCL° 0.2	DIR °	DISP m	Low Gra	v. Solids v. Solids	s  s	% Vol ppb	3.5 31.8 0.2 2.9	Circu Rear	ng ulating ming In ming out		

ASG of Solids

**Cuttings Volume** 

Interval Dilution

Interval Consumption bbi/m 2.2

393

422

461

499

392.8

421.5

459.6

496.2

6.7

10.1

14.8

15.8

188.9

179.8

159.9

148.6

g/cc 2.70

bbi/m 1.0

bbi 128.0

Tripping

AVE ROP

Survey

Other

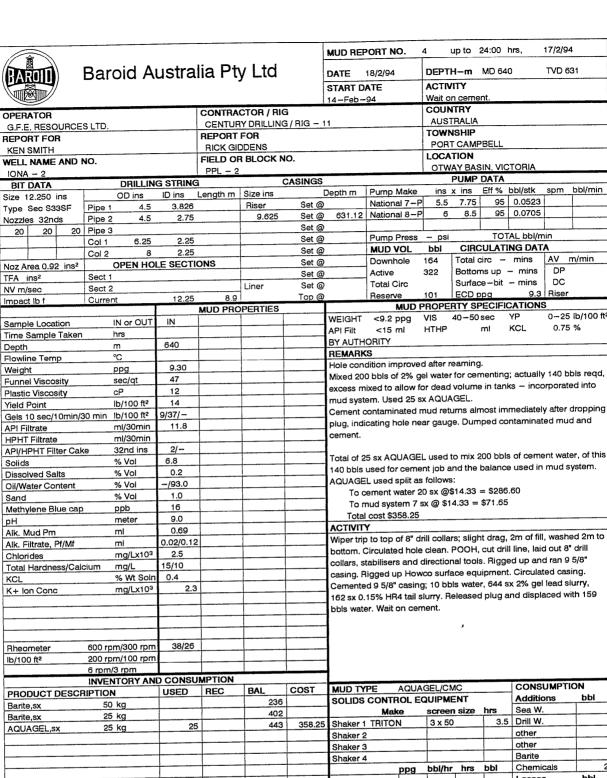
1.5 3.5

m/hr 20.62

					A	AUD REPO	ORT NO.	3	up t	0 24:0	00 hrs	, 10/	2/94	
Baroid Australia Pty Ltd							7/2/94	DE	PTH-	n MC	640	T	/D 631	
AROLL) E	saiolu Au	٠		START DA	TART DATE			ACTIVITY						
					1	4-Feb-9	eb-94 Circulating hole.							
		TOR / RIG				1 - 1	UNTR							
PERATOR S.F.E. RESOURCES	: LTD	Y DRILLING /	RIG - 11				USTRA							
PORT FOR	) L1U.	FOR							3.1.					
EN SMITH	DENS													
ELL NAME AND N	IO.	BLOCK NO					YAWT		VICTO	RIA				
ONA - 2			PPL - 2	C	SINGS					MP DA				
BIT DATA	DRILLING		ength m	Size ins		epth m	Pump Ma	ke	ins x it	ns Ef	f% bb			bl/min
ze 12.250 ins			384.3	Riser	Set @		National 7	'-P		.75		.0523	110	5.753
pe Sec S33SF	Pipe 1 4.5 Pipe 2 4.5	3.826 2.75	55.4	11.007	Set @		National 8	3-P	6	8.5	95 0	.0705	90	6.345
ozzles 32nds	Pipe 2 4.5 Pipe 3	2.70			Set @						TOTAL	. bbl/min	L	12.098
20 20 20	Col 1 6.25	2.25	148.5		Set @		Pump Pre			IBCUI		DATA		
	Col 2 8	2.25	51.8		Set @		Downhole				49 mir		V m	/min
oz Area 0.92 ins²	OPEN HOL	E SECTIO	NS		Set @		Active	32	1 -		up 21 i		DP	29.2
FA ins²	Sect 1				Set @ Set @		Total Circ		- 1		-bit 2 n		DC	44.1
V m/sec 53.8	Sect 2			Liner	Top @		Reserve			CD ppg			Riser	
npact lb f 432	Current	12.25	640	PERTIES	س رور،		MU	JD PRO				TIONS		. 465 "
	151 01.17	IN	MUD FAC	IN		WEIGHT	<9.2 pp		_	-50 se				b/100 f %
ample Location	IN or OUT	10:15		23:40		API Filt	<15 mi		THP	m	ı K	CL.	0.75	/0
ime Sample Taken	hrs m	640		640		BY AUTH		Mı	ud Prog	ram				
epth Tomp		43		38		REMARK	S		LIV/ n==	miv to	maintai	n rheolo	gy and	d reduc
lowline Temp Veight	ppg	9.00		9.30		Added AQUAGEL/CMC – EHV premix to maintain rheology and refiltrate to < 15 ml by casing point.								
unnel Viscosity	sec/qt	43		47		Timbe bal	in Dilwyn	format	tion whi	le runr	ing in,	from kicl	off po	int at
Plastic Viscosity	сР	9		12		11gnt 11016	1m and a	nain fro	m 408	- 524n	n. Tight	hole ag	ain thr	ough
rield Point	lb/100 ft ²	12		14			320 – 351m and again from 408 – 524m. Tight hole again through Pebble Point from 609 –640m.							
Gels 10 sec/10min/	30 min lb/100 ft ²	7/25/-		9/37/-		1	and closed out nill tank and suction tank, in preparation to							
API Filtrate	ml/30min	12.8		11.0			sel water for coment ich. Small leak between desilter tark and							
HPHT Filtrate	ml/30min	2/-		2/-		was table content and mud weight up after trip, also sailu								
API/HPHT Filter Cal	ke 32nd ins % Vol	4.3		6.8		content increased; desander/desilter not run while reaming to minimse								
Solids	% Vol	0.2		0.2		content incleased, described in desilter suction pit aggravates lea aeration and in case agitation in desilter suction pit aggravates lea No downhole losses recorded while out of hole.							o ican	
Dissolved Salts Oil/Water Content	% Vol	-/95.5		-/93.0		No dowr	hole losse	es reco	raea wi	ille out	UI HOIC	••		
Sand	% Vol	Trace		1.0		1								
Methylene Blue car	o ppb	15		16		-								
pН	meter	9.0		9.0		ACTIVIT	Y							
Alk. Mud Pm	ml	0.74	-	0.69			0.4/48 bolo	from 5	500 -64	i0m, bi	uiilding	angle ar	d ther	n maint
Alk. Filtrate, Pf/Mf	ml	0.03/0.10	<del> </del>	0.02/0.12 2.5		1	10 E dog	Reach	ed casi	na poi	nt at 64	om, circi	Jiateo	DOLLOIN
Chlorides	mg/Lx10 ³	2.8	<del> </del>	15/10		1		ant at A	75m ni	ck up l	celiv an	a pumpe	ea out	i siriyi
Total Hardness/Ca		10/10 0.5		0.4		1	Continued pulling out with tight hole from 456 – 379m. Service dow hole assembly, laid out directional tools. Made up BHA for clean out							
KCL	% Wt Soln mg/Lx10 ³	2.9		2.3		hole ass	embly, lai	d out d	irection	ai tools	. Made	up bna	rom 3	20 - 35
K+ Ion Conc	mg/cx10					trip. RIH	, unable to 24 and 60	get th	rough K	ickoπ [	ooini. H	Circula	te hal	e clean
						408 – 5	24 and 60	9 -640	m; reco	orueu c	)	000		
						-				,				
						-1								
Rheometer	600 rpm/300 rpm	30/21		38/26		1								
lb/100 ft²	200 rpm/100 rpm	·				1								
	6 rpm/3 rpm	2 00101	IMPTION			┪								
	INVENTORY AN	USED	REC	BAL	COST	MUD T			EL/CM			CONSU		ON bbl
PRODUCT DESC		USED	11.20	236		SOLID	CONTR	OL EQ	UIPME	NT		Additio Sea W.	ris	וטט
Barite,sx	50 kg 25 kg	+		402		<b>_</b>	Make		screen	size	nrs +e	Drill W.		1
Barite,sx AQUAGEL,sx	25 kg	20	0	468			1 TRITON		3 x 50		10	other		<del>                                     </del>
Caustic Soda	25 kg		3	30							<del>                                     </del>	other		
CMC-EHV	25 kg		2	68							l	Barite		
EZ SPOT	208 lt			2 2	<del> </del>	Shaker		ppg	bbl/hr	hrs	bbl	Chemic	ais	
						Desand		12.1	7.5	10	75	Losses		bbl
					<del> </del>	Desilte		12.6	3.5	10	35			
				_		Desilte						Lost/Du		1
					<del>                                     </del>	Centrif					ļ	Down I		
1		-		_	1	Centrif		L	<u></u>			Newho		-
												NET L	_ರಾವ	
											9/		hanne	1 .
						Solids	Control Ef	fic. LY CO	CT.		%	Discha		

WITHOUT ASSUMPTION OF ANY LIABILITY BY BAROID DRILLING FLUIDS, INC OR IT'S AGENTS, AND ARE STATEMENTS OF OPINION ONLY. TIME BREAKDOWN hrs SOLIDS ANALYSIS SURVEY DATA 10 RESERVE PITS % Vol 6.4 Drilling DIR ° DISP m Low Grav. Solids INCL° bbl MD m TVD m ppb 58.2 Circulating NO TYPE 6 Pill Tank Low Grav. Solids 17.6 145.9 5 538 533.6 Reaming In % Vol 0.4 High Grav. Solids 145.2 18.7 586 579.1 Reaming out 7 Trip Tank High Grav. Solids ppb 5.9 18.5 143.1 613.3 Tripping g/cc 2.70 ASG of Solids 1 67.0 Other Cuttings Volume bbl Interval Dilution bbl/m 1.0 Interval Consumption bbl/m 2.0 AVE ROP m/hr

THE RECOMMENDATIONS MADE HEREON SHALL NOT BE CONSTRUED AS AUTHORIZING THE INFRINGEMENT OF ANY VALID PATENT, AND ARE MADE



17/2/94

TVD 631

spm bbl/min

AV m/min

0-25 lb/100 ft3

0.75 %

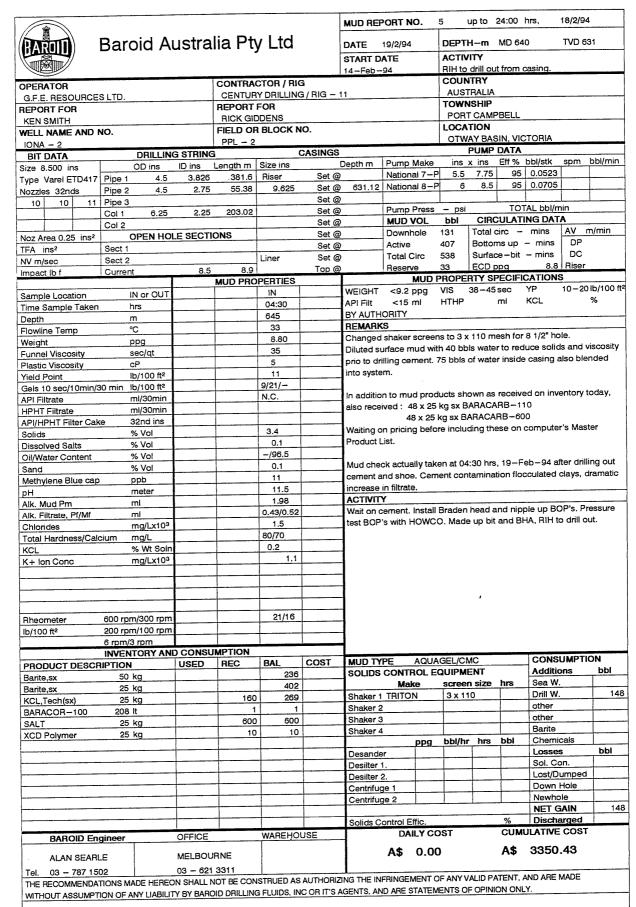
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	INVENTORYA	MUD TYPE AQUAGEL/CMC					CONSUMPTION					
PRODUCT DESCRIPTION		USED	REC	BAL	COST	MUD TYPE				1		
				236		SOLIDS CONT	QUIPME	NT		Additions	bbl	
Barite,sx				402		Ma	screen size		hrs	Sea W.		
Barite,sx	25 kg	25		443	358 25	Shaker 1 TRITO	ON	3 x 50		3.5	Drill W.	i
AQUAGEL,sx	25 kg	25		440	000.20	Shaker 2					other	
				<del>                                     </del>		Shaker 3					other	
						Shaker 4					Barite	
							ppg	bbl/hr	hrs	bbl	Chemicals	2
		_		<del></del>		Desander					Losses	bbl
						Desilter 1.					Sol. Con.	
						Desilter 2.					Lost/Dumped	172
			<b></b>		1	Centrifuge 1					Down Hole	
						Centrifuge 2					Newhole	
					<del> </del>					NET LOSS	170	
			-	-	<del> </del>	Solids Control			%	Discharged	172	
RAROID Engineer OFFICE				WAREHOUSE		DAILY COST			CUMU	CUMULATIVE COST		

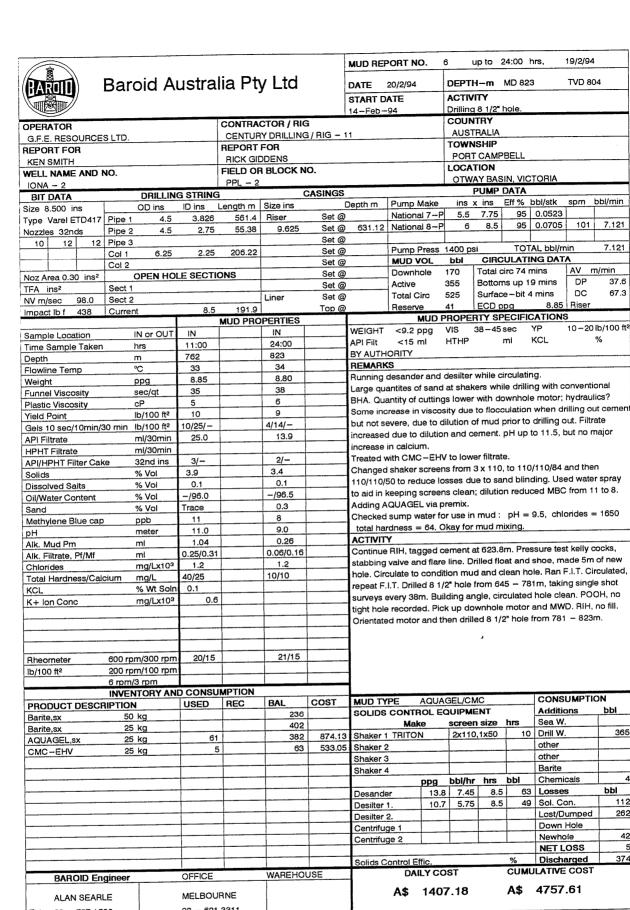
**BAROID Engineer** OFFICE A\$ 3350.43 A\$ 358.25 MELBOURNE ALAN SEARLE 03 - 621 3311 03 - 787 1502

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RESERVE PITS SURVEY DATA							SOLIDS AN	ALYSIS		TIME BREAKDOWN	hrs	
		bbl	MD m	TVD m	INCL°	DIR °	DISP m	Low Grav. Solids	% Vol	6.4	Drilling	
NO	TYPE		IND III	140				Low Grav. Solids	ppb	58.2	Circulating	1.5
6	Pill Tank	68	<del> </del>					High Grav. Solids	% Vol	0.4	Reaming In	
7	Trip Tank	33						High Grav. Solids	ppb	5.9	Reaming out	
			ļ					ASG of Solids	g/cc	2.70	Tripping	9.5
							<del> </del>	Cuttings Volume	bbl		Run & cmt. csg.	6.5
ļ							1	Interval Dilution	bbl/m	1.3	Wait on cmt.	4
				<del></del>	<del> </del>			Interval Consumption	bbl/m	2.0	Other	2.5
ļ			<del> </del>		<del> </del>						AVE ROP m/hr	



TIME BREAKDOWN hrs SOLIDS ANALYSIS SURVEY DATA RESERVE PITS Low Grav. Solids DIR ° DISP m % Vol 3.4 Drilling INCL NO TYPE bbl MD m TVD m Circulating Low Grav. Solids ppb 30.9 Pill Tank Reaming In High Grav. Solids % Vol 33 Trip Tank Reaming out High Grav. Solids ppb 6 g/cc Tripping ASG of Solids 4 bbl Wait on cmt **Cuttings Volume** Nipple up BOP 10 bbl/m Interval Dilution 4 Test BOF bbl/m Interval Consumption m/hr AVE ROP



bbl/min

7.121

7.121

37.6

67.3

bbl

bbl

365

262

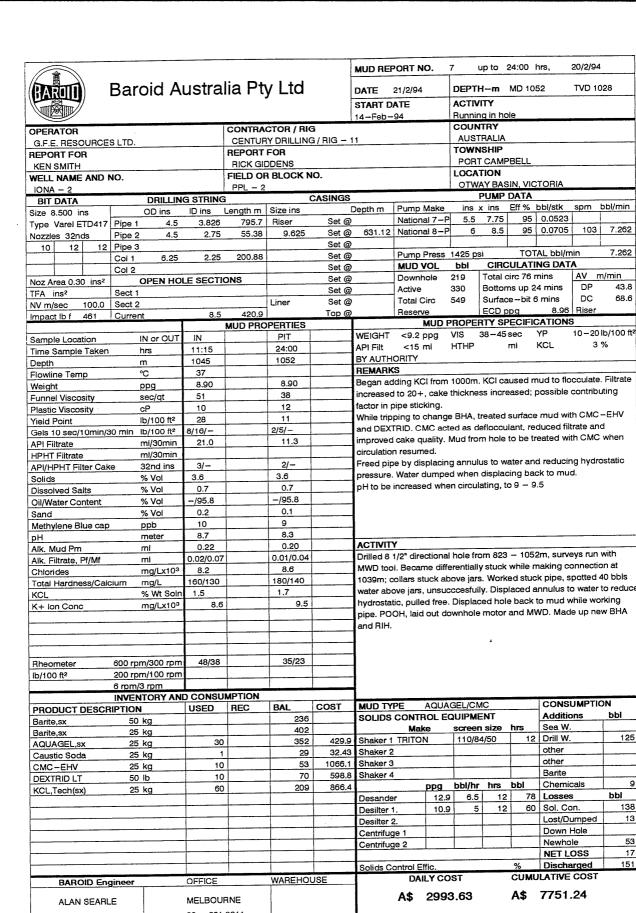
42

5

374

03 - 787 1502 THE RECOMMENDATIONS MADE HEREON SHALL NOT BE CONSTRUED AS AUTHORIZING THE INFRINGEMENT OF ANY VALID PATENT, AND ARE MADE WITHOUT ASSUMPTION OF ANY LIABILITY BY BAROID DRILLING FLUIDS, INC OR IT'S AGENTS, AND ARE STATEMENTS OF OPINION ONLY.

2505	RVE PITS			SURVE	Y DATA			SOLIDS AN	ALYSIS	S	TIME BREAK	DOWN	hrs
NO	TYPE	bbl	MD m	TVD m	INCL°	DIR °	DISP m	Low Grav. Solids	% Vol	3.4	Drilling		7
	Pill Tank	41	660	100	17.75	142.5		Low Grav. Solids	ppb	30.9	Circulating		1.5
7	Trip Tank	41	698		18.25	142.5		High Grav. Solids	% Vol		Reaming In		
<del></del>	Inp rank		736		19.25	145.4		High Grav. Solids	ppb		Reaming out		
<u></u>			813		18.5	148.4		ASG of Solids	g/cc	2.60	Tripping		9
			- 0.0					Cuttings Volume	bbl	42.0	Survey		1.5
			<del> </del>					Interval Dilution	bbl/m	2.0	Other		5
	<del> </del>							Interval Consumption	bbl/m	2.8			
	<del> </del>			-							AVE ROP	m/hr	26.14



103

DP

DC

7.262

7.262

43.8

68.6

125

9

138

13

53

17

151

bbl

m/min

3 %

03 - 621 3311 03 - 787 1502 THE RECOMMENDATIONS MADE HEREON SHALL NOT BE CONSTRUED AS AUTHORIZING THE INFRINGEMENT OF ANY VALID PATENT, AND ARE MADE WITHOUT ASSUMPTION OF ANY LIABILITY BY BAROID DRILLING FLUIDS, INC OR IT'S AGENTS, AND ARE STATEMENTS OF OPINION ONLY.

ргег	RVE PITS			SURVE	Y DATA			SOLIDS AN	ALYSIS	TIME BREAKDOWN	hrs
NO			MD m	TVD m	INCL°	DIR °	DISP m	Low Grav. Solids	% Vol 3.6	Drilling	11.5
6		001	851.4		15.5	144.5		Low Grav. Solids	ppb 32.	8 Circulating	0.5
7	Trip Tank		889.7	872	12.4	139.1		High Grav. Solids	% Vol	Reaming In	
<b>-</b> -	TIP TAIK		918.3	900	11.1	137.5		High Grav. Solids	ppb	Reaming out	
<b></b>			965	947	10	138.7		ASG of Solids	g/cc 2.6	0 Tripping	7.5
			986	9.2	9.2	140.1		Cuttings Volume	bbl 53.	0 Work stuck pipe	4
			1042	1024	8.2	143.1		Interval Dilution	bbl/m 1.3	Oyher	0.5
<del></del>			10-12					Interval Consumption	bbl/m 1.6		
			<del> </del>	<b></b>						AVE ROP m/hr	19.91

- ISI 1	_	۰., ۸	المسلسان	- D+	املا ا	-		ORT NO.	8	F	24:00		TVD	
PAROID)	Baro	id Al	ustral	ıa Pty	Lta	L		22/2/94		TH-m	MD 1	133	100	
							START DA		ACTI	VII Y ng 8 <u>1/2</u>	hole.			
PERATOR			17	CONTRAC	TOR / RIG		14-1-eb	3-		NTRY				
DPERATOR G.F.E. RESOURCE	S LTD.				Y DRILLING		1			TRALIA				
EPORT FOR				REPORT F						' <b>NSHIP</b> RT CAM				
KEN SMITH				RICK GID	BLOCK NO					ATION	POLLE			
VELL NAME AND P	10.			PPL - 2	BLUCK N	J.					SIN, VI	CTORIA		
IONA - 2 BIT DATA	E	RILLING	G STRING		C	CASINGS					DATA			
ize 8.500 ins	0	D ins	ID ins L	ength m			Depth m	Pump Mak		x ins		bbl/stk 0.0523	1	bbl/mir
ype Varel ETD417		4.5	3.826		Riser	Set @ Set @	631.12	National 7- National 8-						7.40
lozzies 32nds	Pipe 2	4.5	2.75	55.38	9.625	Set @		Hadionaro	-					
10 12 12	Pipe 3 Col 1	6.25	2.25	200.88		Set @		Pump Pres	s 1250			TAL bbl/r		7.40
	Col 2					Set @		MUD VOL	bbl		circ 84	ING DAT	AV n	o/min
loz Area 0.30 ins²	1	PEN HOL	LE SECTIO	INS		Set @		Downhole Active	236 386	1		26 mins	DP	44.
FA ins²	Sect 1				Liner	Set @ Set @		Total Circ	622	1	•	6 mins	DC	7
IV m/sec 101.9 mpact lb f 490	Sect 2 Current		8.5	501.9	Linei	Top @		Reserve	71	ECD			Riser	
TIDACLID 1 490	Odiferk			NUD PRO	PERTIES							CATION		11- (4.00
ample Location	IN	or OUT	IN		IN		WEIGHT	<9.2 ppg	VIS HTHP	38-4	5 sec ml	YP KCL	10-20 3	•
ime Sample Taken			12:45		23:30		API Filt BY AUTH	5-7 ml OBITY		, orogran				
Depth	°C		1094		1133 43		REMARK							
Towline Temp Veight	pp		8.95		9.10		Rebuilt pi	t volume.						
unnel Viscosity		c/qt	37		38		Treated v	vith CMC-E	HV and I	DEXTRI	D to re	duce filtre	te and ir	nprove
Plastic Viscosity	сР	)	11		11		filter cake	after getting L added to i	g stuck. I	riitrate i Yield P	reduced	i to o.2 m I funnel v	is. CMC	-EHV
rield Point		/100 ft²	7		8 1/3/-		not suffic	ent to maint	ain visco	sity by	itself.			
Gels 10 sec/10min/3		/100 ft² I/30min	1/2/ 9.6		8.2		Desilter s	hut off for tw	o hours.	, repairi	ng elec	trical faul	t. Decide	ed not
API Filtrate HPHT Filtrate		1/30min	J.,				to run de	silter after re	paired, t	o reduc	e mud	losses ar	nd allow:	solids
PI/HPHT Filter Cak		nd ins	1/-		1/-			ht to build u		Waare	format	ion. Ran	desande	r only,
Solids		Vol	3.3		4.5		to control	sand conte , little or no	nı. viscosity	from fo	rmatio	n solids/c	lays.	
Dissolved Salts		Vol	1.2 -/95.5		1.3 -/94.3		LOWITO	, indic or rio					•	
Dil/Water Content Sand		Vol Vol	0.3	. <del></del>	0.3		1							
Methylene Blue cap			9		12		1							
pH	m	eter	9.0		9.5		ACTRO	<u></u>						
Alk. Mud Pm	m		0.38		0.74		Continue	d RIH. Hit b	ridge at	1034m.	ream/v	ash 1024	1 - 1043	m, one
Alk. Filtrate, Pf/Mf	m m	lg/Lx10 ³	0.06/0.16 13.6		15.0		iet partial	ly blocked.	Blew kell	ly hose	while re	eaming. F	OOH to	casing
Chlorides Total Hardness/Cal		ig/LX10°	120/100		40/32		shoe. Re	placed kelly	hose. R	iH, was	hed 8m	to bottor	n, no fill.	Drilled
KCL	%	Wt Soln	2.7		2.9		8 1/2" ho	le from 1080	– 1133	m; surv	ey at 10	Jyom.		
K+ Ion Conc	m	ig/Lx103	15.2		16.6		1							
			<del>                                     </del>				]							
							1			,				
							į							
Rheometer	600 rpm/				30/19		-							
II- 14 0 0 E2	200 rpm/		<del> </del>				1							
lb/100 ft ²				ADTION										
ID/1UU 11 ²	6 rpm/3 r	ORY AN	D CONSU	WIPHON			1							
	INVENT	ORY AN	D CONSUI	REC	BAL	COST	MUD TY		KCI/Poly				SUMPTIONS	
PRODUCT DESC	INVENT	ORY ANI			236	COST		CONTROL	EQUIP	MENT	hre	Addit	ions	ON bbl
PRODUCT DESCF Barite,sx Barite,sx	INVENTOR RIPTION 50 kg 25 kg	ORY ANI g g	USED		236 402		SOLIDS	CONTROL Make	EQUIP! scre	MENT en size			ions/.	bbl
PRODUCT DESCF Barite,sx Barite,sx AQUAGEL,sx	INVENTOR RIPTION 50 kg 25 kg 25 kg	g g g	USED 67	REC	236 402 285	960.11	SOLIDS Shaker 1	CONTROL Make TRITON	EQUIP! scre	MENT		Additi Sea W	ions /. /	bbl
PRODUCT DESCE Barite,sx Barite,sx AQUAGEL,sx Caustic Soda	1NVENTO RIPTION 50 kg 25 kg 25 kg 25 kg	ORY ANI g g g	USED	REC	236 402	960.11 162.15	Shaker 1 Shaker 2 Shaker 3	CONTROL Make TRITON	EQUIP! scre	MENT en size		Additi Sea W 5 Drill W other other	ions /. /.	bbl
PRODUCT DESCE Barite,sx AQUAGEL,sx Caustic Soda CMC-EHV	INVENTOR RIPTION 50 kg 25 kg 25 kg	ORY ANI g g g g g	USED 67 5	REC	236 402 285 24 37 61	960.11 162.15 1705.76 538.92	Shaker 1 Shaker 2 Shaker 3 Shaker 4	CONTROL Make TRITON	scre 110	MENT en size /84/50	1	Additi Sea W 5 Drill W other other Barite	ions /. /.	<b>bbl</b>
PRODUCT DESCE Barite,sx AQUAGEL,sx Caustic Soda CMC-EHV	1NVENTOR RIPTION 50 kg 25 kg 25 kg 25 kg 25 kg	g g g g g	67 5 16	REC	236 402 285 24 37	960.11 162.15 1705.76 538.92	SOLIDS Shaker 1 Shaker 2 Shaker 3	CONTROL Make TRITON 2 3 4	scre 110	MENT en size /84/50 hr hrs	bbl	Additi Sea W 5 Drill W other other Barite Chem	ions /. /.	33
PRODUCT DESCE Barite,sx AQUAGEL,sx Caustic Soda CMC -EHV DEXTRID LT	1NVENT RIPTION 50 kg 25 kg 25 kg 25 kg 25 kg 50 lb	g g g g g	67 5 16	REC	236 402 285 24 37 61	960.11 162.15 1705.76 538.92	SOLIDS  Shaker 1 Shaker 2 Shaker 4 Desande	CONTROL Make TRITON 2 3 4 Pp:	scre 110 bbl/l 1.7 2	MENT en size /84/50 hr hrs	1   bbl   5   3	Additi Sea W 5 Drill W other other Barite	ions /. /. /. icals	bbl 3
PRODUCT DESCE Barite,sx Barite,sx AQUAGEL,sx Caustic Soda CMC-EHV DEXTRID LT	1NVENT RIPTION 50 kg 25 kg 25 kg 25 kg 25 kg 50 lb	g g g g g	67 5 16	REC	236 402 285 24 37 61	960.11 162.15 1705.76 538.92	SOLIDS Shaker 1 Shaker 2 Shaker 3	CONTROL Make TRITON 2 3 4 pp:	scre 110	MENT en size /84/50 hr hrs	1   bbl   5   3	Additi Sea W 5 Drill W other other Barite Chem 8 Losse 9 Sol. C	ions /. /. /. icals	bbl 3
PRODUCT DESCE Barite,sx AQUAGEL,sx Caustic Soda CMC -EHV DEXTRID LT	1NVENT RIPTION 50 kg 25 kg 25 kg 25 kg 25 kg 50 lb	g g g g g	67 5 16	REC	236 402 285 24 37 61	960.11 162.15 1705.76 538.92	SOLIDS Shaker 1 Shaker 2 Shaker 3 Shaker 4 Desande	CONTROL Make TRITON  2 3 4 pp: er 1 1. 1 2.	scre 110 bbl/l 1.7 2	MENT en size /84/50 hr hrs	bbl 5 3	Additi Sea W 5 Drill W other other Barite Chem 8 Losse 9 Sol. C Lost/I Down	ions  /.  /.  iicals  s con.  Dumped Hole	33:
PRODUCT DESCE Barite,sx Barite,sx AQUAGEL,sx Caustic Soda CMC-EHV DEXTRID LT	1NVENT RIPTION 50 kg 25 kg 25 kg 25 kg 25 kg 50 lb	g g g g g	67 5 16	REC	236 402 285 24 37 61	960.11 162.15 1705.76 538.92	SOLIDS Shaker 1 Shaker 2 Shaker 3 Shaker 4 Desande Desilter Desilter	CONTROL Make TRITON  2 3 4 pp: er 1 1, 1 2, ge 1	scre 110 bbl/l 1.7 2	MENT en size /84/50 hr hrs	bbl 5 3	Additi Sea W 5 Drill W other other Barite Chem 8 Losse 9 Sol. C Lost/C Down Newh	ions  /.  /.  icals  con.  Dumped i Hole ole	bbl 3
PRODUCT DESCE Barite,sx Barite,sx AQUAGEL,sx Caustic Soda CMC-EHV DEXTRID LT	1NVENT RIPTION 50 kg 25 kg 25 kg 25 kg 25 kg 50 lb	g g g g g	67 5 16	REC	236 402 285 24 37 61	960.11 162.15 1705.76 538.92	SOLIDS Shaker 2 Shaker 3 Shaker 4 Desande Desilter Desilter Centrifue	CONTROL Make TRITON 2 3 4 PP: er   1 1,	scre 110 bbl/l 1.7 2	MENT en size /84/50 hr hrs	bbl 5 3 3	Additive Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea W	ions  //  //  picals  ss  con.  Dumped  Hole  iole  GAIN	bbl 3
PRODUCT DESCE Barite,sx Barite,sx AQUAGEL,sx Caustic Soda CMC-EHV DEXTRID LT KCL,Tech(sx)	INVENTO RIPTION 50 kg 25 kg 25 kg 25 kg 50 lb 25 kg	g g g g g	67 5 16 9 63	REC	236 402 285 24 37 61 146	960.11 162.15 1705.76 538.92 909.72	SOLIDS Shaker 2 Shaker 3 Shaker 4 Desande Desilter Desilter Centrifue	CONTROL Make TRITON 2 3 4 PP: er 1 1. 1 2. ge 1 ge 2 ontrol Effic.	EQUIPI scre 1110 110 g bbl/l 1.7 2 1.4	MENT en size /84/50 hr hrs	bbl 5 3 3 3 %	Additive Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea Web Sea W	ions  //  //  sicals  ss  con.  Dumped  Hole  oole  GAIN  narged	bbl 33 bbl 1 1 1 1 1 1 1
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PRODUCT DESCR Barite,sx AQUAGEL,sx Caustic Soda CMC – EHV DEXTRID LT KCL, Tech(sx) BAROID En ALAN SEARI	INVENTON 50 kg 25 kg 25 kg 25 kg 25 kg 25 kg 50 lb 25 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10 kg 10	GRY ANI  9  9  9  9  9  9  9  0  The HERECTY LIABILITY	OFFICE  MELBOUF 03 – 621 DN SHALL N TY BY BARO  SURV	REC  RNE 3311 OT BE CON ID DRILLING EY DATA	236 402 285 24 37 61 146 WAREHOL	960.11 162.15 1705.76 538.92 909.72	Shaker 1 Shaker 2 Shaker 3 Shaker 4 Desande Desilter Desilter Centrifus Centrifus Solids C	CONTROL Make TRITON 2 3 4 pp: er 1 1. 1 2. ge 1 ge 2 ontrol Effic. DAILY A\$ 42 FRINGEMEN ND ARE STAT	EQUIPI SCRE 110 110 110 110 110 110 110 110 110 11	MENT en size //84/50 hr hrs. 5 1 3 3	bbl 5 3 3 SCUM A\$ PATENT, NION ON TIME	Additive Sea W other other other Barite Chem 8 Losses 9 Sol. C Lost/C Down New NET Discription 1202  AND ARE	ions // // // // // // // // // // // // //	bbl
PRODUCT DESCRED Barite, SX AQUAGEL, SX Caustic Soda CMC - EHV DEXTRID LT KCL, Tech(SX)  BAROID En ALAN SEARI Tel. 03 - 787 15 THE RECOMMENDA WITHOUT ASSUMPT  RESERVE PITS NO TYPE	INVENTON   50 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   2	GRY ANI  9  9  9  9  9  9  9  OF HERECTY LIABILITY	OFFICE  MELBOUF 03 - 621 DN SHALL NI TY BY BARO  SURV	REC  RNE  3311  OT BE CON  ID DRILLING  EY DATA  INCL®	236 402 285 24 37 61 146 WAREHOL	960.11 162.15 1705.76 538.92 909.72	Shaker 1 Shaker 2 Shaker 3 Shaker 4 Desande Desilter Desilter Centrifue Centrifue Solids C	CONTROL Make TRITON  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer	EQUIPI SCRE 110 110 110 110 110 110 110 110 110 11	MENT en size //84/50 hr hrs .5 1 3  VALID F OF OPIN	bbl 5 3 3 GUN A\$ PATENT, NION ON	Additive Sea W other other other Search Chem Barite Chem Barite Chem Newh NET Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion Discretion	ions // // // // // // // // // // // // //	bbl
PRODUCT DESCREATE, SX Barite, SX AQUAGEL, SX Caustic Soda CMC - EHV DEXTRID LT KCL, Tech(SX)  BAROID En ALAN SEARI Tel. 03 - 787 15 THE RECOMMENDA WITHOUT ASSUMPT  RESERVE PITS NO TYPE 6 PIII Tank	INVENTON 50 kg 25 kg 25 kg 25 kg 25 kg 25 kg 50 lb 25 kg 50 lb 25 kg 50 lb 25 kg 50 lb 25 kg	GRY ANI  9  9  9  9  9  9  9  0  The HERECTY LIABILITY	OFFICE  MELBOUF 03 - 621 DN SHALL NI TY BY BARO  SURV	REC  RNE 3311 OT BE CON ID DRILLING EY DATA	236 402 285 24 37 61 146 WAREHOL	960.11 162.15 1705.76 538.92 909.72	SOLIDS Shaker 1 Shaker 2 Shaker 3 Shaker 4 Desande Desilter Desilter Centrifue Centrifue Solids C	CONTROL Make TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  TRITON  T	EQUIPING SCREET STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE ST	MENT en size //84/50 hr hrs .5 1 3  VALID F OF OPIN	bbl 5 3 3 6 CUM A\$ PATENT, NION ON TIMI	Additive Sea W other other other Barite Chem 8 Losses 9 Sol. C Lost/C Down New NET Discription 1202  AND ARE	ions // // // // // // // // // // // // //	bbl
PRODUCT DESCR Barite,sx AQUAGEL,sx Caustic Soda CMC – EHV DEXTRID LT KCL, Tech(sx) BAROID En ALAN SEARI Tel. 03 – 787 15 THE RECOMMENDA WITHOUT ASSUMPT NO TYPE	INVENTON   50 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   2	GRY ANI  9  9  9  9  9  9  9  OF HERECTY LIABILITY	OFFICE  MELBOUF 03 - 621 DN SHALL NI TY BY BARO  SURV	REC  RNE  3311  OT BE CON  ID DRILLING  EY DATA  INCL®	236 402 285 24 37 61 146 WAREHOL	960.11 162.15 1705.76 538.92 909.72	SOLIDS Shaker 1 Shaker 2 Shaker 3 Shaker 4 Desande Desilter Desilter Centrifut Centrifut Solids C	CONTROL Make TRITON  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer  Printer	EQUIPING SCREET STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE STATE ST	MENT en size /84/50 hr hrs5 1 3 3 VALID F OF OPIN SIS ol 4.2 38.2 ol 0.3	bbl 5 3 3 3 CUM A\$ PATENT, NION ON TIMI Dril Circ Res	Additive Sea W other other other Barite Chem 8 Losses 9 Sol. 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PRODUCT DESCR Barite,sx Barite,sx AQUAGEL,sx Caustic Soda CMC-EHV DEXTRID LT KCL,Tech(sx)  BAROID En ALAN SEARI Tel. 03 - 787 15 THE RECOMMENDA WITHOUT ASSUMPT  RESERVE PITS NO TYPE 6 Pill Tank	INVENTON   50 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   2	GRY ANI  9  9  9  9  9  9  9  OF HERECTY LIABILITY	OFFICE  MELBOUF 03 - 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PRODUCT DESCR Barite,sx Barite,sx AQUAGEL,sx Caustic Soda CMC-EHV DEXTRID LT KCL,Tech(sx)  BAROID En ALAN SEARI Tel. 03 - 787 15 THE RECOMMENDA WITHOUT ASSUMPT  RESERVE PITS NO TYPE 6 Pill Tank	INVENTON   50 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 kg   25 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Weight Funnel Viscosity	ppg sec/qt	39		39		filtrate be	low 7 ml.							
Plastic Viscosity	cP	12		13		Desilter	shut off to	allow	solids t	to build	and ir	ncrease m	nua wei	grit to
Yield Point	lb/100 ft ²	8		9		9.3+ lb/g	gal prior to	o drillin	g waar	e. Hill roolt	ively lo	w despite	e treatm	ents
Gels 10 sec/10min/		1/5/-		2/7/-		with CMC	and AO	LIAGEL	. No pr	roblem	s with I	hole clear	ning hov	wever.
API Filtrate	ml/30min		-	6.8		Pumpeo	weighte	d pill to	POOH	for bit	chang	e, Barite	intende	d to he
HPHT Filtrate	ml/30min (e 32nd ins	1/-		1/		raise mu	d weight	to requ	ired 9.3	3+				
API/HPHT Filter Cal Solids	% Vol	5.3		6.0										
Dissolved Salts	% Vol	1.2		1.3										
Oil/Water Content	% Val	-/93.5	ļ	-/92.8										
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AVE ROP m/hr

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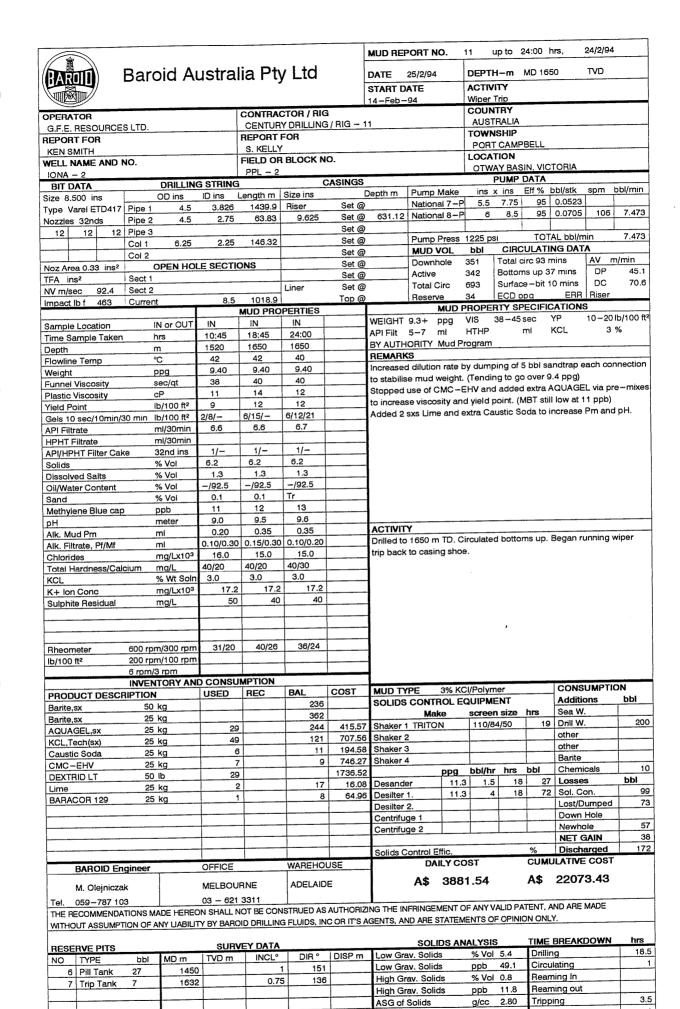
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Cuttings Volume

Interval Dilution

Interval Consumption bbl/m 1.8

ASG of Solids



57.0

bbl

bbl/m 1.3 bbl/m 1.6

Cuttings Volume

Interval Dilution

Interval Consumption

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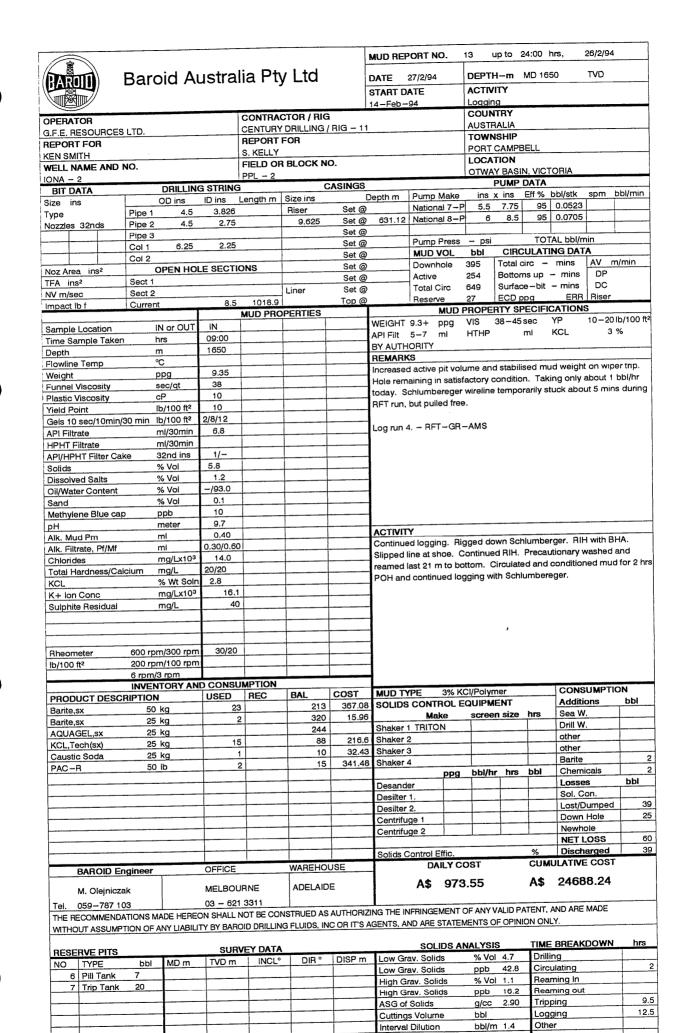
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Alk. Mud Pm		ml	0.35				Continue	d wiper	trip. Ho	ole only	slightl	y tight	coming	out at 105	50 m.
Alk. Mud Pm Alk. Filtrate, Pf/Mf		ml ml					Continue	d wiper	om, pre	caution	nary wa	ashing	and rear	ning last :	5 m.
Alk. Mud Pm Alk. Filtrate, Pf/Mf Chlorides		ml	0.35 0.10/0.20				Continue Ran back Circulate	ed wiper to botto d out, pu	om, pre umped	ecautior slug ar	nary wa	ashing	and rear	out at 105 ming last : nulti-sho	5 m.
Alk. Mud Pm Alk. Filtrate, Pf/Mf	alcium	ml ml mg/Lx10 ³	0.35 0.10/0.20 15.0 40/30 3.0				Continue	ed wiper to botto d out, pu	om, pre umped	ecautior slug ar	nary wa	ashing	and rear	ning last :	5 m.
Alk. Mud Pm Alk. Filtrate, Pf/Mf Chlorides Total Hardness/C KCL K+ Ion Conc	alcium	ml mg/Lx10 ³ mg/L % Wt Soln mg/Lx10 ³	0.35 0.10/0.20 15.0 40/30 3.0 17.2				Continue Ran back Circulate	ed wiper to botto d out, pu	om, pre umped	ecautior slug ar	nary wa	ashing	and rear	ning last :	5 m.
Alk. Mud Pm Alk. Filtrate, Pf/Mf Chlorides Total Hardness/C KCL K+ Ion Conc	alcium	ml mi mg/Lx10 ³ mg/L % Wt Soln	0.35 0.10/0.20 15.0 40/30 3.0				Continue Ran back Circulate	ed wiper to botto d out, pu	om, pre umped	ecautior slug ar	nary wa	ashing	and rear	ning last :	5 m.
Alk. Mud Pm Alk. Filtrate, Pf/Mf Chlorides Total Hardness/C KCL K+ Ion Conc	alcium	ml mg/Lx10 ³ mg/L % Wt Soln mg/Lx10 ³	0.35 0.10/0.20 15.0 40/30 3.0 17.2				Continue Ran back Circulate	ed wiper to botto d out, pu	om, pre umped	ecautior slug ar	nary wa nd stra	ashing	and rear	ning last :	5 m.
Alk. Mud Pm Alk. Filtrate, Pf/Mf Chlorides Total Hardness/C	alcium	ml mg/Lx10 ³ mg/L % Wt Soln mg/Lx10 ³	0.35 0.10/0.20 15.0 40/30 3.0 17.2				Continue Ran back Circulate	ed wiper to botto d out, pu	om, pre umped	ecautior slug ar	nary wa	ashing	and rear	ning last :	5 m.
Alk. Mud Pm Alk. Filtrate, Pf/Mf Chlorides Total Hardness/C KCL K+ Ion Conc Sulphite Residual	alcium	ml mi mg/Lx10 ³ mg/L % Wt Soln mg/Lx10 ³ mg/L	0.35 0.10/0.20 15.0 40/30 3.0 17.2 40				Continue Ran back Circulate	ed wiper to botto d out, pu	om, pre umped	ecautior slug ar	nary wa nd stra	ashing	and rear	ning last :	5 m.
Alk. Mud Pm Alk. Filtrate, Pf/Mf Chlorides Total Hardness/C KCL K+ Ion Conc Sulphite Residual	alcium	ml mg/Lx10 ³ mg/L % Wt Soln mg/Lx10 ³ mg/L	0.35 0.10/0.20 15.0 40/30 3.0 17.2 40				Continue Ran back Circulate	ed wiper to botto d out, pu	om, pre umped	ecautior slug ar	nary wa nd stra	ashing	and rear	ning last :	5 m.
Alk. Mud Pm Alk. Filtrate, Pf/Mf Chlorides Total Hardness/C KCL K+ Ion Conc Sulphite Residual	600 rpi 200 rpi 6 rpm/	ml mi mg/Lx10 ³ mg/L % Wt Soln mg/Lx10 ³ mg/L n/300 rpm n/100 rpm 3 rpm	0.35 0.10/0.20 15.0 40/30 3.0 17.2 40				Continue Ran back Circulate	ed wiper to botto d out, pu	om, pre umped	ecautior slug ar	nary wa nd stra	ashing	and rear	ning last :	5 m.
Alk. Mud Pm Alk. Filtrate, Pf/Mf Chlorides Total Hardness/C KCL K+ Ion Conc Sulphite Residual Rheometer Ib/100 ft²	600 rpi 200 rpi 6 rpm/	ml mg/Lx103 mg/L % Wt Soin mg/Lx103 mg/L % mg/Lx103 mg/L n/300 rpm n/100 rpm 3 rpm TORY AN	0.35 0.10/0.20 15.0 40/30 3.0 17.2 40			COST	Continue Ran bacl Circulate Ran Sch	ed wiper to botton	om, pre umped er logs	ecautior slug ar	nary Wand stra	ashing	and rear	ning last :	5 m. It surv
Alk. Mud Pm Alk. Filtrate, Pf/Mf Chlorides Total Hardness/C K-L K-L Sulphite Residual Rheometer Ib/100 ft² PRODUCT DES	600 rpi 200 rpi 6 rpm/ INVEN	ml ml mg/Lx10³ mg/L % Wt Soin mg/Lx10³ mg/L 1030 rpm n/100 rpm 3 rpm TORY AN	0.35 0.10/0.20 15.0 40/30 3.0 17.2 40	MPTION REC	BAL	COST	Continue Ran back Circulate Ran Sch	ed wiper to to botton dout, pullumberge	om, pre umped er logs	ecaution slug ar	nary wand stra	ashing	and rear	ning last : nulti-sho	5 m. It sun
Alk. Mud Pm Alk. Filtrate, Pf/Mf Chlorides Total Hardness/C KCL K+ Ion Conc Sulphite Residual Rheometer Ib/100 ft² PRODUCT DESE Barite,sx	600 rpi 200 rpi 1 inven CRIPTION	ml ml mg/Lx10³ mg/L % Wt Soin mg/Lx10³ mg/L m/300 rpm m/100 rpm 3 rpm TORY AN	0.35 0.10/0.20 15.0 40/30 3.0 17.2 40 36/24		236	COST 319.2	Continue Ran back Circulate Ran Sch  MUD TY SOLIDS	ed wiper to botton	om, pre umped er logs 3% KC	ecaution slug ar	nary wand stra	ashing pped c	CONSAddit	ning last : nulti — sho  SUMPTIC ions	on bbl
Alk. Mud Pm Alk. Filtrate, Pf/Mf Chlorides Total Hardness/C KCL K+ Ion Conc Sulphite Residual Rheometer Ib/100 ft² PRODUCT DESI Barite,sx Barite,sx	600 rpi 200 rpi 6 rpm/ INVEN CRIPTION 25	ml mg/Lx10³ mg/L % Wt Soln mg/Lx10³ mg/Lx10³ mg/Lx10³ m/300 rpm n/100 rpm 3 rpm TORY AN kg	0.35 0.10/0.20 15.0 40/30 3.0 17.2 40				Continue Ran back Circulate Ran Sch  MUD TY SOLIDS	ed wiper to bottod out, pullumberge	om, pre umped er logs 3% KC BOL EC	ecaution slug ar ci/Polym	nary wand stra	ashing pped c	CONS Addit Sea V	ning last: nulti—sho sumptic ions v.	on bbl
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Alk. Mud Pm Alk. Filtrate, Pf/Mf Chlorides Fotal Hardness/C KCL K+ Ion Conc Sulphite Residual Rheometer b/100 ft² PRODUCT DESt Barite,sx Barite,sx AQUAGEL,sx KCL,Tech(sx) BARACIDE	600 rpi 200 rpi 6 rpm/ INVEN CRIPTION 50 25 25 25	ml ml mg/Lx10³ mg/L % Wt Soin mg/Lx10³ mg/L 10³ mg/L 10³ mg/L  n/300 rpm n/100 rpm 3 rpm TORY AN kg kg kg kg	0.35 0.10/0.20 15.0 40/30 3.0 17.2 40 36/24 D CONSUI USED 40	REC	236 322 244 103	319.2 259.92	Continue Ran back Circulate Ran Sch  MUD TY SOLIDS Shaker Shaker Shaker Shaker	PE CONTR Mak 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	3% KC	ecaution slug ar El/Polym QUIPME screet	nary wand stra	hrs	CONS Addit Sea V Orther other Barite	SUMPTIC ions v.	on bbl
Alk. Mud Pm Alk. Filtrate, Pf/Mf Chlorides Fotal Hardness/C KCL K+ Ion Conc Sulphite Residual Rheometer b/100 ft² PRODUCT DESI Barite,sx Barite,sx AQUAGEL,sx KCL,Tech(sx) BARACIDE PAC-R	600 rp: 200 rp: 200 rp: 1 INVEN CRIPTION 25 25 25 25 50 25	mi mi mg/Lx10³ mg/L % Wt Soin mg/Lx10³ mg/L 100 rpm 100 rpm 3 rpm TORY AN kg kg kg	0.35 0.10/0.20 15.0 40/30 3.0 17.2 40 36/24 D CONSUI USED 40	REC 48	236 322 244 103 17 48	319.2 259.92 549.92	Continue Ran back Circulate Ran Sch  MUD TY SOLIDS Shaker Shaker Shaker Shaker	PE CONTR Mak TRITO	om, pre umped er logs 3% KC BOL EC	ecaution slug ar cl/Polym	nary wand stra	ashing pped c	CONSAddit Sea V Drill V other other Barite Chem	SUMPTIC ions V.	DN bbl
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Alk. Mud Pm Alk. Filtrate, Pf/Mf Chlorides Total Hardness/C KCL K- Ion Conc Sulphite Residual Rheometer Ib/100 ft² PRODUCT DESI Barite,sx Barite,sx AQUAGEL,sx KCL,Tech(sx) BARACIDE PAC – R BARACARB 110	600 rp: 200 rp: 200 rp: 1 INVEN CRIPTION 25 25 25 25 50 25	mi mi mg/Lx10³ mg/L % Wt Soin mg/Lx10³ mg/L 100 rpm 100 rpm 3 rpm TORY AN kg kg kg	0.35 0.10/0.20 15.0 40/30 3.0 17.2 40 36/24 D CONSUI USED 40	REC 48	236 322 244 103 17 48 48	319.2 259.92 549.92 512.22	MUD TO SOLIDS Shaker Shaker Shaker Desand Desilter Desilter Centrifu	PE CONTR Make TRITO 2 3 4 er 1. 2. ge 1 ge 2	om, pre- umped 3% KC OL EC  e N	caution slug ar	nary wand stra	hrs bbl	CONS Addit Sea V Other Other Losse Sol. C Lost/[ Down New! NET Discl	SUMPTIC ions  V. V. Snicals  es Con. Dumped  Hole hole GAIN  harged	DN bbl
Alk. Mud Pm Alk. Filtrate, Pf/Mf Chlorides Fotal Hardness/C KCL K+ Ion Conc Sulphite Residual Rheometer b/100 ft² PRODUCT DESE Barite,sx Barite,sx AQUAGEL,sx KCL,Tech(sx) BARACIDE PAC —R BARACARB 110	600 rp. 200 rp. 200 rp. 6 rpm/ INVEN CRIPTION 25 25 25 25 25 50 25	mi mi mg/Lx10³ mg/L % Wt Soin mg/Lx10³ mg/L 100 rpm 100 rpm 3 rpm TORY AN kg kg kg	0.35 0.10/0.20 15.0 40/30 3.0 17.2 40 36/24 D CONSUI USED 40	REC 48	236 322 244 103 17 48	319.2 259.92 549.92 512.22	MUD TO SOLIDS Shaker Shaker Shaker Desand Desilter Desilter Centrifu	PE CONTR Make TRITO 2 3 4 er 1. 2. ge 1 ge 2	3% KC ROL EC	caution slug ar	nary wand stra	hrs bbl	CONS Addit Sea V Other Other Chem Loss(SOL) CLOST/I DOWN NET Disc	SUMPTIC SUMPTIC SUMPTIC SUMPTIC SUMPTIC SUM SUMPTIC SUM SUM SUM SUM SUM SUM SUM SUM SUM SUM	DN bbl
Nik. Mud Pm Nik. Filtrate, Pf/Mf Chlorides Total Hardness/C CCL (+ Ion Conc Sulphite Residual Rheometer b/100 ft²  PRODUCT DESI Barite,sx Barite,sx Barite,sx AQUAGEL,sx KCL,Tech(sx) BARACIDE PAC —R BARACARB 110 BARACARB 600	600 rpi 200 rpi 6 rpm/ INVEN CRIPTION 25 25 25 25 25 25	mi mi mg/Lx10³ mg/L % Wt Soin mg/Lx10³ mg/L 100 rpm 100 rpm 3 rpm TORY AN kg kg kg	0.35 0.10/0.20 15.0 40/30 3.0 17.2 40 36/24  D CONSUI USED 40 38 31 30 30 30 30 30 30 30 30 30 30 30 30 30	48 48	236 322 244 103 17 48 48	319.2 259.92 549.92 512.22	MUD TO SOLIDS Shaker Shaker Shaker Desand Desilter Desilter Centrifu	PE CONTR Make TRITO 2 3 4 er 1. 2. ge 1 ge 2	3% KC 3% KC ROL EC	caution slug ar	nary wand stra	hrs bbl	CONS Addit Sea V Other Other Chem Loss(SOL) CLOST/I DOWN NET Disc	SUMPTIC ions  V. V. Snicals  es Con. Dumped  Hole hole GAIN  harged	DN bbl
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Alk. Mud Pm Alk. Filtrate, Pf/Mf Chlorides Fotal Hardness/C K+ Ion Conc Sulphite Residual Rheometer Ib/100 ft²  PRODUCT DESt Barite,sx AQUAGEL,sx KCL,Tech(sx) BARACIDE PAC-R BARACARB 110 BARACARB 600  BARACARB 600  BARACARB 110 BARACARB 110 BARACARB 110 BARACARB 110 BARACARB 110 BARACARB 110 BARACARB 110 BARACARB 600  BARACARB 110 BARACARB 600  RESERVE PITS NO TYPE 6 Pill Tank	600 rpp 200 rpp 6 rpm/ INVEN CRIPTION 50 25 25 25 25 25 25 25 25 25 25 25 25 25	mi mi mg/Lx10³ mg/L % Wt Soin mg/Lx10³ mg/L n/300 rpm n/100 rpm 3 rpm TORY AN kg kg kg kg	0.35 0.10/0.20 15.0 40/30 3.0 17.2 40 36/24  D CONSUI USED  18 1 3  OFFICE MELBOUI 03 - 621 DN SHALL N TY BY BARO SURV	A88 488 489 489 489 489 489 489 489 489 4	236 322 244 103 17 48 48 WAREHOL ADELAID STRUED AS 3 FLUIDS, IN	319.2 259.92 549.92 512.22 JSE E	Continue Ran back Circulate Ran Sch  MUD TY SOLIDS Shaker: Shaker: Shaker: Shaker: Shaker: Shaker: Shaker: Shaker: Shaker: Lestiffu Centrifu Centrifu Centrifu Centrifu Centrifu Low Gra Low Gra High Gi	PE CONTR Mak TRITON 2 2 ge 1 ge 2 Control E DAI A\$ IFRINGEN ND ARE S SOLIII av. Solida av. Solida av. Solida av. Solida	3% KC 3% KC ROL EC ROL PPG  MENT O TATEM  S S S S S S S S S S S S S S S S S S	bbl/hr  ST  1.26  FANY V  ENTS OI  ALYSIS % Vol ppb % Vol	hrs hrs 5.4 49.1 0.8	hrs bbl % CUM A\$ ATENT. ION ON TIME Drilli Cilrc Reee Reee	CONSAddit Sea V Drill V other other Lossi Sol. C Lost/I Down NET Disci ULATIV 237	SUMPTIC SUMPTIC SUMPTIC SUMPTIC SUMPTIC SUM SUMPTIC SUM SUM SUM SUM SUM SUM SUM SUM SUM SUM	5 m. t sun
Alk. Mud Pm Alk. Filtrate, Pf/Mf Chlorides Fotal Hardness/C K+ Ion Conc Sulphite Residual Rheometer Ib/100 ft²  PRODUCT DESt Barite,sx AQUAGEL,sx KCL,Tech(sx) BARACIDE PAC-R BARACARB 110 BARACARB 600  BARACARB 600  BARACARB 110 BARACARB 110 BARACARB 110 BARACARB 110 BARACARB 110 BARACARB 110 BARACARB 110 BARACARB 600  BARACARB 110 BARACARB 600  RESERVE PITS NO TYPE 6 Pill Tank	600 rpp 200 rpp 6 rpm/ INVEN CRIPTION 50 25 25 25 25 25 25 25 25 25 25 25 25 25	mi mi mg/Lx10³ mg/L % Wt Soin mg/Lx10³ mg/L n/300 rpm n/100 rpm 3 rpm TORY AN kg kg kg kg	0.35 0.10/0.20 15.0 40/30 3.0 17.2 40 36/24  D CONSUI USED  18 1 3  OFFICE MELBOUI 03 - 621 DN SHALL N TY BY BARO SURV	A88 488 489 489 489 489 489 489 489 489 4	236 322 244 103 17 48 48 WAREHOL ADELAID STRUED AS 3 FLUIDS, IN	319.2 259.92 549.92 512.22 JSE E	Continue Ran back Circulate Ran Sch  MUD TY SOLIDS Shaker Shaker Shaker Shaker Centrifu Centrifu Centrifu Centrifu Centrifu Low Gra Low Gra High Gi High Gi ASG of Cutting	PE CONTR Make I TRITON 2 3 4	3% KCROL ECOROL  PPPG  MENT O CTATEM  DS AN  S S S IS IS IS IS IS IS IS IS IS IS IS I	bbl/hr bbl/hr bbl/hr AUYSIS % Vol ppb % Vol ppb g/cc bbl	ALID P FOPIN  S 5.4 49.1 0.8 2.80	hrs bbl  Katent.  Cum A\$  ATENT.  Circ  Circ  Reas  Trip  Log	CONSAdditt Sea V Drill V other other Barite Cherr Lossi Sol. C Lost/l Down NET Disd ULATIV 237  AND ARE LY.  BREAN ing ulating uning ln uning ou ping	SUMPTIC SUMPTIC SUMPTIC SUMPTIC SUMPTIC SUM SUMPTIC SUM SUM SUM SUM SUM SUM SUM SUM SUM SUM	5 m. t surv
Alk. Mud Pm Alk. Filtrate, Pf/Mf Chlorides Fotal Hardness/C K+ Ion Conc Sulphite Residual Rheometer Ib/100 ft²  PRODUCT DESt Barite,sx AQUAGEL,sx KCL,Tech(sx) BARACIDE PAC-R BARACARB 110 BARACARB 600  BARACARB 600  BARACARB 110 BARACARB 110 BARACARB 110 BARACARB 110 BARACARB 110 BARACARB 110 BARACARB 110 BARACARB 600  BARACARB 110 BARACARB 600  RESERVE PITS NO TYPE 6 Pill Tank	600 rpp 200 rpp 6 rpm/ INVEN CRIPTION 50 25 25 25 25 25 25 25 25 25 25 25 25 25	mi mi mg/Lx10³ mg/L % Wt Soin mg/Lx10³ mg/L n/300 rpm n/100 rpm 3 rpm TORY AN kg kg kg kg	0.35 0.10/0.20 15.0 40/30 3.0 17.2 40 36/24  D CONSUI USED  18 1 3  OFFICE MELBOUI 03 - 621 DN SHALL N TY BY BARO SURV	A88 488 489 489 489 489 489 489 489 489 4	236 322 244 103 17 48 48 WAREHOL ADELAID STRUED AS 3 FLUIDS, IN	319.2 259.92 549.92 512.22 JSE E	Continue Ran back Circulate Ran Sch  MUD TY SOLIDS Shaker: Shaker: Shaker: Shaker: Shaker: Centrifu Centrifu Centrifu Centrifu Low Gra Low Gra High Gr High Gr ASG of Cutting; Interval	PE CONTR Mak TRITOR 2 3 4 4 PE CONTROL MAK TRITOR 2 3 4 PE DAI A\$ UFRINGEN ND ARE S SOLII av. Solida vav. Solida vav. Solida vav. Solida vav. Solida vav. Solida vav. Solida	3% KC 3% KC OL EC  PPG  Iffic. LY CO TATEM DS AN S S S S S S	El/Polyman Screen  bbl/hr bbl/hr 1.26  FANY VENTS OI  ALYSIS  Vol ppb y Vol ppb g/cc	hrs hrs hrs hrs hrs hrs hrs hrs hrs hrs	hrs bbl % CUM A\$ ATENT. ION ON TIME Drilli Cilrc Reee Reee	CONSAdditt Sea V Drill V other other Barite Cherr Lossi Sol. C Lost/I Down NET Disd ULATIV 237  AND ARE LY.  BREAN ing ulating uning ln uning ou ping	SUMPTIC SUMPTIC SUMPTIC SUMPTIC SUMPTIC SUM SUMPTIC SUM SUM SUM SUM SUM SUM SUM SUM SUM SUM	5 m. It surv

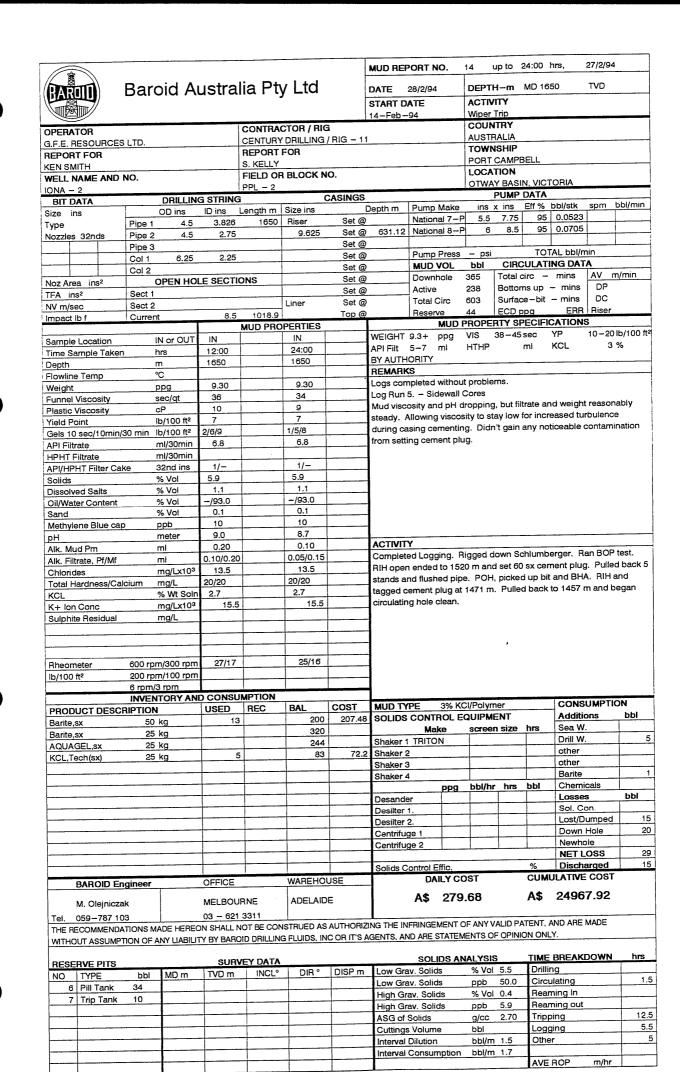


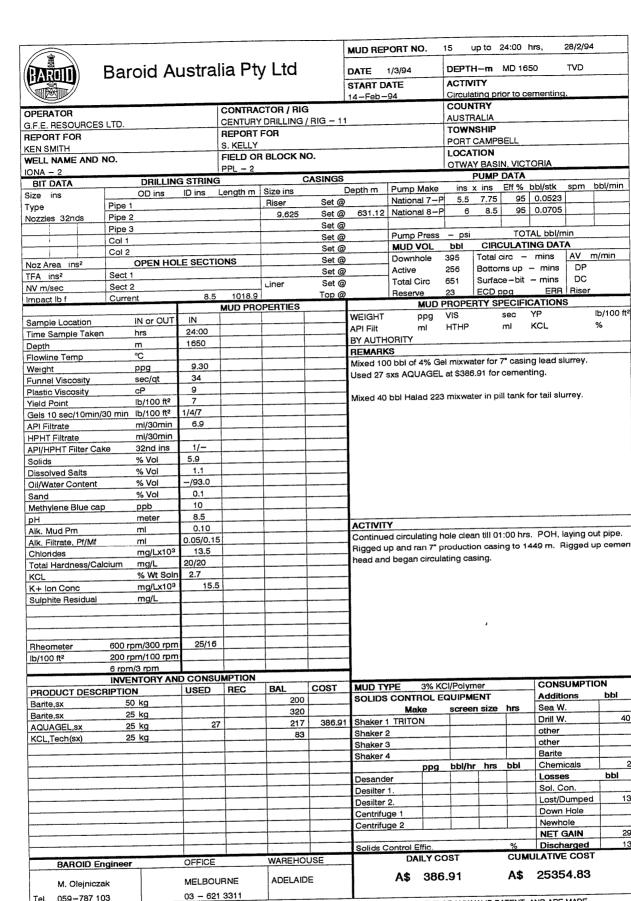
bbl/m 1.7

AVE ROP

m/hr

Interval Consumption





m/min

lb/100 ft

bbl

bbl

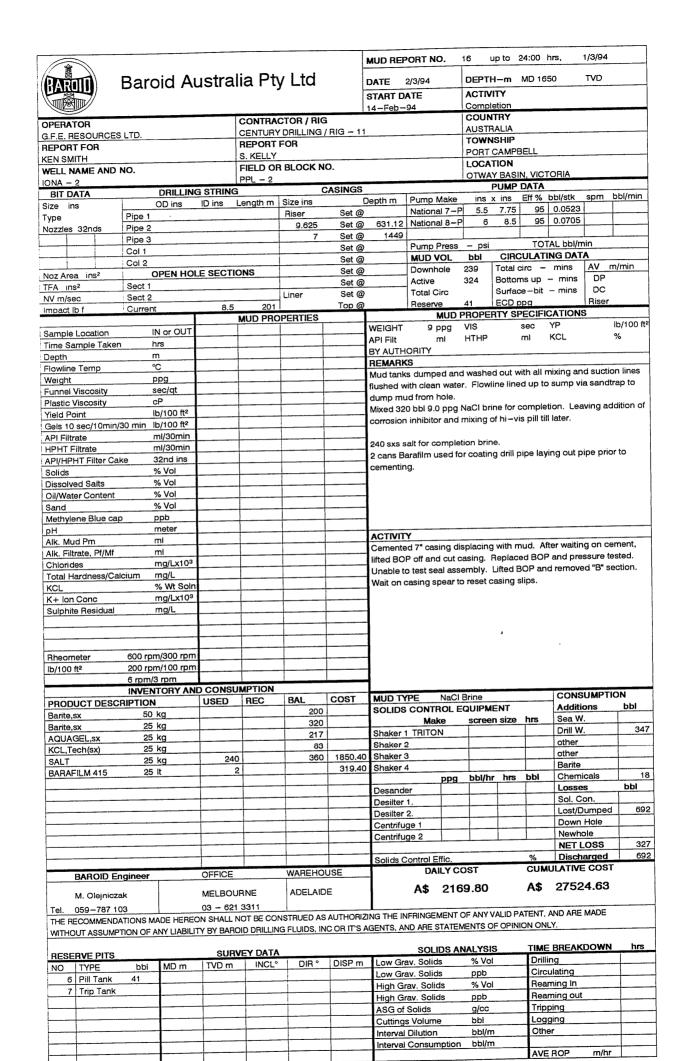
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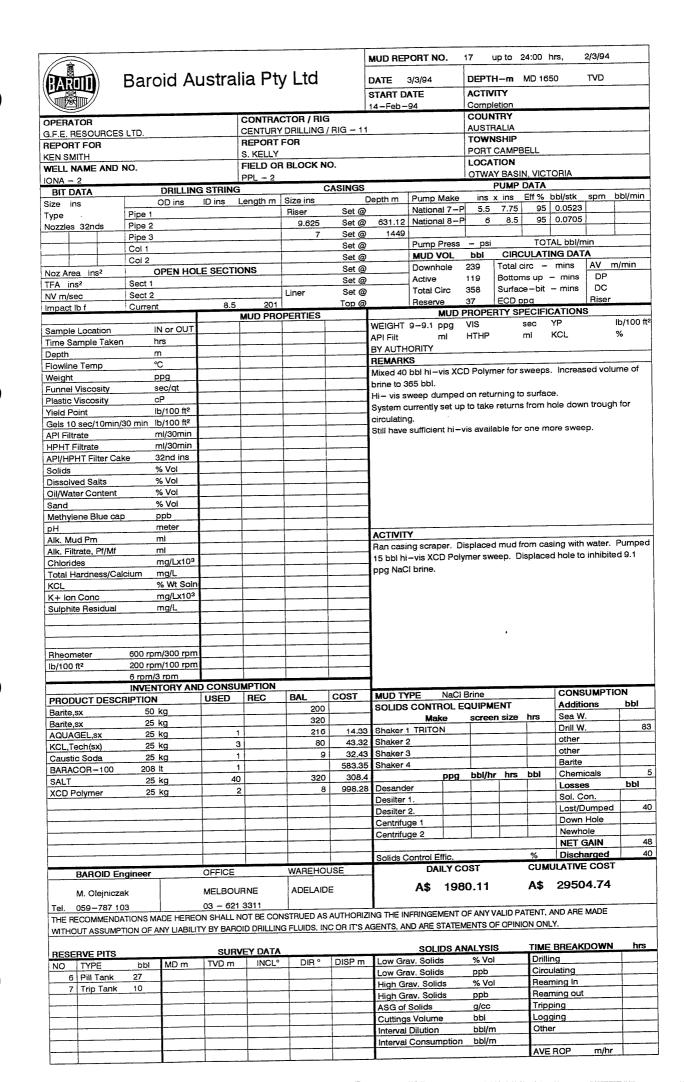
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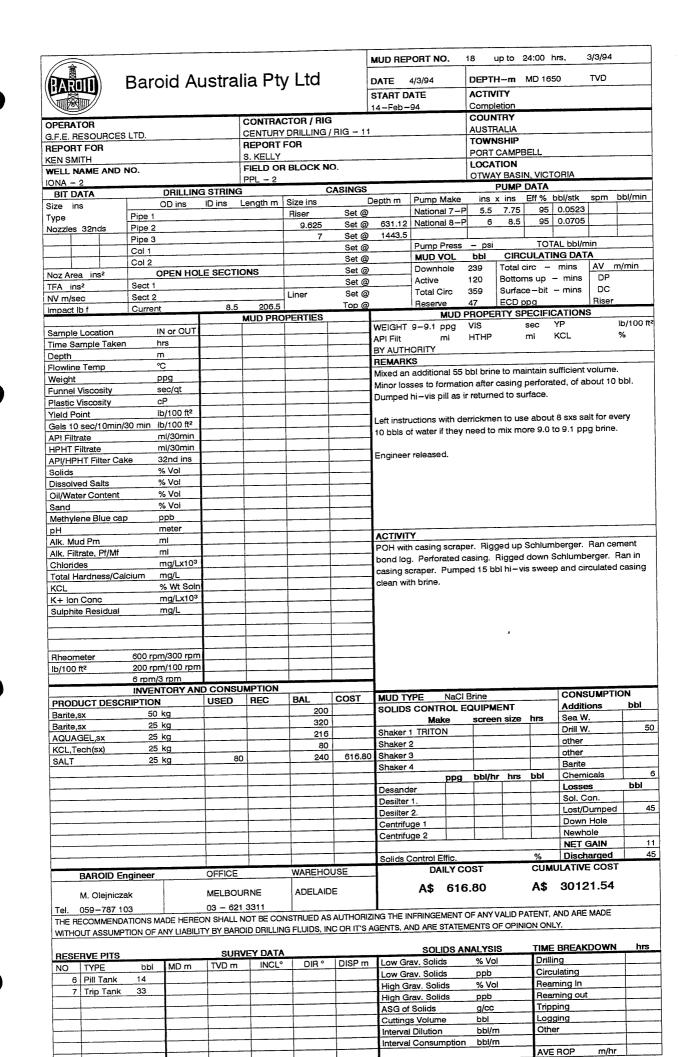
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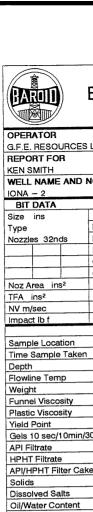
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				ei ib//	EY DATA			SOLIDS AN	ALYSIS	<u> </u>	TIME BREAKDOWN	hrs
	RVE PITS		145	TVD m	INCL°	DIR °	DISP m	Low Grav. Solids	% Vol	5.5	Drilling	
NO	TYPE	bbl	MD m	IVUIII	NUL	Dill		Low Grav. Solids	ppb	50.0	Circulating	2
6	Pill Tank		<u> </u>				+	High Grav. Solids	% Vol	0.4	Reaming In	
7	Trip Tank	23					<del> </del>	High Grav. Solids	ppb	5.9	Reaming out	
L			<del> </del>		ļ			ASG of Solids	g/cc	2.70	Tripping	
								Cuttings Volume	bbl		Logging	
	ļ							Interval Dilution	bbl/m	1.5	Other	22
			<del> </del>					Interval Consumption	bbl/m	1.7		
			<del> </del>		+						AVE ROP m/hr	









### Baroid Australia Pty Ltd

up to 24:00 hrs, MUD REPORT NO. 19 DEPTH-m MD 1650 TVD DATE 5/3/94 ACTIVITY START DATE

lb/100 ft2

14-Feb<u>-94</u> COUNTRY CONTRACTOR / RIG AUSTRALIA CENTURY DRILLING / RIG - 11 G.F.E. RESOURCES LTD. TOWNSHIP REPORT FOR PORT CAMPBEL S. KELLY LOCATION FIELD OR BLOCK NO. WELL NAME AND NO. OTWAY BASIN, VICTORIA

IONA - 2		1 PPL - 2										
BIT DATA	ORILLIN	G STRING		CASINGS				PUMP				
Size ins	OD ins	ID ins Length m	Size ins	Di	epth m	Pump Make	ins	x ins	Eff %	bbl/stk	spm	bbl/min
		ID IIIO LONGETTI	Riser	Set @		National 7-F	5.5	7.75	95	0.0523		
Туре	Pipe 1		9.625		631.12	National 8-F	6	8.5	95	0.0705		
Nozzies 32nds	Pipe 2		7	Set @	1443.5							
ļ	Pipe 3		<del> </del>	Set @	1 1 10.0	Pump Press	- psi	i	TO	TAL bbl/m	nin	
	Col 1		ļ			MUD VOL	bbl		CHLAT	NG DAT	A	
	Col 2			Set @								m/min
Noz Area ins²	OPEN HO	LE SECTIONS		Set @		Downhole	239	Total		mins		тиунин
TFA ins²	Sect 1			Set @		Active	120	1 -		- mins	DP	
	Sect 2		Liner	Set @		Total Circ	359	Surfa	ce-bit	- mins	DC	
NV m/sec	Current	8.5 206.5		Top @		Reserve	47	ECD	ppg		Riser	
Impact lb f	Current		PERTIES			MUD	PROPE	RTY S	PECIFI	CATIONS	3	

Sample Location	IN or OUT				WEIGHT	ppg	VIS	sec	YP	16/100 π²
Time Sample Taken	hrs				API Filt	ml	HTHP	ml	KCL	%
Depth	m				BY AUTHOR	ITY				
Flowline Temp	°C				REMARKS					
Weight	ppg				Stock correc					e after
Funnel Viscosity	sec/qt				the end of th	e well. (D	T 334865 ar	nd DT 334	1857)	
Plastic Viscosity	сР						. to store	-61	-tion often o	nainoor rolease
Yield Point	lb/100 ft ²				27 sxs salt u	sed durin	g remainder	or compi	ellon alter el	ngineer release
Gels 10 sec/10min/30 min	lb/100 ft ²		 		1 PAC-R an	d 2 Soda	Asn most iik	cely used	during 8-1	72 110le.
		4	L	1	3					

**MUD PROPERTIES** 

ml/30min ml/30min

WEIGHT

% Vol Sand Methylene Blue cap ppb meter рΗ Aik. Mud Pm mi Alk. Filtrate, Pf/Mf ml mg/Lx103 Chlorides Total Hardness/Calcium mg/L % Wt Soln mg/Lx10³ K+ Ion Conc Sulphite Residual mg/L

32nd ins % Vol

% Vol

% Vol

600 rpm/300 rpm Rheometer lb/100 ft² 200 rpm/100 rpm 6 rpm/3 rpm

ACTIVITY

INVENTORY AND CONSUMPTION CONSUMPTION REC BAL COST MUD TYPE NaCl Brine PRODUCT DESCRIPTION USED SOLIDS CONTROL EQUIPMENT Additions bbl 200 50 kg Barite,sx Sea W Make screen size 320 25 kg Barite,sx 70 Drill W Shaker 1 TRITON 216 25 kg AQUAGEL,sx other Shaker 2 25 kg 80 KCL, Tech(sx) Shaker 3 other 32.3 25 kg 2 18 Soda Ash 208.17 Barite Shaker 4 27 213 25 kg SALT Chemicals 170.74 ppg bbl/hr hrs 14 PAC-R 50 lb bbl Losses Desander Sol. Con. Desilter 1. 72 Lost/Dumped Desilter 2 Down Hole Centrifuge 1 Newhole Centrifuge 2 **NET GAIN** 72 Discharged Solids Control Effic DAILY COST **CUMULATIVE COST** WAREHOUSE

**BAROID Engineer** OFFICE A\$ 30532.75 A\$ 411.21 ADELAIDE M. Olejniczak MELBOURNE 03 - 621 3311 059-787 103 Tel

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DESE	RVE PITS			SURVE	Y DATA			SOLIDS AN	IALYSIS	TIME BREAKDOWN	hrs
NO	TYPE	bbl	MD m	TVD m	INCL°	DIR °	DISP m	Low Grav. Solids	% Vol	Drilling	
	Pill Tank	14	IVID III	1,45,				Low Grav. Solids	ppb	Circulating	
- 0		33	<del> </del>					High Grav. Solids	% Vol	Reaming In	
	Trip Tank	33	<del> </del>					High Grav. Solids	ppb	Reaming out	
				<del></del>				ASG of Solids	g/cc	Tripping	
			<del> </del>					Cuttings Volume	bbl	Logging	
			<del> </del>	-				Interval Dilution	bbl/m	Other	
			-		<u> </u>			Interval Consumption	bbl/m		L
			<del> </del>				-			AVE ROP m/hr	<u> </u>

# APPENDIX 3

# **APPENDIX 3**

# A. DRILLING AND COMPLETION SUMMARY

IONA-2

#### **DRILLING SUMMARY**

Iona-2 was designed as a development well to better access the Waarre Formation reservoir discovered in Iona-1. The downhole location was approximately 270 metres from Iona-1, however the surface location was situated only approximately 50 metres away for operational reasons. The well was deviated to hit the target at the required location. The following is a short history of the well:

- Iona-2 was spudded at 1200 hrs on 14/2/94.
- 12¹/₄" hole was drilled to 320mKB.
- At this depth the downhole assembly was changed and a downhole motor, bent sub and Measured While Drilling (MWD) equipment were added. The hole was drilled to 640mKB building angle from 0° to 18.5° at a rate of 1.5°/30m.
- 54 joints of 9 ⁵/₈" 36 lb/ft, K55, BTC casing was run and cemented at 637mKB with lead slurry of 644 sacks of class 'A' cement and 2% pre-hydrated gel (13.2ppg) and tail slurry of 162 sacks of class 'A' cement (15.6ppg).
- After waiting on cement the Blow Out Preventers were nippled up and pressure tested. The shoe was drilled out and a leak off test was performed.
- 8½" hole was drilled to 774mKB. Deviation was monitored using single shot surveys.
- At this stage the bottom hole assembly was changed again, with a downhole motor and MWD equipment installed to bring the deviation angle back at the approximate rate of 2°/30m.
- 8½" hole was drilled to 1052mKB at which stage the pipe became differentially stuck.
- Water was spotted in the hole and the pipe was freed.
- The bottom hole assembly was then changed and a pendulum assembly was installed to bring back the deviation which, at this stage was 8°.
- 8½" hole was drilled to 1250mKB. Deviation was monitored using single shot surveys.
- The well was on target at this stage and the angle was  $2\frac{1}{2}^{\circ}$  so a bit and BHA change were made to control the angle and keep the well on target.
- 8½" hole was drilled to TD at 1650mKB at which stage a multi-shot survey was run.
- At this stage logs were run.
- A plug was run from 1470-1520mKB with 60 sacks class 'A' and 3% HR4.

• 120 joints of 7" 26 1b/ft, L80 NEWVAM-RS casing was run to 1448.8m KB and cemented with lead slurry of 439 cu ft of class 'G' cement with 4% pre-hydrated gel and tail slurry of 230 cu ft of class 'G' cement with 1% Halad 322. The cement was displaced with 180 bbls of mud.

#### **COMPLETION SUMMARY**

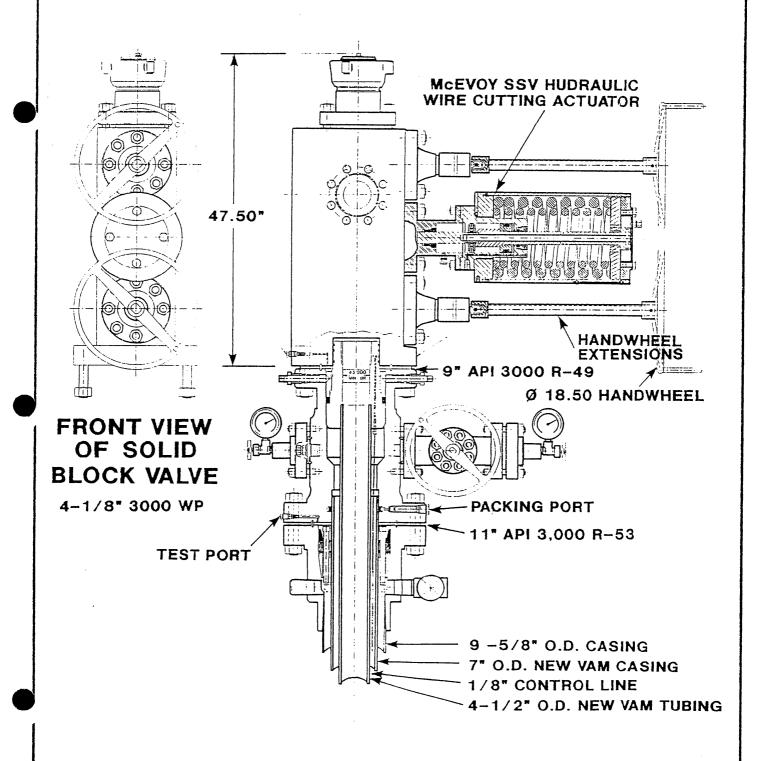
The well was completed in the Waarre Formation as a gas producer. There are two separate zones in the Waarre Unit C, both are in the same pressure regime. The bottom zone was perforated (overbalance) using a 4½" casing gun with Ultrapack 51B, 37 gram charges at 5spf run on wireline.

A permanent packer was set between the two zones and the completion was with  $4\frac{1}{2}$ " NEWVAM-RS, L80 12.6 ppf tubing and hydraulic set permanent packer set above the top zone. The top zone was left unperforated. However, there is provision to blank off the lower zone and perforate the top zone on wireline at a later date. The downhole completion diagram is shown in Figure A. The well head diagram is shown in Figure B.

A third gas zone was encountered in the Waarre Unit B. With no equivalent in Iona-1, this five-metre zone was not anticipated, and thus did not figure in the planned completion. However, it does represent an additional reserve, and how best to exploit it is still being investigated.



### IONA-2 SOLID BLOCK VALVE



### GFE RESOURCES LIMITED - IONA -2 WELL SCHEMATIC

<u>h)</u>	D Min ID (inch)	1 AR 1		KB = ! LENGTH (m)	
			4-1/2" 12.6 ppf L-80 New Vam RS Tubing (1 joint - #131)	9.320	15.020
4.892	3.958		4-1/2" 12.6 ppf L-80 New Vam RS Pup Joint	1.890	16.910
4.892	3.958		4-1/2" 12.6 ppf L-80 New Vam RS Tubing (130 joints #1-130)	1241.540	1258.450
4.892	3.958		4-1/2" 12.6 ppf 13% Cr New Vam RS Tubing (1 joint)	9.085	1267.535
4.990	2.992		4-1/2" x 3-1/2" New Vam RS Crossover 9 Cr 1 Mo (469-10-7886)	0.225	1267.760
3.900	2.992		3-1/2" 9.2 ppf 13% Cr New Vam RS Tubing (1 joint)	9.598	1277.358
4.580	2.813		3-1/2" x 2.813" XD SSD with 2.813" X profile (121 XD 28163) and 3-1/2" 9.2 ppf New Vam box x pin (9 Cr 1Mo)	1.274	1278.632
3.900	2.992		3-1/2" 9.2 ppf 13% Cr New Vam RS Tubing (1 joint)	9.602	1288.234
50	3.250		Size 80 DA 40 K-22S Anchor Tubing Seal Nipple with one V-Ryte Seal Unit and 3-1/2" 9.2 ppf New Vam box x blank chamfered bottom 9 Cr 1 Mo material & commodity number: 443-60-5000	0.317 (above packer)	1288.551
5.687	3.250		Size 84 SAB 40x32 Model SAB-3 Hydro-Set Packer with 4-1/2" 12.6 ppf New Vam box guide 70H Nitrile packing element and 9 Cr 1 Mo material & commodity number: 409-07-8426	1.506	1290.057
7.656	6.276 6.151 (drift)		7"26.0 ppf L-80 Casing (Setting Depth = 1450 m)		
4.510	3.960		Size 80 - 32 Millout Extension with 4-1/2" 12.6 ppf New Vam pin x pin, 9 Cr 1 Mo material & commodity number: 01-84643-1G	1.649	1291.706
4.510	3.960		Crossover with 4-1/2" 12.6 ppf New Vam box x 3-1/2" 9.2 ppf New Vam pin, 9 Cr 1 Mo material & commodity number: 469-10-898C	0.220	1291.926
4.920	2.992		3-1/2" 9.2 ppf 13% Cr New Vam RS Tubing (1 joint)	9.610	1301.536
	2.635 (no-go)		3-1/2" x 2.750" XN no-go Landing Nipple with 3-1/2" 9.2 ppf New Vam box x pin & 9 Cr 1 Mo material Serial Number:931001 0126	0.436	1301.972
3.980	3.010		3-1/2" Wireline Re-Entry Guide with 3-1/2" 9.2 ppf New Vam (RS) box x blank chamferred bottom, 9 Cr 1 Mo material & commodity number 469-21-355J	0.181	1302.133
.687	2.688		Size 84 - 26 Model DB Packer with 70H Nitrile packing element, 03.406" 8 Sub Acme box, 9 Cr 1 Mo material & commodity number: 415-05-8710	3 Packer Setting Dept 1. 106	h = 1330.000 1331.106
.610	2.688		Size 80 - 26 Seal Bore Extension with 3.406" 8 Stub Acme box x box, 9 Cr 1 Mo material & commodity number: 02-47470-83	1.637	1332.743
.990	2.390		Crossover with 3.406" 8 Stub Acme box x 2-7/8" 6.4 ppf New Vam pin 9 Cr 1 Mo material & commodity number: 02-43277-54	0.189	1322.932
	2.205 (no-go)	75	2-7/8" x 2.313" XN no-go Landing Nipple (11 XN 23187 04T-H4) with 2-7/8" 6.4 ppf New Vam box x pin & 9 Cr 1 Mo material	0.369	1333.328
.350	2.380	AA+	2-7/8" Wrieline Re-Entry Guide with 2-7/8" 6.4 ppf New Vam RS box x blank chamferred bottom & 9 Cr 1 Mo material	0.134	1333.462
		<b>I</b>	<u> </u>	along the hole Date : 5th Ma	
T 470	3			FIGI	JRE B

### **APPENDIX 3**

### **B. SUMMARY OF WELLSITE OPERATIONS**

**IONA-2** 

### DAILY DRILLING OPERATIONS SUMMARY

Date	Time	Hours	0	perations
14/2/94	0800-0900	1	-	Finalise rigging up
	0900-1200	3	-	Rig inspection by DME. Pre-spud meeting conducted by Rod Harris with all contractor personnel and service company personnel. Pre-spud safety meeting with rig crews by R. Giddens and K. Smith.
	1200-1530	31/2	-	Spud in and drill 12 1/4" hole from 16m to 61.7m
	1530-1600	1/2	-	Circulate and Survey @ 48.7m
	1600-1700	1	-	Drill 12¼" hole from 61.7m to 97.7m
	1700-1730	1/2	-	Circulate and Survey @ 84.7m
	1730-1800	1/2	-	Drill 12¼" hole from 97.7m to 132.4m
	1800-1830	1/2	-	Circulate and Survey @ 119.45m
	1830-1900	1/2	-	Drill 12¼" hole from 132.4m to151m
	1900-1930	1/2	-	Clear mud ring from conductor and flow-line
	1930-2100	1 1/2	-	Drill 12¼" hole from 151m to 168.7m with reduced bit weight
	2100-2130	1/2	-	Circulate and Survey @ 155.7m
	2130-2300	1 1/2	-	Drill 12¼" hole from 168.7m to 204.8m
	2300-2330	1/2	-	Circulate and Survey @ 191.8m
	2330-2400	1/2	-	Drill 12¼" hole from 204.8m to 232m
15/2/94	2400-0030	1/2	-	Drill 12¼" hole from 232m to 242m
	0030-0100	1/2	-	Circulate and Survey @ 229m
	0100-0200	1	-	Drill 12¼" hole from 242m to 270m
	0200-0230	1/2	-	Circulate and Survey @ 257m
	0230-0330	1	-	Drill 12¼" hole from 270m to 299m
	0330-0400	1/2	-	Circulate and Survey @ 286m
	0400-0430	1/2	-	Drill 12¼ " hole from 299m to 320m
	0430-0500	1/2	-	Circulate hole clean
	0500-0700	2	-	Pull out of hole to pick up kick-off assembly
	0700-0800	1	-	Make up kick-off assembly
	0800-1000	2	-	Pick up and make up kick-off assembly
	1000-1200	2	-	Run in hole with kick-off assembly. Install jars. Test run mud motor
	1200-1230	1/2	-	Continue RIH - Hole bridged @ 293m
	1230-1300	1/2	-	Repair shear-relief valve on pump - plugged bit jet
	1300-1330	1/2	-	Ream bridge from 293m to 305m. Continue to RIH
	1330-1400	1/2	-	Circulate and orientate motor
16/2/94	1400-0800	18	-	Drill deviated 12 ¼ " hole from 320m to 615m with Austoil, taking MWD surveys
	0800-1000	2	-	Drill deviated hole from 615m to 640m taking MWD surveys.

	1000-1030	1/2	-	Circulate bottoms up and work pipe. POOH, tight from 475m - pick up kelly and wash. Continue POOH, tight from
				456m to 579m.
	1030-1530	5	-	Work pipe @ 20,000lbs over-pull maximum - lay out jars.
	1530-1630	1	-	Service down-hole assembly and lay out same.
	1630-1830	2	-	Make up reaming BHA and run in hole
	1830-2330	5	-	Hang-up at kick-off point. Ream from 320m to 351m. Ream
				from 408m to 524m. Ream from 609m to 640m. (Run stand where possible) 3m of fill.
	2330-2400	1/2	-	Circulate hole clean.
17/2/94	2400-0500	5	-	Wiper trip to 8" drill collars. Strap out. Maximum drag 15,000lbs over. RIH. Maximum hold-up 10,000lbs. 2m of fill.
	0500-0530	1/2	-	Break circulation, wash and light ream to bottom.
	0530-0600	1/2	-	Circulate hole clean prior to running casing.
	0600-0800	2	-	Pull out of hole to run 95/8" casing.
	0800-0830	1/2	-	Lay out jars and slip 20' of drill-line.
	0830-1100	21/2	-	Continue POOH, lay out 8" DC's, stabilisers, Monel, hang-
				off sub, break bit and recover MWD tool.
	1100-1300	2	-	Rig up to run 9 ⁵ /8" casing - conduct safety meeting.
	1300-1700	4	-	Run 9 ⁵ /8" casing - loosen top casing collar.
	1700-1730	1/2	_	Safety meeting. Rig up Halliburton and load head.
	1730-1800	1/2	-	Circulate 1 ¹ / ₂ times casing volume.
	1800-2000	2	-	Pressure test lines, mix and displace cement with Halliburton.
			_	Wait on cement.
18/2/94	2000-0400	8	-	Head Halliburton. Lay out landing joint and conductor and
	0400-0800	4		nipple up BOP's.
			-	Nipple up BOP's.
	0800-1200	4	-	Install choke manifold and float line. Function test BOP's.
	1200-1400	2		Flush choke and BOP's.
			-	Pressure test. Blind rams to 300psi and 100psi. Pick up cup
	1400-1800	4		tester and test stack and pipe rams and all manifold valves to 2000psi. As well as HCR valve, manual choke line valve and both kill line valves. Repaired all leaks and re-tested until okay. Pressure test pipe rams to 300psi low and pressure
10/2/04	1900 0020	61/		tested angular preventor to 300psi and 1000psi.
19/2/94	1800-0030	61/2	-	Rig up floor. Pick up and clean and make up 8½: BHA and run in hole. Install casing protector rubbers every second joint and down pipe.
	0030-0100	1/2	_	Break circulation and tag cement @ 623-83m.
	0100-0230	11/2	_	Pressure test upper and lower Kelly cocks stabbing valve and
				flare line to 1000psi and secure flare line.
	0230-0300	1/2	-	Drill out cement and 5m of new hole.
	0300-0530	21/2	-	Circulate hole and run formation integrity tests -2.
	0530-0630	1	-	Drill 8½" hole from 645m to 666m.
	0630-0700	1/2	-	Run Single Shot Survey @ 660m.
	0700-0730	1/2	-	Drill 8½" hole from 666m to 705m.
	0730-0800	1/2	_	Run Single Shot Survey @ 660m.

		0800-0900	1	_	Drill 8½" hole from 705m to 743m.
)		0900-0930	1/2	-	Circulate and survey @ 736m. Single Shot.
		0930-1200	21/2	_	Drill 8½" hole from 743m to 781m.
		1200-1230	1/2	_	Circulate and survey @ 774m. Single Shot.
		1230-1300	1/2	_	Circulate hole clean.
		1300-1630	31/2	_	POOH. Lay out Jars, Stabiliser and Pony DC.
		1630-2130	5	-	Pick up stabiliser, Drillex motor, HO tool Jars and make up.
					Function Drillex motor. Run in hole.
		2130-2200	1/2	-	Pick up Kelly, Break circulation, tag bottom (no fill), orientate motor.
	20/2/94	2200-0800	10	_	Drill 8½" hole from 781m to 985m, taking mud surveys.
	20/2/2	0800-1130	$3^{1/2}$	-	Drill 8 ¹ / ₂ " hole from 823m to 1052m with MWD surveys.
		1130-1530	4	_	Work differentially stuck pipe. Spot water in hole and free
		1130 1330			pipe.
		1530-1600	1/2	-	Circulate water out of hole. Work pipe.
		1600-2030	$4^{1/2}$	-	Pull out of hole. Lay out jars, stabiliser and Drillex motor.
		2030-2300	$2^{1/2}$	-	Make up pendulum assembly and run in hole.
		2300-2330	1/2	-	Slip 20' of drill line.
	21/2/94	2330-0030	1	-	Run in hole. Bridge @ 1034m.
		0030-0130	1	-	Break circulation, ream and wash from 1024m to 1045m.
		0130-0230	1	-	Pull back to shoe to change out blown Kelly hose.
		0230-0530	3	-	Change out Kelly hose.
		0530-0600	1/2	-	Pressure test Kelly hose and fittings. Leaked @ goose neck
					nipple @ 1800psi.
		0600-0730	$1^{1}/2$	-	Remove goose neck for welding of new nipple to goose neck
					and re-install and pressure test to 1800psi.
		0730-0800	1/2	-	Install Kelly spinner, hose and Exlog depth measures.
		0800-0900	1	-	Run in hole from casing shoe. Clean to bottom 8m. No fill.
		0900-1830	$9^{1/2}$	-	Drill 8½" hole from 1052m to 1114m.
		1830-1900	1/2	-	Circulate and survey @ 1096m.
		1900-2030	11/2	-	Drill 8½" hole from 1114m to 1124m.
		2030-2100	1/2	_	Centre crown of mast over rotary table. Moved while
					working stuck pipe.
,	22/2/94	2100-0730	101/2	_	Drill 8½" hole 1124m to 1181m.
		0730-0800	1/2	-	Circulate and survey @ 1180m.
		0800-0830	1/2	-	Work pipe free - grabbed while working pipe on survey.
		0830-1900	101/2	-	Drill 8½" hole from 1181m to 1268m.
		1900-1930	1/2	-	Circulate hole clean prior to wiper trip.
		1930-2100	11/2	-	Wiper trip back to 900m. Hole okay. No fill.
		2100-2200	1	-	Circulate hole clean.
		2200-2230	1/2	-	Survey @ 1250m.
		2230-2300	1/2	-	Displace Barite pill.
		2300-2330	1/2	-	Re-run survey @ 1250m.
	23/2/94	2330-0200	21/2	-	Pull out of hole for new bit and BHA change. Flow check.
		0200-0330	1 1/2	-	Lay out 6 x 6 ¹ / ₄ " DC's, Jars and key seat wiper.
		0330-0430	1	-	Continue pulling out of hole, lay out stabilisers, cross overs
					and Monel.
		0430-0600	1 1/2	_	Make up new BHA.
)		0600-0800	2	-	Run in hole.

	0800-0830	1/2	-	Slip 20ft of drill-line.
	0830-0930	1	-	Continue running in hole.
	0930-1030	1	-	Pick up drill pipe. Break circulation. Wash and light ream
				1245 to 1268m.
	1030-1830	8	_	Drill 8½ hole from 1268m to 1363m with flow checks.
	1830-1900	1/2	_	Circulate and survey @ 1345m.
24/2/94	1900-0530	101/2	_	Drill 8½" hole from 1363 to 1468m.
2 ., 2. , .	0530-0600	1/2	_	Circulate and survey @ 1450m.
	0600-0800	2	_	Drill 8½" hole from 1468m to 1498m.
	0800-1900	11	_	Drill 8½" hole from 1498m to 1650m TD.
	1900-2000	1	_	Circulate bottoms up for geological sample.
	2000-2030	1/2	_	Single Shot Survey @ 1632m.
	2030-2400	31/2	_	Wiper trip from 1650m to 631m - hole tight through
	2030-2400	372	-	Eumeralla Fm. after pulling two stands.
25/2/94	2400-0200	2		Run in hole to T.D hole good.
23/2/94	0200-0330	1 1/2	-	
		1/2	-	Break circulation and circulate prior to logging - 5m of fill.
	0330-0400		-	Pump barite pill and drop multi-shot survey barrel.
	0400-0600	2	-	Pull out of hole to log - strap pipe.
	0600-0630	1/2	-	Recover survey barrel.
	0630-0800	1 1/2	-	Pull out of hole.
26/2/04	0800-0930	$1\frac{1}{2}$	-	Pull out of hole.
26/2/94	0930-0100	$16\frac{1}{2}$	-	riora parcel macring man community and ab and ram refer
				with Schlumberger. Run #1 DLT, SDT, SRT, GR and
				AMS. Run #2 LDL, CNL, GR and AMS. Run #3 WST.
	0100 0200	2		Rig down Schlumberger.
	0100-0300	2	-	Made up BHA and RIH to shoe.
	0300-0400	1	-	Slip 26 ft and cut 130 ft of drill line.
	0400-0630	1 1/2	-	Continue running in hole - Hole good - 1m of fill.
	0630-0800	11/2	-	Circulate hole and condition mud.
		_		Hole took 27.5 bbl while logging.
	0800-0900	1	-	Condition mud while circulating - flow check.
	0900-1230	31/2	-	Pull out of hole.
27/2/94	1230-0530	17	-	Rig up Schlumberger and run RFT-GR-AMS. Run CST.
	0.700 0.700	411		Diale up our testor and test DOD stock and manifold to 2000
	0530-0700	1 1/2	-	Pick up cup-tester and test BOP stack and manifold to 2000
	0700 0000	4		psi and 300 psi. Run in hole with BHA.
	0700-0800	1	-	
	0800-1030	21/2	-	Lay out 8½" BHA.
	1030-1330	3	-	Run in hole with open end down pipe to 1520m.
	1330-1430	1	-	Circulate bottoms up from 1520m.
	1430-1530	1	-	Rig up Halliburton and run Plug #1 at 1520-1470m with 60
				sacks Class 'A' and 3% HR-4.
	1530-1830	3	-	Pull out of hole.
	1830-2030	2	-	Pick up 4 DC, make up bit and RIH to casing shoe.
	2030-2200	1 1/2	-	Wait on cement.
	2200-2330	1 1/2	-	RIH. Tag top of plug at 1471m. Pull back to 1459m.
28/2/94	2330-0100	1 1/2	-	Circulate hole clean.
	0100-0500	4	-	Lay out drill pipe.
	0500-0700	2	-	Lay out Kelly and swivel.
	0700-0730	1/2	-	Run extra pipe from derrick in hole.
	0730-0800	1/2	-	Lay out drill pipe.

	0800-0930 0930-1000 1000-1300	1½ ½ 3	-	Lay out down pipe and 4 drill collars.  Re-centre crown of derrick over rotary table.  Change pipe rams to 7". Make up cup tester and test ram door seals to 600 psi. Rig up Enterra equipment and trial.  Rig up to run 7" casing. Safety meeting with Enterra crew.
	1300-2230 2230-2400	9½ 1½	-	Run 7" casing.  Head up Halliburton and circulate casing - casing differentially stuck while heading up.
1/3/94	2400-0230	21/2	-	Safety meeting with Halliburton. Pressure test lines, pump pre-flush, mix and displace cement as per programme.
	0230-0330	1	-	Flush BOP's and set slip and seal assembly in bowl.
	0330-0800	41/2	-	Tear out and lift BOP. cut casing, remove spacer, spool and make final cut and trim on casing.
	0800-1330	$5\frac{1}{2}$	-	Install 'B' section and nipple up BOP's.
	1330-1530	2	-	Energise secondary seal and try to pressure test - unable to pressure test secondary seal - bypassing slip and seal assembly.
	1530-1700	1 1/2	-	Lift stack and remove 'B' section.
	1700-2400	7	-	Wait on casing spear to re-set slip and seal assembly.
2/3/94	2400-0300	3	-	Make up casing spear. engage casing and pull to 175,000lbs (70,000lbs over casing weight) and re-set slips. Lay out casing spear and drill collars.
	0300-0600	3	- ·	Make final cut and trim to casing, nipple up 'B' section, energise secondary seal and test to 3,000 psi - Okay.
	0600-0800	2	-	Nipple up BOP's.
	0800-0830	1/2	-	Nipple up BOP. Function rams.
	0830-1030	2	-	Make up cup-tester on $2^7/8$ " tubing, hang power tong and Enterra tong to make-up tools.
	1030-1130	1	-	Rig up North Paaratte pump and attempt to pressure test - nil pressure.
	1130-1200	1/2	-	Pressure test with Halliburton - unable to hold pressure.
	1200-1230	1/2	-	Remove rams and inspect - one ram block installed upside down - replace correctly.
	1230-1330	1	-	Pressure test 2 ⁷ / ₈ " pipe rams to 300psi and 2000psi; HCR and manual choke line valves to 2000psi; flare line to 1500psi.
			-	Lay out cup tester, make up casing scraper and 6" bit and run
	1330-2200	$8^{1/2}$		in hole picking up $2^{7/8}$ " tubing.
	2200-2330	11/2	-	Displace hole to water by reverse circulation, pump Hi-vis sweep and displace hole to brine. Pull out of hole with casing scraper.
			_	Slip 40' of drill line and change 27/8" rams to 7" rams.
3/3/94	2330-0200 0200-0800	2½ 6	-	Rig up Schlumberger, install 7" joint of casing in rams for line wiper and run logs with Schlumberger.
		-		1

	0800-0930	1 1/2		Run CBL, VDL, GR and CCL with Schlumberger and rig
	0800-0930	1 72	-	down.
	0930-1100	1 1/2	-	Make up and fit safety chain pad eyes to 7" lubricator prior to running perforating gun.
	1100-1530	41/2	-	Load perforating gun, install 7" lubricator, perforate 7" casing at 1340.5m to 1334.5m and rig down Schlumberger.
	1530-1630	1	-	Make up cup-tester, change 7" rams to $2^{7/8}$ ". Pressure test rams to 350psi and 1800psi with rig pump.
	1630-2000	31/2	-	Run in hole with casing scraper on $2^{7/8}$ " tubing. Flow-check, work scraper from 1325.23m to 1354.17m.
	2000-2030	1/2	-	Pump Hi-vis sweep and circulate back to surface.
4/3/94	2030-2330	3	-	Pull out of hole with work string and scraper.
	2330-0530	6	-	Rig up Schlumberger and run gauge rings and junk basket - Run #1. Set production packer at 1330m - Run #2.
	0530-0600	1/2	-	Break out bit and scraper and make up seal assembly on work string.
	0600-0800	2	_	Run in hole with seal assembly on work string.
	0800-0930	1 1/2	-	Run in hole with seal assembly on work string.
	0930-1000	1/2	-	Pressure test annulus and packer to 1000psi with Halliburton.
	1000-1530	$5^{1/2}$	_	Lay out 2 ⁷ / ₈ " work string.
	1530-1900	31/2	-	Rig up Enterra and rig up to run 4½" tubing. Change pipe rams, test to 400psi low and 1800psi high. Held safety meeting with Enterra and Baker prior to running 4½" tubing.
5/3/94	1900-0600	11	-	Make up upper assembly with Baker and run in hole on 4½" production tubing with Enterra. Land 131 Joints and 1 Pup at 1288.80m.
	0600-0730	1 1/2	-	Rig up Expertest and make up Pup Joints to mount Expertest lubricator.
	0730-0800	1/2	-	Run PXX plug in hole on wire-line with Expertest.
				Hole began taking on fluid following perforating at 1240hrs on 3 March, 1994 at a rate of 2.3bbl/hr.
				It took 34bbl's in 22hrs and 5bbl's in the next 14 hrs.
				It displaced a calculated 17bbl's while running 4½" tubing.
	0800-0900	1	-	Set PXX Plug with Expertest and pull out of hole and run prong.
	0900-1000	1	-	Pressure up on tubing to set packer - pressure drop from 500psi. Increase up to 2500psi and maintain with pump - pressure still droping with pump off.
	1000-1230	21/2	-	Run in hole with Expertest to retrieve prong - washed due to shallow engagement - RIH with shorter prong, failed to shear, changed shear pin and located.
	1230-1300	1/2	_	Re-run packer setting routine to 2500psi - no leak.
	1300-1330	1/2	_	Pressure test annulus to 1000psi - no leak.
	1330-1430	1	_	Run in hole with Expertest and open 3½" SSD.
	1330 1430	1		Trail III II II II II II II II II II II II I

	1430-1500	1/2	-	Install back pressure valve and pressure test annulus and underside of BPV to 1000psi - no leak.
	1500-1800	3	_	Nipple down BOP's and lay out.
	1800-2230	41/2	-	Install Christmas Tree and pressure test with Cooper Oil
	1000-2250	7/2		Tools engineer as per completion program.
	2230-2300	1/2	_	Rig up Expertest and pressure test lubricator.
	2300-2400	1		Displace hole with 62bbl of diesel fuel.
6/3/94	2400-0030	1/2	-	RIH with Expertest and close SSD. Rig up Halliburton and
				pressure test tubing to 2000psi.
	0030-0230	3	-	Bleed pressure back to 200psi and run in hole with Expertest and recover 3½" OTIS PXX plug and prong.
	0230-0300	1/2	_	Pressure test annulus to 1000psi.
	0300-0330	1/2	-	Rig down Expertest and dismantle lubricator.
	0330-0430	1	-	Rig up and displace 62bbl of diesel fuel into production tubing.
	0430-0600	1 1/2	_	Wait on day-light to flow well.
	0600-0800	2	-	Bring well on stream, recover at much diesel fuel as possible, divert to flare-line and flow well.
			No	te: Change from Daylight Saving (Eastern Summer time) to Eastern Standard Time at 0200hrs 6/3/94. (i.e., gain extra hour by shifting clock back.)
	0800-0830	1/2	-	Flow and burn off gas to clean up well.

Rig released at 1000hrs Eastern Standard Time 6 March, 1994

Tools' equipment and chicksans. Release Rig.

Install BPV, bleed-off pressure to check BPV holding, bleed

trapped pressure from master valve and rig down Cooper Oil

0830-1000

11/2

# APPENDIX 4

# **APPENDIX 4**

### A. SAMPLE DESCRIPTIONS

**IONA-2** 

WELL:	IONA	A NO.2 DATE: 14/02/94 to 19/02/94				SHOWS			
GEOLOGIST:	MUD	LOGGERS PAGE: 1 of 9		GAS	СОМРО	NENTS	(PPM)	FL	JOR
DEPTH (m)	%	SAMPLE DESCRIPTION	TOTAL GAS UNITS	C1	C2	СЗ	C4	NAT.	СИТ
150-280	100	Marl; medium green-grey, brownish-grey; very fossiliferous with abundant bryozoa, gastropods, spong spicules, shell fragments; foraminifera; soft, massive		-	_	-	-	_	-
280-290	30	Marl; as above	-	-	_	-	-	-	_
	70	Sandstone; dark brown, orange-brown; vf-pebbly, dom. cse-v cse; poorly sorted; subang-subrndd, dom. subrndd qtz; abdt. brown FeO; strong calcite cement grading to sandy limestone							
290-300	80	Sandstone; as for 280-290		-	-	-	-	-	_
	20	Marl; as for 150-280							
300-450	100	Sandstone; as for 280-290	-	-	-	_	-	-	-
450-460	80	Sandstone; as for 280-290	-	-	-	-	-	_	-
	10	Siltstone; meddark brown; tr. micromicaceous; occ. arenaceous grading into very fine sandstone							
	10	Claystone; dark brown, dark grey; very silty; micromicaceous; soft; dispersive							
460-470	70	Sandstone as for 450-460	-	-	-	-	_	_	-
	10	Siltstone as for 450-460							
	20	Claystone as for 450-460							
470-490	80	Sandstone as for 450-460	-	-	_	-	-	-	-
	10	Siltstone as for 450-460							
	10	Claystone as for 450-460							
490-500	90	Sandstone as for 450-460	-	-	-	-	-	-	-
	10	Claystone as for 450-460				,			

WELL:	IONA	A NO.2 DATE: 14/02/94 to 19/02/94				SHOWS	3		
GEOLOGIST:	MUD	LOGGERS PAGE: 2 of 9		GAS	СОМРО	NENTS	(PPM)	FLU	JOR
DEPTH (m)	%	SAMPLE DESCRIPTION	TOTAL GAS UNITS	C1	C2	СЗ	C4	NAT.	CUT
500-510	20	Claystone as for 450-460	-	_	-	_	-	-	_
	80	Sandstone; off white, very light grey-brownish; fine-very fine, dom. very fine; ang- subrndd; very strong calcite cement; com. white argillaceous matrix; mod. Silty; com. dark brown and red lithics; occ. vf glauconite; poor vis. porosity; mod. hard							
510-520	90	Sandstone as for 500-510	-	_	-	-	-	_	-
	10	Claystone as for 500-510							
520-530	100	Sandstone as for 500-510	-	-	-	-	-		-
530-540	40	Sandstone as for 500-510	0.1	1	-	-	-	-	-
530-540	60	Claystone; meddark brownish grey; occ. mod. silty; tr. vf-cse subang qtz grains; tr. glauconite; tr. dolomite nodules; tr. common pyrite and maracsite; tr. micromicaceous; massive; soft, sticky							
540-550	80	Claystone as for 530-540	0.1	15	1	1		-	-
	20	Sandstone as for 530-540							
550-570	10	Sandstone as for 530-540	1.0	120	15	11	-	-	-
	90	Claystone as for 530-540							
570-610	100	Claystone as for 530-540	1.6	180	35	22	_	_	_

WELL:	IONA	NO.2 <b>DATE:</b> 19/02/94 to 25/02/94				SHOWS	3		
GEOLOGIST:	V. A	(BARI PAGE: 3 of 9		GAS	СОМРО	NENTS	(PPM)	FLU	JOR
DEPTH (m)	%	SAMPLE DESCRIPTION	TOTAL GAS UNITS	C1	C2	СЗ	C4	NAT.	CUT
610-620	80	Claystoneas for 530-540	0.4	35	2	1		-	_
	20	Sandstone; light brown; vf-pebbly at top becoming vf-cse, dom. cse with depth; mod. sorted; subang-rndd; weak silica cement; abdt. meddark brownish grey argillaceous and silty matrix; trace volcanic lithics, tr. brown FeO stain; dom. Loc very poor to good visual porosity		55	3	2	-	-	_
620-630	80	Sandstone as for 610-620, dom. fine grained							
	20	Claystone as for 530-540							
630-640	30	Claystone as for 530-540	0.1	10	1	-	-	-	-
	70	Sandstone as for 610-620							<u> </u>
640-675	100	Sandstone; light brown; vf-cse-pebbly, dom. med; poorly sorted; subang-subrnd dom. subrndd qtz; abdt. dark brown silty matrix; tr. lithics; tr. FeO; loose; poor vis porosity		1	-	-	, -	-	-
	tr.	Coal; dark brown-black. firm							
705-745	90	Sandstone; light-med grey; vf-cse-pebbly, dom. cse.; poorly sorted; subang- subrndd, dom. subrndd qtz; tr. multi-colour lithics; tr. mica; tr. pyrite; no apparent cement; unconsolidated; good vis. porosity							
	tr.	Coal; dark brown-black; firm							
	tr.	Claystone; dark brown-greyish; silty, soft and dispersive							
745-775	100	Sandstone; as for 705-745 becoming f-med., dom. med. grained	0.1	5	-	-	_	_	-
775-820	100	Sandstone; as for 745-775m becoming coarse and pebbly with depth	0.1	4	-	-	-	_	-

		NO.2 <b>DATE</b> : 19/02/94 to 25/02/94				SHOWS	3		
GEOLOGIST:	V. Al	KBARI PAGE: 4 of 9		GAS (	ОМРО	(PPM)	FLUOR		
DEPTH (m)	%	SAMPLE DESCRIPTION	TOTAL GAS UNITS	C1	C2	СЗ	C4	NAT.	CUT
820-930	90	Sandstone; light-med. grey; vf-cse-pebbly, dom. coarse; poorly-mod.sorted; subang-subrndd dom. subrndd qtz; tr. mica; tr. pyrite, common multi-coloured lithics; no apparent cement Good intergranular porosity; soft; unconsolidated	0.1	4	-	-	-	-	_
	5	Coal dark brown-black; firm with conchoidal fracture							
	5	Claystone; med. grey; silty; micaceous; carbonaceous; soft, dispersive							
930-965	90	Sandstone as for 820-930	0.1	3	-	-	-	-	-
	5	Claystone as for 820-930							
	5	<b>Coal</b> as for 820-930							
965-985	80	Sandstone; light grey; vf-cse; often pebbly, dom. fine; poorly-mod. sorted; subang-subrndd; dom. subrndd. qtz, com. pyrite, com. lithics, com. carb. detritus; rare mica; com. clay matrix; poor porosity; soft							
	20	Claystone; light grey; micromic; carbonaceous silty, soft, dispersive							
985-1030	90	Sandstone; light grey, translucent; f-cse often pebbly, dom. med; poorly-mod. sorted; subang-subrndd, dom. subrndd qtz; rare pyrite, rare-com. multi-colour lithics; rare mica; com. dark grey argill. matrix increasing with depth; poor vis. porosity; soft; friable							
	10	Claystone; med-dark grey, silty; com. carb. detritus; micromicaceous; soft; dispersive							
	tr.	Coal; dark brown-black; firm							
1030-1505	80	Sandstone; as 985-1030 becoming very fine often grading into argillaceous	0.1	5	1	-	-	-	-
	20	<b>Claystone</b> as 985-1030	***************************************			·			

WELL: GEOLOGIST:		DATE: 19/02/94 to 25/02/	94		SHOWS							
	1 %	PAGE: 5 0f 9		GAS	COMP	DNENTS	(PPM)	FI	UOR			
DEPTH (m)	/0	SAMPLE DESCRIPTION	TOTAL GAS Units	C1	C2	СЗ	C4	NAT.	CU.			
1050-1060	20	Sandstone; light-medium grey, brownish; vf-cse, dom. f; mod. sorted; subang subrndd, dom. subrndd. qtz; rare lithics; rare mica; rare-com. carb. detritus; trargillaceous matrix; rare silica cement; poor porosity; soft	J- 0.1 com.	3	-	-	-					
	80	Claystone; medium-dark grey, brownish; very silty; often grading to siltstone; carb. detritus; micromicaceous; very soft and dispersive	com.									
1060-1080	90	Claystone as 1050-1060	0.1	5								
	10	Sandstone as 1050-1060			-							
1080-1090	30	Sandstone as 1050-1060	0.1	9								
	70	Claystone as 1050-1060		-								
1090-1105	90	Claystone as 1050-1060	0.2	36	2							
	10	Sandstone as 1050-1060										
1105-1115	100	Claystone; dark grey, greenish; silty; carbonaceous; micromicaceous; rare glauconite; soft, dispersive	0.4	75	3	1						
1115-1120	80	Claystone as 1105-1115	1.9	350	5	4						
	20	Sandstone; light grey; transl; fmed; dom.f; subang-subrndd, dom. subrndd; qcom.f. multi-colour lithics; rare mica; rare pyrite; rare-com. carbonaceous detriticom. argillaceous matrix; poor vis. porosity; soft	z; ıs;		0	4						
1120-1140	100	Claystone as for 1105-1115 beocming more silty with depth grading into argillaceous siltstone	2.8	500	10	8						
1140-1145	100	Siltstone; light-med. grey, brownish; carbonaceous, micromicaceous; abdt. argillaceous matrix; soft, dispersive	6.5	1240	12	8	1					
1145-1163	100	Siltstone as 1140-1145	0.0				- 1					
/ac:ionasd.dsk			9.9	1765	48	30	4					

WELL:	ION	NO.2 <b>DATE</b> : 19/0	2/94 to 25/02/94				SHOWS	;		
GEOLOGIST:	V. A	KBARI PAGE: 6 of	<b>PAGE</b> : 6 of 9			СОМРО	FLUOR			
DEPTH (m)	%	SAMPLE DESCRIPTION	V	TOTAL GAS UNITS	C1	C2	С3	C4	NAT.	сит
1163-1175	100	Sandstone; greenish, translucent; vf-med; dom.f; subang-sub qtz; rare-com. dark green glauconite, no apparent matrix; good porosity, loose	rndd, dom. subrndd. d intergranular	32.4	6000	160	40	10		
1175-1180	100	Sandstone; very light green; vf-med., dom. med; mod-sorted; dom. subrndd qtz; rare com dark green glauconite; rare colour matrix; good vis. porosity; soft; loose	subang-subrndd, ed lithics; no apparent	28	5185	105	45	20		
1180-1190	80	Sandstone; as 1175-1180		6.5	1240	12	8			
	20	Claystone; med-dark grey; silty grading to argillaceous siltstor carbonaceous; soft and dispersive	ne; micromicaceous;							
1190-1245	90	Sandstone as 1175-1180 becoming more glauconitic with dep	oth	26.4	5050	80	18	4		
	10	Claystone as 1180-1190								
1245-1250	20	Claystone as 1180-1190								
	80	Sandstone as 1190-1245		6.5	1280	8	3	1		
1250-1265	80	Claystone; dark grey-greenish; silty; comabdt. glauconite no carbonaceous detritus; rare pyrite; very soft and dispersive	dules; com.	2.3	448	6	2			
	15	Sandstone as for 1175-1180								
	5	Coal; dark brown-black; firm		***************************************						
1265-1270	90	Claystone as for 1250-1265	24/02/94	1.7	312	9	3	0	· · · · · · · · · · · · · · · · · · ·	
	10	Sandstone as for 1190-1245								
1270-1295	95	Claystone; dark grey, silty; very glauconite. abdt. fine-med. no glauconite, decreasing with depth; com. pyrite; carbonaceous,	odules of dark green very soft; dispersive	6.7	1200	30	23	2		
	6	Sandstone as for 1190-1245								

WELL:	IONA	NO.2 DATE: 19/02/94 to 25/02/94				SHOWS	3		
GEOLOGIST:	V. A	KBARI PAGE: 7 of 9		GAS	СОМРО	FLUOR			
DEPTH (m)	%	SAMPLE DESCRIPTION	TOTAL GAS UNITS	C1	C2	СЗ	C4	NAT.	CUT
1295-1300	80	Claystone as for 1270-12950 rare-com. glauconite	8	1400	59	23	2		I
	20	Sandstone; light grey-tan-brownish; fmed.; dom. med.; poorly-mod. sorted; subang-subrndd dom. subrndd qtz; rare-com. glauconite; com. pyrite; weak calc. cement; poor vis. porosity; soft-mod. hard  TOP WARRE FM. UNIT D 1299m							
1300-1317.5	90	Claystone; dark grey, silty; carbonaceous rare-com. glauconite; rare pyrite, soft; dispersiv	32	5073	425	126	28		
	10	Sandstone as 1295-1300							
		TOP UNIT C: 1317.5m							
1317.5-1350	90	Sandstone; light-brownish-grey; translucent; vf-cse, dom. med; poorly -med sorted; subang-subrndd; dom-subrndd qtz; weak silica cement; slightly calc; tr. pyrite; tr. glauconite; tr-com. multi-colour lithics; good intergranular porosity; softmod. firm	255	43200	2006	794	279		
	10	<b>Claystone</b> as for 1300-1317.5							
		TOP UNIT -B: 1349.5							
1350-1355	50	Claystone as for 1300-1317.5	10.7	1840	60	47	9		
	50	Sandstone as for 1317.5-1350							
1355-1365	40	<b>Sandstone</b> as for 1317.5-1350	36.5	6240	263	120	40		
	60	Claystone as 1300-1317.5							
1365-1375	70	Claystone as 1300-1317.5	159	31000	310	57	33		
	30	Sandstone 1317.5-1350 tr. mod. bright yellow fluor with instant milky cut with thin residue						10-30	milk
		TOP UNIT A; 13082m						mod br yell	white

WELL:	IONA	ONA NO.2 DATE: 19/02/94 to 25/02/94		19/02/94 to 25/02/94	SHOWS							
GEOLOGIST:	V. A	KBARI	14 A	PAGE:	8 of 9		GAS	СОМРО	NENTS	(PPM)	FLU	JOR
DEPTH (m)	%		SAMPLE 1	DESCRIPT	ION	TOTAL GAS UNITS	C1	C2	СЗ	C4	NAT.	CUT
1375-1400	90	dom. subrndd qtz	z; com-rare multi-color or fair vis. porosity mo	ur lithics; rare mid	sorted; subang-subrndd, ca; com. carb-detritus; mod.	77	1500	133	22	6		
1400-1415	80	Sandstone; whit subradd qtz; com		rare-com. altered		12.4	2200	60	40	8	br yell 10-30	residue
	20		-med grey, brownish; s ; carbonaceous; soft a		olour lithics;							
1415-1435	70	Sandstone as 14	400-1415			390	61000	3150	960	70	10	milky white
	30	Claystone as 14	100-1415									
1435-1460	90	Claystone as 14	100-1415									
	10	Sandstone as 14	400-1415									
1460-1485	60	Sandstone as 14	400-1415									
	40	Claystone as 14	100-1415									
1485-1500	80	Sandstone as fo	or 1400-1415			175	21600	2190	1630	860	tr.	
	20	Claystone as for	r 1400-1415									
1500-1520	70	Claystone; very coloured lithics; v	light grey-bluish; silty; very soft, sticky	; micromicaceous	s; carbonaceous; rare-com.	41	7600	135	90	22		
	30	subang-subrndd,	dom. subrndd qtz; co	m. multi-colour lit	f; poorly-mod. sorted; hics, tr. white and brown vis. porosity, mod. firm							
1520-1530	60	Sandstone as 15	500-1520			33	6080	115	80	17		
	40	Claystone as 15	500-1520						T-			

WELL:	IONA	A NO.2 DATE: 19/02/94 to 25/02/94	DATE: 19/02/94 to 25/02/94 SHOWS							
GEOLOGIST:	V. A	KBARI PAGE: 9 of 9		GAS	GAS COMPONENTS (PPM)				FLUOR	
DEPTH (m)	%	SAMPLE DESCRIPTION	PLE DESCRIPTION GAS UNITS	C1	C2	С3	C4	NAT.	CUT	
######################################										
1530-1545	80	Claystone as 1500-1520	15.5	2720	105	57	14			
	20	Sandstone as 1500-1520								
1545-1590	90	Sandstone; light grey-greenish; vf-med; dom. f; mod. sorted; subang-subrndd; dom. subrndd qtz; comabdt. multi-colour lithics; rare white and black mica; tr. altered feldspars; weak silica cement; slightly calcareous; poor porosity; mod. firm	46	800	398	119	30			
1590-1600	60	Claystone as 1545-1590	39	6960	260	94	24			
	40	Sandstone as 1545-1590								
1600-1615	80	Sandstone as 1545-1590	31	5440	254	63	9			
	20	<b>Claystone</b> as 1545-1590								
1615-1625	70	Claystone as1545-1590	31.2	5400	265	82	16			
	30	Sandstone as 1545-1590								
1625-1630	50	Sandstone as for 1545-1590	13	2280	106	44	3			
	50	<b>Claystone</b> as 1545-1590								
1630-1645	70	Claystone as 1545-1590	18.8	2960	177	69	16			
	30	<b>Sandstone</b> as 1545-1590								
1645-1650	90	Claystone as 1545-1590	6	1032	40	20	2			
	10	<b>Sandstone</b> as 1545-1590								

TOTAL DEPTH: 1650m REACHED AT 1915 HOURS ON 24 FEBRUARY 1994

### **APPENDIX 4**

### **B. DAILY LITHOLOGICAL DESCRITPIONS**

IONA-2

Interval	De	escription	Total Gas (units)	R.O.P. (m/hr)
320-336	-	SANDSTONE: light to occasionally dark brown, medium brown to orange, fine to occasionally very coarse, dominantly subrounded, occasionally round, poor sorting, occasional brown to orange marl matrix, commonly brown iron oxide stain quartz, occasionally glauconitic, trace pyrite, micaceous flakes, fossil fragments, loose grains with occasional brittle aggregates, poor to fair visual porosity, no oil fluor.	NIL	40-120 (Av. 75)
336-541	-	SANDSTONE: grading to and interbedded SILTY CLAYSTONE. SANDSTONE: light grey to light brownish grey, clear to translucent quartz grains occasionally with brown iron oxide stain, very fine to very coarse, dominantly fine to coarse, subangular to subrounded, moderately sorted, very weak silica cement, occasional streaks calcareous cement, trace to abundant medium to dark brownish grey argillaceous and silica matrix, trace glauconite, micacaeous flakes, fossil fragments, black coal, brown to reddish lithics, pyrite, loose to friable, poor to good visual porosity, no oil fluor. SILTY CLAYSTONE: dark brown, often very fine to coarse dispersive, quartz grains in place, non calcareous, commonly metamorphic, soft, sticky, moderately to very dispersive, massive.	NIL	3.5-260 (Av. 100)
541-612	-	MASSIVE CLAYSTONE. CLAYSTONE: medium to dark brown to dark brownish grey, occasionally moderately silty, trace dispersed very fine to coarse quartz grains, trace glauconite, dolomitic nodules, pyrite marcasite and metamorphics, soft, sticky, massive.	0.1 - 1.6	22-55 (Av. 40)

•	Interval	Description	Total Gas (units)	R.O.P. (m/hr)
•	612-640	- SANDSTONE: interbedded with and grading to CLAYSTONE. SANDSTONE: light brown, very fine to pebbly, becoming coarse with depth, subangular to rounded, very poor sorting at top becoming moderately sorted with depth, weak siliceous cement, abundant medium to dark brown grey argillaceous and silty matrix in place, rare volcanic lithics, commonly brown argillaceous and iron oxide rich lithics in part, trace brown iron oxide stain on quartz grains, friable to dominantly loose, very poor to good visual porosity, no oil fluorescence.  CLAYSTONE: medium brown, trace brick red, occasional quartz pebbles, trace volcanic lithics, trace brown limestone, trace fossil fragments, trace pyrite, firm, massive.	0.1 - 1.6	6-240 (Av. 75)
	640-675	- SANDSTONE: light brown, very fine to coarse to pebbly, dominantly medium, poorly sorted, subangular to subrounded quartz, trace lithics, trace iron oxide, abundant brown, silty matrix, poor visual porosity, friable.	NIL	40-240 (Av. 100)
ı	675-705	- SANDSTONE: white to light grey, translucent, very fine to coarse to pebbly, dominantly coarse, poorly sorted, subangular to subrounded, dominantly subrounded quartz, trace multi-color lithics, trace mica, trace pyrite, trace brownish to grey silty matrix, poor visual porosity, soft unconsolidated, trace COAL: dark brown to black, firm.	NIL	80-300 (Av. 160)
	705-745	- SANDSTONE: light to medium grey, very fine to coarse to pebbly, dominantly coarse, poorly sorted, subangular to subrounded, dominantly subrounded quartz, trace mica, trace multi-color lithics, no apparent cement, good inter-granular porosity unconsolidated, interbedded with thin COAL: dark brown to black, firm and CLAYSTONE: medium grey silty, dispersive.	NIL	50-30 (Av. 120)
	745-775	- SANDSTONE: as from 705-775, becoming fine to medium, dominantly medium.	0.1	20-50 (Av. 30)
į	775-820	- SANDSTONE: as from 745-775 becoming coarse and pebbly with depth.	0.1	40-220 (Av. 120)

	Interval	Description	Total Gas (units)	R.O.P. (m/hr)
	820-930	- SANDSTONE: light to medium grey, very fine to pebbly, dominantly coarse, poorly to moderately sorted, subangular to subrounded, dominantly subrounded quartz, trace mica, trace pyrite, commonly multi-color lithics, good inter-granular porosity, soft, unconsilidated interbedded with COAL: dark brown to black, firm and CLAYSTONE: medium grey, silty, micaceous, carbonaceous, soft, dispersive.	0.1	20-260 (Av. 120)
	930-962	- SANDSTONE: as from 920-930	0.1	80-280
,	962-985	- SANDSTONE: as above, becoming dominantly fine with increasing clay matrix, interbedded with CLAYSTONE: medium grey, silty, carbonaceous, micromicaceous.	0.1	60-280
	985-1030	- SANDSTONE: light grey, translucent, fine to coarse, often pebbly, dominantly medium, poorly to moderately sorted, subangular to subrounded, dominantly subrounded quartz, rare pyrite, rare to common multi-color lithics, rare mica, common and argillaceous matrix increasing with depth, poor visual porosity, soft, interbedded with CLAYSTONE: medium to dark grey, silty, common carbonaceous detritus, micromicaceous, soft, dispersive and minor COAL: dark brown to black, firm.	0.1	20-260 (Av. 120)
	1030-1050	- SANDSTONE: as 985-1030 becoming very fine with depth, oftern grading into argillaceous SILTSTONE interbedded with CLAYSTONE and minor COAL as above.	0.1	20-140 (Av. 60)
	1050-1060	- SANDSTONE: light to medium grey, brownish, very fine to coarse, dominantly fine, moderately sorted, subangular to subrounded. dominantly subrounded quartz, rare lithics, rare mica, rare to common carbonaceous detritus, trace to common argillaceous matrix, rare silica cement, poor porosity, soft interbedded with CLAYSTONE: medium to dark grey brownish, very silty often grading to SILTSTONE: common carbonaceous detritus, micromicaceous, soft, very dispersive.	0.1	

Interval	Description	Total Gas (units)	R.O.P. (m/hr)
1060-1080	- SILTY CLAYSTONE: interbedded with thin SANDSTONE: as 1050-1060.	0.1	5-10 (Av. 4)
1080-1100	- SANDSTONE interbedded with thin SILTY CLAYSTONE: as 1060-1080.	0.1	20-80 (Av. 40)
1100-1115	- SILTY CLAYSTONE: as 1060-1080.	0.1-0.4	5-15 (Av. 4)
1115-1120	- SANDSTONE: light grey, translucent, fine to medium dominantly fine, subangular to subrounded, dominantly subrounded quartz, common lithics, rare mica, rare pyrite, rare to common carbonaceous detritus, common argillaceous matrix, poor visual porosity, soft interbedded with CLAYSTONE: as from 1050-1060.	0.4-1.9	5
1120-1163	- CLAYSTONE: medium to dark grey, greenish silty, carbonaceous, micromicaceous becoming increasingly silty with depth grading into argillaceous SILTSTONE.	0.7-9.9	4-20 (Av. 8)
1163-1175	- SANDSTONE: translucent, greenish, very fine to medium, dominantly fine, subangular to subrounded, dominantly subrounded quartz, rare to common dark green glauconite, no apparent cement, good intergranular porosity, loose.	8.7-32.4	40-50 (Av. 45)
1175-1250	- SANDSTONE: very light grey; very fine to medium, dominantly medium; moderately sorted; subangular to subrounded, dominantly subrounded quartz; rare to common dark green glauconite; rare multi-colored lithics, no apparent matrix, good intergranular porosity; loose, interbedded with thin CLAYSTONE; medium to dark grey; silty; grading to argillaceous SILTSTONE; micromicaceous; carbonaceous; soft and dispersive.	3-26.4	8-50 (Av. 20)
1250-1265	<ul> <li>CLAYSTONE: dark grey to greenish; common to abundant glauconite nodules; common carbonaceous detritus; rare pyrite, very soft and dispersive.</li> <li>Interbedded with thin SANDSTONE; as in 1170- 1250m and minor COAL; dark brown to black; firm.</li> </ul>	1.0-2.3	2-8 (Av. 4)

Interval De	scription	Total Gas (units)	R.O.P. (m/hr)
1265-1300 -	CLAYSTONE: dark grey; silty; very glauconitic; abundant dark green, fine to medium glauconite grains decreasing with depth; common pyrite; carbonaceous; very soft; dispersive.	1.0-8.0	3-30 (Av. 17)
1300-1317.5 -	1299m Top Waarre Unit D (1275m TVD) CLAYSTONE: as for 1265-1300m interbedded with SANDSTONE; light grey to tan to brownish; fine to medium (dominantly medium); poorly to moderately sorted; subangular to subrounded (dominantly subrounded quartz); rare to common glauconite; common pyrite; weak calcareous cement; poor porosity; soft to moderately hard.	5.6-32	6-33 (Av. 10)
1317.5-1350 -	1317.5m Top Waarre Unit C (1293m TVD) SANDSTONE: light to brownish to grey; translucent, very fine to coarse (dominantly medium); poorly to moderately sorted; subangular to subrounded (dominantly subrounded quartz); trace pyrite; trace glauconite; trace lithics; weak silica cement (slightly calcareous); good inter-granular porosity; soft to moderately firm.	13.5-255	40-60 (Av. 50)
1350-1382 -	1349-5m Top Waarre Unit B (1326m TVD) CLAYSTONE: dark grey; silty; rare to common dark green glauconite; rare pyrite; soft and dispersive. Interbedded with SANDSTONE; white to light grey; very fine to coarse (dominantly fine); moderately sorted; subangular to subrounded (dominantly subrounded quartz); common to rare lithics; rare mica; moderately calcareous cement, poor visible porosity.	9.0-159	7-35 (Av. 10)
1382-1400 -	1382 Top Waarre Unit A (1356.5m TVD) SANDSTONE interbedded with thin CLAYSTONE; as for 1350-1382m.	3.2-77	30-60 (Av. 45)

Interval	De	escription	Total Gas (units)	R.O.P. (m/hr)
1400-1435	-	1400m Top Eumeralla (1376m TVD) SANDSTONE: white to light grey; very fine to medium (dominantly medium); moderately sorted; subangular to subrounded (dominantly subrounded quartz); common multi-colored lithics; common altered feldspar; common carbonaceous detritus; moderate silica cement (slightly calcareous); poor visible porosity; moderately firm. Interbedded with CLAYSTONE; light to medium grey to brownish; silty; common multi-colored lithics; micromicaceous; carbonaceous; soft and sticky.	3.2-390	5-25 (Av. 15)
1435-1460	-	CLAYSTONE: interbedded with thin SANDSTONE; as for 1400-1435m	10.5-20.0	
1460-1485	-	Interbedded SANDSTONE and thin CLAYSTONE	11.0-175	
1485-1510	-	Interbedded SANDSTONE and CLAYSTONE as for 1400-1415m.	8-34	10-45 (Av. 20)
1510-1530	-	SANDSTONE: off white to light grey greenish; very fine to medium (dominantly fine); poorly to moderately sorted; subangular to subrounded (dominantly subrounded quartz); common multicolored lithics; trace white mica and biotite; commonly altered feldspar; moderately silica cement; poor porosity; firm. Interbedded with CLAYSTONE; light grey to bluish; silty; micromicaceous; carbonaceous; rare to common lithics; soft; dispersive.	8-41	20-45 (Av. 40)
1530-1550	-	CLAYSTONE: interbedded with thin SANDSTONE; as for 1510-1530m.	6.5-46	10-20 (Av. 12)
1550-1590	-	SANDSTONE: as for 1510-1530m, interbedded with thin CLAYSTONE.	6.4-39.0	20-60 (Av. 40)
1590-1600	-	CLAYSTONE: as for 1510-1530m, interbedded with thin SANDSTONE.	4-23	5-40 (Av. 15)
1600-1615	-	SANDSTONE: as for 1510-1530m, interbedded with thin CLAYSTONE.	31	20-50 (Av. 45)
1615-1645	-	Interbedded SANDSTONE and CLAYSTONE as for 1510-1530m.	6-31.2	10-45 (Av. 20)

Interval	Description	Total Gas (units)	R.O.P. (m/hr)
1645-1650	- CLAYSTONE: as for 1510-1530m	6.0-7.0	10-12 (Av. 11)

• TOTAL DEPTH: 1650m MD Reached at 1915hrs on 24 / 2 / 1994

## APPENDIX 5

## **APPENDIX 5**

### SIDEWALL CORE DESCRIPTIONS

IONA-2

**WELL NAME:** 

IONA No. 2

**GEOLOGIST:** 

V. AKBARI

DATE:

swc	DEPTH	REC'D	LITHOLOGY (FLUORESCENCE)		GAS * (ppm)					
No.	(m)	(cm)		C ₁	C ₂	C ₃	iC ₄	nC ₄		
1	1599.0	1.5	CLAYSTONE: grey to bluish grey, micromicaceous very soft, sticky	75	3	3	1	nd		
2	1590.0	1.5	CLAYSTONE: as for SWC 1	26	2	1	nd	nd		
3	1550.5	3.0	SANDSTONE: white to light grey, bluish, very fine to medium, dominantly medium, moderately sorted, subangular to subrounded, dominantly subrounded, quartz, abundant dark coloured lithics, rare to common biotite, common altered feldspar, common silica cement, poor visual porosity, moderately firm	26	3	2	nd	nd		
4	1537.0	-	NO RECOVERY							
5	1516.5	6.5	SANDSTONE: medium to dark grey, greenish, very fine to medium, dominantly fine, moderately sorted, subangular to subrounded, dominantly subrounded quartz, common silt, common dark green lithics, rare reddish lithics, rare to common biotite, common altered feldspar, strong silica cement, poor visual porosity, firm to moderately hard	137	5	2	nd	nd		
6	1469.0	3.5	SANDSTONE: as for SWC 5	31	2	nd	nd	nd		
7	1457.5	5.0	CLAYSTONE: light to medium grey, bluish, slightly calcareous, micromicaceous, massive, soft	851	108	72	15	16		
8	1437.5	2.5	CLAYSTONE: as for SWC 7	713	95	74	10	18		

**WELL NAME:** 

IONA No. 2

**GEOLOGIST:** 

V. AKBARI

DATE:

swc	DEPTH	REC'D	LITHOLOGY (FLUORESCENCE)		GA:	S * (pp	m)	
No.	(m)	(cm)		C ₁	C ₂	C ₃	iC ₄	nC₄
9	1426.0	3.5	SANDSTONE: medium greenish-grey, very fine to coarse, dominantly medium, moderately sorted, subangular to subrounded, dominantly subrounded, quartz, common dark green and red lithics, rare muscovite and biotite, common altered feldspar, very weak calcareous cement, strong silica cement, poor visual porosity, moderately firm. Moderately bright yellow fluorescence, with a slow streaming dull yellow milky cut	2328	492	761	644	752
10	1418.0	3.5	SANDSTONE: as for SWC 9	62	17	61	69	80
11	1412.0	5.0	SILTSTONE: medium greenish-grey, common greenish lithics, rare biotite, rare red lithics, argillaceous, moderately calcareous, often grading to very fine SANDSTONE	845	77	87	60	76
12	1408.5	3.5	SANDSTONE: medium to dark grey, greenish, very fine to coarse, dominantly medium, poorly to moderately sorted, subangular to subrounded, dominantly subrounded quartz, common dark green lithics, rare biotite, rare carbonaceous detritus, moderate to strong calcareous cement, poor visual porosity, soft. Bright to moderately bright yellow cut with an instant bright milky cut	3823	1612	94	295	276
13	1402.0	2.5	CLAYSTONE: light to medium grey, bluish to grey, slightly calcareous, micromicaceous, massive, soft	134	8	12	8	14
14	1392.0	3.5	SANDSTONE: off white to light grey, translucent, fine to coarse, dominantly coarse, poorly sorted, subangular to subrounded, dominantly subrounded quartz, rare lithics, rare to common carbonaceous detritus, weak argillaceous cement, very weak calcareous matrix, good intergranular porosity, soft, friable	284	7	6	nd	nd
15	1386.0	4.5	SANDSTONE: as for SWC 14	133.5	23	5	nd	nd

**WELL NAME:** 

IONA No. 2

**GEOLOGIST:** 

V. AKBARI

DATE:

SWC	SWC DEPTH I		LITHOLOGY (FLUORESCENCE)	GAS * (ppm)						
No.	(m)	(cm)		C ₁	C ₂	C ₃	iC₄	nC₄		
16	1381.0	4.5	SANDSTONE: off white to brownish, very fine to medium, dominantly fine, moderately sorted, subangular to subrounded quartz, rare green lithics, rare mica, rare cabonaceous detritus, pyritic with small bands of micritic pyrite, common argillaceous matrix, weak calcareous cement, good visual porosity, soft. 70% banded bright to moderately bright yellow fluorescence with an instant bright to milky white cut	63	6	2	nd	nd		
17	1374.0	3.0	SANDSTONE: off white to brownish, very fine to fine, dominantly very fine, well sorted, subangular to subrounded, dominantly subrounded quartz, rare lithics, rare mica, rare pyrite, common to abundant fine carbonaceous detritus, strong silica matrix, very weak calcareous cement, poor visual porosity. Trace patchy, moderately bright medium yellow fluorescence with a slow streaming dull milky white cut	-	-	-	-	-		
18	1371.0	3.0	CLAYSTONE: dark grey to brownish, silty, micromicaceous, carbonaceous, blocky, soft	1290	98	25	17	9		
19	1362.0	2.5	SANDSTONE: off white to brownish, translucent, fine to medium, dominantly fine, well sorted, subangular to subrounded, dominantly subrounded quartz, rare lithics, abundant argillaceous matrix, very weak calcareous cement, poor visual porosity, soft. Band of 90% solid moderately bright yellow fluorescence with an instant bright, milky white cut	205	13	24	10	9		
20	1358	2.0	SANDSTONE: off white, translucent, very fine to pebbly, dominantly coarse, poorly to moderately sorted, subangular to subrounded, dominantly subrounded quartz, rare pyrite, rare to common carbonaceous detritus, weak argillaceous cement, good visual porosity, soft, friable. 100% bright, medium yellow fluorescence with an instant moderately bright milky white cut	-	-	-	-	-		
21	1353	3.0	CLAYSTONE: dark grey, greenish, carbonaceous, weakly calcareous, abundant light green to dark green glauconite, massive, soft, sticky	-	-	-	-	-		

**WELL NAME:** 

IONA No. 2

**GEOLOGIST:** 

V. AKBARI

DATE:

swc	DEPTH	REC'D	LITHOLOGY (FLUORESCENCE)	GAS * (ppm)				
No.	(m)	(cm)		C ₁	C ₂	C ₃	IC ₄	nC₄
22	1315	2.0	SILTSTONE: medium to dark grey, very argillaceous, grading to silty CLAYSTONE: rare pyrite, very carbonaceous with common to abundant carbonaceous detritus, micromicaceous, weakly calcareous, massive, soft	-	-		-	-
23	1303.5	5.0	LAYSTONE: dark grey, greenish, micromicaceous, rare lithics, common white altered dspar, very glauconitic with abundant fine to medium glauconite nodules, rare pyrite, assive, soft			-	-	-
24	1290	4.0	CLAYSTONE: as for SWC 23	_	_	-	-	-
25	1281	3.5	CLAYSTONE: medium to dark grey, micromicaceous, very glauconitic with abundant fine to medium glauconite nodules, massive, soft	-	-	-	-	-
26	1260	3.0	CLAYSTON: as for SWC 25, with more glauconite		-	-	-	-
27	1161	4.0	CLAYSTONE: medium to dark grey, micromicaceous, common carbonaceous detritus, sub-fissile, soft to moderately firm			-	-	-
28	1129	4.0	SILTSTONE: dark grey to brownish, argillaceous, weakly to moderately calcareous, carbonaceous, micromicaceous, massive, soft	-	-	-	-	-
29	1090.5	4.0	<b>SANDSTONE:</b> off white to very light brown, very fine to fine, dominantly fine, well sorted, subangular to subrounded, dominantly subrounded quartz, rare to common pyritic cement, rare lithics, rare carbonaceous detritus, strong argillaceous matrix, no visual porosity, soft	-	-	-	-	-
30	1034.5	5.0	SANDSTONE: as for SWC 29, with very thin bands of carbonaceous material	_	-	-	-	-

## APPENDIX 6

## **APPENDIX 6**

### PALYNOLOGY REPORT

IONA-2

# Palynological Analysis of Iona-2 in Port Campbell Embayment Otway Basin

by

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A.C.N. 053 800 945

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### INTERPRETATIVE DATA

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### Introduction

Eighteen sidewall cores samples and four cutting samples between 1034.5-1599m were analysed in Iona-2. The selected sidewall cores where forwarded for processing to Laola Pty Ltd in Perth in early March and an initial version of this report was submitted on 14 April. It was then decided to analyse four cuttings samples between 1292.5-1350m to improve the dating on the Waarre Formation and at the same time additional palynological slides were prepared and examined from remaining palynological residues from sidewall cores in this interval. These new preparations provided new information necessitating revision of the original report. The changes were needed once it was realised SWC-22 at 1325m was significantly contaminated, due either to drilling mud which could not be cleaned from the sample or cross-contamination during laboratory preparation. The contamination from higher in the section resulted in assignment of an erroneous younger age to this sample in the original report.

Between 6.5 to 15.8 grams (average 11.2 g) of the sidewall cores, and 10 to 24 grams (average 16.9 g) of the cuttings, were processed for palynological analysis. Residue yields vary from very low to very high while the palynomorphs are mostly present in low to moderate concentrations on the slides. Preservation of palynomorphs varies from poor to good but overall is fair. A problem with the preservation is that many of the dinoflagellates are broken which means that some species may only be represented by fragments rather than complete specimens. Spore-pollen diversity is consistently high through the Sherbrook Group averaging 33+ species per sample, but rather bimodal in the Eumeralla Formation where it is either very low (1-3 species) or moderate to high (17-38 species). Average spore-pollen diversity through the Eumeralla Formation was 19+ species per sample. Microplankton diversity is low to moderate (9-18 species) in the Sherbrook Group with an average of 12+ species, and very low in the Eumeralla Formation with and average of 2+ species per sample.

Geological ages, formations and palynological zones for the interval sampled in Iona-2 are given in Table-1. Additional interpretative data with zone identification and Confidence Ratings are recorded in Table-4, whilst basic data on residue yields, preservation and diversity are recorded on Tables-5 and 6. For the sidewall cores all species which have been identified with binomial names are tabulated on the palynomorph range charts which present the recorded assemblages on separate charts in order of highest and lowest appearances. The assemblages recorded from the cuttings samples are recorded in Appendix-1.

### **Geological Comments**

- 1. The sequence sampled in Iona-2, with only minor modifications, can be readily assigned to the Mesozoic spore-pollen and microplankton zones defined by Helby, Morgan & Partridge (1987). The time interval sampled is from the Late Albian to basal Campanian.
- 2. The spore-pollen zone nomenclature of Helby *et al.* (1987) used in this report is a modification of an earlier zonation scheme proposed by Dettmann & Playford (1969). This earlier scheme over the interval analysed here was originally erected upon wells in the Port Campbell Embayment and is still widely used in the Otway Basin. The equivalence between the two zonation schemes, for those zones applicable to Iona-2 is as follows:

Dettmann & Playford (1969)	Helby et al. (1987)			
Nothofagidites Microflora	N. senectus Zone			
(in part only)				
T. pachyexinus Zone	T. apoxyexinus Zone			
C. triplex Zone	P. mawsonii Zone			
A. distocarinatus Zone	A. distocarinatus Zone			
P. pannosus Zone	P. pannosus Zone			

Explanations of the reasons for the zone name changes can be found in Helby et al. (1987).

- 3. Of the microplankton or dinoflagellate zones identified in Iona-2 the Nelsoniella aceras and Isabelidinium (al. Deflandrea) cretaceum Zones were originally established in the Otway Basin by Evans (1966), while the older Odontochitina porifera Zone is an Australia-wide zone defined in Helby et al. (1987). At the base of the marine sequence the new local Cribroperidinium edwardsii Acme Zone is recognised. The current preferred correlation of this zone is with all or part of the Turonian Palaeohystrichophora infusorioides Zone of Helby et al. (1987). However, as exact equivalence cannot yet be convincingly demonstrated, new terminology is preferred to avoid possible ambiguity.
- 4. The spore-pollen succession in Iona-2 lacks clear evidence for the presence of the *A. distocarinatus* Zone. This is supported by the ages derived from the microplankton assemblages, and is identical to the results reported by Morgan (1988) from the adjacent Iona-1.

Table-1: Palynological Summary Iona-2

AGE	UNIT	SPORE-POLLEN ZONES	MICROPLANKTON ZONES	
CAMPANIAN		N. senectus 1034.5m	N. aceras	
	SKULL CREEK MUDSTONE		1034.5-1129m	
SANTONIAN	NULLAWAARE GREENSAND	T. apoxyexinus 1090-1295m	I. cretaceum 1161-1281m	
	BELFAST MUDSTONE		O. porifera 1290-1295m	
TURONIAN	WAARRE FORMATION	P. mawsonii 1303.5-1371m	C. edwardsii 1303.5-1371m	
LATE ALBIAN	EUMERALLA FORMATION	<i>P. pannosus</i> 1402-1590m		

- 5. The dinoflagellates succession in the sidewall cores is incomplete because the *Conosphaeridium striatoconus* dinoflagellate Zone was not recognised in Iona-2 although present in Iona-1 (Table-2). The possibility that the zone might be present was subsequently tested by analysis of four cuttings samples below the base of the *O. porifera* Zone. Unfortunately neither *Conosphaeridium striatoconus* nor any other index species for the zone were recorded and it is therefore concluded this zone is not present in Iona-2.
- 6. Between 1290m and the shallowest sample at 1034.5m the microplankton succession displays a normal sequence for the Senonian consisting of in ascending order the *O. porifera*, *I. cretaceum* and *N. aceras* Zones.
- 7. Table-2 provides a correlation of sidewall core samples between Iona-1 and Iona-2 with comments on the key species events used for the correlations. The striking feature is that while the *C. striatoconus* Zone is missing or not sampled in Iona-2 the overlying *O. porifera* Zone is missing or not sampled in Iona-1. The proposed correlations are based solely on the palynological data and have not been verified by electric log correlation. They do however suggest that further resolution is still possible in both wells using palynology.

Table-2: Co	orrelation	of	samples	between	Iona-1	and	Iona-2.
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Spore-Pollen and Iona-1 (Microplankton) Zones		Iona-2 (Depths m)	Key species datums				
N. senectus (N. aceras)			FAD for <i>N. senectus</i> and <i>F. sabulosus</i> with dinoflagellates <i>N. aceras</i> and/or <i>N. tuberculatus</i> together with questionable <i>X. australis</i> .				
T. apoxyexinus (N. aceras) 1075.5 1090-1129		1090-1129	FAD of <i>N. aceras</i> without presence of <i>N. senectus</i> .				
T. apoxyexinus (I. cretaceum)			FAD of <i>I. cretaceum</i> associated with increased dominance of <i>Proteacidites</i> spp.				
T. apoxyexinus NOT 1290 (O. porifera) SAMPLED		1290	FAD of <i>O. porifera</i> and FAD of <i>P. gillii</i> .				
(C. striatoconus)	1276.5	NOT SAMPLED	FAD & LAD of C. striatoconus with consistent P. mawsonii and C. triplex.				
P. mawsonii 1287-1347.5 1303.5-1371 (C. edwardsii)		1303.5-1371	Total local range of <i>C. edwardsii</i> with rare but consistent <i>P. mawsonii</i> and <i>C. triplex</i> .				
P. pannosus 1383-1481 1402-1590		1402-1590	Assemblage containing non-marine algae with FAD for <i>P. pannosus</i> .				

LAD = Last Appearance Datum. FAD = First Appearance Datum.

8. All samples analysed from the Sherbrook Group are considered to be marine based on the abundance and diversity of their contained microplankton. Abundance of microplankton expressed as a percentage varies from 6% to 32% (Table-3). The palynomorphs in the count include spores, pollen and microplankton, but exclude fungal spores and hyphae and any palynomorphs that are obviously reworked or contaminants.

Microplankton species diversity is low to moderate with between 9-18 species recorded from individual samples. As the total diversity recorded for the interval is 50+ species it is suspected the true diversity of the samples is higher than recorded being limited by low recoveries and only moderate palynomorph concentrations in individual samples. Even though the microplankton abundances of three of the four samples from Units B and D of the Waarre Formation are lower than the other samples the species diversity is consistent (Table-6). Overall, whilst the species diversity is consistently less than the diversity found in equivalent age marine rocks on the western margin of Australia, as for example recorded by Marshall (1984), it is nevertheless consistent with the style of most other marine microplankton assemblages found in the Late Cretaceous basins along the southern margin of Australia.

Table-3: Microplankton Abundance for Selected Samples.

Sample Type	Depth (m)	Microplankton Zone	Microplankton Abundance as % Relative to total Spore-pollen	Most abundant microplankton species as % of total microplankton
SWC-30	1034.5	N. aceras	12%	Heterosphaeridium spp. >40%.
SWC-29	1090	N. aceras	19%	Heterosphaeridium spp. >45%.
SWC-28	1129	N. aceras	25%	Heterosphaeridium spp. >60% Nelsoniella aceras 16%
SWC-26	1260	I. cretaceum	26%	Heterosphaeridium spp. >42% . Hexagonifera spp. 25%.
SWC-25	1281	I. cretaceum	21%	Heterosphaeridium spp. >50%.
SWC-24	1290	O. porifera	21%	Heterosphaeridium spp. >52% Odontochitina spp. 6%.
SWC-23	1303.5	C. edwardsii	11%	Spiniferites spp. 30% Heterosphaeridium spp. >15%.
SWC-22	1315	C. edwardsii	32%	Heterosphaeridium spp. >35% Odontochitina spp. 13%
SWC-21	1353	C. edwardsii	11%	Cribroperidinium edwardsii 24%.
SWC-18	1371	C. edwardsii	6%	Amosopollis cruciformis 14%.
SWC-13	1402		5%	Sigmopollis carbonis 50%.
SWC-11	1412		2%	Sigmopollis carbonis 33%.
SWC-8	1437.5		5%	Sigmopollis carbonis 70%.
SWC-7	1457.5		4%	Sigmopollis spp. 90%.
SWC- 2	1590		0.5%	Sigmopollis carbonis 100%.

9. Buffin (1989) has proposed a depositional model for units identified in the Waarre Formation in which significant restricted marine units including back-water lagoons, swamps, tidal channels and tidal deltas are deposited behind or associated with a beach-barrier. None of the four assemblages recorded from the Waarre Formation in Iona-2 could be considered typical of these environments, which would be expected to have microplankton "blooms" consisting of the very abundant occurrence (microplankton typically >75% of total count) of one or just a few species. Instead the samples contain moderate diversity assemblages without any particular species being dominant.

- 10. The organic microplankton recorded from the Eumeralla Formation would generally be classed as acritarchs and are here all considered to be derived from non-marine lacustrine environments. The deposition of the Otway Group at high latitudes in the Early Cretaceous can be compared to modern deposition environments above the Arctic Circle where there are typically thousands of lakes of all sizes in the modern depositional basins as a consequence of low temperatures and low evaporation. It is easy to envisage algal cysts deposited in such lakes being reworked by fluvial processes throughout the depositional basin. These microplankton in the Otway Group have been recorded and discussed by other palynologists dating back to Evans (1966, p.31).
- 11. Nearly all of the samples analysed contained reworked palynomorphs. The commonest or most distinctive reworked spore-pollen are from the Permian with a minor component of distinctive Triassic spores and pollen. The Sherbrook Group contains obvious reworked Early Cretaceous spores the most distinctive of which are *Cyclosporites hughesii* and *Pilosisporites notensis*. The counts suggest the assemblages contain between 1% to 5% reworked palynomorphs. This is likely to be a conservative estimate because of the difficulty with long ranging species, which dominate all assemblages, of deciding which specimens are reworked and which insitu. Making such a distinction is only possible where there are clear differences in the maturation colour of the reworked palynomorphs.

### Biostratigraphy

Zone and age determinations are based on the Australia wide spore-pollen and microplankton zonation schemes described by Helby, Morgan & Partridge (1987). As applied to the Otway Basin these schemes modified and improved on the spore-pollen zonation scheme of Dettmann & Playford (1969) and the microplankton zonation scheme of Evans (1966). An additional local microplankton association called the *Cribroperidinium edwardsii* Acme Zone is recognised in this report to better express local correlations.

Author citations for most spore-pollen species can be sourced from Helby, Morgan & Partridge (1987), Dettmann (1963) or other references cited herein. Author citations for dinoflagellates can be found in the indexes of Lentin & Williams (1985, 1989) or other references cited herein. Species names followed by "ms" are unpublished manuscript names.

### Spore-Pollen Zones

Nothofagidites senectus Zone.

Interval: 1034.5 metres Age: Basal Campanian

The shallowest sample analysed is assigned to this zone on the occurrence of a single specimen of the eponymous species *N. senectus*. A position low in the zone is suggested by presence of *Forcipites* (al. *Tricolpites*) sabulosus with *Tricolporites* apoxyexinus but without the presence of *Gambierina rudata* (see range chart in Helby *et al.* 1987, fig. 33). Other noteworthy species are *Tricolpites waipawaensis* and *Forcipites stipulatus*. The commonest elements in the assemblage are *Proteacidites* spp. (17%) and *Podocarpidites* spp. (13%).

**Tricolporites apoxyexinus Zone** (formerly the *Tricolpites pachyexinus Zone*).

Interval: 1090.0-1295.0 metres (200+ metres).

Age: Santonian

Of the six sidewall core samples assigned to this zone the eponymous species *T. apoxyexinus* is recorded from only three, and then usually only as a single specimen. A variety of accessory species indicative of the zone are more common. These include the first appearance datums (FADs) in this well for *Peninsulapollis gillii* (at 1290m), *Forcipites stipulatus* (1281m), *Lygistepollenites balmei* (1161m), *Camarozonosporites bullatus* (1161m, with a questionable specimen at 1303.5m), *Latrobosporites ohaiensis* (1161m) and *L. amplus* (1260m).

The species Australopollis obscurus, Clavifera triplex and Phyllocladidites mawsonii although known to range into older zones are consistently recorded in most samples in this zone.

On overall composition this zone can be characterised as the level in the Late Cretaceous when angiosperm pollen first became common in the assemblage counts. They range in abundance from 11% to 28% with an average of 18%. *Proteacidites* spp. and other triporate pollen are also conspicuous ranging from 4% to 16%. Thus, these assemblages readily conform to characteristic of *Proteacidites* Superzone of Helby *et al.* (1987).

The cuttings samples suggests the zone extends at least as deep as 1295m.

Phyllocladidites mawsonii Zone (formerly the Clavifera triplex Zone).

Interval: 1303.5-1371.0 metres (68+ metres).

Age: Turonian (Coniacian absent or not sampled).

The eponymous species *P. mawsonii*, whose FAD defines the base of this zone was recorded in three of the four sidewall cores and all of the cuttings within this interval. The formerly used zone species *Clavifera triplex* was also consistently recorded in most of the samples.

Important accessory species are rare but include *Cyatheacidites tectifera* at 1353m and 1371m. This species is considered to range no older than this zone on the southern margin (Helby *et al.* 1987, fig.33). Other species are *Cicatricosisporites cuneiformis* and *C. pseudotripartitus* which are considered to range no younger than this zone by Dettmann & Playford (1969, table 9.4). *Appendicisporites distocarinatus* was also recorded from most samples and its occurrence is consistent with its range given by Helby *et al.* (1987, fig.33), but is a younger extension of the original range given by Dettmann & Playford (1969).

There are also several new species or variety previously recorded from the *P. mawsonii* Zone in the Gippsland and Bass Basins but hitherto not recorded from the Otway Basin. These include *Densoisporites muratus* ms, *Rugulatisporites admirabilis* ms, *Hoegisporis trinalis* ms, *Laevigatosporites musa* ms, *Cupressacites* sp. and *Dilwynites granulatus* (small variety).

Counts of the two assemblages show they can be characterised by frequent to abundant *Dilwynites granulatus* (3%-39%; average 21%) with frequent to common *Cupressacites* sp. (3%-10%) and *Glecheniidites/Clavifera* spp. (6%-9%). The abundance of these three species groups clearly distinguish these samples from those assigned to the underlying *P. pannosus* Zone.

The absence of the *C. striatoconus* dinoflagellate Zone in Iona-2 suggests the upper part of the *P. mawsonii* Zone of Coniacian age may not to be present in Iona-2.

Upon initial examination the sample at 1315m was assigned to the overlying *T. apoxyexinus* Zone on the presence of the eponymous species and *Forcipites* sp. and the supporting evidence of the associated dinoflagellates. Examination of additional slides showed that these younger index species were extremely rare and the bulk of the assemblage was more similar to the other *P. mawsonii* Zone samples. It is concluded therefore that this sample has been contaminated.

### Appendicisporites distocarinatus Zone.

Interval: Not recorded in Iona-2.

Age: Cenomanian.

Assemblages characteristic of this zone were not recorded in Iona-2 but may be present in the 31 metre unsampled interval between 1371-1402m. The zone was also lacking in Iona-1 where there is a similar unsampled interval of 35 metres lying between 1347.5m-1383m (Morgan 1988).

#### Phimopollenites pannosus Zone.

Interval: 1402.0-1599.0 metres (197+ metres).

Age: Late Albian.

Six of the seven samples from the Eumeralla Formation could be assigned to the *P. pannosus* Zone. The seventh and deepest sample in the well was virtually barren and could not be assigned to any age.

Phimopollenites pannosus was only recorded from the samples at 1457.5m and 1516.5m, while *Perotrilites jubatus* which Dettmann & Playford (1969) considers as also having its FAD within this zone was recorded in the four samples at 1412m, 1437.5m, 1457.5m and 1590m.

Other significant species recorded include *Tricolpites cooksoniae* at 1437.5m and 1457.5m, a poorly preserved specimen of *Trilobosporites purverulentus* at 1412m and a interpreted reworked specimen of *Pilosisporites notensis* at 1402m.

Overall the species diversity recorded is not high for the zone and certain species which would have been expected were either absent or very rare. These include Coptospora paradoxa and Trilobosporites trioreticulosus which were not recorded and Crybelosporites striatus which was only seen at 1437.5m.

Confidence in assigning all the samples to the zone is based mainly on the assemblage count. These clearly differ from the overlying *P. mawsonii* and younger Zones by the increased abundance of *Corollina* spp., *Retitriletes* spp. and spores of the *Baculatisporites/Osmundacidites* complex, and lack of any significant abundances of *Gleicheniidites* spp., *Dilwynites* spp. and *Cupressacites* sp.

The sample at 1590m was considered to be a particularly favourable lithology and duly gave a good yield. Unfortunately the spore-pollen assemblage was overwhelmingly dominated by *Baculatisporites-Osmundacidites* style spores which

comprise 85% of the count, amongst which index species were very difficult to find.

A single specimen of *Amosopollis cruciformis* was recorded at 1457.5m which is flagged as a possible new downward extension of its range or alternatively evidence of downhole contamination which is indicated as possible problem with this sample (Table-5). Significant contamination was interpreted as present in the shallowest sample at 1402m which could only be assigned to this zone after counting the limited residue recovered.

### **Microplankton Zones**

Nelsoniella aceras Zone.

Interval: 1034.5-1129.0 metres (95+ metres).

Age: Late Santonian - Early Campanian.

The three samples conform to this zone by containing either *Nelsoniella aceras* or *N. tuberculata* and lacking *Xenikoon australis*. A possible specimen of the latter species was recorded in the shallowest sample but additional searching did not reveal further specimens. It is noted that Morgan (1988) also records a questionable specimen of *X. australis* at 1018m in Iona-1 but still assigns the sample to the *N. aceras* Zone.

The associated dinoflagellates disappointingly only displayed a low diversity. Of potential local correlative value is consistent present of *Heterosphaeridium* evansii ms Marshall 1984 (= *H. laterobrachius* as recorded by Morgan 1988). The LAD of *Odontochitina porifera* was also recorded for the well at 1129m.

All three assemblages are dominated by *Heterosphaeridium* spp. (Table-3).

Isabelidinium cretaceum Zone.

Interval: 1161.0-1281.0 metres (120+ metres).

Age: Santonian.

Three samples with low to moderate diversity microplankton assemblages are assigned to the *I. cretaceum* Zone on the presence of the eponymous species and lack of the succeeding zone indicator. The shallowest sample is the most problematical assignment as the specimens of *I. cretaceum* recorded are like the variety illustrated by Cookson & Eisenack (1961, p.11, figs 1,2) from the Belfast No. 4 bore. This variety is larger and characteristically circumcavate rather than simply cavate at the apices like the holotype and most of the paratypes of

*I. cretaceum.* This sample also contains a folded specimen which could be *N. aceras*.

The assemblages are dominated by *Heterosphaeridium* spp. One significant occurrence is the first record for the Otway Basin of *Odontochitina indigena* described from the Santonian in the Gippsland Basin by Marshall (1988).

Odontochitina porifera Zone.

Interval: 1290.5-1295.0 metres (25+ metres).

Age: Santonian.

The sidewall core assemblage can be characterised by abundant Heterosphaeridium heteracanthum with common Odontochitina porifera and the cuttings sample is very similar. Most specimens of Odontochitina porifera found in this zone and in younger samples in Iona-2 can be characterised by a constricted and non-perforate ring at the bases to both the apical and antapical horns. In this the specimens are closer to the holotype of O. porifera illustrated by Cookson (1956, pl.1, fig.17) rather than the specimen illustrated by Helby et al. (1987, fig.41C) which lack this non-perforate ring. Some specimens where the non-perforate parts of the horns become broader have been compared to O. cribropoda Deflandre & Cookson 1955 but no specimens were recorded which could be considered conspecific with this latter species, as originally erroneously suggested in the provisional reports.

Although both the sidewall core and cuttings contain moderate diversity assemblages none of the other recorded species can be considered age diagnostic for this zone.

Conosphaeridium striatoconus Zone.

Interval: Not recorded in Iona-2.

Age: Coniacian.

Assemblages assignable to the *C. striatoconus* Zone were not found in Iona-2, but one was recorded from a single sample at 1276.5m in Iona-1 (Morgan, 1988). Although it was suggested after the initial examination of the sidewall cores that the zone may be present in the unsampled gap between samples the subsequent analysis of cuttings found no insitu or caved specimens of the eponymous species, or any other diagnostic species, suggesting strongly that the zone is not present in Iona-2.

Cribroperidinium edwardsii Acme Zone.

Interval: 1303.5-1371.0 metres (68+ metres).

Age: Turonian.

The four sidewall core samples from the Waarre Formation are assigned to a new local acme zone which is characterised by the rare to common occurrence of the dinoflagellate *Cribroperidinium edwardsii*. Microplankton are considered to be present in the samples in low abundance (6% to 11%). The higher abundance at 1315m of 32% is considered to reflect the contamination of that sample with microplankton from higher in the well. Although samples are of moderate diversity, all species are either long ranging forms or species whose ranges are imprecisely known. In particular the diagnostic zone species of the standard zonation of Helby *et al.* (1987) are absent. As well as *C. edwardsii* the main elements in the assemblages comprise species of *Cyclonephelium* spp., *Odontochitina costatae* and *O. operculata*, and *Oligosphaeridium pulcherrimum* and *O. complex. Heterosphaeridium* spp. although present is noticeably less common than recorded from younger zones in Iona-2. Although *Palaeohystrichophora infusorioides* is recorded in three of the four samples it is certainly not prominent.

Cribroperidinium edwardsii was considered by Helby et al. (1987, fig.37) to have a prominent occurrence in the upper part of the D. multispinum Zone and through most of the P. infusorioides Zone and to be inconsistent above this last zone. This is currently the strongest evidence for an assignment no younger than the P. infusorioides Zone and hence a Turonian age. An age no older than the P. infusorioides Zone is based on the absence of species that become extinct in the underlying D. multispinum Zone yet have been recorded in basins along the southern margin rift. The most significant of these are Pseudoceratium ludbrookiae, Litosphaeridium siphoniphorum and Canninginopsis denticulata. Direct assignment of the samples to the P. infusorioides Zone cannot be confidently made in the absence of any prominent occurrence of the eponymous species as well as absence of other index species. The assignment of the samples to the P. mawsonii spore-pollen Zone also supports the Turonian age.

The sample at 1315m is considered to be contaminated with material from the *O. porifera* Zone because of the presence of the eponymous species and the related morphotype *Odontochitina* sp. cf. *O. cribropoda* and lack of younger zone indicators. Because the samples at 1290m and 1315m were both in the initial batch of four samples processed it is speculated that the sample at 1315m was cross contaminated with the shallower sample at 1290m during laboratory preparation.

### Non-marine microplankton in Eumeralla Formation.

Interval: 1402.0-1599.0 metres (197+ metres).

Age: Late Albian.

Samples from the Eumeralla Formation are characterised by a limited suite of microplankton comprising *Sigmopollis carbonis*, *S. hispidus*, *Micrhystridium* sp. A of Marshall (1989) and *Veryhachium reductum*. Most of the other forms recorded over this interval can be dismissed as caved.

The most abundant cyst is *S. carbonis* which occurs in all but the barren sample at 1590m and the very low yielding sample at 1516.5m. This form has been compared to Holocene microfossil algae occurring in eutrophic and mesotrophic freshwater environments by Pals *et al.* (1980, p.407) and Srivastava (1984, p.528).

Notwithstanding that all of the above species are also recorded in overlying marine section in Iona-2 their association in the Eumeralla Formation is interpreted to indicate deposition in freshwater, most likely lacustrine environments. Abundant shallow and ephemeral lakes are to be expected in the high latitude setting suggested for deposition of the Otway Group. These types of deposits would be readily reworked by fluviatile processes to subsequently distribute the algal microfossils throughout the sedimentary section.

### References

- BUFFIN, A.J., 1989. Waarre Sandstone development within the Port Campbell Embayment. *APEA J.* 29 (1), 299-311.
- BURGER, D., 1980. Palynology of the Lower Cretaceous in the Surat Basin. Bull. Bur. Miner. Resour. Geol. Geophys. Aust. 189, 1-106.
- COOKSON, I.C. & EISENACK, A., 1961. Upper Cretaceous microplankton from the Belfast No. 4 bore, south-western Victoria. *Proc. Roy. Soc. Vict.* 74 (1), 69-76, pls 11-12.
- COOKSON, I.C., 1956. Additional microplankton from Australian Late Mesozoic and Tertiary sediments. *Aust. J. Mar. Freshwater Res.* 7 (10), 183-191.
- DEFLANDRE, G. & COOKSON, I.C., 1955. Fossil microplankton from Australian Late Mesozoic and Tertiary sediments. *Aust. J. Mar. Freshwater Res.* 6, 242-313.
- DETTMANN, M.E., 1963. Upper Mesozoic microfloras from southeastern Australia. *Proc. R. Soc. Vict.* 77, 1-148.
- DETTMANN, M.E. & PLAYFORD, G., 1969. Palynology of the Australian Cretaceous: a review. In stratigraphy and palaeontology. *Essays in honour of Dorothy Hill*, K.S.W. Campbell, ed., A.N.U. Press Canberra, 174-210.
- EVANS, P.R., 1966. Mesozoic stratigraphic palynology of the Otway Basin. *Rec. Bur. Miner. Resour.* Geol. Geophys. Aust. 1966/69, 1-45, pls 1-4 (unpubl.).
- HELBY, R., MORGAN, R. & PARTRIDGE, A.D., 1987. A palynological zonation of the Australian Mesozoic. *Mem. Ass. Australas. Palaeontols* 4, 1-94.
- LENTIN, J.K. & WILLIAMS, G.L., 1985. Fossil Dinoflagellates: Index to genera and species, 1985 Edition. *Canadian Tech. Rep. Hydrog. Ocean Sci. 60*, 1-451.
- LENTIN, J.K. & WILLIAMS, G.L., 1989. Fossil Dinoflagellates: Index to genera and species, 1989 Edition. *AASP Contribution Series No. 20*, 1-473.
- MARSHALL, N.G., 1984. Late Cretaceous dinoflagellates from the Perth Basin, Western Australia. PhD thesis, University of Western Australia (unpubl.).
- MARSHALL, N.G., 1988. A Santonian dinoflagellate assemblage from the Gippsland Basin, southeastern Australia. *Mem. Ass. Australas. Palaeontols* 5, 195-215.

- MARSHALL, N.G., 1989. An unusual assemblage of algal cysts from the Late Cretaceous of the Gippsland Basin, southeastern Australia. *Palynology 13*, 21-56.
- MARSHALL, N.G., 1990. Campanian dinoflagellates from southeastern Australia. *Alcheringa* 14, 1-38.
- MORGAN, R., 1988. Palynology of Beach Iona-1, Otway Basin, Victoria. *Report for Beach Petroleum*, 19p., range chart (May).
- PALS, J.P., Van GEEL, B. & DELFOS, A., 1980. Palaeoecological studies in the Klokkeweel bog Hoogkarspel (Prov. of Noord-Holland). *Rev. Palaeobot. Palynol.* 30, 371-418.
- SRIVASTAVA, S.K., 1984. Genus Sigmopollis from the Maastrichtian Scollard Formation, Alberta (Canada), and its algal affinity. *Pollen et Spores 26*, 519-530.

Table-4: Interpretative Palynological Data for Iona-2, Otway Basin.

Sample Type	Depth (m)	Spore-Pollen Zone	CR	Microplankton Zone	CR	Comments or Key Species
SWC-30	1034.5	N. senectus	B1	N. aceras	В3	Only single specimens of Nothofagidites senectus, and Nelsoniella tuberculata.
SWC-29	1090	T. apoxyexinus	B1	N. aceras	B2	FAD Lygistepollenites florinii
SWC-28	1129	T. apoxyexinus	B4	N. aceras	B3	FAD Nelsoniella aceras.
SWC-27	1161	T. apoxyexinus	B1	I. cretaceum	B2	Isabelidinium thomasii. FAD Lygistepollenites balmei.
SWC-26	1260	T. apoxyexinus	B1	I. cretaceum	B2	Canningia rotundata.
SWC-25	1281	T. apoxyexinus	B2	I. cretaceum	B2	FAD Isabelidinium cretaceum.
SWC-24	1290	T. apoxyexinus	B1	O. porifera	В3	Abundant Cupressacites sp.
Cuttings	1292.5 -1295	T. apoxyexinus	D3	O. porifera	D3	T. apoxyexinus and F. stipulatus present.
SWC-23	1303.5	P. mawsonii	B1	C. edwardsii	B2	Abundant <i>Dilwynites granulatus</i> (small variety).
Cuttings	1312.5 -1315	P. mawsonii	D1	C. edwardsii		LAD Laevigatosporites musa.
SWC-22	1315	P. mawsonii	B2	C. edwardsü	B3	Sample contaminated with assemblage from SWC-24 at 1290m.
Cuttings	1332.5 -1335	P. mawsonii	D2			Frequent P. mawsonii.
Cuttings	1347.5 -1350	P. mawsonii	D2	C. edwardsii	D3	Densoisporites muratus ms present.
SWC-21	1353	P. mawsonii	B4	C. edwardsii	B2	LAD Hoegisporis trinalis.
SWC-18	1371	P. mawsonii	B1	C. edwardsii	B2	FAD Phyllocladidites mawsonii, Clavifera triplex and Cribroperidinium edwardsii.
SWC-13	1402	P. pannosus	B5			Low yielding contaminated sample assigned to zone on basis of assemblage count.
SWC-11	1412	P. pannosus	B5			Reworking conspicuous.
SWC-8	1437.5	P. pannosus	B2			Perotrilites jubatus.
SWC- 7		P. pannosus	В1			Amosopollis cruciformis with P. pannosus.
swc-5	1516.5	P. pannosus	B3			FAD Phimopollenites pannosus.
SWC- 2	1590	P. pannosus	B2			Dominated by <i>Baculatisporites</i> spp with <i>P. jubatus</i> .
SWC- 1	1599	Indeterminate				Virtually barren.

Abbreviations:

CR = Confidence Ratings LAD = Last Appearance Datum FAD = First Appearance Datum

#### **Confidence Ratings**

The Confidence Ratings assigned to the zone identifications on Table-4 are quality codes used in the STRATDAT relational database being developed by the Australian Geological Survey Organisation (AGSO) as a National Database for interpretive biostratigraphic data. Their purpose is to provide a simple relative comparison of the quality of the zone assignments. The alpha and numeric components of the codes have been assigned the following meanings:

Alpha codes: Linked to sample type

- A Core
- B Sidewall core
- C Coal cuttings
- **D** Ditch cuttings
- E Junk basket
- F Miscellaneous/unknown
- **G** Outcrop

Numeric codes: Linked to fossil assemblage

1 Excellent confidence: High diversity assemblage recorded with

key zone species.

2 Good confidence: Moderately diverse assemblage recorded

with key zone species.

3 Fair confidence: Low diversity assemblage recorded with

key zone species.

4 Poor confidence: Moderate to high diversity assemblage

recorded without key zone species.

5 Very low confidence: Low diversity assemblage recorded

without key zone species.

#### **BASIC DATA**

Table 5: Basic Sample Data - Iona-2, Otway Basin

Table-6: Basic Palynomorph Data for Iona-2, Otway Basin

Appendix 1: Species Lists for Cuttings Samples.

Palynomorph Range Charts for Iona-2, Otway Basin

Chart 1: Relative Abundance by Lowest Appearance

Chart 2: Relative Abundance by Highest Appearance

Table 5: Basic Sample Data - Iona-2, Otway Basin.

SAMPLE TYPE	DEPTH (metres)	LITHOLOGY	SAMPLE WT (g)	RESIDUE YIELD
SWC 30	1034.5	Med. gry, f. gn. sandstone with laminae ~1mm, some with carbonaceous flecks <1mm.	12.1	Moderate
SWC 29	1090	Med. gry, f. gn. sandstone with laminae <1mm with 4mm layer of chocolate coloured claystone on one edge.	15.4	High
SWC 28	1129	Carbonaceous dk gry claystone with med. gry mottled sandstone.	10.6	High
SWC 27	1161	Dk gry-blk claystone with faint mottling of sandy claystone.	12.0	Very High
SWC 26	1260	Dk grn-blk glauconite (<25%) claystone.	12.9	Moderate
SWC 25	1281	Meddk grn-gry glauconite (<30%) claystone.	13.2	Moderate
SWC 24	1290	Med. dk gry mottled, glauc. (<20%) claystone.	7.8	High
Cuttings	1292.5- 1295	Medium gry shale, very fine grained with >50% less than 1mm.	10.2	High
SWC 23	1303.5	Mottled med. gry claystone with lt. gry sandstone. Accessory mica (<2mm) and white clay or feldspar flecks.	15.8	Low
Cuttings	1312.5- 1315	Claggy dk gry claystone, very f.grn. with >70% less than 1mm.	18.8	High
SWC 22	1315	Dk gry-blk homogeneous soft claystone which is contaminated by drilling mud.	8.3	High
Cuttings	1332.5- 1335	Coarse grn. quartz sandstone with <5% shale fragments.	23.8	Low
Cuttings	1347.5- 1350	Lt-med. gry shale & siltstone mixed with crs qtz sand (50%).	14.6	Low
SWC 21	1353	Mottled gry claystone with f. gn. micaceous sandstone. Possible glauconite, some drilling mud contamination.	11.2	High
SWC 18	1371	Faintly laminated dk gry claystone and mottled med. gry carbonaceous/micaceous sandstone. Laminae up to 11mm.	10.2	High
SWC 13	1402	Soft Ltmed. gry mottled claystone.	9.6	Low
SWC 11	1412	Med. gry, med. grained homogeneous sandstone with white clay flecks.	12.0	Very Low
SWC 8	1437.5	Med. gry claystone with occasional laminae.	10.0	Moderate
SWC 7	1457.5	Med. gry homogeneous claystone with subconcoidal fractures. Some drilling mud contamination.	11.0	Moderate
SWC 5	1516.5	Dk gry med. gn homogeneous sandstone. Drilling mud could not be cleaned off sample.	15.2	Very Low
SWC 2	1590	Med. gry claystone with drilling mud contamination.	7.0	Moderate
SWC 1	1599	Med. grn-gry homogeneous claystone.	6.5	Very Low

Table-6: Basic Palynomorph Data for Iona-2, Otway Basin

Sample Type	Depth (m)	Palynomorph Concentration		Number S-P Species*	Microplankton Abundance	Number MP Species*
SWC-30	1034.5	Moderate	Good	43+	Common	9+
SWC-29	1090	Moderate	Fair-good	37+	Common	14+
SWC-28	1129	Low	Fair-good	28+	Very Common	9+
SWC-27	1161	Moderate	Fair-good	32+	Common	9+
SWC-26	1260	Moderate	Fair-good	31+	Abundant	18+
SWC-25	1281	Moderate	Poor-good	26+	Common	14+
SWC-24	1290	Moderate	Fair	32+	Common	12+
Cuttings	1292.5- 1295	Moderate	Fair-good	19+	Frequent	12+
SWC-23	1303.5	Moderate	Poor-fair	34+	Frequent	15+
Cuttings	1312.5- 1315	Moderate	Fair	27+	Frequent	10+
SWC-22	1315	Low	Poor-fair	26+	Abundant	12+
Cuttings	1332.5- 1335	Low	Fair	26+	Rare	4+
Cuttings	1347.5- 1350	Low	Fair	23+	Rare	5+
SWC-21	1353	High	Poor-fair	36+	Common	13+
SWC-18	1371	Low	Fair	38+	Frequent	16+
SWC-13	1402	Low	Poor-fair	24+	Rare	4+
SWC-11	1412	High	Poor-fair	17+	Rare	3
SWC-8	1437.5	High	Poor-fair	34+	Rare	2
SWC-7	1457.5	High	Poor-fair	38+	Very rare	5
SWC-5	1516.5	Very low	Fair	3+		
SWC-2	1590	High	Fair-good	20+	Very rare	1
SWC-1	1599	Very low	Very poor	1+		

**Diversity:** Very low = 1-5 species Low = 6-10 species Moderate = 11-25 species High = 26-74 species Very high = 75+ species

## APPENDIX 1

## **Species Lists for Cuttings Samples.**

## Cuttings at 1292.5 to 1295 metres

Spore-pollen s	species
----------------	---------

Australopollis obscurus	Rare
Baculatisporites comaumensis	Rare
Cicatricosisporites australiensis	Rare
Clavifera triplex	Frequent
Coptospora pileolus ms	Rare
Cyathidites australis	Rare
Forcipites stipulatus	Rare
Granulatisporites trisinus RW	Rare
Herkosporites elliottii	Rare
Latrobosporites ohaiensis	Rare
Microcachryidites antarticus	Frequent
Phyllocladidites mawsonii	Frequent
Plicatipollenites spp. <b>RW</b>	Rare
Podocarpidites/Falcisporites spp.	Rare
Proteacidites spp.	Frequent
Retitriletes austroclavatidites	Rare
Retitriletes spp.	Rare
Tricolpites spp.	Rare
Tricolporites apoxyexinus	Rare
A 7	

#### Microplankton species

Milor opium poolos	
Amosopollis cruciformis	Common
Gillinia sp.	Rare
Heterosphaeridium conjunctum	Rare
Heterosphaeridium heteracanthum	Common
Hexagonifera glabra	Frequent
Hexagonifera vermiculata	Rare
Isabelidinium cretaceum	Frequent
Micrhystridium spp.	Rare
Odontochitina costata	Rare
Odontochitina porifera	Rare
Spiniferites furcatus/ramosus	Rare
•	

#### Cuttings at 1312.5 to 1315 metres.

Spore-pollen species

Rare Aequitriradites spinulosus Frequent Australopollis obscurus Rare Baculatisporites comaumensis Rare Cicatricosisporites cuneiformis Rare Cicatricosisporites n.sp. Rare Cicatricosisporites pseudotripartitus Rare Clavifera triplex Rare Cupressacites sp. Rare Cyathidites australis Rare Densoisporites velatus Rare Dilwynites echinatus ms Rare Dilwynites granulatus (small variety) Rare Dilwynites granulatus sensus strictus Rare Foraminisporis wonthaggiensis Rare Gleicheniidites circinidites Rare/caved Haloragacidites harrisii

Laevigatosporites major

Laevigatosporites musa ms

Microcachryidites antarticus

Rare

Rare

Rare

Nothofagidites emarcidus Frequent/caved
Peninsulapollis gillii Rare/caved
Perotrilites jubatus Rare

Phyllocladidites mawsonii
Plicatipollenites spp. **RW**Podosporites microsaccatus

Frequent
Rare
Rare

Proteacidites spp. Common/mostly caved

Protohaploxypinus spp. RW Rare
Retitriletes circolumenus Rare
Retitriletes spp. Rare
Rugulatisporites mallatus Rare
Stereisporites antiquisporites Rare
Stereisporites pocockii Rare

Microplankton species

Common Amosopollis cruciformis Rare Apteodinium sp. Rare Chlamydophorella nyei Common Heterosphaeridium heteracanthum Rare Isabelidinium belfastense Rare Odontochitina operculata Frequent Odontochitina porifera Rare Oligosphaeridinium complex Rare Spiniferites furcatus/ramosus Rare Wuroia? sp.

Rare

### Cuttings at 1332.5 to 1335 metres.

Spore-pollen species

Aequitriradites spinulosus Rare Appendicisporites distocarinatus Rare Araucariacites australis Rare Asteropollis asteroides Rare Baculatisporites comaumensis Rare Ceratosporites equalis Rare Cicatricosisporites cuneiformis Rare Cicatricosisporites pseudotripartitus Rare Clavifera triplex Rare Cyathidites australis Rare Dilwynites granulatus (small variety) Rare Dilwynites granulatus sensus strictus Rare Gleicheniidites circinidites Rare Laevigatosporites musa ms Rare Laevigatosporites ovatus Rare Microcachryidites antarticus Rare/caved Nothofagidites senectus Rare Phyllocladidites eunuchus ms Frequent Phyllocladidites mawsonii Rare Plicatipollenites spp. RW Rare Podocarpidites/Falcisporites spp. Rare Podosporites microsaccatus Rare Proteacidites spp. Frequent Rugulatisporites admirabilis ms Rare Schizea fromensis

Rare Stereisporites antiquisporites

Rare/caved Tricolporites apoxyexinus

Rare Fungal fruiting bodies

Microplankton species

Common Amosopollis cruciformis Common Heterosphaeridium heteracanthum Rare Isabelidinium sp. cf. I. belfastense Rare Isabelidinium cretaceum Rare Spiniferites furcatus/ramosus

#### Cuttings at 1347.5 to 1350 metres.

Spore-pollen species

Aequitriradites spinulosusRareAppendicisporites distocarinatusRareAraucariacites australisRareAustralopollis obscurusRare

Camarozonosporites apiculatus ms Rare/caved

Cicatricosisporites pseudotripartitus
Cupressacites sp.
Cyathidites australis
Densoisporites muratus
Dictyophyllidites spp.
Dictyotosporites speciosus
Rare
Rare
Rare
Rare

Forcipites stipulatus Rare/caved

Rare Gleicheniidites circinidites Rare Laevigatosporites ovatus Rare Lygistepollenites florinii Rare Microcachryidites antarticus Rare Phyllocladidites mawsonii Rare Podocarpidites/Falcisporites spp. Podosporites microsaccatus Rare Rare Proteacidites spp. Rare Rugulatisporites admirabilis ms Rare

Stereisporites antiquisporites Rare
Tricolporites apoxyexinus Rare/caved

Fungal fruiting bodies Rare

Microplankton species

Amosopollis cruciformis

Cribroperidinium edwardsii

Heterosphaeridium heteracanthum

Odontochitina porifera

Common

Frequent

Frequent

Rare/caved

Spiniferites furcatus/ramosus Rare

#### PE900757

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The enclosure PE900757 has the following characteristics:

ITEM_BARCODE = PE900757

CONTAINER_BARCODE = PE900963

NAME = Palynomorph Range Chart, 1 of 2

BASIN = OTWAY

PERMIT = PPL2 TYPE = WELL

SUBTYPE = DIAGRAM

DESCRIPTION = Palynomorph Range Chart, 1 of 2, Iona-2

REMARKS =

DATE_CREATED = 20/06/94

DATE_RECEIVED = 19/01/95

 $W_NO = W1095$ 

WELL_NAME = IONA-2

CONTRACTOR =

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BASIN = OTWAY

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TYPE = WELL

SUBTYPE = DIAGRAM

DESCRIPTION = Palynomorph Range Chart, 2 of 2, Iona-2

REMARKS =

DATE_CREATED = 20/06/94

DATE_RECEIVED = 19/01/95

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WELL_NAME = IONA-2

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APPENDIX 7

## **GFE RESOURCES LTD**

# **APPENDIX 7**

## PETROGRAPHY REPORT

**IONA-2** 



PETROLOGY REPORT

IONA #2

OTWAY BASIN



#### PETROLOGY REPORT

IONA #2

OTWAY BASIN

Report prepared for GFE Resources Ltd

by

Dr J KEENE

on behalf of

ACS LABORATORIES PTY LTD Unit 1, 167 Richmond Rd Richmond SA 5033

June 1994

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#### 1. INTRODUCTION

GFE Resources Ltd submitted 7 sidewall cores from Iona #2 in the Otway Basin, for detailed petrological analysis. No interpretation of the data was requested.

The following samples were examined:

Swc	Depth (m)	Thin section	XRD
12	1408.5	*	*
11	1412	*	-
10	1418	*	-
9	1426	*	-
6	1469	*	-
5	1516.5	*	-
3	1550.5	*	=

#### 2. METHODS

Sidewall cores were impregnated with araldite prior to thin section preparation. Blue dye was used in the araldite to facilitate description of porosity and permeability. Thin sections were systematically scanned to determine lithology, composition, porosity and textural relationships. All percentages given in thin section descriptions are based on visual estimates, not point counts. Rock classifications are based on the work of Folk (1974) for clastics and Dunham (1962) for carbonates.

To determine bulk mineralogy by X-ray diffraction, one sample was ground in a Siebtechnick mill and back mounted into an aluminium holder. A continuous scan was run of this powder pressing from 3° to 75° 2 theta, at 1°/minute, using Co K alpha radiation, 50kV and 35mA, on a Philips PW1050 diffractometer. For detailed clay mineralogy a less than 5 micron size fraction was separated. This was done by hand crushing, addition of dispersion solution, mechanical shaking for 10 minutes and settling of the dispersed material in a water column according to Stokes' Law. The less than 5 micron fraction was pipetted off and prepared as an oriented sample on ceramic plates held under vacuum. Samples were saturated with Mg solution and treated with glycerol. Continuous scans of oriented clay samples were run from 3° to 35° 2 theta at 1°/minute. Peaks were identified by comparison with JCPDS files stored in a computer program called XPLOT.

#### 3. PETROLOGY

#### 3.1 Iona #2, Swc 12, depth 1408.5m

Thin section description

Rock classification:

Feldspathic litharenite

#### Texture:

This feldspathic litharenite is moderately well to mineralogically immature and texturally submature to mature. Detrital grains range in diameter from approximately 0.05mm (coarse silt) to 0.75mm (coarse sand) and have an average size of 0.3mm (medium sand). Typically the grains of quartz and feldspar are angular with moderate to high sphericity whereas the lithics are rounded to subrounded with low sphericity (Fig. 1a). Texturally the feldspathic litharenite is grain supported with concavo-convex and sutured grain contacts dominant. and deformed lithic grains indicate that there has been considerable mechanical compaction. Elongate lithic grains and micas give the rock a slight fabric. No sedimentary structures are evident.

#### Porosity:

Porosity is mainly primary with only a minor contribution from secondary pores. Primary pores are intergranular in nature but do not appear to be interconnected in thin section. Rare fracturing of feldspar and quartz and possible solution of carbonate cement has enhanced the interconnections. There is no evidence of dissolution of lithic grains.

Visual Estimate of Con	nposition	%
Framework grains	Quartz	12
	Feldspar	18
	Lithics	47
	Mica	2
	Accessory minerals	tr
Matrix		nd
Authigenic minerals	Chlorite	8
and cements	Carbonate	2
	Kaolin	2
	Glaucony	tr
	Pyrite	tr
Porosity	Intergranular	8
	Dissolution	tr
·	Fractures	tr

#### Framework grains:

Quartz is mostly monocrystalline with a minor amount of polycrystalline grains. Monocrystalline quartz has straight extinction, is water clear and some grains are subhedral indicating a volcanic source. Polycrystalline quartz has undulose extinction and is often as elongate grains suggesting a metamorphic origin. Feldspars are generally very fresh and display a variety of twinning and zoning (Fig. la). Plagioclase dominates with minor amounts of perthite and microcline. Rare grains have a dusty appearance due to alteration and sericitisation while others have been partly replaced by carbonate. More than half the framework grains are lithics and these are mostly a variety of volcanic rock fragments and fine grained metasediments and a small amount of chert. Lithics are deformed and squashed to fill the pore spaces and

include some larger shale clasts (up to 1mm). Biotite stacks and flakes are typically bent and replaced in part by chlorite and FeO.

Authigenic minerals and cements:

A green chlorite forms a rim cement throughout the rock (Fig. 1b). It lines all pores and has a fairly uniform thickness of 5-10 microns. This early cement was followed by isolated patches of clear carbonate spar. Where it occurs it is a pore filling cement and has also replaced feldspar. The lack of exposed crystal faces may indicate that it has undergone some dissolution. A minor amount of authigenic kaolin is also present and postdates the chlorite. The books of kaolin fill or partly fill pores. A trace of euhedral to subhedral opaque grains are most likely pyrite. A few green sand size grains are composed of clay and have been interpreted as glaucony. Most of the detrital grains have a brownish staining due to organic matter (hydrocarbons?).

X-ray diffraction

Bulk XRD (Fig. 2a) indicates that quartz (Q) and feldspars (F) are the dominant minerals with lesser amounts of mica (M), chlorite (C) and kaolinite (K). The trace also indicates a very small amount of calcite (Ca), however the composition of the carbonate should be confirmed by other techniques because the optical properties are similar to siderite. The clay fraction (Fig. 2b) is dominated by chlorite/mixed layer clay mineral (C/S) and kaolinite with a minor amount of mica (illite?).

#### PE906677

This is an enclosure indicator page. The enclosure PE906677 is enclosed within the container PE900963 at this location in this document.

The enclosure PE906677 has the following characteristics:

ITEM_BARCODE = PE906677
CONTAINER_BARCODE = PE900963

NAME = Photomicrograph, Appendix 7, 1 of 4

BASIN = OTWAY PERMIT = PPL2

 $\begin{array}{rcl} \mathtt{TYPE} &=& \mathtt{WELL} \\ \mathtt{SUBTYPE} &=& \mathtt{PHOTOMICROGRAPH} \end{array}$ 

DESCRIPTION = Photomicrograph, Appendix 7, Figure 1,

1 of 4, Iona-2

REMARKS =

DATE_CREATED = 30/06/94 DATE_RECEIVED = 19/01/95

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WELL_NAME = IONA-2

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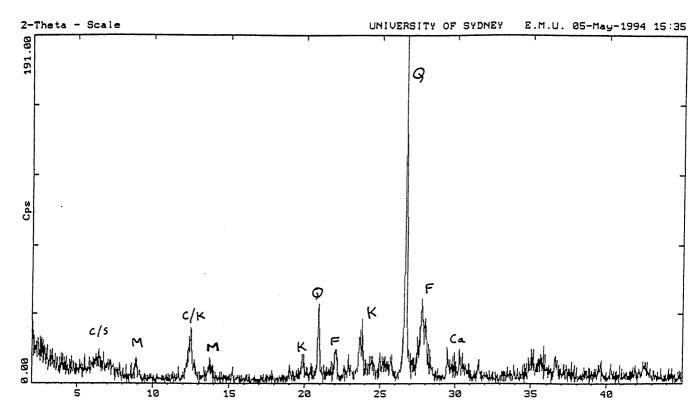


Figure 2a
Bulk XRD trace of Iona #2, Swc 12, depth 1408.5m.

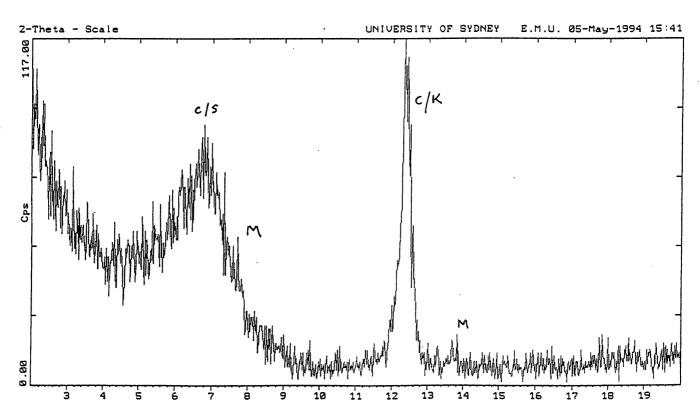


Figure 2b
XRD trace of the clay fraction from Iona #2, Swc 12, depth 1408.5m.

#### 3.2 <u>Iona #2, Swc 11, depth 1412m</u>

Thin section description

Rock classification:

Feldspathic litharenite

#### Texture:

This feldspathic litharenite is moderately sorted, mineralogically immature and texturely submature to immature. Detrital grains range in diameter from approximately 0.05mm (coarse silt) to 0.5mm (medium sand) and have an average size of 0.2mm (fine sand). Typically the grains of quartz and feldspar are angular with low to moderate sphericity whereas the lithics are rounded to subrounded with low sphericity (Fig. 3a). Texturally the feldspathic litharenite is grain supported with concavoconvex and sutured grain contacts dominant. Bent micas and deformed lithic grains indicate that there has been considerable mechanical compaction. Elongate lithic grains and micas give the rock an indistinct lamination with coarser, better sorted laminae (5mm) containing less mica. No other sedimentary structures are evident.

#### Porosity:

Porosity is mainly primary with only a minor contribution from secondary pores. Primary pores are intergranular in nature but do not appear to be interconnected in thin section. Rare dissolution of feldspar has had little effect on porosity. Micas lying parallel to bedding prevent interconnection of pores and squashed lithic fragments have deformed to fill most pores. There is no evidence of dissolution of lithic grains.

Visual Estimate of Con	%	
Framework grains	Quartz	16
1	Feldspar	22
	Lithics	30
	Mica	10
	Accessory minerals	tr
Matrix		nd
Authigenic minerals	Chlorite	10
and cements	Zeolite	1
	Pyrite	tr
Porosity	Intergranular	10
	Dissolution	tr

#### Framework grains:

Quartz is mostly monocrystalline with a minor amount of polycrystalline. Monocrystalline quartz has straight extinction, is water clear and some grains are subhedral indicating a volcanic source. Polycrystalline quartz has undulose extinction and is often as elongate grains suggesting a metamorphic origin particularly since there are rock fragments of this quartz intergrown with muscovite. There are more feldspars than quartz and they are generally very fresh and display a variety of twinning and Plagioclase dominates with minor amounts of perthite and zoning. microcline. Rare grains have a dusty appearance due to alteration and Lithics are the most abundant clasts and are mostly a sericitisation. variety of volcanic rock fragments and fine grained metasediments and a small amount of chert. They are deformed and squashed to fill the pore spaces. Biotite is by far the most abundant detrital mica, forming stacks and flakes which are typically bent and replaced in part by chlorite and FeO. Muscovite is unaltered. Traces of accessory minerals are apatite, tourmaline and amphibole.

Authigenic minerals and cements:

A green chlorite forms a rim cement throughout the rock and is generally 5-10 microns thick. It lines most pores and in some cases fills the pores forming a pseudo-matrix. This early cement is followed by isolated crystals of a low birefringent zeolite (laumontite?). Where it occurs it is a pore filling cement. No carbonate is present in this sample.

#### PE906678

This is an enclosure indicator page. The enclosure PE906678 is enclosed within the container PE900963 at this location in this document.

The enclosure PE906678 has the following characteristics:

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CONTAINER_BARCODE = PE900963

NAME = Photomicrograph, Appendix 7, 2 of 4

BASIN = OTWAY PERMIT = PPL2

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REMARKS =

DATE_CREATED = 30/06/94

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 $W_NO = W1095$ 

WELL_NAME = IONA-2

CONTRACTOR =

CLIENT_OP_CO = GFE RESOURCES LTD

(Inserted by DNRE - Vic Govt Mines Dept)

#### 3.3 Iona #2, Swc 10, depth 1418m

#### Thin section description

Rock classification:

Feldspathic litharenite

#### Texture:

moderately This feldspathic litharenite is to well sorted, mineralogically immature and texturely submature to mature. Detrital grains range in diameter from approximately 0.05mm (coarse silt) to 1mm (coarse sand) and have an average size of 0.3mm (medium sand). Typically the grains of quartz and feldspar are larger and angular with moderate to high sphericity whereas the lithics are rounded to subrounded with low Texturally the feldspathic litharenite is grain supported sphericity. with tangental and concavo-convex grain contacts dominant. sandstone has an open framework, nevertheless bent micas and deformed lithic grains indicate that there has been some mechanical compaction. Elongate lithic grains and micas give the rock a weak fabric. sedimentary structures are evident.

#### Porosity:

Porosity is mainly primary with only a minor contribution from secondary pores. Primary pores are intergranular in nature and do appear to be interconnected in thin section. This sample has a definite open framework which does not appear to be an artifact of the drilling process. Fracturing of feldspar and quartz is common and may enhance permeability. Some of the feldspar grains have undergone dissolution. There is no evidence of dissolution of lithic grains.

Visual Estimate of Con	%	
Framework grains	Quartz	15
-	Feldspar	20
	Lithics	35
	Mica	2
<u> </u>	Accessory minerals	tr
Matrix		nd
Authigenic minerals	Chlorite	5
and cements	Carbonate	tr
	Pyrite	tr
Porosity	Intergranular	20
-	Dissolution	1
•	Fractures	1

#### Framework grains:

Quartz occurs mostly as monocrystalline clasts with a minor amount of Monocrystalline quartz has straight extinction, is polycrystalline. water clear and some grains are subhedral indicating a volcanic source. Polycrystalline quartz has undulose extinction and is often as elongate grains suggesting a metamorphic origin. Feldspars are generally very fresh and display a variety of twinning and zoning. Plagioclase dominates with minor amounts of perthite and microcline. Rare grains have a dusty appearance due to alteration and sericitisation. Lithics dominate the composition and are mostly a variety of volcanic rock fragments and fine grained metasediments and a small amount of chert. Some are deformed and squashed to fill the pore spaces. Biotite is the most abundant mica and its grains are typically bent and replaced in part by chlorite and FeO. Traces of accessory mineral are epidote.

Authigenic minerals and cements:

A green chlorite forms a rim cement throughout the rock 5-10 microns thick. It lines most pores and it fills some of the smaller pores to form a pseudo-matrix. A few green sand size grains are composed of clay and are the most squashed. They have been interpreted as glaucony. There is a trace of a subhedral opaque mineral, most likely pyrite. Carbonate fills some pores near a shale intraclast. Most of the grains have a brownish staining due to organic matter.

#### 3.4 Iona #2, Swc 9, depth 1426m

Thin section description

Rock classification:

Feldspathic litharenite

#### Texture:

This feldspathic litharenite is moderately sorted, mineralogically immature and texturely submature to mature. Detrital grains range in diameter from approximately 0.05mm (coarse silt) to 0.75mm (coarse sand) and have an average size of 0.25mm (fine to medium sand). Typically the grains of quartz and feldspar are larger and angular with moderate to high sphericity whereas the lithics are rounded to subrounded with low sphericity (Fig. 4). Texturally the feldspathic litharenite is grain supported with tangential and concavo-convex grain contacts dominant. This sandstone has an open framework, nevertheless bent micas and deformed lithic grains indicate that there has been some mechanical compaction. Elongate lithic grains and micas give the rock a weak fabric. No sedimentary structures are evident.

#### Porosity:

Porosity is mainly primary with only a minor contribution from secondary pores (Fig. 4). Primary pores are intergranular in nature and do appear to be interconnected in thin section. This sample has a definite open framework which does not appear to be an artefact of the drilling process. Fracturing of feldspar and quartz is common and may enhance permeability. Some of the feldspar grains have undergone dissolution. There is no evidence of dissolution of lithic grains.

Visual Estimate of Composition %				
Framework grains	Quartz	9		
_	Feldspar	20		
	Lithics	38		
	Mica	5		
	Accessory minerals	tr		
Matrix		nd		
Authigenic minerals	Chlorite	10		
and cements	Pyrite	tr		
Porosity	Intergranular	15		
	Dissolution	1		
	Fractures	1		

#### Framework grains:

Quartz is less than ten percent of the framework grains and occurs mostly as monocrystalline clasts with a minor amount of polycrystalline. Monocrystalline quartz has straight extinction, is water clear and some grains are subhedral indicating a volcanic source. Polycrystalline quartz has undulose extinction and is often as elongate grains suggesting a metamorphic origin. Feldspars form more than a quarter of the framework and are generally very fresh and display a variety of twinning Plagioclase dominates with minor amounts of perthite and and zoning. Rare grains have a dusty appearance due to alteration and microcline. sericitisation. sericitisation. Lithics dominate the composition and are mostly a variety of volcanic rock fragments and fine grained metasediments and a small amount of chert. Some are deformed and squashed to fill the pore Biotite is the most abundant mica and its grains (stacks and flakes) are typically bent and replaced in part by chlorite and FeO. Muscovite is rare and traces of accessory mineral are sphene and

pyroxene.

Authigenic minerals and cements:

A green chlorite forms a rim cement throughout the rock 5-10 microns thick. It lines all pores and it fills some of the smaller pores to form a pseudo-matrix. A few green sand size grains are composed of clay and are the most squashed. They have been interpreted as glaucony. There is a trace of a subhedral opaque mineral, most likely pyrite. Most of the grains have a brownish staining due to organic matter.

#### PE906679

This is an enclosure indicator page. The enclosure PE906679 is enclosed within the container PE900963 at this location in this document.

The enclosure PE906679 has the following characteristics:

ITEM_BARCODE = PE906679
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NAME = Photomicrograph, Appendix 7, 3 of 4

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PERMIT = PPL2
TYPE = WELL

SUBTYPE = PHOTOMICROGRAPH

DESCRIPTION = Photomicrograph, Appendix 7, Figure 4,

3 of 4, Iona-2

REMARKS =

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> W_NO = W1095 WELL_NAME = IONA-2

CONTRACTOR =

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(Inserted by DNRE - Vic Govt Mines Dept)

#### 3.5 Iona #2, Swc 6, depth 1469m

Thin section description

Rock classification: Feldspathic litharenite

#### Texture:

This feldspathic litharenite is mineralogically immature and texturely submature to mature. The sorting of the sand fraction is variable ranging from well to poorly sorted (bioturbated?). Detrital grains range in diameter from approximately 0.05mm (coarse silt) to 0.4mm (medium sand) and have an average size of 0.3mm (medium sand). Typically the grains of quartz and feldspar are larger and angular with moderate to high sphericity whereas the lithics are rounded to subrounded with low sphericity. Texturally the feldspathic litharenite is grain supported with tangential and concavo-convex grain contacts dominant. This sandstone has an open framework, nevertheless bent micas and deformed lithic grains indicate that there has been some mechanical compaction.

#### Porosity:

Porosity is mainly primary with only a minor contribution from secondary pores. Primary pores are intergranular in nature and do appear to be interconnected in thin section. This sample has a definite open framework which does not appear to be an artifact of the drilling process. Fracturing of feldspar and quartz is common and may enhance permeability. Some of the feldspar grains have undergone dissolution. There is no evidence of dissolution of lithic grains.

Visual Estimate of Composition %				
Framework grains	Quantz	10		
	Feldspar	23		
	Lithics	33		
	Mica	4		
Matrix		nd		
Authigenic minerals	Chlorite	8		
and cements	Pyrite	tr		
Porosity	Intergranular	20		
-	Fracture	1		

#### Framework grains:

Quartz occurs mostly as monocrystalline clasts with a minor amount of polycrystalline. Monocrystalline quartz has straight extinction, is water clear and some grains are subhedral indicating a volcanic source. Polycrystalline quartz has undulose extinction and occurs as elongate grains suggesting a metamorphic origin. Feldspars are generally very fresh and display a variety of twinning and zoning. Plagioclase dominates with minor amounts of perthite and microcline. Rare grains have a dusty appearance due to alteration and sericitisation. Lithics dominate the composition and are mostly a variety of volcanic rock fragments and fine grained metasediments and a small amount of chert. Some are deformed and squashed to fill the pore spaces. Biotite is the most abundant mica and its grains are typically bent and replaced in part by chlorite and FeO.

#### Authigenic minerals and cements:

A green chlorite forms a rim cement throughout the rock 5-10 microns thick. It lines most pores and it fills some of the smaller pores to form a pseudo-matrix. There is a trace of a subhedral opaque mineral,

most likely pyrite.

#### 3.6 Iona #2, Swc 5, depth 1516.5m

Thin section description

Rock classification:

Feldspathic litharenite

#### Texture:

This feldspathic litharenite is moderately to well sorted. mineralogically immature and texturely submature to mature. Detrital grains range in diameter from approximately 0.05mm (coarse silt) to 0.5mm (medium sand) and have an average size of 0.35mm (medium sand). Typically the grains of quartz and feldspar are angular with moderate to high sphericity whereas the lithics are rounded to subrounded with low sphericity (Fig. 5a). Texturally the feldspathic litharenite is grain supported with concave convey and support grain contacts deminant. supported with concavo-convex and sutured grain contacts dominant. micas, deformed lithic grains and fractured quartz and feldspar indicate that there has been considerable mechanical compaction. Elongate lithic grains and micas give the rock a weak fabric. No sedimentary structures are evident.

#### Porosity:

Porosity is mainly primary with only a minor contibution from secondary pores. Porimary pores are intergranular in nature but do not appear to be interconnected in thin section. Rare fracturing of feldspar and quartz has enhanced the interconnections and some dissolution of feldspars has occurred. There is no evidence of dissolution of lithic grains.

Visual Estimate of Con	nposition	%
Framework grains	Quartz	18
	Feldspar	20
	Lithics	34
	Mica	2
	Accessory minerals	1
Matrix		nd
Authigenic minerals	Chlorite	8
and cements	Apatite	tr
	Glaucony	1
	Zeolite	1
Porosity	Intergranular	12
	Dissolution	1
	Fractures	1

#### Framework grains:

Quartz and feldspar are present in approximately equal amounts. is mostly monocrystalline with a minor amount of polycrystalline. Monocrystalline quartz has straight extinction, is water clear and some grains are subhedral indicating a volcanic source. Polycrystalline quartz has undulose extinction and is often as elongate grains suggesting a metamorphic origin. Feldspars are generally very fresh and display a variety of twinning and zoning. Plagioclase dominates with minor amounts of perthite and microcline. Rare grains have a dusty appearance due to alteration and sericitisation. Lithics form about half the framework grains and are mostly a variety of volcanic rock fragments and fine grained metasediments and a small amount of chert. They are deformed and squashed to fill the pore spaces and include some grains of devitrified Biotite stakes and flakes are typically bent and volcanic glass. replaced in part by chlorite and FeO. Muscovite is rare. Accessory

minerals are sphene and epidote.

Authigenic minerals and cements:

A green chlorite cement forms a rim of fibres (plates) 5-15 microns thick coating the detrital grains throughout the rock. It lines all pores and fills many. This early cement is followed by clear zeolite, probably laumontite. Where the zeolite occurs it is a pore filling cement (Fig. 5b). A few green sand size grains are composed of clay and have been interpreted as glaucony. These grains could be devitrified volcanic glass. Euhedral apatite forms small (20 microns) prismatic crystals in one of the pores. Most of the detrital grains have a brownish staining due to organic matter. Opaque grains of pyrite are also present in trace amounts.

#### PE906680

This is an enclosure indicator page.

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The enclosure PE906680 has the following characteristics:

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SUBTYPE = PHOTOMICROGRAPH

REMARKS =

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> W_NO = W1095 WELL_NAME = IONA-2

CONTRACTOR =

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#### 3.7 <u>Iona #2, Swc 3, depth 1550.5m</u>

#### Thin section description

Rock classification:

Feldspathic litharenite

Texture:

This feldspathic litharenite is mineralogically immature and texturally submature. The sorting of the sand fraction is moderate. Detrital grains range in diameter from approximately 0.05mm (coarse silt) to 0.5mm (medium sand) and have an average size of 0.25mm (medium sand). Typically the grains of quartz and feldspar are larger and angular with moderate to high sphericity whereas the lithics are rounded to subrounded with low sphericity. Texturally the feldspathic litharenite is grain supported with tangential and concavo-convex grain contacts dominant. This sandstone has an open framework, nevertheless bent micas and deformed lithic grains indicate that there has been some mechanical compaction.

#### Porosity:

Porosity is mainly primary with only a minor contribution from secondary pores. Primary pores are intergranular in nature and do appear to be interconnected in thin section. This sample has a definite open framework which does not appear to be an artifact of the drilling process. Fracturing of feldspar and quartz is common and may enhance permeability. Some of the feldspar grains have undergone dissolution. There is no evidence of dissolution of lithic grains.

Visual Estimate of Composition		%
Framework grains	Quartz	12
	Feldspar	25
	Lithics	30
	Mica	tr
	Accessory	tr
Matrix		nd
Authigenic minerals	Chlorite	8
and cements	Pyrite	tr
Porosity	Intergranular	24
	Fracture	tr
	Solution	tr

#### Framework grains:

Quartz occurs mostly as monocrystalline clasts with a minor amount of polycrystalline. Monocrystalline quartz has straight extinction, is water clear and some grains are subhedral indicating a volcanic source. Polycrystalline quartz has undulose extinction and is often as elongate grains suggesting a metamorphic origin. Feldspars are generally very fresh and display a variety of twinning and zoning. Plagioclase dominates with minor amounts of perthite and microcline. Rare grains have a dusty appearance due to alteration and sericitisation. Lithics dominate the composition and are mostly a variety of volcanic rock fragments and fine grained metasediments and a small amount of chert. Some are deformed and squashed to fill the pore spaces. Biotite is present as squashed and bent flakes and accessory minerals are epidote and sphene.

Authigenic minerals and cements:
Well developed green chlorite rims form a cement throught the rock 5-10 microns thick. It lines most pores and it fills some of the smaller pores to form a pseudo-matrix. There is a trace of a subhedral opaque mineral, most likely pyrite.

#### 4. GLOSSARY OF TERMS

Boehm lamellae

Parallel trails of vacuoles in quartz that are thought to form during deformation (metamorphism) of grains.

Framboid

A cluster of pyrite crystals with a spheroidal outline.

**Glaucony** 

A term used to describe green minerals without any genetic connotations. If the green minerals can be identified, a specific mineral name is given.

**Granophyric Texture** 

A variety of micrographic intergrowth of quartz and alkali feldspar that is either crudely radiate or is less regular than micrographic texture.

Honeycomb Porosity

Secondary porosity produced by the corrosion (etching) of detrital grains.

Hydrocarbon envelope

Solid bitumen surrounding a mineral containing radioactive elements. Radiation causes polymerisation of hydrocarbon chains within oil that rims grains.

Micrographic Intergrowth

A regular intergrowth of two minerals.

nd

Abbreviation meaning not detected.

Neomorphism

All transformations between a mineral and the same mineral, or another of the same general composition.

**Poikilitic** 

A textural term for an igneous rock in which a relatively large crystal of one mineral encloses numerous smaller crystals of one, or more, other minerals which are randomly oriented and generally, but not necessarily, uniformly distributed.

**Poikilotopic** 

A sedimentary textural term denoting a single crystal of carbonate enclosing more than one framework grain.

Radiate Texture

Textures in which elongate crystals diverge from a common nucleus.

<u>Porphyritic</u>

A textural term applied to igneous rocks in which there are two distinct grain sizes present.

**Spherulitic** 

The presence of more or less globular masses of generally acicular crystals, having a radial arrangement. spherulites form as a result

of devitrification of volcanic glass.

#### **Trachytic**

A textural term applied to the groundmasses of volcanic rocks in which there is a subparallel arrangement of microcrystalline, lath shaped feldspars. The term is not restricted in use to rocks of trachyte composition.

#### <u>Vacuole</u>

Gas or liquid filled inclusion.

# APPENDIX 8

### **GFE RESOURCES LTD**

## **APPENDIX 8**

### **GEOCHEMISTRY REPORT**

**IONA-2** 

# HYDROCARBON CHARACTERISATION STUDY IONA-2

Prepared for:

GFE Resources Limited

April 1994



## HYDROCARBON CHARACTERISATION STUDY IONA-2

#### **Introduction**

Hydrocarbon shows in the well lona-2, drilled by GFE Resources Ltd in permit PPL-2 in the Otway Basin, were analysed geochemically.

The purpose of this study was to characterise these hydrocarbons in terms of source, maturity and possible biodegradation and to correlate them with hydrocarbons in Iona-1, SWC 7, 1391.5m.

#### **Analytical Procedure**

Three cuttings samples form 1365m, 1385m and 1410m depth were submitted for thermal extract GC during drilling (25.2.94) of the well in order to quickly characterise the hydrocarbons present, and SWC 1358m was analysed by the same method later (4.3.94).

Eight SWCs between 1358m and 1550.5m were solvent extracted and three whole extracts were subsequently analysed by GC (1392.0m, 1469.0m, 1550.5m). The five other extracts were submitted for liquid chromatography and GC of their saturate fractions and two of them (1358m and 1408.4m) also to GC-MS of their branched/cyclic saturates as well as their aromatic fractions.

One SWC from the well lona-1 (SWC7, 1391.5m) was solvent extracted and analysed by LC and GC sat, and these data were compared with lona-2 extracts.

Standard water analysis was carried out on a sample from Iona-2, 1361.8m.

Analytical results obtained are presented in the following figures and tables:

Type of Analysis	Figure	Table
Water analysis	-	1
Thermal extract GC	1	2
Solvent extraction/ liquid chromatography	· _	3
GC (whole extract and saturate fraction)	2	4
GC-MS b/c	3	5
GC-MS arom	4	6

#### Water analysis

Analytical procedures applied are summarised in the "Theory and Methods" chapter in the back of this report.

#### **General Information**

Two copies of this report have been sent to Noel Newell from GFE Resources Ltd. Any queries related to it may be directed to Dr. Birgitta Hartung-Kagi of Geotechnical Services Pty Ltd.

All data and information are proprietary to GFE Resources Ltd and regarded as highly confidential by all Geotech personnel.

Geotechnical Services Pty Ltd shall not be responsible or liable for the results of any actions taken on the basis of the information contained in this study, nor for any errors or omissions in it.

#### Results and Interpretation

#### A. Gas chromatography

Thermal extract GC performed on four samples between 1358m and 1410m characterises the hydrocarbons in SWC at 1358.0m as an oil depleted in nalkanes below  $C_{17}$  and rich in  $C_{23+}$  compounds. The reason for this lack of low molecular weight n-alkanes is probably a minor degree of biodegradation rather than the residual nature of the oil which would have resulted in a lack of all light saturates, not just n-alkanes.

An S₁ value of 20.10mg/g calculated for this depth indicates that the sediment is very rich in free hydrocarbons whereas the three deeper samples (cuttings at 1365m, 1385m, 1410m) are considerably leaner (S₁ values between 0.40 and 0.59).

The overall pictures of these three samples are characterised by considerable levels of hydrocarbons in the low molecular weight range and the presence of a baseline hump underneath the  $C_{18+}$  n-alkane profile. This hump is particularly strong at 1410m and believed to represent a pipe dope-like drilling additive rather than a natural part of the extracts.

Particularly the trace obtained at 1385m clearly characterises the terrestrial nature of the hydrocarbons superimposed on the baseline hump (odd-even predominances in the  $C_{23+}$  n-alkane range).

Differences between thermal extract GC data for sample 1358m on one hand and the three deeper samples on the other are probably (at least partly) due to reservoir properties, that is, the lack of light compounds at 1358m is believed to be secondary.

**Upon** solvent extaction, three SWCs between 1358m and 1381m yielded excellent amounts of free hydrocarbons, decreasing from 10700 to 5600ppm throughout this interval.

The overall picture of the GC traces obtained for these three samples are very similar and are believed to characterise the same mature, migrated oil. Odd-even predominances in the  $n-C_{23+}$  range reflect considerable input

from a terrestrial source, which is in agreement with high pristane/n- $C_{17}$  ratios (1.17 to 3.02) usually found in coaly samples. Pristane/phytane ratios between 4.81 and 5.39 characterise an oxic environment during deposition of the organic source matter.

The sample at 1392m yielded very low amounts of total extract (69.4ppm), which might suggest that this depth is below the palaeo OWC. Liquid chromatography/GC saturate analyses were not possible due to the small amount of extract recovered. GC of the whole extract was performed instead but, because interference of non-alkanes, no meaningful results could be obtained.

SWCs at 1408.5m and 1426m yielded good and poor amounts of total extract, respectively (1414 and 143ppm), and GC sat traces with well developed n-alkanes between n-C₉ and n-C₃₁ indicative of a mature, undegraded oil in both cases.

Slight odd-even predominances in the  $n-C_{23+}$  range suggest input from higher plant waxes, and pristane/phytane ratios of 5.12 and 4.73 reflect oxic conditions during deposition of the organic source matter.

The two deepest samples, at 1469m and 1550.5m, contain only very low amounts of extractable organic matter (approximately 40 and 30ppm, respectively) and the overall pictures of their GC traces are similar to the one obtained at 1392m. The decrease in extractable organic matter from 1408.5m to 1550.5m and the GC characteristics suggest that the two deeper samples may have been below the palaeo OWC.

A sample from Iona-1, 1391.5m, was also analysed by liquid chromatography and GC of the saturate fraction. The sediment is rich in total extract (2450ppm) and the overall picture of its GC trace is similar to traces obtained for Iona-2, 1358m to 1381m, ie appears to be mature and shows a lack of compounds below  $n-C_{17}$ , as well as slight odd-even predominances in the  $n-C_{23+}$  range. However, while GC traces for 1358m to 1381m are only depleted in light n-alkanes (believed to be caused by biodegradation), the almost total lack of compounds below  $C_{17}$  in this sample is probably due to long storage time and resulting evaporation effects.

The major differences between the two lona-2 and the lona-1 extracts are their pristane/n- $C_{17}$  ratios which are high in lona-2 (1.17 to 3.02) and low in lona-1 (0.53). As bacterial attack suspected in lona-2 would preferentially reduce n- $C_{17}$  (straight chain), compared with pristane (isopenoid structure), the value for pristane/n- $C_{17}$  in this well may be "artificially" high. In lona-1, on the other hand, the loss of light ends due to storage would probably also have affected pristane, and the same ratio in the old well could be "artificially" low.

The predominance of pristane over n- $C_{17}$  can be due to the coaly nature of organic material or to low maturity levels, the lona-2 extracts, however, are believed to be fully mature to date (see below). It may therefore be possible that the source material which generated the hydrocarbons reservoired in lon-1, 1391.5m was less coaly/terrestrial than the sediments which generated the lona-2 oil. GC-MS analysis would be necessary to confirm this assumption.

#### B. GC-MS Analysis

Biomarker distributions were determined for the branched/cyclic and aromatic fractions of samples 1358m and 1408m and these patterns are virtually identical for the two samples which reflects their genetic relationship and which supports the GC-based assumptions that the lack of light ends in the shallower sample is secondary, probably due to biodegradational effects.

Oil recovered from 1358m and 1408.5m was sourced from very terrestrial, coaly organic matter characterised by the presence of codalene and retene, a strong predominance of C₂₉ over C₂₇ diasteranes and steranes and a suite of bi-, tri- and tetracyclic diterpenoids (19-norlabdane, isopimarane, beyerane, 17-nortetracyclane), markers for resinous matter in higher plants.

Though pristane/phytane ratios of around 5 appear to suggest oxic conditions during deposition of the source sediment, the presence of methylhopanes and  $C_{29}$  as well as  $C_{30}$  diahopanes characterise more suboxic depositional environments.

The oil is fully mature to date as reflected in  $C_{29}$  20S/20R ratios of 0.94 and 0.95 and by MP1 values of between 1.06 and 1.21, equivalent to  $V_R$  values of approximately 1 to 1.1%.

9 March, 1994

GFE Resources Ltd 11th Floor 151 Flinders Street Melbourne VIC 3000

#### Table 1

## WATER ANALYSIS IONA # 2 RFT 1361.8m

Ph			6.05
Conductivity @ 25°C	29400		
Resistivity (ohm.m)	0.34		
Density @ 25 ⁰ C (g/cr	1.012		
Total Dissolved Solids	18815		
		<u>(mg/l)</u>	(me/l)
Sodium	Na	3180	138.26
Potassium	K	3350	85.90
Calcium	Ca	100	5.00
Magnesium	Mg	35.5	2.96
Soluble iron	Fe(s)	5.0	-
Chloride	CI	7300	205.63
Carbonate	CO ₃	Nil	-
Bicarbonate	HCO ₃	1205	19.75
Sulphate	S0 ₄	42	0.88
Nitrate	NO3	4.9	0.08
Sum of lons		15217	

TABLE 2

IONA 2	GHM Bulk Composition and Thermal Extraction Data
A. Bulk Compositional Data	

DEPTH(m)	Sample Type	S1	\$2	Pi	S1/TOC	НІ
1358.0	swc	20.10	1.43	0.93	nd	nd
1365.0	Cuttings	0.47	1.09	0.30	nd	nd
1385.0	Cuttings	0.59	2.34	0.20	nd	nd
1410.0	Cuttings	0.40	0.51	0.44	nd	nd

TABLE 2

IONA 2

GHM Bulk Composition and Thermal Extraction Data

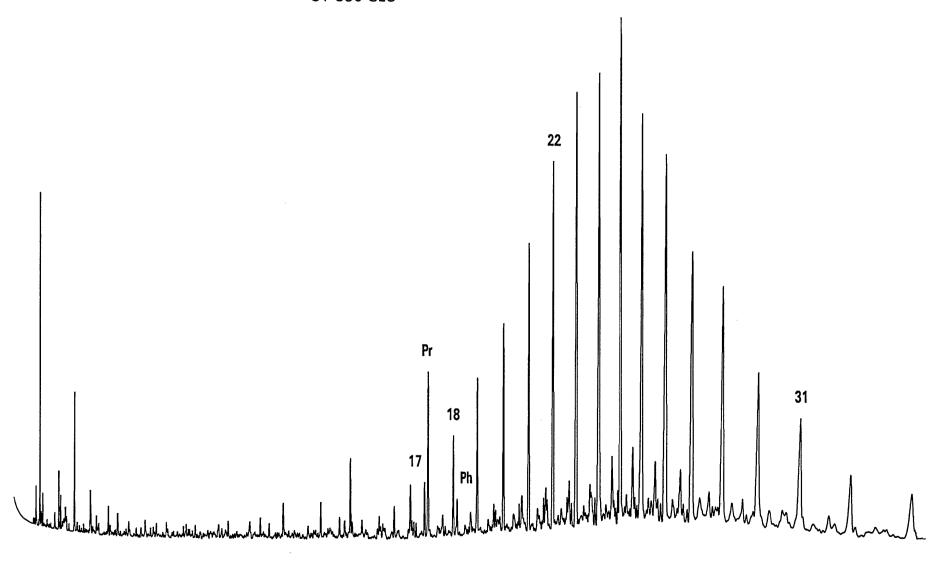
#### B. Thermal Extraction Data

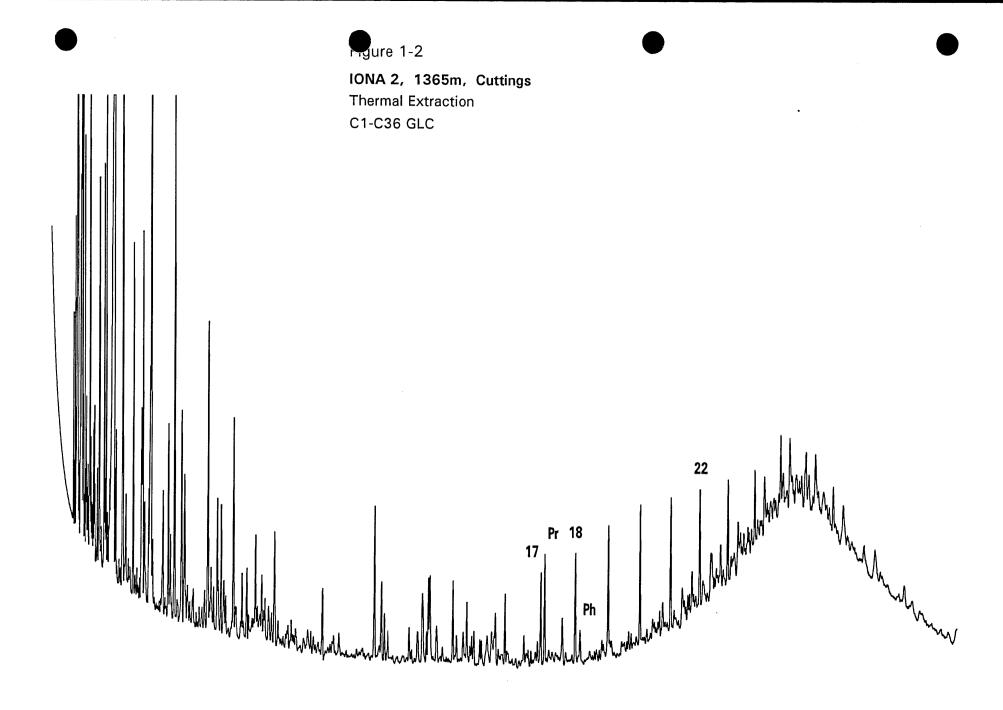
DEPTH(m)	Sample Type	Prist./Phyt.	Prist./n-C17	Phyt./n-C18
1358.0	swc	4.9	3.3	0.4
1365.0	Cuttings	nd	nd	nd
1385.0	Cuttings	nd	nd	nd
1410.0	Cuttings	nd	nd	nd

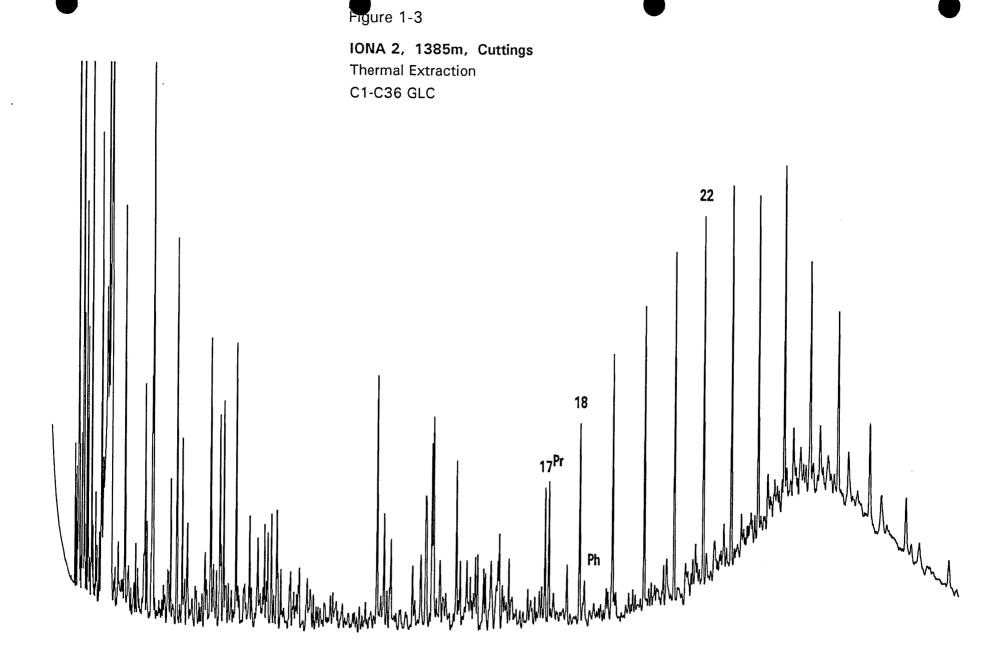
Mar-94

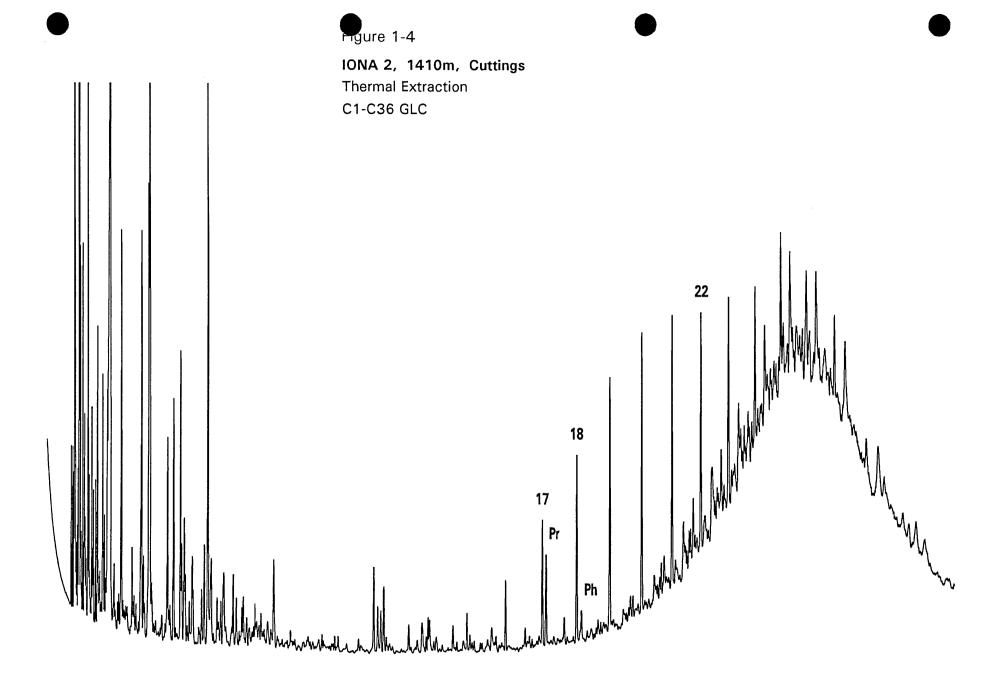
Figure 1-1 IONA 2, 1358.0m, SWC

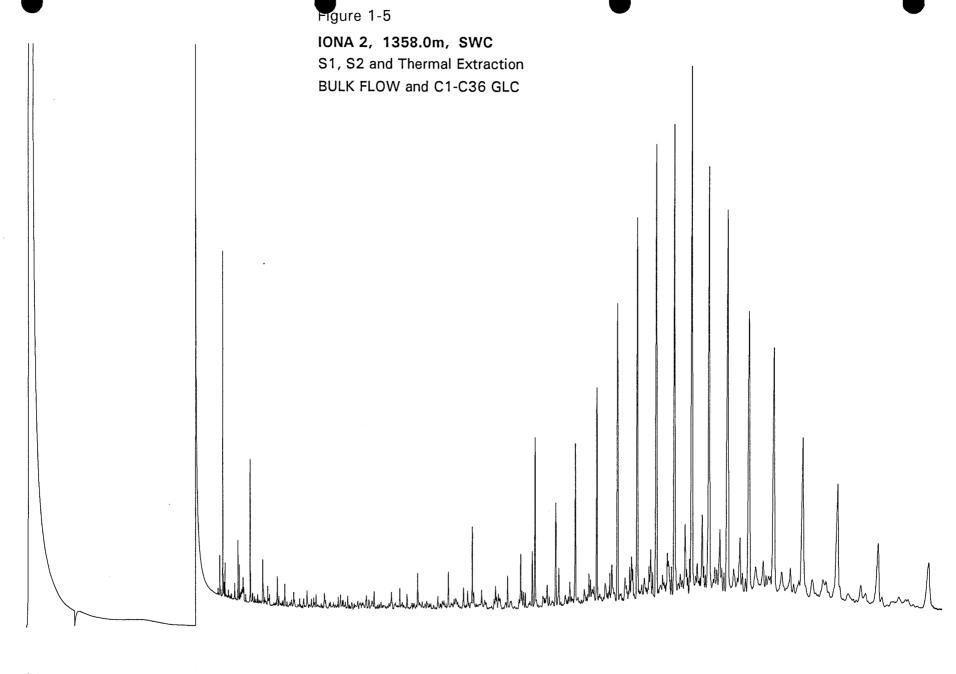
Thermal Extraction
C1-C36 GLC

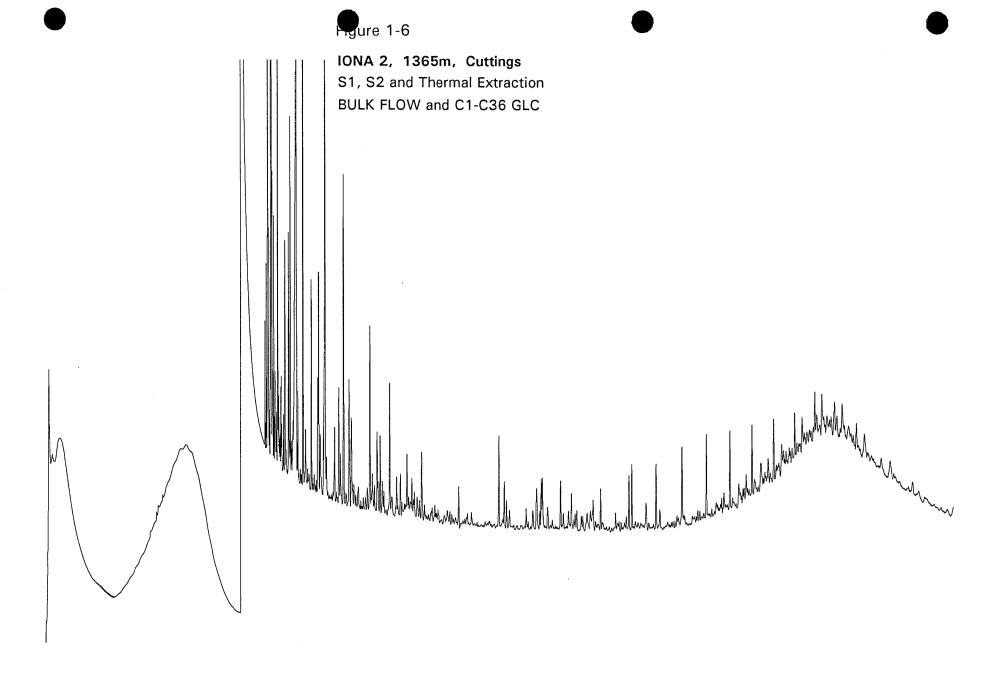


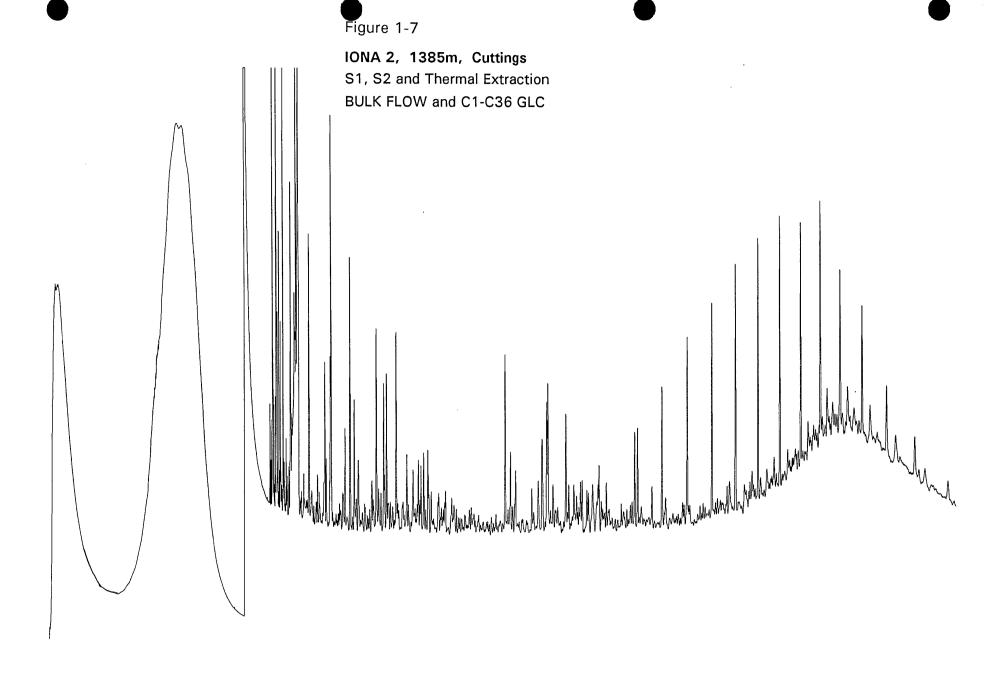












S1

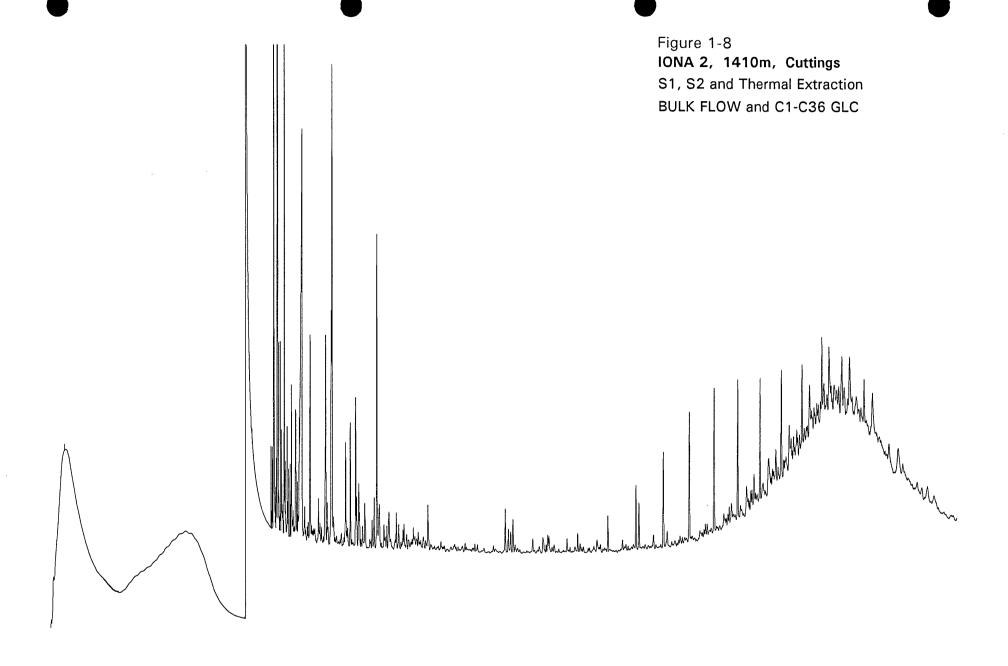


TABLE 3

#### Summary of Extraction and Liquid Chromatography

IONA 2 Mar-94

#### A. Concentrations of Extracted Material

				Hyd	rocarbons-		Non	Nonhydrocar		
	Weight of	Total	Loss on			HC			NonHC	
	Rock Extd	Extract	Column	Saturates	Aromatics	Total	NSO's	Asphalt	Total	
DEPTH(m)	(grams)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	(ppm)	
1358.0	11.7	10724.0	1382.4	7121.4	1591.8	8713.3	628.4	nd	628.4	
362.0	10.8	6849.4	1384.8	4070.6	1040.9	5111.5	353.2	nd	353.2	
1381.0	11.6	5636.4	484.8	3818.2	926.4	4744.6	406.9	nd	406.9	
1392.0	13.0	69.4	nd	nd	nd	nd	nd	nd	nd	
1408.5	12.2	1414.5	82.2	1019.7	189.1	1208.9	123.4	nd	123.4	
1426.0	14.0	143.3	nd	nd	nd	nd	nd	nd	nd	
1469.0	14.6	41.2	nd	nd	nd	nd	nd	nd	nd	
1550.5	16.0	31.3	nd	nd	nd	nd	nd	nd	nd	

TABLE 3

#### Summary of Extraction and Liquid Chromatography

ICHA 2 Mar-94

#### B. Compositional Data

	H	ydrocarbo	ns	Nonhydrocarbons E		EOM(mg)	SAT(mg)	SAT	ASPH	HC	
DEPTH(m)	%SAT	%AROM	%HC's	%NSO	%ASPH	%Non HC's	TOC(g)	TOC(g)	AROM	NSO	Non HC
1358.0	76.2	17.0	93.3	6.7	nd	6.7	nd	nd	4.5	nd	13.9
1362.0	74.5	19.0	93.5	6.5	nd	6.5	nd	nd	3.9	nd	14.5
1381.0	74.1	18.0	92.1	7.9	nd	7.9	nd	nd	4.1	nd	11.7
1392.0	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd
1408.5	76.5	14.2	90.7	9.3	nd	9.3	nd	nd	5.4	nd	9.8
1426.0	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd
1469.0	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd
1550.5	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd

TABLE 4

#### IONA 2

#### Summary of Gas Chromatography Data

#### A. Alkane Compositional Data

DEPTH(m)	Prist./Phyt.	Prist./n-C17	Phyt./n-C18	CPI(1)	CPI(2)	(C21 + C22)/(C28 + C29)
_1358.0	5.37	2.86	0.37	1.11	1.10	1.40
362.0	5.39	3.02	0.38	1.10	1.09	1.49
1381.0	4.81	1.17	0.15	1.08	1.07	2.22
1392.0	nd	nd	nd	nd	nd	nd
1408.5	5.12	0.37	0.07	1.07	1.08	2.71
1426.0	4.73	0.34	0.07	1.07	1.07	2.78
1469.0	nd	nd	nd	nđ	nd	nd
1550.5	nd	nd	nd	nd	nd	nd

#### TABLE 4



#### Summary of Gas Chromatography Data

#### B. n-Alkane Distributions

DEPTH(m)	nC12	nC13	nC14	nC15	nC16	nC17	iC19	nC18	iC20	nC19	nC20	nC21	nC22	nC23	nC24	nC25	nC26	nC27	nC28	nC29	nC30	nC31	
1358.0	-	-	-	1.1	1.5	2.2	6.4	3.3	1.2	4.1	5.1	6.4	8.2	9.6	9.0	9.8	7.7	7.3	5.5	5.0	3.5	3.1	
1362.0	-	-	-	1.1	1.4	2.1	6.4	3.2	1.2	4.0	5.1	6.6	8.3	9.8	9.6	10.0	7.7	7.1	5.2	4.8	3.2	2.8	
1381.0	-	-	-	8.0	1.8	3.6	4.2	5.7	0.9	7.4	8.0	8.5	8.8	9.3	8.6	8.2	6.0	5.4	4.1	3.7	2.6	2.3	
1392.0	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	
1408.5	4.2	4.8	5.4	5.9	6.1	6.4	2.4	6.6	0.5	6.8	6.5	6.3	6.3	6.3	5.6	5.2	3.8	3.4	2.5	2.2	1.7	1.3	
1426.0	3.5	4.1	4.9	5.9	6.4	6.8	2.3	7.0	0.5	7.0	6.8	6.6	6.4	6.3	5.6	5.2	3.8	3.5	2.6	2.1	1.5	1.4	
1469.0	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	
1550.5	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	

Figure 2-1 IONA 2, 1358.0m, SWC Saturate Fraction C12+ GLC

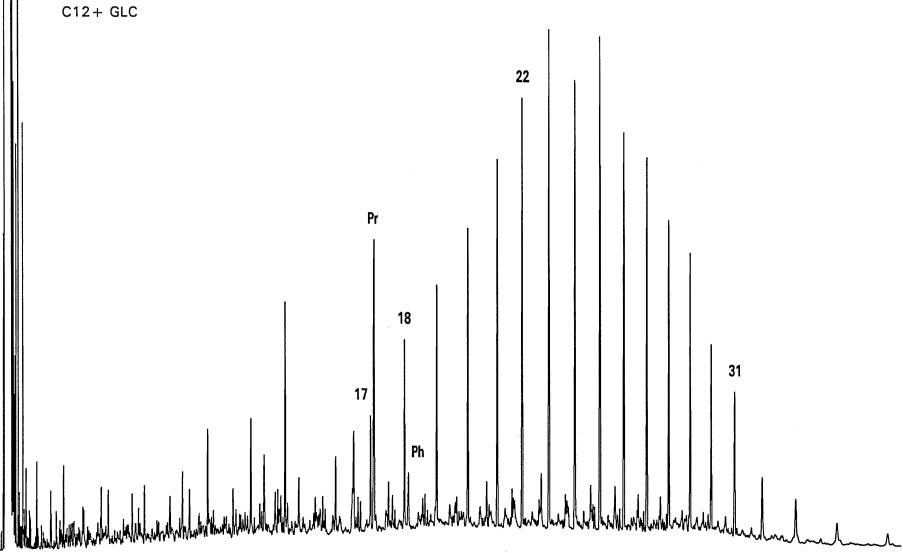


Figure 2-2
IONA 2, 1362.0m, SWC
Saturate Fraction
C12+ GLC

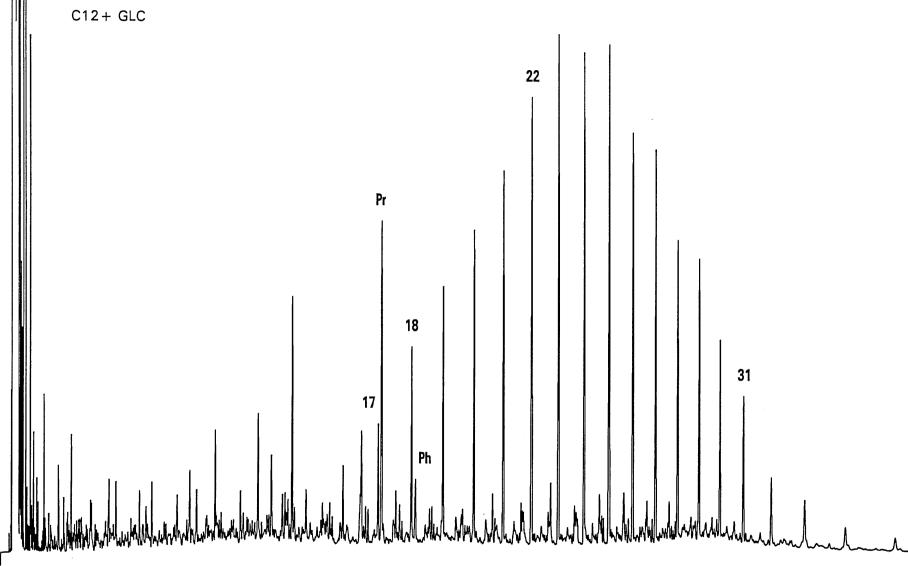


Figure 2-3
IONA 2, 1381.0m, SWC
Saturate Fraction
C12 + GLC

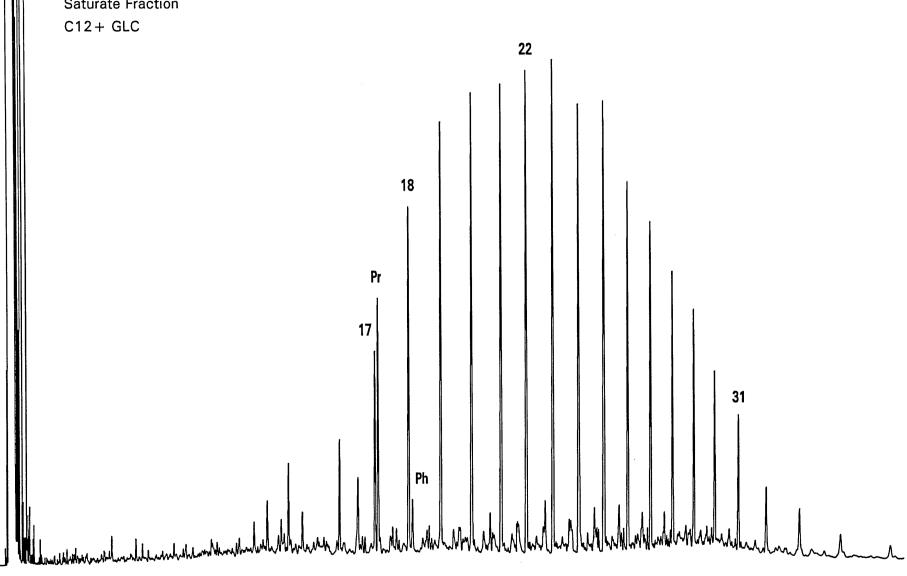
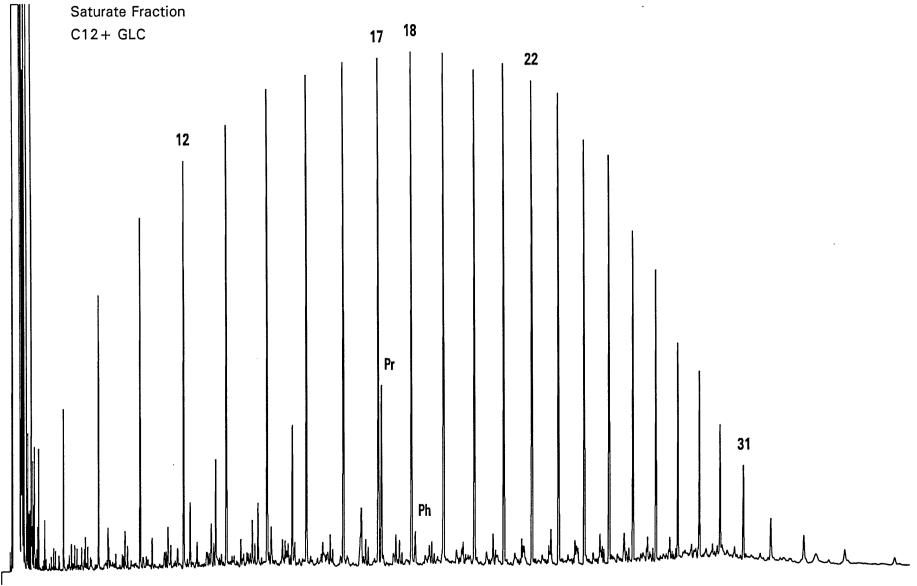


Figure 2-4 IONA 2, 1392.0m, SWC Whole Extract C12+ GLC

Figure 2-5
IONA 2, 1408.5m, SWC
Saturate Fraction



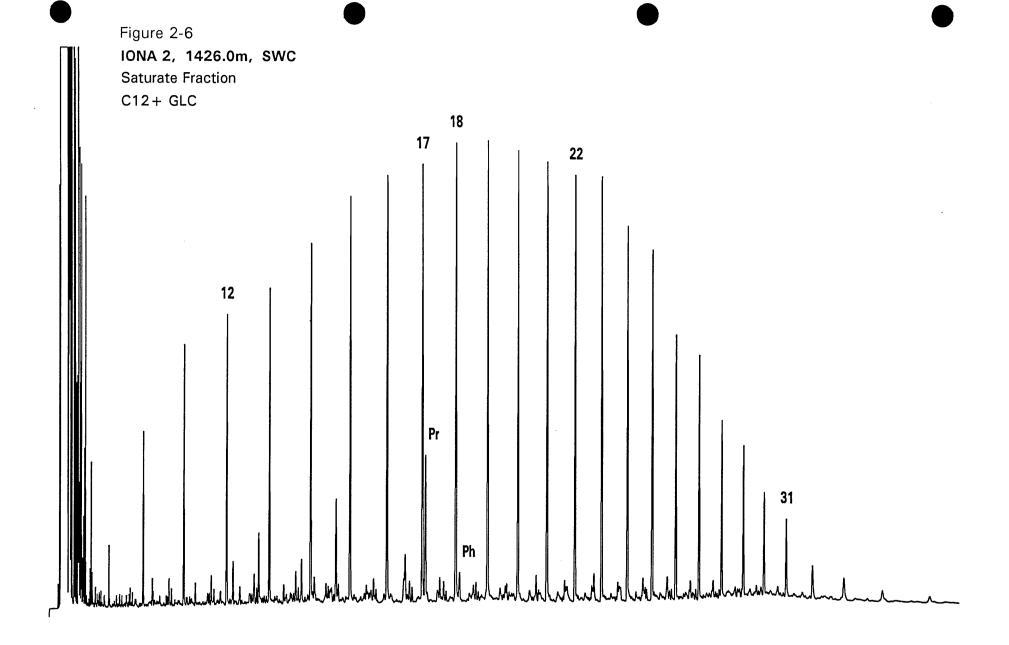


Figure 2-7 IONA 2, 1469.0m, SWC Whole Extract C12+ GLC 18_{Ph} 12

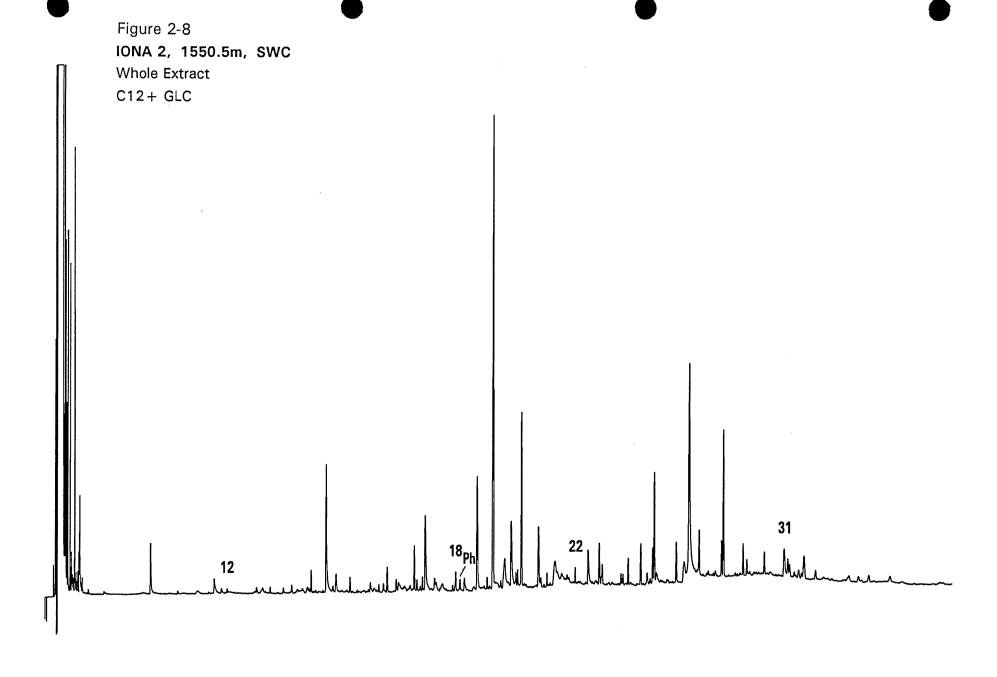


Table 3

		Sum	mary of Extr	action and Liqu	ula Chroma	atograpny	<b>,</b>		
IONA 1				•					Mar-94
A. Concentratio	ns of Extrac	ted Mate	erial						
				Hydr	ocarbons		Non	hydrocar	bons
	Weight of	Total	Loss on			HC			NonHC
	Rock Extd	Extract	Column	Saturates A	Aromatics	Total	NSO's	Asphalt	Total
DEPTH(m)	(grams)	(ppm)	(ppm) 295.7	(ppm) 1530 4	(ppm)	(ppm)	(ppm) 434.8	(ppm)	(ppm) 434.8

Table 3

#### Summary of Extraction and Liquid Chromatography

IONA 1										Mar-94			
B. Compositional Data													
	H	ydrocarbo	ns	Nonh	ydrocarb	ons	EOM(mg)	SAT(mg)	SAT	ASPH	НС		
DEPTH(m)	%SAT	%AROM	%HC's	%NSO	%ASPH	%Non HC's	TOC(g)	TOC(g)	AROM	NSO	Non HC		
1391.5	71.0	8.9	79.8	20.2	nd	20.2	nd	nd	8.0	nd	4.0		

Table 4

IONA 1

Summary of Gas Chromatography Data

A. Alkane Compositional Data

DEPTH(m) 1391.5

Prist./Phyt. 2.80

Prist./n-C17 0.53

Phyt./n-C18 0.08

CPI(1) 1.07

CPI(2) (C21 + C22)/(C28 + C29) 1.07

2.54

Table 4

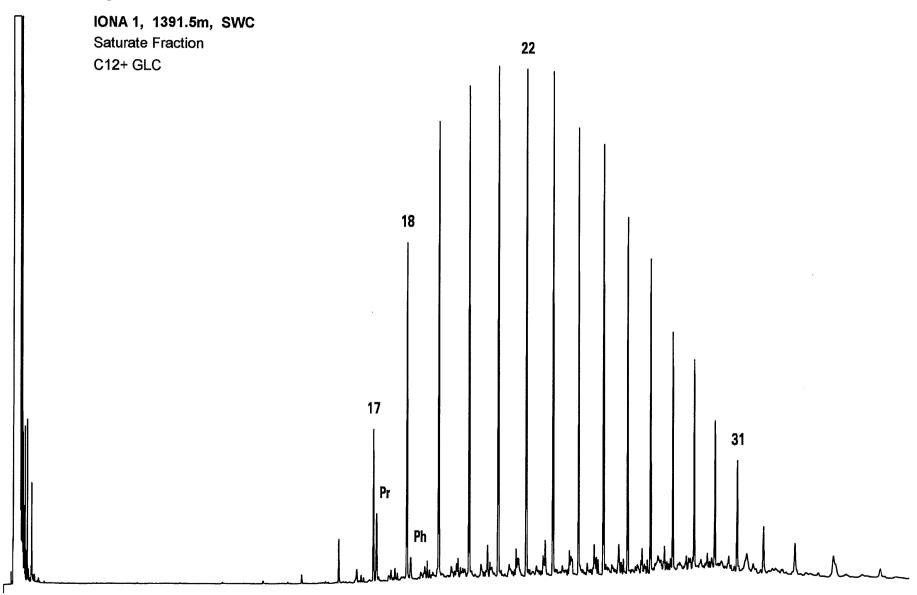
IONA 1

Summary of Gas Chromatography Data

B. n-Alkane Distributions

DEPTH(m) nC12 nC13 nC14 nC15 nC16 nC17 iC19 nC18 iC20 nC19 nC20 nC21 nC22 nC23 nC24 nC25 nC26 nC27 nC28 nC29 nC30 nC31 - - 0.1 0.7 2.6 1.4 5.9 0.5 8.6 9.3 9.6 9.8 9.9 8.9 8.4 6.3 5.6 4.1 3.5 2.6 2.2

Figure 2-9



#### SELECTED PARAMETERS FROM GC/MS ANALYSIS

#### IONA 2, 1358.0m, SWC

	<u>Parameter</u>	<u>lon(s)</u>	<u>Value</u>
1.	18 $\alpha$ (H)- hopane/17 $\alpha$ (H)-hopane (Ts/Tm)	191	0.81
2.	C30 hopane/C30 moretane	191	8.76
3.	C31 22S hopane/C31 22R hopane	191	1.39
4.	C32 22S hopane/C32 22R hopane	191	1.43
5.	C29 20S $\alpha\alpha\alpha$ sterane/C29 20R $\alpha\alpha\alpha$ sterane	217	0.94
6.	C29 $\alpha\alpha\alpha$ steranes (20S / 20S+20R)	217	0.49
7.	C29 $\alpha\beta\beta$ steranes	217	0.58
	C29 $\alpha\alpha\alpha$ steranes + C29 $\alpha\beta\beta$ steranes		
8.	C27/C29 diasteranes	259	nd
9.	C27/C29 steranes	217	0.24
10.	18 $\alpha$ (H)-oleanane/C30 hopane	191	nd
11.	C29 diasteranes	217	0.40
	C29 $\alpha\alpha\alpha$ steranes + C29 $\alpha\beta\beta$ steranes		0.40
12.	C30 (hopane + moretane)	191/217	0.04
	C29 (steranes + diasteranes)		0.94
13.	C15 drimane/C16 homodrimane	123	0.92
14.	Rearranged drimanes/normal drimanes	123	1.05

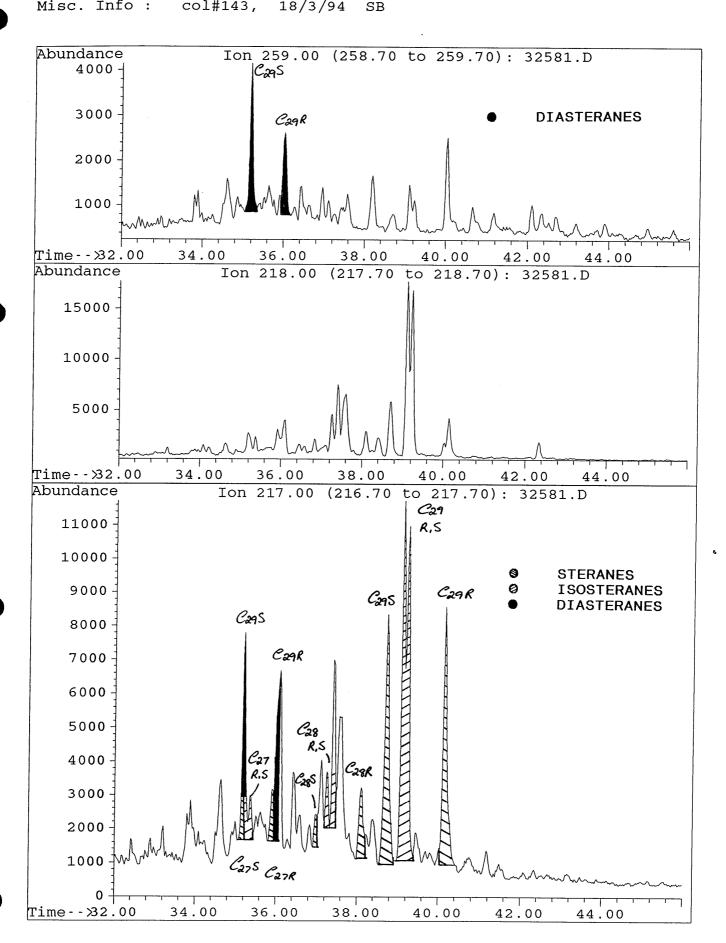
nd = not detectable

Figure 3-1

File :

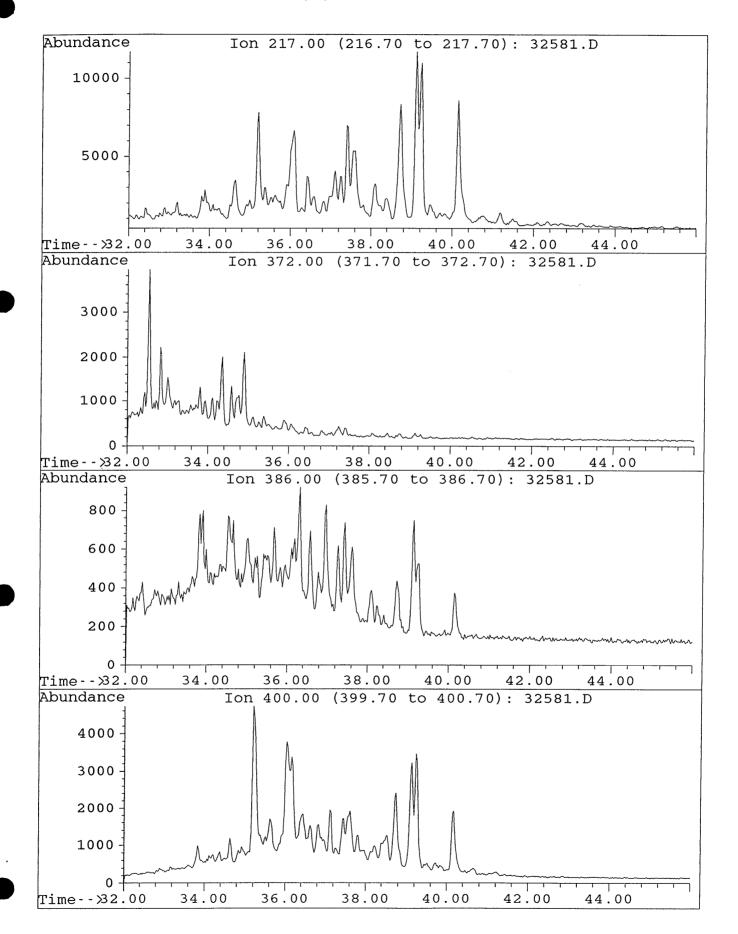
32581.D

Sample: IONA-2 1358.0m Misc. Info: col#143, 18/3/94

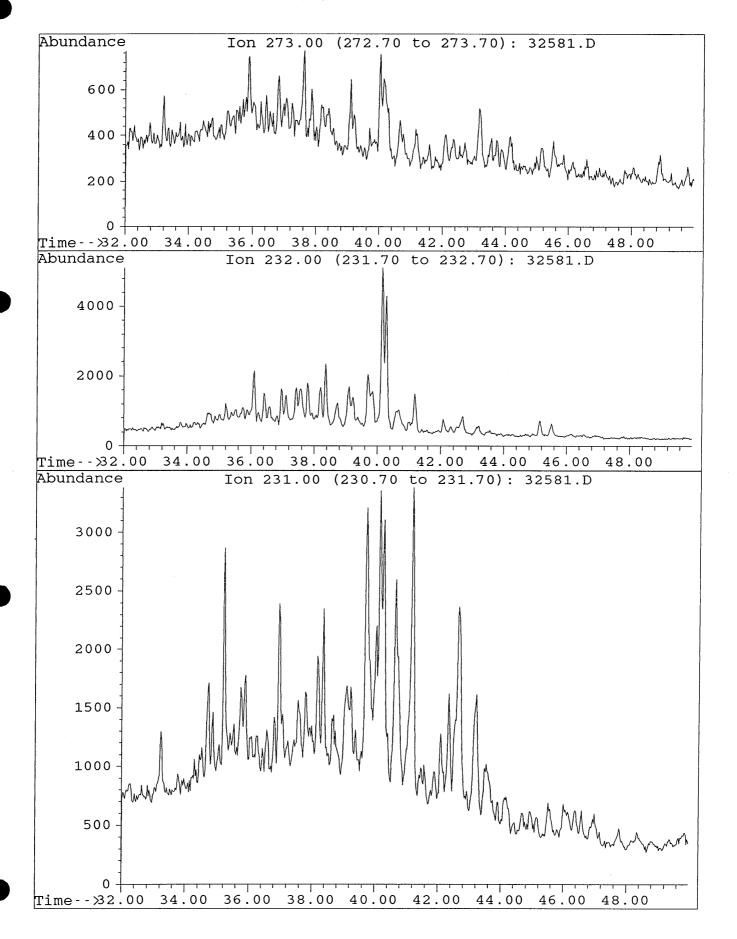


B/C

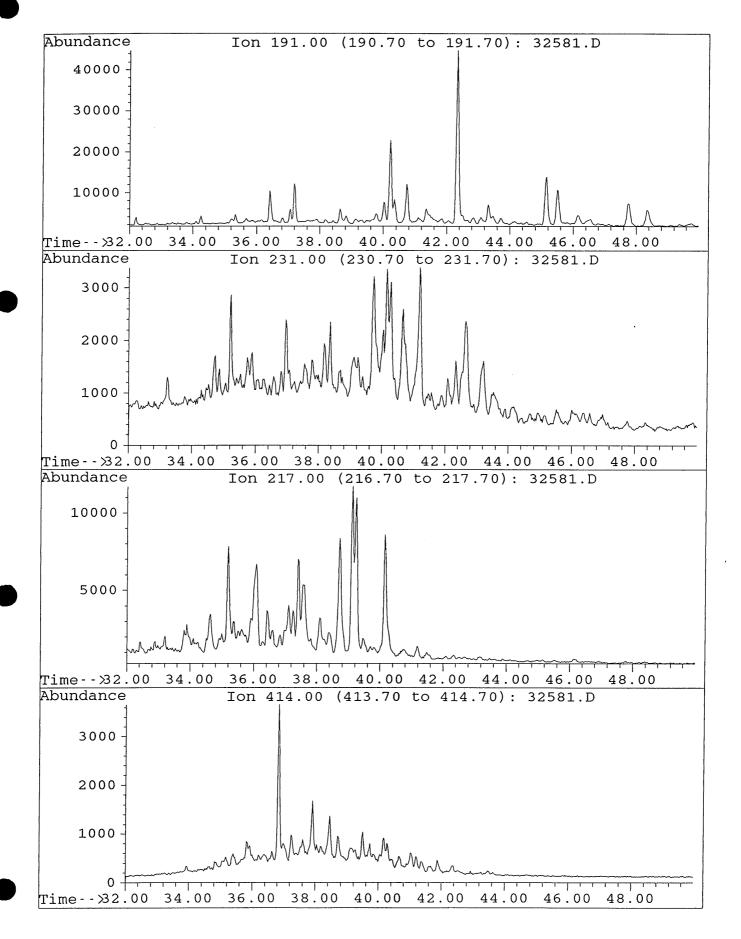
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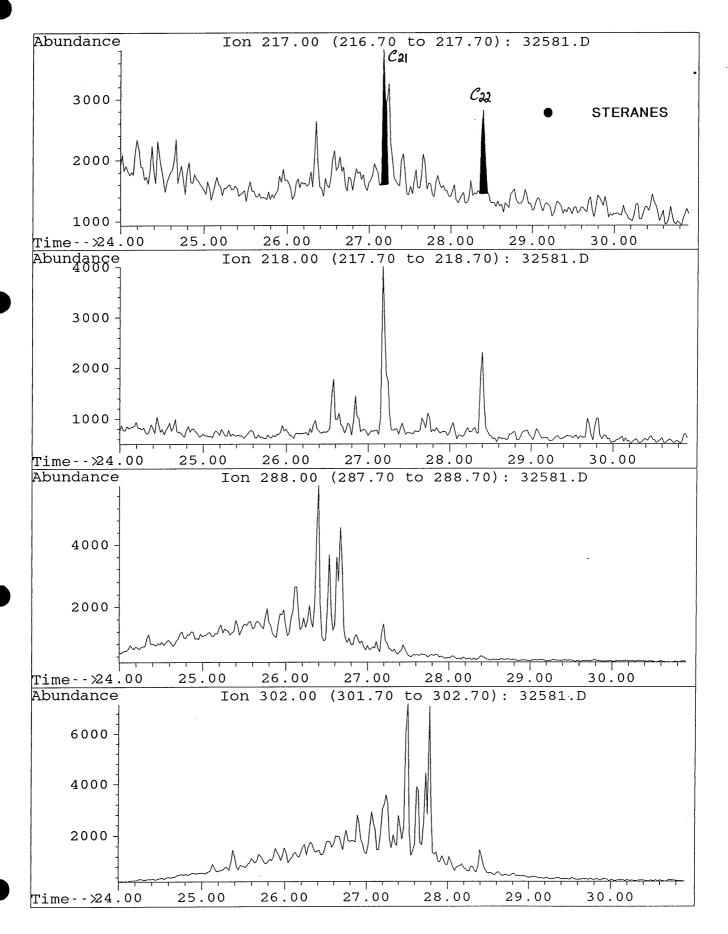
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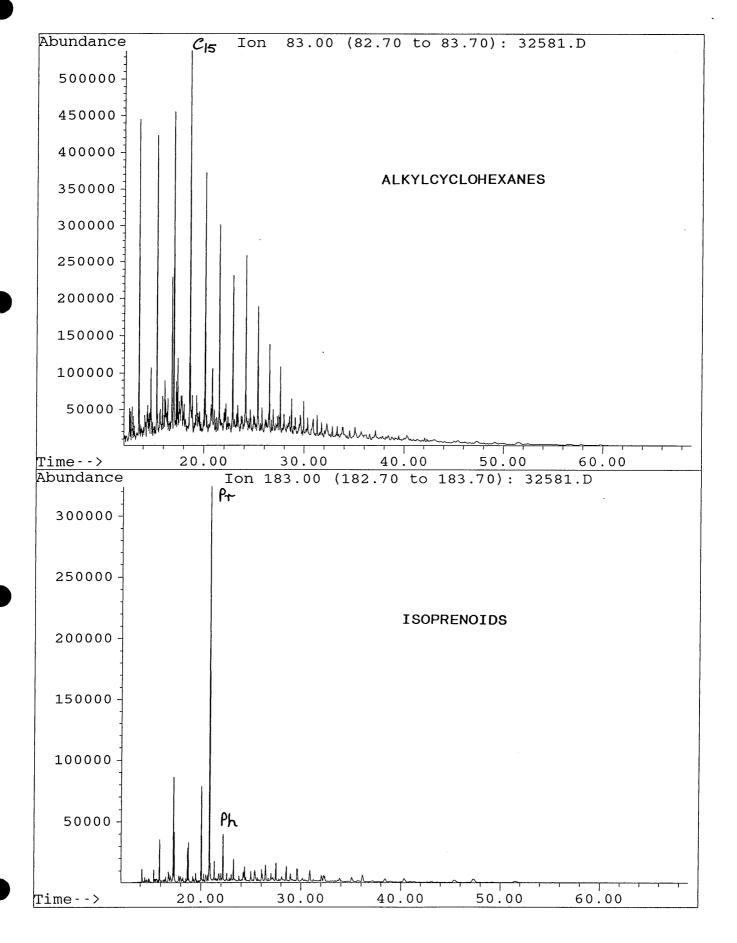
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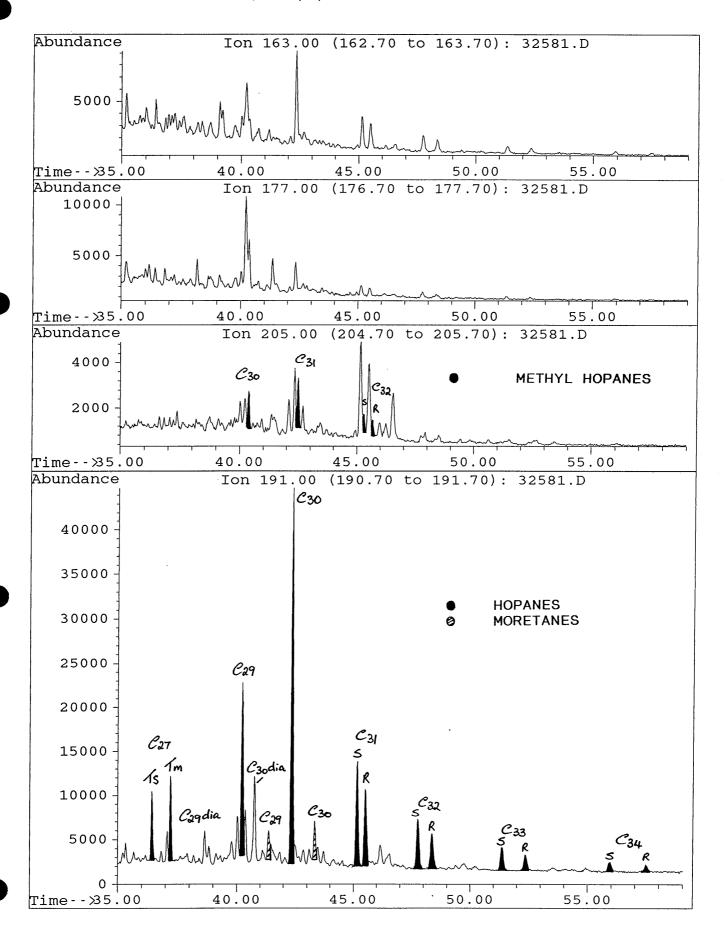
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32581.D



File: 32581.D



32581.D

Sample : Misc. Info :

IONA-2 1358.0m B/C col#143, 18/3/94 SB

Abundance Ion 259.00 (258.70 to 259.70): 32581.D 4000 -3000 2000 1000 Time-->35.00 45.00 50.00 55.00 Abundance Ion 191.00 (190.70 to 191.70): 32581.D 40000 -30000 20000 10000 Time - - >35.00 40.00 45.00 50.00 55.00 Abundance Ion 370.00 (369.70 to 370.70): 32581.D 2000 -1000 Time-->35.00 40.00 45.00 50.00 55.00 Abundance Ion 398.00 (397.70 to 398.70): 32581.D 4000 -2000 -40.00 Time-->35.00 45.00 50.00 55.00 Abundance Ion 412.00 (411.70 to 412.70): 32581.D 4000 -2000 -Time-->35.00 40.00 45.00 50.00 55.00

32581.D

Sample : Misc. Info :

Time-->20.00

22.00

IONA-2 1358.0m B/C col#143, 18/3/94 SB

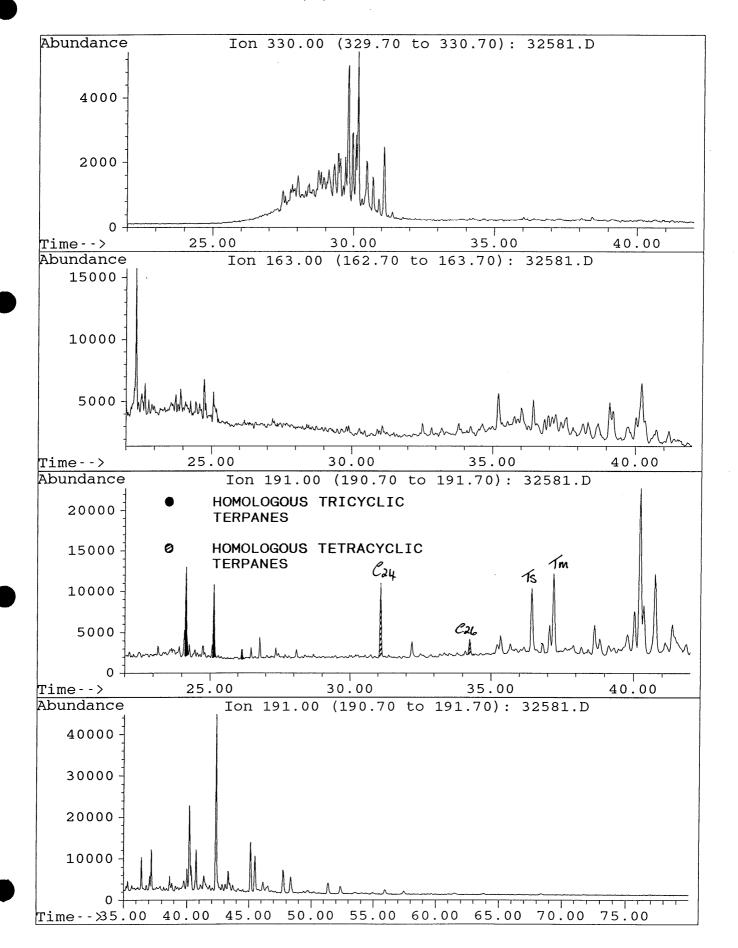
Abundance Ion 259.00 (258.70 to 259.70): 32581.D 6000 4000 2000 Time - ->20.00 22.00 24.00 26.00 28.00 Abundance Ion 274.00 (273.70 to 274.70): 32581.D 8000 -6000 4000 2000 22.00 Time - ->20.00 24.00 26.00 28.00 Abundance Ion 123.00 (122.70 to 123.70): 32581.D 25000 CaoL **ISOPIMARANES** 0 **BEYERANE** 0 17-NORTETRACYCLANE 17-NOR 17-NOR **LABDANES** 20000 CIBL 15000 10000 5000

24.00

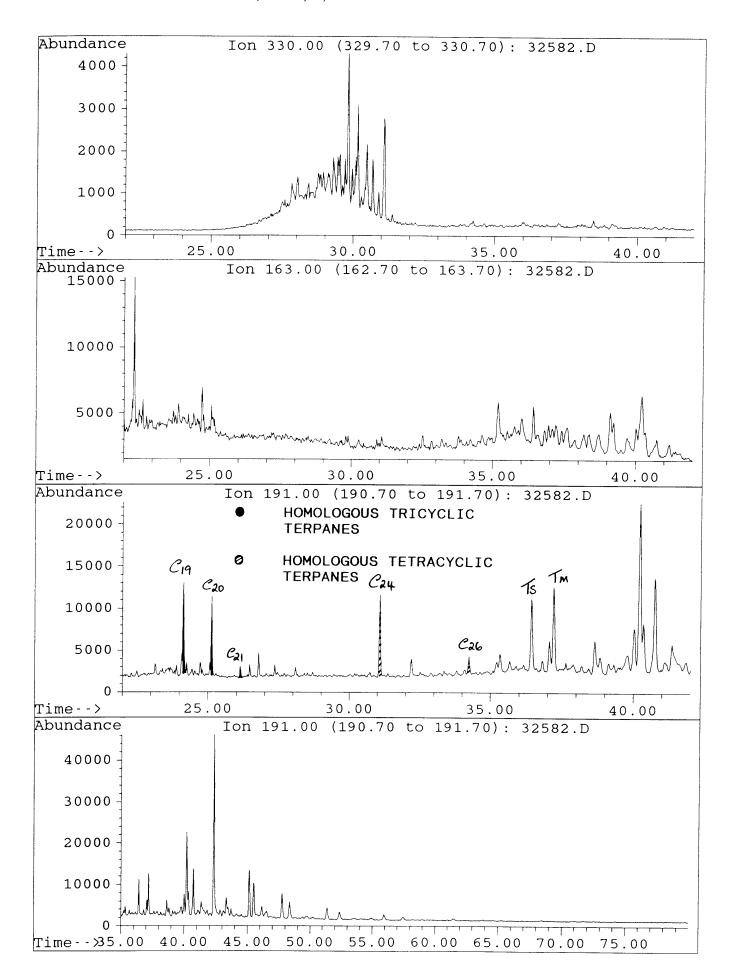
26.00

28.00

File: 32581.D



32582.D

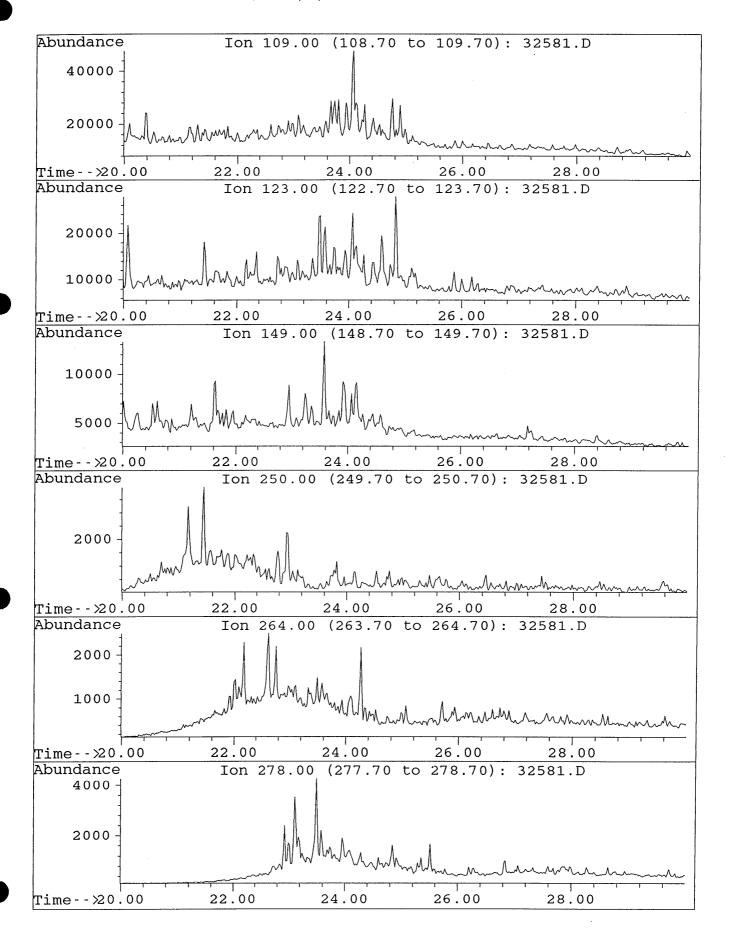


32581.D

Sample : Misc. Info : IONA-2 1358.0m B/C col#143, 18/3/94 SB

Abundance Ion 193.00 (192.70 to 193.70): 32581.D 400000 200000 15.00 17.00 Time - - >14.00 16.00 18.00 19.00 20.00 Abundance Ion 165.00 (164.70 to 165.70): 32581.D 60000 -40000 -20000 -15.00 Time - - >14.00 16.00 17.00 18.00 19.00 20.00 Abundance Ion 123.00 (122.70 to 123.70): 32581.D 220000 -C15 **DRIMANES** REARRANGED DRIMANES 200000 C16 180000 -C15 160000 -140000 -C15 120000 100000 80000 60000 40000 20000 0 Time-->14.00 15.00 16.00 17.00 18.00 19.00 20.00

32581.D



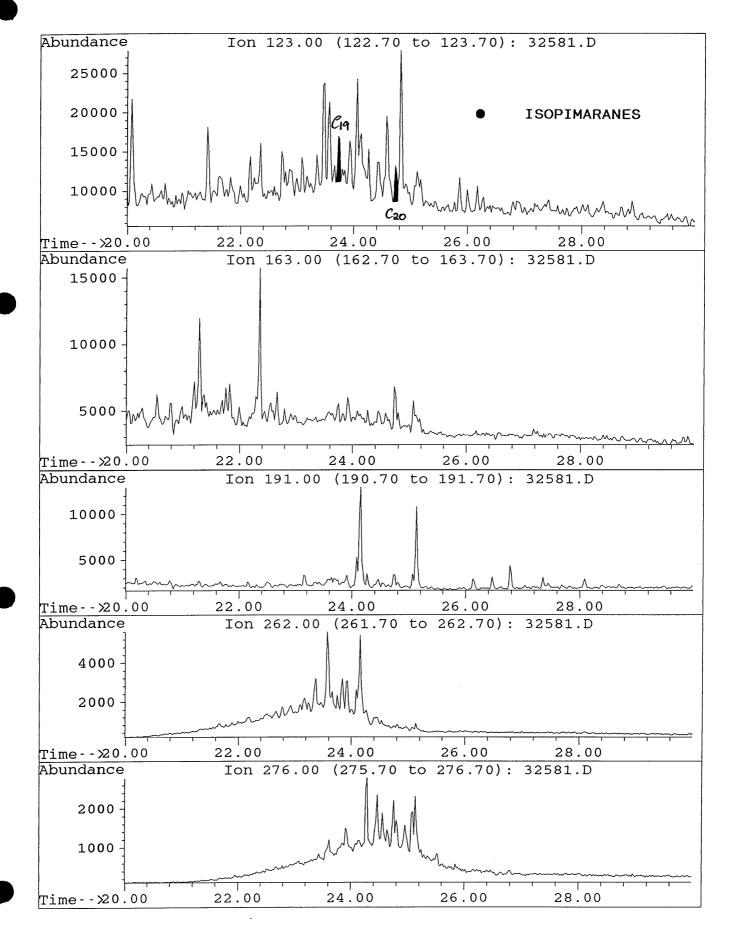
32581.D

Sample : Misc. Info :

IONA-2 1358.0m B/C col#143, 18/3/94 SB

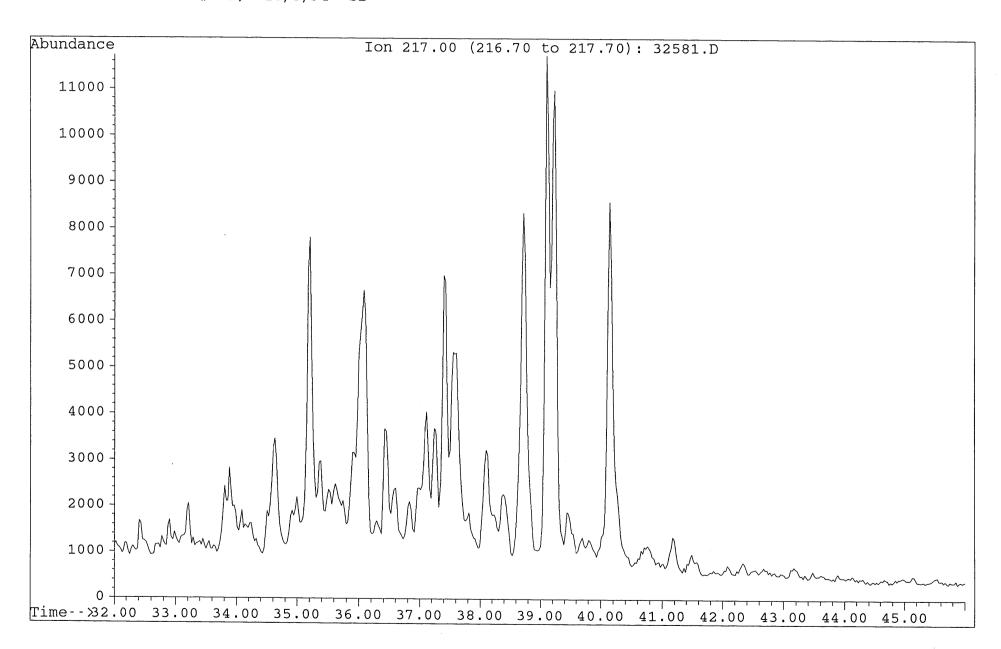
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32581.D



Fle:

32581.D



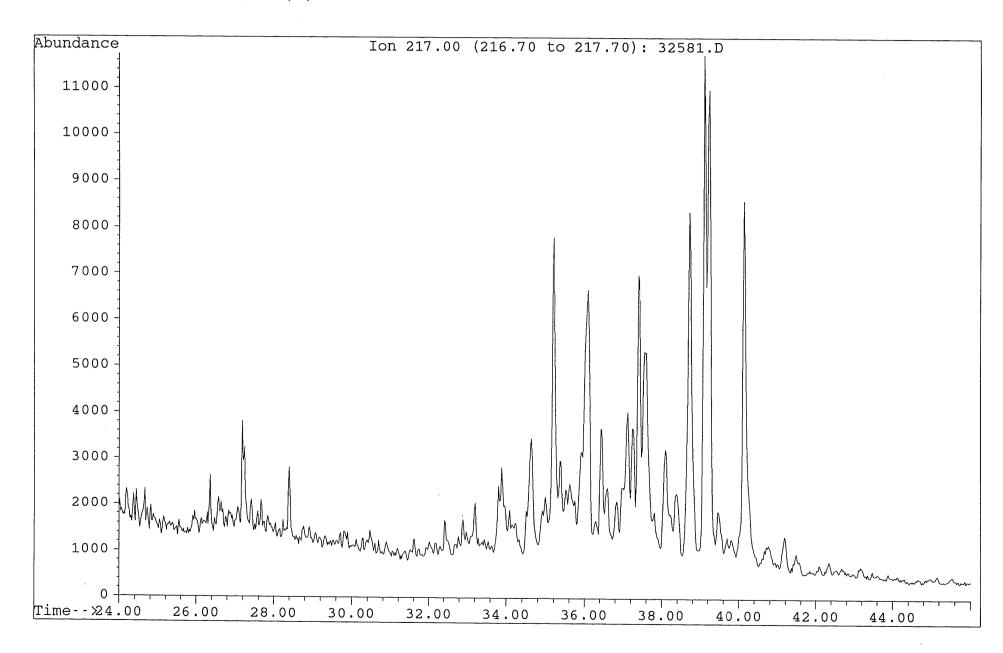
æ:

32581.D

IONA-2 1358.0m B/C

Sample : Misc. Info :

col#143, 18/3/94 SB



Fe :

32581.D

Sample : Misc. Info : IONA-2 1358.0m B/C col#143, 18/3/94 SB

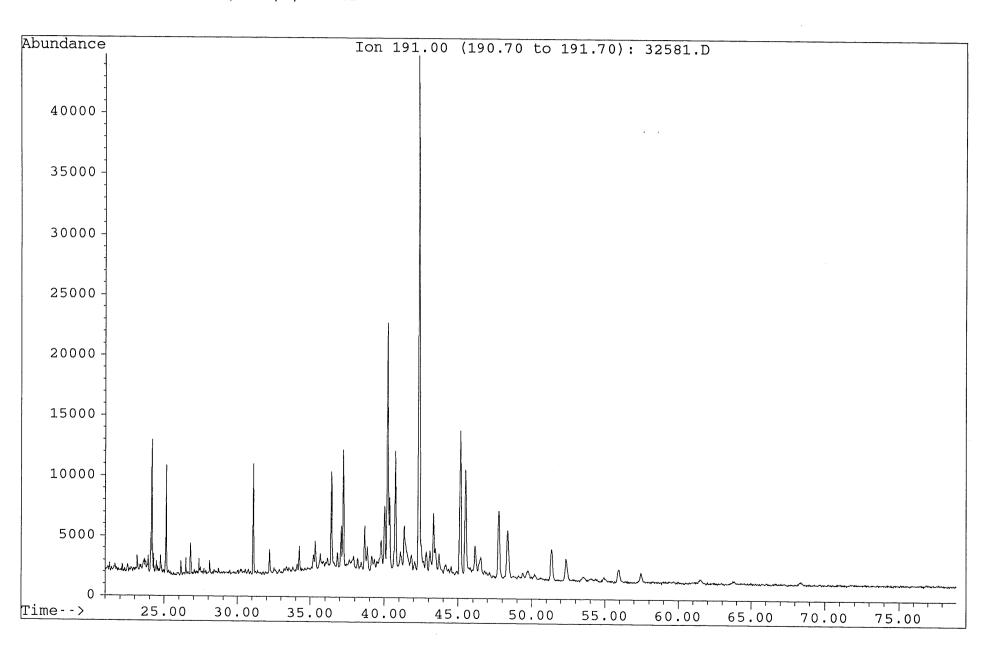
Abundance Ion 191.00 (190.70 to 191.70): 32581.D 40000 35000 30000 25000 20000 15000 -10000 5000 0 -60.00 65.00 70.00 Time-->35.00 75.00 40.00 45.00 50.00 55.00

32581.D

IONA-2 1358.0m

Sample : Misc. Info :

col#143, 18/3/94 SB



## SELECTED PARAMETERS FROM GC/MS ANALYSIS

## IONA 2, 1408.5m, SWC

	<u>Parameter</u>	<u>lon(s)</u>	<u>Value</u>
1.	18 $\alpha$ (H)- hopane/17 $\alpha$ (H)-hopane (Ts/Tm)	191	0.85
2.	C30 hopane/C30 moretane	191	9.81
3.	C31 22S hopane/C31 22R hopane	191	1.39
4.	C32 22S hopane/C32 22R hopane	191	1.49
5.	C29 20S $\alpha\alpha\alpha$ sterane/C29 20R $\alpha\alpha\alpha$ sterane	217	0.95
6.	C29 $\alpha\alpha\alpha$ steranes (20S / 20S + 20R)	217	0.49
7.	C29 $\alpha\beta\beta$ steranes  C29 $\alpha\alpha\alpha$ steranes + C29 $\alpha\beta\beta$ steranes	217	0.58
8.	C27/C29 diasteranes	259	nd
9.	C27/C29 steranes	217	0.23
10.	18 $\alpha$ (H)-oleanane/C30 hopane	191	nd
11.	C29 diasteranes  C29 $\alpha\alpha\alpha$ steranes + C29 $\alpha\beta\beta$ steranes	217	0.35
12.	C30 (hopane + moretane)C29 (steranes + diasteranes)	191/217	0.94
13.	C15 drimane/C16 homodrimane	123	0.89
14.	Rearranged drimanes/normal drimanes	123	0.87

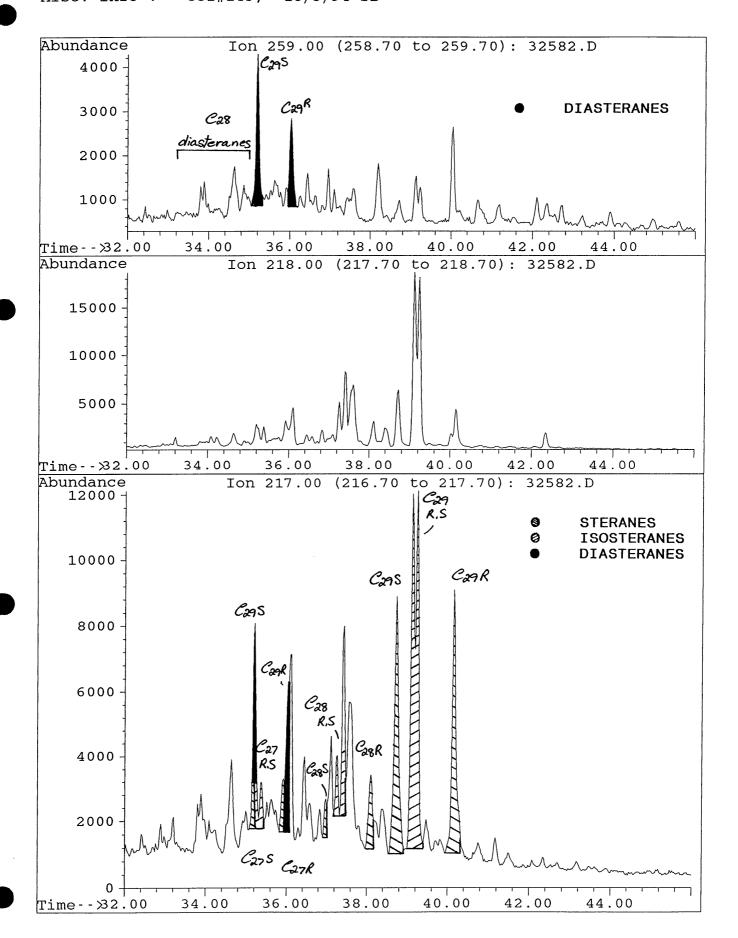
nd = not detectable

Figure 3-2

File :

32582.D

Sample : Misc. Info : IONA-2 1408.5m B/C col#143, 18/3/94 SB



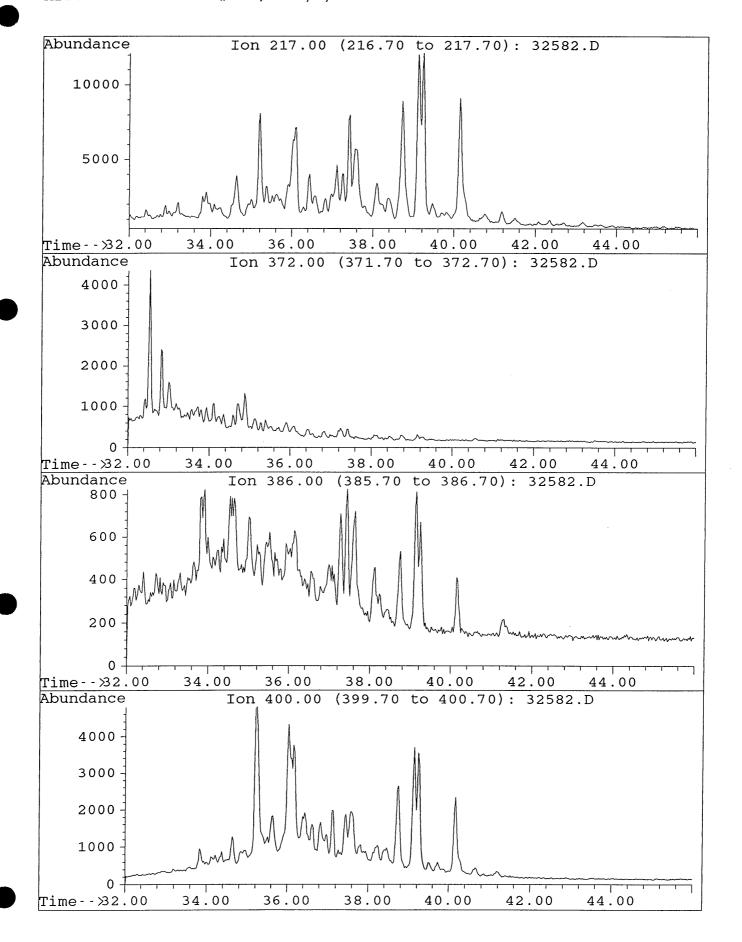
32582.D

Sample :

IONA-2 1408.5m B/C

Misc. Info :

col#143, 18/3/94 SB



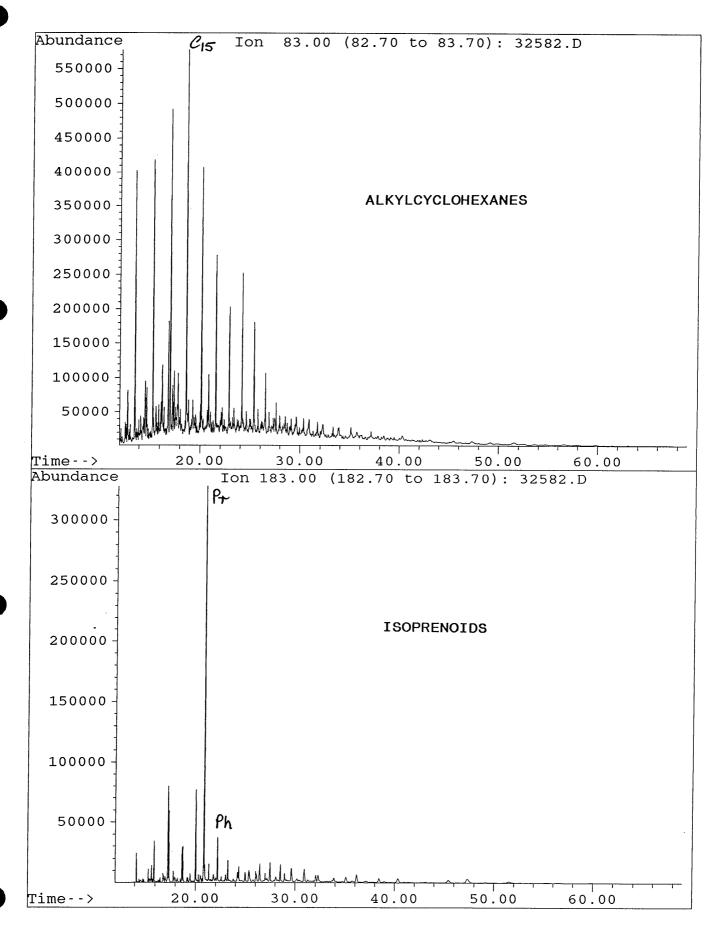
32582.D

Sample :
Misc. Info :

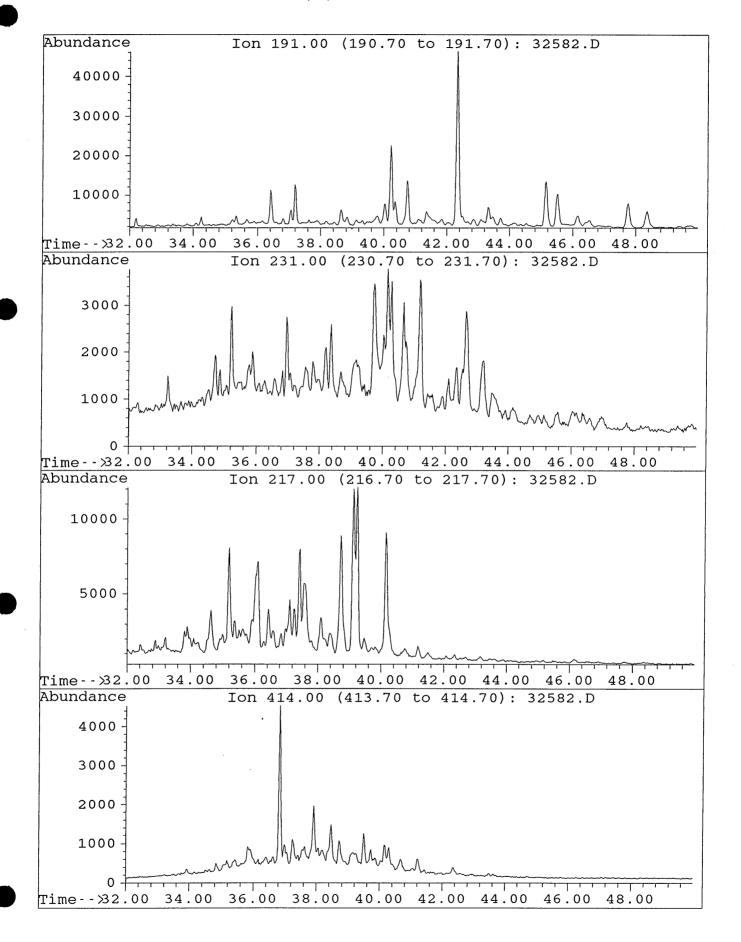
IONA-2 1408.5m B/C col#143, 18/3/94 SB

Abundance Ion 273.00 (272.70 to 273.70): 32582.D 800 600 200 0 -Time-->32.00 34.00 48.00 36.00 38.00 40.00 42.00 44.00 46.00 Abundance Ion 232.00 (231.70 to 232.70): 32582.D 4000 2000 0 48.00 36.00 Time-->32.00 34.00 38.00 40.00 42.00 44.00 46.00 Ion 231.00 (230.70 to 231.70): 32582.D Abundance 3500 3000 2500 2000 1500 1000 500 0 Time-->32.00 34.00 36.00 38.00 40.00 42.00 44.00 46.00

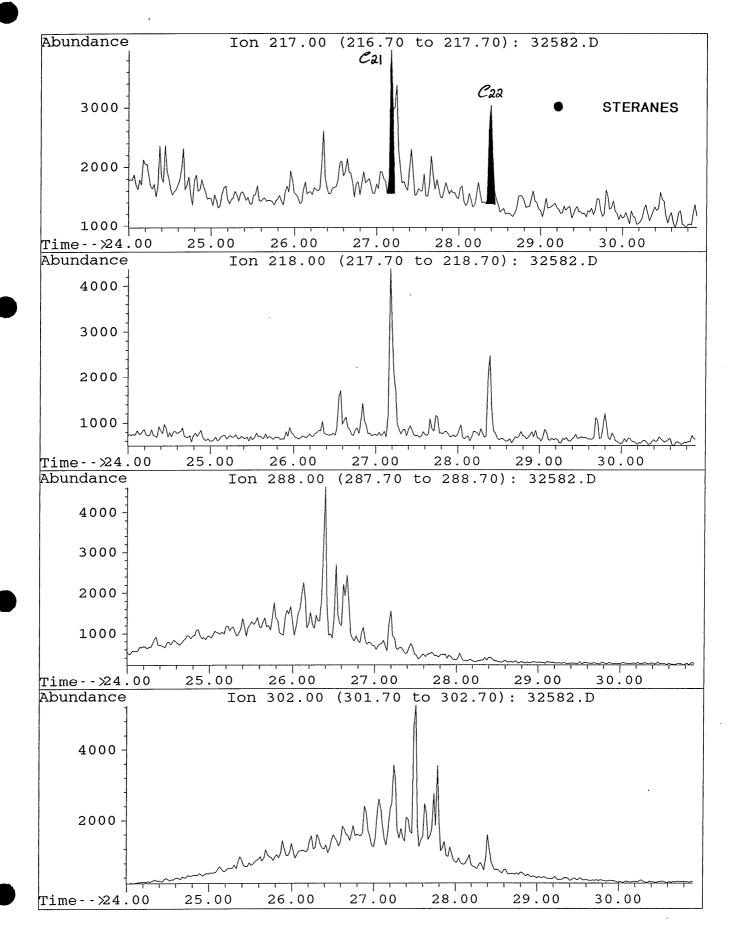
File: 32582.D



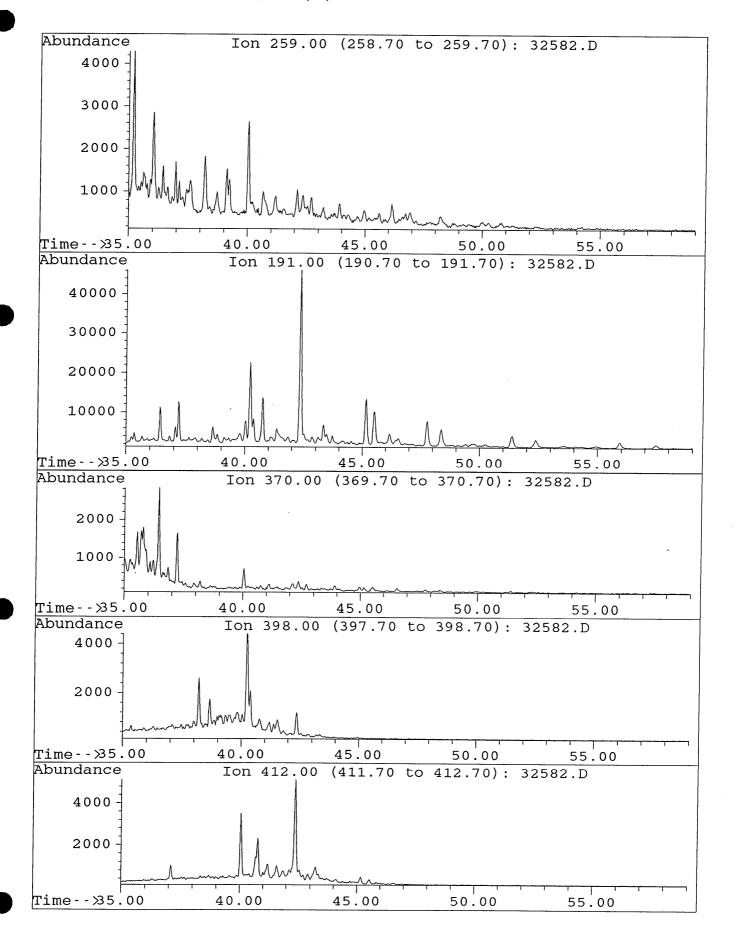
32582.D



32582.D

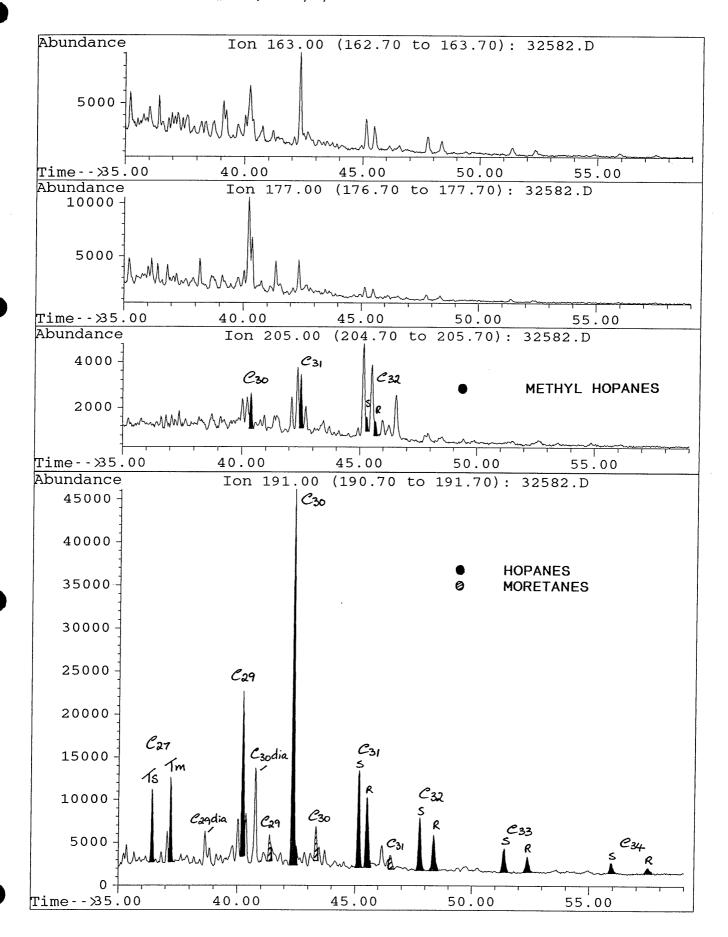


32582.D



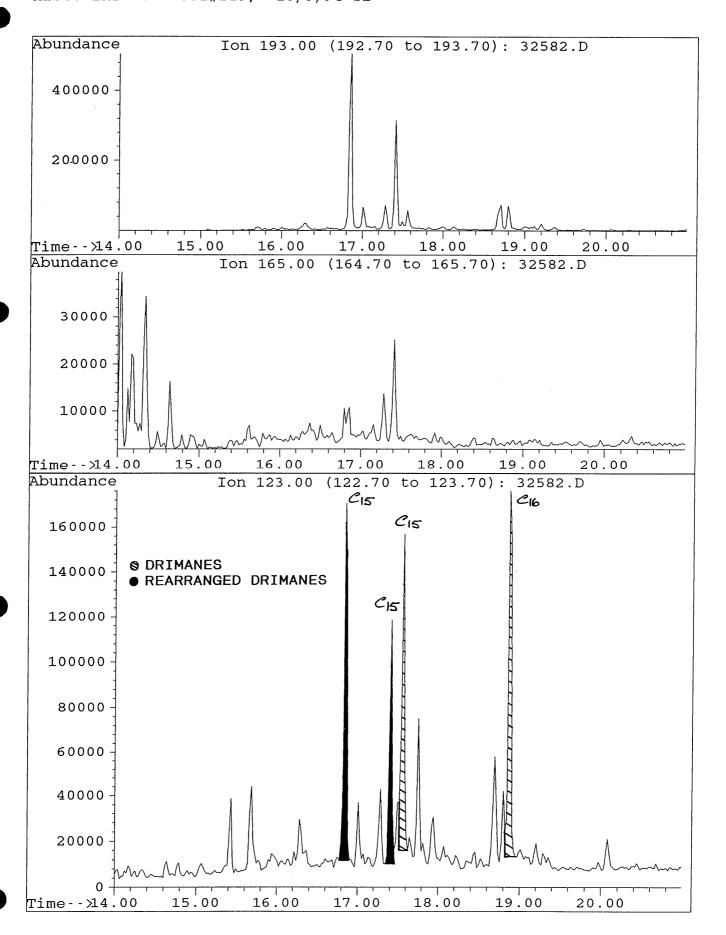
32582.D

Sample : Misc. Info : IONA-2 1408.5m B/C col#143, 18/3/94 SB

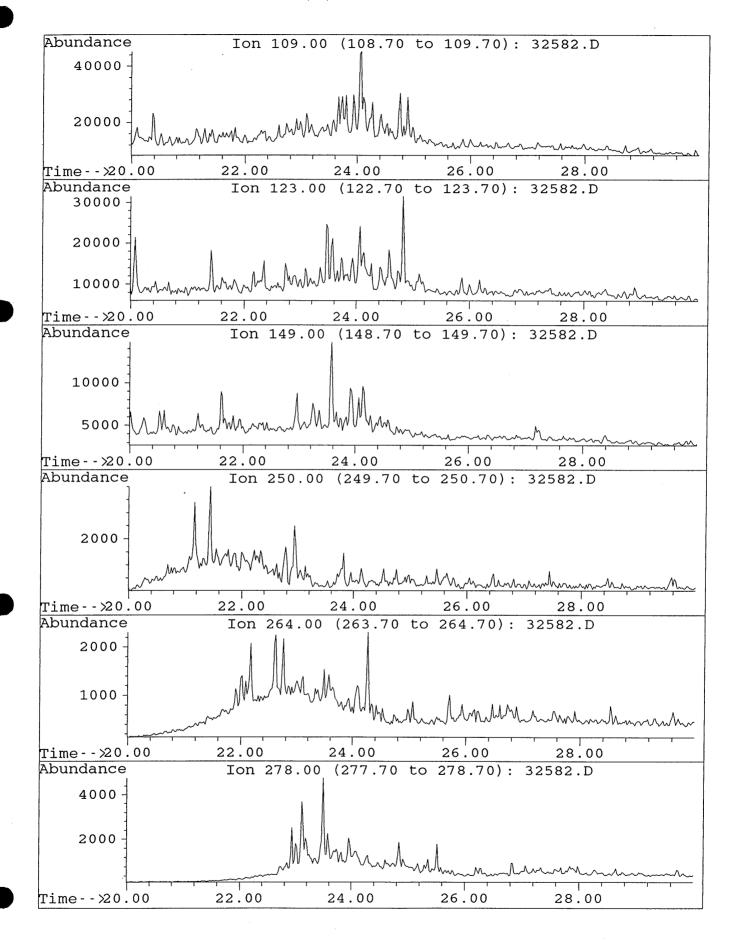


32582.D

Sample :



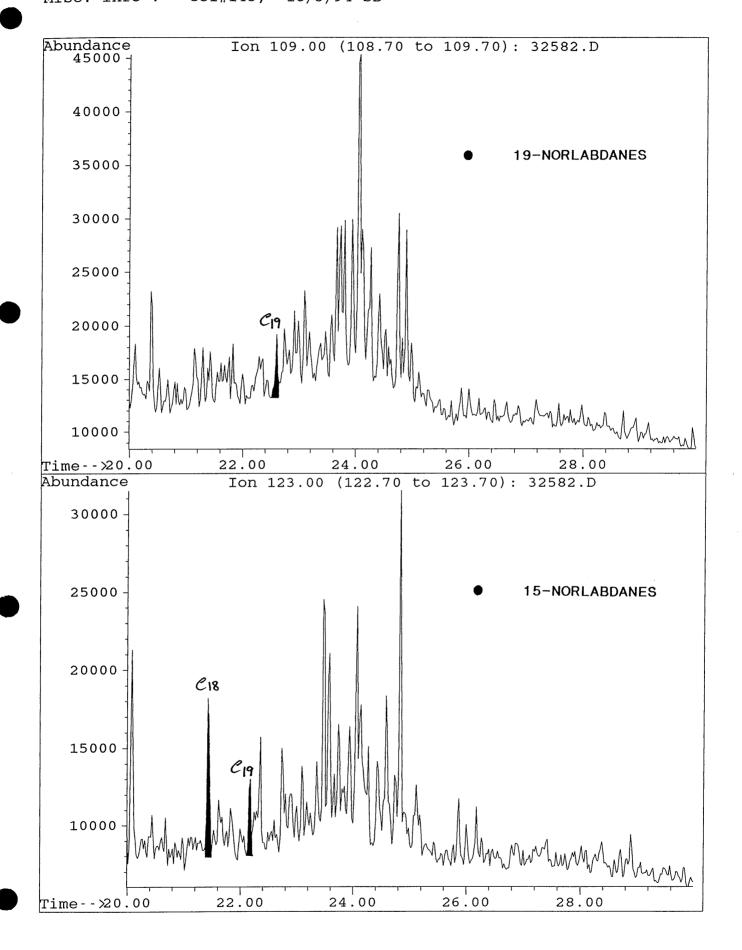
32582.D



32582.D

Sample : Misc. Info :

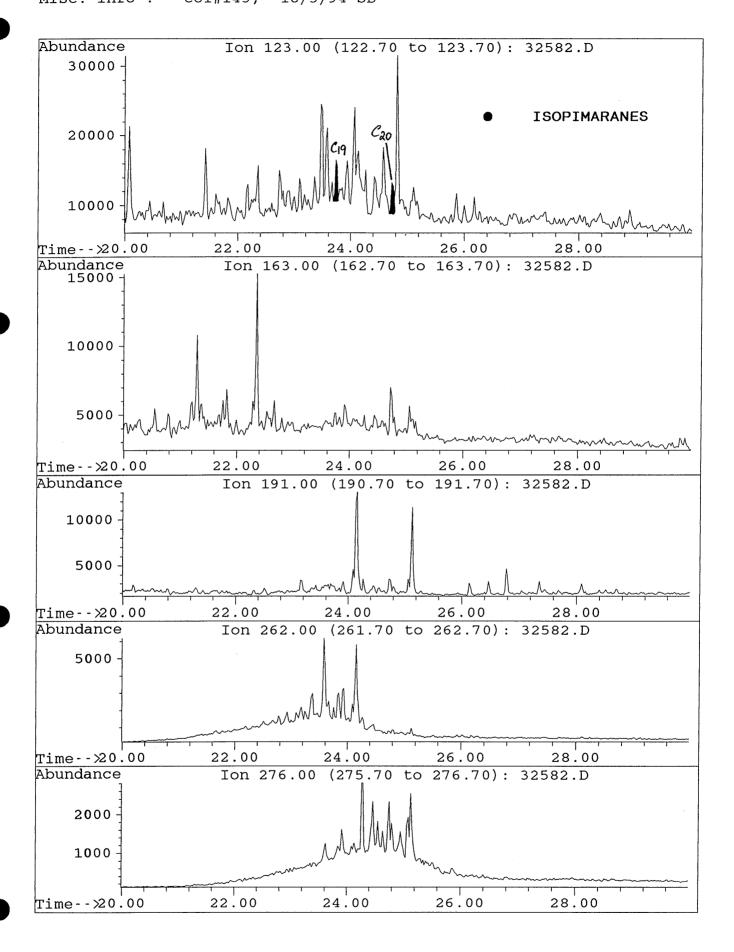
IONA-2 1408.5m B/C col#143, 18/3/94 SB



32582.D

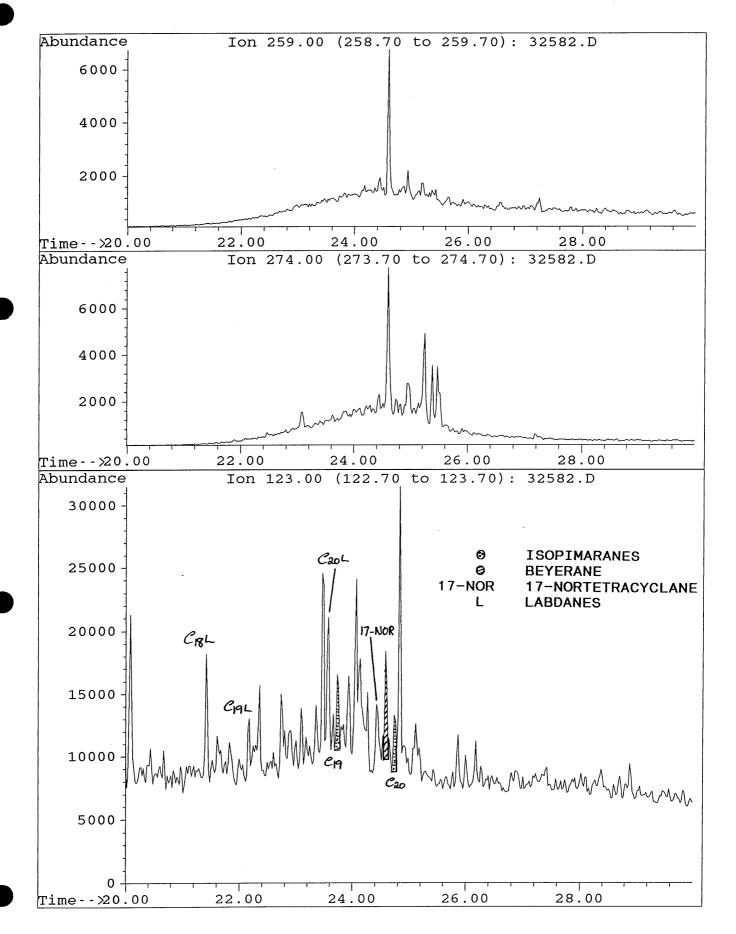
Sample : Misc. Info :

IONA-2 1408.5m B/C col#143, 18/3/94 SB



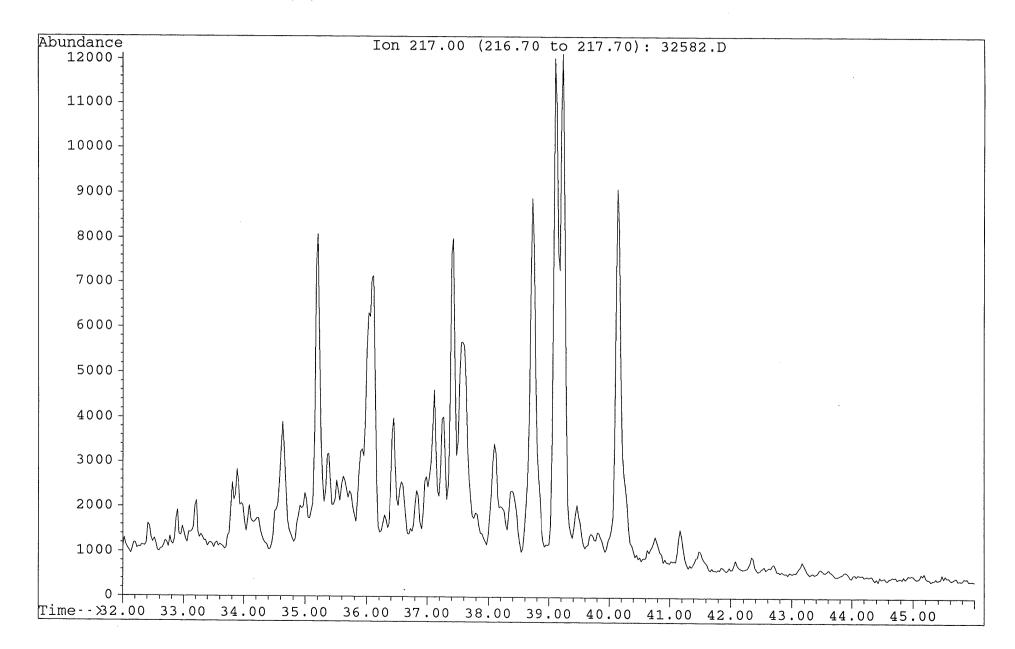
32582.D

Sample : Misc. Info: IONA-2 1408.5m B/C col#143, 18/3/94 SB B/C



F**y**e :

32582.D

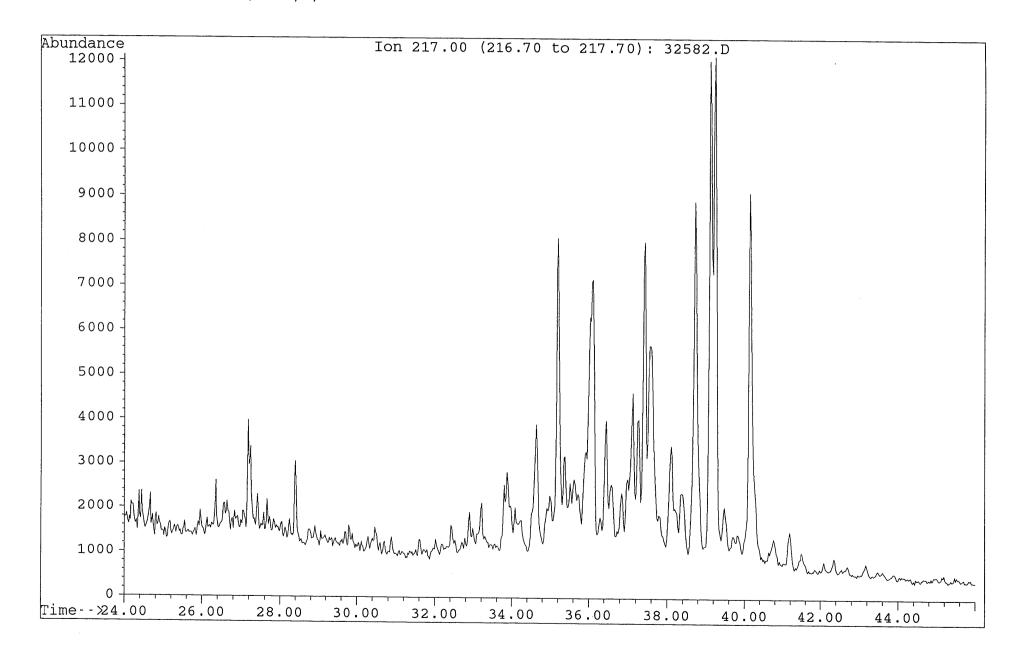


Ege :

32582.D

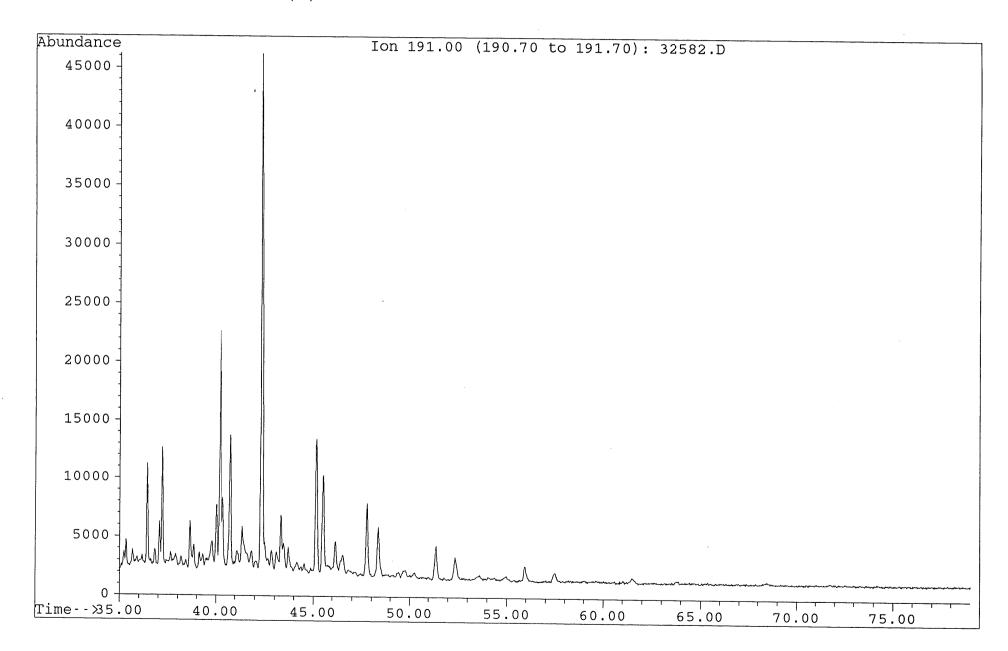
Sample : Misc. Info :

IONA-2 1408.5m B/C col#143, 18/3/94 SB



le :

32582.D



32582.D

Sample: IONA-Misc. Info: col#1

IONA-2 1408.5m B/C col#143, 18/3/94 SB

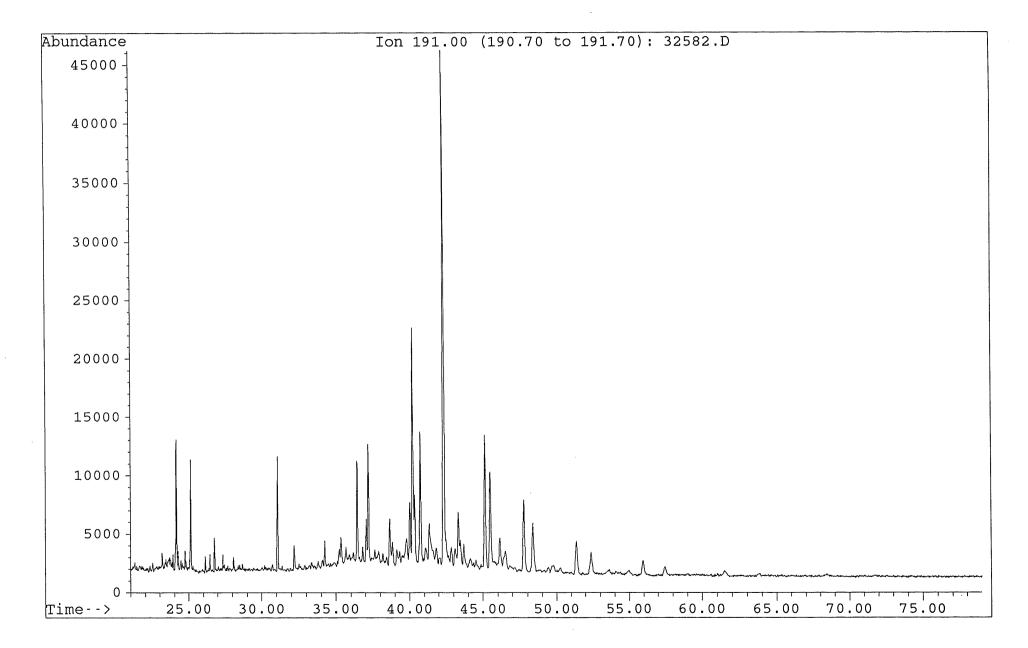


Table 6

## SELECTED AROMATIC PARAMETERS

IONA 2												Mar-94
DEPTH	TYPE	DNR-1	DNR-5	DNR-6	TNR-1	TNR-5	TNR-6	MPR-1	MPI-1	MPI-2	Rc(a)	Rc(b)
1358.0m	SWC	5.94	194.4	3.09	0.60	0.74	nd	2.42	1.06	1.09	1.03	1.67
1408.5m	SWC	6.00	147.2	3.04	0.70	0.76	nd	2.34	1.17	1.21	1.10	1.60

response factors have been applied to DNR 6, TNR 1, TNR 5, MPI 1 and MPI 2

Table 6

## SELECTED AROMATIC PARAMETERS CONT.

IONA 2					Mar-94
DEPTH	TYPE	1,7-DMP/X (m/z 206)	RETENE/9-MP (m/z 219,192)	1MP/9MP	
1358.0m	SWC	0.59	2.20	0.90	
1408.5m	SWC	0.67	0.92	1.00	

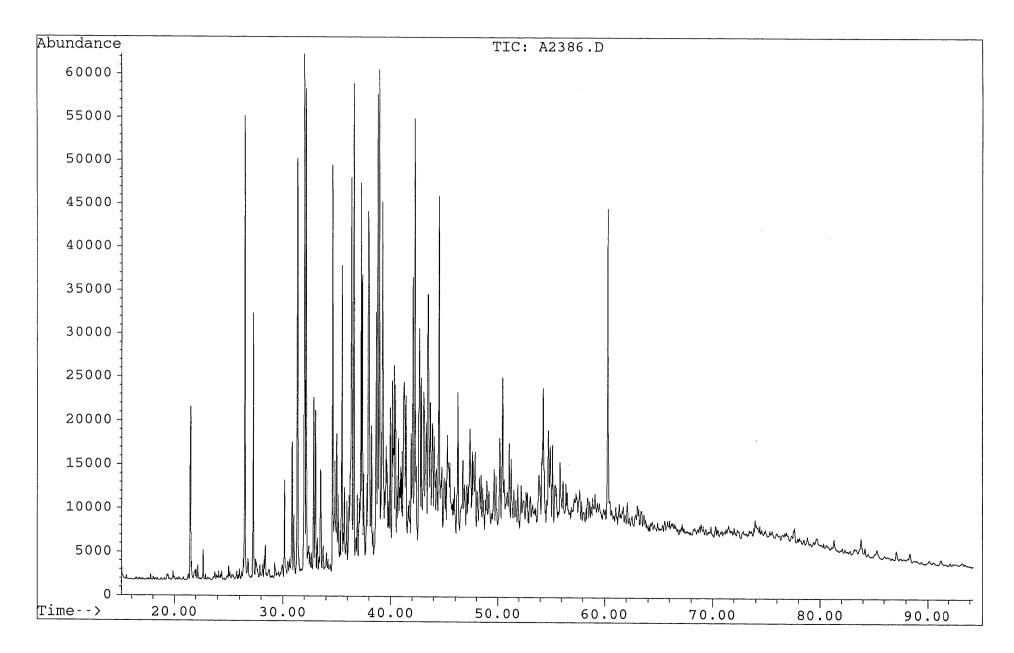
Figure 4-1

A2386.D

Sample:

IONA-2, 1358. AROS

Misc. Info: COL#155. 16-3-94. SB

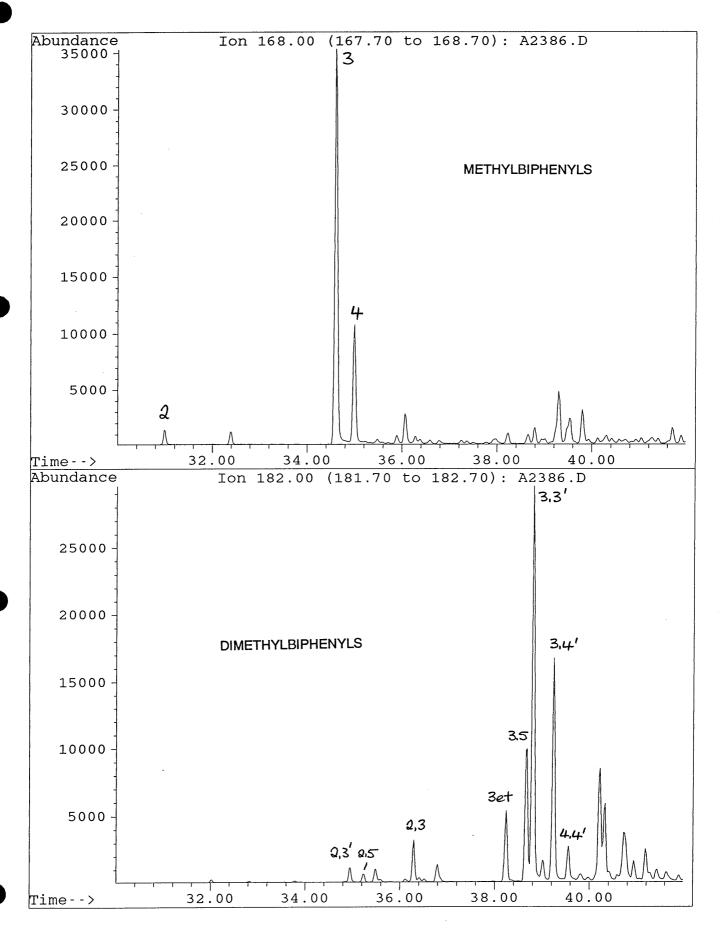


A2386.D

Sample:

IONA-2, 1358. AROS COL#155. 16-3-94. SB

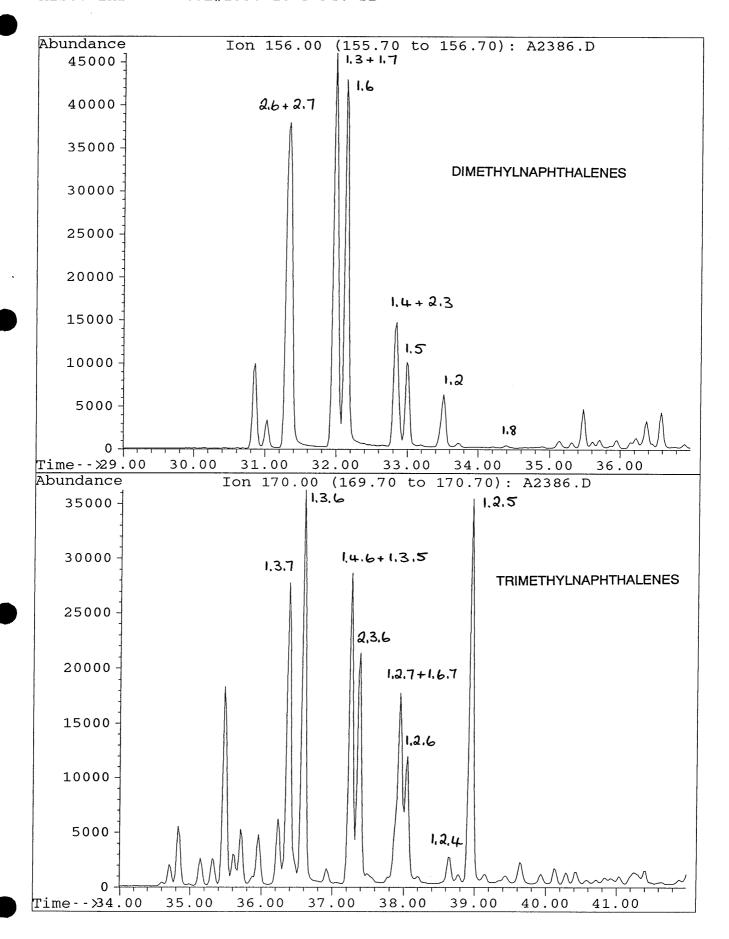
Misc. Info :



A2386.D

Sample : Misc. Info :

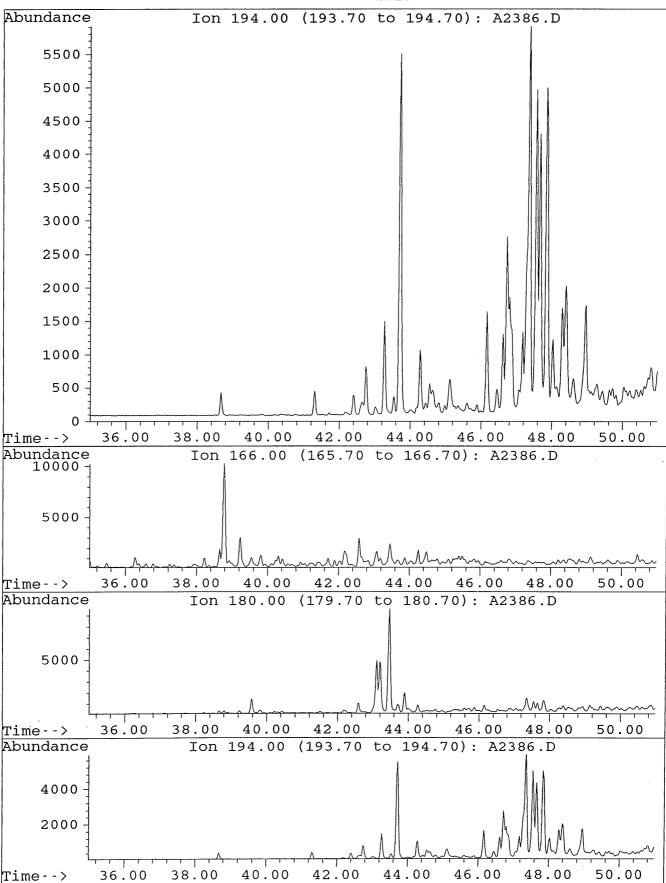
IONA-2, 1358. AROS COL#155. 16-3-94. SB



A2386.D

Sample : Misc. Info : IONA-2, 1358. AROS COL#155. 16-3-94. SB

**FLUORENES** 



A2386.D

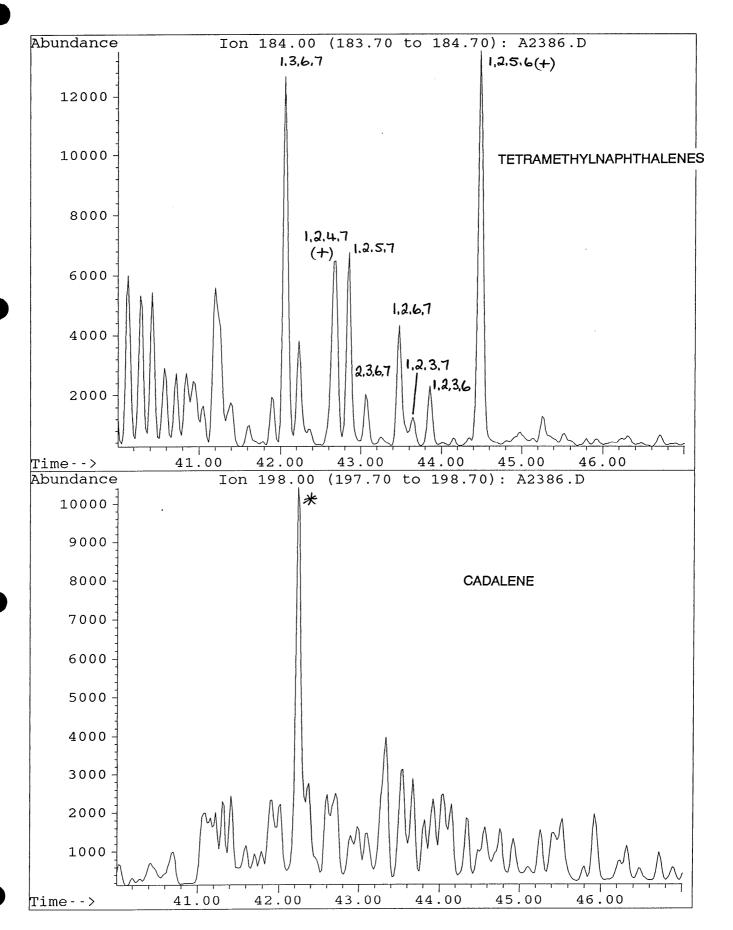
Sample: ION Misc. Info: COL

IONA-2, 1358. AROS COL#155. 16-3-94. SB

Abundance Ion 170.00 (169.70 to 170.70): A2386.D 35000 -30000 25000 20000 15000 10000 -5000 Time - ->34.00 35.00 37.00 38.00 39.00 36.00 40.00 41.00 Abundance Ion 184.00 (183.70 to 184.70): A2386.D 7000 6000 -5000 4000 3000 2000 1000 -37.00 35.00 36.00 38.00 39.00 40.00 Time - ->34.00 41.00

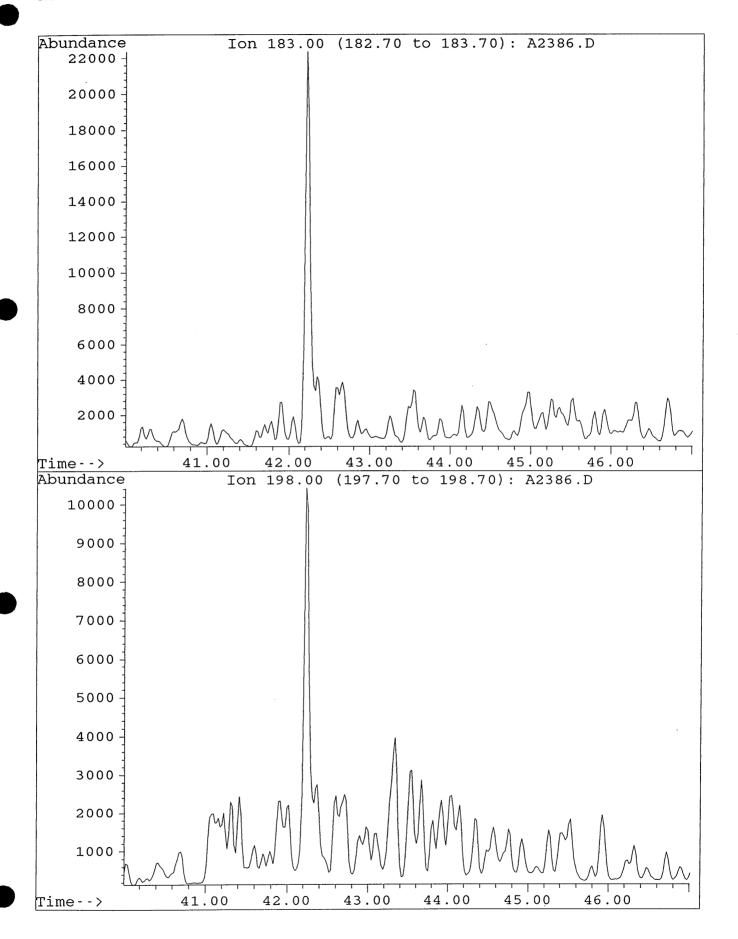
File: A2386.D

Sample: IONA-2, 1358. AROS Misc. Info: COL#155. 16-3-94. SB



File: A2386.D

Sample: IONA-2, 1358. AROS Misc. Info: COL#155. 16-3-94. SB



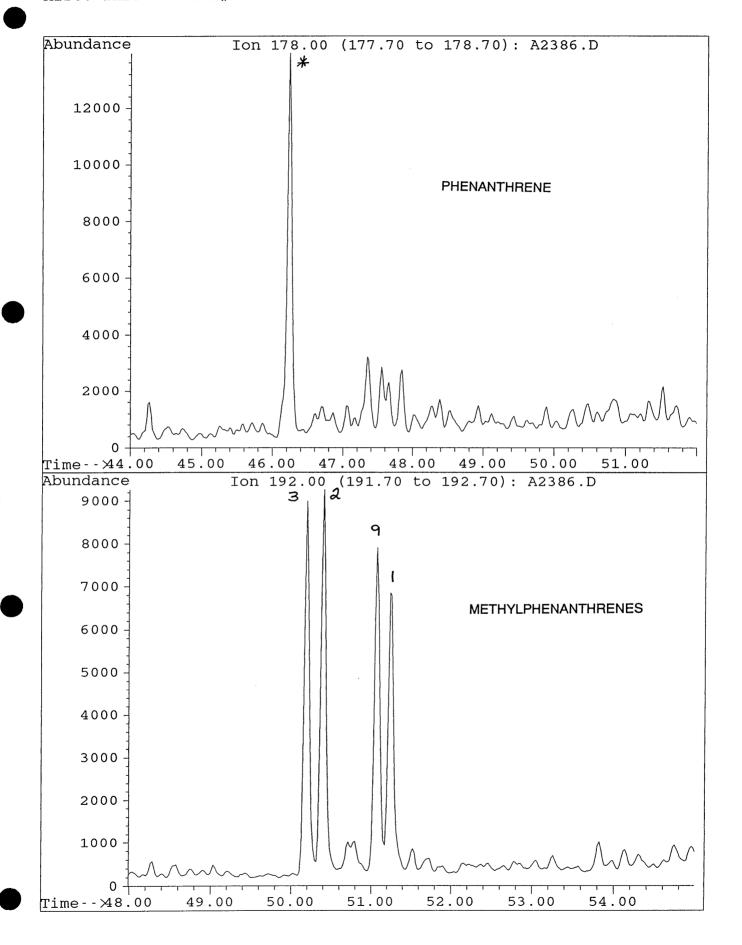
A2386.D

Sample :

IONA-2, 1358. AROS

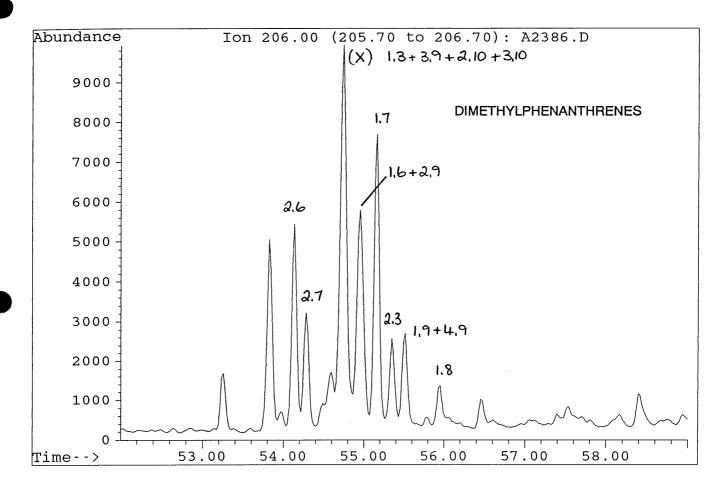
Misc. Info :

COL#155. 16-3-94. SB



File: A2386.D

Sample: IONA-2, 1358. AROS Misc. Info: COL#155. 16-3-94. SB



A2386.D

Sample : Misc. Info :

IONA-2, 1358. AROS COL#155. 16-3-94. SB

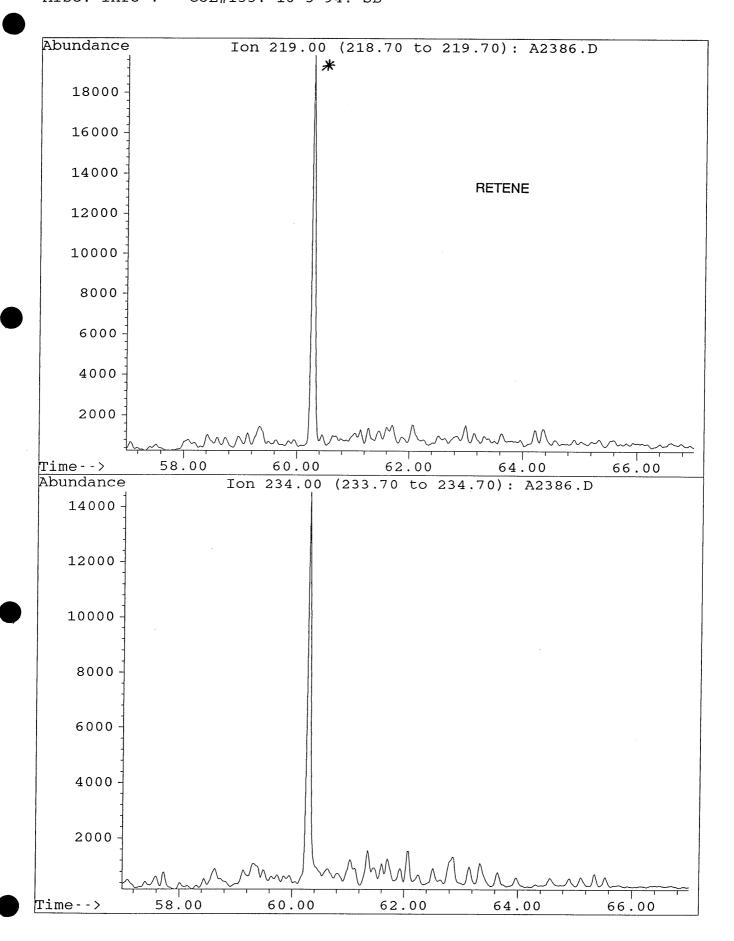
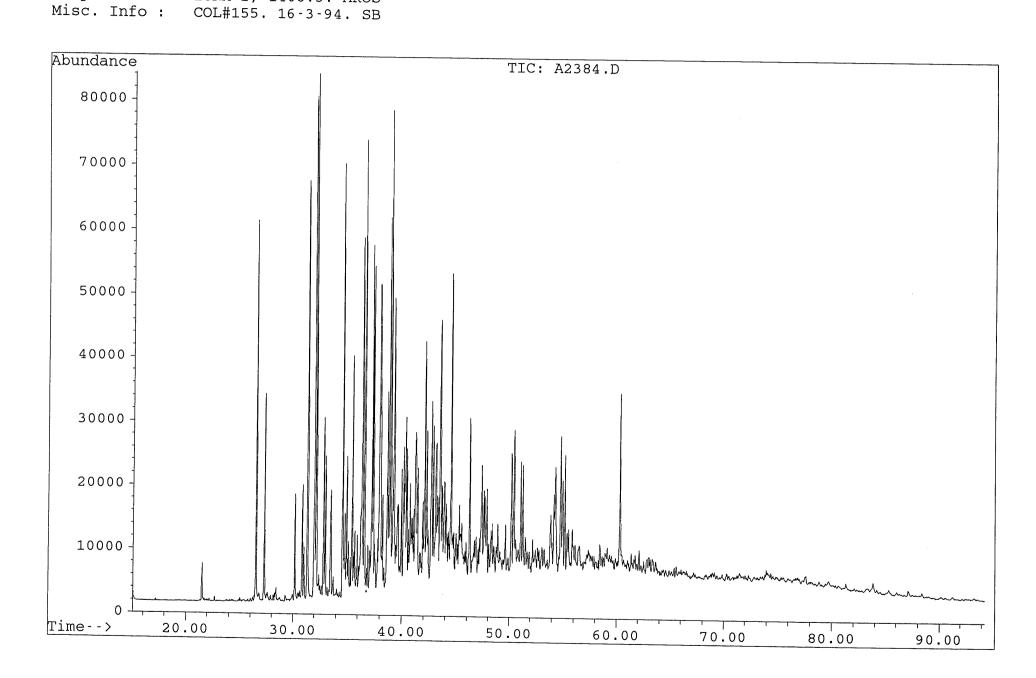


Figure 4-2

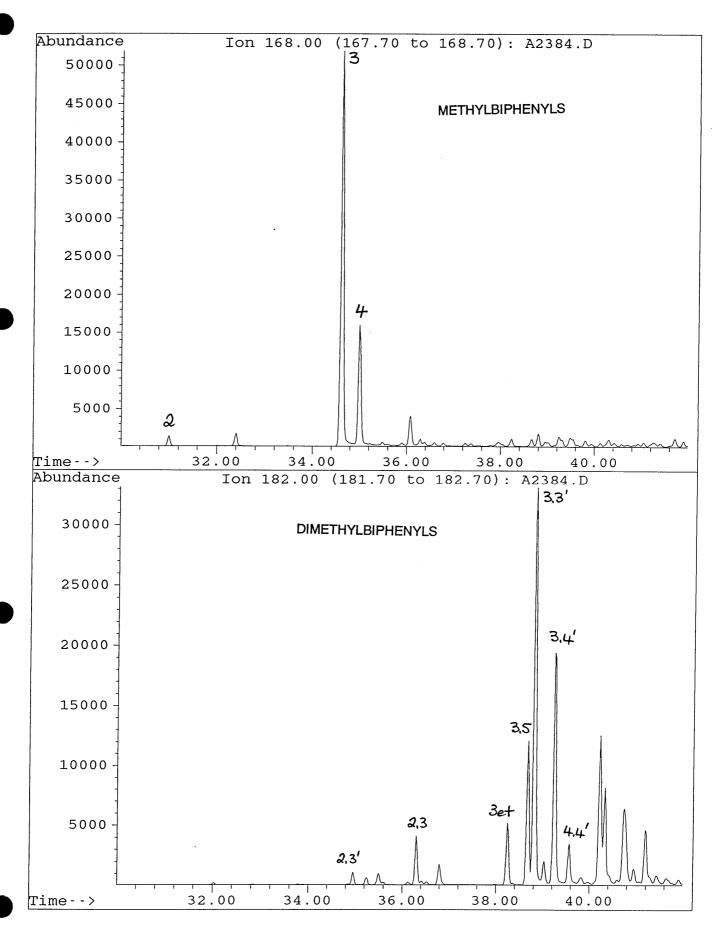
Le : Sample : A2384.D

IONA-2, 1408.5. AROS



File: A2384.D

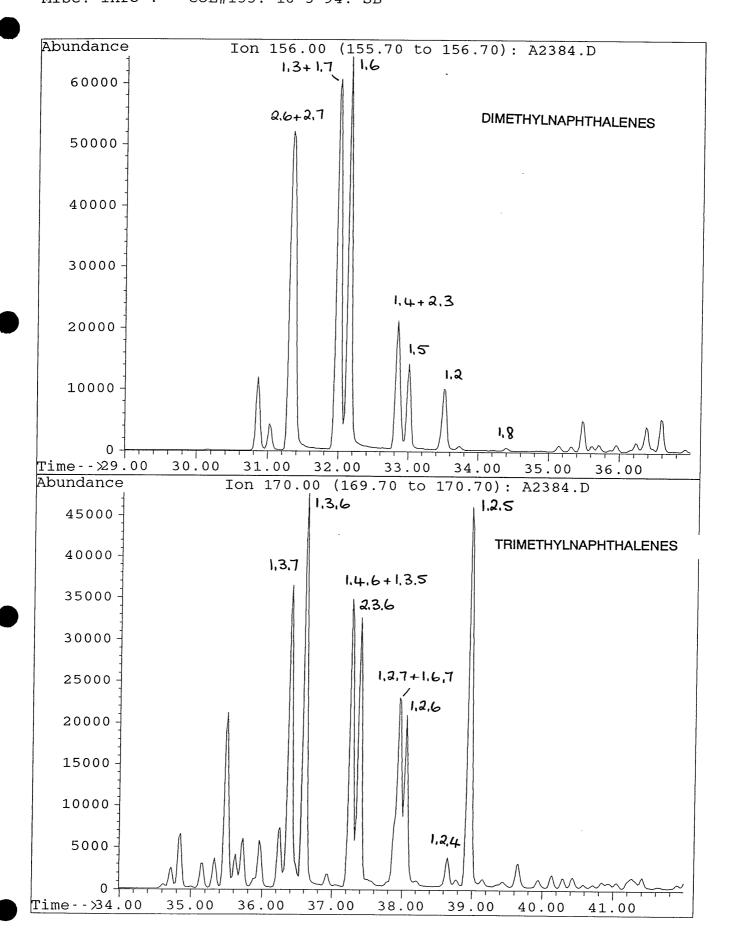
Sample: IONA-2, 1408.5. AROS Misc. Info: COL#155. 16-3-94. SB



A2384.D

Sample : Misc. Info :

IONA-2, 1408.5. AROS COL#155. 16-3-94. SB

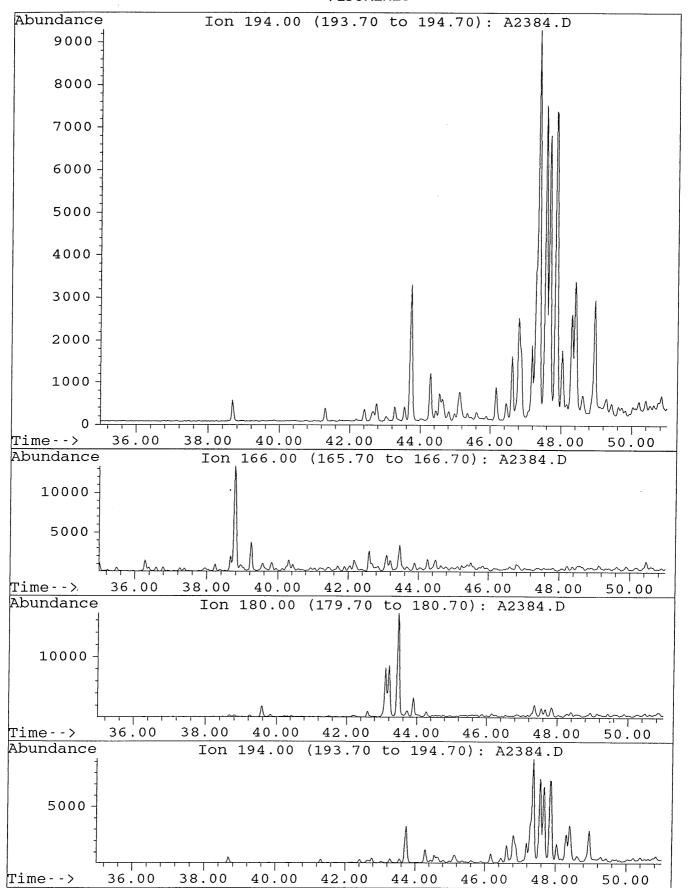


A2384.D

Sample :

IONA-2, 1408.5. AROS Misc. Info: COL#155. 16-3-94. SB

**FLUORENES** 



A2384.D

Sample : Misc. Info : IONA-2, 1408.5. AROS COL#155. 16-3-94. SB

Abundance Ion 170.00 (169.70 to 170.70): A2384.D 45000 -40000 35000 30000 25000 20000 15000 10000 5000 -35.00 Time - - >34.00 Abundance 37.00 38.00 36.00 39.00 40.00 41.00 Ion 184.00 (183.70 to 184.70): A2384.D 8000 7000 -6000 5000 -4000 3000 2000 1000 Time-->34.00 35.00 36.00 37.00 38.00 39.00 40.00 41.00

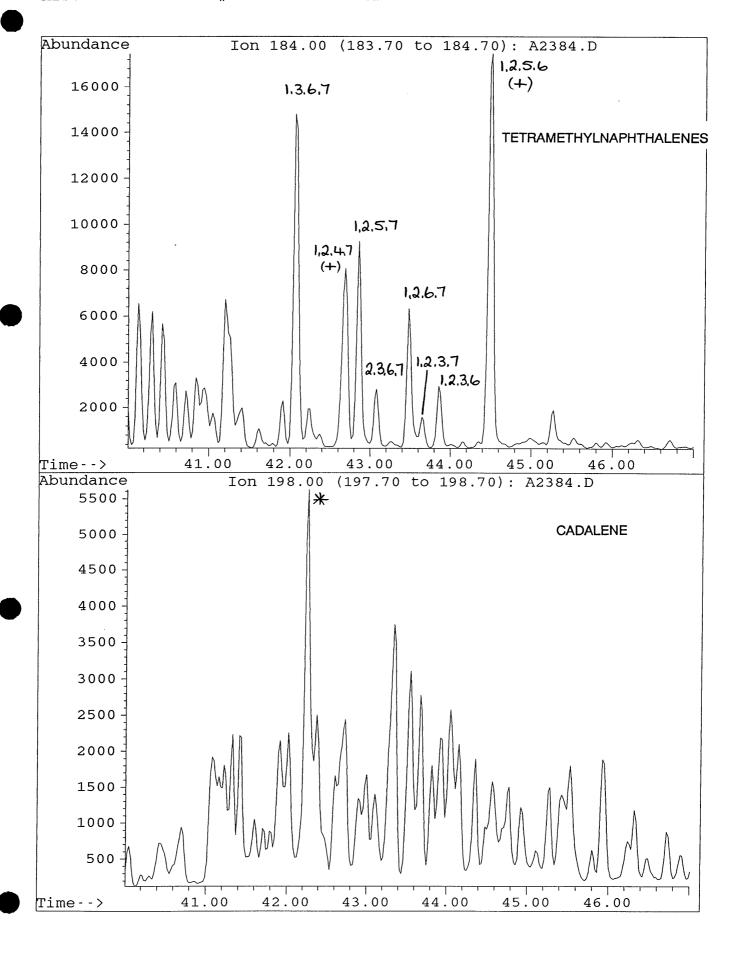
A2384.D

Sample :

IONA-2, 1408.5. AROS

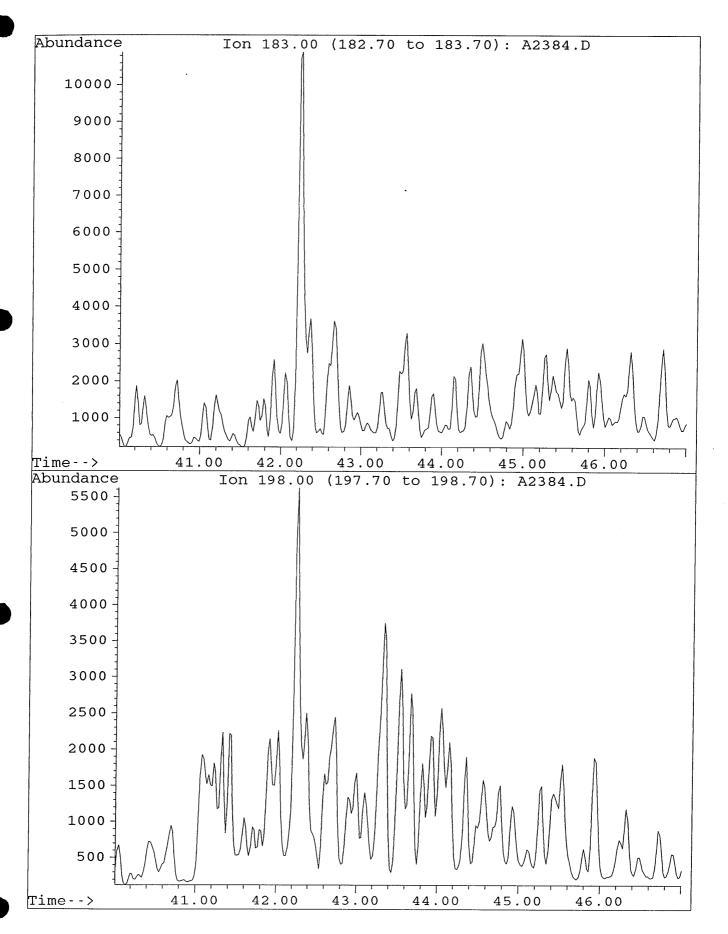
Misc. Info :

COL#155. 16-3-94. SB



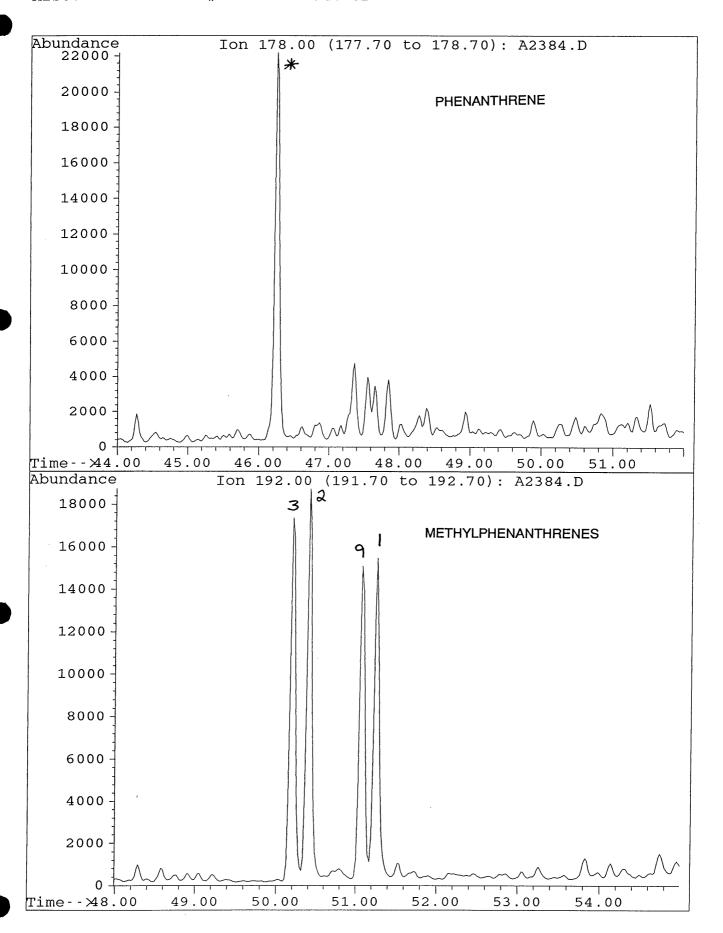
File: A2384.D

Sample: IONA-2, 1408.5. AROS Misc. Info: COL#155. 16-3-94. SB



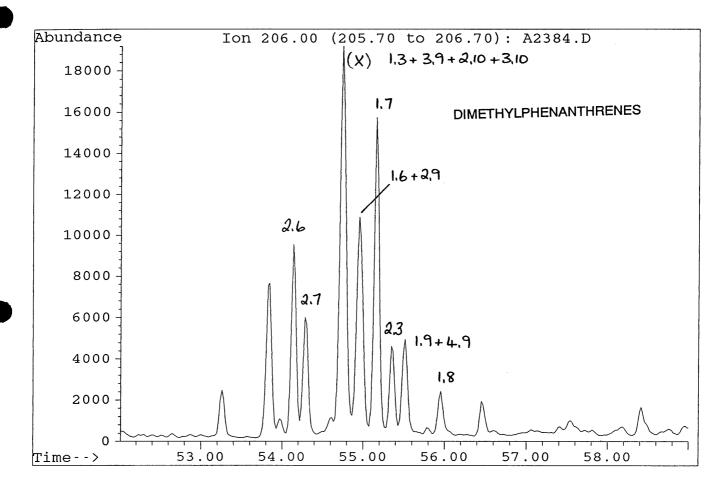
File: A2384.D

Sample: IONA-2, 1408.5. AROS Misc. Info: COL#155. 16-3-94. SB



A2384.D

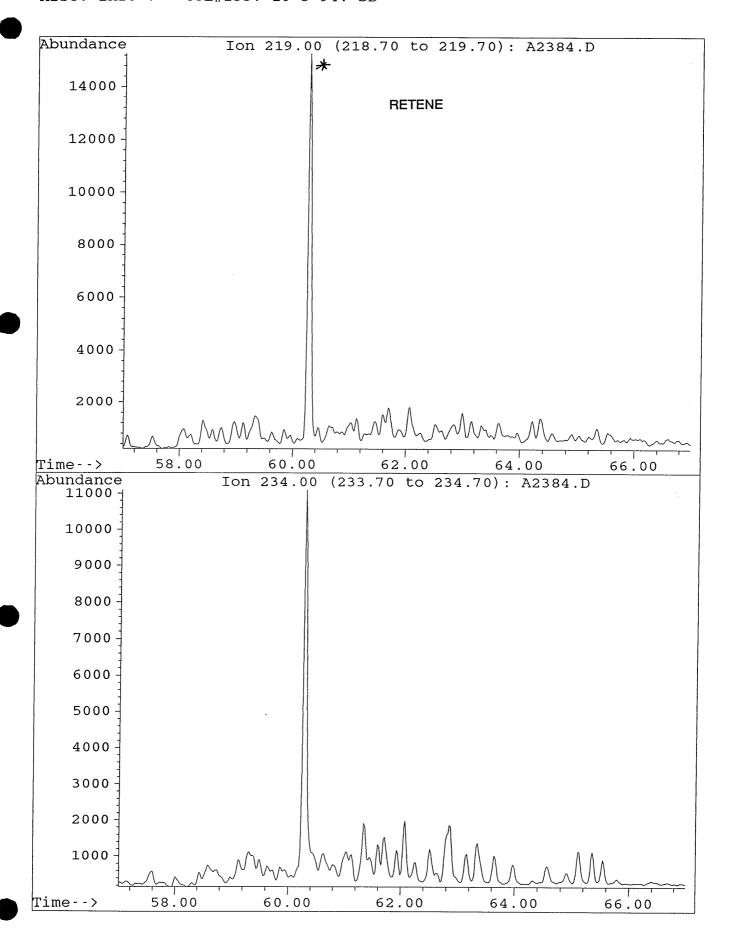
Sample: IONA-2, 1408.5. AROS Misc. Info: COL#155. 16-3-94. SB

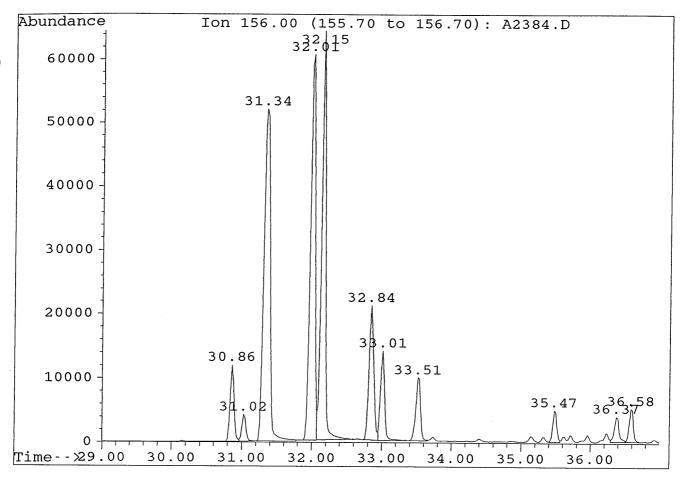


A2384.D

Sample : Misc. Info :

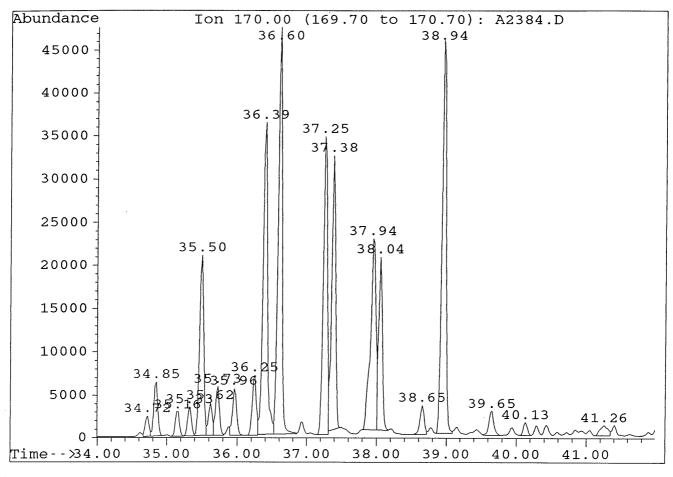
IONA-2, 1408.5. AROS COL#155. 16-3-94. SB





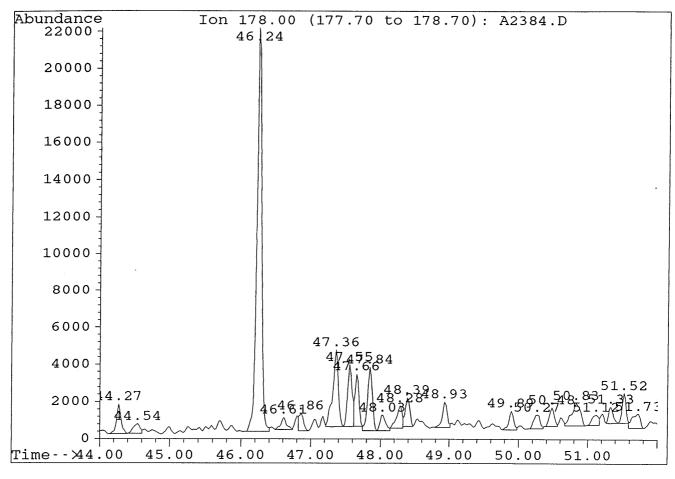
Sample: IONA-2, 1408.5. AROS

Peak	Ret.Time	Area	a	Height	Area %	Ratio %
1	30.86	46366	<i></i>	11949	3.84	13.97
2	31.02	16639	)	4211	1.38	5.01
3	31.34	331964	26+	52012	27.49	100.00
4	32.01	290726	<del>-</del>	60383	24.07	87.58
5	32.15	258280	16	63984	21.39	77.80
6	32.84	99459	14+	20874	8.24	29.96
7	33.01	55326	15	13908	4.58	16.67
8	33.51	47360	<del></del>	9821	3.92	14.27
9	35.47	0.7 🛖 20808	1,8	4957	1.72	6.27
10	36.37	<b>8.3</b> 19083	-	3978	1.58	5.75
11	36.58	21697		5171	1.80	6.54



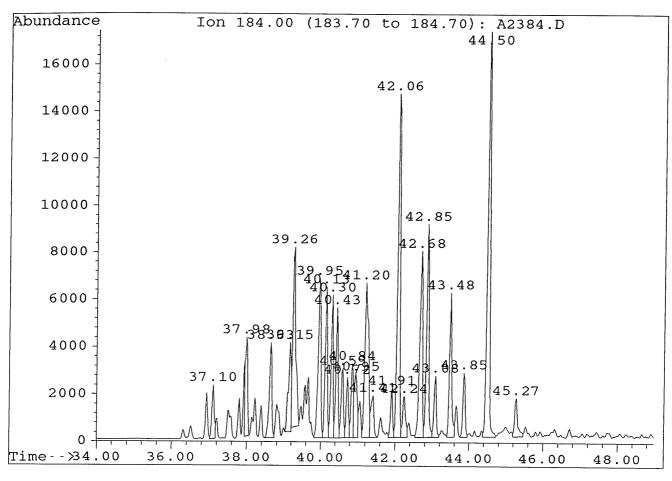
Sample: IONA-2, 1408.5. AROS

Peak	Ret.Time	Area	Height	Area %	Ratio %
1	34.72	9130	2406	0.71	4.71
2	34.85	24672	6316	1.93	12.72
3	35.16	11676	2871	0.91	6.02
4	35.33	13052	3462	1.02	6.73
5	35.50	85350	20928	6.68	44.00
6	35.62	14836	3855	1.16	7.65
7	35.73	21753	5724	1.70	11.21
8	35.96	21912	5489	1.71	11.30
9	36.25	29260	7032	2.29	15.08
10	36.39	159004 <i>/</i> 37	36181	12.44	81.97
11	36.60	190782/36	47284	14.93	98.35
12	37.25	143667 146+	34558	11.24	74.06
13	37.38	122198 236	31649	9.56	62.99
14	37.94	122922	22142	9.62	63.37
15	38.04	70355 _	20083	5.50	36.27
16	38.65	14472	3437	1.13	7.46
17	38.94	193984_ <i>\&amp;\$</i>	45656	15.18	100.00
18	39.65	13336	2825	1.04	6.87
19	40.13	6014	1527	0.47	3.10
20	41.26	9731	1196	0.76	5.02



Sample: IONA-2, 1408.5. AROS

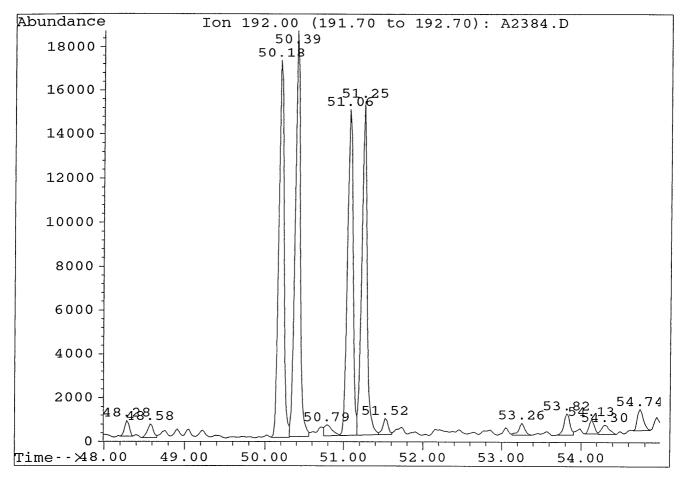
Peak	Ret.Time	Area	Height	Area %	Ratio %
1	44.27	7341	1597	2.81	6.97
2	44.54	3630	529	1.39	3.45
3	46.24	105284	ρ 21777	40.32	100.00
4	46.61	3909	<del>-</del> 667	1.50	3.71
5	46.86	3992	957	1.53	3.79
6	47.36	22792	4121	8.73	21.65
7	47.55	15831	3319	6.06	15.04
8	47.66	10560	2791	4.04	10.03
9	47.84	16398	3404	6.28	15.58
10	48.03	4904	842	1.88	4.66
11	48.28	6892	1193	2.64	6.55
12	48.39	6843	1525	2.62	6.50
13	48.93	6760	1365	2.59	6.42
14	49.89	4957	1015	1.90	4.71
15	50.27	4920	740	1.88	4.67
16	50.48	5070	1002	1.94	4.82
17	50.83	10755	1195	4.12	10.22
18	51.12	3835	5 <b>4</b> 4	1.47	3.64
19	51.33	3986	864	1.53	3.79
20	51.52	6196	1581	2.37	5.89
21	51.73	6273	761	2.40	5.96



Sample :

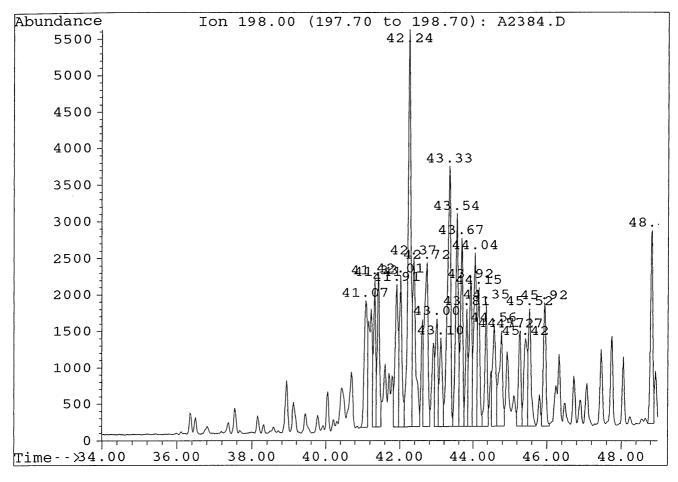
IONA-2, 1408.5. AROS

Peak	Ret.Time	Area	Height	Area %	Ratio %
1	37.10	9707	2278	1.54	11.93
2	37.98	16438	4196	2.61	20.20
3	38.63	19577	4022	3.10	24.06
4	39.15	20916	3783	3.32	25.70
5	39.26	42712	7577	6.77	52.48
6	39.95	35232	6728	5.58	43.29
7	40.13	26245	6373	4.16	32.25
8	40.30	24847	6019	3.94	30.53
9	40.43	22537	5494	3.57	27.69
10	40.59	13206	2934	2.09	16.23
11	40.72	10634	2562	1.69	13.07
12	40.84	13322	3136	2.11	16.37
13	40.95	15265	2684	2.42	18.76
14	41.20	43889	6535	6.96	53.93
15	41.41	10208	1787	1.62	12.54
16	41.91	8585	2087	1.36	10.55
17	42.06	66267	14585	10.50	81.43
18	42.24	9648	1733	1.53	11.86
19	42.68	42406	7867	6.72	52.11
20	42.85	38809	9024	6.15	47.69
21	43.08	11264	2596	1.79	13.84
22	43.48	26594	6097	4.22	32.68
23	43.85	11827	2720	1.87	14.53
24	44.50	81381	17205	12.90	100.00
25	45.27	9334	1625	1.48	11.47



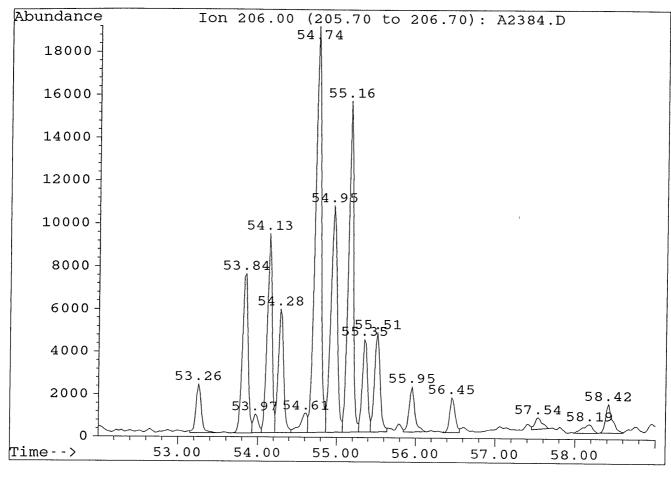
Sample: IONA-2, 1408.5. AROS

Peak	Ret.Time	Area	Height	Area %	Ratio %
1	48.28	2793	716	0.82	3.27
2	48.58	3190	628	0.94	3.74
3	50.18	81029 3	17172	23.81	94.90
4	50.39	85384 2	18522	25.09	100.00
5	50.79	3289	504	0.97	3.85
6	51.06	_71152 <b>9</b>	14823	20.91	83.33
7	51.25	<u>71115</u> ,	15171	20.90	83.29
8	51.52	3404	725	1.00	3.99
9	53.26	3005	556	0.88	3.52
10	53.82	5116	977	1.50	5.99
11	54.13	3007	662	0.88	3.52
12	54.30	2734	405	0.80	3.20
13	54.74	5048	962	1.48	5.91



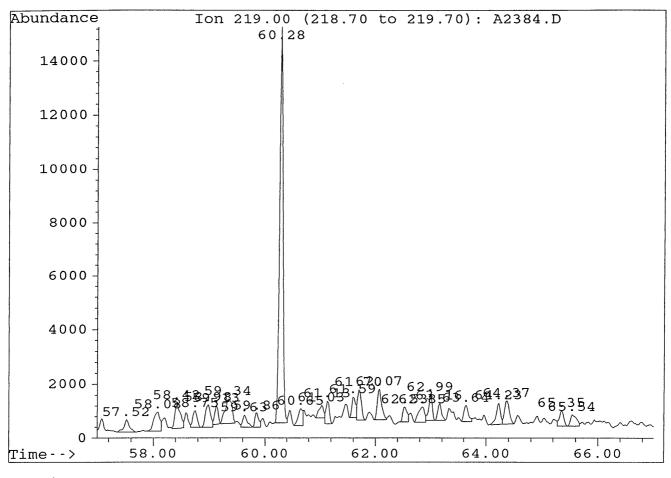
Sample: IONA-2, 1408.5. AROS

Peak	Ret.Time	Area	Height	Area %	Ratio %
1	41.07	11095	1735	3.95	36.21
2	41.33	8334	2045	2.97	27.20
3	41.41	8815	2026	3.14	28.77
4	41.91	12149	1956	4.33	39.65
5	42.01	9239	2068	3.29	30.16
6	42.24	30637	5439	10.92	100.00
7	42.37	12651	2315	4.51	41.29
8	42.72	15404	2251	5.49	50.28
9	43.00	6843	1481	2.44	22.34
10	43.10	6675	1215	2.38	21.79
11	43.33	23314	3564	8.31	76.10
12	43.54	15918	2915	5.67	51.96
13	43.67	12037	2585	4.29	39.29
14	43.81	6773	1613	2.41	22.11
15	43.92	10988	1992	3.92	35.87
16	44.04	13222	2380	4.71	43.16
17	44.15	8250	1905	2.94	26.93
18	44.35	7501	1701	2.67	24.48
19	44.56	8491	1386	3.03	27.71
20	44.77	8963	1310	3.19	29.26
21	45.27	6251	1304	2.23	20.40
22	45.42	8343	1202	2.97	27.23
23	45.52	7734	1606	2.76	25.24
24	45.92	8385	1689	2.99	27.37
25	48.83	12563	2641	4.48	41.01



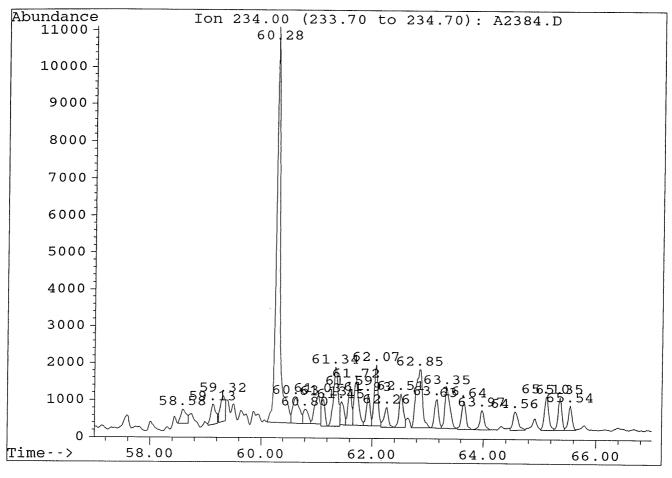
Sample: IONA-2, 1408.5. AROS

Peak	Ret.Time	Area	Height	Area %	Ratio %
1	53.26	10949	2317	2.49	10.52
2	53.84	37673	7506	8.56	36.20
3	53.97	4179	908	0.95	4.02
4	54.13	41662	9366	9.46	40.03
5	54.28	27663	5826	6.28	26.58
6	54.61	6117	936	1.39	5.88
7	54.74	104065 🗶	18989	23.64	100.00
8	54.95	60376	10629	13.71	58.02
9	55.16	69879 <i>17</i>	15501	15.87	67.15
10	55.35	20122	4365	4.57	19.34
11	55.51	23155	4686	5.26	22.25
12	55.95	10936	2136	2.48	10.51
13	56.45	8294	1669	1.88	7.97
14	57.54	3458	533	0.79	3.32
15	58.19	3577	406	0.81	3.44
16	58.42	8122	1356	1.84	7.80



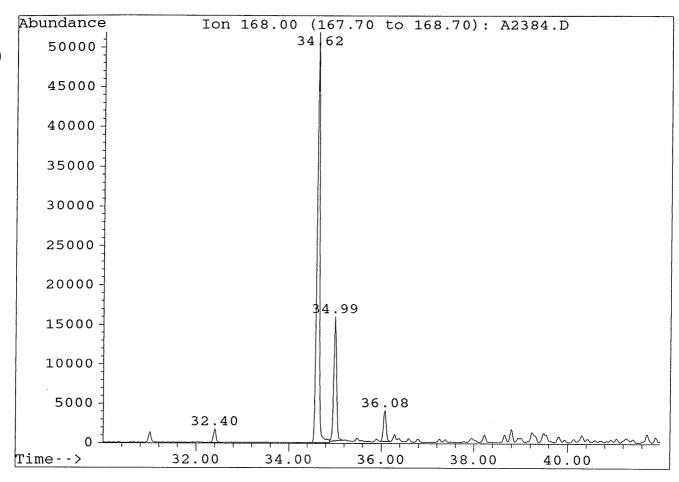
Sample: IONA-2, 1408.5. AROS

Peak	Ret.Time	Area	Height	Area %	Ratio %
1	57.52	3181	472	1.92	4.85
2	58.08	5938	727	3.58	9.05
3	58.42	6474	949	3.91	9.86
4	58.75	3151	619	1.90	4.80
5	58.98	5443	839	3.29	8.29
6	59.13	2878	685	1.74	4.38
7	59.34	8093	902	4.88	12.33
8	59.63	2570	458	1.55	3.91
9	59.86	2769	533	1.67	4.22
10	60.28	_65649 <b>R</b>	14717	39.62	100.00
11	60.65	4020	647	2.43	6.12
12	61.03	2996	480	1.81	4.56
13	61.13	3360	849	2.03	5.12
14	61.59	3623	763	2.19	5.52
15	61.70	5284	1128	3.19	8.05
16	62.07	6350	1140	3.83	9.67
17	62.53	3199	558	1.93	4.87
18	62.85	4438	569	2.68	6.76
19	62.99	4160	954	2.51	6.34
20	63.16	2931	645	1.77	4.46
21	63.64	3467	610	2.09	5.28
22	64.23	4287	801	2.59	6.53
23	64.37	5139	867	3.10	7.83
24	65.35	3055	583	1.84	4.65
25	65.54	3235	432	1.95	4.93



Sample: IONA-2, 1408.5. AROS

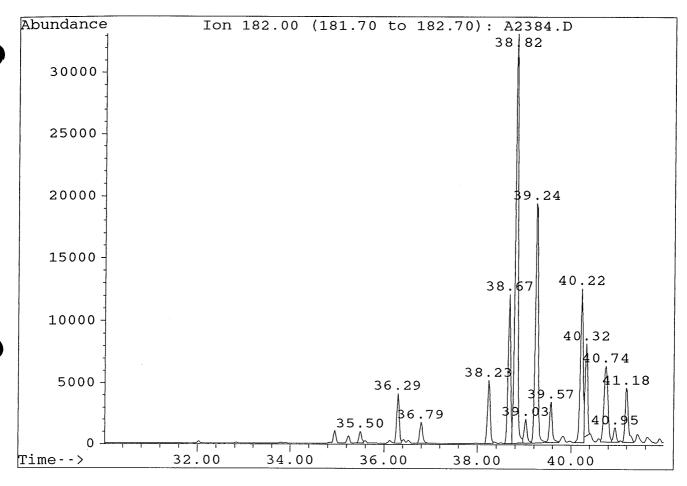
Peak	Ret.Time	Area	Height	Area %	Ratio %
1	58.58	2884	384	1.67	5.05
2	59.13	3422	562	1.99	5.99
3	59.32	4259	697	2.47	7.45
4	60.28	57140	10694	33.15	100.00
5	60.63	5700	671	3.31	9.98
6	60.80	2363	380	1.37	4.14
7	61.03	5603	747	3.25	9.81
8	61.13	2704	728	1.57	4.73
9	61.34	9419	1595	5.46	16.48
10	61.45	2658	618	1.54	4.65
11	61.59	4557	971	2.64	7.98
12	61.72	6746	1184	3.91	11.81
13	61.93	3711	832	2.15	6.49
14	62.07	7693	1649	4.46	13.46
15	62.26	3007	539	1.74	5.26
16	62.51	4876	904	2.83	8.53
17	62.85	12708	1568	7.37	22.24
18	63.16	3848	778	2.23	6.73
19	63.35	6840	1095	3.97	11.97
20	63.64	4050	765	2.35	7.09
21	63.97	2914	534	1.69	5.10
22	64.56	3202	501	1.86	5.60
23	65.10	4912	890	2.85	8.60
24	65.35	4045	876	2.35	7.08
25	65.54	3098	657	1.80	5.42



Sample :

IONA-2, 1408.5. AROS

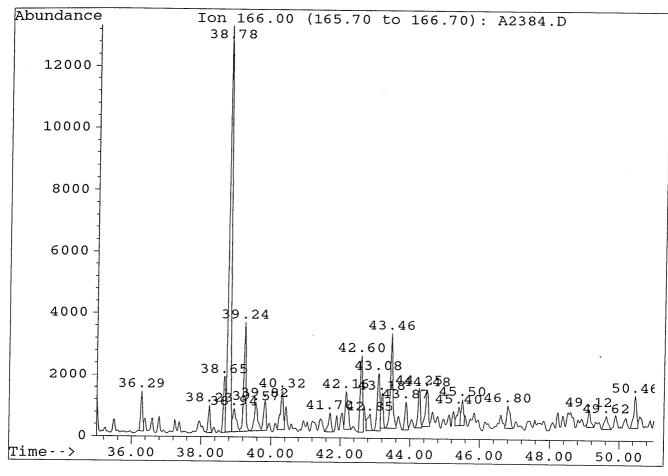
Peak	Ret.Time	Area	Height	Area %	Ratio %
1	32.40	6528	1687	2.21	3.13
2	34.62	208805	51797	70.76	100.00
3	34.99	63478	15687	21.51	30.40
4	36.08	16294	3903	5.52	7.80



Sample :

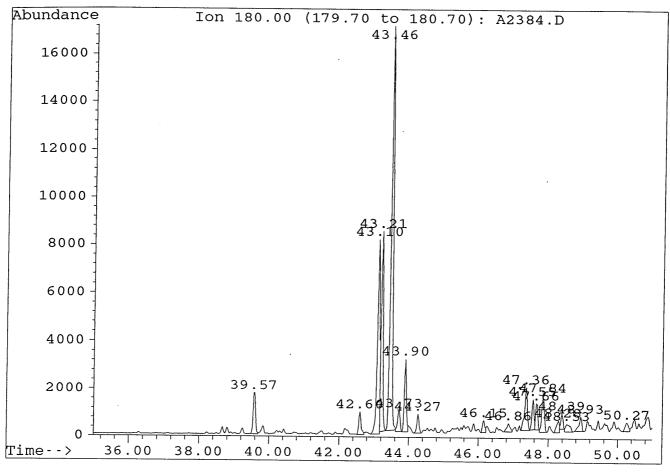
IONA-2, 1408.5. AROS

Peak	Ret.Time	Area	Height	Area %	Ratio %
1	35.50	4151	969	0.87	3.09
2	36.29	15416	4065	3.24	11.48
3	36.79	7213	1738	1.52	5.37
4	38.23	20109	5154	4.23	14.97
5	38.67	45930	12036	9.66	34.20
6	38.82	134302	33045	28.25	100.00
7	39.03	8087	1937	1.70	6.02
8	39.24	80863	19297	17.01	60.21
9	39.57	14889	3332	3.13	11.09
10	40.22	54219	12432	11.40	40.37
11	40.32	25740	7377	5.41	19.17
12	40.74	37652	6221	7.92	28.04
13	40.95	5270	1179	1.11	3.92
14	41.18	21583	4451	4.54	16.07



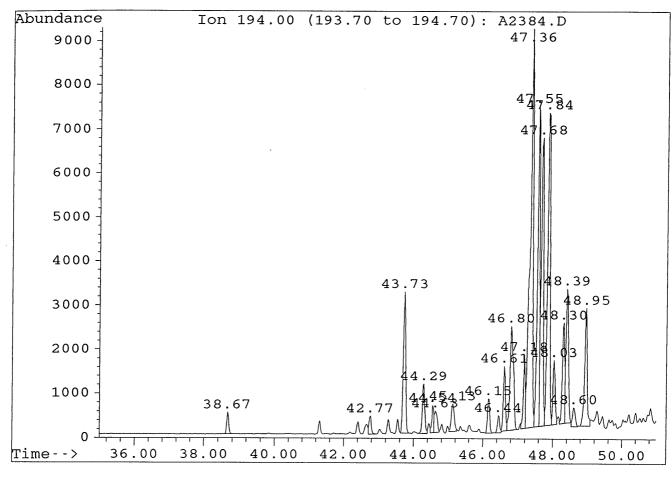
Sample: IONA-2, 1408.5. AROS

Peak	Ret.Time	Area	Height	Area %	Ratio %
1	36.29	5266	1303	2 44	
2	38.23	3421	892	2.44	8.08
3	38.65	7346	1820	1.58	5.25
4	38.78	65189	13186	3.40	11.27
5	38.94	5199	751	30.15	100.00
6	39.24	14387	3543	2.40	7.98
7	39.57	6009		6.65	22.07
8	39.82	4801	887	2.78	9.22
9	40.32	7567	970	2.22	7.36
10	41.70	3514	1249	3.50	11.61
11	42.16	6788	619	1.63	5.39
12	42.60		1224	3.14	10.41
13	42.85	11618	2497	5.37	17.82
14	43.08	3460	538	1.60	5.31
15		10083	1868	4.66	15.47
	43.18	4735	1137	2.19	7.26
16	43.46	15243	3076	7.05	23.38
17	43.87	4212	905	1.95	6.46
18	44.25	5891	1298	2.72	9.04
19	44.48	6681	1197	3.09	10.25
20	45.40	3582	600	1.66	5.49
21	45.50	4004	844	1.85	6.14
22	46.80	4852	736	2.24	7.44
23	49.12	2991	557	1.38	4.59
24	49.62	3232	419	1.49	4.96
25	50.46	. 6164	1046	2.85	9.46



Sample : IONA-2, 1408.5. AROS

Peak	Ret.Time	Area	Height	Area %	Ratio %
1	39.57	7825	1746	3.48	10.65
2	42.60	4201	956	1.87	5.72
3	43.10	40773	8133	18.12	55.52
4	43.21	30307	8377	13.47	41.27
5	43.46	73443	16932	32.64	100.00
6	43.73	4657	891	2.07	6.34
7	43.90	12763	3060	5.67	17.38
8	44.27	3466	800	1.54	4.72
9	46.15	2533	504	1.13	3.45
10	46.86	2319	342	1.03	3.16
11	47.36	10209	1824	4.54	13.90
12	47.55	5555	1288	2.47	7.56
13	47.66	4206	1101	1.87	5.73
14	47.84	7786	1544	3.46	10.60
15	48.28	2936	501	1.30	4.00
16	48.39	2692	653	1.20	3.67
17	48.53	2992	330	1.33	4.07
18	48.93	3665	621	1.63	4.99
19	50.27	2676	360	1.19	3.64



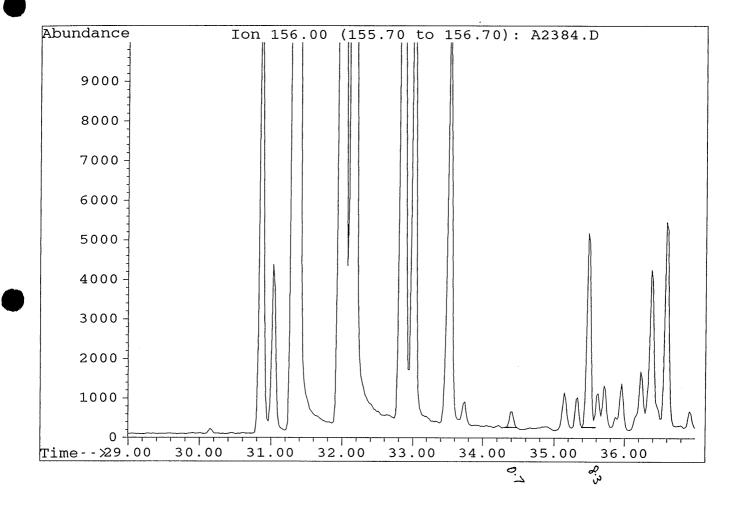
Sample: IONA-2, 1408.5. AROS

Peak	Ret.Time	Area	Height	Area %	Ratio %
1	38.67	1952	490	0.73	3.66
2	42.77	1699	403	0.64	3.19
3	43.73	15359	3194	5.76	28.79
4	44.29	5275	1114	1.98	9.89
5	44.54	2564	605	0.96	4.81
6	44.63	2562	473	0.96	4.80
7	45.13	3978	616	1.49	7.46
8	46.15	3450	769	1.29	6.47
9	46.44	1776	387	0.67	3.33
10	46.61	6234	1464	2.34	11.69
11	46.80	16343	2345	6.13	30.64
12	47.18	6621	1668	2.48	12.41
13	47.36	53342	9047	20.00	100.00
14	47.55	34072	7257	12.78	63.87
15	47.68	28364	6533	10.64	53.17
16	47.84	34934	7079	13.10	65.49
17	48.03	6306	1449	2.36	11.82
18	48.30	11023	2276	4.13	20.66
19	48.39	14810	3028	5.55	27.76
20	48.60	2346	419	0.88	4.40
21	48.95	13684	2672	5.13	25.65

A2384.D

Sample :

Sample: IONA-2, 1408.5. AROS Misc. Info: COL#155. 16-3-94. SB



#### PETROLEUM GEOCHEMISTRY

#### 1.0 INTRODUCTION

Petroleum geochemistry is primarily concerned with the application of organic chemistry to samples of geological interest in hydrocarbon exploration.

Analyses can be carried out on cuttings, sidewall cores, conventional cores, relatively unweathered outcrop samples and fluid hydrocarbons (oil, condensate, gas).

Source rock evaluation is best performed on sidewall cores, since cuttings are more susceptible to contamination from both cavings and organic additives in the mud system. In petroleum geochemical studies it is vitally important for the geochemist/geologist to be aware of the type of mud additives used and the stage at which they are used during the drilling program. Any anomalous results must be carefully considered in conjunction with mud system records.

Petroleum geochemistry in exploration is applied for three major purposes:

- 1. First identification of richness, maturity and type of kerogen in (a large number of) whole rock samples by screening analyses.
- 2. Semi-detailed characterisation of kerogen in sediments from selected source intervals, to determine maturity, source type and genetic potential.
- 3. Detailed characterisation of petroleum fluids (extracts, oils and condensates) by assessment of thermal maturity, source type and depositional environment to enable oil-to-oil and oil-to-source rock correlation studies.

#### 2.0 THEORY & METHODS

Samples are analysed according to the scheme illustrated in Figure 1 which shows th order and type of analysis for both screening and detailed tests.

#### 2.1 <u>Screening Analyses of Whole Rock Samples</u>

#### 2.1.1 Headspace/Cuttings Gas Analysis

The headspace sample is usually provided in a sealed tin can which holds both cuttings and water to approximately three quarters capacity. This allows the volatile hydrocarbons to diffuse easily into an appreciable headspace.

The gas is taken into a syringe through a silicone seal on the lid of the containe and analysed by packed column gas chromatography using the following conditions:

Instrument:

Shimadzu GC-8APF

Column:

6'x 1/8" Chromosorb 102

Injector/Detector Temperature:

120°C

Column Temperature:

110°C

Carrier Gas:

Nitrogen

Cuttings gas analysis is performed in the same manner but on samples which do not liberate volatile gases readily. These sediments are subjected to very vigorous agitation prior to sampling.

Values are given as volume of gas per million volumes of sediment (ppm) for each hydrocarbon (methane, ethane, propane, iso- and n-butane), as composite values including  $C_5$ - $C_7$ , and as ratios.

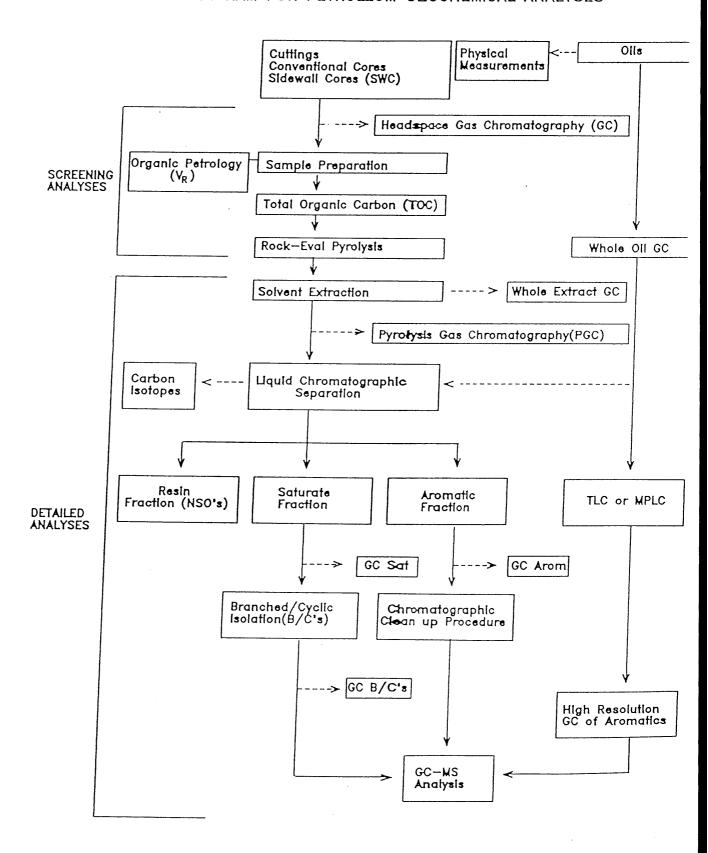
Headspace/cuttings gas analyses are used as a screening technique to identify zones of significant gas generation and out-of-place gas (Letran et al, 1974). The classification for gas content is listed below:

	_	s content ; or C ₅ -C ₇ )	Description
10	-	100ppm	very lean - lean
100	-	1,000	lean - moderate
1,000	-	10,000	moderate - rich
10,000	-	100,000	rich - verv rich

The abundance of  $\rm C_2\text{-}C_4$  components (wet gas) is used to locate the zone of oil generation, since wet gas is commonly associated with petroleum (Fuex, 1977).

It is important to ensure that the gases analysed are not of a biogenic origin, so an anti-bacterial agent must be added to the cuttings when they are stored in water.

FIGURE 1
FLOW DIAGRAM FOR PETROLEUM GEOCHEMICAL ANALYSES



#### 2.1.2 Sample Preparation

Depending on drilling mud content, cuttings samples may be water washed before they are air dried, picked free of contaminants and cavings, and ther crushed to 0.1mm using a ring pulveriser.

Sidewall cores are freed of mud cake and other visible contaminants, sampled according to homogeneity, air dried and hand crushed to 0.1mm grain size.

Conventional core and outcrop samples are inspected for visible contaminants and crushed to 1/8" chips using a jaw crusher. After air drying, the chips are crushed with a ring pulveriser to small particle size (0.1mm).

Petroleum aqueous mixtures are separated into oil and water/mud fractions by decanting off the oil layer and producing a clean separation by gently centrifuging the oil. If separation by this method is not effective, the petroleum is solvent extracted.

#### 2.1.3 Total Organic Carbon (TOC)

The TOC value is determined on crushed sediment. The minimum sample requirement is one gram, however, results may be obtained from as little as 0.2gm in very rich samples. Carbonate minerals are first removed by acid digest (HCI) and the remaining sample heated to 1700°C (Leco Induction Furnace) in an atmosphere of pure oxygen. The CO₂ produced is measured with an infra-red detector, and values calculated according to standard calibration.

TOC is expressed as % of rock and is used as a screening procedure to classify source rock richness:

0.00 - 0.50	0.00 - 0.25
1.00 - 2.00	0.25 - 0.50 0.50 - 1.00
2.00 - 4.00 > 4.00	1.00 - 2.00 > 2.00
	0.50 - 1.00 1.00 - 2.00 2.00 - 4.00

#### 2.1.4 Rock-Eval Pyrolysis

Although a preliminary source rock classification is made using TOC data, a more accurate assessment of organic source type and maturity is possible by Rock-Eval pyrolysis. Two types of Rock-Eval analyses are offered: "one run" which involves pyrolysis of the crushed but otherwise untreated sediment and "two run" which involves pyrolysis of both the crushed, untreatment sediment and the decarbonated sediment. The "two run" method provides more accurate  $S_3$  values than the "one run" method.  $S_1$  and  $S_2$  values are of the same accuracy in both methods.

The method requires 0.4g of sample material, although reliable results can often be obtained from smaller amounts.

The crushed sediment is heated in an inert atmosphere of helium over a programmed temperature range. The resulting pyrogram is shown in Figure 2.

Hydrocarbons present in the free or adsorbed state ( $S_1$ ) are thermally distilled at 300°C and measured by a flame ionisation detector (FID). Hydrocarbons are then cracked from the kerogen ( $S_2$ ) during a temperature ramp from 300° to 550°C and also measured by FID.  $CO_2$  released during the kerogen cracking process ( $S_3$ ) is trapped and subsequently measured by a thermal conductivity detector.

The amount of free hydrocarbons in the sediment  $(S_1)$  represents milligrams of hydrocarbons distilled from one gram of rock and is a measure of both in situ and out-of-place petroleum.

Free hydrocarbon richness is described by the following:

#### S₁ (mg/g or kg/tonne)

0.20 - 0.40	fair
0.40 - 0.80	good
0.80 - 1.60	very good
> 1.60	excellent

The total amount of hydrocarbons present in the free state and as kerogen is a measure of the potential yield (genetic potential) of the sample  $(S_1 + S_2)$  and is expressed as mg/g of rock.

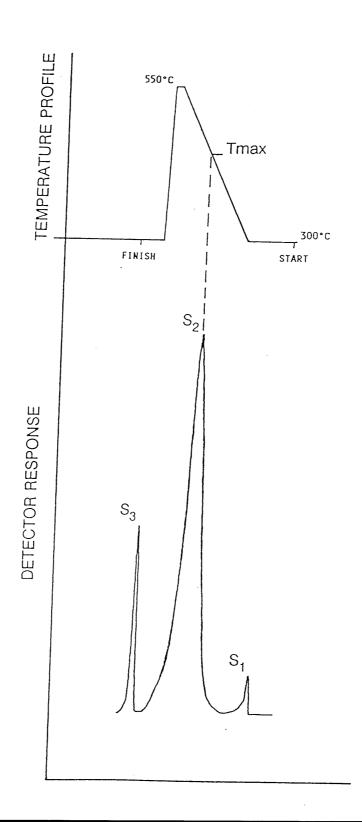
Source rocks are classified accordingly:

$S_1 + S_2$	(mg/g)	Source Rock Qualit
0.00 -	1.00	poor
1.00 -	2.00	marginal
2.00 -	6.00	moderate
6.00 -	10.00	good
10.00 -	20.00	very good
>	20.00	excellent

The Production Index (PI) represents the amount of petroleum generated relative to the total amount of hydrocarbons present  $(S_1/(S_1+S_2))$ . It is a measure of the level of maturity of the sample. For oil prone sediments PI ranges from 0.1 at the onset of oil generation to 0.4 at peak oil generation. For gas prone sediments, PI shows only a small change with increasing maturity.

The temperature at which the maximum amount of S2 hydrocarbons is generated is called Tmax (Figure 2). This temperature increases with the increasing maturity of sediments.

FIGURE 2 , SCHEMATIC PYROGRAM OF ROCK-EVAL PYROLYSIS



The variation of Tmax is summarised as

< 430°C immature 430/435° - 460°C mature (oil window) > 460°C overmature

Hydrogen Index (HI = S2 x 100/TOC) and Oxygen Index (OI = S3 x 100/TOC) when plotted against one another, provide information about the type of keroger and the maturity of the sample. Both parameters decrease in value with increasing maturity. Samples with high HI and low OI are dominantly oil prone and samples with low HI and high OI are gas prone.

#### 2.2 Analysis of Kerogen

#### 2.2.1 Organic Petrology - Vitrinite Reflectance

Vitrinite is a coal maceral which responds to increasing levels of thermal maturity. This response is measured microscopically by the percent of light reflected off the polished surface of a vitrinite particle immersed in oil.

Measurement of vitrinite reflectance can be carried out on uncrushed, washed and dried cuttings (10-50gms of sample material required), sidewall cores (2-10gms), conventional cores (2-10gms) or outcrop samples (2-10gms).

The values given are for standard lower size limits. In special cases, however, useful data may be obtained from as little as 0.1gm.

For each sample a minimum of 25 fields is measured in order to establish a range and mean for reflectance values.

Maturity classifications according to vitrinite reflectance values are:

% V _R (approx)	Maturity
0.2 - 0.55 0.55 - 1.2 1.2 - 1.8 > 1.8	immature mature overmature severely altered
	ooverely altered

Following vitrinite reflectance measurements, microscopic examination in fluorescence mode allows the description of liptinite macerals and an estimate of their abundances. The amount of dispersed organic matter is reported and its composition described.

Vitrinite reflectance results and maceral descriptions are best obtained from coals or rocks deposited in environments which received large influxes of terrestrially derived organic matter. Vitrinite reflectance cannot be measured in rocks older than Devonian age, since land plants had not evolved prior to this time.

#### 2.2.2 Pyrolysis Gas Chromatography

Pyrolysis gas chromatography (PGC) is performed on solvent extracted source rocks or isolated kerogens. The sample is pyrolysed by an SGE pyrojector which is coupled directly to a Hewlett Packard 5890 gas chromatograph. The operating conditions are:

Pyrolysis temperature:

600°C

Column:

25m x 0.22mm ID BP-1 (SGE)

Carrier gas:

helium

Oven conditions:

-20° to 280°C @ 4°/min

Data are collected and recovered using DAPA scientific software.

Pyrolysis GC allows the examination of kerogen on the molecular level and thereby a better classification of source rocks with regard to source type and generative capacity than conventional bulk pyrolysis (ie. Rock-Eval). Two analytical procedures are possible:

- 1. Semi quantitative (with yield related to S2 of Rock-Eval)
- 2. Fully quantitative (with the inclusion of an internal standard)

Samples are characterised according to the amounts of aliphatic, aromatic and phenolic components in the kerogen. The aliphatic carbon content of a kerogen is the critical factor in determining catagenic hydrocarbon yields in the earth's crust, while the gas/oil ratio is dictated by the distribution of the various structural elements in the kerogen (Larter, 1985). Using pyrogram fingerprint data, it is possible to distinguish substantial variations between kerogens, even those of the same bulk chemical type.

A major strength of pyrolysis methods is that, while quantitative yields of kerogens are maturity related, the qualitative pyrogram fingerprints obtained are relatively rank independent over much of the oil window (Espitatlie et al, 1977; Van Graas et al, 1980; Larter, 1985). At high maturities (>1.2% V_R) characteristics for all kerogen types tend to converge (Horstfield, 1984).

Data are presented by percentage and mg/g of individual substances as well as groups of compounds.

Significant parameters are:

 $(C_1 - C_5)/C_6 + abundance$ 

gas/oil ratio

C₉ - C₃₁ (alkenes + alkanes)

oil yield

Type Index R:

aromaticity

(Larter & Douglas 1979, Larter and Senftle, 1985).

#### 2.3 <u>Detailed Analyses of Petroleum Fluids</u>

#### 2.3.1 Solvent Extraction of Sediment

The finely crushed sample (up to 100g) is extracted with dichloromethane (300mL) using sonic vibration. After Buchner flask filtration, the filtrate is revibrated with activated copper powder (1g) to remove elemental sulphur. The extractable organic matter (EOM) is afforded by further filtration and fractional distillation of the solvent.

Source rock richness based upon EOM is classified accordingly:

Yield	ppm
Poor	< 500
Fair/Good	500 - 2000
Very Good	2000 - 4000
Excellent	> 4000

#### 2.3.2 Liquid Chromatography Separation

Sediment extracts, crude oil and condensate samples are separated into fractions corresponding to three structural types:

saturated hydrocarbons	(SAT)
aromatic hydrocarbons	(AROM)
resins plus ashphaltenes	(NSO)

This separation is achieved by liquid column chromatography using activated silicic acid adsorbent and eluting solvents of varying polarity. Saturated, aromatic and NSO concentrates are recovered by fractional distillation/evaporation of the solvent and quantitative transfer to a small vial.

The amount of hydrocarbons (SAT plus AROM) can be used to classify source rock richness and the amount of saturates to classify oil source potential, according to the following criteria:

Classification	ppm HC	ppm SAT
Poor Fair	0 - 300 300 - 600	0 - 200 200 - 400
Good	600 - 1200	400 - 800
Very Good	1200 - 2400	800 - 1600
Excellent	>2400	> 1600

The composition of the extracts can also provide information about their levels of maturity and/or source type (LeTran et. al., 1974; Philippi, 1974). Generally, marine extracts have relatively low concentrations of saturated and NSO compounds at low levels of maturity, but these concentrations increase with increasing maturation. Terrestrially derived organic matter often has a low level of saturates and large amount of aromatic and NSO compounds, irrespective of the level of maturity.

Specific ratios are measured from solvent extraction and liquid chromatography data which give an indication of source type and maturity. EOM (mg)/TOC(g) can be used as a maturation indicator when plotted against depth for a given sedimentary sequence. Generally an EOM/TOC value of >100 indicates high maturity. If such a sample has a SAT (mg)/TOC (g) ratio <20, it is likely that the organic matter is gas prone. A value for SAT (mg)/TOC (g) >40 suggests an oil prone source type.

#### 2.3.3 Capillary Gas Chromatography (GC)

 $C_{12}^{+}$  gas chromatography is most commonly carried out on saturate fractions, but in certain instances it is used to examine whole extracts/oils, aromatic or branched/cyclic fractions. It is also used as a tool to identify contamination. The analyses are performed under the following conditions:

Instruments:

Hewlett Packard 5890 Gas Chromatography

Injector: Column:

SGE OCI-3 on column 25m x 0.2mm ID BP-1

Injector Temp:

280°C

Detector Temp:

320°C

Column Temp:

45°C to 280°C at 4°/min

Carrier Gas:

hydrogen

Data are collected using an IBM compatible PC and DAPA scientific software.

#### 2.3.3.1 C₁₂+ Saturate Gas Chromatography

Saturate GC results provide information pertaining to source type, maturity and depositional environment.

The n-alkane distribution from n-C $_{12}$  to n-C $_{31}$  is determined from the area under the peaks representing each of these n-alkanes. The profile can yield information about maturity and source type and is quantified in the C $_{21}$  + C $_{22}$ /C $_{28}$  + C $_{29}$  ratio and Carbon Preference Indices (CPI 1 and 2).

$$CPI(1) = \frac{(C_{23} + C_{25} + C_{27} + C_{29}) wt\% + (C_{25} + C_{27} + C_{29} + C_{31}) wt\%}{2 \times (C_{25} + C_{26} + C_{28} + C_{30}) wt\%}$$

$$CPI(2) = \frac{(C_{23} + C_{25} + C_{27}) wt\% + (C_{25} + C_{27} + C_{29}) wt\%}{2 \times (C_{24} + C_{26} + C_{28}) wt\%}$$

- carbon preference indices are approximately 1 for marine samples, regardless of maturity
- decrease from 20 --> 1 for terrestrial samples as maturity increases

The  $C_{21}$  +  $C_{22}/C_{28}$  +  $C_{29}$  ratio is generally > 1.5 for aquatic source material and < 1.2 for terrestrial organic matter, however, the values increase with maturity.

Pristane/phytane (Pr/Ph) ratios can indicate depositional environments:

< 3.0 - relatively reducing depositional environments;

3.0-4.5 - mixed (reducing/oxidising) environments;

>4.5 - relatively oxidising depositional environments.

### 2.3.3.2 C₁ - C₃₁ Whole Oil Gas Chromatography

This analytical method is applied to oil and condensate samples. It provides a picture of the whole oil up to  $n-C_{31}$  and allows quantitation of components with more than 4 carbons atoms. Several parameters are measured which illustrate changes in the degree of biodegradation and water washing in the reservoir. Because these measurements are performed on very volatile components in the oil, care should be taken during sampling, transportation and storage of the fluid to minimise evaporation.

Whole oil analytical conditions are listed below:

Instrument: Shimadzu GC-9A

Column: 25m x 0.2mm ID BP-1

Injector/Detector Temperature: 290°C

Column Temperature: -20°C to 280°C at 4°/min

Carrier Gas: hydrogen

#### 2.3.4 Carbon Isotope Analysis

This measurement is normally carried out on one or more of the following mixtures: topped oil, saturate fraction, aromatic fraction, NSO fraction. The organic matter is combusted in oxygen to produce carbon dioxide which is purified and transferred to an isotope mass spectrometer. The carbon isotope ratio  $(\delta C_{13}/\delta C_{12})$  is measured and compared to an international standard (the Peedee Belemnite Limestone - PDB).

Carbon isotope analysis is most commonly used to identify the source of methane according to the following criteria (Fuex 1977):

 $\delta^{13}$ C ‰ PDB

-75 to -55 Biogenic methane

-58 to -40 Methane associated with oil

-40 to -25 Thermal methane

Source rock-crude oil correlations have been attempted by observing the change in  $\delta^{13}C$  values of components of oils and rocks (Stahl 1977). Source rock extracts are usually isotopically heavier than the corresponding crude oil but are lighter than the asphaltenes of the oil and the kerogen of the rock (Hunt 1979). It has also been observed that marine organic carbon is generally isotopically heavier than contemporaneous terrestrial organic carbon (Tissot & Welte 1978). However, it should be noted that increasing maturity and biodegradation produce a shift toward heavier isotope values.

#### 2.3.5 Gas Chromatography - Mass Spectrometry (GC/MS)

GC/MS analysis is normally performed on the branched and cyclic alkane fraction and/or the aromatic fraction of oils, condensates and sediment extracts. The specific fraction is first isolated and then injected into a gas chromatograph which is linked in series with a mass spectrometer. As compounds are eluted from the chromatography column they are bombarded with high energy electrons. This causes them to fragment into a number of ions each with a molecular weight less than that of the parent molecule. Individual compounds give a characteristic fragmentation pattern (mass spectrum), the major ions of which are presented in a series of mass fragmentograms [ie. plots of ion concentration against GC retention time].

GC/MS analysis can be carried out using one of the following modes of operation:

- (i) Acquire mode in which all ions (within a broad range) in each mass spectrum are memorised by the data system.
- (ii) Selective Ion Monitoring (SIM) mode in which only selected ions of interest are memorised by the data system.

#### 2.3.5.1 GC/MS Analysis of Branched/Cyclic Alkanes

The group of compounds to be analysed is first isolated from the saturate fraction by refluxing the sample with activated 5Å molecular sieves in cyclohexane for 24 hours. Branched/cyclic alkanes, including alkylcyclohexanes, are recovered from the solvent by fractional distillation.

For condensates, and samples where information about alkylcyclochexanes is not required, the saturate fraction is passed through a small column packed with silicalite adsorbent. The branched/cyclic alkanes are recovered from the eluting solvent by fractional distillation.

Analysis is carried out in the SIM mode with a total of 33 ions being recorded over different time spans.

#### Operating conditions are:

Instrument:

5987HP GC mass spec data system

Column:

60m x 0.25mm ID cross linked methyl-silicone DB-1 (J&W)

column of 0.25 micron film thickness connected directly to

the ion source

Injector:

OCI-3 (SGE)

Carrier gas:

hydrogen

Oven Conditions:

50° to 274°C at 8°/min 274° to 280°C at 1°/min

EM Voltage:

2,000 - 2,300V

Electron Energy:

70eV

Source temperature:250°C

GC/MS mass fragmentograms are examined for particular 'biomarker' compounds which can be related to biological precursors. These allow the characterisation of petroleum with regard to thermal maturity, source, depositional environment and biodegradation.

The significance of selected parameters from branched/cyclic GC/MS analysis is outlined below:

#### 1. $18\alpha$ (H)-hopane/17 $\alpha$ (H)-hopane (Ts/Tm)

<u>Maturity</u> indicator. The ratio of  $18\alpha$  (H) trisnorhopane to  $17\alpha$  (H) trisnorhopane increases exponentially with increasing maturity from approximately 0.2 at the onset to approximately 1.0 at the peak of oil generation, ie. Tm decreases with maturity. This parameter is not reliable in very immature samples.

# 2. $C_{30}$ hopane/ $C_{30}$ moretane

<u>Maturity</u> indicator. The conversion of  $C_{30}$  17 $\beta$ , 21 $\beta$  hopane to 17 $\beta$ , 21 $\alpha$  moretane is maturity dependent. Values increase from approximately 2.5 at the onset of oil generation to approximately 10. Once the hopane/moretane ratio has reached 10, no further changes occur. A value of 10 is believed to represent a maturity stage just after the onset of oil generation and hopane/moretane ratios are therefore useful mainly as indicators of immaturity in a qualitative sense.

# 3&4. $C_{31}$ and $C_{32}$ 22S/22R hopanes

<u>Maturity</u> indicator. An equilibrium between the biological R- and the geological S- configuration occurs on mild thermal maturation. A ratio of S:R = 60:40, ie, a value of 1.5, characterises this equilibrium which occurs <u>before</u> the onset of oil generation. The  $C_{32}$  hopane pair is often more reliable for this purpose since co-elution sometimes affects the  $C_{31}$  ratio.

# 5. $C_{29} 20S \alpha \alpha \alpha / C_{29} 20R \alpha \alpha \alpha$ steranes

<u>Maturity</u> indicator. Upon maturation, the biologically produced 20R stereoisomer is diminished relative to the 20S form and a stabilisation is reached at approximately 55% 20R and 45% 20S compounds.  $V_R$  equivalents are approximately 0.45% for a 20S/20R value of 0.2 and 0.8% for a 20S/20R value of 0.75. This parameter is most useful between maturity ranges equivalent to 0.4% to 1.0%  $V_R$ .

# 6. $C_{29} 20S \alpha \alpha \alpha / C_{29} 20R \alpha \alpha \alpha + C_{29} 20S \alpha \alpha \alpha$ steranes

Maturity indicator. This ratio is a different way of expressing the relative abundance of the biological 20R to the geological 20S normal sterane (see parameter 5). Expressed as a percentage, a value of about 25% indicates the onset of oil generation, and of about 50% the peak of oil generation.

# 7. $C_{29} \alpha \beta \beta / C_{29} \alpha \alpha \alpha + C_{29} \alpha \beta \beta$ steranes

Maturity indicator. The  $\alpha\alpha$  form is produced biologically. Its abundance diminishes upon maturation until a mixture of 65%  $\beta\beta$  (iso) steranes and 35%  $\alpha\alpha$  (normal) steranes is reached, which is equivalent to approximately 0.9%  $V_{B}$ .

# 8&9. $C_{27}/C_{29}$ diasteranes and steranes

Source indicator. It has been suggested that marine phytoplankton is characterised by a dominance of  $C_{27}$  steranes and diasteranes whereas a preponderance of  $C_{29}$  compounds indicates strong terrestrial contributions. Values smaller than 0.85 for  $C_{27}/C_{29}$  diasterane and sterane ratios are believed to be indicative for terrestrial organic matter, values between 0.85 and 1.43 for mixed organic material, and values greater than 1.43 for an input of predominantly marine organic matter.

It has been suggested, however, that marine sediments can also contain a predominance of  $C_{29}$  steranes, so the above rules have to be applied with caution. Any simplistic interpretation of  $C_{27}/C_{29}$  steranes and diasteranes can be dangerous and the interpretation of these data should be consistent with other geological evidence.

### 10. $18\alpha$ (H) - oleanane/ $C_{30}$ hopane

<u>Source</u> indicator. Oleanane is a triterpenoid compound which has often been reported from deltaic sediments of Late Cretaceous to Tertiary age. It is thought to be derived from certain angiosperms which developed in the late Cretaceous. If the  $18\alpha$  (H) - oleanane/ $C_{30}$  hopane ratio is below 10, no significant proportions of oleanane are present. At higher values, it can be used as indicator for a reducing environment during deposition of land plant-derived organic matter.

# 11. $C_{29}$ diasteranes/ $C_{29}$ $\alpha\alpha\alpha$ steranes + $C_{29}$ $\alpha\beta\beta$ steranes

<u>Source</u>, indicator. This parameter is used to characterise the oxidity of depositional environments. High values (up to 10) indicate oxic conditions, low values (down to 0.1) indicate reducing environments.

## 12. C₃₀ (hopanes + moretanes)/C₂₉ (steranes + diasteranes)

<u>Source</u> indicator. Triterpanes are believed to be of prokariotic (bacterial) origin, whereas steranes are derived from eukariotic organisms. This ratio reflects the preservation of primary organic matter derived from eukariots, relative to growth and preservation of bacteria in the sediment after deposition.

#### 13. C₁₅ drimane/C₁₆ homodrimane

Drimanes and homodrimanes are ubiquitous compounds most likely derived from microbial activity in sediments. The  $C_{15}$  drimane/ $C_{16}$  homodrimane ratio is a useful parameter for <u>correlation</u> purposes in the low molecular weight region, especially for condensates which lack most conventional biomarkers. Drimanes are also useful to assess the degree of biodegradation as the removal of  $C_{15}$  to  $C_{16}$  bicyclics characterises an extensive level of biodegradation.

#### 14. Rearranged/normal drimanes

Like parameter 13, this ratio can be used for <u>correlation</u> purposes in samples without conventional biomarkers, and to assess levels of biodegradation.

# 15. $C_{15}$ alkylcyclohexane/ $C_{16}$ homodrimane

Like parameters 13 and 14, this ratio is useful for correlation purposes.

#### 2.3.5.2 GC/MS Analysis of Aromatics

The aromatic fraction or the oil to be analysed is first subjected to thin layer chromatography (TLC) or medium pressure liquid chromatography (MPLC), depending upon the analytical requirements.

1. Di- and tri- nuclear aromatic compounds are isolated by TLC. To effect this separation, the sample is applied to an alumina coated glass plate (0.6mm thickness). The plate is developed with hexane and the required band located using short wavelength UV light. The fraction is recovered by extraction and fractional distillation.

This aromatic fraction may be analysed by GC-FID, but GC/MS is recommended because of possible co-elution problems during GC.

Samples are analysed by GC/MS in the aquire mode scanning from 50 to 450 atomic mass units (amu).

#### Analytical conditions are:

Instrument:

**HP5970 MSD** 

Column:

60m x 0.25mm ID, 0.25 micron film thickness, 5% phenylmethyl

silicone column DB-5 (J&W) connected directly to the ion source

Injector:

automatic on-column

Carrier Gas:

helium

Over Conditions 70%

Oven Conditions:70°C for 1min

70°C --> 300°C at 3°/min

Data collection commences at 10 mins

Mass Spectrometry

Em Voltage

1500 - 1800V

Electron Energy

70eV

Mass fragmentograms are presented for alkylbiphenyls, alkylnaphthalenes, alkylfluorenes and alkylphenanthrenes from a comprehensive data base. Aromatic compounds provide valuable information concerning thermal maturity since they can be applied outside the dynamic range of saturate biomarker indicators and are particularly useful when conventional biomarkers are present in low amounts (Radke & Welte, 1983; Alexander et al, 1985). Maturity ratios are tabled below:

#### **Aromatic Maturity Indicators**

		Ra	ange
Abbrev.	Definition	oil onset	wet gas
DNR 1	(2,6DMN + 2,7DMN)/1,5DMN	1.5	10
DNR 2	2,7DMN/1,8DMN	50	2500
DNR 5	1,6DMN/1,8DMN	50	>3000
DNR 6	(2,6DMN + 2,7DMN)/(1,4DMN + 2,3 DMN)	0.8	2
TNR 1	(1,4,6TMN + 1,3,5TMN)/2,3,6TMN	0.5	4
MPR 1	(2MP + 3MP)/1MP	1.5	3
MPI 1	$1.5 \times (2MP + 3MP)/(PH + 1MP + 9MP)$	0.3	1
MPI 2	$(3 \times 2MP)/(PH + 1MP + 9MP)$	0.3	2
Rc(a) Rc(b)	0.6 (MPI-1) + 0.4 (for % Rm < 1.35) -0.6 (MPI-1) + 2.3 (for % Rm ≥1.35)		

(from Radke et al, 1982; Radke & Welte, 1983; Alexander et al, 1985)

Some aromatic marker compounds have specific natural product precursors and can be used as signatures for sediments of a particular source, depositional environment or geological age:

TNR 5

1,2,5TMN/1,3,6TMN

TNR 6

1,2,7TMN/1,3,7TMN

(Strachan et al, 1988)

1,7/X

1,7DMP/(1,3 + 3,9 + 2,10 + 3,10 DMP)

Retene/9MP

1MP/9MP

(Alexander et al, 1988)

2. Mono- and triaromatic steranes are analysed by GC/MS under the same analytical conditions as used for di- and tri-nuclear aromatics. However, isolation of this fraction is performed by MPLC. To achieve this, the saturate plus aromatic mixture is injected onto a Merck Si60 column. The separation is monitored with a refractive index detector for saturates and a UV absorbance detector for aromatics.

As aromatic steranes are generally present in low abundances, especially in oils, samples are analysed in the SIM mode and 16 ions are recorded.

The conversion of monoaromatic steranes to triaromatic steranes and the dimethylation of triaromatic steranes in sediments are considered to be maturity dependent (Mackenzie et al, 1981; Mackenzie, 1984). The triaromatic sterane maturity indicator should, however, not be applied to crude oils because migration effects appear to selectively deplete the triaromatic steranes.

#### 4.0 RECOMMENDED LITERATURE

ALEXANDER R., KAGI R.I., ROWLAND S.J., SHEPPARD P.N. and CHIRILA T.V. (1985) The effects of thermal maturity on distributions of dimethylnaphthalenes and trimethylnaphthalenes in some ancient sediments and petroleum. Geochim.Cosmochim.Acta 49, 385-395.

ALEXANDER R., KAGI R.I. and NOBLE R.A. (1987) Fossil resin biomarkers and their application in oil to source-rock correlation, Gippsland Basin, Australia. APEA J. 27, 63-72.

ALEXANDER R., LARCHER A.V., KAGI R.I. and PRICE P.L. (1988) The use of plant-derived biomarkers for correlation of oils with source rocks in the Cooper/Eromanga Basin system, Australia. <u>APEA J</u> 28, 310-324.

ALEXANDER R., MARZI R. and KAGI R.I. (1990) A new method for assessing the thermal history of sediments: A case study from the Exmouth Plateau in north Western Australia. <u>APEA J.</u>, 30, 364-372.

CUMBERS K.M., ALEXANDER R. and KAGI R.I. (1987) Methylbiphenyl, ethylbiphenyl and dimethylbiphenyl isomer distributions in some sediments and crude oils. <u>Geochem.Cosmochim.Acta</u> **51**, 3105-3111.

DEMBRICKI H., HORSFIELD B. and HO T.T.Y (1983) Source rock evaluation by pyrolysisgas chromatography. AAPG Bull, 67, 1094-1103.

DIDYK B.M., SIMONEIT B.R.T, BRASSELL S.C. and EGLINTON G. (1978) Organic geochemical indicators of palaeoenvironmental conditions of sedimentation. <u>Nature</u>, **272**, 216-222.

ESPITALIE' J., LAPORT J.L., MADEC M., MARQUIS F., LEPLAT P., PAULET J. and BOUTEFEU A. (1977) Méthode rapide de caractérisation des roches méres, de leur potential pétrolier et de leur degré d'évolution. <u>Rev.Inst.</u>, 32, 23-43.

FUEX A.N. (1977) The use of stable carbon isotopes in hydrocarbon exploration. <u>J.Geochem.Expl.</u>, 7, 155-188.

GRANTHAM P.J., POSTHUMA J. and BAAK A. (1983) Triterpanes in a number of Far-Eastern Crude Oils. In Advances in Organic Geochemistry, 1981 (eds. M.Bjorøy et al), pp 675-683. Wiley & Sons.

HORSFIELD B. (1984) Pyrolysis studies and petroleum exploration. In <u>Advances in Petroleum Geochemistry, Vol 1</u> pp 247-292. Academic Press.

HUNT J.M. (1979) <u>Petroleum Geochemistry and Geology</u>. pp 488-491. W.H. Freeman & Co, San Francisco.

LARTER S.R. (1985) Integrated kerogen typing in the recognition and quantitative assessment of petroleum source rocks. In <u>Petroleum Geochemistry in Exploration of the Norwegian Shelf</u>, pp 269-286. Graham and Trotman, London.

LARTER S.R. (1989) Chemical models of vitrinite reflectance evolution. <u>Geologische Rundschau 78/1</u>, 349-355, Stuttgart.

LARTER S.R. and DOUGLAS A.G. (1980) A pyrolysis-gas chromatographic method for kerogen typing. In <u>Advances in Organic Geochemistry</u>, 1979 (eds. A.G. Douglas and J.R. Maxwell), pp 579-584. Pergamon Press, Oxford.

LARTER S.R. and SENFTLE J.T. (1985) Improved kerogen typing for petroleum source rock analysis. Nature, 318, 277-280.

LE TRAN K., CONNAN J. and VAN DER WEIDE B. (1974) Diagenesis of organic matter and occurrence of hydrocarbons and hydrogen sulphide in the S.W. Aquitaine Basin. Bull.Centre.Rech. Pau-SNPA, 8, 111.

MACKENZIE A.S. (1984) Applications of biological markers in petroleum geochemistry. In <u>Advances in Petroleum Geochemistry</u>, 1984 (eds. J.Brooks and D.Welte), pp 115-214. Academic Press.

MACKENZIE A.S., BRASSELL S.C., EGLINTON G. and MAXWELL J.R. (1982) Chemical fossils: the geological fate of steroids. <u>Science</u>, **217**, 491-504.

MACKENZIE A.S., HOFFMANN C.F. and MAXWELL J.R. (1981) Molecular parameters of maturation in the Toarcian Shales, Paris Basin, France- III. Changes in aromatic steroid hydrocarbons. <u>Geochim.Cosmochim.Acta</u> 45, 1345-1355.

MUKHOPADHYAY P.K. (1989) Characterisation of amorphous and other organic matter types by microscopy and pyrolysis-gas chromatography. <u>Org Geochem</u>, **14**, 269-284.

PETERS K.E. (1986) Guidelines for evaluating petroleum source rock using programmed pyrolysis. <u>AAPG Bull</u>, 70, 318-329.

PHILIPPI G.T. (1974) The influence of marine and terrestrial source material on the composition of petroleum. <u>Geochim.Cosmochim.Acta</u> 38, 947.

RADKE M., WELTE D.H. and WILLSCH H. (1982) Geochemical study on a well in the Western Canada Basin: relation of the aromatic distribution pattern to maturity of organic matter. Geochim.Cosmochim.Acta 46, 1-10.

RADKE M. and WELTE D.H. (1983) The methylphenanthrene Index (MPI): a maturity parameter based on aromatic hydrocarbons. In <u>Advances in Organic Geochemistry</u>, 1981 (eds. M.Bjorøy et al), pp 504-512. Wiley & Sons.

SIEFERT W.K. and MOLDOWAN J.M. (1978) Applications of steranes, terpanes and monoaromatics to the maturation, migration and source of crude oils. Geochim.Cosmochim.Acta, 42, 77-95.

STAHL W.J. (1977) Carbon and nitrogen isotopes in hydrocarbon research and exploration. Chem. Geol., 20, 121-149.

STRACHAN M.G., ALEXANDER R. and KAGI R.I. (1988) Trimethylnaphthalenes in crude oils and sediments: Effects of source and maturity. <u>Geochim.Cosmochim.Acta</u>, 52, 1255-1264.

STRACHAN M.G., ALEXANDER R., SUBROTO E.A. and KAGI R.I. (1989) Constraints upon the use of 24-ethylcholestane diastereomer ratios as indicators of the maturity of petroleum. Org Geochem, 14, 423-432.

SUMMONS R.E., VOLKMAN J.K. and BOREHAM C.J. (1987) Dinosterane and other steroidal Hydrocarbons of dinoflagellate origin in sediments and petroleum. Geochim.Cosmochim.Acta, 51, 3075-3082.

THOMPSON K.F.M. (1979) Light hydrocarbons in subsurface sediments. <u>Geochim.Cosmochim.Acta</u>, **43**, 657-672.

THOMPSON K.F.M. (1983) Classification and thermal history of petroleum based on light hydrocarbons. <u>Geochim.Cosmochim.Acta</u>, 47, 303-316.

TISSOT B.P. and WELTE D.H. (1978) <u>Petroleum Formation and Occurrence</u>. Springer-Verlag pp 442-447.

VAN AARSSEN B.G.K., COX H.C., HOOGENDOORN P. and DE LEEUW J.W. (1990) A cadinene biopolymer present in Fossil and extant dammer resins as a source for cadinanes and bicadinanes in crude oils from South east Asia. <u>Geochim.Cosmochim.Acta</u> In press.

VAN GRAAS G., DE LEEUW J.W. and SHENK P.A. (1980) Analysis of coals of different ranks by Curie-point pyrolysis-gas chromatography - mass spectrometrey and Curie-point pyrolysis-mass spectrometry. In <u>Advances in Organic Geochemistry</u>, 1979 (eds. A.G. Douglas and J.R. Maxwell), p 485. Pergamon Press, Oxford.

VOLKMAN J.K., ALEXANDER R., KAGI R.I., NOBLE R.A. and WOODHOUSE G.W. (1983) A geochemical reconstruction of oil generation in the Barrow Sub-Basin of Western Australia. Geochim.Cosmochim.Acta, 47, 2091-2105

VOLKMAN J.K. (1986) A review of sterol markers for marine and terrigenous organic matter. Org. Geochem 9, 83-99.

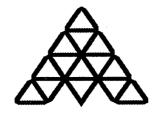
ZUMBERGE J. (1987) Prediction of source rock characteristics based on terpane biomarkers in crude oils: A multivariate statistical approach. <u>Geochim.Cosmochim.Acta</u>, 51, 1625-1637.

# APPENDIX 9

# **APPENDIX 9**

# **DIRECTIONAL DRILLING REPORT**

IONA-2



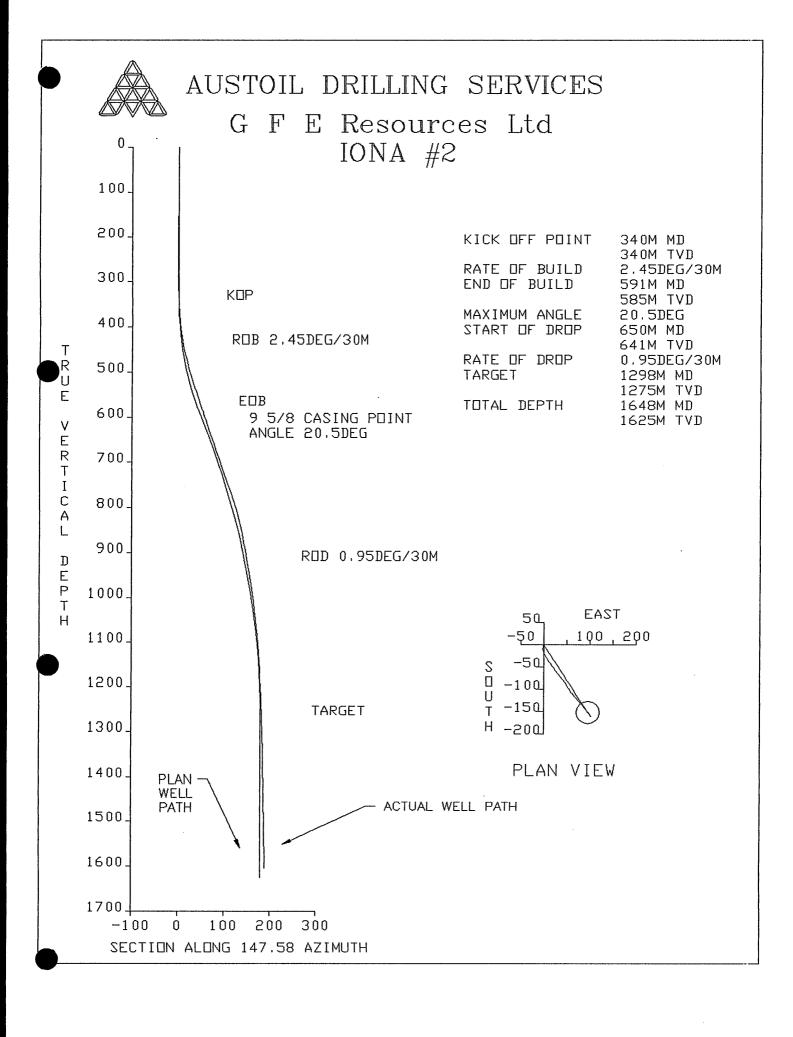
# **AUSTOIL DRILLING SERVICES PTY LTD**

ACN 088 963 835

# **G.F.E.RESOURCES LTD**

IONA 2

DIRECTIONAL DRILLING REPORT





# AUSTOIL DRILLING SERVICES G F E Resources Ltd IONA #2

KICK OFF POINT

RATE OF BUILD

END OF BUILD

MAXIMUM ANGLE START OF DROP

RATE OF DROP

TARGET

TOTAL DEPTH

340M MD

340M TVD

2.45DEG/30M

591M MD

585M TVD

20.5DEG 650M MD

641M TVD

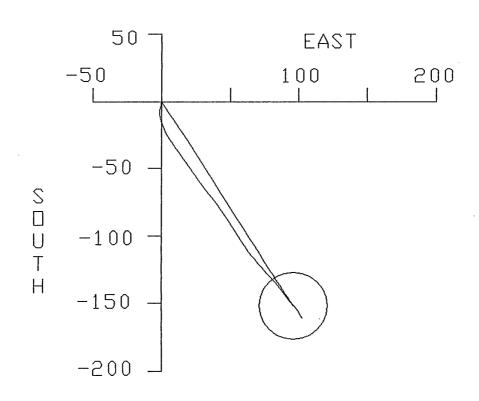
0.95DEG/30M

1298M MD

1275M TVD

1648M MD

1625M TVD



PLAN VIEW

FIDNAME: IONA COMPANY : GFE RESOURCES LTD SURVEY TYPE: DIFINITIVE FILENAME: IONA2 MAGNETIC DECL. : 10.74 DEG. VERTICAL SECTION AZIMUTH: 147.58 DEG. REC INS MD INCL AZIM NORTH EAST TVD DLS/ V/SECT NUM TYP METRES----DEG----DEG----METRES----METRES----30M---METRES o.j Dear 45.0 K.10 4 4 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 1 MW 2 MW 302.00 0.20 354.80 0.52 -0.05 302.00 0.02 -0.473 MW 317.00 0.40 193.60 0.50 -0.06 317.00 1.19 -0.464 MW -0.38 326.00 1.20 199.40 0.38 -0.10326.00 2.68 2.30 5 MW 336.00 197.00 0.09 -0.19335.99 3.31 -0.186 MW 355.00 4.70 194.30 -1.03-0.50354.96 3.80 0.60 7 MW -1.88 -0.70364.92 1.89 365.00 5.30 192.10 1.21 8 MW 374.00 5.80 190.60 -2.73-0.87373.88 1.74 1.84 9 MW 384.00 6.10 190.40 -3.75-1.06383.82 0.90 2.60 10 MW 393.00 6.70 188.90 -4.74-1.22392.77 2.08 3.34 -6.00 11 MW 403.00 7.90 187.30 -1.40402.69 3.65 4.31 12 MW 413.00 9.10 184.40 -7.47-1.55412.58 3.82 5.47 13 MW 422.00 10.10 179.80 -8.97 -1.60421.45 4.20 6.71 11.90 14 MW 440.10 441.00 167.00 -12.54 -1.15 4.77 9.97 15 MW 461.00 14.80 159.90 -16.95 0.19 459.56 4.99 14.41 -19.14 16 MW 470.00 15.40 158.30 1.02 468.25 2.44 16.71 17 MW 480.00 15.50 155.50 -21.59 2.07 477.89 2.26 19.34 18 MW 489.00 15.70 150.80 -23.75 3.16 486.56 4.26 21.74 15.80 19 MW 499.00 148.60 -26.09 4.53 496.18 1.82 24.45 20 MW 509.00 16.10 148.20 -28.435.97 505.80 0.96 27.20 21 MW 518.00 16.00 148.40 -30.557.28 514.45 0.38 29.69 22 MW 528.00 16.40 147.10 -32.918.77 524.05 1.62 32.48 23 MW 538.00 17.60 145.90 -35.35 10.38 533.61 3.75 35.4C MW 548.00 18.40 145.20 -37.8912.13 543.12 2.49 38.49 MW 558.00 18.70 145.00 -40.5013.95 552.60 0.92 41.67 567.00 18.70 26 MW 144.90 -42.8615.61 561.13 0.11 44.55 27 MW 18.90 577.00 145.00 -45.5017.46 570.59 47.77 0.61 28 MW 586.00 18.70 145.20 -47.8819.12 579.11 0.70 50.67 145.40 29 MW 596.00 18.70 -50.52 0.19 20.94 588.59 53.87 30 MW 604.00 18.50 145.20 -52.6222.40 596.17 0.79 56.42 31 MW 614.00 18.20 143.80 -55.18 24.22 605.66 1.60 59.57 25.72 32 MW 622.00 18.50 143.10 -57.20 613.25 1.40 62.08 33 SS 660.00 17.75 142.47 -66.62 32.87 649.37 0.61 73.86 34 SS 698.00 18.25 142.47 -75.93 40.03 685.51 0.39 85.55 35 SS 736.00 19.25 145.41 -85.80 47.21 721.49 1.09 97.74 36 SS 774.00 20.00 150.00 -96.59 54.01 757.29 1.35 110.49 19.70 37 MW 786.00 149.10 -100.10 56.08 768.57 1.07 114.57 WM 795.00 18.50 57.61 777.08 4.07 117.51 148.40 -102.62MW 805.00 17.30 145.90 -105.2059.27 786.59 4.27 120.58 795.20 123.21 40 MW 814.00 16.70 145.40 -107.3860.75 2.06

		E : IONA : IONA2					PANY : GFE VEY TYPE: D		RCES LTD
MAG	NETIC	DECL. :	10.74 D	EG.	VER'	TICAL SECT	ION AZIMUTH	: 147	.58 DEG.
REC	INS	MD	INCL	AZIM	NORTH	EAST	TVD	DLS/	
V/S	ECT								
MUM	TYP	METRES-	DEG-	DEG-	METRES-	METRES	METRES	30M-	METRES
41	MW	824.00	16.20	145.60	-109.71	62.36	804.79	1.51	126.04
42	MW	833.00	15.50	144.50	-111.72	63.77	813.45	2.54	128.50
43	MW	853.00	12.90	139.20	-115.59	66.78	832.84	4.36	133.38
44	MW	862.00	12.80	138.90	-117.10	68.09	841.61	0.40	135.36
45	MW	872.00	12.40	139.10	-118.75	69.52	851.37	1.21	137.51
	MW	881.00	11.80	138.20	-120.17	70.77	860.17	2.10	139.38
	MW	891.00	11.50	138.70	-121.68	72.11	869.96	0.95	141.37
	MW	900.00	11.10	137.50	-122.99	73.28	878.79	1.55	143.11
	MW	919.00	10.80	139.20	-125.69	75.68	897.44	0.70	146.67
5	MW	928.00	10.80	139.40	<b>-</b> 126 <b>.</b> 96	76.78	906.28	0.12	148.34
<b>5</b> 1	MW	938.00	10.40	138.70	-120 25	77 00	016 11	1 26	150 16
	MW	947.00	10.40	138.70	-128.35 -129.55	77.99 79.04	916.11	1.26	150.16
	MW	957.00	10.00	138.00	-129.55 -130.85		924.97	1.33	151.73
	MW	967.00				80.19	934.82	0.36	153.45
	MW	976.00	9.70 9.60	137.70	-132.12	81.34	944.67	0.91	155.13
55	14144	976.00	9.60	139.90	-133.25	82.33	953.55	1.27	156.62
56	MW	986.00	9.20	140.10	-134.50	83.38	963.41	1.20	158.24
57	WM	996.00	9.20	141.20	-135.74	84.40	973.28	0.53	159.83
58	MW	1005.00	8.90	142.40	-136.85	85.27	982.17	1.18.	161.24
59	MW	1015.00	8.50	142.40	-138.05	86.20	992.05	1.20	162.74
60	MW	1024.00	8.20	143.10	-139.09	86.99	1000.96	1.06	164.05
61	ММ	1052.00	7.00	144.00	-142.07	89.19	1028.71	1.29	167.74
	MM	1071.00	6.50	144.00	-142.07 -143.87	90.50	1047.58	0.79	167.74
	MM	1090.00		145.00	-145.56	91.70			
	MM	1109.00	5.25	141.00	-147.05		1066.47	0.81	172.04
	MM	1129.00	4.50	139.00	-147.05 -148.35	92.82	1085.38	1.34	173.89
65	MM	1129.00	4.50	139.00	-148.35	93.91	1105.30	1.15	175.58
66	MM	1148.00	4.00	138.00	-149.40	94.84	1124.25	0.80	176.97
67	MM	1167.00	3.50	135.00	-150.31	95.70	1143.21	0.85	178.19
68	MM	1187.00	3.00	136.00	-151.11	96.49	1163.18	0.75	179.29
69	MM	1206.00	2.75	141.00	-151.83	97.13	1182.16	0.56	180.23
70	MM	1225.00	2.75	144.00	-152.55	97.68	1201.13	0.23	181.14
71	MM	1244.00	2.75	140.00	-153.27	98.24	1220.11	0.30	182.05
	MM	1264.00	2.50	141.00	-153.27 -153.97	98.82	1240.09	0.38	
	MM	1283.00	2.25	145.00	-154.60	99.30		0.38	182.96
	MM	1301.00	2.23	150.00	-154.60 -155.16	99.66	1259.07 1277.06	0.47	183.74 184.41
	MM	1301.00	1.75	148.00	-155.16 -155.72	99.66	1297.05	0.32	184.41
, 5	THI	T22T.00	1.75	T40.00	- IJJ • /2	99.33	129/.00	0.39	TC 2.00
76	MM	1340.00	1.50	153.00	-156.19	100.26	1316.04	0.45	185.60
72	MM	1359.00	1.25	160.00	-156.61	100.44	1335.04	0.47	186.05
75	MM	1377.00	1.25	161.00	-156.98	100.58	1353.03	0.04	186.43
79	MM	1397.00	1.25	159.00	-157.39	100.73	1373.03	0.07	186.86
80	MM	1417.00	1.25	153.00	<del>-</del> 157.79	100.90	1393.02	0.20	187.29

LDNAME : IONA COMPANY : GFE RESOURCES LTD FILENAME: IONA2 SURVEY TYPE: DIFINITIVE MAGNETIC DECL. : 10.74 DEG. VERTICAL SECTION AZIMUTH: 147.58 DEG. REC INS MDINCL AZIM NORTH EAST TVD DLS/ V/SECT NUM TYP METRES----DEG----METRES----METRES----METRES----30M---METRES 81 MM 1435.00 1.25 148.00 -158.13101.10 1411.02 0.18 187.68 82 MM 1455.00 1.25 151.00 -158.50 101.32 1431.02 0.10 188.12 83 MM 1.00 151.00 0.39 1474.00 -158.83 101.50 1450.01 188.49 84 MM 1493.00 1.00 145.00 -159.11 101.67 1469.01 0.17 188.82 85 MM 1512.00 1.00 151.00 -159.39 101.85 1488.01 0.17 189.15 86 MM 1531.00 1.00 151.00 -159.68 102.01 1507.00 0.00 189.48 87 MM 1550.00 0.75 154.00 -159.94102.14 0.40 189.77 1526.00 88 MM 1570.00 0.75 149.00 -160.17102.27 1546.00 0.10 190.03 89 MM 1589.00 0.75 141.00 -160.37102.41 0.17 1565.00 190.28 90 MM 1608.00 0.75 143.00 -160.57102.56 1584.00 0.04 190.53 91 MM 1627.00 0.75 148.00 -160.77 102.71 1602.99 0.10 190.78 92 PR 1650.00 0.75 136.00 -161.01 102.89 0.20 1625.99 191.07

Surveys computed using the MINIMUM CURVATURE method..

: GFE RESOUCES LTD LDNAME: IONA COMPANY SURVEY TYPE : SINGLESHOT FILENAME: IONA2 MAGNETIC DECL. : 10.74 DEG. VERTICAL SECTION AZIMUTH: 147.58 DEG. DLS/ REC INS MD INCL NORTH EAST TVD V/SECT AZIM NUM TYP METRES----DEG----METRES----METRES----METRES----30M---METRES 1 MW 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 2 MW 302.00 0.20 354.80 0.52 -0.05 302.00 0.02 -0.47317.00 1.19 3 MW 0.40 193.60 0.50 -0.06 317.00 -0.464 MW 326.00 1.20 199.40 0.38 -0.10326.00 2.68 -0.38 5 MW 2.30 336.00 197.00 0.09 -0.19335.99 3.31 -0.18 6 MW 355.00 4.70 194.30 -1.03-0.50 354.96 3.80 0.60 7 MW 365.00 5.30 192.10 -1.88 -0.70364.92 1.89 1.21 MW 374.00 5.80 190.60 -2.73-0.87 1.74 8 373.88 1.84 9 MW 384.00 6.10 190.40 -3.75-1.06383.82 0.90 2.60 10 MW 393.00 6.70 188.90 -4.74-1.22392.77 2.08 3.34 11 MW 403.00 7.90 187.30 -6.00 -1.40402.69 3.65 4.31 12 MW 413.00 9.10 184.40 -7.47-1.55412.58 3.82 5.47 10.10 13 MW 422.00 179.80 -8.97 421.45 6.71 -1.604.20 11.90 14 MW 441.00 167.00 -12.54-1.15 440.10 4.77 9.97 15 MW 461.00 14.80 159.90 **-16.95** 0.19 459.56 4.99 14.41 16 MW 470.00 15.40 158.30 -19.14 1.02 468.25 16.71 2.44 17 MW 480.00 15.50 155.50 -21.592.07 477.89 2.26 19.34 489.00 15.70 150.80 -23.75 3.16 4.26 21.74 18 MW 486.56 19 MW 499.00 15.80 148.60 -26.09 4.53 496.18 1.82 24.45 20 MW 509.00 16.10 148.20 -28.435.97 505.80 0.96 27.20 21 MW 518.00 16.00 148.40 -30.55 7.28 514.45 0.38 29.69 22 MW 528.00 16.40 147.10 -32.918.77 524.05 1.62 32.48 23 MW 538.00 17.60 145.90 -35.3510.38 533.61 3.75 35.40 MW 548.00 18.40 -37.89145.20 12.13 543.12 2.49 38.49 MW 18.70 558.00 145.00 -40.5013.95 552.60 0.92 41.67 26 MW 567.00 18.70 144.90 -42.8615.61 561.13 0.11 44.55 27 MW 577.00 18.90 145.00 -45.5017.46 570.59 0.61 47.77 28 MW 586.00 18.70 145.20 -47.8819.12 579.11 0.70 50.67 29 MW 596.00 18.70 145.40 -50.52 20.94 588.59 0.19 53.87 30 MW 604.00 18.50 145.20 -52.62 22.40 596.17 0.79 56.42 31 MW -55.18 614.00 18.20 143.80 24.22 605.66 1.60 59.57 32 MW 622.00 18.50 143.10 -57.20 25.72 613.25 1.40 62.08 33 SS 660.00 17.75 142.47 32.87 -66.62 649.37 0.61 73.86 34 SS 698.00 18.25 142.47 -75.93 40.03 685.51 0.39 85.55 35 SS 97.74 736.00 19.25 145.41 -85.80 47.21 721.49 1.09 36 SS 774.00 20.00 150.00 -96.59 54.01 757.29 1.35 110.49 37 MW 786.00 19.70 149.10 -100.1056.08 768.57 1.07 114.57 MW 795.00 18.50 148.40 -102.6257.61 777.08 4.07 117.51 MW 805.00 17.30 145.90 -105.2059.27 786.59 4.27 120.58 795.20 2.06 16.70 40 MW 814.00 145.40 -107.3860.75 123.21

	ME : IONA				COI	MPANY : G	FE RESO	UCES LTD
FILENAM						SURVEY TY		
	C DECL. :	10.74 E			CICAL SECT	ION AZIMUTI	H : 147	.58 DEG.
REC INS		INCL	AZIM	NORTH	EAST T			
•			DEG	DEGM	IETRESI	METRES		
METRES-	30MN	IETRES						
41 MW	824.00	16.20	145 60	100 71	60.06	004 50		
41 MW 42 MW			145.60	-109.71	62.36	804.79	1.51	126.04
	833.00	15.50	144.50	-111.72	63.77	813.45	2.54	128.50
43 MW	853.00	12.90	139.20	-115.59	66.78	832.84	4.36	133.38
44 MW	862.00	12.80	138.90	-117.10	68.09	841.61	0.40	135.36
45 MW	872.00	12.40	139.10	-118.75	69.52	851.37	1.21	137.51
46 MW	881.00	11.80	138.20	-120.17	70.77	860.17	2.10	139.38
47 MW	891.00	11.50	138.70	-121.68	72.11	869.96	0.95	141.37
48 MW	900.00	11.10	137.50	-122.99	73.28	878.79	1.55	143.11
49 MW	919.00	10.80	139.20	-125.69	75.68	897.44	0.70	146.67
WM C	928.00	10.80	139.40	-126.96	76.78	906.28	0.12	148.34
			107.10	120.30	70.70	500.20	0.12	140.34
51 MW	938.00	10.40	138.70	-128.35	77.99	916.11	1.26	150.16
52 MW	947.00	10.00	138.70	-129.55	79.04	924.97	1.33	151.73
53 MW	957.00	10.00	138.00	-130.85	80.19	934.82	0.36	153.45
54 MW	967.00	9.70	137.70	-132.12	81.34	944.67	0.91	155.13
55 MW	976.00	9.60	139.90	-133.25	82.33	953.55	1.27	156.62
56 MW	986.00	9.20	140.10	-134.50	83.38	963.41	1.20	158.24
57 MW	996.00	9.20	141.20	-135.74	84.40	973.28	0.53	159.83
58 MW	1005.00	8.90	142.40	<b>-</b> 136.85	85.27	982.17	1.18	161.24
59 MW	1015.00	8.50	142.40	-138.05	86.20	992.05	1.20	162.74
60 MW	1024.00	8.20	143.10	-139.09	86.99	1000.96	1.06	164.05
		-						
61 SS	1096.00	5.50	140.74	-145.87	92.26	1072.44	1.13	172.59
62 SS	1165.00	3.75	136.00	-150.05	95.92	1141.21	0.78	178.09
63 SS	1250.00	2.50	143.00	-153.53	98.96	1226.08	0.46	182.66
Ss ss	1345.00	1.50	153.00	-156.30	100.77	1321.03	0.33	185.96
65 SS	1450.00	1.00	151.00	-158.32	101.84	1426.00	0.14	188.24
66 SS	1632.00	0.75	136.00	-160.57	103.44	1607.98	0.06	191.00
67 PR	1650.00	0.75	136.00	-160.74	103.44	1625.98	0.00	191.00
J. 110	1000.00	0.75	130.00	100.74	T02.00	1020.90	0.00	TAT. 72

Surveys computed using the MINIMUM CURVATURE method..

Hore: Moo useb his AUSTOIL DRILLING SERVICES Miles sir son oc

FIMONA	ME : IONA				COME	ANY : GFE	RESOU	RCES LTD
FILENAM		1				SURVEY TY	PE : M	ULTISHOT
	C DECL. :		EG.	VER!	TICAL SECTI	ON AZIMUTE	: 147	.58 DEG.
REC INS	MD	INCL	AZIM	NORTH	EAST	TVD	DLS/	V/SECT
NUM TYP	METRES-	DEG-	DEG-	METRES-	METRES	METRES	30M-	METRES
1 MW	622.00	18.50	143.10	-57.20	25.72	613.25	0.00	62.07
2 MM	648.00	17.75	142.00	-63.62	30.64	637.96	0.95	70.13
3 MM	668.00	18.00	142.00	-68.46	34.42	656.99	0.38	76.24
4 MM	688.00	18.25	143.00	-73.40	38.20	676.00	0.60	82.44
5 MM	707.00	19.00	144.00	-78.27	41.81	694.01	1.29	88.49
6 MM	726.00	19.25	145.00	-83.34	45.43	711.96	0.65	94.71
7 MM	764.00	20.00	150.00	-94.10	52.27	747.75	1.45	107.46
8 MM	783.00	19.00	149.00	-99.57	55.49	765.66	1.66	113.80
9 MM	802.00	17.00	146.00	-104.52	58.63	783.73	3.48	119.67
10 MM	821.00	15.75	146.00	-108.96	61.63	801.96	1.97	125.02
				444 ==				
11 MM	860.00	12.75	138.00	-116.55	67.47	839.76	2.76	134.56
12 MM	879.00	11.75	138.00	-119.55	70.17	858.33	1.58	138.53
13 MM	898,00	10.75	138.00	-122.30	72.65	876.96	1.58	142.19 145.60
14 MM	917.00	10.25	138.00	-124.87	74.96	895.64	0.79 0.39	148.90
15 MM	936.00	10.00	138.00	-127.36	77.20	914.35	0.39	140.90
16 MM	975.00	9.00	140.00	-132.21	81.43	952.81	0.81	155.26
10 MM	994.00	8.25	140.00	-134.39	83.26	971.60	1.18	158.08
17 MM 18 MM	1013.00	8.00	143.00	-136.49	84.93	990.41	0.78	160.75
19 MM		7.25	143.00	-138.51	86.45	1009.24	1.18	163.26
20 MM	1052.00	7.23	144.00	-140.50	87.92	1029.09	0.42	165.74
20 1111	1032.00	7.00	144.00	140.30	07.52	1025.05	0.12	100111
21 MM	1071.00	6.50	144.00	-142.31	89.24	1047.95	0.79	167.97
22 MM	1090.00	6.00	145.00	-143.99	90.44	1066.84	0.81	170.03
23 MM	1109.00	5.25	141.00	-145.48	91.55	1085.75	1.34	171.89
24_MM	1129.00	4.50	139.00	-146.78	92.64	1105.68	1.15	173.57
2 <b>9</b> MM	1148.00	4.00	138.00	-147.84	93.58	1124.62	0.80	174.96
26 MM	1167.00	3.50	135.00	-148.74	94.43	1143.58	0.85	176.18
27 MM	1187.00	3.00	136.00	-149.55	95.23	1163.55	0.75	177.29
28 MM	1206.00	2.75	141.00	-150.26	95.86	1182.53	0.56	178.23
29 MM	1225.00	2.75	144.00	-150.98	96.41	1201.51	0.23	179.14
30 MM	1244.00	2.75	140.00	-151.70	96.97	1220.48	0.30	180.05
31 MM	1264.00	2.50	141.00	-152.41	97.56	1240.46	0.38	180.96
32 MM	1283.00	2.25	145.00	-153.03	98.03	1259.45	0.47	181.74
33 MM	1301.00	2.00	150.00	-153.60	98.39	1277.43	0.52	182.41
34 MM	1321.00	1.75	148.00	-154.16	98.73	1297.42	0.39	183.06
35 MM	1340.00	1.50	153.00	-154.63	98.99	1316.42	0.45	183.60
2 (* 1838	1250 00	1 05	160 00	155_04	00 10	1225 41	0.47	184.05
36 MM	1359.00	1.25	160.00	-155.04 -155.41	99.18 99.31	1335.41 1353.41	0.47	184.43
37 MM 3 MM	1377.00 1397.00	1.25 1.25	161.00 159.00	-155.41 -155.82	99.46	1373.41	0.04	184.86
39 MM	1417.00	1.25	153.00	-156.22	99.48	1393.40	0.07	185.29
39-MM 40 MM	1417.00	1.25	148.00		99.83	1411.39	0.20	185.68
40 11111	1433.00	1.23	T40.00	T20.20	99.03	T4TT•33	0.10	100.00

FILENAME					COMF			RCES LTD ULTISHOT
MAGNETIC	DECL. :	11.00 D	EG.	VERT	ICAL SECTI	ON AZIMUTH	: 147	.58 DEG.
REC INS	MD	INCL	AZIM	NORTH	EAST	TVD	DLS/	V/SECT
NUM TYP	METRES-	DEG-	DEG-	METRES	METRES	METRES	30M-	METRES
41 MM	1455.00	1.25	151.00	-156.94	100.05	1431.39	0.10	186.12
42 MM	1474.00	1.00	151.00	-157.26	100.23	1450.38	0.39	186.49
43 MM	1493.00	1.00	145.00	-157.54	100.41	1469.38	0.17	186.82
44 MM	1512.00	1.00	151.00	-157.82	100.58	1488.38	0.17	187.15
45 MM	1531.00	1.00	151.00	-158.11	100.74	1507.37	0.00	187.48
46 MM	1550.00	0.75	154.00	-158.37	100.88	1526.37	0.40	187.77
47 MM	1570.00	0.75	149.00	-158.60	101.00	1546.37	0.10	188.03
48 MM	1589.00	0.75	141.00	-158.80	101.14	1565.37	0.17	188.28
49 MM	1608.00	0.75	143.00	-159.00	101.30	1584.37	0.04	188.53
50 MM	1627.00	0.75	148.00	-159.21	101.44	1603.37	0.10	188.77

Surveys computed using the MINIMUM CURVATURE method..

In:- bit-motor 1.15deg-stab-monel-hos-4*8"dc's-2*6 1/4"dc's-jar-12*6 1/4"dc's-6*hwdp					Date _	15/2/94
District Victoria Lease/Block Ken Smith Cont.T.P. Rick Giddens Contr. Century Drilling  DPERATIONS: Continue drilling 12 1/4" hole to 320m, taking totco surveys POOH and made up the kick off assembly — RIH to HWDP and tested equipment Continue RIH reaming from 293m to 305m Drilled deviated hole from 320m to 500m  Drilled deviated hole from 320m to 500m  BHA NO: out:-bit -dc-dc-stab-dc in:- bit-motor 1.15deg-stab-monel-hos-4*8*dc*s-2*6 1/4*dc*s-jar-12*6 1/4*dc*s-6*hwdp  Motor Make Sperry Drill Type 8* Adjustable Motor Ser. No.  Motor RPM 76 Press on btm 1575 psi Off btm 1450 psi Pressure Drop Across Bit 970 psi  Motor Usage Information Time In Hole 09:15 15/2/94 Out Depth In 320m Depth Out Footage  Bit Make Security (116) Type \$33SF Nozzles 16-16-16  Mud Weight 8.9ppg PV / YP 6/10 Vis 37 Sand tr Annula Vel. 28 / 48.2 m/min Gel  Drilling Parameters WOB 10,000 lbs RPM 77 Pump Press. 1450psi GPM 480  SURVEYS: NO. Depth Inc. Azim. REMARKS Formation very soft , having difficulty getting the	Company	GFE Resources	Country	Australia	Rep.No	#1
Continue drilling 12 1/4* hole to 320m , taking totco surveys  POOH and made up the kick off assembly – RIH to HWDP and tested equipment  Continue RIH reaming from 293m to 305m  Drilled deviated hole from 320m to 500m  BHA NO : out: -bit -dc-dc-stab-dc in: - bit-motor 1.15deg-stab-monel-hos-4*8*dc's-2*6 1/4*dc's-jar-12*6 1/4*dc's-6*hwdp Motor Make Sperry Drill Type 8*Adjustable Motor Ser. No.  Motor RPM 76 Press on btm 1575 psi Off btm 1450 psi Pressure Drop Across Bit 970 psi Motor Usage Information Time In Hole 09:15 15/2/94 Out Poeth In 320m Depth Out Footage  Bit Make Security (116) Type S33SF Nozzles 16-16-16  Mud Weight 8.9ppg PV / YP 6/10 Vis 37  Sand tr Annula Vel. 28 / 48.2 m/min Gel  Drilling Parameters WOB 10,000 lbs RPM 77  Pump Press. 1450psi GPM 480  SURVEYS:  NO. Depth Inc. Azim. REMARKS  Formation very soft , having difficulty getting the						
Continue drilling 12 1/4* hole to 320m , taking totco surveys  POOH and made up the kick off assembly — RIH to HWDP and tested equipment  Continue RIH rearning from 293m to 305m  Drilled deviated hole from 320m to 500m  BHA NO : out:—bit —dc—dc—stab—dc in:— bit—motor 1.15deg—stab—monel—hos—4*8*dc's—2*6 1/4*dc's—jar—12*6 1/4*dc's—6*hwdp  Motor Make Sperry Drill Type 8* Adjustable Motor Ser. No.  Motor RPM 76 Press on btm 1575 psi Off btm 1450 psi  Pressure Drop Across Bit 970 psi  Motor Usage Information Time In Hole 09:15 15/2/94 Out  Depth In 320m Depth Out Footage  Bit Make Security (116) Type S33SF Nozzles 16—16—16  Mud Weight 8.9ppg PV / YP 6/10 Vis 37  Sand tr Annula Vel. 28 / 48.2 m/min Gel  Drilling Parameters WOB 10,000 lbs RPM 77  Pump Press. 1450psi GPM 480  SURVEYS:  NO. Depth Inc. Azim. REMARKS  Formation very soft , having difficulty getting the	Co.Man	Ken Smith	Cont.T.P.	Rick Giddens	Contr.	Century Drilling
Continue drilling 12 1/4" hole to 320m , taking totco surveys  POOH and made up the kick off assembly — RIH to HWDP and tested equipment  Continue RIH rearning from 293m to 305m  Drilled deviated hole from 320m to 500m  BHA NO : out:-bit -dc-dc-stab-dc in:- bit-motor 1.15deg-stab-monel-hos-4*8*dc's-2*6 1/4*dc's-jar-12*6 1/4*dc's-6*hwdp Motor Make Sperry Drill Type 8* Adjustable Motor Ser. No.  Motor RPM 76 Press on btm 1575 psi Off btm 1450 psi Pressure Drop Across Bit 970 psi Motor Usage Information Time In Hole 09:15 15/2/94 Out Poeth In 320m Pepth Out Footage  Bit Make Security (116) Type S33SF Nozzles 16-16-16  Mud Weight 8.9ppg PV / YP 6/10 Vis 37  Sand tr Annula Vel. 28 / 48.2 m/min Gel  Drilling Parameters WOB 10,000 lbs RPM 77  Pump Press. 1450psi GPM 480  SURVEYS:  NO. Depth Inc. Azim. REMARKS  Formation very soft , having difficulty getting the		10.				
POOH and made up the kick off assembly — RIH to HWDP and tested equipment Continue RIH reaming from 293m to 305m  Drilled deviated hole from 320m to 500m  BHA NO : out:—bit —dc—dc—stab—dc in:— bit—motor 1.15deg—stab—monel—hos—4*8"dc's—2*6 1/4"dc's—jar—12*6 1/4"dc's—6*hwdp Motor Make Sperry Drill Type 8" Adjustable Motor Ser. No.  Motor RPM 76 Press on btm 1575 psi Off btm 1450 psi Pressure Drop Across Bit 970 psi Motor Usage Information Time In Hole 09:15 15/2/94 Out Depth In 320m Depth Out Footage  Bit Make Security (116) Type S33SF Nozzlet 16—16—16  Mud Weight 8.9ppg PV / YP 6/10 Vis 37 Sand tr Annula Vel. 28 / 48.2 m/min Gel  Drilling Parameters WOB 10,000 lbs RPM 77 Pump Press. 1450psi GPM 480  SURVEYS: NO. Depth Inc. Azim. REMARKS Formation very soft , having difficulty getting the	-		Om taking tota	O CLIDAGNE		
Continue RIH reaming from 293m to 305m					equinment	
Drilled deviated hole from 320m to 500m				OTIVDI and tested	equipment	
BHA NO : out: -bit -dc -dc -stab - dc     in: - bit -motor 1.15deg - stab - monel - hos - 4*8"dc's - 2*6 1/4"dc's - jar - 12*6 1/4"dc's - 6*hwdp     Motor Make   Sperry Drill   Type   8" Adjustable Motor   Ser. No.     Motor RPM   76   Press on btm   1575 psi   Off btm   1450 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Across Bit   970 psi     Pressure Drop Acciss   970 psi     Pressure Drop Acciss   970 psi     Pressure Drop Acciss   970 psi     Pressure Drop Acciss   970 psi     Pressure Drop Acciss   970 psi     Pressure Drop Acciss   970 psi     Pressure Drop Acciss   970 psi     Pressure Drop Acciss   970 psi     Pressure Drop Acciss   970 psi     Pressure Drop Acciss   970 psi     Pressure Drop Acciss   970 psi     Pressure Drop Acciss   970 psi     Pressure Drop						
Motor Make         Sperry Drill         Type         8" Adjustable Motor         Ser. No.           Motor RPM         76         Press on btm         1575 psi         Off btm         1450 psi           Pressure Drop Across Bit         970 psi           Motor Usage Information         Time In Hole         09:15         15/2/94         Out           Depth In         320m         Depth Out         Footage           Bit Make         Security (116)         Type         \$33SF         Nozzles         16-16-16           Mud Weight         8.9ppg         PV / YP         6/10         Vis         37           Sand         tr         Annula Vel.         28 / 48.2 m/min         Gel           Drilling Parameters         WOB         10,000 lbs         RPM         77           Pump Press.         1450psi         GPM         480   SURVEYS:  NO. Depth Inc. Azim.  REMARKS Formation very soft, having difficulty getting the		Diffica deviated field from 02011 to	300111			
in:- bit-motor 1.15deg-stab-monel-hos-4*8"dc's-2*6 1/4"dc's-jar-12*6 1/4"dc's-6*hwdp  Motor Make Sperry Drill Type 8" Adjustable Motor Ser. No.  Motor RPM 76 Press on btm 1575 psi Off btm 1450 psi  Pressure Drop Across Bit 970 psi  Motor Usage Information Time In Hole 09:15 15/2/94 Out  Depth In 320m Depth Out Footage  Bit Make Security (116) Type S33SF Nozzlet 16-16-16  Mud Weight 8.9ppg PV / YP 6/10 Vis 37  Sand tr Annula Vel. 28 / 48.2 m/min Gel  Drilling Parameters WOB 10,000 lbs RPM 77  Pump Press. 1450psi GPM 480  SURVEYS:  NO. Depth Inc. Azim. REMARKS  Formation very soft , having difficulty getting the						
in:- bit-motor 1.15deg-stab-monel-hos-4*8"dc's-2*6 1/4"dc's-jar-12*6 1/4"dc's-6*hwdp  Motor Make Sperry Drill Type 8" Adjustable Motor Ser. No.  Motor RPM 76 Press on btm 1575 psi Off btm 1450 psi  Pressure Drop Across Bit 970 psi  Motor Usage Information Time In Hole 09:15 15/2/94 Out  Depth In 320m Depth Out Footage  Bit Make Security (116) Type S33SF Nozzlet 16-16-16  Mud Weight 8.9ppg PV / YP 6/10 Vis 37  Sand tr Annula Vel. 28 / 48.2 m/min Gel  Drilling Parameters WOB 10,000 lbs RPM 77  Pump Press. 1450psi GPM 480  SURVEYS:  NO. Depth Inc. Azim. REMARKS  Formation very soft , having difficulty getting the						
in:- bit-motor 1.15deg-stab-monel-hos-4*8"dc's-2*6 1/4"dc's-jar-12*6 1/4"dc's-6*hwdp  Motor Make Sperry Drill Type 8" Adjustable Motor Ser. No.  Motor RPM 76 Press on btm 1575 psi Off btm 1450 psi  Pressure Drop Across Bit 970 psi  Motor Usage Information Time In Hole 09:15 15/2/94 Out  Depth In 320m Depth Out Footage  Bit Make Security (116) Type S33SF Nozzlet 16-16-16  Mud Weight 8.9ppg PV / YP 6/10 Vis 37  Sand tr Annula Vel. 28 / 48.2 m/min Gel  Drilling Parameters WOB 10,000 lbs RPM 77  Pump Press. 1450psi GPM 480  SURVEYS:  NO. Depth Inc. Azim. REMARKS  Formation very soft , having difficulty getting the	· · · · · · · · · · · · · · · · · · ·			<del></del>	* · · · · · · · · · · · · · · · · · · ·	
in:- bit-motor 1.15deg-stab-monel-hos-4*8"dc's-2*6 1/4"dc's-jar-12*6 1/4"dc's-6*hwdp  Motor Make Sperry Drill Type 8" Adjustable Motor Ser. No.  Motor RPM 76 Press on btm 1575 psi Off btm 1450 psi  Pressure Drop Across Bit 970 psi  Motor Usage Information Time In Hole 09:15 15/2/94 Out  Depth In 320m Depth Out Footage  Bit Make Security (116) Type S33SF Nozzlet 16-16-16  Mud Weight 8.9ppg PV / YP 6/10 Vis 37  Sand tr Annula Vel. 28 / 48.2 m/min Gel  Drilling Parameters WOB 10,000 lbs RPM 77  Pump Press. 1450psi GPM 480  SURVEYS:  NO. Depth Inc. Azim. REMARKS  Formation very soft , having difficulty getting the			· · · · · · · · · · · · · · · · · · ·			
in:- bit-motor 1.15deg-stab-monel-hos-4*8"dc's-2*6 1/4"dc's-jar-12*6 1/4"dc's-6*hwdp  Motor Make Sperry Drill Type 8" Adjustable Motor Ser. No.  Motor RPM 76 Press on btm 1575 psi Off btm 1450 psi  Pressure Drop Across Bit 970 psi  Motor Usage Information Time In Hole 09:15 15/2/94 Out  Depth In 320m Depth Out Footage  Bit Make Security (116) Type S33SF Nozzlet 16-16-16  Mud Weight 8.9ppg PV / YP 6/10 Vis 37  Sand tr Annula Vel. 28 / 48.2 m/min Gel  Drilling Parameters WOB 10,000 lbs RPM 77  Pump Press. 1450psi GPM 480  SURVEYS:  NO. Depth Inc. Azim. REMARKS  Formation very soft , having difficulty getting the						
in:- bit-motor 1.15deg-stab-monel-hos-4*8"dc's-2*6 1/4"dc's-jar-12*6 1/4"dc's-6*hwdp  Motor Make Sperry Drill Type 8" Adjustable Motor Ser. No.  Motor RPM 76 Press on btm 1575 psi Off btm 1450 psi  Pressure Drop Across Bit 970 psi  Motor Usage Information Time In Hole 09:15 15/2/94 Out  Depth In 320m Depth Out Footage  Bit Make Security (116) Type S33SF Nozzlet 16-16-16  Mud Weight 8.9ppg PV / YP 6/10 Vis 37  Sand tr Annula Vel. 28 / 48.2 m/min Gel  Drilling Parameters WOB 10,000 lbs RPM 77  Pump Press. 1450psi GPM 480  SURVEYS:  NO. Depth Inc. Azim. REMARKS  Formation very soft , having difficulty getting the						
Motor Make         Sperry Drill         Type         8" Adjustable Motor         Ser. No.           Motor RPM         76         Press on btm         1575 psi         Off btm         1450 psi           Pressure Drop Across Bit         970 psi           Motor Usage Information         Time In Hole         09:15         15/2/94         Out           Depth In         320m         Depth Out         Footage           Bit Make         Security (116)         Type         \$33SF         Nozzles         16-16-16           Mud Weight         8.9ppg         PV / YP         6/10         Vis         37           Sand         tr         Annula Vel.         28 / 48.2 m/min         Gel           Drilling Parameters         WOB         10,000 lbs         RPM         77           Pump Press.         1450psi         GPM         480   SURVEYS:  NO. Depth Inc. Azim.  REMARKS Formation very soft , having difficulty getting the	-					
Motor RPM   76		<b>o</b>			•	•
Motor Usage Information  Time In Hole 09:15 15/2/94 Out  Depth In 320m  Depth Out  Type S33SF  Nozzles 16-16-16  Mud Weight 8.9ppg  PV / YP 6/10  Sand tr  Annula Vel. 28 / 48.2 m/min  Drilling Parameters  WOB 10,000 lbs  PUMP Press. 1450psi  SURVEYS:  NO. Depth Inc. Azim.  REMARKS  Formation very soft , having difficulty getting the	Motor Make	Sperry Drill	_ Туре	8" Adjustable Moto	<del></del>	
Motor Usage Information         Time In Hole Depth In 320m         Out Depth Out Depth Out Source         Footage           Bit Make Security (116)         Type S33SF Nozzles 16-16-16           Mud Weight 8.9ppg Sand tr         PV / YP 6/10 Vis 37           Sand tr         Annula Vel. 28 / 48.2 m/min Gel           Drilling Parameters         WOB 10,000 lbs RPM 77 Pump Press. 1450psi GPM 480           SURVEYS:         NO. Depth Inc. Azim. REMARKS Formation very soft , having difficulty getting the	Motor RPM	76	_Press on btm	1575 psi	Off btm_	1450 psi
Depth In 320m Depth Out Footage  Bit Make Security (116) Type S33SF Nozzles 16–16–16  Mud Weight 8.9ppg PV / YP 6/10 Vis 37  Sand tr Annula Vel. 28 / 48.2 m/min Gel  Drilling Parameters WOB 10,000 lbs RPM 77  Pump Press. 1450psi GPM 480  SURVEYS:  NO. Depth Inc. Azim. REMARKS  Formation very soft , having difficulty getting the				Pressure Drop Acr	oss Bit	970 psi
Bit Make Security (116)  Type S33SF  Nozzles 16–16–16  Mud Weight 8.9ppg  PV / YP 6/10  Vis 37  Sand tr  Annula Vel. 28 / 48.2 m/min  Gel  Drilling Parameters  WOB 10,000 lbs  RPM 77  Pump Press. 1450psi  GPM 480  SURVEYS:  NO. Depth Inc. Azim.  REMARKS  Formation very soft , having difficulty getting the	Motor Usage	e Information	Time In Hole	09:15 15/2/94	Out	
Mud Weight 8.9ppg PV / YP 6/10 Vis 37 Sand tr Annula Vel. 28 / 48.2 m/min Gel  Drilling Parameters WOB 10,000 lbs RPM 77 Pump Press. 1450psi GPM 480  SURVEYS: NO. Depth Inc. Azim. REMARKS Formation very soft , having difficulty getting the	Depth In	320m	_Depth Out		Footage	!
Mud Weight 8.9ppg PV / YP 6/10 Vis 37 Sand tr Annula Vel. 28 / 48.2 m/min Gel  Drilling Parameters WOB 10,000 lbs RPM 77 Pump Press. 1450psi GPM 480  SURVEYS: NO. Depth Inc. Azim. REMARKS Formation very soft , having difficulty getting the						
Sand tr Annula Vel. 28 / 48.2 m/min Gel  Drilling Parameters WOB 10,000 lbs RPM 77 Pump Press. 1450psi GPM 480  SURVEYS: NO. Depth Inc. Azim. REMARKS Formation very soft , having difficulty getting the	Bit Make	Security (116)	Туре	S33SF	Nozzles	16-16-16
Sand tr Annula Vel. 28 / 48.2 m/min Gel  Drilling Parameters WOB 10,000 lbs RPM 77 Pump Press. 1450psi GPM 480  SURVEYS: NO. Depth Inc. Azim. REMARKS Formation very soft , having difficulty getting the	•		_			
Drilling Parameters  WOB 10,000 lbs RPM 77  Pump Press. 1450psi GPM 480  SURVEYS:  NO. Depth Inc. Azim. REMARKS  Formation very soft , having difficulty getting the	Mud Weight	8.9ppg	PV / YP	6/10	Vis_	37
Pump Press. 1450psi GPM 480  SURVEYS:  NO. Depth Inc. Azim. REMARKS  Formation very soft , having difficulty getting the	Sand	tr	 Annula Vel.	28 / 48.2 m/min	Gel	
Pump Press. 1450psi GPM 480  SURVEYS:  NO. Depth Inc. Azim. REMARKS  Formation very soft , having difficulty getting the	•					
SURVEYS :  NO. Depth Inc. Azim. REMARKS  Formation very soft , having difficulty getting the	Drilling Para	meters	WOB	10,000 lbs	RPM_	77
NO. Depth Inc. Azim. REMARKS  Formation very soft , having difficulty getting the			Pump Press.	1450psi	GPM_	480
NO. Depth Inc. Azim. REMARKS  Formation very soft , having difficulty getting the						
Formation very soft , having difficulty getting the	SURVEYS:					
	NO.	Depth Inc. Azim	n. _.	REMAR	RKS	
weight on bit to maintain a constant toolface				Formation very soft ,	having diff	iculty getting the
				weight on bit to mair	ntain a cons	stant toolface
	NAME OF TAXABLE PARTY OF TAXABLE PARTY.					
	M. T. C. C. C. C. C. C. C. C. C. C. C. C. C.					
			•			
		DIRECTIONAL SUPERVISOR		COMPANY M	<b>~</b> 1¥	

				Date _	16/2/94
Company	GFE Resources	Country	Australia	Rep.No_	#2
District	Victoria	Lease/Block		Well No	lona #2
Co.Man	Ken Smith	Cont.T.P.	Rick Giddens	Contr	Century Drilling
OPERATIO	NS.	•			
OI LIMITO	Continue drilling deviated h	ole from 500m to 640m	<u> </u>		
	POOH with kickoff assemble			m to 379m	
	Made up reaming assembly	k			n,609m to 640m
	Circulate hole clean				
					***************************************
BHA NO :	out:- bit-motor 1.15deg-s	etah_monol_hoe_4*8	"do'e_2*6 1/4"do'e	_ior_12*6	1/4*dc's_6*hwdi
. טאואווט	in -bit-stab-monel-hos-				
Motor Make	e Sperry Drill		8" Adjustable Mot		
Motor RPM		Press on btm		<del></del>	1450 psi
			Pressure Drop Acı		970 psi
Motor Usag	ge Information		09:15 15/2/94	Out	15:20 16/2/94
Depth In	320m	Depth Out	640m	Footag	640m
		-			
Bit Make	Security (116)	Туре	S33SF	Nozzles_	16-16-16
Mud Weigh	t 8.9ppg	PV / YP	6/10	Vis_	37
Sand	tr	Annula Vel.	28 / 48.2 m/min	Gel _	
Drilling Par	ameters	WOB	10 – 25000lbs	RPM	77
•		Pump Press.		GPM	480
		• • -	-		
SURVEYS:					
NO. Depth Inc.		Azim.	REMA	RKS	
		F	Run #1: motor and	M.W.D	, i., i.
			Time in -	09:15 15/	/2/94
			Time out -	15:20 16/	2/94
	DIRECTIONAL SUPERVIS	SOR	COMPANY M	IAN	

				Date _	17/2/94
Company	GFE Resources	Country	Australia	Rep.No	#3
District	Victoria	Lease/Block			lona #2
Co.Man	Ken Smith	Cont.T.P.	Rick Giddens	Contr.	Century Drilling
00504710	NO				
OPERATIO	NS: POOH to 8" drill collars the	n PIH to bottom			
	Circulate hole clean - POC				
	Run 9 5/8" casing and cem	······································			
	W.O.C				
		<u> </u>			
					<del></del>
BHA NO :	in -bit-stab-monel-hos-	dcstab3* 8"dc's2	2* 6 1/4"dc's-iar-1	12* 6 1/4*dc	s-6* hwdp
Motor Make	e			Ser. No.	
Motor RPM		Press on btm		Off btm.	
			Pressure Drop Ac	ross Bit	
Motor Usaç	ge Information	Time In Hole		Out	
Depth In		Depth Out		Footage	
Bit Make		Туре		Nozzles	
Mud Weigh	t 9.3ppg	PV / YP	12/14	Vis_	47
Sand	1%	Annula Vel.	28 / 48.2 m/min	Gel	9/37
n :::: n		14/O.D.	0 5000%	DDM	<b>.</b>
Drilling Par	ameters	WOB .	0-5000lbs	RPM _	50
		Pump Press.	1450psi	GPM _	480
	·				
SURVEYS:					
NO. Depth Inc. Azi		Azim.	REMA		
			Run #2 : M.W.D o		
			Time in		16/2/94
			Time out	- 10:30	17/2/94
			· · · · · · · · · · · · · · · · · · ·		
	DIRECTIONIAL SLIDEDVI	SOR	COMPANY	IAN	
	DIRECTIONAL SUPERVI	SOR	COMPANY M	IAN	

	•			Date _	18/2/94
Company	GFE Resources	Country	Australia	Rep.No	#4
District	Victoria	Lease/Block		Well No	
Co.Man	Ken Smith	Cont.T.P.	Rick Giddens	Contr.	Century Drilling
OPERATIO	NS:				
	W.O.C	***************************************			
	Nipple up B.O.P – test same	etc			
	Made up rotary assembly an	d R.I.H			
		**************************************	,		
BHA NO:	bit-stab-pony-stab-mone	el-stab-6* dc's-jar-	-18* dc's-6* hwo	dp	
	_			0 11-	
	e	Press on btm			
Motor RPM		<del></del>	<del></del>		
Motor Head	ge Information		Pressure Drop A		
Motor Osaç Depth In	ge information	Depth Out		Footage	* *************************************
Dopar III		bopui out			
Bit Make	Varel	Туре	ETD 417	Nozzles	10-10-11
		.,,,,,			<u></u>
Mud Weigh	t 8.8ppg	PV / YP	5/11	Vis	35
Sand		Annula Vel.		Gel _	9/21
Drilling Par	amatara	WOB	0-5000lbs	RPM	50
Dinning i ai	ameters	Pµmp Press.	1450psi		480
		i pilip riess.	1430psi		400
SURVEYS :					
NO.	Depth Inc.	Azim.	REM	ARKS	
				<u></u>	
				· · · · · · · · · · · · · · · · · · ·	
	•		<del></del>		••••••••••••••••••••••••••••••••••••••
	DIRECTIONAL SUPERVIS	OR -	COMPANY	MAN	

					Date	19/2/94
Company	GFE Resources		Country	Australia	Rep.No	#5
District	Victoria		Lease/Block	PPL – 2		lona #2
Co.Man	Ken Smith		Cont.T.P.	Rick Giddens	Contr.	
			<del></del>			
OPERATIO						
	RIH tagged cemer					
	Drilled float, shoe a					
			aking single she	ot surveys – the ang	gie continue	es to build
	POOH for assemb					
	Made up motor an					
	Orientate and drille	ed with motor to	drop the well ar	ngle -781m to 823n	1	
BHA NO :	bit-stab-pony-s	tab-monel-sta	b-6* dc's-jar-	-18* dc's-6* hwdp		
	in-bit-motor-sta	ab-monel-hos-	-2* dc's-jar-1	8* dc's-6* hwdp-l	KSW	
Motor Make	e Drilex		_ Туре	D675	Ser. No_	50218
Motor RPM	84		Press on btm	1550psi	Off btm_	1400psi
			1	Pressure Drop Acr	oss Bit	861psi
Motor Usag	ge Information		Time In Hole	18:30 19/2/94	Out	
Depth In	781m		_Depth Out		Footage	
Bit Make	Varel		Туре	ETD 417	Nozzles_	10-10-11
Mud Weigh	t 8.8ppg		_ PV / YP	6/8	Vis_	38
Sand	tr		Annula Vel.	37.6 / 67.3 m/min	Gel _	4/14
Drilling Par	ameters		WOB	10-15000lbs	RPM _	40
			Pump Press.	1400psi	GPM _	300
SURVEYS:		•				
NO.	Depth Inc	c. Azim	•	REMAI	RKS	
				•		· · · · · · · · · · · · · · · · · · ·
	· · · · · · · · · · · · · · · · · · ·					
	DIRECTIONAL S	SUPERVISOR	-	COMPANY M	AN	

				Date	20/2/94
Company	GFE Resources	Country	Australia	Rep.No	#6
District	Victoria	Lease/Block	PPL – 2	Well No	
Co.Man	Ken Smith	Cont.T.P.	Rick Giddens		Century Drilling
001111001					
OPERATIO	NS:				•
	Continue drilling with motor dro	pping off the angle	e - 823m to 1052m		
	The pipe stuck while making a c	connection			
	Displaced the mud with water a	nd worked the pipe	e free		·
	POOH laying out the motor MW	D etc.			
	Made up a pendulum assembly	and RIH			
			MANUFACTURE SAME SAME SAME SAME SAME SAME SAME SAM		
BHA NO :	:out-bit-motor-stab-monel-	hos-2* dc's-jar-	-18* dc's-6* hwdp-	-ksw	
	in- bit-monel-dc-stab-dc-	stab-10* dc's-st	ab-6* dc-jar-2* d	c's-6* hwo	lp-ksw
Motor Make	e Drilex	Туре	D675	Ser. No	50218
Motor RPM	84	Press on btm	1550psi	Off btm	1400psi
		The second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second second secon	Pressure Drop Acr	oss Bit	861psi
Motor Usag	je Information	Time In Hole	18:30 19/2/94	Out	20:00 20/2/94
Depth In	781m	Depth Out	1052m	Footage	271m
•					
Bit Make	Varel	Туре	ETD 417	Nozzles	12-12-10
Mud Weight	t 8.9ppg	PV / YP	12/11	Vis	38
Sand	tr	Annula Vel.	43.8/68.6 m/min	Gel	2/5
		-			
Drilling Para	ameters	WOB	10-15000lbs	RPM	40
_		Pump Press.	1400psi	GPM	300
		•			
SURVEYS:					
NO.	Depth Inc. Az	im.	REMAR	RKS	
	•		Run #3 : motor and	M.W.D	
			Time in	- 18:30	19/12/94
			Time out	- 20:00	20/2/94

	•			Date	21/2/94
Company	GFE Resources	Country	Australia	Rep.No	#7
District	Victoria	Lease/Block	PPL – 2	Well No	
Co.Man	Ken Smith	Cont.T.P.	Rick Giddens	Contr.	Century Drilling
OPERATION	<u>NS:</u> RIH to 1024m — wash an	d roomed to 1042m			
	Blew the kelly hose – PC				<del></del>
	Replaced kelly hose etc	OFFIG SHOE			
	RIH and drilled from 1052	2m to 1133m			
	Till Talle dillocalitotti Tool		<del></del>	•	
	A STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STATE OF THE STA			· · · · · · · · · · · · · · · · · · ·	
		1			
BHA NO :	bit-monel-dc-stab-do	c-stab-10* dc's-stab-	-6* dc-jar-2* dc's	-6* hwdp-	ksw
Motor Make		Туре		Ser. No <u>.</u>	· · · · · · · · · · · · · · · · · · ·
Motor RPM	****	Press on btm		Off btm.	
			Pressure Drop Ac	-	***************************************
_	e Information	Time In Hole	V. M. V. 11131111111111111111111111111111111	Out _	
Depth In		Depth Out		Footag <u>e</u>	
Da Mala	Vanal	<b>T</b>	ETD 447	Namelaa	10 10 10
Bit Make	Varel	Туре	ETD 417	NOZZIE\$_	12-12-10
Mud Weight	9.1ppg	PV / YP	11/8	Vis	38
Sand	0.3%	Annula Vel.	47.7/70 m/min	Gel	
Drilling Para	meters	WOB	10-15000lbs	RPM	110
_		Pump Press.		GPM	······································
		• -			
SURVEYS:					
NO.	Depth Inc.	Azim.	REMA	RKS	
			•		
<del> </del>					
				w.,	
			A CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR		
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_					
-	DIRECTIONAL SUPERV	VISOR	COMPANY M	1AN	

						Date _	22/2/94		
Company	GFE Res	ources		Country	Australia	Rep.No_	#8		
District	Victoria			_ Lease/Block	PPL - 2	Well No	Iona #2		
Co.Man	Ken Smit	h		_Cont.T.P.	Rick Giddens	Contr.	Century Drilling		
OPERATIO	NS:								
	Continue d	Irilling 8 1/2" h	ole from 1	133m to 1182n	n – circulate and to	ok survey			
	While takin	g the survey t	the pipe st	uck – worked	same free				
	Drilled to 1	268m – circu	late and m	ade short trip t	o 900m – no hole p	roblems			
	Circulate b	ottoms up an	d took two	surveys ( one	misrun )				
	POOH for I	oit and assem	bly change	9					
							·		
							<del></del>		
BHA NO	: bit-mone	I-dc-stab-d	dc-stab-1	10* dc's-stab-	-6* dc-jar-2* dc's	-6* hwdp-	ksw		
Motor Make			_ Type		Ser. No <u>.</u>				
Motor RPM	A			Press on btm		Off btm.			
		_			Pressure Drop Ac	_			
	ge Informat	ion		Time In Hole		Out	· · · · · · · · · · · · · · · · · · ·		
Depth In				_Depth Out		Footage			
Bit Make	Varel			Туре	ETD 417	Nozzles	12-12-10		
Dit Make	- Valor			_ '}					
Mud Weigh	nt 9.3ppg	٠		PV / YP	13/9	Vis	39		
Sand	0.1%			Annula Vel.	47.7/70 m/min	Gel	2/7		
Drilling Par	rameters			WOB	10-15000lbs	RPM	305		
				Pump Press.		GPM			
SURVEYS	:								
NO.	Depth	Inc.	Azim	•	REMA	RKS			
62	1165	3.75	136		Continue reaming k	ellys etc. to	ellys etc. to keep		
63	1250	2,5	143		the angle down.				
		•							
	DIRECTI	ONAL SUPER	RVISOR	-	COMPANY	IAN			

					Date	23/2/94		
Company	GFE Resourc	es	Country	Australia	Rep.No	#9		
District	Victoria		Lease/Block		Well No			
Co.Man	Ken Smith		 _Cont.T.P.	S. Kelly	Contr.	Century Drilling		
ODEDATIO	MC.							
OPERATIO		nd assembly chang	<b>a</b>					
		mbly , bit and jar						
		- broke circulation	and washed to		· · · · · · · · · · · · · · · · · · ·			
	Drilled from 12		······································					
<u> </u>	Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Control of the Contro							
BHA NO	: bit-stab-pony	/-stab-monel-sta	ıb-7* dc's-sta	ab-7* dc's-2* hwd	p-jar-4* hv	vdp-32* dp-ksw		
						· · · · · · · · · · · · · · · · · · ·		
Motor Mak	e		Type		Ser. No.			
Motor RPM	Motor Make Motor RPM			1	Off btm.			
				Pressure Drop Ac	ross Bit			
Motor Usag	ge Information		Time In Hole		Out			
Depth In			_Depth Out		Footage			
Bit Make	Varel		_ Type	ETD 417	Nozzles_	12-12-12		
Mud Weigh			_ PV / YP	12/8	Vis_			
Sand	tr	***************************************	_Annula Vel.	47.7/70 m/min	Gel _	1/5		
Drilling Par	rametere		WOB	20-25000ibs	RPM	90		
Drining r ai	ameters		Pump Press.	<del></del>	GPM	····		
			i ump i iess.	1220psi	OI W	010		
SURVEYS :	•							
NO.	Depth	Inc. Azim	l.	REMA	RKS			
64	1345	1.5 153	1	•		reduce		
			Layed out six drill collars to help reduce differential sticking problems					
				Bit out - Varel ETD				
				Footage 6				
***************************************			Hours 50.5					
			Condition 1–1–in					
		-						
	DIRECTIONA	L SUPERVISOR	_	COMPANY	IAN			
				, ,				

						Date	24/2/94
Company	GFE Res	ources		Country	Australia	Rep.No_	#10
District	Victoria			Lease/Block	PPL – 2		lona #2
Co.Man	Ken Smit	h		Cont.T.P.	S. Kelly	Contr.	Century Drilling
ODEDATIO	ue.						
OPERATIO		rilling 8 1/2" h	ole to 165	0m			
		ottoms up an		· · · · · · · · · · · · · · · · · · ·			
			·····	abbing in place	S		
	····						
BHA NO :	bit-stab-p	ony-stab-n	nonel-sta	b-7* dc's-sta	b-7* dc's-2* hwo	dp-jar-4* hv	vdp-32* dp-ksw
Motor Make			Туре		Ser. No <u>.</u>		
Motor RPM				Press on btm		Off btm.	
					Pressure Drop Ac		
Notor Usag	e Informati	ion		Time In Hole		Out	
Depth In		····	<del> </del>	Depth Out		Footag <u>e</u>	
Nik Admira	Manal			<b>T</b> :	ETD 447	Manuelas	10 10 10
Bit Make	Varel			_ Type	ETD 417	Nozzies_	12-12-12
/lud Weight	9.35ppa			PV / YP	12/8	Vis	39
Sand	tr			Annula Vel.	47.7/70 m/min	Gel	
				-			
rilling Para	ameters			WOB	20-25000ibs	<del></del>	90
				Pump Press.	1225psi	GPM _	310
SURVEYS:							
	Depth	Inc.	Azim.		REMA	ARKS	
65	1450	1	151			2 <del></del>	
66	1632	0.75	136				
					· · · · · · · · · · · · · · · · · · ·		
	<del></del>	· · · · · · · · · · · · · · · · · · ·					
	DIRECTION	ONAL SUPER	VISOR		COMPANY	MAN	

						Date	25/5/94	
Company	GFE Res	ources		_Country	Australia	Rep.No	#11	
District	Victoria			Lease/Block	PPL – 2		lona #2	
Co.Man	Ken Smi	.h		 Cont.T.P.	S. Kelly	Contr.	Century Drilling	
OPERATIO	JNG.							
OPERATIO		iper trip to bot	tom		<del>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</del>			
		· <del></del>		- drop multisho	t			
				e multishot inst				
	Continue F	OOH to surfa	ce – rig u	p and start logg	ging			
BHA NO	: bit-stab-	pony-stab-m	nonel-sta	b-7* dc's-sta	b-7* dc's-2* hwd	lp-jar-4* hv	wdp-32* dp-ks	
						<u> </u>	· · · · · · · · · · · · · · · · · · ·	
Motor Make			Туре	Туре				
Motor RPN				Press on btm	1	Off btm.		
					Pressure Drop Ad	ross Bit		
Motor Usa	ge Informat	ion		Time In Hole		Out		
Depth In	•			Depth Out		Footage	!	
Bit Make	Varel			Туре	ETD 417	Nozzles_	12-12-12	
_	ht 9.35ppg	·		PV / YP	12/8	Vis_		
Sand	l tr		· · · · · · · · · · · · · · · · · · ·	_Annula Vel.	47.7/70 m/min	Gel _	1/5	
Drilling Pa	rameters			WOB	20-25000ibs	RPM	90	
				Pump Press.		GPM		
				, a.i.p 1 1000.				
SURVEYS	:							
NO.	Depth	Inc.	Azim		REMA	RKS		
				1	Bit out Varel 417			
66	1632	0.75	136	<del> </del>	Footage 382m			
				† ·	Condition 1-1-in			
				Depart rig on 25/2/94				
					13			
	DIRECTI	ONAL SUPER	VISOR	_	COMPANY	IAN		
		1						

COMPANY: GFE Resources

DATE IN:

14/2/94

FIELD NAME:

DATE OUT:

15/2/94

WELL NAME: lona #2 ASSEMBLY NO: #1

DEPTH IN: 0

DEPTH OUT: 320M

				FISH	BLADE	SERIAL	TOOL
THREAD	ITEM	O.D.	I.D.	NECK	LENGTH	NUMBER	LENGTH
	BIT	12 1/4					0.3
	2* 8"DC'S	7 7/8	3 1/8				17.98
	STAB	8	27/8			7790417	1.89
	2* 8*DC'S						18.12
,							
				·	TOTAL AC	CEMPLY LENGTH	20.00

TOTAL ASSEMBLY LENGTH 38.29

COMPANY: GFE Resources

DATE IN: 16/2/94

FIELD NAME:

WELL NAME: Iona #2

DEPTH IN: 640m DEPTH OUT: 640m

DATE OUT: 17/2/94

ASSEMBLY NO: #3

				FISH	BLADE	SERIAL	TOOL
THREAD	ITEM	O.D.	I.D.	NECK	LENGTH	NUMBER	LENGTH
	BIT	12 1/4					0.3
6 5/8REG BOX / BOX	STAB	8	2 13/16	0.50	0.61	248	1.55
6 5/8REG PIN / BOX	MONEL	8	27/8			51349AB	9.12
6 5/8REG PIN / BOX	H.O.S	8 1/8	3 5/16			SSDS 00026	1.95
6 5/8REG PIN / BOX	DC						9.11
6 5/8REG PIN / BOX	STAB	7 15/16	3	0.49	0.74	7790417	1.59
6 5/8REG PIN / BOX	3* 8" DC'S						27.3
8REG PIN / 4IF BOX	CROSS OVER						0.59
4IF PIN / BOX	2* 6 1/4" DC'S						17.98
4IF PIN / BOX	JAR	6 9/16	3 1/4			DJ6 65028	5.93
4IF PIN / BOX	14* 6 1/4" DC'S						124.9
4IF PIN / BOX	6 * HWDP						55.38
					TOTAL AS	SSEMBLY LENGTH	255.7

COMPANY: GFE Resources

DATE IN: 18/2/94

FIELD NAME:

WELL NAME: lona #2

DATE OUT: 19/2/94 DEPTH IN: 640m

ASSEMBLY NO: #4

DEPTH OUT: 781m

		)		FISH	BLADE	SERIAL	TOOL
THREAD	ITEM	O.D.	I.D.	NECK	LENGTH	NUMBER	LENGTH
	BIT	8 1/2					0.24
4 1/2REG BOX / 4IF PIN	STAB	6 3/8	27/8	0.36	0.51	1010	1.4
4"IFPIN/BOX	PONY DC	6 3/8	3			1540	3.5
4IF PIN / BOX	STAB	6 3/8	27/8	0.59	0.54	0185	1.71
4IFPIN / 4 1/2IF BOX	CROSS OVER	6 1/4	2 3/4			SSDS A-128	0.41
4 1/2 PIN / BOX	MONEL	6 3/4	27/8			SSDS C410	9.23
4 1/2IF PIN / 4IF BOX	CROSS OVER	6 1/4	27/8			SSDS A-125	0.49
4IF PIN / BOX	STAB	6 3/8	27/8	0.70	0.47	268	1.58
4IF PIN / BOX	2 * 6 1/4 DC'S						17.98
4IF PIN / BOX	JAR	6 9/16	3 1/4			DJ6 65028	5.93
4IF PIN / BOX	18 * 6 1/4 DC'S						160.55
4IF PIN / BOX	6 * HWDP						55.38
4IF PIN / 4 1/2IF BOX	CROSS OVER	6 3/8	27/8			1553	0.35
4 1/2IF PIN / BOX	K.S.W	6 3/8	3 1/8	0.76	0.51	7002	1.84
4 1/2IF PIN / 4IF BOX	CROSS OVER	6 3/16	27/8			AUS 210	0.47
					TOTAL AS	SEMBLY LENGTH	261.06

COMPANY: GFE Resources

DATE IN: 19/2/94

FIELD NAME:

WELL NAME: lona #2

DATE OUT: DEPTH IN:

20/2/94 781m

ASSEMBLY NO: #5

DEPTH OUT: 1052m

				FISH	BLADE	SERIAL	TOOL
THREAD	ITEM	O.D.	I.D.	NECK	LENGTH	NUMBER	LENGTH
	BIT	8 1/2					0.24
4 1/2R BOX / 4 1/2F BOX	DRILEX MOTOR	6 3/4				50218	7.17
4 1/2IF PIN / 4IF BOX	CROSS OVER	6 5/8	27/8			SSDS 3127	0.77
4IF PIN / BOX	STAB	6 3/8	27/8	0.76	0.51	D88911	1.72
4IFPIN / 4 1/2IF BOX	CROSS OVER	6 1/4	2 3/4			SSDS A-128	0.41
4 1/2 PIN / BOX	MONEL	6 3/4	27/8			SSDS C410	9.23
4 1/2IF PIN / BOB	H.O.S	-				SSDS 00030	1.83
4 1/2IF PIN / 4IF BOX	CROSS OVER	6 1/4	27/8			SSDS A-125	0.49
4IF PIN / BOX	2 * 6 1/4 DC'S						17.98
4IF PIN / BOX	JAR	6 9/16	3 1/4			DJ6 65028	5.93
4IF PIN / BOX	18 * 6 1/4 DC'S						160.55
4IF PIN / BOX	6 * HWDP						55.38
4IF PIN / 4 1/2IF BOX	CROSS OVER	6 3/8	27/8			1553	0.35
4 1/2IF PIN / BOX	K.S.W	6 3/8	3 1/8	0.76	0.51	7002	1.84
4 1/2IF PIN / 4IF BOX	CROSS OVER	6 3/16	27/8			AUS 210	0.47
<u> </u>					TOTAL AS	SSEMBLY LENGTH	264.36

COMPANY: GFE Resources

15/2/94 DATE IN:

FIELD NAME:

DATE OUT:

16/2/94 .

WELL NAME: Iona #2

DEPTHIN: 320M

ASSEMBLY NO: #2

DEPTH OUT: 640m

				FISH	BLADE	SERIAL	TOOL
THREAD	ITEM	O.D.	I.D.	NECK	LENGTH	NUMBER	LENGTH
	BIT	12 1/4					0.3
6 5/8REG BOX / BOX	MOTOR 1.15DEG	8				800-050	8.38
6 5/8REG PIN / BOX	STAB 11 3/4"	7 7/8	3 1/8			7790594	1.88
6 5/8REG PIN / BOX	MONEL	8	27/8			51349AB	9.12
6 5/8REG PIN / BOX	H.O.S	8 1/8	3 5/16			SSDS 00026	1.95
6 5/8REG PIN / BOX	4* 8"DC'S						36.41
6 5/8REG PIN / 4IF BOX	CROSS OVER						0.59
4IF PIN / BOX	2* 6 1/4" DC'S						17.98
4IF PIN / BOX	JAR	6 9/16	3 1/4			DJ6 65028	5.93
4IF PIN / BOX	12* 6 1/4" DC'S						107.33
4IF PIN / BOX	6 * HWDP						55.38
		<u> </u>				OCMBLY LENGTH	045.05

TOTAL ASSEMBLY LENGTH 245.25

COMPANY: GFE Resources

FIELD NAME:

DATE IN: 20/2/94 DATE OUT: 23/2/94 DEPTH IN: 1052m

WELL NAME: lona #2 ASSEMBLY NO: #6

DEPTH OUT: 1268M

				FISH	BLADE	SERIAL	TOOL
THREAD	ITEM	O.D.	I.D.	NECK	LENGTH	NUMBER	LENGTH
	BIT	8 1/2					0.24
4 1/2REG / 4IF	BIT SUB	6 3/8	2 13/16				0.92
4IF PIN / 4 1/2IF BOX	CROSS OVER	6 1/4	2 3/4			SSDS A-128	0.41
4 1/2IF PIN / BOX	MONEL	6 3/4	27/8			SSDS C410	9.23
4 1/2IF PIN / 4IF BOX	CROSS OVER	6 1/4	27/8			SSDS A-125	0.49
4IF PIN / BOX	DRILL COLLAR						9.39
4IF PIN / BOX	STAB	6 3/8	27/8	0.59	0.54	0185	1.71
4IF PIN / BOX	DRILL COLLAR						8.59
4IF PIN / BOX	STAB	6 3/8	27/8	0.70	0.47	268	1.58
4IF PIN / BOX	10 DC'S						89.38
4IF PIN / BOX	STAB	6 3/8	27/8	0.76	0.51	D88911	1.72
4IF PIN / BOX	6 DC'S						53.32
4IF PIN / BOX	JAR	6 9/16	3 1/4			DJ6 65028	5.93
4IF PIN / BOX	2 DC'S						17.85
4IF PIN / BOX	6 HWDP						55.38
4IF PIN / 4 1/2IF BOX	CROSS OVER	6 3/16	27/8			1553	0.35
4 1/2IF PIN / BOX	K.S.W	6 3/8	3 1/8	0.76	0.51	7002	1.84
4 1/2IF PIN / 4IF BOX	CROSS OVER	6 3/16	27/8			AUS 210	0.47
					TOTAL AS	SSEMBLY LENGTH	258.8

**COMPANY: GFE Resources** 

DATE IN: 23/2/94

FIELD NAME:

DATE OUT:

WELL NAME: lona #2 ASSEMBLY NO: #7

DEPTH IN: 1268m DEPTH OUT: 1650m

				FISH	BLADE	SERIAL	TOOL
THREAD	ITEM	O.D.	I.D.	NECK	LENGTH	NUMBER	LENGTH
	BIT	8 1/2					0.24
4 1/2REG / 4 1/2IF	STAB	6 3/8	27/8	0.63	0.52	237	1.32
4 1/2IF PIN / 4IF BOX	CROSS OVER	6 3/8	27/8			1569	0.8
4IF PIN / BOX	PONY DC	6 3/8	3			1540	3.5
4IF PIN / BOX	STAB	6 3/8	27/8	0.70	0.47	268	1.58
4IF PIN / 4 1/2IF BOX	CROSS OVER	6 1/4	2 3/4			SSDS A-128	0.41
4 1/2IF PIN / BOX	MONEL	6 3/4	27/8			SSDS C410	9.23
1/2IF PIN / 4IF BOX	CROSS OVER	6 1/4	27/8			SSDS A-125	0.49
4IF PIN / BOX	STAB	6 3/8	27/8	0.59	0.54	0185	1.71
4IF PIN / BOX	7* DC'S	6 1/4					63.31
4IF PIN / BOX	STAB	6 3/8	27/8	0.76	0.51	D88911	1.72
4IF PIN / BOX	7* DC'S	6 1/4					62.01
4IF PIN / BOX	2* HWDP						18.41
4IF PIN / BOX	JAR	6 7/16	3			DJ6 65003	5.79
4IF PIN / BOX	4* HWDP						36.97
4IF PIN / BOX	32* DP (16 STDS = 3	07m)					
4IF PIN / 4 1/2IF BOX	CROSS OVER	6 3/16	27/8			1553	0.35
4 1/2IF PIN / BOX	K.S.W	6 3/8	3 1/8	0.76	0.51	7002	1.84
4 1/2IF PIN / 4IF BOX	CROSS OVER	6 3/16	27/8	<u> </u>	<u> </u>	AUS 210	0.47
L					TOTAL A	SSEMBLY LENGTH	210.15

# APPENDIX 10

# **APPENDIX 10**

### **CHECK SHOT CALCULATIONS**

IONA-2

### **IONA-2 CHECK SHOT CALCULATIONS**

A WST survey was acquired in the Iona-2 well by Schlumberger on 25 February, 1994. A total of twenty levels were acquired with one shot per level. One level was acquired on the way into the hole with this level being repeated on the way out.

The raw data from the survey is as follows:

Depth (mMDKB)	Transit Time (ms)
530.0	273.4
620.0	309.7
675.0	330.2
675.0	328.1
725.0	348.6
810.0	382.5
930.0	428.1
1032.0	467.3
1163.0	513.7
1200.0	527.8
1258.0	547.2
1275.0	553.3
1297.0	561.9
1317.0	568.3
1348.0	581.1
1382.0	589.4
1400.0	595.4
1450.0	611.0
1500.0	627.5
1570.0	650.2
1649.5	675.1

The quality of the data is generally very good with only the data at 1348.0 mMDKB being questionable. The time pick has been made from a noisy signal and the result of this shows up clearly on the time-depth curve as an area of anomalous interval velocities.

Of the two shots at 675.0 mMDKB, the value of 330.2 ms was chosen as this belongs to the data acquired going up the hole.

A number of corrections had to be applied to the data to obtain a set of time versus depth values below seismic reference datum (SRD) and they consist of:

- correction for deviated hole,
- correction for difference between shot position and SRD,
- correction for shot and geophone geometry.

### Correction for deviated hole

Iona-2 was a deviated hole so corrections had to be made to true vertical depth. These were made using the single-shot and multi-shot survey data shown in Appendix 9. Table 1 shows the calculations to correct measured depth to true vertical depth. Linear interpolation was used between surveyed points to calculate a true vertical depth for each of the check shot survey depths.

### **Correction to SRD**

Seismic reference datum for the area is 150 metres above sea-level. The well was drilled close to VP 248 on seismic line IONA93-01. An uphole was acquired at VP 259, a distance of some 220 m from the well. The basic information for the uphole is:

Elevation = 129.9 metres above sea level

Base weathering = 121.9 metres above sea level i.e. weathering is 8 metres thick

Weathering velocity = 650 metres/second

Sub-weathering velocity = 1591 metres/second

This produces a one-way time static shift of -5.4 ms, i.e. 5.4 ms needs to be added to one-way time values to shift data to a 150 m datum. The calculation of this value is shown in Appendix 10a.

The ground level at Iona-2 is at 130 m above sea level and this, therefore, equates to a static shift of -5.3 ms.

For the difference between shot depth and ground level (a difference of 2 m) a further static shift of -3.1 ms needs to be applied (i.e. 2 m at 650 m/s) resulting in a total one-way static shift of -8.4 ms.

### Correction for shot and geophone geometry

This exercise is the standard procedure used for vertical hole calculations and this is outlined in Table 2.

# CALCULATION OF GEOPHONE POSITION

	MDKB (m)	m N	m E	TVDKB (m)		MDKB (m)	m N	m E	TVDKB (m)
Required MDKB	530	-33.40	9.09	525.96	Required MDKB	1275	-152.77	97.83	1251.45
Measured values	528	-32.91	8.77	524.05	Measured values	1264	-152.41	97.56	1240.46
	538	-35.35	10.38	533.61		1283	-153.03	98.03	1259.45
	MDKB (m)	m N	m E	TVDKB (m)		MDKB (m)	m N	m E	TVDKB (m)
Required MDKB	620	-56.70	25.35	611.35	Required MDKB	1297	-153.47	98.31	1273.43
Measured values	614	-55.18	24.22	605.66	Measured values	1283	-153.03	98.03	1259.45
	622	-57.20	25.72	613.25		1301	-153.60	98.39	1277.43
	MDKB (m)	m N	m E	TVDKB (m)		MDKB (m)	m N	m E	TVDKB (m)
Required MDKB	675	-70.19	35.74	663.64	Required MDKB	1317	-154.05	98.66	1293.42
Measured values	668	-68.46	34.42	656.99	Measured values	1301	-153.60	98.39	1277.43
	688	-73.40	38.20	676.00		1321	-154.16	98.73	1297.42
	MDKB (m)	m N	m E	TVDKB (m)		MDKB (m)	m N	m E	TVDKB (m)
Required MDKB	725	-83.07	45.24	711.02	Required MDKB	1348	-154.80	99.07	1324.42
Measured values	707	-78.27	41.81	694.01	Measured values	1340	-154.63	98.99	1316.42
	726	-83.34	45.43	711.96		1359	-155.04	99.18	1335.41
	MDKB (m)	m N	m E	TVDKB (m)		MDKB (m)	m N	m E	TVDKB (m)
Required MDKB	810	-106.39	59.89	791.41	Required MDKB	1382	-155.51	99.35	1358.41
Measured values	802	-104.52	58.63	783.73	Measured values	1377	-155.41	99.31	1353.41
	821	-108.96	61.63	801.96		1397	-155.82	99.46	1373.40
	MDKB (m)	m N	m E	TVDKB (m)		MDKB (m)	m N	m E	TVDKB (m)
Required MDKB	930	-126.57	76.49	908.44	Required MDKB	1400	-155.88	99.49	1376.40
Measured values	917	-124.87	74.96	895.64	Measured values	1397	-155.82	99.46	1373.40
	936	-127.36	77.20	914.35		1417	-156.22	99.63	1393.40
	MDKB (m)	m N	m E	TVDKB (m)		MDKB (m)	m N	m E	TVDKB (m)
Required MDKB	1032	-138.51	86.45	1009.24	Required MDKB	1450	-156.85	100.00	1426.39
					Measured values	1435	-156.56	99.83	1411.39
						1455	-156.94	100.05	1431.39
	MDKB (m)	m N	m E	TVDKB (m)	,	MDKB (m)	m N	m E	TVDKB (m)
Required MDKB	1163	-148.55	94.25		Required MDKB	1500	-157.64	100.47	1476.38
Measured values	1148	-147.84	93.58		Measured values	1493	-157.54	100.41	1469.38
	1167	-148.74	94.43	1143.58		1512	-157.82	100.58	1488.38
B. C. LUDICE	MDKB (m)	m N	m E	TVDKB (m)	B ( ) ( ) ( ) ( )	MDKB (m)	m N	m E	TVDKB (m)
Required MDKB	1200	-150.04	95.66		Required MDKB	1570	-158.60	101.00	1546.37
Measured values	1187	-149.55	95.23						
	1206	-150.26	95.86	1182.53					
- · · · · · · · · · · · · · · · · · · ·	MDKB (m)	m N	m E	TVDKB (m)		MDKB (m)	m N	m E	TVDKB (m)
Required MDKB	1258	-152.20	97.38		Required MDKB	1649.5	-159.46	101.61	1625.87
Measured values	1244	-151.70	96.97	1220.48	Measured values	1608	-159.00	101.30	1584.37
	1264	-152.41	97.56	1240.46		1627	-159.21	101.44	1603.37

### **IONA-2 CHECK SHOT CALCULATIONS**

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1 2	530 620	526.0 611.4	541.7 627.1	-33.4 -56.7	9.1 25.4	519.9 606.7	519.7	273.4	273.3	281.7	1923	85.4	35.6	2398
3		663.6	679.3	-56.7 -70.2	25.4 35.7	660.1	605.1 657.3	309.7 330.2	308.9 328.8	317.3 337.2	1976 2015	52.2	19.9	2622
4	725	711.0	726.7	-83.1	45.2	708.9	704.7	348.6	346.5	354.9	2047	47.4	17.8	2670
5	810	791.4	807.1	-106.4	59.9	792.0	785.1	382.5	379.2	387.6	2082	80.4	32.6	2465
6	930	908.4	924.1	-126.6	76.5	911.5	902.1	428.1	423.7	432.1	2139	117.0	44.5	2628
7	1032	1009.2	1024.9	-138.5	86.5	1013.5	1002.9	467.3	462.4	470.8	2177	100.8	38.7	2602
8	1163	1139.6	1155.3	-148.6	94.3	1144.4	1133.3	513.7	508.7	517.1	2234	130.4 36.9	46.3	2816
9	1200	1176.5	1192.2	-150.0	95.7	1181.2	1170.2	527.8	522.9	531.3	2244	58.0	14.2 19.5	2606 2971
10	1258	1234.5	1250.2	-152.2	97.4	1239.0	1228.2	547.2	542.4	550.8	2270	17.0	6.1	2763
11	1275	1251.5	1267.2	-152.8	97.8	1255.9	1245.2	553.3	548.6	557.0	2275	22.0	8.6	2540
12		1273.4	1289.1	-153.5	98.3	1277.8	1267.1	561.9	557.2	565.6	2279	20.0	6.5	3100
13 14	1317 1348	1293.4 1324.4	1309.1 1340.1	-154.1 -154.8	98.7 99.1	1297.7 1328.6	1287.1 1318.1	568.3 581.1	563.6 576.5	572.0 584.9	2288 2291	31.0	12.9	2410
15		1358.4	1374.1	-155.5	99.4	1362.4	1352.1	589.4	584.9	593.3	2316	34.0	8.4	4034
16		1376.4	1392.1	-155.9	99.5	1380.3	1370.1	595.4	591.0	599.4	2323	18.0	6.1	2975
17	1450	1426.4	1442.1	-156.9	100.0	1430.1	1420.1	611.0	606.7	615.1	2344	50.0	15.7	3177
18	1500	1476.4	1492.1	-157.6	100.5	1479.8	1470.1	627.5	623.4	631.8	2362	50.0	16.6	3006
19	1570	1546.4	1562.1	-158.6	101.0	1549.5	1540.1	650.2	646.2	654.6	2386	70.0	22.9	3060
20	1649.5	1625.9	1641.6	-159.5	101.6	1628.7	1619.6	675.1	671.3	679.7	2415	79.5	25.1	3168

#### Additional data

KB = 134.3m asl

Ground level = 130m asl

SRD = 150m asl

Shot depth = 2m below GL

Shot location:

21 mS, 0 mE

Well location:

38 34' 30.989" S 143 02' 01.585" E

Seismic line:

IONA93-01 VP 248

Source to SRD time correction: 8.4 ms

Col. 1	Level number	Col. 6	Metres East	Col. 11	Transit time corrected from source to SRD (ms)
Col. 2	Measured depth KB (m)	Col. 7	Distance source-geophone (m)	Col. 12	Average velocity from SRD (m/s)
Col. 3	True vertical depth KB (m)	Col. 8	Vertical distance source-geophone (m)	Col. 13	Depth differences (m)
Col. 4	Depth below Seismic Reference Datum (m)	Col. 9	Raw transit time source-geophone (ms)	Col. 14	Time differences (ms)
Col. 5	Metres North	Col. 10	Corrected vertical transit time source-geophone (ms)	Col. 15	Interval velocity (m/s)

#### APPENDIX 10a

### Corrections for ground level to datum and shot depth

To calculate the static shift from ground level to SRD it is easiest to consider the problem in depth-time space with depth on the y-axis and time on the x-axis. The slope of any line in this space is then equal to the velocity.

The basic data for the calculations is shown in the figure below.

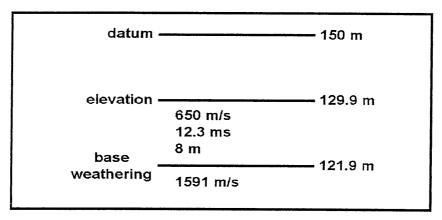


Figure 1 Basic data for static calculation for VP 248 on line IONA93-01

The equation for a straight line is:

$$y = mx + b \qquad \dots (1)$$

where:

$$m = \text{slope (or velocity)}$$
  
 $b = y$ -intercept

This equation can be used to determine the one-way static shift by substituting in the subweathering velocity of 1591 m/s for m and 12 ms (0.0123 s) for x. This gives a b value, once equation (1) is rearranged, of:

$$b = y - mx \qquad .... (2)$$
  
= 121.9 + 1591 * 0.0123  
= 141.47

The value of the time shift is then calculated by substituting in 141.47 for b and 150 (which is the seismic reference datum) for y into equation (1) to give:

$$x = \underbrace{y - b}_{m} \qquad \dots (3)$$

$$= \frac{150 - 141.47}{1591}$$
$$= 5.4 \text{ ms}$$

This infers that the replacement velocity is 3749 m/s (= 20.1m/5.4ms). Using this replacement velocity for the difference between ground level and SRD at the well location (= 20m), the static shift is:

For the correction for shot depthto ground level , use the average weathering velocity from the uphole of 650 m/s, therefore the correction:

$$= 2 / 650$$
  
= 3.1 ms

This gives the total shot to SRD static correction

$$= 5.3 + 3.1$$
  
= 8.4 ms

# APPENPIX 11

### **GFE RESOURCES LTD**

# **APPENDIX 11**

### LOG ANALYSIS DATA

IONA-2

### GFE RESOURCES LTD

### Company

### : GFE RESOURCES LTD

Well : IONA-2 Field : IONA

Nation : AUSTRALIA State : VICTORIA

Location : PORT CAMPBELL
Latitude : 38° 34′ 30.989″ S
Longitude : 143° 02′ 01.585″ E

Well Datum : KELLY BUSHING Elevation of Datum : 134.2 mAMSL

### Software by Crocker Data Processing Pty Ltd

Program revision no. 4.10 1 Mar 1993

Hole depth M Temperature C Gradient Deg C / 100 M 1650.0 66.20 2.9212 0.0 18.00

### Log data

Column Position	Logs Available	Logs Used	Column Position	Logs Available	Logs Used
1	DEPT	DEPT	14	DT	
2	DEVI	DEVI	15	CALS	
3	TVD	TVD	16	GR	GR
4	AZIM	AZIM	17	RHOB	RHOB
5	NORT		18	NPHI	NPHI
6	EAST		19	PEF	PEF
7	OFFS		20	DRHO	DRHO
8		GR	21	DRHO	
9	CALI	CALI	22	OFFS	
10	SP	SP	23	DT	DT
11	LLD	LLD			
12	LLS	LLS			
13	MSFL	MSFL			

Logs recorded by : SCHLUMBERGER Caliper recorded in : Inches Mud weight units : Lbs/qal Mud type : KCl Formation water type: NaCl Density log units : q/cc log units DRHO : q/cc Sonic log units : Us/ft Neutron log type : Compensated Neutron log units : LS POR Density tool type : LDT Density-CNL Chart : 1988 RHO (H, MA, f) units : q/cc Dens. X-plots units : g/cc

#### Permeability equation used

a) SWirrcutoff <1.0

Koil = Kcoef * PHIE ** Kexp / SW**2 Kcoef Kexp Computed if SW<=SWirrcutoff Coates 62500 6.0 Timur 8581 4.4

b) SWirrcutoff >=1 Koil = Kcoef * 10**(PHIE * Kexp)

#### CPX flag values

- VCL greater than 0.95
- greater than 0.75
- greater than 0.75
- Bad hole condition
- 5. Matrix density greater than Lithological model
- Matrix density less than Lithological model 6.
- Porosity derived from Sonic Log
- Porosity derived from or limited by PHIMAX
- Porosity derived from Density Log
- \$. Pay zone

#### Water saturation equations

------

- 1. Indonesia
- Simandoux
- 3. Fertl & Hammock
- 4. Laminar
- 5. Bussian
- 6. User defined

#### VGRTYPE : Vclay from GR Equations used

Not Used

IGR=(GR-GRmin)/(GRmax-GRmin)

- 1. Linear VGR=IGR
- 2. Asymetric (S shaped)

Defined by 2 sets of intermediate points through which the S bend passes through.

GR1, VGR1 and GR2, VGR2.

Steiber equation: VGR = IGR/(A + (A-1.0)*IGR)

- 3. Stieber 1 A = 2.0
- 4. Stieber 2 A = 3.0
- Stieber 3 A = 4.0
- 6. Stieber 50%

A is computed to give VGR= 0.5 when GR = GR50%)

- 7. Larinov Old Rocks: VGR= (2**(2*IGR)-1.0)/3.0
- Larinov Tertiary: VGR= 0.083*(2.0*(3.7058*IGR)-1.0)
- 9. Clavier : VGR= 1.7-SQRT(3.38-(IGR+0.7)**2.0)

Complex Lithology Results 24-10-94 Zone no. 1 2 3 5 6 7 8 1. Top depth 1160.069 1260.043 1296.924 1316.431 1347.978 1371.905 1401.470 2. Bottom depth 1260.043 1296.924 1316.431 1347.978 1371.905 1398.575 1438.504 1627.937 3. No logs SP SP SP SP SP SP SP SP 4. RM 0.340 0.340 0.340 0.340 0.340 0.340 0.340 0.340 Temp. RM 19.000 19.000 19.000 19.000 5. 19.000 19.000 19.000 19.000 6. RMF 0.268 0.268 0.268 0.268 0.268 0.268 0.268 0.268 7. Temp. RMF 21.000 21.000 21.000 21.000 21.000 21.000 21.000 21.000 8. RMC 0.498 0.498 0.498 0.498 0.498 0.498 0.498 0.498 9. Temp. RMC 19.000 19.000 19.000 19.000 19.000 19.000 19.000 19.000 Bit size 8.500 8.500 8.500 8.500 8.500 8.500 8.500 8.500 11. Mud wt 9.400 9,400 9.400 9.400 9.400 9.400 9.400 9.400 12. SSP 28.000 32.000 28.000 28.000 28.000 28.000 28.000 28.000 13. FT=Form temp 48.468 49.795 56.171 56.970 57.742 51.865 52.539 54.735 14. RW @ FT 0.600 0.183 0.250 0.250 0.450 0.300 0.370 0.300 6.089 21.471 13.910 15. KPPM (RW) 13.757 7.246 9.696 21.050 21.282 16. RMF @ FT 0.163 0.160 0.147 0.145 0.144 0.155 0.149 0.154 KPPM (RMF) 24.886 24.886 24.886 24.886 24.886 24.886 24.886 24.886 18. RM @ FT 0.193 0.177 0.176 0.197 0.174 0.188 0.186 0.181 19. RHO H 0.200 0.200 0.150 0.150 0.150 0.150 0.200 0.200 20. RHO F 1.015 1.015 1.013 1.013 1.012 1.015 1.015 1.014 21. t F 188.993 188.993 188.993 188.993 188.993 188.993 188.993 188.993 22. RHOMA 2.650 2.650 2.650 2.680 2.680 2.650 2.650 2.650 23. PHIN min -0.035 -0.035 -0.035 -0.035 -0.035 -0.035 -0.035 -0.035 24. t MA 55.500 55.500 55.500 55.500 55.500 55.500 55.500 55.500 25. t MA min 48.000 48.000 48.000 48.000 48.000 48.000 48.000 48.000 26. Sonic option 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 27. Compact fact 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 28. CAL cut off 16.000 16.000 16.000 10.000 10.000 16.000 16.000 16.000 29. RUGO.cut off 1.000 1.000 0.750 0.750 1.000 1.000 1.000 1.000 30. DRHO cut off 0.150 0.150 0.150 0.150 0.150 0.150 0.150 0.150 31. No clay S SN SD RTRTMN SN SD 32. VclayGR type 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 26.297 33. GR clean 33.059 21.789 18.809 18.182 20.000 45.000 45.000 34. GR clay 117.209 117.585 122.093 119.749 119.749 121.000 125.000 124.765 35. GR1 46.000 46.000 46.141 46.141 46.141 46.141 46.141 46.141

36. VGR1

0.100

0.100

0.100

0.100

0.100

0.100

0.100

0.100

Complex Lithology Results 24-10-94 2 Zone no. 1 3 4 5 6 7 8 37. GR2 60.000 60.000 60.000 60.000 60.000 60.000 60.000 60.000 38. VGR2 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 39. GR50% 70.000 70.000 70.000 70.000 70.000 70.000 70.000 70.000 40. R clay 2.500 2.500 7.000 8.000 6.000 7.000 5.000 3.000 41. R limit 1000.000 1000.000 1000.000 1000.000 1000.000 1000.000 1000.000 1000.000 42. RHOB clay 2.420 2.436 2.552 2.539 2.542 2.455 2.382 2.414 43. PHIN clay 0.428 0.464 0.373 0.333 0.353 0.318 0.345 0.363 44. t clay 111.709 110.533 92.218 89.373 91.254 91.724 104.803 98.792 45. M clay 0.550 0.552 0.629 0.653 0.639 0.676 0.615 0.645 46. N clay 0.407 0.378 0.407 0.437 0.423 0.473 0.479 0.455 47. PHIN 2.2 0.307 0.142-0.0085868 0.207 -0.014 0.173 0.235 0.235 48. t 2.2 66.673 105.930 100.671 88.462 89.213 91.467 91.467 91.467 49. COER (a) 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 50. MXP (m) 1.800 1.800 1.740 1.740 1.740 1.740 1.800 1.800 51. SXP (n) 2.000 2.000 2.080 2.080 2.080 2.080 2.000 2.000 52. Lithomod 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 53. SXO limit 0.200 0.200 0.200 0.200 0.200 0.200 0.200 0.200 54. PHI max 0.400 0.378 0.347 0.400 0.370 0.350 0.250 0.250 55. EXPX 1.500 1.500 1.500 1.500 1.500 1.500 1.500 1.500 56. Clay cut off 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 57. Por. cut off 0.050 0.050 0.050 0.050 0.050 0.050 0.050 0.050 58. SW cut off 0.500 0.500 0.500 0.500 0.500 0.500 0.500 0.500 59. Sat Equation 1.000 1.000 1.000 1.000 1.000 1.000 1.000 1.000 60. SWirr.cutoff 0.300 0.300 0.300 0.300 0.300 0.300 0.300 0.300 61. Perm Expon. 6.000 6.000 6.000 6.000 6.000 6.000 6.000 6.000 62. PERM K coef 62500.000 62500.000 62500.000 62500.000 62500.000 62500.000 62500.000 63. RHOMA 1 2.641 2.641 2.641 2.522 2.522 2.522 2.567 2.522 64. RHOMA 2 2.817 2.817 2.817 2.829 2.829 2.829 2.901 2.882 65. RHOMA 3 2.991 2.991 3.000 2.981 2.981 3.000 2.995 2.997 66. UMA 1 6.179 6.179 6.179 5.152 5.152 5.152 6.955 5.152 67. UMA 2 17.474 17.474 17.474 15.521 15.521 15.521 16.472 13.818 68. UMA 3 11.388 11.388 8.959 7.606 7.606 8.558 9.660 8.959 69. UF 0.400 0.400 0.400 0.400 0.400 0.400 0.400 0.400

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Complex Lithology Results 24-10-94

DEPTH M	GR	RT	RXO	PHIN	RHOB	DD	SPI	SWU	sxou	PHIS	VCL FVCI	RHOMAU	sxo	SW	PHIE R	AMOHS	POR-M	HC-M	FLAGS	
1315.1	111	8.7	10.5	34.1	2.489	-0.1	00.0	90.0	79.1	26.3	89.8 SD	2.680	90.0	90.0	1.3 2	2.970	0.00	0.00	8	
1315.2	113	8.6	9.8	33.3	2.486	-0.1	00.0	90.4	81.6	26.4	89.6 SD	2.680	90.4	90.4	1.3 2	2.961	0.00	0.00	8	
1315.4	113	8.3	9.6	33.1	2.487	-0.1	00.0	88.9	78.9	25.7	86.5 SD	2.680	88.9	88.9	2.0 2	2.960	0.00	0.00	8	
1315.5	116	8.3	9.6	32.0	2.488	-0.1	00.0	90.3	80.5	25.9	87.8 SD	2.680	90.3	90.3	1.7 2	2.952	0.00	0.00	8	
1315.7	115	8.2	8.2	30.3	2.503	-0.1	00.0	93.3	90.1	26.9	90.6 SN	2.680	93.3	93.3	1.1 2	2.948	0.00	0.00	8	
1315.8	112	7.9	9.0	29.0	2.514	-0.1	00.0	91.9	82.2	26.0	87.2 SN	2.680	91.9	91.9	1.8 2	2.945	0.00	0.00	8	
1316.0	104	7.7	9.0	31.3	2.514	-0.1	00.0	90.6	79.5	25.5	84.8 GR	2.680	90.6	90.6	2.4 2	2.965	0.00	0.00	8	
1316.1	96	7.4	8.4	31.6	2.518	-0.1	00.0	85.1	73.0	22.6	76.6 GR	2.680	85.1	85.1	4.5 2	2.971	0.00	0.00	8	
1316.3	87	6.1	7.0	28.7	2.520	-0.1	00.0	93.2	78.3	21.9	68.0 GR	2.791	93.2	93.2	5.6 2	2.946	0.00	0.00		
1316.4	77	5.4	5.9	23.9	2.530	-0.1	00.0	112.2	96.9	21.1	57.8 GR	2.708	100.0	100.0	4.7 2	2.903	0.00	0.00		
1316.6	66	6.2	3.1	19.6	2.489	-0.3	00.0	105.6	129.6	25.4	46.5 GR	2.647	100.0	100.0	6.4 2	2.810	0.00	0.00		
1316.7	54	7.9	1.6	13.8	2.404	-0.4	00.0	89.8	157.8	32.2	20.2 DN	2.622	97.9	89.8	11.9 2	2.678	0.00	0.00		
1316.9	43	13.0	4.9	7.0	2.259	-0.5	00.0	61.3	76.4	36.0	4.5 DN	2.598	76.4	61.3	17.8 2	2.617	0.00	0.00	6	
1317.0	32	46.2	5.9	2.4	2.129	-0.5	00.0	28.8	59.6	37.5	0.4 DN	2.575	59.6	28.8	22.0 2	2.617	0.03	0.02	6	\$
1317.2	27	207.6	4.7	1.7	2.046	-0.5	00.0	13.0	62.4	37.3	3.6 SN	2.487	62.4	13.0	23.4 2	2.632	0.07	0.05	6	\$
1317.3	27	330.3	4.7	1.5	2.006	-0.5	00.0	9.8	58.6	37.5	2.6 SD	2.490	58.6	9.8	25.3 2	2.630	0.11	0.09	6	\$
1317.5	27	273.8	4.2	1.5	1.984	-0.5	00.0	10.4	59.5	36.3	00.0 SD	2.502	59.5	10.4	26.8 2	2.622	0.15	0.13	6	\$
1317.7	27	211.8	4.6	1.8	1.976	-0.5	00.0	11.6	56.4	41.8	2.5 SN	2.495	56.4	11.6	26.8 2	2.635	0.19	0.16	6	\$
1317.8	29	206.0	5.7	2.3	1.988	-0.5	00.0	11.6	50.5	42.8	3.5 SN	2.538	50.5	11.6	27.0 2	2.624	0.23	0.20	6	\$
1318.0	28	200.3	5.0	2.0	1.992	-0.5	00.0	12.0	54.7	42.1	3.1 SN	2.511	54.7	12.0	26.4 2	2.635	0.27	0.23	6	\$
1318.1	30	201.2	4.4	1.6	1.983	-0.5	00.0	12.0	58.2	42.5	1.7 SN	2.494	58.2	12.0	26.5 2	2.627	0.31	0.27	6	\$
1318.3	29	206.7	11.1	1.4	1.970	-0.5	00.0	10.9	34.4	41.6	1.4 SN	2.652	34.4	10.9	29.5 2		0.36	0.31		\$
1318.4	29	206.0	7.3	1.7	1.978	-0.5	00.0	11.3	43.6	40.8	2.5 SN	2.583	43.6	11.3	28.1 2	2.623	0.40	0.35	6	\$
1318.6	25	207.1	5.3	1.6	1.996	-0.5	00.0	11.9	53.7	41.3	2.1 SN	2.526	53.7	11.9	26.4 2	2.621	0.44	0.38	6	\$
1318.7	25	199.8	4.4	1.8	1.999	-0.5	00.0	12.4	59.7	40.5	2.9 SN	2.483	59.7	12.4	25.5 2	2.625	0.48	0.42	6	\$
1318.9	26	179.0	11.4	1.8	1.993	-0.5	00.0	12.0	34.7	41.6	2.6 SN	2.648	34.7	12.0	28.5 2	2.662	0.52	0.46		\$
1319.0	28	137.6	5.8	2.3	1.983	-0.5	00.0	14.0	49.5	42.8	3.5 SN	2.543	49.5	14.0	27.3 2	2.629	0.56	0.49	6	\$
1319.2	29	110.4	5.3	2.5	1.985	-0.5	00.0	15.7	52.4	44.4	3.6 SN	2.527	52.4	15.7	27.0 2	2.634	0.60	0.53	6	\$
1319.3	30	116.9	9.6	2.3	2.003	-0.5	00.0	14.9	38.4	42.5	3.5 SN	2.628	38.4	14.9	27.8 2	2.649	0.65	0.56		\$
1319.5	30	148.2	9.2	1.7	2.038	-0.5	00.0	14.1	41.5	41.0	2.5 SN	2.614	41.5	14.1	26.1 2	2.631	0.69	0.60	6	\$
1319.6	29	239.7	8.4	1.1	2.058	-0.5	00.0	11.7	45.1	39.2	1.2 SN	2.600	45.1	11.7	25.0 2	2.627	0.72	0.63	6	\$
1319.8	26	601.8	10.2	1.0	2.063	-0.5	00.0	7.4	40.8	39.1	0.9 SN	2.627	40.8	7.4	25.2 2	2.633	0.76	0.67		\$
1319.9	22	1780.7	6.4	1.2	2.050	-0.5	00.0	4.5	52.1	39.5	1.4 SN	2.554	52.1	4.5	24.5 2	2.624	0.80	0.70	6	\$
1320.1	19	2127.3	4.7	1.4	2.044	-0.5	00.0	4.1	59.3	39.7	0.5 GR	2.562	52.8	4.1	25.1 2	2.625	0.84	0.74	6	\$
1320.2	18	1957.5	3.5	1.5	2.056	-0.5	00.0	4.3	69.3	40.3	00.0 GR	2.570	53.3	4.3	24.8 2	2.630	0.88	0.77	6	\$
1320.4	19	1412.2	3.2	1.7	2.083	-0.5	00.0	5.2	75.9	40.0	0.5 GR	2.565	55.5	5.2	23.6 2	2.628	0.91	0.81	6	\$
1320.5	21	1197.2	2.9	2.2	2.116	-0.5	00.0	5.9	82.9	38.0	1.9 GR	2.568	56.8	5.9	22.1 2	2.619	0.95	0.84	6	\$
1320.7	23	1211.0	2.1	2.3	2.122	-0.5	00.0	6.0	97.6	37.2	3.8 GR	2.556	56.9	6.0	21.4 2	2.619	0.98	0.87	6	\$

Zone No. 4

Zone No. Complex Lithology Results 24-10-94 DEPTH M GR RT RXO PHIN RHOB DDSPI SWU SXOU PHIS VCL FVCL RHOMAU SXO SW PHIE RHOMA POR-M HC-M FLAGS 1320.9 21 1145.8 2.3 2.113 -0.5 00.0 6.0 96.1 37.7 2.2 GR 2.1 2.565 57.0 6.0 22.2 2.618 0.90 1.01 6 1321.0 20 1042.7 1.9 2.092 -0.5 00.0 6.1 81.4 38.3 0.9 GR 57.2 23.2 2.629 2.563 6.1 1.05 0.94 1321.2 18 793.6 2.4 2.086 -0.5 00.0 6.9 85.7 00.0 GR 2.569 2.4 39.6 58.6 6.9 23.8 2.629 1.08 0.97 6 1321.3 18 582.8 3.1 2.7 2.086 -0.5 00.0 8.0 76.1 41.1 00.0 GR 2.563 60.3 '8.0 23.8 2.623 1.12 1.00 6 20 450.0 3.2 2.087 -0.5 00.0 1321.5 2.5 9.0 84.6 40.7 0.8 GR 2.557 61.8 9.0 23.7 2.622 1.04 1.16 276.9 1321.6 20 3.5 2.072 -0.5 00.0 11.2 84.1 39.2 0.7 GR 2.538 64.6 11.2 24.2 2.623 1.19 1.07 1321.8 20 171.9 4.9 2.086 -0.5 00.0 73.2 2.548 3.3 14.1 38.2 0.7 GR 67.6 14.1 24.2 2.632 1.23 1.10 1321.9 21 131.4 5.7 2.115 -0.5 00.0 16.5 2.4 88.1 34.8 1.9 GR 2.554 69.8 16.5 23.2 2.625 1.27 1.13 1322.1 24 101.7 5.8 2.164 -0.5 00.0 19.9 97.0 30.4 0.6 DN 2.576 72.4 19.9 21.7 2.619 1.30 1.16 1322.2 26 81.9 3.3 5.6 2.199 -0.5 00.0 23.6 85.2 2.570 35.4 2.3 DN 74.9 23.6 19.7 2.621 1.33 1.18 1322.4 31 7.3 2.197 -0.5 00.0 68.2 24.8 77.5 39.3 1.9 DN 75.6 2.589 24.8 20.8 2.618 1.20 1.36 1322.5 34 57.5 9.1 2.155 -0.500.023.8 63.0 43.9 4.9 DN 2.632 63.0 23.8 23.5 2.653 1.23 1.40 1322.7 51.6 9.9 2.094 -0.5 00.0 38 22.6 49.5 46.2 8.8 DN 2.654 49.5 22.6 25.9 2.693 1.44 1.26 1322.8 38 55.9 8.6 2.047 -0.5 00.0 21.2 57.5 50.6 4.4 DN 2.611 57.5 21.2 27.7 2.638 1.48 1.29 1323.0 -0.5 00.0 39 59.6 7.5 2.008 19.8 58.0 55.0 0.1 DN 2.617 58.0 19.8 29.8 2.618 1.52 1.33 1323.1 38 75.3 2.5 8.5 1.973 -0.5 00.0 17.7 70.0 52.2 3.8 DN 2.496 70.0 17.7 29.2 2.625 1.57 1.37 6 1323.3 36 130.2 8.0 9.0 1.956 -0.5 00.0 12.4 37.1 57.4 11.9 DN 2.648 37.1 12.4 30.8 2.719 1.41 1.61 1323.4 31 181.8 8.2 1.970 -0.5 00.0 65.2 64.7 2.8 11.4 52.1 2.5 DN 2.537 11.4 30.0 2.635 1.45 1.66 1323.6 6.2 2.024 -0.5 00.0 27 343.9 10.8 8.6 35.5 54.0 7.7 GR 2.664 35.5 8.6 27.9 2.704 1.70 1.49 1323.7 23 542.7 4.9 2.087 -0.5 00.0 8.0 59.5 50.0 2.560 59.5 5.0 4.6 GR 8.0 23.8 2.629 1.74 1.52 1323.9 25 520.5 4.8 2.137 -0.5 00.0 8.7 109.6 22.9 2.624 1.5 41.9 0.9 DN 2.600 61.3 8.7 1.77 1.55 1324.1 25 550.3 1.6 3.4 2.149 -0.5 00.0 8.9 113.7 39.1 0.7 DN 2.586 61.6 21.6 2.629 8.9 1.81 1.58 1324.2 24 577.2 2.5 2.124 -0.5 00.0 8.5 94.5 37.9 0.4 DN 2.567 61.1 22.1 2.629 8.5 1.84 1.61 1324.4 23 538.9 1.7 2.122 4.3 -0.5 00.0 9.1 71.3 39.4 3.0 SN 2.532 61.9 20.9 2.629 9.1 1.87 1.64 1324.5 25 467.0 1.8 2.122 -0.5 00.0 9.7 73.3 39.5 2.527 62.7 4.13.3 SN 9.7 20.8 2.626 1.90 1.67 1324.7 27 404.1 2.0 2.137 -0.5 00.0 10.7 95.7 2.5 39.7 3.8 SN 2.528 63.9 10.7 20.1 2.630 1.94 1.70 1324.8 26 332.0 -0.5 00.0 11.8 105.9 2.521 2.1 2.3 2.143 39.0 4.6 SN 65.3 11.8 19.7 2.628 1.97 1.72 1325.0 24 238.1 1.8 2.4 2.148 -0.5 00.0 14.1 114.5 38.6 5.0 GR 2.513 67.6 14.119.3 2.622 1.75 1.99 6 1325.1 23 137.6 2.4 3.9 2.135 -0.5 00.0 17.4 94.2 37.5 3.9 GR 2.523 70.5 17.4 20.8 2.625 2.03 1.78 1325.3 24 112.9 7.9 2.121 -0.5 00.0 17.1 79.0 37.1 0.0 DN 2.596 70.2 17.1 24.7 2.616 2.06 1.81 1325.4 28 118.0 8.3 2.116 -0.5 00.0 37.5 3.4 16.7 71.2 3.9 DN 2.573 69.9 16.7 24.1 2.615 2.10 1.84 -0.5 00.0 1325.6 29 130.9 5.6 5.7 2.114 15.7 55.1 37.5 0.2 DN 2.642 55.1 15.7 25.0 2.642 2.14 1.87 1325.7 28 166.0 9.1 1.8 2.119 -0.5 00.0 15.2 47.6 37.4 3.9 SN 2.588 47.6 15.2 22.0 2.632 1.90 2.17 6 1.3 2.129 1325.9 25 216.5 10.7 -0.5 00.0 13.5 44.3 36.5 2.6 SN 2.612 44.3 13.5 22.0 2.627 2.21 1.93 6 1326.0 -0.5 00.0 24 194.1 4.0 1.6 2.132 15.4 77.1 37.3 3.3 SN 2.503 68.8 15.4 19.8 2.623 2.24 1.95 6 1326.2 24 116.2 -0.5 00.0 2.2 2.103 19.0 74.6 37.6 4.8 SN 2.470 4.0 71.7 19.0 20.5 2.620 2.27 1.98 6 1326.3 27 5.3 2.056 -0.5 00.0 38.3 67.1 3.5 21.4 68.4 2.9 DN 2.518 68.4 21.4 24.8 2.617 2.30 2.01 6 1326.5 29 58.1 2.7 8.7 2.036 -0.5 00.0 21.5 72.2 38.9 5.0 DN 2.512 72.2 21.5 26.6 2.625 2.35 2.04 6

DEPTH M	GR	RT	RXO	PHIN	RHOB	DD	SPI	SWU	sxou	PHIS	VCL FVCL	RHOMAU	sxo	SW	PHIE RHOMA	POR-M	HC-M	FLAGS	
1326.6	31	57.4	2.8	8.8	2.048	-0.5	00.0	21.5	70.4	39.5	1.8 DN	2.560	70.4	21.5	27.3 2.631	2.39	2.07	6	\$
1326.8	29	59.5	3.8	5.1	2.052	-0.5	00.0	22.1	64.1	40.1	0.2 DN	2.562	64.1	22.1	26.1 2.623	2.43	2.10	6	\$
1326.9	26	115.7	10.2	1.7	2.042	-0.5	00.0	15.8	39.2	40.9	2.5 SN	2.629	39.2	15.8	26.2 2.644	2.47	2.14		\$
1327.1	23	207.7	7.8	1.2	2.032	-0.5	00.0	12.1	45.4	39.3	1.4 SN	2.589	45.4	`12.1	25.9 2.619	2.51	2.17	6	\$
1327.3	21	247.9	14.5	1.4	2.043	-0.5	00.0	10.9	33.0	39.8	1.9 SN	2.661	33,.0	10.9	26.4 2.671	2.55	2.21		\$
1327.4	23	265.7	6.7	1.6	2.066	-0.5	00.0	11.5	51.9	39.0	2.8 SN	2.555	51.9	11.5	23.8 2.633	2.58	2.24	6	\$
1327.6	23	223.5	3.5	1.8	2.102	-0.5	00.0	13.7	78.9	35.2	4.4 GR	2.487	67.2	13.7	20.8 2.615	2.61	2.27	6	\$
1327.7	26	147.4	5.6	2.4	2.117	-0.5	00.0	16.3	60.4	36.5	0.7 DN	2.564	60.4	16.3	22.3 2.628	2.65	2.30	6	\$
1327.9	28	103.5	6.7	4.1	2.117	-0.5	00.0	18.5	53.5	37.4	4.0 DN	2.591	53.5	18.5	22.9 2.635	2.68	2.32	6	\$
1328.0	32	72.0	6.6	5.7	2.113	-0.5	00.0	20.8	50.7	38.9	2.9 DN	2.642	50.7	20.8	24.6 2.655	2.72	2.35		\$
1328.2	37	59.3	5.6	8.5	2.119	-0.5	00.0	22.5	54.3	41.3	8.3 DN	2.623	54.3	22.5	24.2 2.664	2.76	2.38		\$
1328.3	42	59.5	8.8	8.6	2.133	-0.5	00.0	22.5	44.3	40.3	12.8 DN	2.639	44.3	22.5	23.1 2.697	2.79	2.41		\$
1328.5	41	65.0	5.6	7.8	2.114	-0.5	00.0	21.5	54.3	39.2	5.7 DN	2.632	54.3	21.5	24.7 2.659	2.83	2.44		\$
1328.6	35	65.7	9.0	5.4	2.071	-0.5	00.0	20.7	41.8	41.9	8.0 DN	2.629	41.8	20.7	25.3 2.671	2.87	2.47		\$
1328.8	29	82.7	8.8	5.0	2.051	-0.5	00.0	18.0	41.1	42.3	5.3 DN	2.646	41.1	18.0	26.6 2.673	2.91	2.50		\$
1328.9	30	89.2	7.9	5.2	2.068	-0.5	00.0	17.8	44.4	42.0	6.0 DN	2.630	44.4	17.8	25.7 2.661	2.95	2.53		\$
1329.1	31	88.4	11.2	4.8	2.090	-0.5	00.0	18.4	38.7	39.6	6.9 DN	2.649	38.7	18.4	24.7 2.682	2.99	2.57		\$
1329.2	32	93.1	11.7	4.6	2.088	-0.5	00.0	17.9	37.8	39.2	6.4 DN	2.653	37.8	17.9	24.8 2.684	3.02	2.60		\$
1329.4	29	89.7	10.1	5.0	2.085	-0.5	00.0	18.1	40.1	38.0	5.1 DN	2.656	40.1	18.1	25.3 2.680	3.06	2.63		\$
1329.5	28	74.1	9.4	6.9	2.093	-0.5	00.0	19.6	41.3	38.9	9.4 GR	2.647	41.3	19.6	24.8 2.692	3.10	2.66		\$
1329.7	25	62.0	15.2	10.5	2.096	-0.5	00.0	19.3	29.5	39.2	6.4 GR	2.819	29.5	19.3	28.8 2.855	3.14	2.69		\$
1329.8	28	48.5	12.7	15.0	2.099	-0.5	00.0	20.8	30.8	38.0	8.9 GR	2.861	30.8	20.8	30.0 2.902	3.19	2.73		\$
1330.0	33	41.8	10.2	18.6	2.082	-0.5	00.0	21.5	33.2	39.5	13.9 GR	2.849	33.2	21.5	30.4 2.908	3.24	2.77		\$
1330.1	38	47.2	18.9	16.1	2.080	-0.5	00.0	20.8	25.5	38.0	19.2 GR	2.797	25.5	20.8	28.2 2.901	3.28	2.80		\$
1330.3	37	57.4	8.5	11.3	2.088	-0.5	00.0	20.8	41.3	38.9	18.0 GR	2.639	41.3	20.8	25.0 2.739	3.32	2.83		\$
1330.5	33	62.6	13.7	7.4	2.113	-0.5	00.0	21.6	35.3	38.8	14.5 GR	2.643	35.3	21.6	23.3 2.715	3.35	2.86		\$
1330.6	32	83.0	29.9	9.4	2.132	-0.5	00.0	18.2	23.3	39.8	12.9 GR	2.759	23.3	18.2	24.8 2.846	3.39	2.89		\$
1330.8	38	58.0	19.1	14.1	2.161	-0.5	00.0	21.2	28.6	38.3	18.6 GR	2.767	28.6	21.2	24.2 2.876	3.43	2.92		\$
1330.9	51	40.1	12.7	21.5	2.212	-0.5	00.0	25.0	35.2	35.8	32.2 GR	2.754	35.2	25.0	21.8 2.916	3.43	2.92		
1331.1	80	35.9	12.8	30.5	2.308	-0.3	00.0	27.5	38.2	33.0	60.9 GR	2.699	38.2	27.5	15.2 2.965	3.43	2.92		
1331.2	107	28.4	8.3	36.0	2.388	-0.2	00.0	48.2	82.4	31.5	84.3 SD	2.680	82.4	48.2	2.5 2.915	3.43	2.92	8	3
1331.4	117	25.6	7.3	34.7	2.440	-0.2	00.0			30.9	96.8 SD	2.680	100.0	100.0	00.0 2.940	3.43	2.92	L	
1331.5	105	27.0	10.1	30.2	2.436	-0.3	00.0	50.1	76.1	31.2	85.7 GR	2.680	76.1	50.1	2.2 2.896	3.43	2.92	8	3
1331.7	90	24.8	6.4	27.7	2.408	-0.3	00.0	44.7	76.7	30.9	70.7 GR	2.680	76.7	44.7	6.3 2.848	3.43	2.92	8	3
1331.8	86	25.0	5.3	26.6	2.401	-0.3	00.0	40.2	73.6	29.7	61.8 DN	2.618	73.6	40.2	9.7 2.886	3.43	2.92		
1332.0	81	26.7	7.3	24.2	2.400	-0.3	00.0	40.1	64.3	27.9	56.6 DN	2.630	64.3	40.1	9.9 2.882	3.43	2.92		
1332.1	73	27.5	7.9	20.4	2.406	-0.5	00.0	42.6	66.4	29.8	48.8 DN	2.621	66.4	42.6	9.5 2.835	3.43	2.92		
1332.3	59	26.7	5.1	18.5	2.401	-0.5	00.0	44.5	83.1	30.0	40.0 GR	2.620	83.1	44.5	10.4 2.769	3.43	2.92		

Zone No. 4 Complex Lithology Results 24-10-94 RXO PHIN DEPTH M GR RT RHOB DD SPI SWU SXOU PHIS VCL FVCL RHOMAU SXO SW PHIE RHOMA POR-M HC-M FLAGS 1332.4 53 26.9 5.2 17.1 2.392 -0.5 00.0 44.6 81.4 30.6 33.6 GR 2.630 81.4 44.6 11.5 2.746 3.43 2.92 43.9 1332.6 50 28.8 4.6 16.7 2.399 -0.5 00.0 43.9 87.6 30.4 31.1 GR 2.638 84.8 11.6 2.738 2.92 3.43 85.9 1332.7 4.7 16.6 2.393 -0.5 00.0 42.7 29.8 GR 2.640 12.0 2.735 2.93 49 29.8 30.0 84.4 42.7 3.45 \$ 1332.9 4.3 16.9 2.399 -0.5 00.0 2.93 52 32.1 41.6 91.2 29.7 32.7 GR 2.634 83.9 41.6 11.3 2.742 3.45 1333.0 4.7 16.4 2.405 -0.5 00.0 52 34.6 41.2 89.7 29.8 33.3 GR 2.627 83.8 41.2 10.7 2.738 3.45 2.93 1333.2 52 34.4 4.7 15.7 2.387 -0.5 00.0 40.3 85.8 32.1 27.8 DN 2.636 83.4 40.3 12.2 2.719 3.46 2.94 1333.3 49 32.7 5.3 17.3 2.360 -0.5 00.0 37.6 73.8 34.6 29.8 GR 2.652 73.8 37.6 13.8 2.764 2.95 3.49 1333.5 52 29.6 4.4 20.0 2.328 -0.5 00.0 35.8 73.1 36.1 33.3 GR 2.651 73.1 35.8 15.5 2.787 3.49 2.95 3.5 23.3 2.333 -0.5 00.0 35.1 1333.7 61 26.6 36.2 79.2 42.1 GR 2.636 79.2 14.8 2.807 2.95 36.2 3.49 1333.8 3.5 25.7 2.344 -0.5 00.0 35.6 79.2 77 26.4 33.3 48.1 DN 2.646 79.2 35.6 14.2 2.841 2.95 3.49 1334.0 29.0 4.4 29.4 2.371 -0.5 00.0 34.0 72.7 30.8 62.9 DN 34.0 11.9 2.905 2.95 87 2.644 72.7 3.49 1334.1 95 33.7 4.6 27.4 2.390 -0.5 00.0 40.3 95.2 31.5 75.0 GR 2.680 83.4 40.3 5.0 2.829 3.49 2.95 1334.3 86 42.7 7.9 21.0 2.363 -0.5 00.0 31.4 59.7 33.3 46.3 DN 2.630 59.7 31.4 12.0 2.844 3.49 2.95 9.1 13.0 2.273 -0.5 00.0 1334.4 68 54.5 27.1 51.3 36.0 22.2 DN 2.654 51.3 27.1 17.3 2.755 3.51 2.97 1334.6 67.2 8.7 2.170 -0.5 00.0 22.6 63.3 39.2 3.5 DN 2.640 63.3 22.6 23.1 2.653 3.55 3.00 46 1334.7 94.4 7.0 2.119 -0.5 00.0 18.4 60.3 41.7 1.8 DN 18.4 24.7 2.633 31 2.623 60.3 3.59 3.03 -0.5 00.0 1334.9 24 142.8 4.7 2.096 15.6 67.1 40.0 0.5 DN 2.557 67.1 15.6 23.9 2.620 3.62 3.06 1335.0 24 220.8 3.2 2.096 -0.5 00.0 13.1 63.1 39.8 2.520 22.1 2.630 5.0 4.8 GR 63.1 13.1 3.66 3.09 1335.2 23 423.7 6.8 2.9 2.096 -0.5 00.0 9.452.7 39.5 4.4 GR 2.568 52.7 9.4 22.9 2.615 3.69 3.12 1335.3 24 820.2 3.1 2.108 -0.5 00.0 6.7 51.0 38.6 0.3 DN 2.619 51.0 6.7 24.0 2.621 3.16 3.73 1335.5 24 973.7 3.5 2.121 -0.5 00.0 58.9 38.9 0.5 DN 2.597 57.7 23.1 2.620 3.19 5.5 6.4 6.4 3.76 1335.6 25 962.8 3.6 2.122 -0.5 00.0 64.8 37.8 1.5 DN 2.591 57.8 22.9 2.619 3.22 4.6 6.4 6.4 3.80 984.0 36.5 22.6 2.623 3.25 1335.8 24 3.9 3.4 2.134 -0.5 00.0 6.5 71.1 0.4 DN 2.601 57.8 6.5 3.83 1335.9 23 1034.6 3.2 2.150 -0.5 00.0 79.3 35.5 2.570 20.7 2.634 3.28 3.5 6.6 4.4 GR 58.1 6.6 3.86 57.8 1336.1 22 1156.8 4.3 2.9 2.170 -0.5 00.0 6.5 74.2 35.6 3.6 GR 2.581 6.5 20.0 2.620 3.89 3.31 23 1351.7 3.1 2.166 -0.5 00.0 66.3 35.7 20.3 2.625 1336.2 5.2 5.9 3.7 GR 2.585 56.8 5.9 3.92 3.34 2.9 2.169 -0.5 00.0 5.8 69.2 34.5 2.581 56.5 20.0 2.623 3.37 1336.4 23 1471.3 4.3 GR 5.8 3.95 34.0 1336.5 20 1540.6 2.6 2.190 -0.5 00.0 5.8 73.3 1.5 GR 2.605 56.5 5.8 19.8 2.632 3.98 3.40 4.5 1336.7 20 1644.8 2.4 2.219 -0.5 00.0 5.9 70.2 33.4 1.1 GR 2.614 56.7 5.9 18.8 2.619 3.43 5.5 4.01 1336.9 19 1527.1 6.3 2.4 2.237 -0.5 00.0 6.3 67.9 34.0 0.6 GR 2.620 57.5 6.3 18.2 2.623 4.04 3.45 1337.0 20 1304.6 2.7 2.227 -0.5 00.0 34.8 1.6 GR 2.612 58.1 18.4 2.619 3.48 7.6 6.6 61.1 6.6 4.07 22 1089.9 2.8 2.215 -0.5 00.0 7.1 64.8 35.9 2.7 GR 2.598 59.0 7.1 18.5 2.631 3.50 1337.2 6.5 4.10 21 888.3 2.8 2.197 -0.5 00.0 7.7 74.2 37.4 2.0 GR 2.593 59.8 19.3 2.623 3.53 1337.3 7.7 4.13 4.6 -0.5 00.0 73.7 38.9 1337.5 21 812.2 4.3 2.6 2.165 7.7 1.8 GR 2.580 59.8 7.7 20.4 2.629 4.16 3.56 1337.6 18 789.5 2.4 2.123 -0.5 00.0 7.2 57.5 38.7 00.0 GR 2.587 57.5 7.2 22.5 2.627 4.19 3.59 1337.8 19 777.0 4.6 2.0 2.098 -0.5 00.0 7.2 64.8 39.5 0.6 GR 2.560 59.0 7.2 22.9 2.624 4.23 3.62 -0.5 00.0 7.4 1337.9 21 742.4 4.3 1.9 2.100 67.9 39.2 2.1 GR 2.546 59.4 7.4 22.3 2.619 4.26 3.66 7.9 1338.1 22 664.1 5.7 2.3 2.106 -0.5 00.0 60.2 39.2 3.2 GR 2.539 60.2 7.9 21.9 2.618 4.29 3.69

Zone No. Complex Lithology Results 24-10-94 DEPTH M GR RT RXO PHIN RHOB DD SPI SWU SXOU PHIS VCL FVCL RHOMAU SXO SW PHIE RHOMA POR-M HC-M FLAGS 1338.2 22 499.6 5.9 2.8 2.109 -0.5 00.0 8.9 58.1 39.2 3.0 GR 2.561 58.1 8.9 22.4 2.619 4.33 3.72 6 1338.4 20 349.1 3.6 2.100 -0.5 00.0 10.2 57.0 5.6 40.0 1.1 GR 2.587 57.0 10.2 23.8 2.634 4.36 3.75 1338.5 21 267.8 4.7 2.124 -0.5 00.0 11.9 63.3 39.8 2.2 GR 4.8 2.574 63.3 11.9 22.7 2.627 4.40 3.78 1338.7 5.2 2.153 -0.5 00.0 24 192.7 14.2 64.9 39.3 0.2 DN 2.602 64.9 14.2 22.5 2.623 4.43 3.81 1338.8 29 150.5 5.8 2.177 -0.5 00.0 63.3 39.9 5.2 16.3 0.4 DN 2.625 63.3 16.3 22.1 2.627 3.84 4.47 1339.0 33 136.4 5.6 2.169 -0.5 00.0 16.7 53.4 39.6 3.7 DN 2.639 53.4 16.7 22.1 2.654 3.87 4.50 1339.1 33 119.3 -0.5 00.0 5.2 2.162 18.4 64.6 41.0 2.7 DN 2.587 64.6 18.4 21.4 2.621 3.89 4.53 6 1339.3 31 70.5 4.4 2.172 -0.5 00.0 2.620 6.1 23.8 59.5 40.5 0.4 DN 59.5 23.8 21.7 2.622 3.92 4.57 1339.4 31 51.9 4.8 2.200 -0.5 00.0 29.0 64.2 39.5 5.8 1.6 DN 2.607 64.2 29.0 20.2 2.634 4.60 3.94 6 31 1339.6 50.8 4.6 2.200 -0.5 00.0 38.9 28.4 53.0 1.5 DN 2.652 53.0 28.4 21.0 2.658 4.63 3.96 1339.7 30 3.8 2.179 -0.5 00.0 53.8 29.9 81.0 39.1 4.3 DN 2.513 78.6 29.9 18.6 2.616 4.66 3.98 6 1339.9 28 71.3 8.8 2.5 2.155 -0.5 00.0 24.1 51.0 40.3 4.9 SN 2.587 51.0 24.1 20.4 2.634 4.01 4.69 1340.1 25 162.3 -0.5 00.0 2.0 2.158 16.5 53.9 39.8 3.8 SN 2.580 53.9 16.5 20.2 2.620 4.72 4.03 1340.2 229.6 -0.5 00.0 24 7.9 2.3 2.164 14.1 55.3 39.5 4.5 SN 2.573 55.3 14.1 19.8 2.618 4.75 4.06 1340.4 24 3.6 2.173 -0.5 00.0 38.6 149.5 16.7 56.0 0.2 DN 2.628 56.0 16.7 21.6 2.629 4.08 4.78 1340.5 28 72.9 8.0 2.174 -0.5 00.0 21.9 51.7 38.6 9.0 GR 2.640 51.7 21.9 21.8 2.678 4.11 4.82 1340.7 33 44.4 6.5 13.4 2.177 -0.5 00.0 25.9 51.2 42.5 14.5 GR 2.675 51.2 25.9 22.8 2.746 4.14 4.85 1340.8 44 31.3 3.6 17.7 2.172 -0.5 00.0 29.0 65.2 44.1 20.3 DN 2.643 65.2 29.0 23.3 2.729 4.89 4.16 1341.0 52 25.3 2.3 20.1 2.168 -0.5 00.0 31.3 77.9 44.5 17.7 DN 2.634 77.9 31.3 24.7 2.697 4.92 4.19 1341.1 2.3 20.2 2.170 -0.5 00.0 58 25.3 31.4 79.1 44.8 18.4 DN 2.627 79.1 31.4 24.4 2.694 4.21 4.96 1341.3 55 2.5 19.2 2.194 -0.5 00.0 78.7 27.6 31.4 45.2 16.2 DN 2.641 78.7 31.4 23.5 2.696 4.24 5.00 1341.4 54 30.4 3.0 17.6 2.211 -0.5 00.0 31.3 75.1 45.3 19.5 DN 2.625 75.1 31.3 21.6 2.697 5.03 4.26 1341.6 50 35.1 3.4 14.6 2.209 -0.5 00.0 30.2 73.0 51.9 10.5 DN 73.0 4.28 2.647 30.2 22.4 2.683 5.06 1341.7 47 37.5 2.7 12.7 2.198 -0.5 00.0 29.8 81.5 47.6 3.0 DN 2.635 78.5 29.8 23.3 2.647 5.10 4.31 1341.9 46 43.0 9.3 2.214 -0.5 00.0 30.7 89.1 44.1 3.8 DN 2.596 20.6 2.633 79.0 30.7 5.13 4.33 6 1342.0 57.1 4.4 7.3 2.227 -0.5 00.0 28.1 44.5 46 74.9 2.8 DN 2.601 74.9 28.1 19.6 2.633 5.16 4.35 1342.2 80.5 5.3 2.175 -0.5 00.0 54.2 44 21.8 43.3 2.3 DN 2.642 54.2 21.8 22.0 2.652 5.19 4.38 1342.3 38 132.5 4.6 2.094 -0.5 00.0 16.3 65.3 45.3 4.5 DN 2.531 65.3 16.3 22.9 2.619 5.23 4.41 6 197.1 -0.5 00.0 1342.5 35 4.9 2.031 12.0 53.0 48.1 4.5 DN 2.573 53.0 12.0 26.5 2.624 5.27 4.44 1342.6 37 224.1 5.6 2.023 -0.5 00.0 10.9 51.9 46.7 2.1 DN 2.614 51.9 10.9 28.1 2.628 5.31 4.48 1342.8 37 172.4 7.5 2.037 -0.5 00.0 12.2 52.7 46.6 2.8 DN 12.2 4.8 2.639 52.7 28.4 2.652 5.36 4.52 1342.9 38 112.7 9.3 2.067 -0.5 00.0 15.2 55.5 47.5 4.4 DN 2.643 55.5 15.2 27.5 2.663 5.40 4.56 1343.1 39 79.9 3.2 11.3 2.090 -0.5 00.0 18.3 66.9 47.3 4.9 DN 2.615 66.9 18.3 26.8 2.641 5.44 4.59 1343.3 41 60.7 2.5 13.2 2.110 -0.5 00.0 20.9 74.5 47.7 2.4 DN 2.634 73.1 20.9 27.3 2.644 5.48 4.62 1343.4 2.2 14.6 2.115 -0.5 00.0 23.1 78.4 44 48.3 48.5 5.0 DN 2.629 74.6 23.1 27.0 2.650 5.52 4.65 2.5 16.2 2.113 -0.5 00.0 72.3 1343.6 46 45.9 23.1 44.3 7.1 DN 2.644 72.3 23.1 27.5 2.672 5.56 4.69 2.7 16.0 2.129 -0.5 00.0 23.5 72.7 44.0 10.7 DN 1343.7 50 46.4 2.626 72.7 23.5 25.9 2.670 4.72 5.60 1343.9 50 47.8 2.5 14.5 2.145 -0.5 00.0 24.1 78.0 44.2 5.7 DN 2.635 75.2 24.1 25.7 2.657 5.64 4.75

Zone No. Complex Lithology Results 24-10-94 SXOU DEPTH M GR RT RXO PHIN RHOB DD SPI SWU PHIS VCL FVCL RHOMAU SXO SW PHIE RHOMA POR-M HC-M FLAGS 1344.0 49 52.2 3.0 12.3 2.141 -0.5 00.0 23.7 72.8 44.3 5.0 DN 2.619 72.8 23.7 25.0 2.643 5.68 4.77 1344.2 46 60.1 2.6 10.9 2.114 -0.5 00.0 22.0 44.9 22.0 77.0 1.5 DN 2.603 73.8 26.0 2.631 5.72 4.81 6 1344.3 43 71.9 2.8 10.9 2.092 -0.5 00.0 19.7 72.6 46.2 3.6 DN 2.587 72.3 19.7 26.3 2.627 5.76 4.84 6 1344.5 41 86.0 2.4 11.1 2.090 -0.5 00.0 17.8 76.1 45.8 17.8 1.9 DN 2.609 70.8 27.1 2.620 4.87 6 5.80 1344.6 42 82.7 3.1 12.0 2.085 -0.5 00.0 17.6 66.3 44.3 3.0 DN 2.638 66.3 17.6 27.9 2.651 4.91 5.84 1344.8 44 76.2 2.9 13.1 2.084 -0.5 00.0 18.1 67.3 44.1 4.8 DN 2.637 67.3 18.1 28.0 2.657 5.89 4.94 1344.9 -0.5 00.0 43 71.6 2.3 13.1 2.091 19.0 77.1 44.9 4.4 DN 2.615 71.7 19.0 27.4 2.638 5.93 4.98 6 2.1 12.6 2.099 1345.1 42 -0.5 00.0 19.2 71.8 80.9 44.9 3.2 DN 2.619 71.9 19.2 27.2 2.636 5.97 5.01 1345.2 42 78.4 2.3 11.0 2.092 -0.5 00.0 18.8 79.2 45.7 3.2 DN 2.594 71.6 18.8 26.5 2.632 6.01 5.04 6 1345.4 41 95.5 2.7 9.5 2.071 -0.5 00.0 17.1 72.7 2.578 46.2 2.3 DN 70.2 17.1 26.8 2.631 5.08 6.05 6 1345.5 41 114.0 8.5 2.052 -0.5 00.0 15.5 72.5 44.8 1.1 DN 2.570 68.9 15.5 27.3 2.617 6.09 5.11 1345.7 9.4 2.060 39 111.0 -0.5 00.0 15.8 71.1 44.3 4.9 DN 2.556 69.1 15.8 26.5 2.627 5.14 6.13 1345.8 39 91.9 2.6 11.6 2.082 -0.5 00.0 17.1 72.9 42.8 4.8 DN 2.593 70.2 17.1 26.9 2.621 6.17 5.18 1346.0 35 78.6 2.6 13.6 2.108 -0.5 00.0 18.4 74.0 44.2 6.4 DN 2.617 71.3 18.4 26.6 2.648 6.21 5.21 1346.1 35 70.2 2.4 14.2 2.133 -0.5 00.0 19.8 77.5 43.7 5.8 DN 2.639 72.3 19.8 26.1 2.661 6.25 5.24 1346.3 38 67.7 2.2 14.2 2.173 -0.5 00.0 21.2 86.4 43.0 8.8 DN 2.633 73.3 21.2 23.9 2.666 5.27 6.29 1346.5 2.4 13.6 2.226 -0.5 00.0 39 73.0 22.1 89.0 42.4 10.1 DN 2.640 74.0 22.1 21.3 2.675 5.30 6.32 1346.6 42 79.1 2.6 12.3 2.243 -0.5 00.0 22.2 89.7 40.4 7.9 DN 2.644 74.0 22.2 20.6 2.670 6.35 5.32 -0.5 00.0 1346.8 41 73.7 3.8 13.4 2.208 21.5 70.7 39.6 11.9 DN 2.632 70.7 21.5 21.6 2.677 6.39 5.35 -0.5 00.0 1346.9 44 58.6 3.3 15.7 2.166 22.0 69.4 41.3 14.5 DN 2.632 69.4 22.0 23.7 2.689 6.42 5.38 1347.1 46 45.4 3.8 19.7 2.159 -0.5 00.0 23.2 61.1 45.0 26.6 GR 2.637 61.1 23.2 23.5 2.767 6.46 5.40 1347.2 51 36.4 2.3 19.9 2.177 -0.5 00.0 26.6 79.7 46.3 16.6 DN 76.7 26.6 2.648 24.5 2.705 6.50 5.43 1347.4 57 2.4 20.2 2.180 -0.5 00.0 28.3 30.0 77.4 47.4 18.2 DN 2.641 77.4 30.0 24.2 2.704 6.53 5.46 1347.5 61 3.1 21.3 2.190 -0.5 00.0 33.2 22.5 68.9 43.6 26.6 DN 2.646 68.9 33.2 22.7 2.765 6.57 5.48 1347.7 63 19.2 2.7 23.9 2.219 -0.5 00.0 35.9 74.7 43.4 33.4 DN 2.633 74.7 35.9 21.2 2.777 6.57 5.48 1347.8 3.3 25.6 2.265 -0.5 00.0 64 16.8 39.7 71.2 40.2 40.2 DN 2.655 71.2 39.7 18.8 2.832 6.57 5.48 1348.0 68 15.7 3.2 27.9 2.313 -0.5 00.0 42.5 76.4 36.0 48.5 GR 2.661 76.4 42.5 16.2 2.860 6.57 5.48 1348.1 16.1 3.9 31.1 2.358 -0.5 00.0 77 43.0 72.5 33.0 58.1 GR 2.708 72.5 43.0 13.9 2.921 6.57 5.48 1348.3 3.9 34.1 2.408 -0.3 00.0 84 16.5 43.4 74.3 29.4 64.3 GR 2.822 74.3 43.4 12.4 2.965 6.57 5.48 1348.4 6.4 34.0 2.430 -0.2 00.0 52.2 78.9 28.3 78.9 92 18.8 72.9 GR 2.680 52.2 5.6 2.927 6.57 5.48 1348.6 -0.1 00.0 53.7 74.0 GR 93 18.2 7.0 32.1 2.443 76.7 26.8 2.680 76.7 53.7 5.3 2.920 6.57 5.48 1348.7 92 17.8 7.8 30.7 2.450 -0.1 00.0 53.6 71.7 26.8 72.8 GR 2.680 71.7 53.6 5.7 2.912 5.48 6.57 1348.9 4.8 30.0 2.485 -0.1 00.0 48.6 85.0 26.2 67.8 GR 85.0 48.6 7.3 2.954 87 19.5 2.784 6.57 5.48 1349.0 4.8 30.9 2.495 -0.1 00.0 77.8 84 19.5 49.8 26.5 64.7 GR 2.831 77.8 49.8 7.9 2.980 0.00 0.00 1349.2 4.5 32.2 2.480 -0.1 00.0 89 19.1 49.0 78.6 26.9 69.4 GR 2.798 78.6 49.0 7.6 2.977 0.00 0.00 -0.1 00.0 1349.3 95 20.3 11.1 33.5 2.449 53.6 62.6 28.0 75.6 GR 2.680 62.6 53.6 3.6 2.937 0.00 0.00 10.5 35.0 2.456 1349.5 97 19.9 -0.1 00.0 54.3 65.5 28.2 77.2 GR 2.680 65.5 54.3 3.2 2.953 0.00 0.00 8 -0.1 00.0

1349.7

94

19.5

8.0 34.1 2.507

54.5

72.7

26.1

74.3 GR

2.680

54.5

3.8 2.983

0.00

0.00

72.7

DEPTH M GR RXO PHIN RHOB DD SPI SWU SXOU PHIS VCL FVCL RHOMAU SXO SW PHIE RHOMA POR-M HC-M FLAGS RT6.3 32.6 2.527 -0.1 00.0 57.9 81.2 26.4 74.3 GR 2.680 81.2 3.8 2.986 0.00 8 1349.8 94 17.2 57.9 0.00 9.9 31.7 2.500 -0.1 00.0 55.6 66.3 26.2 75.9 GR 2.680 66.3 55.6 3.5 2.958 0.00 1350.0 95 18.8 0.00 8 1350.1 94 9.9 32.2 2.481 -0.1 00.0 54.9 65.8 27.1 74.8 GR 2.680 65.8 0.00 0.00 19.2 54.9 3.7 2.949 1350.3 92 18.9 10.3 35.2 2.514 -0.1 00.0 55.1 63.7 27.1 73.1 GR 2.680 63.7 55.1 4.1 2.995 0.00 0.00 1350.4 86 19.1 10.7 35.5 2.544 -0.1 00.0 49.4 52.1 25.5 67.0 GR 3.067 52.1 49.4 7.9 3.064 0.00 0.00 5 0.00 52.6 1350.6 82 11.3 33.6 2.573 -0.1 00.0 47.6 52.6 23.4 63.2 GR 3.095 47.6 7.7 3.073 0.00 1350.7 74 10.0 30.9 2.649 -0.1 00.0 49.5 60.7 19.9 55.2 GR 3.151 60.7 49.5 7.2 3.102 0.00 0.00 5 25.0 5 1350.9 69 25.6 30.3 2.696 -0.1 00.0 51.4 40.2 20.7 50.3 GR 3.203 51.4 51.4 7.2 3.134 0.00 0.00 25.6 43.3 3.129 54.6 54.6 7.5 3.094 0.00 5 1351.0 75 19.6 19.2 30.8 2.629 -0.1 00.0 54.6 20.5 55.7 GR 0.00 1351.2 84 16.2 9.5 33.1 2.515 -0.1 00.0 52.9 53.6 23.8 64.4 GR 2.982 53.6 52.9 8.7 3.039 0.00 0.00 1351.3 94 11.7 8.3 33.4 2.449 -0.1 00.0 69.7 71.3 29.3 74.4 GR 2.680 71.3 69.7 3.8 2.936 0.00 0.00 8 1351.5 91 88.4 29.4 71.7 GR 88.4 74.8 4.4 2.930 0.00 9.9 5.1 34.5 2.427 -0.1 00.0 74.8 2.680 0.00 63.5 102.5 29.1 91.3 63.5 9.0 2.915 0.00 0.00 1351.6 89 10.1 2.3 32.8 2.407 -0.1 00.0 69.6 GR 2.647 1351.8 84 1.9 31.1 2.413 -0.1 00.0 61.0 108.4 28.2 65.2 GR 2.697 90.6 61.0 10.0 2.908 0.00 0.00 10.9 1351.9 85 11.9 13.4 30.3 2.422 -0.1 00.0 59.6 44.0 27.8 66.2 GR 2.686 59.6 59.6 9.2 2.956 0.00 0.00

26.4

26.4

23.6

67.6 SD

71.2 GR

71.1 GR

68.8 GR

70.8 GR

75.0 SD

2.706

2.680

2.680

2.680

2.912 77.0

2.680 83.5

56.3

66.9

67.7

92.3

2.680 63.7 63.7

56.3

65.2

67.6

63.1

66.9

65.8

8.9 2.968

4.5 2.918

4.6 2.955

6.9 3.005

4.6 2.962

3.7 2.946

3.5 2.935

0.00

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0.00

5

8

Zone No. 4

1352.1 87

1352.2 91

1352.4 90

1352.6 88

1352.7 90

1352.9 96

1353.0 97

13.4

13.2

12.2

12.0

12.5

13.2

10.7 30.8 2.429

5.2 32.2 2.522

9.0 31.4 2.449 -0.1 00.0

8.7 32.2 2.490 -0.1 00.0

6.1 30.4 2.498 -0.1 00.0

-0.1 00.0

-0.1 00.0

1.9 30.7 2.516 -0.1 00.0 66.9 140.1 24.3

14.2 12.5 30.0 2.489 -0.2 00.0 63.7 59.3 24.5 75.7 SD

56.3

65.2

67.6

49.3

66.9

67.7

63.1 77.0 25.5

65.8 83.5 23.7

Complex Lithology Results

24-10-94

### Complex Lithology Results 24-10-94

Zone No. 4

### Hydrocarbon Volume Report

FROM	M	1316.431
TO	M	1347.978
INTERVAL	M	31.547
PHIE Cut off		0.050
SW Cut Off		0.500
Vclay Cut Off		0.300
Net Pay	M	27.584
Average PHIE	%	23.808
Average SW	%	16.705
Average Vclay	%	5.293
Integrated PHI	M	6.567
um PHI*(1-SW)	M	5.479

DEPTH M	GR	RT	RXO E	PHIN	RHOB	DD	SPI	SWU	sxou	PHIS	VCL FVCL	RHOMAU	sxo	SW	PHIE RHOMA	POR-M	HC-M	FLAGS	
1349.0	84	19.5	4.8 3	30.9	2.495	-0.1	00.0	49.8	77.8	26.5	64.7 GR	2.831	77.8	49.8	7.9 2.980	0.00	0.00		
1349.2	89	19.1	4.5 3	32.2	2.480	-0.1	00.0	49.0	78.6	26.9	69.4 GR	2.798	78.6	49.0	7.6 2.977	0.00	0.00		
1349.3	95	20.3	11.1 3	33.5	2.449	-0.1	00.0	51.5	58.9	28.0	75.6 GR	2.680	58.9	51.5	4.5 2.937	0.00	0.00	8	
1349.5	97	19.9	10.5 3	35.0	2.456	-0.1	00.0	52.4	61.9	28.2	77.2 GR	2.680	61.9	52.4	4.0 2.953	0.00	0.00	8	
1349.7	94	19.5	8.0 3	34.1	2.507	-0.1	00.0	52.2	68.2	26.1	74.3 GR	2.680	68.2	52.2	4.8 2.983	0.00	0.00	8	
1349.8	94	17.2	6.3 3	32.6	2.527	-0.1	00.0	55.5	76.1	26.4	74.3 GR	2.680	76.1	55.5	4.8 2.986	0.00	0.00	8	
1350.0	95	18.8	9.9 3	31.7	2.500	-0.1	00.0	53.5	62.5	26.2	75.9 GR	2.680	62.5	53.5	4.4 2.958	0.00	0.00	8	
1350.1	94	19.2	9.9 3	32.2	2.481	-0.1	00.0	52.6	61.8	27.1	74.8 GR	2.680	61.8	52.6	4.7 2.949	0.00	0.00	8	
1350.3	92	18.9	10.3 3	35.2	2.514	-0.1	00.0	52.7	59.5	27.1	73.1 GR	2.680	59.5	52.7	5.2 2.995	0.00	0.00	8	
1350.4	86	19.1	10.7 3	35.5	2.544	-0.1	00.0	49.4	52.1	25.5	67.0 GR	3.067	52.1	49.4	7.9 3.064	0.00	0.00	5	
1350.6	82	22.3	11.3 3	33.6	2.573	-0.1	00.0	47.6	52.6	23.4	63.2 GR	3.095	52.6	47.6	7.7 3.073	0.00	0.00	5	
1350.7	74	25.0	10.0 3	30.9	2.649	-0.1	00.0	49.5	60.7	19.9	55.2 GR	3.151	60.7	49.5	7.2 3.102	0.00	0.00	5	
1350.9	69	25.6	25.6 3	30.3	2.696	-0.1	00.0	51.4	40.2	20.7	50.3 GR	3.203	51.4	51.4	7.2 3.134	0.00	0.00	5	
1351.0	75	19.6	19.2 3	30.8	2.629	-0.1	00.0	54.6	43.3	20.5	55.7 GR	3.129	54.6	54.6	7.5 3.094	0.00	0.00	5	
1351.2	84	16.2	9.5 3	33.1	2.515	-0.1	00.0	52.9	53.6	23.8	64.4 GR	2.982	53.6	52.9	8.7 3.039	0.00	0.00	5	
1351.3	94	11.7	8.3 3	33.4	2.449	-0.1	00.0	66.8	66.9	29.3	74.4 GR	2.680	66.9	66.8	4.8 2.936	0.00	0.00	8	
1351.5	91	9.9	5.1 3	34.5	2.427	-0.1	00.0	71.3	82.4	29.4	71.7 GR	2.680	82.4	71.3	5.6.2.930	0.00	0.00	8	
1351.6	89	10.1	2.3 3	32.8	2.407	-0.1	00.0	61.3	97.7	29.1	69.6 GR	2.651	90.7	61.3	10.0 2.920	0.00	0.00		
1351.8	84	10.9	1.9 3	31.1	2.413	-0.1	00.0	61.0	108.4	28.2	65.2 GR	2.658	90.6	61.0	10.0 2.910	0.00	0.00		
1351.9	85	11.9	13.4 3	30.3	2.422	-0.1	00.0	59.6	44.0	27.8	66.2 GR	2.683	59.6	59.6	9.2 2.957	0.00	0.00		
1352.1	87	13.4	10.7 3	30.8	2.429	-0.1	00.0	56.2	49.3	26.4	67.6 SD	2.696	56.2	56.2	8.9 2.968	0.00	0.00		
1352.2	91	13.2	9.0 3	31.4	2.449	-0.1	00.0	62.1	62.3	26.4	71.2 GR	2.680	62.3	62.1	5.7 2.918	0.00	0.00	8	
1352.4	90	12.2	8.7 3	32.2	2.490	-0.1	00.0	64.4	63.0	23.6	71.1 GR	2.680	64.4	64.4	5.7 2.955	0.00	0.00	8	
1352.6	88	12.0	5.2 3	32.2	2.522	-0.1	00.0	63.1	77.0	25.5	68.8 GR	2.912	77.0	63.1	6.9 3.005	0.00	0.00	5	
1352.7	90	12.5	1.9 3	30.7	2.516	-0.1	00.0	63.7	130.3	24.3	70.8 GR	2.680	91.4	63.7	5.8 2.962	0.00	0.00	8	
1352.9	96	13.2	6.1 3	30.4	2.498	-0.1	00.0	63.2	78.4	23.7	75.0 SD	2.680	78.4	63.2	4.6 2.946	0.00	0.00	8	
1353.0	97	14.2	12.5 3	30.0	2.489	-0.2	00.0	61.2	55.9	24.5	75.7 SD	2.680	61.2	61.2	4.4 2.935	0.00	0.00	8	
1353.2	100	15.6	12.8 3	33.6	2.489	-0.2	00.0	52.8	46.1	23.4	69.7 MN	2.916	52.8	52.8	8.3 3.024	0.00	0.00	5	
1353.3	97	18.1	12.3 2	29.0	2.487	-0.2	00.0	53.1	52.9	23.3	70.1 SD	2.680	53.1	53.1	6.1 2.924	0.00	0.00	8	
1353.5	92	24.7	14.7	19.2	2.464	-0.2	00.0	54.7	54.5	23.2	46.8 DN	2.653	54.7	54.7	7.1 2.870	0.00	0.00		
1353.6	75	36.3	12.3	6.7	2.380	-0.4	00.0	57.9	61.1	25.9	12.0 DN	2.639	61.1	57.9	12.1 2.681	0.00	0.00		
1353.8	53	71.0	28.0	1.5	2.222	-0.5	00.0	34.1	31.9	30.6	6.7 SN	2.639	34.1	34.1	17.9 2.669	0.03	0.02	\$	;
1353.9	42	260.1	13.9	0.9	2.101	-0.5	00.0	15.5	37.0	36.6	3.5 SN	2.626	37.0	15.5	23.1 2.647	0.06	0.05	\$	
1354.1	38	882.0	8.8	0.9	2.027	-0.5	00.0	7.9	42.5	38.7	3.0 SN	2.583	42.5	7.9	25.6 2.625	0.10	0.08	6 \$	
1354.2	40	1122.8	7.5		2.016		00.0	7.0	45.7	40.1	3.0 SN	2.562	45.7	7.0	25.8 2.624	0.14	0.12	6 \$	
1354.4	41	1257.7	4.2		2.024		00.0	7.0	63.5	39.2	3.8 SN	2.485	58.7	7.0	24.1 2.633	0.18	0.15	6 \$	
1354.5		1221.4			2.045		00.0	7.3	69.1	39.3	4.0 SN	2.492	59.2	7.3	23.3 2.621	0.21	0.19	6 \$	
1354.7		1160.9			2.059		00.0	7.6	73.6	39.3	4.0 SN	2.497	59.7	7.6	22.7 2.626	0.25	0.22	6 \$	

DEPTH M	GR	RT	RXO I	PHIN	RHOB	DD	SPI	SWU	sxou	PHIS	VCL FVCL	RHOMAU	sxo	SW	PHIE RHOMA	POR-M	HC-M	FLAGS	
1354.8	41	1090.0	3.1	1.2	2.066	-0.5	00.0	7.9	78.2	39.2	3.8 SN	2.497	60.2	7.9	22.4 2.623	0.28	0.25	6	\$
1355.0	40	1118.2	4.0	1.1	2.066	-0.5	00.0	7.8	68.7	38.9	3.6 SN	2.501	60.1	7.8	22.5 2.626	0.32	0.28	6	\$
1355.1	38	1101.4	3.5	1.1	2.049	-0.5	00.0	7.7	72.1	39.8	3.4 SN	2.494	59.9	7.7	23.2 2.618	0.35	0.31	6	\$
1355.3	38	1070.1	3.1	1.2	2.050	-0.5	00.0	7.8	76.4	40.0	3.6 SN	2.493	60.1	7.8	23.1 2.619	0.39	0.35	6	\$
1355.4	38	1027.0	2.7	1.3	2.050	-0.5	00.0	8.0	80.9	40.5	3.8 SN	2.492	60.3	8.0	23.1 2.619	0.42	0.38	6	\$
1355.6	40	883.3	2.8	1.5	2.056	-0.5	00.0	8.6	81.5	40.7	4.3 SN	2.486	61.3	8.6	22.7 2.617	0.46	0.41	6	\$
1355.8	41	578.7	3.1	1.9	2.054	-0.5	00.0	10.5	75.2	40.8	0.4 DN	2.515	63.7	10.5	24.0 2.618	0.49	0.44	6	\$
1355.9	41	377.7	3.0	2.6	2.066	-0.5	00.0	13.1	78.1	40.4	2.3 DN	2.498	66.6	13.1	23.2 2.634	0.53	0.47	6	\$
1356.1	42	287.3	3.4	3.0	2.075	-0.5	00.0	15.0	74.7	40.3	3.5 DN	2.489	68.5	15.0	22.6 2.633	0.56	0.50	6	\$
1356.2	43	230.8	2.8	3.0	2.082	-0.5	00.0	16.9	82.5	39.5	3.7 DN	2.484	70.1	16.9	22.1 2.628	0.60	0.53	6	\$
1356.4	42	215.2	3.8	2.7	2.084	-0.5	00.0	17.7	71.9	39.3	2.8 DN	2.486	70.7	17.7	22.1 2.624	0.63	0.56	6	\$
1356.5	44	220.0	3.1	2.5	2.077	-0.5	00.0	17.4	78.5	38.4	2.4 DN	2.482	70.5	17.4	22.3 2.619	0.66	0.59	6	\$
1356.7	44	221.4	3.8	2.4	2.080	-0.5	00.0	17.5	72.3	38.1	2.2 DN	2.485	70.6	17.5	22.2 2.620	0.70	0.62	6	\$
1356.8	45	216.1	4.4	2.8	2.079	-0.5	00.0	17.2	65.3	38.3	3.3 DN	2.507	65.3	17.2	22.7 2.629	0.73	0.64	6	\$
1357.0	44	205.9	3.8	3.9	2.087	-0.5	00.0	17.7	70.0	37.7	1.4 DN	2.517	70.0	17.7	23.1 2.626	0.77	0.67	6	\$
1357.1	44	198.4	3.4	6.4	2.098	-0.5	00.0	17.3	71.3	38.2	3.2 DN	2.540	70.4	17.3	23.7 2.620	0.80	0.70	6	\$
1357.3	44	147.4	3.1	11.0	2.120	-0.5	00.0	18.7	68.8	36.8	0.5 DN	2.641	68.8	18.7	26.5 2.643	0.84	0.74		\$
1357.4	43	103.6	2.9	16.2	2.140	-0.5	00.0	20.6	70.6	35.6	14.4 DN	2.615	70.6	20.6	24.7 2.680	0.88	0.77		\$
1357.6	44	74.2	2.8	19.8	2.166	-0.5	00.0	23.2	70.0	35.0	20.5 DN	2.639	70.0	23.2	24.1 2.726	0.92	0.79		\$
1357.7	45	53.6	2.9	21.2	2.197	-0.5	00.0	27.1	71.1	34.7	26.1 GR	2.634	71.1	27.1	22.3 2.752	0.95	0.82		\$
1357.9	45	42.0	3.0	21.7	2.217	-0.5	00.0	31.0	71.3	36.9	26.1 GR	2.650	71.3	31.0	21.7 2.768	0.99	0.84		\$
1358.0	46	38.0	4.4	22.6	2.219	-0.5	00.0	32.0	58.4	37.4	27.2 GR	2.703	58.4	32.0	22.0 2.846	1.02	0.86		\$
1358.2	43	35.6	4.0	22.7	2.203	-0.5	00.0	32.7	59.8	37.0	24.7 GR	2.708	59.8	32.7	23.1 2.840	1.05	0.89		\$
1358.3	43	34.0	5.5	22.5	2.201	-0.5	00.0	32.7	50.1	37.0	24.4 GR	2.761	50.1	32.7	24.0 2.881	1.09	0.91		\$
1358.5	42	28.2	5.9	21.8	2.200	-0.5	00.0	36.0	48.3	35.2	23.3 GR	2.769	48.3	36.0	24.1 2.884	1.13	0.94		\$
1358.6	47	20.0	5.0	21.5	2.212	-C.5	00.0	43.6	55.0	36.4	28.2 GR	2.687	55.0	43.6	21.6 2.840	1.16	0.96		\$
1358.8	53	15.2	4.8	21.7	2.251	-0.5	00.0	50.9	59.5	33.0	33.9 GR	2.656	59.5	50.9	19.0 2.830	1.16	0.96		
1359.0	61	11.9	4.0	25.2	2.296	-0.5	00.0	56.7	66.1	31.6	42.6 GR	2.654	66.1	56.7	16.8 2.857	1.16	0.96		
1359.1	69	10.1	3.4	29.2	2.355	-0.5	00.0	61.8	75.2	28.8	49.8 GR	2.694	75.2	61.8	14.5 2.898	1.16	0.96		
1359.3	74	9.9	4.6	30.8	2.405	-0.4	00.0	62.8	67.3	25.8	55.3 GR	2.778	67.3	62.8	12.8 2.957	1.16	0.96		
1359.4	69	11.9	3.1	25.2	2.440	-0.4	00.0	67.5	96.9	22.0	49.8 GR	2.669	92.4	67.5	9.6 2.861	1.16	0.96		
1359.6	60	16.3	4.2	18.5	2.476	-0.4	00.0	71.6	103.8	17.1	40.7 SD	2.642	93.5	71.6	7.2 2.796	1.16	0.96		
1359.7	50	23.1	8.9	16.7	2.525	-0.4	00.0	69.9	81.3	13.3	31.4 GR	2.704	81.3	69.9	7.0 2.836	1.16	0.96		
1359.9	48	26.2	52.5	20.1	2.576	-0.4	00.0	55.1	27.3	12.7	29.5 GR	2.944	55.1	55.1	11.0 3.006	1.16	0.96	5	
1360.0	51	21.2	12.9	24.4	2.557	-0.5	00.0	54.2	47.5	19.6	32.4 GR	3.008	54.2	54.2	13.0 3.046	1.16	0.96	5	
1360.2	53	13.6	4.7	26.8	2.478	-0.5	00.0	61.4	70.2	26.4	34.7 GR	2.914	70.2	61.4	14.7 2.981	1.16	0.96	5	
1360.3	59	9.7	4.5	27.8	2.401	-0.5	00.0	66.3	66.5	28.9	40.6 GR	2.827	66.5	66.3	15.5 2.949	1.16	0.96		
1360.5	65	8.3	2.8	28.8	2.351	-0.5	00.0	68.3	81.7	30.2	46.5 GR	2.689	81.7	68.3	15.1 2.875	1.16	0.96		

DEPTH M GR	RT	RXO PHIN RHOB	DD SPI	SWU	SXOU	PHIS	VCL FVCL	RHOMAU	sxo	SW	PHIE RHOMA	POR-M	HC-M	FLAGS
1360.6 73	7.8	2.5 29.5 2.332	-0.5 00.0	67.3	83.8	30.3	53.6 GR	2.631	83.8	67.3	14.7 2.860	1.16	0.96	
1360.8 80	8.0	3.0 31.1 2.331	-0.5 00.0	65.5	75.1	28.9	51.3 SD	2.699	75.1	65.5	15.9 2.904	1.16	0.96	
1360.9 85	8.4	2.9 32.4 2.345	-0.5 00.0	63.3	77.2	29.4	57.0 SD	2.692	77.2	63.3	14.7 2.914	1.16	0.96	
1361.1 81	8.2	3.2 32.3 2.357	-0.5 00.0	64.5	75.3	30.6	62.1 GR	2.665	75.3	64.5	13.2 2.919	1.16	0.96	
1361.2 69	7.2	3.6 31.0 2.344	-0.5 00.0	69.7	69.0	32.0	50.2 GR	2.741	69.7	69.7	15.8 2.927	1.16	0.96	
1361.4 51	6.0	2.7 29.0 2.299	-0.5 00.0	76.9	74.1	33.3	32.5 GR	2.761	76.9	76.9	20.6 2.880	1.16	0.96	
1361.5 46	5.5	1.8 28.8 2.250	-0.5 00.0	79.3	88.3	34.8	27.1 GR	2.693	88.3	79.3	22.7 2.798	1.16	0.96	
1361.7 43	5.4	1.4 29.1 2.235	-0.5 00.0	79.4	96.7	34.5	24.1 GR	2.672	95.5	79.4	23.8 2.752	1.16	0.96	
1361.8 50	5.5	1.8 30.3 2.255	-0.5 00.0	77.4	86.4	33.5	31.4 GR	2.704	86.4	77.4	22.2 2.827	1.16	0.96	
1362.0 53	6.2	2.3 30.2 2.292	-0.5 00.0	74.3	78.9	32.6	33.9 GR	2.758	78.9	74.3	20.9 2.879	1.16	0.96	
1362.2 56	6.4	2.0 29.3 2.301	-0.4 00.0	74.6	88.7	32.4	37.3 GR	2.688	88.7	74.6	19.0 2.830	1.16	0.96	
1362.3 56	6.7	2.0 28.8 2.304	-0.4 00.0	73.8	89.9	31.8	36.9 GR	2.681	89.9	73.8	18.7 2.821	1.16	0.96	
1362.5 63	7.3	2.7 30.1 2.317	-0.4 00.0	69.3	78.1	30.7	43.9 GR	2.708	78.1	69.3	17.4 2.885	1.16	0.96	
1362.6 72	7.9	3.2 35.1 2.341	-0.4 00.0	62.5	68.5	30.6	53.3 GR	2.816	68.5	62.5	17.1 2.959	1.16	0.96	
1362.8 84	8.9	3.9 37.8 2.357	-0.4 00.0	61.4	68.7	31.5	64.7 GR	2.800	68.7	61.4	13.1 2.966	1.16	0.96	8
1362.9 91	8.5	3.9 40.0 2.361	-0.3 00.0	77.1	93.4	32.6	72.1 GR	2.680	93.4	77.1	5.5 2.926	1.16	0.96	8
1363.1 96	8.2	6.5 38.5 2.400	-0.2 00.0	80.0	77.3	31.0	77.0 GR	2.680	80.0	80.0	4.1 2.941	1.16	0.96	8
1363.2 102	8.4	4.7 37.4 2.441	-0.2 00.0	81.0	96.2	30.8	82.5 GR	2.680	95.9	81.0	2.7 2.961	1.16	0.96	8
1363.4 107	8.3	4.7 36.0 2.470	-0.1 00.0	83.0	101.6	31.2	87.1 GR	2.680	96.3	83.0	1.7 2.971	1.16	0.96	8
1363.5 115	8.9	5.9 36.0 2.474	-0.1 00.0			30.1	95.1 GR	2.680	100.0	100.0	00.0 2.973	1.16	0.96 1	•
1363.7 113	9.9	7.5 35.6 2.481	-0.2 00.0	100.0	100.0	29.3	93.2 GR	2.680	100.0	100.0	0.6 2.975	1.16	0.96	8
1363.8 111	10.5	7.5 35.1 2.487	-0.2 00.0	74.5	82.2	27.6	88.5 SD	2.680	82.2	74.5	1.4 2.976	1.16	0.96	8
1364.0 105	11.0	8.5 32.8 2.489	-0.2 00.0	71.4	72.9	26.2	83.0 SD	2.680	72.9	71.4	2.6 2.960	1.16	0.96	8
1364.1 101	12.3	10.2 32.1 2.510	-0.2 00.0	67.3	65.8	25.2	81.6 GR	2.680	67.3	67.3	2.9 2.969	1.16	0.96	8
1364.3 95	13.4	10.4 32.0 2.550	-0.2 00.0	62.8	60.9	23.3	75.6 GR	2.680	62.8	62.8	4.5 2.997	1.16	0.96	8
1364.4 92	13.3	12.6 31.2 2.591	-0.2 00.0	65.5	57.8	23.9	72.6 GR	2.680	65.5	65.5	4.1 3.022	1.16	0.96	
1364.6 93	13.4	15.4 31.6 2.581	-0.2 00.0	64.5	51.8	22.4	73.5 GR	2.680	64.5	64.5	4.3 3.017	1.16	0.96	
1364.7 97	13.1	9.0 30.5 2.553	-0.2 00.0	65.1	68.2	23.5	77.3 GR	2.680	68.2	65.1	3.6 2.988	1.16	0.96	
1364.9 99	12.7	11.8 32.3 2.523	-0.2 00.0	65.6	59.7	24.0	79.3 GR	2.680	65.6	65.6	3.5 2.980	1.16	0.96	8
1365.0 102	12.9	11.5 33.4 2.514	-0.2 00.0	64.7	59.5	23.7	77.8 MN	2.680	64.7	64.7	3.9 2.982	1.16	0.96	8
1365.2 104	13.2	11.4 32.8 2.503	-0.2 00.0	63.5	58.6	23.7	76.0 MN	2.680	63.5	63.5	4.3 2.970	1.16	0.96	8
1365.4 99	12.5	9.7 32.3 2.525	-0.2 00.0	65.2	63.4	22.7	76.0 MN	2.680	65.2	65.2	4.3 2.982	1.16	0.96	8
1365.5 101	10.7	11.4 32.6 2.548	-0.2 00.0	71.8	62.6	24.3	81.8 GR	2.680	71.8	71.8	2.9 3.001	1.16	0.96	8
1365.7 100	10.0	12.6 35.4 2.544	-0.2 00.0	74.2	59.0	25.5	81.0 GR	2.680	74.2	74.2	3.1 3.017	1.16	0.96	8
1365.8 114	9.2	7.2 35.3 2.519	-0.2 00.0	100.0	100.0	27.8	94.4 GR	2.680	100.0	100.0	0.5 2.999	1.16	0.96	8
1366.0 118	8.3	4.2 35.1 2.507	-0.2 00.0			28.6	98.1 SD	2.680	100.0	100.0	00.0 2.989	1.16	0.96 1	•
1366.1 121	8.4	8.6 34.8 2.504	-0.2 00.0			28.3	96.0 SD	2.680	100.0	100.0	00.0 2.985	1.16	0.96 1	•
1366.3 121	8.5	8.3 36.6 2.508	-0.2 00.0			28.2	96.5 SD	2.680	100.0	100.0	00.0 3.000	1.16	0.96 1	

DEPTH M GR	RT	RXO PHIN RHOB	DD SPI	swu sxou	PHIS	VCL FVCL	RHOMAU	sxo	sw	PHIE RHOMA	POR-M	HC-M	FLAGS
1366.4 117	8.3	7.5 37.2 2.511	-0.2 00.0		28.3	97.3 GR	2.680 1	100.0	100.0	00.0 3.005	1.16	0.96 1	
1366.6 119	8.2	7.7 38.0 2.511	-0.2 00.0		28.5	98.6 SD	2.680 1	100.0	100.0	00.0 3.009	1.16	0.96 1	
1366.7 117	8.2	7.7 36.4 2.515	-0.2 00.0		27.5	95.5 SD	2.680 1	100.0	100.0	00.0 3.003	1.16	0.96 1	
1366.9 116	8.1	8.0 34.8 2.520	-0.2 00.0		27.2	95.6 SD	2.680 1	100.0	100.0	00.0 2.996	1.16	0.96 1	
1367.0 116	8.2	7.2 33.3 2.537	-0.2 00.0	100.0 100.0	27.4	94.2 SN	2.680 1	100.0	100.0	0.5 2.998	1.16	0.96	8
1367.2 107	8.1	6.8 32.9 2.530	-0.2 00.0	84.5 85.5	27.6	87.7 GR	2.680	85.5	84.5	1.6 2.990	1.16	0.96	8
1367.3 112	8.0	8.5 33.1 2.518	-0.2 00.0	85.9 80.2	27.8	92.1 GR	2.680	85.9	85.9	0.8 2.982	1.16	0.96	8
1367.5 109	8.1	7.6 33.1 2.508	-0.2 00.0	84.8 82.8	27.5	89.7 GR	2.680	84.8	84.8	1.2 2.975	1.16	0.96	8
1367.6 117	8.5	7.2 33.3 2.501	-0.2 00.0	82.5 83.7	26.7	88.5 SD	2.680	83.7	82.5	1.4 2.972	1.16	0.96	8
1367.8 111	9.0	8.0 32.5 2.530	-0.2 00.0	81.0 82.1	25.5	91.1 GR	2.680	82.1	81.0	1.0 2.987	1.16	0.96	8
1367.9 108	9.1	8.3 32.5 2.551	-0.2 00.0	79.7 78.1	24.9	88.0 GR	2.680	79.7	79.7	1.5 3.002	1.16	0.96	8
1368.1 101	8.9	9.6 32.5 2.559	-0.2 00.0	78.8 68.1	25.2	81.9 GR	2.680	78.8	78.8	2.9 3.008	1.16	0.96	8
1368.2 106	8.4	8.4 32.3 2.516	-0.2 00.0	82.2 76.0	25.8	86.0 GR	2.680	82.2	82.2	1.9 2.975	1.16	0.96	8
1368.4 110	7.8	7.5 31.8 2.492	-0.2 00.0	84.9 80.1	26.7	85.7 SD	2.680	84.9	84.9	2.0 2.953	1.16	0.96	8
1368.6 113	7.5	6.6 32.4 2.490	-0.2 00.0	87.2 86.4	27.2	87.4 SD	2.680	87.2	87.2	1.6 2.957	1.16	0.96	8
1368.7 115	7.6	7.4 33.4 2.499	-0.2 00.0	88.0 85.2	27.6	91.5 SD	2.680	88.0	88.0	0.9 2.971	1.16	0.96	8
1368.9 114	7.8	7.3 32.7 2.503	-0.2 00.0	86.7 85.9	27.3	91.6 SD	2.680	86.7	86.7	0.9 2.969	1.16	0.96	8
1369.0 117	7.9	7.4 31.6 2.519	-0.2 00.0	85.7 83.6	27.1	89.6 SN	2.680	85.7	85.7	1.2 2.971	1.16	0.96	8
1369.2 111	7.8	8.5 32.6 2.529	-0.2 00.0	85.9 77.9	25.0	88.9 SD	2.680	85.9	85.9	1.4 2.987	1.16	0.96	8
1369.3 112	6.6	8.9 33.6 2.538		100.0 100.0	27.3	92.5 GR	2.680			0.8 3.001	1.16	0.96	8
1369.5 113	5.8	7.4 35.4 2.517		100.0 100.0	29.1	93.4 GR	2.680 1			0.6 2.998	1.16	0.96	8
1369.6 116	5.5	6.6 34.8 2.474	-0.2 00.0		31.2	96.6 GR	2.680 1			00.0 2.964	1.16	0.96 1	
1369.8 117	5.4	2.1 34.8 2.438		100.0 100.0	32.1	93.9 SD	2.680			0.6 2.939	1.16	0.96	8
1369.9 118	5.7	5.2 35.7 2.431	-0.2 00.0		33.9	98.4 GR	2.680			00.0 2.942	1.16	0.96 1	
1370.1 121	6.4	6.7 38.9 2.414		100.0 100.0	33.7	94.3 SD	2.680			0.5 2.953	1.16	0.96	8
1370.2 119	6.5	6.8 40.5 2.383	-0.2 00.0		34.3	88.4 SD	2.680	94.2	94.2	1.5 2.943	1.16	0.96	8
1370.4 115	6.3	3.3 40.1 2.358	-0.2 00.0	93.8 115.1	34.8	83.5 SD	2.680	98.7	93.8	2.5 2.925	1.16	0.96	8
1370.5 112	6.1	3.0 36.7 2.381	-0.2 00.0	93.6 117.6	32.5	80.2 SD	2.680	98.7	93.6	3.2 2.915	1.16	0.96	8
1370.7 117	6.3	5.2 34.8 2.401	-0.2 00.0	93.9 94.8	32.4	85.1 SD	2.680	94.8	93.9	2.1 2.913	1.16	0.96	8
1370.8 117	6.8	5.6 34.2 2.410	-0.2 00.0	90.5 90.6	31.7	84.7 SD	2.680	90.6	90.5	2.2 2.915	1.16	0.96	8
1371.0 115	6.9	6.3 35.7 2.425	-0.2 00.0	91.1 88.2	31.4	87.5 SD	2.680	91.1	91.1	1.6 2.938	1.16	0.96	8
1371.1 112	6.8	7.3 38.3 2.447		100.0 100.0	31.5	92.6 GR	2.680			0.7 2.970	1.16	0.96	8
1371.3 111	6.6	6.3 37.7 2.445	-0.2 00.0	94.5 92.3	31.5	91.7 GR	2.680	94.5	94.5	0.9 2.965	1.16	0.96	8
1371.4 113	6.4	6.2 35.5 2.452		100.0 100.0	31.3	93.1 GR	2.680			0.7 2.955	1.16	0.96	8
1371.6 114	6.6	5.9 33.7 2.456	-0.2 00.0	93.9 95.0	30.3	91.2 SD	2.680	95.0	93.9	1.0 2.943	1.16	0.96	8
1371.8 114	7.0	6.4 32.5 2.452	-0.2 00.0	90.3 87.9	29.7	87.5 SD	2.680	90.3	90.3	1.6 2.930	1.16	0.96	8
1371.9 111	7.3	6.1 30.8 2.444	-0.2 00.0	90.7 90.3	29.3	81.2 SN	2.650	90.7	90.7	2.9 2.908	0.00	0.00	8

### Complex Lithology Results 24-10-94

### Zone No. 5

### Hydrocarbon Volume Report

FROM	M	1347.978
TO	M	1371.905
INTERVAL	M	23.927
PHIE Cut off		0.050
SW Cut Off		0.500
Vclay Cut Off		0.300
Net Pay	M	5.029
Average PHIE	%	23.081
Average SW	%	17.943
Average Vclay	%	8.814
Integrated PHI	M	1.161
um PHI*(1-SW)	M	0.955

### Hydrocarbon Volume Report

ZONE #	1	2	3	4	5	6	7	8
FROM M	1160.069	1260.043	1296.924	1316.431	1347.978	1371.905	1401.470	1438.504
TO M	1260.043	1296.924	1316.431	1347.978	1371.905	1398.575	1438.504	1627.937
INTERVAL M	99.974	36.881	19.507	31.547	23.927	26.670	37.033	189.433
PHIE Cut off	0.050	0.050	0.050	0.050	0.050	0.050	0.050	0.050
SW Cut Off	0.500	0.500	0.500	0.500	0.500	0.500	0.500	0.500
Vclay Cut Off	0.300	0.300	0.300	0.300	0.300	0.300	0.300	0.300
Net Pay M	0.000	0.000	0.000	27.584	5.029	0.000	0.000	0.000
Average PHIE %	n/a	n/a	n/a	23.808	23.081	n/a	n/a	n/a
Average SW %	n/a	n/a	n/a	16.705	17.943	n/a	n/a	n/a
Average Vclay %	n/a	n/a	n/a	5.293	8.814	n/a	n/a	n/a
Integrated PHI M	n/a	n/a	n/a	6.567	1.161	n/a	n/a	n/a
Sum PHI*(1-SW) M	n/a	n/a	n/a	5.479	0.955	n/a	n/a	n/a