

DEPT. NAT. RES & ENV
PE902189



BEACH PETROLEUM N.L.

(Incorporated in South Australia)

PETROLEUM DIVISION

CALLISTA No. 1

Well Completion Report
Text & Appendices

by B. L. Rayner
Beach Petroleum N.L.
October, 1988

W972. CALLISTA-1.

W.C.R. Vol 1 of 2.
02/188.

NOV 1988

02 NOV 1988

PETROLEUM DIVISION

CALLISTA NO. 1

WELL COMPLETION REPORT

by

B. L. RAYNER

Beach Petroleum N.L.
345 George Street,
SYDNEY NSW 2000

October, 1988.

CONTENTS

SUMMARY	PAGE
1. INTRODUCTION	1
2. WELL HISTORY	
2.1 Location	3
2.2 General Data	3
2.3 Drilling Data	6
2.3.1 Drilling Contractor	6
2.3.2 Drilling Rig	6
2.3.3 Casing and Cementing Details	6
2.3.4 Drilling Fluid	8
2.3.5 Water Supply	8
2.4 Formation Sampling and Testing	8
2.4.1 Cuttings	8
2.4.2 Cores	9
2.4.3 Tests	9
2.5 Logging and Surveys	10
2.5.1 Mud Logging	10
2.5.2 Wireline Logging	10
2.5.3 Deviation Surveys	11
2.5.4 Velocity Survey	11
3. RESULTS OF DRILLING	
3.1 Stratigraphy	12
3.2 Lithological Descriptions	12
3.2.1 Heytesbury Group	12
3.2.2 Nirranda Group	15
3.2.3 Wangerrip Group	15
3.2.4 Sherbrook Group	16
3.2.5 Otway Group	18
3.3 Hydrocarbon Indications	19
3.3.1 Mud Gas Readings	19
3.3.2 Sample Fluorescence	19
4. GEOLOGY	
4.1 Structure	20
4.2 Porosity and Water Saturation	23
4.3 Relevance to Occurrence of Hydrocarbons	24

FIGURES

1. Regional Location Map.
2. Detailed Location Map.
3. Prognosed and Actual Stratigraphy.
4. Stratigraphy of the Otway Basin.
5. Seismic Line MD84-112.
6. Time Structure Map of the Top Waarre Sandstone (Pre-Drill).

APPENDICES

1. Details of Drilling Plant.
2. Summary of Wellsite Operation.
3. Drilling Fluid Recap.
4. Sidewall Core Descriptions.
5. Velocity Survey.
6. Palynology.
7. X-ray Diffraction Analysis
8. Synthetic Seismogram

ENCLOSURES

	<u>Scale</u>
1. Composite Well Log.	1:1000
2. Gearhart Mud Log.	1:500
3. Gearhart Wireline Logs.	
BCS-GR	1:200 & 1:500
DLL-MSFL-GR	1:200 & 1:500
SLD-CNL-GR	1:200 & 1:500

PEP 104 OTWAY BASIN

CALLISTA NO. 1 BEACH PETROLEUM N.L.

Status: P & A, Dry Hole
 Hole Size: 12¼" to 8½" 1800m
 Casing Shoe: 9 5/8" @ 299m
 Plugs: 1690-1640m, 1380-1330m,
 950-900m, 310-355m, surface

Location: Lat. 38°28'0.22"
 Long 142°50'12.64"E
 Seismic: SP100, MD84-112
 Elevation: 77.0m GL 81.9 KB A.S.L.
 Spudded: 27-3-88 Rig Release: 7-4-88
 Rig: GDSA Rig 2

Rock Unit	KB(m)	Thickness
-----------	-------	-----------

Rock Unit	KB(m)	Thickness
-----------	-------	-----------

Heytesbury Gp

Port Campbell	surface	169.1
Gellibrand Marl	174	313
Clifton Fm	487	16

Sherbrook Gp

Paaratte Fm	960	308
Skull Ck Mdst Mbr	1268	101
Nullawarre Gs Mbr	1369	211
Belfast Mdst	1580	28
Flaxmans Fm	1608	63
Waarre Sst	1671	64

Nirranda Gp

Narrawaturk Marl	503	44
Mepunga Fm	547	84

Otway Gp

Eumeralla	1735	+65
-----------	------	-----

Wangerrip Gp

Dilwyn Fm	631	245
Pember Mdst Mbr	876	33
Pebble Point Fm	909	51

<u>Total Depth (Driller)</u>	1800m
------------------------------	-------

<u>Total Depth (Logger)</u>	1800m
-----------------------------	-------

Logs: DLL/MSFL, BCS, SLD/CNS, SWC, Velocity Survey, Mudlog

Tests: Nil

Cores: 23 SWC, nil conventional

Conclusions

Callista No. 1 was a Waarre Sandstone play drilled largely on the strength of the amplitude anomaly observed on the seismic.

No significant hydrocarbons were observed in the well.

The seismic amplitude anomaly coincided with a lithology change at the Belfast Mudstone/Flaxmans Fm. interface and is not representative of gas saturated sands as is seen in PPL 1.

Prepared by: B. L. Rayner

Date: October, 1988

SUMMARY

Callista No.1 was drilled as a wildcat exploration well in PEP 104, Otway Basin, Victoria.

Participants in the well were Beach Petroleum N.L. (Operator), Gas and Fuel Exploration N.L. and Bridge Oil Limited.

Callista No.1, was located approximately 14km northwest of the Port Campbell gasfield.

The Waarre Sandstone, which was the primary target, was predicted to be gas bearing by seismic interpretation.

Drilling commenced on the 27th of March, 1988 and reached a total depth of 1800m (KB) on the 5th of April, 1988.

At total depth the following wireline logs were run: Dual Laterolog/Microspherically Focused Resistivity, Borehole Compensated Sonic, Spectral Lithodensity/Compensated Neutron, Velocity Survey and Sidewall Cores.

No formation tests or conventional coring operations were performed. Significant shows were not observed during drilling and all horizons are interpreted to be water saturated.

The Callista No.1 well was plugged and abandoned as a dry hole, and the rig was released on the 7th of April, 1988.

1. INTRODUCTION

The Callista No. 1 well was a Waarre Sandstone play drilled primarily on the strength of an amplitude anomaly observed on the seismic.

It has been recognised that some Waarre Sandstone gas accumulations in the eastern Otway Basin can be related to a characteristic high amplitude seismic event at the Waarre Sandstone level. It is also apparent that this high amplitude seismic event can extend beyond the structural boundaries of a feature suggesting an element of stratigraphic control to the gas accumulation.

The Callista prospect arose from a detailed seismic modelling and geological study undertaken in nearby PPL-1 and PEP 108 and extended into PEP 104.

The seismic modelling involved evaluation Waarre Sandstone amplitude anomalies on seismic lines, considering the effect of a gas accumulation in the Waarre Sandstone through the seismic velocity inversion method and estimation of Poissons ratio at that level by the SAMPLE method (Seismic Amplitude Measurement for Primary Lithology Estimation) to predict the presence of hydrocarbons.

In PEP 104, the Callista region was one area which showed high prospectivity for gas in the Waarre Sandstone using the above seismic modelling techniques. The proposed location was recognised to be on the flank of a small "Base Upper Cretaceous" faulted culmination but modelling indicated a more extensive gas accumulation.

Geologically, the Waarre Sandstone in the Callista region was known to be highly variable in terms of reservoir quality. Westgate No.1A, 5km east and Rowans No. 1, 4.5km west of the proposed location, both proved to have a relatively thin and poorly developed Waarre Sandstone reservoir section compared to the Port Campbell area. Nullawarre-3, 3.75km to the north, however, displays good SP deflection and presumably a porous and permeable Waarre Sandstone. In all cases the Waarre Sandstone was capped by an effective seal rock, the Belfast Mudstone and underlain by the regional source rock, the Eumeralla Formation.

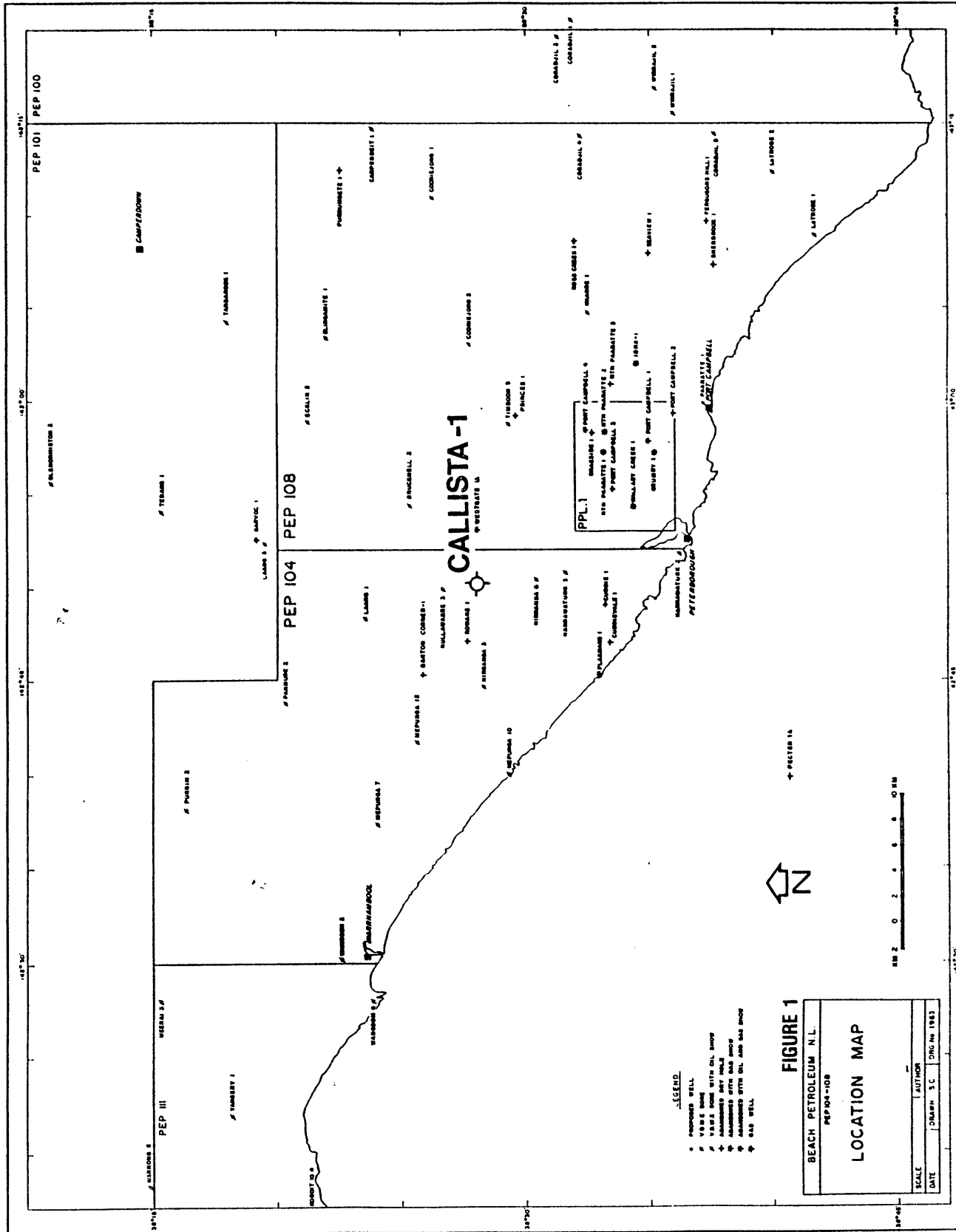
Hence while it was recognised pre-drill that the Waarre Sandstone in the Callista region may not have been as well developed as it is elsewhere, the combination of seal, reservoir and source rocks was recognised to be adequate for a hydrocarbon accumulation.

2. WELL HISTORY2.1 Location (See Figure 1)

Co-ordinates:	Latitude 38° 28' 0.22"S Longitude 142° 50' 12.64"E
Geophysical Control:	Shot Point 100 Seismic Line MD84-112
Real Property Description:	County of Heytesbury Parish of Nullawarre Shire of Warrnambool
Propery Owner:	A.S. Payne Rowans Road, Nullawarre VIC 3268

2.2 General Data (See Figure 2)

Well Name and Number:	Callista No.1
Operator:	Beach Petroleum N.L. Level 7, 345-355 George Street <u>SYDNEY NSW 2000</u>
Participants:	Gas and Fuel Exploration N.L. 151 Flinders Street <u>MELBOURNE VIC 3000</u> Bridge Oil Limited 60 Margaret Street <u>SYDNEY NSW 2000</u>
Elevation:	Ground Level 77.0m ASL Kelly Bushing 81.9m ASL (unless otherwise stated, all depths refer to K.B.)
Total Depth:	Driller 1800m Wireline Logger 1800m



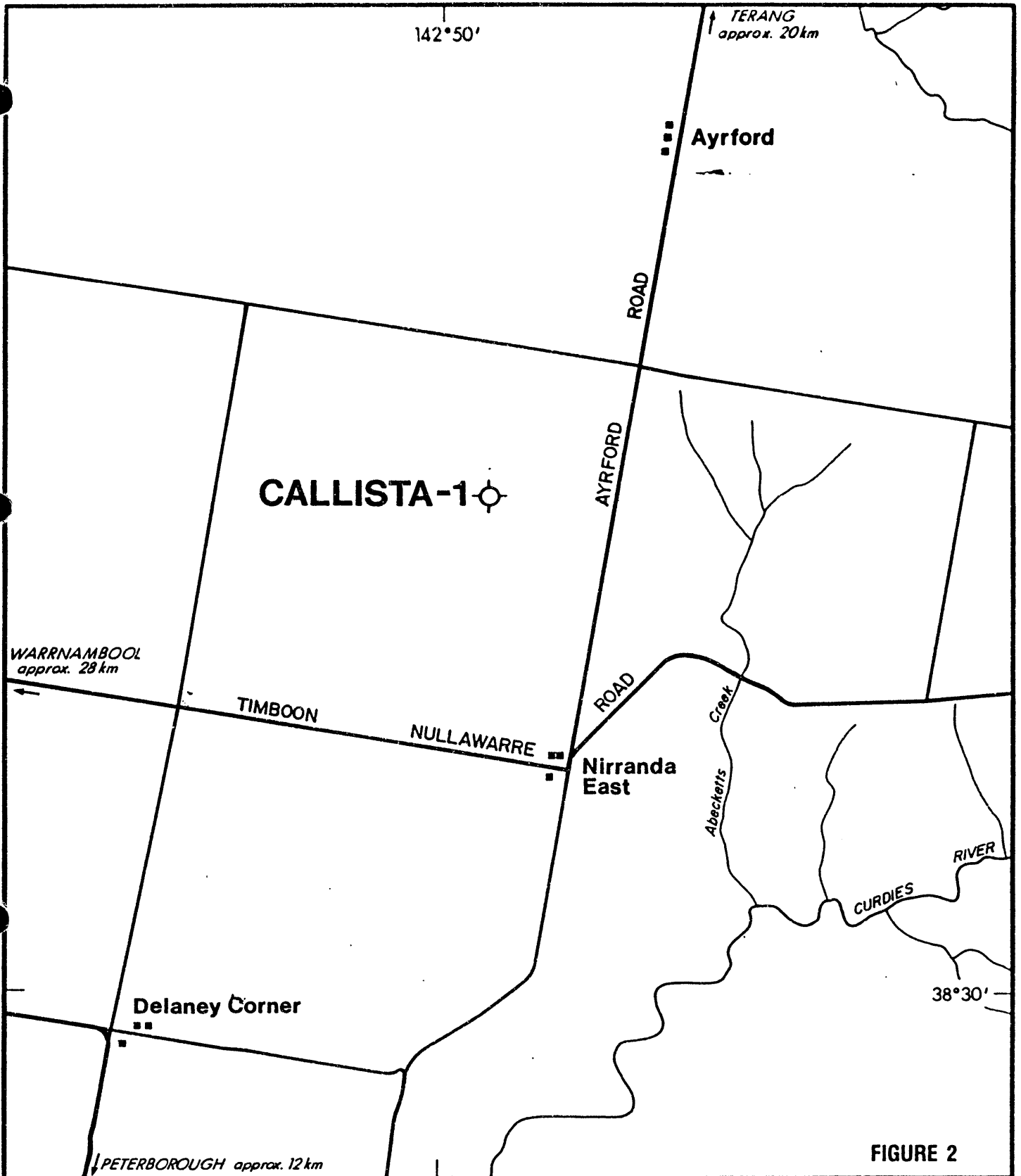
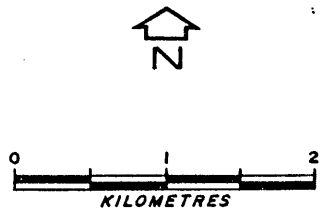


FIGURE 2

Beach Petroleum NL
PEP 104
CALLISTA-1

DETAILED LOCATION MAP



2.2 General Data (cont)

Drilling Commencement: 27th March, 1988 @ 1200 hours
 Total Depth Reached: 5th April, 1988 @ 1300 hours
 Rig Released: 7th April, 1988 @ 1230 hours
 Drilling Time to T.D.: 10 days
 Status: Plugged and abandoned, dry hole.

2.3 Drilling Data (See also Appendices 1 and 2)

2.3.1. Drilling Contractor

Gearhart Drilling Services Australia

2.3.2 Drilling Rig

G.D.S.A. Rig 2

2.3.3 Casing and Cementing Details

A 16" conductor pipe as set at 9.0m prior to rig up.

Surface Casing

Size: 9 5/8"
 Weight and Grade: 40lb/ft BTC 8rd
 Centralisers: 296m, 282m and 273m
 Float Collar: 287m
 Shoe: 299m
 Cement: 195 sacks Class "A" with 2.5% prehydrated gel and 162 sacks Class "A" neat.
 Method: Single plug displacement. (Top plug only).
 Equipment: Halliburton Services

2.3.3 Casing and Cementing Details (cont.)Cement PlugsPlug No.1

Interval: 1690 - 1640m
Cement: 55 sacks Class "A" neat
Method: Balanced
Tested: No

Plug No.2

Interval: 1380 - 1330m
Cement: 55 sacks Class "A" neat
Method: Balanced
Tested: No

Plug No.3

Interval: 950m - 900m
Cement: 61 sacks Classs "A" neat
Method: Balanced
Tested: No

Plug No.4

Interval: 310m - 355m
Cement: 80 sacks Class "A" plus 1% CaCl₂
Method: Balanced
Tested: 10,000lbs weight

Plug No.5

Interval: Surface
Cement: 25 sacks Class "A" neat.

2.3.4 Drilling Fluid

The hole was drilled with a freshwater-bentonite-polymer mud system. Some tight hole was experienced during trips but wireline logging was completed without incident. The Caliper log showed the hole to be very close to gauge. (See Appendix 3 for details).

2.3.5 Water Supply

Drilling water was obtained from a dam close to the wellsite.

2.4 Formation Sampling and Testing

2.4.1 Cuttings

Cuttings samples were collected at 10 metre intervals from the surface to 870m and at 5m intervals from 870m to T.D. Each sample was washed, air dried, divided into five splits, four of which were stored in labelled polythene bags and one which was stored in plastic trays. The sets of washed and dried samples in polythene bags were distributed to the following:

Gas and Fuel Exploration N.L. Bridge Oil Ltd. Victorian Department of Industry, Technology and Resources.

Beach retained one set of washed and dried cuttings in polythene bags and another in plastic trays.

In addition, from surface to T.D., unwashed samples were collected at 10 metre intervals. These samples were stored in labelled cloth bags, air dried and retained by Beach.

2.4.2. Cores

- (i) No conventional coring operations were performed.
- (ii) Twenty-four sidewall cores were attempted, twenty-three were recovered and one misfired. Listed below are the depths and recovery of these sidewall cores. (See Appendix 4 for description)

<u>SWC No.</u>	<u>Depth (m)</u>	<u>Recovery (cm)</u>
1	1794	2.5
2	1792	3.5
3	1788	3.2
4	1737	3.0
5	1734	3.0
6	1731	3.0
7	1722	2.8
8	1719.5	2.5
9	1715	4.0
10	1699.5	2.8
11	1694	3.0
12	1689	3.2
13	1681.5	2.7
14	1678	2.1
15	1674	2.4
16	1665	3.5
17	1616	3.0
18	1605	3.2
19	1583	3.1
20	1370.5	2.3
21	1153	1.8
22	930	3.0
23	misfire	nil
24	903	4.0

2.4.3 Tests

No tests were performed.

2.5 Logging and Surveys (See Enclosure 1)

2.5.1 Mud Logging

A standard skid-mounted Gearhart Geodata Division unit was used to provide penetration rate, continuous mud gas monitoring, intermittent mud and cuttings gas analysis, pump rate and mud volume data. The mudlog is included as Enclosure 2.

2.5.2 Wireline Logging

Wireline logging was performed by Gearhart Pty Ltd using a truck mounted unit. One logging suite was performed at T.D. Details are listed below.

<u>Suite 1</u>	<u>Interval</u>
Dual Laterolog/Microspherically Focused Resistivity Log (DLL/MSFL)	1800-299m (GR to surface)
Borehole Compensated Sonic Log (BCS/GR)	1800-299m
Spectral Lithodensity/ Compensated Neutron Log (SLD/CNL)	1800-1500m 1015-850m

2.5.3 Deviation Surveys

Regular hole deviation surveys were conducted, the results of which are listed below:

<u>Depth (m)</u>	<u>Deviation (°)</u>	<u>Depth (m)</u>	<u>Deviation (°)</u>
58	0.00	734	0.25
130	0.25	933	0.75
197	0.00	989	1.00
252	0.25	1200	0.75
290	0.25	1398	0.75
498	0.25	1615	0.75
526	0.25	1794	1.00

2.5.4 Velocity Survey

A velocity survey was carried out by Velocity Data Pty Ltd, the result of which is included as Appendix 5.

3. RESULTS OF DRILLING

3.1 Stratigraphy

The following stratigraphic intervals have been delineated using clay analysis, palynology, penetration rate, lithology and wire-line log interpretation. (See Figures 3 & 4, Appendices 6 & 7)

<u>Group</u>	<u>Formation</u>	<u>Depth (m)</u>	<u>Thickness (m)</u>
Heytesbury	Port Campbell Limestone	Surface	169.1
	Gellibrand Marl	174	313
	Clifton	487	16
Nirranda	Narrawaturk	503	44
	Mepunga	547	84
Wangerrip	Dilwyn	631	245
	Pember Mudstone Member	876	33
	Pebble Point	909	51
Sherbrook	Paaratte	960	308
	Skull Creek Mudstone Member	1268	101
	Nullawarre Greensand Member	1369	211
	Belfast Mudstone	1580	28
	Flaxmans	1608	63
Otway	Waarre	1671	64
	Eumeralla	1735	+65
	T.D.	1800	

3.2 Lithological Descriptions

3.2.1 Heytesbury Group (Surface to 503)

Port Campbell Limestone Surface to 174m
CALCARENITE, light grey, mottled yellow in part, friable to moderately hard, granular, abundant fossil fragments, trace glauconite, slightly silty in part, poor visual porosity.

Gellibrand Marl 174m to 487m
CALCILUTITE, medium grey, light grey green, medium brown grey, soft to firm, sticky in part, micromicaceous in part, carbonaceous detritus in part, abundant fossil fragment (mainly echinoid spines and bryozoa), with minor CALCARENITE as above.

PROGNOSED

ACTUAL

DEPTHS REFER TO K.B.(81.9m ASL)

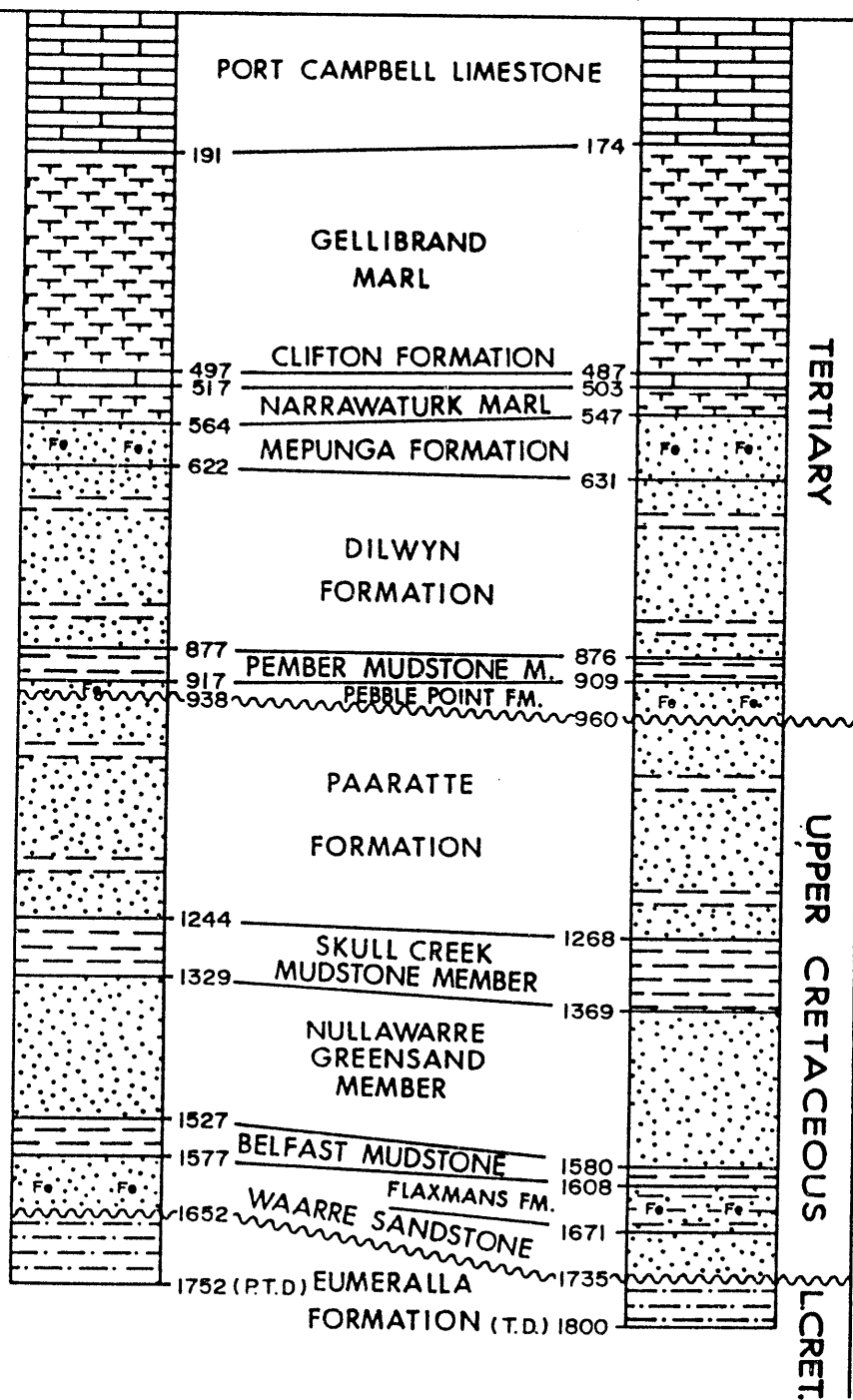


FIGURE 3

Beach Petroleum NL

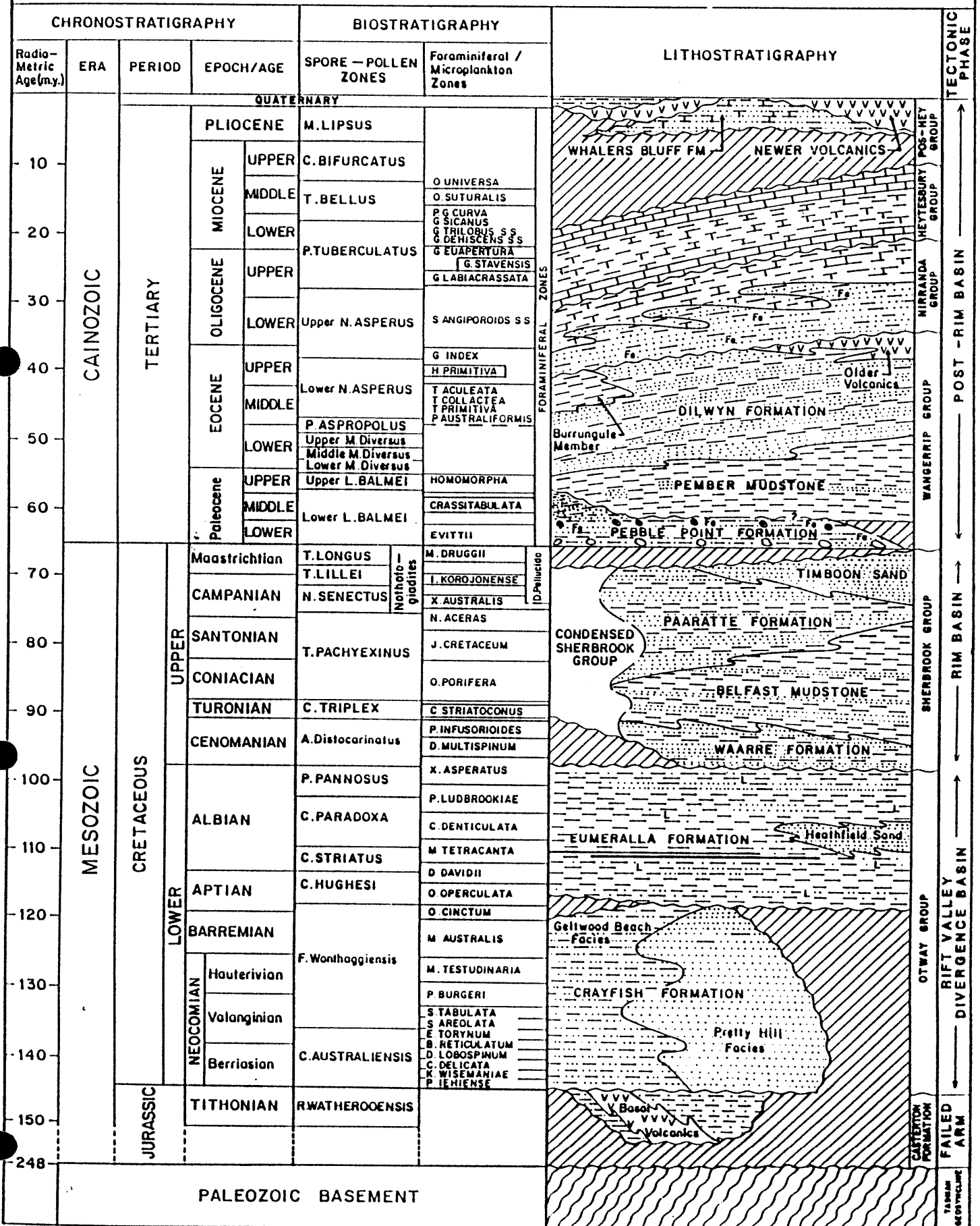
PEP 104

CALLISTA-1

PROGNOSED AND ACTUAL STRATIGRAPHY

STRATIGRAPHIC TABLE

FIGURE 4



Clifton Formation 487m to 503m

CALCARENITE, medium to dark orange brown, light yellow orange in part, friable to hard with iron rich matrix and cement, common fine to very coarse, rounded iron oxide pellets and medium to very coarse iron oxide stained quartz grains, poor to fair visual porosity.

3.2.2 Nirranda Group (503m to 631m)

Narrawaturk Marl 503m to 547m

CALCILUTITE, medium grey green, medium to dark brown grey in part, firm, subfissile, common fossil fragments, common fine, subrounded to rounded quartz grains.

Mepunga Formation 547m to 631m

SANDSTONE, quartzose, very light brown, fine to very coarse, dominantly medium to coarse grained, loose, subangular to rounded, moderately sorted, translucent quartz, trace iron oxide pellets, good visual porosity with minor SILTSTONE, light to dark brown, soft, slightly sticky, slightly calcareous, argillaceous in part, grades to very fine grained SANDSTONE.

3.2.3 Wangerrip Group (631m to 960m)

Dilwyn Formation 631m to 876m

SANDSTONE, quartzose, off white, light to medium grey, loose, medium to very coarse grained, subangular to subrounded, moderate to well sorted quartz, weak siliceous and calcite cement in part, pyritic in part, argillaceous in part, good to fair visual porosity, with minor SILTSTONE, dark brown to black, grey brown in part, firm to hard, subfissile, very carbonaceous, pyritic in part, micromicaceous, arenaceous in part, with minor DOLOMITE and CALCILUTITE.

Pember Mudstone Member 876m to 909m

CLAYSTONE, dark grey brown, dark grey green, soft, firm in part, sticky, very carbonaceous, micromicaceous in part, slightly calcareous, trace to abundant, very fine quartz grains, trace very dark green, fine grained, rounded ? chamositic pellets.

Pebble Point Formation 909m to 960m

SANDSTONE, quartzose, light to medium brown, medium orange brown, friable, medium to coarse grained, subangular to subrounded, poor to moderate sorted, clear, translucent and iron stained quartz, abundant medium to dark brown, very dispersive, silty, iron oxide rich matrix, non calcareous, trace dark brown soft lithics, trace dark green ? chamositic pellets, poor to fair visual porosity. With minor SILTSTONE, dark brown grey, soft, dispersive in part, carbonaceous in part, slightly calcareous, trace pyrite.

3.2.4 Sherbrook Group (960m to 1735m)

Paaratte Formation 960m to 1268m

SANDSTONE, quartzose, off-white, very light grey, loose, friable in part, medium to very coarse, dominantly medium grained with a finer grained component towards the base, subangular to subrounded, moderately sorted quartz, trace siliceous and pyritic cement, common white silty and argillaceous matrix in part, trace carbonaceous detritus, fair to good visual porosity, with minor CLAYSTONE, medium grey, soft, dispersive, trace to occasional carbonaceous detritus, very arenaceous in part, very minor COAL, black, dull, earthy, soft to firm in part, subblocky, and very rare DOLomite, buff, grey, hard, cryptocrystalline.

Skull Creek Mudstone Member 1268m to 1369m

CLAYSTONE, light to medium grey, dark brown grey medium to dark grey at base, very soft, puggy, slightly calcareous, micromicaceous, silty in part, very arenaceous with fine grained quartz, trace to common carbonaceous detritus and lithics, common microfossils. With common SANDSTONE, quartzose, off-white, friable, very fine to coarse, dominantly very fine to fine grained, subangular to subrounded, poor to moderate sorted quartz, siliceous cement, trace pyritic and calcareous cement, white argillaceous matrix in part, trace coally lithics, very poor visual porosity.

Nullawarre Greensand Member 1369m to 1580m

From 1369m to 1383m SANDSTONE, quartzose, medium green, green olive grey, friable, fine to coarse, dominantly medium grained, subangular to subrounded, moderately sorted, clear, light brown, light green quartz, patchy off white, medium green argillaceous and silty matrix, common dark green medium grained rounded ? chamosite pellets, fair to poor visual porosity.

From 1383 to 1580m SANDSTONE, quartzose, light to medium yellow brown, loose to friable, fine to medium grained, dominantly medium grained, subangular to subrounded, moderately sorted iron oxide stained quartz, weak siliceous cement in part, trace brown iron rich, dispersive argillaceous and silty matrix, common brown, medium grained, rounded iron oxide pellets, poor to fair visual porosity, with trace DOLomite, buff, cream, light grey, hard cryptocrystalline, and minor LIMONITIC CLAYSTONE, yellow brown, medium to dark brown, hard to moderately hard, brittle, very arenaceous with fine quartz and iron oxide pellets.

Belfast Mudstone 1580m to 1671m
CLAYSTONE, dark grey, firm, dispersive, micromicaceous,
 very carbonaceous, silty.

Flaxmans Formation 1608m to 1671m
CLAYSTONE, dark green, medium to dark green grey, dark grey
 black in part, soft to firm, dispersive in part, very
 arenaceous in part with abundant iron oxide and ?
 chamositic pellets and medium grained quartz, grades to a
LITHIC SANDSTONE.

Waarre Sandstone 1671m to 1735m
SANDSTONE, quartzose, light to medium grey, light brown,
 off white, very fine to medium grained, dominantly fine
 grained, subangular to subrounded, moderate to well sorted
 quartz, common grey white argillaceous matrix, good calcite
 cement in part, trace to abundant carbonaceous detritus and
 laminae, fair to good visual porosity, with interbedded
SILTSTONE, medium grey, medium grey brown, firm subfissile
 dispersive in part, slightly calcareous, micromicaceous,
 common carbonaceous detritus and laminae, arenaceous in
 part, and minor CLAYSTONE, dark grey, soft, dispersive,
 very carbonaceous, silty and arenaceous.

3.2.5 Otway Group (1735m to 1800m)

Eumeralla Formation 1735m to 1800m
SANDSTONE, lithic, green grey, off white, friable, fine to
 very coarse, dominantly medium grained, subangular,
 moderately sorted, clear and translucent quartz, abundant
 white argillaceous matrix, good calcite cement in part,
 trace pyrite cement in part, abundant dark green, medium
 grained, rounded ? chamositic lithics, common off white
 feldspathic lithics, poor visual porosity, with inter
 bedded SILTSTONE, medium green grey, medium to light grey,
 soft to firm, dispersive, slightly calcareous in part,
 trace to common carbonaceous detritus, very argillaceous
 and minor CLAYSTONE, light grey, very soft, brittle in
 part, dispersive, common silt and very fine quartz.

3.3 Hydrocarbon Indications

3.3.1 Mud Gas Readings

The mud gas detection equipment was operational from surface to total depth.

Levels of gas in the drilling mud from surface to approximately 1000m were below the detection capabilities of the system.

From 1000m to 1550m the background level of gas rose to a steady trace C₁.

From 1550m to 1800m (T.D.) background mud gas readings were relatively stable at 2 units C₁, 0.25 units C₂ and trace C₃.

The increase in mud gas over the basal portion of the hole probably relates to increased concentration and maturity of organics in the sediments drilled. Minor fluctuations of the total gas readings corresponds to the rate of penetration.

No significant anomalous mud gas readings were observed.

3.3.2 Sample Fluorescence

Cuttings samples were routinely inspected for oil fluorescence at 10 metre intervals from surface to 870m and at 5 metre intervals from 870m to 1800m (T.D.). All sidewall cores were also examined for oil fluorescence.

No oil fluorescence was observed in any of the cuttings or sidewall cores.

4. GEOLOGY

4.1 Structure

The Callista prospect was interpreted to be one of a series of Waarre Sandstone seismic amplitude anomalies observed within PEP 104 and PPL 1. Gas saturation was predicted by the seismic inversion method and the SAMPLE technique (Seismic Amplitude Measurement for Primary Lithology Estimation).

The Callista No. 1 well was located on the flank of a small "Base Upper Cretaceous" culmination in the Rowans Platform area (Figures 5 & 6.). As the seismic amplitude anomaly, originally interpreted to be at the Waarre Sandstone level, extends beyond structural closure it was thought to represent stratigraphic control to the gas accumulation. The well was optimally located with respect to the seismic anomaly rather than structural considerations.

The drill results show that the Waarre Sandstone is deeper in both time and depth than originally interpreted and is water saturated. The high amplitude event coincides with the interface between the Belfast Mudstone and the Flaxmans Formation and is a lithology effect rather than gas saturation related.

The obvious differences between the control point for the amplitude anomaly study (North Paaratte No. 1) and the Callista No. 1 well is the significantly greater thickness of the Flaxmans Formation and the poorer reservoir quality of the Waarre Sandstone in the subject exploration well.

Despite the disappointing results from the Callista No. 1 well, other amplitude anomalies in PEP 104 remain valid exploration targets in areas where the basal Upper Cretaceous lithologies are more similar to that of the successful North Paaratte No. 1 well.

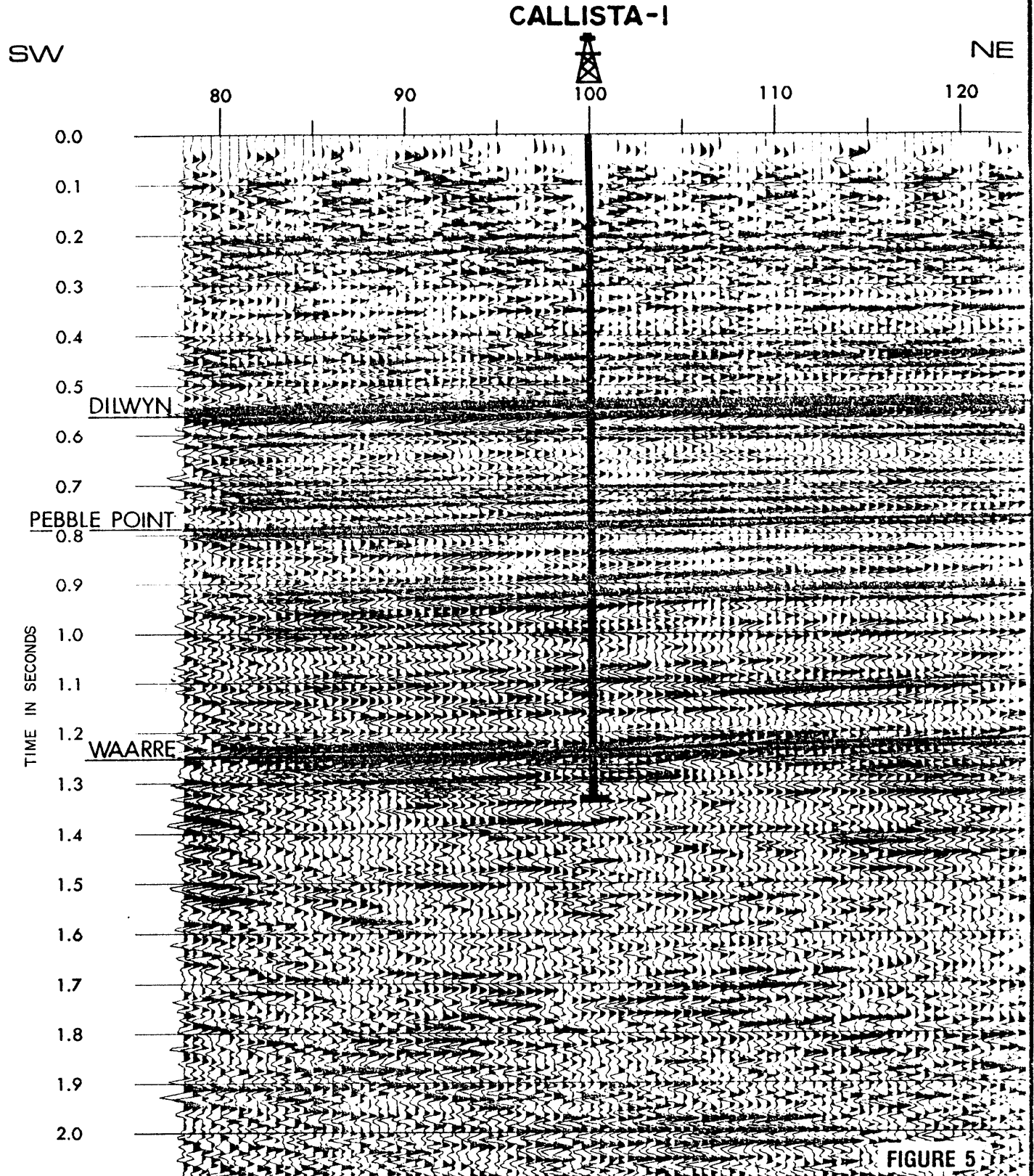


FIGURE 5

Beach Petroleum NL
 PEP 104
CALLISTA-1
 SEISMIC LINE MD-112
 Migrated Stack
 (Pre-Drill Interpretation)

AUTHOR : B. RAYNER DATE : OCTOBER 1988 DRAWN : LG

4.2 Porosity and Water Saturation

Wireline log evaluation was facilitated by a Gearhart Well Evaluation Log.

No conventional cores were cut and no formation waters were recovered. All porosity and salinity values are therefore log derived.

No significant anomalous zones are inferred from the analysis of the ditch cuttings, the mud or the electric logs and all horizons appear to be water wet.

The Dilwyn Formation consists of a sequence of relatively clean, quartzose sandstones with interbedded claystones. The log derived porosity of these sandstones is in excess of 27%.

Within the Pebble Point Formation the better porosity is developed in the middle 15 metres of this interval. The top and base of the Pebble Point Formation are very argillaceous. The better porosity is of the 23-28% order with a V_{clay} of 0.25.

The Paaratte Formation sands are reasonably well developed with an average porosity of 26% and a V_{clay} of 0.15.

The Nullawarre Greensand Member was observed in the cuttings and sidewall cores to contain a dispersive silty to argillaceous matrix. This is not reflected in the wireline log response and the log estimates of less than 0.1 V_{clay} and an average of 25% porosity may be too optimistic.

The Waarre Sandstone contained a sequence of relatively argillaceous sandstones with interbedded claystones and siltstones. In the better sandstones, V_{clay} was between 0.1 and 0.4 and effective porosity between 10% and 22%. The best reservoir sandstone was observed at the top of the sequence.

4.3 Relevance to Occurrence of Hydrocarbons

Callista No. 1 was the first well to be drilled in the Otway Basin on the strength of direct hydrocarbon indications from the seismic.

The technique used was based on the nearby North Paaratte No. 1 well which discovered a thick, gas saturated Waarre Sandstone and shows a coincident seismic amplitude anomaly.

As the Callista feature was seen to have a very similar Waarre Sandstone seismic character to that of North Paaratte No. 1, it too was presumed to be gas filled.

Post-drill results show that the amplitude anomaly in the Callista No. 1 well is coincident with the Belfast Mudstone/Flaxmans Formation interface. In addition the Flaxmans Formation is relatively well developed and has obscured to a certain extent the seismic response of the poorly developed, underlying Waarre Sandstone. This is not the case in the North Paaratte field where the Flaxmans Formation is thin and has a relatively weak seismic response.

The problem with the Callista prognosis therefore lay in applying the North Paaratte No. 1 case as an analogy to an area with slightly different basal Upper Cretaceous lithologies.

Unless lithology and gas effects can be separated from the seismic response in PEP 104, then this exploration tool is only applicable to areas geologically similar to the North Paaratte No. 1 control point, i.e. thin/absent Flaxmans Formation together with a thick, well developed Waarre Sandstone.

The absence of hydrocarbons shows that no stratigraphic trapping of hydrocarbons has occurred at this feature and suggests that the well was either drilled too far down the flank of the structural feature to be within closure or that the fault closure was not an effective seal to migrating hydrocarbons.

APPENDIX 1

Details of Drilling Plant

RIG #2

SUPERIOR MODEL 700E SCR
CAPACITY 11,000FT, 3,350M NOMINAL

DRAWWORKS

ONE SUPERIOR MODEL 700E SCR ELECTRIC DRIVEN DRAWWORKS COMPLETE WITH AUXILIARY BRAKE AND SANDREEL. MAXIMUM INPUT H.P. 1000. DRIVEN BY EMD MOTOR.

ONE FOSTER MODEL 37 MAKE-UP SPINNING CATHEAD. MOUNTED ON DRILLERS SIDE.

ONE FOSTER MODEL 24 BREAK-OUT CATHEAD. MOUNTED OFF DRILLERS SIDE.

TRANSMISSION - 2 SPEED TRANSMISSION WITH HIGH CHAIN 1 1/4" TRIPLE 26T TO 24T. TWIN DISC PO218 AIR CLUTCH. LOW CHAIN 1 1/4" TRIPLE 20T TO 39T TWIN DISC PO218 AIR CLUTCH.

ENGINES

FOUR CATERPILLAR MODEL 3412 PCTA DIESEL ENGINES.

MAST

FLOOR MOUNTED CANTILEVER MAST DRECO - MODEL NO: M12713-510 DESIGNED IN ACCORDANCE WITH A.P.I. SPECIFICATION 4E 'DRILLING AND WELL SERVICING STRUCTURES'.

CLEAR WORKING HEIGHT - 127'

BASE WIDTH - 13' 6"

HOOK LOAD

GROSS NOMINAL CAPACITY - 510,000 LBS

HOOK LOAD CAPACITY WITH:

10 LINES STRUNG 410,000 LBS

8 LINES STRUNG 365,000 LBS

6 LINES STRUNG 340,000 LBS

4 LINES STRUNG 306,000 LBS

MAXIMUM WIND LOAD 100 MPH - NO SETBACK

MAXIMUM WIND LOAD 84 MPH - RATED SETBACK

ADJUSTABLE RACKING BOARD WITH CAPACITY FOR 108 STANDS OF 4 1/2" DRILL PIPE, 10 STANDS OF 6 1/2" DRILL COLLARS, 3 STANDS OF 8" DRILL COLLARS DESIGNED TO WITHSTAND AN A.P.I. WINDLOAD OF 84 MPH WITH PIPE RACKED.

CROWN BLOCK

215 TON WITH FIVE 36" SHEAVES, AND ONE 36" FASTLINE SHEAVE GROOVED 1 1/8".

SUBSTRUCTURE

ONE PIECE SUBSTRUCTURE. 14' H X 13' 6" W X 50' L W/ 12' BOP CLEARANCE.
SET-BACK - 200,000 LBS - CASING = 210,000 LBS.

RIG LIGHTING

EXPLOSION PROOF FLUORESCENT.

TRAVELLING BLOCK

ONE 667 CROSBY MCKISSICK 250 TONE COMBINATION BLOCK HOOK WEB WILSON
250 TON HYDRA - HOOK UNIT 5 - 36" SHEAVES.

KELLY DRIVE

ONE 20 HDP VARCO KELLY DRIVE BUSHING.

KELLY

ONE SQUARE KELLY DRIVE 4 1/4" X 40' COMPLETE WITH SCABBARD.

SWIVEL

ONE OILWELL PC-300 TON SWIVEL.

ROTARY TABLE

ONE OILWELL A 20 1/2" ROTARY TABLE TORQUE TUBE DRIVEN FROM
DRAWWORKS.

AIR COMPRESSORS & RECEIVERS

TWO LEROI DRESSER MODEL 660A AIR COMPRESSOR PACKAGES C/W 10 H.P.
MOTORS RATED AT 600 VOLT 60 HZ 3 PHASE. RECEIVERS EACH 120 GALLON
CAPACITY AND FITTED WITH RELIEF VALVES.

INSTRUMENTATION

ONE (1) 6 PEN DRILL SENTRY RECORDER TO RECORD:
WEIGHT (D) 1-MARTIN DECKER SEALTITE
1-CAMERON DEADLINE TYPE
PENETRATION (FEET)
PUMP PRESSURE (0 - 6000 P.S.I.)
ELECTRIC ROTARY TORQUE
ROTARY SPEED (R.P.M.)
PUMP S.P.M. (WITH SELECTOR SWITCH)

INSTRUMENTATION

(Cont)

ONE (1) DRILLERS CONSOLE INCLUDING THE FOLLOWING EQUIPMENT:

MARTIN DECKER WEIGHT INDICATOR TYPE 'D' ELECTRIC ROTARY TORQUE GAUGE.

PIT SCAN.

S.P.M. GAUGE (2 PER CONSOLE).

ROTARY R.P.M. GAUGE.

ONE SET OF 'DOUBLE SHOT'

DEVIATION INSTRUMENT 'TOTCO'.

ONE SET OF MUD TESTING LABORATORY STANDARD KIT (BAROID).

DRILLING LINE

5000' OF 1 1/8" - TIGER BRAND.

MUD PUMPS

TWO GARDNER DENVER MUD PUMPS MODEL NO: PZHVE 750 EACH DRIVEN BY 800 HP EMD MOTOR.

GENERATOR

FOUR BROWN BOVERI 600 VOLT 3 PHASE 60 HZ AC GENERATORS. POWERED BY FOUR CAT 3412 PCTA DIESEL ENGINES.

B.O.P'S AND ACCUMULATOR

ONE HYDRIL 13 5/8" X 3000 P.S.I. SPHERICAL ANNULAR B.O.P., STUDDED TOP AND FLANGED BOTTOM. HEIGHT 14"

ONE HYDRIL 13 5/8" X 5000 P.S.I. FLANGED DOUBLE GATE B.O.P.

ONE GALAXIE 13 5/8" X 5000 P.S.I. 3000 DOUBLE STUDDED ADAPTOR FLANGES COMPLETE WITH STUDS AND NUTS.

ONE CUP TESTER. GRAY C/W TEST CUPS FOR 9-5/8" AND 13-3/8"

ONE WAGNER MODEL 130 - 160 3 BND 160 GALLON ACCUMULATOR CONSISTING OF:

SIXTEEN 11 GALLON BLADDER TYPE BOTTLES.

ONE 20 H.P. ELECTRIC DRIVEN TRIPLEX PUMP 600 VOLT 60 HZ 3 PHASE MOTOR AND CONTROLS.

ONE WAGNER MODEL A - 60 AUXILIARY AIR PUMP 4.5 GALS/MINUTE.

ONE WAGNER MODEL UM2SCB5S MOUNTED HYDRAULIC CONTROL PANEL WITH FIVE (5) 1" STAINLESS STEEL FITTED SELECTOR VALVES AND TWO (2) STRIPPING CONTROLS AND PRESSURE REDUCING VALVES. THREE (3) 4" HYDRAULIC READOUT GAUGES:

- ONE FOR ANNULAR PRESSURE
- ONE FOR ACCUMULATOR PRESSURE
- ONE FOR MANIFOLD PRESSURE

ONE WAGNER MODEL GMSB - 5A 5 STATION REMOTE DRILLERS CONTROL WITH THREE PRESSURE READBACK GAUGES, INCREASE AND DECREASE CONTROL FOR ANNULAR PRESSURE.

SPOOLS

ONE SET FLANGED ADAPTOR SPOOLS TO MATE 13 5/8" LOT X 5000 P.S.I. A.P.I.
B.O.P. FLANGE TO FOLLOWING WELLHEAD FLANGES:

12" X 900 SERIES, HEIGHT 14"

10" X 900 SERIES " "

8" X 900 SERIES " "

B.O.P. SPACER. FLANGE 12" 3000 R57 STUDDED X 6" 3000 R45 FLANGE, HEIGHT 16"

B.O.P. SPACER SPOOL (DRILLING SPOOL) 12" 5000 X 12" 5000 BX160, HEIGHT 14"

KELLY COCKS

ONE GRIFFITH LOWER KELLY COCK 6 1/2" O.D. WITH 4 1/2" X H CONNECTIONS.
ONE GRIFFITH UPPER KELLY COCK 7 3/4" WITH 6 5/8" A.P.I. CONNECTIONS.

DRILL PIPE

SAFETY VALVE

ONE GRIFFITH 6 1/2" INSIDE BLOWOUT PREVENTORS (4 1/2" X H)
ONE GRIFFITH 6 1/2" STABBING VALVE (4 1/2" X H)

CHOKE MANIFOLD

ONE MCEVOY CHOKE AND KILL MANIFOLD 3" - 5000 P.S.I.

MUD SYSTEM

ONE PILL TANK CAPACITY 25 BBLs.
TWO MIX TANKS CAPACITY 108 BBLs. (EACH)
ONE RESERVE TANK CAPACITY 120 BBLs.
ONE DESILT TANK CAPACITY 120 BBLs.
ONE DESAND TANK CAPACITY 120 BBLs.
ONE SHAKER TANK CAPACITY 130 BBLs.
ONE SAND TRAP CAPACITY 15 BBLs.

FUEL TANKS

ONE 140 BBLs.
ONE 6000 GALS - 30,000 LITRES.

WATER TANKS

ONE 400 BBLs

MIXING PUMPS

FIVE MISSION MAGNUM 5" X 6" X 14" CENTRIFUGAL PUMPS COMPLETE WITH 50 H.P. 600
VOLT HZ 3 PH EXPLOSION PROOF ELECTRIC MOTORS.

TRIP TANK PUMP

ONE MISSION MAGNUM 2" X 3" CENTRIFUGAL PUMP COMPLETE WITH 20 H.P. 600 VOLT 60 HZ 3 PH EXPLOSION PROOF MOTORS.

WATER TRANSFER PUMPS

THREE MISSION MAGNUM 2" X 3" CENTRIFUGAL PUMPS C/W 20 H.P. 600 VOLT 60 HZ 3 PH EXPLOSION PROOF MOTORS.

MUD AGITATORS

SIX GEOLOGRAPH/PIONEER 40 TD - 15" 'PITBULL' MUD AGITATORS WITH 15 H.P. 600 VOLT 60 HZ 3 PH ELECTRIC MOTORS.

SHALE SHAKER

ONE BRANDT - DUAL TANDEM SHALE SHAKER.

DESANDER

ONE PIONEER T8-6 'SANDMASTER' DESANDER.

DESILTER

ONE PIONEER T12-4 'SILTMASER' DESILTER.

DRILL PIPE

10000 FT OF 4 1/2" GRADE 'E' 16.60 LBS/FT HARD BANDED DRILL PIPE 326 JOINTS.

DRILL COLLARS

1 - 6 1/2" OD DRILL COLLAR (SHORT) 15'
27 - 6 1/2" OD DRILL COLLARS.
3 ACTUAL 8" OD DRILL COLLARS.
9 ACTUAL JOINTS OF 4 1/2" HEVI-WATE DRILL PIPE.

TWO (2) BIT SUBS - 6-5/8" REG DBL BOX
TWO (2) BIT SUBS - 4-1/2" REG X 4-1/2" XH DBL BOX
ONE (1) XO SUB - 7-5/8" REG X 6-5/8" REG DBL BOX
ONE (1) XO SUB - 4-1/2" XH BOX X 4-1/2" IF PIN
ONE (1) XO SUB - 4-1/2" REG X 4-1/2" XH DBL PIN
TWO (2) XO SUB - 6-5/8" REG PIN X 4-1/2" XH BOX
ONE (1) JUNK SUB - 6-5/8" REG PIN X 6-5/8" REG BOX
ONE (1) JUNK SUB - 4-1/2" REG BOX X 4-1/2" REG PIN
ONE (1) JUNK SUB - 4-1/2" REG BOX X 4-1/2" XH BOX
TWO (2) KELLY SAVER SUB S/W RUBBER 4-1/2" XH PXB
TWO (2) CIRCULAR SUBS - 4-1/2" XH X 1502 HAMMR UNION
TWO (2) 12-1/4" EZI CHANGE S/STAB 6-5/8 REG PXB
TWO (2) 8-1/2" INTEGRAL BLADE STABILIZERS 4-1/2" XH PXB

ELEVATORS

ONE (1) 4-1/2" BJ 250 TON 18 DEGREE TAPER D/P ELEVATORS
ONE (1) 2-7/8" IUS 100 TON TUBING ELEVATORS
ONE (1) 2-7/8" EUI 100 TON TUBING ELEVATORS
ONE (1) 13-3/8" BAASH ROSS 150 TON S/DOOR ELEVATORS
ONE (1) 13-3/8" S/JOINT P.U. ELEVATORS
ONE (1) 9-5/8" WEBB WILSON 150 TON S/DOOR ELEVATORS
ONE (1) 9-5/8" S/JOINT P.U. ELEVATORS
ONE (1) 7" BJ 200 TON S/DOOR ELEVATORS
ONE (1) 7" S/JOINT P.U. ELEVATORS
ALL P.U. ELEVATORS C/W SLINGS & SWIVEL

ONE (1) 8" WEBB WILSON 150 TON S/DOOR ELEVATORS D/C
ONE (1) 5-3/4" WEBB WILSON 150 TON S/DOOR ELEVATORS D/C
ABOVE C/W LIFT NUBBING AND BAILS

ROTARY SLIPS D/P TUBING

TWO (2) 4-1/2" VARCO SDML D/P SLIPS
ONE (1) 3-1/2" VARCO SDML TUBING SLIPS
TWO (2) 8" - 6-1/2" DCS-R DRILL COLLAR SLLIPS

ROTARY TONGS

ONE (1) BJ TYPE 'B' C/W LATCH & LUG JAWS 13-3/8" - 3-1/2"

CASING SLIPS

THREE (3) 13-3/8" - 9-5/8" - 7" VARCO CSML CASING SLIPS

BIT BREAKERS

FOUR (4) 17-1/2" - 12-1/4" - 8-1/2" - 6"

FISHING TOOLS

ONE (1) 8-1/8" BOWEN SERIES 150 F.S. O/SHOT
ONE (1) 10-5/8" BOWEN SERIES 150 F.S. O/SHOT
C/W GRAPPLES & PACKOFFS TO FISH CONTRACTORS DOWN HOLE EQUIPMENT.
ONE (1) 8 O.D. FISHING MAGNET 4-1/2" REG PIN
ONE (1) REVERSE CIRC JUNK BASKET 4-1/2" XH BOX
ONE (1) JUNK BASKET MILL TYPE C/W MILL SHOE 4-1/2" REG PIN
ONE (1) JARS 6-1/2" O.D. GRIFFITHS FISHING 4-1/2" XH PXB
ONE (1) JAR ACCELERATOR GRIFFITHS FISHING 6-1/2" O.D. 4-1/2" XH PXB
ONE (1) BUMPER SUB 6-1/2" O.D. FISHING 4-1/2" XH PXB
ONE (1) 12" JUNK MILL - 6-5/8" REG PIN
ONE (1) 8" JUNK MILL 4-1/2" REG PIN

ROTARY REAMERS

ONE (1) 6-1/2" O.D. DRILCO N.B. ROLLER REAMER C/W TYPE K CUTTERS 8-1/2" HOLE

PUP JOINTS

THREE (3) 5' - 10; - 15; 4-1/2" O.D. GRADE 'G' PUP JOINTS

AUGER

ONE (1) 27-1/2" AUGER 4-1/2" XH BOX

RATHOLE DIGGER

ONE (1) FABRICATED ROTARY TABLE CHAIN DRIVEN

POWER TONG

ONE (1) FARR 13-5/8" - 5-1/2" HYDRAULIC POWER TONS
C/W HYD. POWER PACK & HOSES & TORQUE GUAGE ASSY

APPENDIX 2

Summary of Wellsite Operations

SUMMARY OF DRILLING OPERATIONS

The Callista No. 1 drill site was prepared by Mr. R. Andrew of Timboon.

Prior to the rig arriving a 16" conductor pipe had been installed to 9.0m.

The G.D.S.A. Rig 2 was rigged up and Callista No. 1 was spudded at 1200 HRS, 27th March, 1988.

A 12½" hole was drilled to 302m where the 9 5/8" casing was set.

The B.O.P.'s were installed and all functions tested to 1500 p.s.i.

Drilling resumed with 8½" hole to 308m at which point a leak-off test established a formation integrity of 14.2 ppg.

The 8½" hole was continued to total depth with bit changes at 1001m and 1655m.

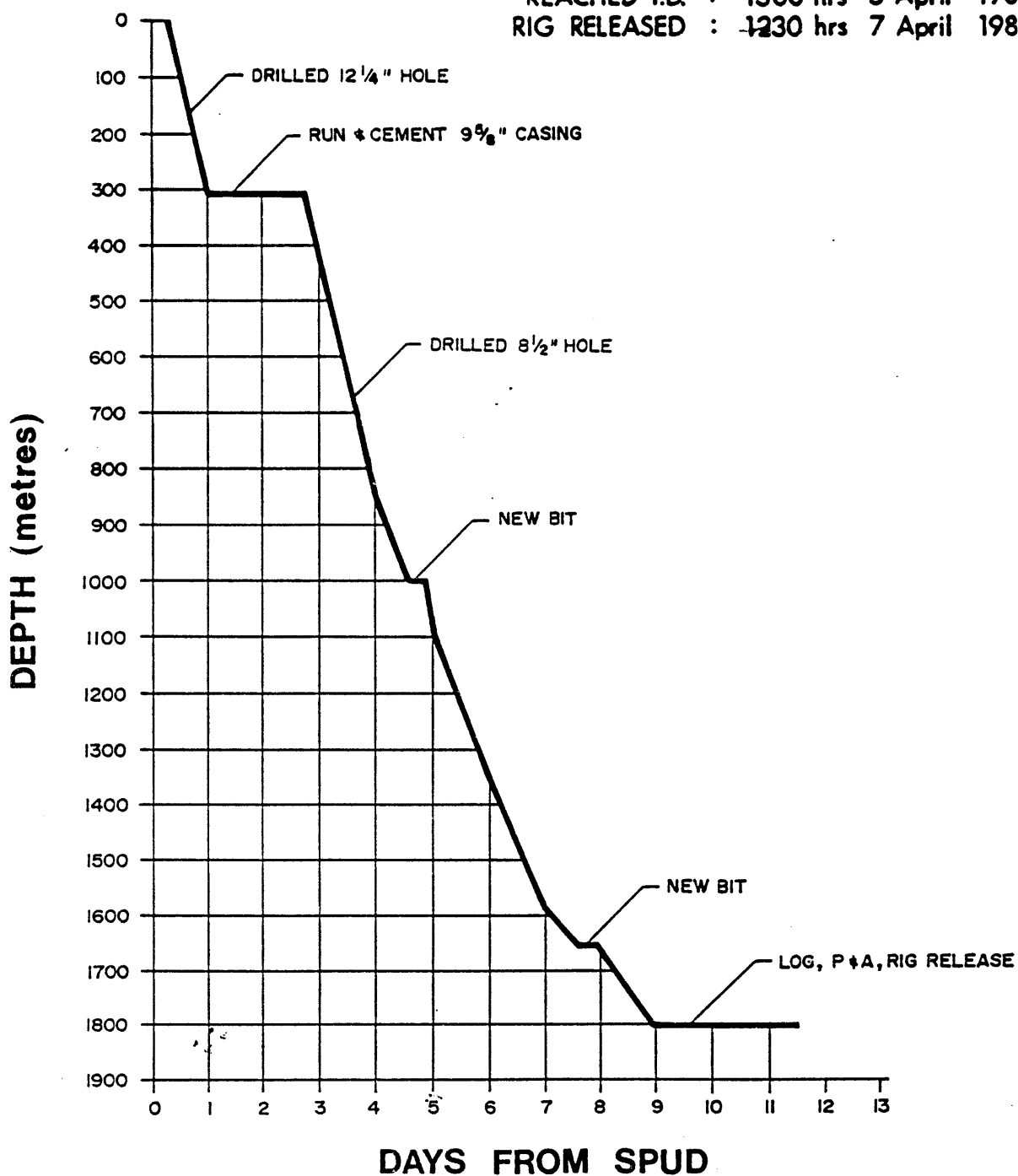
Total depth of 1800m was reached at 1300 HRS, 5th April, 1988.

Gearhart Australia then ran the following log; DLL/MSFL/GR, BCS/GR, SLD/CNS/GR, CIS and SWC.

Cement plugs were then set over the interval 1690-1640m, 1380-1330m, 950-900m, 310-255m and at the surface.

The rig was released out 1230 HRS, 7th April, 1988.

SPUD : 1200 hrs 27 March 1988
REACHED T.D. : 1300 hrs 5 April 1988
RIG RELEASED : 1230 hrs 7 April 1988



Beach Petroleum NL
PEL 28
CALLISTA -1
TIME VS DEPTH

APPENDIX 3

Drilling Fluid Recap



WELL SUMMARY

OPERATOR: BEACH PETROLEUM N.L.

WELLSITE REP: V. SANTOSTEFANO

CONTRACTOR: GEARHART DRILLING

CONTRACTOR REP: G. NICOT

RIG: #2

WELL: CALLISTA #1

TOTAL DRILLING DAYS: 10

SPUD DATE: 27.3.88

TOTAL DAYS ON WELL: 11

TOTAL DEPTH DATE: 5.4.88

DRILLING FLUID BY INTERVAL:

MUD COST BY INTERVAL:

SPUD MUD..... 0..to..302 METRES\$.1334.44.....

..... 302..to..1800 METRES\$.7328.60.....

.....to.....

.....to.....

TOTAL MUD COST:

.....\$.8663.04.....

DRESSER MAGCOBAR ENGINEERS:

M. OLEJNICZAK.

WELL SUMMARY

INTRODUCTION

WELL SUMMARY

INTRODUCTION

Callista #1 had a very similar prognosed lithology to the Iona #1 well which had been drilled immediately before it. As the use of a Frestwater-Bentonite-Polymer mud in conjunction with low hydraulics had resulted in a very good guage hole, at the expense of some tight hole problems, it was planned to follow the same procedure on Callista #1.

With a deeper T.D. of 1750 metres expected, the total mud cost was anticipated at being in the \$9,000 to \$11,000 range.

WELL SUMMARY

BEACH PETROLEUM N.L.

- CALLISTA #1

FORMATION TOPS

PORT CAMPBELL LST	SURFACE
GELLIBRAND MARL	177 METRES
CLIFTON FORMATION	486 METRES
NARRAWATURK FORMATION	502 METRES
MEPUNGA FORMATION	546 METRES
DILWYN FORMATION	630 METRES
PEMBER MUDSTONE	863 METRES
PEBBLE POINT FORMATION	909 METRES
PARAATE FORMATION	960 METRES
SKULL CREEK MUDSTONE	1268 METRES
NULLAWARRE GREENSAND	1369 METRES
BELFAST MUDSTONE	1580 METRES
FLAXMAN'S FORMATION	1608 METRES
WARRE FORMATION	1671 METRES
EUMERALLA FORMATION	1735 METRES
T.D.	1800 METRES

WELL SUMMARY

MUD SUMMARY BY INTERVAL
OBSERVATIONS AND RECOMMENDATIONS

WELL SUMMARY

MUD SUMMARY BY INTERVAL
OBSERVATIONS AND RECOMMENDATIONS

WELL SUMMARY

SUMMARY BY INTERVAL

INTERVAL: 0-302 METRES

12 1/4" HOLE

9 5/8" CASING

From the digging of the conductor hole it had been observed that the Port Campbell Limestone and the water table were about 4 metres from surface. To minimise chances of hole washout around the conductor, or loss circulation, the well was spudded in with Lime flocculated Bentonite spud mud of 45 seconds funnel viscosity.

There appeared to be a partial mud loss, amounting to about 50 bbls during the drilling of the first three singles through soft porous Limestone immediately beneath the conductor.

Drilling then continued with apparently full returns, with prehydrated Kwik-Thik, and Lime being added to maintain a Lime flocculated Bentonite mud of 34-36 seconds viscosity, and an 18 lb/100 sq ft yield point. There was very little native clay in the section to aid viscosity, but Bentonite additions were minimised, as the top of the Gellibrand Marl was anticipated at about 190 metres. Cuttings returns at the shakers with the relatively low viscosity but high yield point mud were reasonably consistent and cleared up quickly during circulation suggesting a reasonably gauge hole with the mud having sufficient cuttings carrying capacity.

The top of the Gellibrand Marl was reached at 177 metres, with drilling stopped at 190 metres for half an hour due to partial lost circulation of about 200 bbl. Apparently the annulus had loaded up with excessive cuttings from the Marl, probably resulting in partial mud loss below the conductor shoe. As it was anticipated this would heal itself with reduced weight in the annulus with the native clay being drilled, the mud was watered back, and the pump rate cut back from 460 gpm to 310 gpm. Drilling continued with full circulation, and the pump rate was gradually increased back to 460 gpm. Viscosity was controlled to about 36 seconds with mud weight maintained at 8.9 ppg with water dilution to minimise the chance of a mud ring forming.

At the 302 metres casing point, a wiper trip was run without problems, with a Lime flocculated hi-viscosity sweep pumped around. The 9 5/8" casing was then run in and cemented to 299 metres, with cement returning to the surface after 30 bbl of displacement, indicating the hole had been in reasonably good gauge.

WELL SUMMARY

INTERVAL: 302-1800 METRES

8 1/2" HOLE

As almost another 200 metres of Gellibrand Marl was anticipated below the 9 5/8" casing shoe, the surface mud was diluted with water by dumping and cleaning out the sandtrap, degasser, and desander tanks.

After nipling up was completed the cement and casing shoe plus an additional 6 meters of new hole to 308 metres was drilled out with predominantly water. A leak off test was run giving a 14.2 ppg equivalent at 308 metres.

Drilling then continued steadily through the Gellibrand Marl, with a small amount (1-1 1/2% by weight) of Potassium Chloride added. This was done to improve clay inhibition just sufficiently to give good cuttings at the shakers, and drastically reduce dilution rates, thus saving on water consumption. At the time water consumption was actually of some concern, as the turkey's nest did not appear to be holding water properly. Initially the pumps were run at 260 gpm in the 8 1/2" hole but with some hydraulicking of the kelly on early connections due to apparent tight hole, this was increased to 285 gpm and connections improved. With residual cement contamination retained in the mud through most of the Marl for increased inhibition, Bicarbonate was added and the Potassium Chloride allowed to drop off towards the end of the Marl. This was to allow the native clay content to increase, prior to entering the Dilwyn Sands. Mud weight rose only to 8.8 ppg with viscosity controlled between 33-35 seconds through the Marl, and no problems were experienced.

With the top of the Dilwyn Sand formation at 630 metres, the pump rate was decreased to 215 pgm, with a corresponding nozzle velocity of 248 ft/sec, and impact force of 240-250 lb. The drill rate still improved in the looser sands and hole cleaning was quite adequate with the flocculated Bentonite mud with yield points of 20-30 lb/100 sq ft. Sand returns at the shakers were steady and not excessive with the B40/B60 mesh screens giving no real problems, indicating the hole was not washing out badly. Bentonite additions were minimised with only a small amount of prehydrated Kwik Thik added through this section to bring the viscosity up to 38 seconds. This was both to minimise costs, and also to allow for additional Polymers and Bentonite to be added later on towards the bottom of the Dilwyn formation to reduce the filtration control while drilling through the Pember Mudstone. In this way the mud was gradually converted from a flocculated Bentonite mud with no water loss control, to a deflocculated Freshwater-Bentonite-Polymer mud with a filtrate of

WELL SUMMARY

9 cc's by the time the Pebble Point formation was reached at 909 metres, using Bicarbonate, CMC EHV, Polysal and additional Kwik Thik.

After circulating out the drilling break at 913 metres, drilling continued to 1001 metres, through the top of the Paraate formation at 960 metres, before tripping for a bit change. With a stabiliser and jars added to the bottom hole assembly, it was necessary to ream back in from 746 metres to bottom. This suggested that the hole must have been in reasonably good gauge through this interval.

While continuing drilling through the Paraate formation, the mud was maintained with additions of prehydrated Kwik Thik and CMC EHV to maintain rheology, but only control the filtrate to about 12 cc's. With the desilter out of order for most of the rest of the well it was necessary to begin regular dumping of the sandtrap together with increased dilution and finer shaker screens to control the mud weight at 9.3 ppg. A 7 stand wiper trip at 1211 metres had tight hole from 1200 metres to 1000 metres requiring working with the kelly. On running back in, the mud was hydraulicking up the string indicating packing off around the bottom hole assembly, so the mud was circulated for half an hour, before being able to run back in and resume drilling.

In the Skull Creek Mudstone from 1268 metres the samples became very, very sticky with the dumping and dilution rate having to be increased to control the mud weight to 9.3 ppg. Mud properties were being stabilised with the viscosity at 44-46 seconds and filtration control reduced to 8 ccs, with a yield point of 12-14 lb/100 sq ft.

After circulating out a drilling break in the top of the Nullawarre Greensand at 1372 metres, another wiper trip was made at 1398 metres. Again it was necessary to work tight hole up to 1151 metres with the kelly, but it was possible to run back in satisfactorily. Then drilling continued steadily through the Nullawarre Greensand, maintaining the same consistent mud properties with additions of premixed Bentonite, CMC EHV and Polysal with the filtration control steadily reduced to around 6.5 ccs. The top of the Belfast Mudstone was reached at 1580 metres, but there wasn't much thickness of true mudstone with the Flaxman's formation coming in at 1608 metres, and the drilling break circulated out at 1613 metres.

Another wiper trip was made at 1627 metres, with tight hole requiring working with the kelly up to 1426 metres, but running back in without problems. At the time, it was hoped that with the last of

WELL SUMMARY

the very sticky mudstones having been drilled, trips would improve, and this did occur. At 1655 metres a trip for a bit change was made, still in the Flaxman's formation, as the main target, the Warre Sandstone, was much deeper than predicted. This complete round trip was very good, with no significant tight hole, only requiring 3 singles to be reamed to bottom, as the old bit had been slightly undergauge.

The major target, the Warre Sandstone, was then reached at 1671 metres, with drilling breaks circulated out at 1674 metres, 1680 metres and 1700 metres but with no shows, so drilling continued on with the Eumeralla formation being reached at 1735 metres, to T.D. at 1800 metres.

A ten stand wiper trip was run with tight hole from 1637 metres to 1551 metres, so reamed back in from 1579 metres to 1687 metres, to ease the problem. After circulating out again, pulled out to run Gearhart wireline logs, with no significant tight hole.

The logs were then run for 14 1/2 hours with no hole problems, with the logger's T.D. being exactly the same at 1800 metres. The caliper log showed the hole to be in very good gauge overall with a degree of washout above 600 metres at around a 10" average, but excellent gauge below that to T.D.

After completing logging, the well was plugged and abandoned.

WELL SUMMARY

CONCLUSION AND SUMMARY

Callista #1 was spudded in on 27th March, 1988 and drilled with a Freshwater-Bentonite-Polymer mud, reaching it's 1800 metres T.D. on 5th April. Following wireline logging, it was then plugged and abandoned as a dry hole on 6th April, 1988.

No significant mud problems were experienced at all, with the final mud bill reaching \$8663.04 which included some damaged stock, and materials used for cementing. The actual mud consumption for drilling would have been close to \$8000.00. This can be considered as quite a low cost for this well, with the short duration of the well helping to keep maintenance costs down.

Tight hole problems were experienced again, as on Iona #1, and could be related to the drilling of the major mudstone/siltstone sequences. It appeared that sticky clay would build up around the bottom hole assembly while pulling back through the recently drilled mudstone or siltstone and then become tight in the near gauge hole being drilled. With time and periodic wiper trips to clean off the side of the hole the problem decreased, so that by T.D. the wireline logging runs had no problems at all, with the hole showing good stability.

As on Iona #1, the 8 1/2" hole was in very good gauge, particularly below 600 metres where the pump rate was reduced from 285 gpm. The extra washout above 600 metres serves to highlight the susceptibility of these formations to hydraulic erosion. For this reason it is still recommended to maintain low nozzle velocity of around 250 ft/sec on these wells through formations of interest.

The use of a small amount of KCl while drilling through the Gellibrand Marl, to give a 1-1 1/2% by wt solution is recommended to be repeated in future. For a small cost, which is fairly insignificant by the end of the well, it virtually eliminated chances of a mud ring, gives much better cuttings for samples, greatly reduces water consumption, and consequently results in much less filling up of the sump.

Overall the results on the Iona #1 and Callista #1 wells show definitely that a Freshwater-Bentonite-Polymer mud in conjunction with low hydraulics can produce a good hole. Through the upper cretaceous and tertiary Otway Basin sequences. The only problems experienced being some tight hole on trips, and sticky mudstone

WELL SUMMARY

cuttings through the Skull Creek, Belfast Mudstones and the top of the Eumeralla formation. The use of a KCl mud most likely would not improve the tight hole situation very much, if at all, from past experiences with close to gauge holes. Mudstone/siltstone samples would be improved, and if this is considered as a strong enough priority, then a KCl mud should be used, for this reason alone.

WELL SUMMARY

MUD CONSUMPTION BY INTERVAL

TOTAL MATERIAL CONSUMPTION

WELL SUMMARY

OPERATOR: BEACH PETROLEUM

WELL: CALLISTA #1

HOLE SIZE..12 1/4"...

INTERVAL..SURFACE - 302 METRES

CASING SIZE..9 5/8"....
(at 299 metres)

PRODUCT	QUANTITY	COST
MAGCOGEL	12 x 100 lb sx	\$ 195.12
KWIK THIK	90 x 25 kg sx	\$ 972.00
CAUSTIC SODA	5 x 25 kg sx	\$ 113.75
LIME	5 x 25 kg sx	\$ 23.75
POTASSIUM CHLORIDE	2 x 50 kg sx	\$ <u>29.82</u>
TOTAL INTERVAL COST :		\$ 1334.44

WELL SUMMARY

OPERATOR: BEACH PETROLEUM

WELL: CALLISTA #1

HOLE SIZE...8 1/2"...

INTERVAL....302 - 1800 METRES

CASING SIZE...-.....

PRODUCT	QUANTITY	COST
BARITE	47 x 50 kg sx	\$ 314.90
MAGCOGEL	42 x 100 lb sx	\$ 682.92
KWIK THIK	72 x 25 kg sx	\$ 777.60
CAUSTIC SODA	16 x 25 kg sx	\$ 364.00
LIME	7 x 25 kg sx	\$ 33.25
S. BICARBONATE	5 x 40 kg sx	\$ 84.90
POTASSIUM CHLORIDE	36 x 50 kg sx	\$ 536.76
CMC EHV	26 x 25 kg sx	\$ 1392.82
MAGCOPOLYSAL	61 x 25 kg sx	\$ 2363.75
D.I. - CIDE	4 x 25 lt drum	\$ 148.20
PIPE LAX	1 x 205 lt drum	\$ 587.50
CALCIUM CHLORIDE	3 x 25 kg sx	\$ <u>42.00</u>
TOTAL INTERVAL COST :		\$ 7328.60

WELL SUMMARY

TOTAL MATERIAL CONSUMPTION

OPERATOR: BEACH PETROLEUM

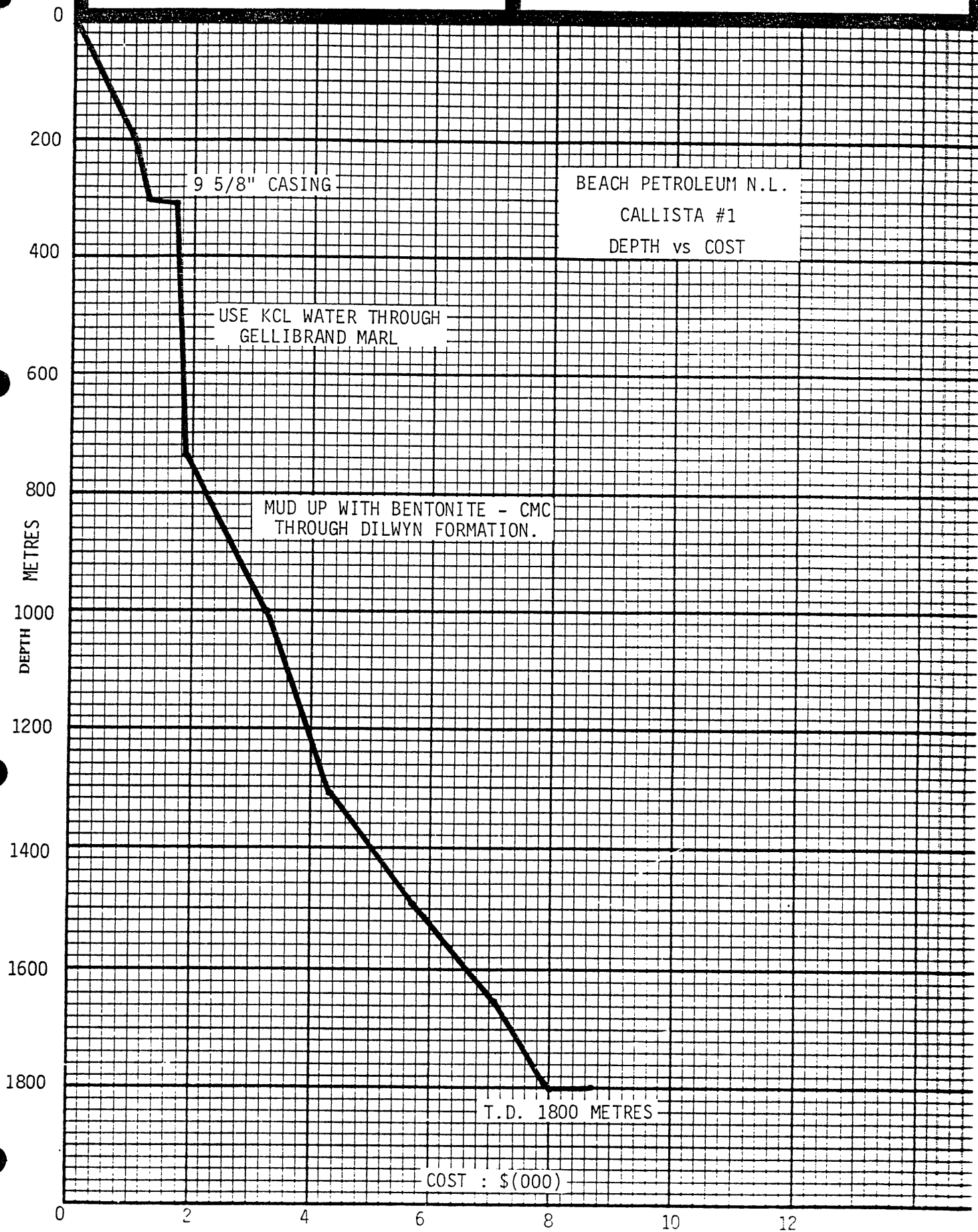
WELL: CALLISTA #1

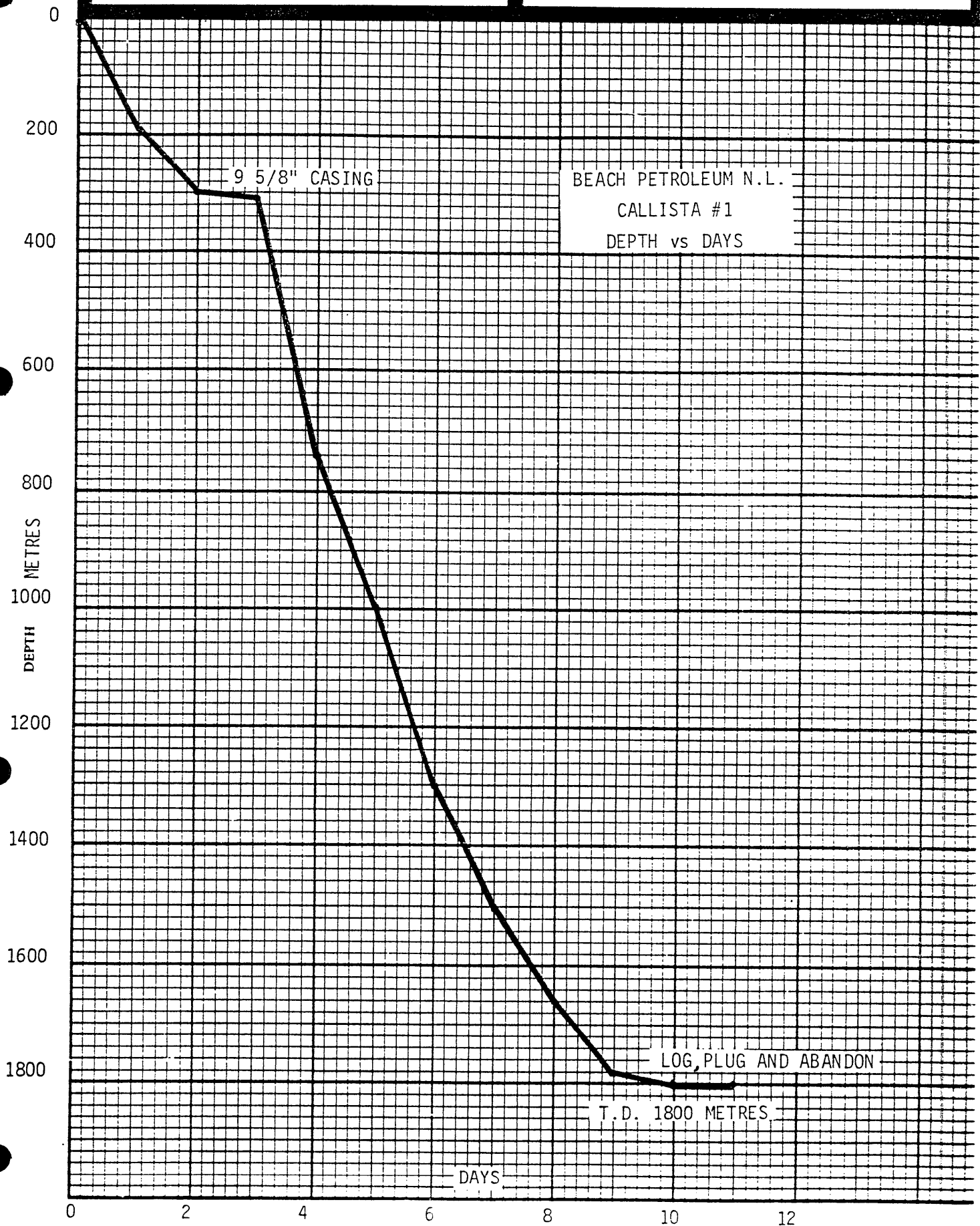
LOCATION: OTWAY BASIN, VICTORIA

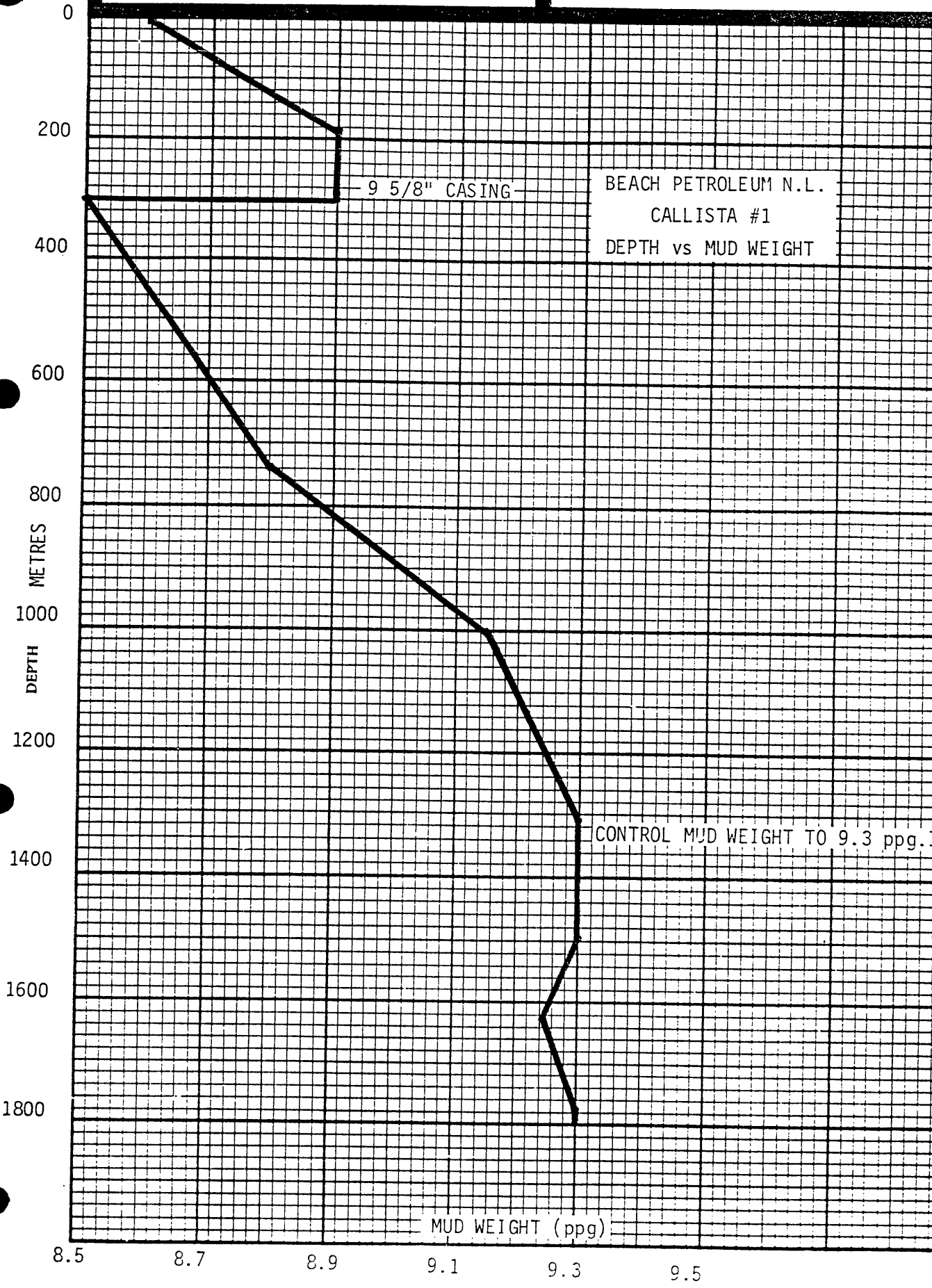
PRODUCT	UNIT	COST	%
BARITE	47 x 50 kg sx	\$ 314.90	3.63
MAGCOGEL	54 x 100 lb sx	\$ 878.04	10.14
KWIK THIK	162 x 25 kg sx	\$ 1749.60	20.20
CAUSTIC SODA	21 x 25 kg sx	\$ 477.75	5.50
LIME	12 x 25 kg sx	\$ 57.00	0.66
BICARBONATE	5 x 40 kg sx	\$ 84.90	0.98
POTASSIUM CHLORIDE	38 x 50 kg sx	\$ 566.58	6.54
CMC EHV	26 x 25 kg sx	\$ 1392.82	16.08
MAGCOPOLYSAL	61 x 25 kg sx	\$ 2363.75	27.29
D.I. - CIDE	4 x 25 lt drum	\$ 148.20	1.71
PIPE LAX	1 x 205 lt drum	\$ 587.50	6.78
CALCIUM CHLORIDE	3 x 25 kg sx	\$ <u>42.00</u>	<u>0.49</u>
TOTAL MATERIAL COST :		\$ 8663.04	100.00

WELL SUMMARY

GRAPHS







WELL SUMMARY

BIT AND HYDRAULICS RECORD

WELL SUMMARY

DAILY MUD REPORTS

DRILLING MUD REPORT

M-I Drilling Office



DRILLING MUD REPORT NO. 1

DATE 27/3 19 88 DEPTH 190m

SPUD DATE 27/3/88 PRESENT ACTIVITY DRILLING

P.O. BOX 42842 ■ HOUSTON, TEXAS 77242 USA

OPERATOR BRON PETROLEUM CONTRACTOR GRADING DRILLING RIG NO. 2

REPORT FOR H WALKER REPORT FOR S. MOORE SECTION, TOWNSHIP, RANGE T10S00N

WELL NAME AND NO. COLUSA No 1 FIELD OR BLOCK NO. FFC 108 COUNTY, PARISH OR OFFSHORE AREA GRADY PARISH STATE/PROVINCE VICTORIA

DRILLING ASSEMBLY			CASING	MUD VOLUME (BBL)		CIRCULATION DATA		
BIT SIZE	TYPE	JET SIZE	SURFACE	HOLE	PITS	PUMP SIZE	X IN.	ANNULAR VEL (ft/min)
12 1/4	IC 3	12/12/16	16" in. @ 5m	80 bbl	400 bbl	5 1/2 x 2 6 x 2		DP 27 DC 131
PIPE SIZE	TYPE	LENGTH	INTERMEDIATE	TOTAL CIRCULATING VOLUME		PUMP MAKE, MODEL	ASSUMED EFF	CIRCULATION PRESSURE (psi)
6 1/2	16.6 lb		in. @	400 bbl		GD 128	97 %	400
PIPE SIZE	TYPE	LENGTH	INTERMEDIATE	IN STORAGE	WEIGHT	bbl/stk	stk/min	BOTTOMS UP (min) (strk)
4 1/2	11.0 lb	12.4m	in. @	80 bbl	11.015 G/G	005/065	9.0/7m	7
DRILL COLLAR SIZE	LENGTH	PRODUCTION OR LINER	MUD TYPE			bbl/min	gal/min	TOTAL CIRC TIME (min) (strk)
6 1/2 x 3 1/2	15.6m	in. @	FW GEL/WATER			11.0	401	8

MUD PROPERTIES				MUD PROPERTY SPECIFICATIONS			
Sample From	<input type="checkbox"/> FL <input checked="" type="checkbox"/> PIT	<input type="checkbox"/> FL <input checked="" type="checkbox"/> PIT	WEIGHT	VISCOSITY		FILTRATE	
Sample Taken			14.00	24.00			
Mudline Temperature (°F)							
Depth (ft)	(TVD)	(ft)	RECOMMENDED TREATMENT				
Height	<input checked="" type="checkbox"/> (ppg)	<input type="checkbox"/> (lb/cu ft)	<input type="checkbox"/> (sp gr)				
Annular Viscosity (sec/qt) API @	°F	45	36				
Plastic Viscosity cp @	°F	7	15				
Gel Point (lb/100 ft²)		1	8.12				
Gel Strength (lb/100 ft²) 10 sec/10 min							
Filtrate API (cm³/30 min)		N.C.	N.C.				

				REMARKS			
API HTHP Filtrate (cm³/30 min) @	°F			AIRLINE ON SIZE 2 1/2 x 3 1/2 PIC 5' TO 4' 10" DEPTH			
Shake Thickness (32nd in. API/HTHP)		1	1	100 mesh 120 bbl (KNOX) IN 1000 LITERS			
Solids Content (% by Vol) <input type="checkbox"/> calculated <input type="checkbox"/> retort			4	SOLID IN MUD WITH API 4/10 FROM 1000 LITERS			
Liquid Content (% by Vol) Oil/Water		1	196	DUE TO MUD OIL AND WATER CONTENT IN 1000 LITERS			
Sand Content (% by Vol)			TRAC	DISPERSED WITH MUD IN 1000 LITERS			
Methylene Blue Capacity (1 lb/bbl equiv / 1 cm³/cm³ mud)				SOLID IN MUD 12-06 100 LITERS IN 1000 LITERS			
Alkalinity Mud (P _m)			10.4	SOLID IN MUD 12-06 100 LITERS IN 1000 LITERS			
Alkalinity Filtrate (P _f /M _f)		1	15.1-35	DUE TO 100 bbl, 1000 LITERS CONTAINED WITH			
Chloride (mg/L)			700	DUE TO 100 bbl, 1000 LITERS CONTAINED WITH			
Total Hardness as Calcium (mg/L)			70	DUE TO 100 bbl, 1000 LITERS CONTAINED WITH			

PRODUCT INVENTORY	SOLIDS EQUIPMENT														
	BRAND	MODEL	TYPE	SIZE	QTY	QTY	QTY	QTY	QTY	QTY	QTY	QTY	QTY	QTY	QTY
STARTING INVENTORY	612	112	49	134	61	21	22	22	11	32	25	38	40	9	1
RECEIVED															
USED LAST 24 HRS		30	5							5		2			
ENDING INVENTORY	412	22	44	134	61	21	23	27	11	35	25	36	40	9	1
COST FROM IADC		840	112							2375		2180			

M-I REPRESENTATIVE M. GILBERT PHONE 281 727-103 WAREHOUSE PHONE DAILY COST 91031.22 CUMULATIVE COST 91031.22

DRILLING MUD REPORT



DRILLING MUD REPORT NO. 2

DATE 28/3/19 DEPTH 302

SPUD DATE 27/3/19 PRESENT ACTIVITY U.O.C.L.

P.O. BOX 42842 ■ HOUSTON, TEXAS 77242 USA

OPERATOR BRACH PETROLEUM CONTRACTOR GENCO/BRACH RIG NO. 2

REPORT FOR H WALKER REPORT FOR S MAIN SECTION, TOWNSHIP, RANGE 7

WELL NAME AND NO. CONCRETE NO. 1 FIELD OR BLOCK NO. PIT 102 COUNTY, PARISH OR OFFSHORE AREA STAMPAH CO. STATE/PROVINCE TX

DRILLING ASSEMBLY			CASING	MUD VOLUME (BBL)		CIRCULATION DATA		
BIT SIZE	TYPE	JET SIZE	SURFACE	HOLE	PITS	PUMP SIZE	X IN.	ANNULAR VEL (ft/min)
2 1/4	16.5	12/18/14	9 1/8 in. @ 297 ft.	70 bbl	350 bbl	5' x 3, 6 x 8		DP 77 DC 131
WELL PIPE SIZE	TYPE	LENGTH	INTERMEDIATE	TOTAL CIRCULATING VOLUME		PUMP MAKE, MODEL	ASSUMED EFF.	CIRCULATION PRESSURE (psi)
4 1/2	16.611		in. @ ft.	420 bbl		CA 128	91%	600
WELL PIPE SIZE	TYPE	LENGTH	INTERMEDIATE	IN STORAGE	WEIGHT	bbl/stk	stk/min	BOTTOMS UP (min) (strk)
4 1/2	11.25	12.4	in. @ ft.	6 bbl	1000	0.57/0.06	2.7/10	10
DRILL COLLAR SIZE	LENGTH	PRODUCTION OR LINER	MUD TYPE			110	4.4	TOTAL CIRC TIME (min) (strk)
6 1/2 EHO	15.6	in. @ ft.	F.L. GEL/PROV					40

Sample From	MUD PROPERTIES		MUD PROPERTY SPECIFICATIONS		
	<input type="checkbox"/> FL <input type="checkbox"/> PIT	<input type="checkbox"/> FL <input type="checkbox"/> PIT	WEIGHT	VISCOSITY	FILTRATE
Time Sample Taken	08:00		RECOMMENDED TREATMENT		
Downline Temperature (°F)			CONT. ADDS THROUGH MAIN LINE. ADD 17 GAL PER MIN. MIX WATER FOR GRAB SAMPLES.		
Depth (ft) (TVD)	1	ft)	DROPPED AND CLEANED SANDTRAP, BEHIND MAIN DISCHARGE TANKS, AND FILLED WITH WATER.		
Weight (ppg)	<input type="checkbox"/> (lb/cu ft)	<input type="checkbox"/> (sp gr)	8.9		
Annular Viscosity (sec/qt) API @ °F			36		
Plastic Viscosity cp @ °F			7		
Gel Point (lb/100 ft²)			15		
Gel Strength (lb/100 ft²) 10 sec/10 min			6/12	1	
Filtrate API (cm³/30 min)			NC	REMARKS	
API HTHP Filtrate (cm³/30 min) @ °F			-	STOPPED DRILLING AT 1700. PAUSE TO BUILD UP MORE DR. VOLUME WITH WATER DUE TO LAST CIRC. (PARTIAL - LOST 200 BBL TO MUD)	
Shake Thickness (32nd in. API/HTHP)			-	1	PRESUME BEHIND MAIN LINE WITH WATER. MUD REQUIRES PUMP RATE OF 120 SPM. WITH THIS CIRCULATION.
Solids Content (% by Vol) <input type="checkbox"/> calculated <input type="checkbox"/> retort			4	CONTINUED DRILLING THROUGH MAIN LINE. PUMP RATE GRABBERED APPROX 120 SPM. AT THIS POINT APPROXIMATELY 1000	
Liquid Content (% by Vol) Oil/Water			- 17%	1	AT 3000 FEET THE DR. BEHIND MAIN LINE WAS SEEN. DR. BEHIND MAIN LINE WAS SEEN ON 2000 FEET. DR. BEHIND MAIN LINE WAS SEEN ON 2000 FEET.
Sand Content (% by Vol)			Trace	DR. BEHIND MAIN LINE WAS SEEN ON 2000 FEET. DR. BEHIND MAIN LINE WAS SEEN ON 2000 FEET.	
Methylene Blue Capacity <input type="checkbox"/> lb/bbl equiv <input type="checkbox"/> cm³/cm³ mud			-	DR. BEHIND MAIN LINE WAS SEEN ON 2000 FEET. DR. BEHIND MAIN LINE WAS SEEN ON 2000 FEET.	
Fluid Loss <input type="checkbox"/> Strip <input type="checkbox"/> Meter @ °F			95	DR. BEHIND MAIN LINE WAS SEEN ON 2000 FEET. DR. BEHIND MAIN LINE WAS SEEN ON 2000 FEET.	
Alkalinity Mud (P _m)			-	DR. BEHIND MAIN LINE WAS SEEN ON 2000 FEET. DR. BEHIND MAIN LINE WAS SEEN ON 2000 FEET.	
Alkalinity Filtrate (P _f /M _f)			110/13	1	DR. BEHIND MAIN LINE WAS SEEN ON 2000 FEET. DR. BEHIND MAIN LINE WAS SEEN ON 2000 FEET.
Chloride (mg/L)			750	DR. BEHIND MAIN LINE WAS SEEN ON 2000 FEET. DR. BEHIND MAIN LINE WAS SEEN ON 2000 FEET.	
Total Hardness as Calcium (mg/L)			30	DR. BEHIND MAIN LINE WAS SEEN ON 2000 FEET. DR. BEHIND MAIN LINE WAS SEEN ON 2000 FEET.	

PRODUCT INVENTORY	BRAND	ALUMINA	CAUSTIC	GEL	LOSS PREVENTION	PHOSPHATE	BIOMASS	SPERM	DT CAP	LIME	SEAL	WAX	CELL	WATER	SOLIDS EQUIPMENT
STARTING INVENTORY	414	72	44	134	61	21	23	72	11	33	24	36	40	1	SHAKER #1 140, 100 mesh
RECEIVED															SHAKER #2 140, 100 mesh
USED LAST		10		12											MUD CLEANER mesh
CLOSING INVENTORY	414	72	44	122	61	21	23	72	11	33	24	36	40	1	CENTRIFUGE 114 hours
COST		10.2		115.8											DESANDER 114 hours
NET FROM IADC															DESILTER 3 hours

DATE PRESENTATIVE _____ PHONE _____ WAREHOUSE PHONE _____ DAILY COST \$ 20.12 ✓ CUMULATIVE COST \$ 1200.00 ✓

DRILLING MUD REPORT

M-I DISTRICT OFFICE



DRILLING MUD REPORT NO. **3**

DATE **2/1/31** 19 **28** DEPTH **308**

SPUD DATE **27/5/33** PRESENT ACTIVITY **LEAN CUTTING**

P.O. BOX 42842 ■ HOUSTON, TEXAS 77242 USA

OPERATOR **BENJAMIN PETERSON** CONTRACTOR **GRANITE DRILLING** RIG NO. **2**

REPORT FOR **11 WICKER** REPORT FOR **G. NICO** SECTION, TOWNSHIP, RANGE **14-00-00**

WELL NAME AND NO. **GRANITE No. 1** FIELD OR BLOCK NO. **P.E.P. 128** COUNTY, PARISH OR OFFSHORE AREA **OTWAI 13700** STATE/PROVINCE **VIC 00.0**

DRILLING ASSEMBLY			CASING		MUD VOLUME (BBL)		CIRCULATION DATA				
BIT SIZE 2 1/4	TYPE S11	JET SIZE 3x11	SURFACE 9 1/2 in. @ 219 ft	HOLE 60 bbl.	PITS 470 bbl.	PUMP SIZE 5 1/2 x 8	X 628	IN.	ANNULAR VEL (ft/min)		
DRILL PIPE SIZE 4 1/2	TYPE 16.0H	LENGTH	INTERMEDIATE	TOTAL CIRCULATING VOLUME 420 bbl.		PUMP MAKE, MODEL G.O. P22	ASSUMED EFF % 77		CIRCULATION PRESSURE (psi)		400
DRILL PIPE SIZE 4 1/2	TYPE 16.0H	LENGTH 57.0 ft	INTERMEDIATE	IN STORAGE	WEIGHT	bbl/stk 1057/061	stk/min 110/-		BOTTOMS UP (min) (strk)		8
DRILL COLLAR SIZE 6 1/2 R10	LENGTH 167.8 ft	PRODUCTION OR LINER	MUD TYPE FW @ NANOCOL			bbl/min 6.27	gal/min 263		TOTAL CIRC TIME (min) (strk)		75

Sample From	MUD PROPERTIES		MUD PROPERTY SPECIFICATIONS		
	<input type="checkbox"/> FL. <input checked="" type="checkbox"/> PIT	<input type="checkbox"/> FL. <input type="checkbox"/> PIT	WEIGHT	VISCOSITY	FILTRATE
Time Sample Taken	24.00				
Flowline Temperature (°F)					

RECOMMENDED TREATMENT					
Depth (ft) (TVD	1	ft)			Drilled out cement with PRODOMON
Weight (lb) (ppg)	<input type="checkbox"/> (lb/cu ft)	<input type="checkbox"/> (sp gr)	8.5		Water base mud system, 100% water
Annular Viscosity (sec/qt) API @	°F		2.0		60% iron cement for clay inhibition
Plastic Viscosity cp @	°F		2		Added additional 20% KCL for clay
Yield Point (lb/100 ft²)			3		Inhibitor to reduce water consumption and
Gel Strength (lb/100 ft²) 10 sec/10 min			1/3	1	Directional improve cuttings, loss stick, etc.

Filtrate API (cm³/30 min)	REMARKS	
	N.C.	Continued W.O.C. to 0300 hrs. Suspended at B.O.P. and pressure tested R.I.H. with 2 1/2" R10
API HTHP Filtrate (cm³/30 min) @	°F	-
Mudcake Thickness (32nd in. API/HTHP)		-/1
Solids Content (% by Vol) <input type="checkbox"/> calculated <input type="checkbox"/> retort		1
Liquid Content (% by Vol) Oil/Water		199
Sand Content (% by Vol)		Trace
Methylene Blue Capacity <input type="checkbox"/> 1bbl equiv <input type="checkbox"/> 1cm³/cm³ mud		-
Alkalinity Mud (P _m)		-
Alkalinity Filtrate (P _f /M _f)		4/5
Chloride (mg/L)		8000
Total Hardness as Calcium (mg/L)		450

PRODUCT INVENTORY	SOLIDS EQUIPMENT																	
	BRAIN	KWIK	TRUCK	CASING	GAL	CMC	PERMAN	BICARB	SODASOL	D.F. EM	LIME	SEDA	KCL	CaCl2	KWIK	DESL	DESIL	
STARTING INVENTORY	415	72	44	122	61	81	23	22	11	33	25	36	40	9	1			
RECEIVED																		
USED LAST hr	-	-	-	-	-	-	-	-	-	-	-	26	-	-	-			
CLOSING INVENTORY	415	72	44	122	61	81	23	22	11	33	25	10	40	9	1			
COST LAST hr												327.66						
USED (from IADC)																		
M-I REPRESENTATIVE	PHONE			WAREHOUSE PHONE			DAILY COST			CUMULATIVE COST								
MANAGER OLIVE	281-787102						\$ 327.66			\$ 1722.10								

DRILLING MUD REPORT

M-F DISTRICT OFFICE



P.O. BOX 42842 ■ HOUSTON, TEXAS 77242 USA



DRILLING MUD REPORT NO. 4

DATE 30/3/1988 DEPTH 737m

SPUD DATE 2/1/88 PRESENT ACTIVITY Drilling

OPERATOR Blaker Corporation CONTRACTOR Garwood Drilling RIG NO. 2

REPORT FOR H. Williams REPORT FOR G. Nicot SECTION, TOWNSHIP, RANGE 13N 10E 10W

WELL NAME AND NO. Calista No 1 FIELD OR BLOCK NO. F.P. 138 COUNTY, PARISH OR OFFSHORE AREA Orange Basin STATE/PROVINCE Victoria

DRILLING ASSEMBLY			CASING		MUD VOLUME (BBL)		CIRCULATION DATA		
BIT SIZE <u>8 1/2</u>	TYPE <u>S11</u>	JET SIZE <u>3x11</u>	SURFACE <u>9 1/8 in. @ 299m</u>	HOLE <u>170 bbls</u>	PITS <u>500 bbls</u>	PUMP SIZE <u>5 1/2 x 2, 6 x 2</u>	X	IN.	ANNULAR VEL (ft/min)
DRILL PIPE SIZE <u>4 1/2</u>	TYPE <u>16-6 1/8</u>	LENGTH <u>55 4m</u>	INTERMEDIATE <u>in. @ ft.</u>	TOTAL CIRCULATING VOLUME <u>670 bbls</u>		PUMP MAKE, MODEL <u>GO P2 8</u>	ASSUMED EFF <u>97%</u>		DP _____ DC _____
DRILL PIPE SIZE <u>4 1/2</u>	TYPE <u>11-0.08</u>	LENGTH <u>55 4m</u>	INTERMEDIATE <u>in. @ ft.</u>	IN STORAGE	WEIGHT	bbl/stk <u>0.57/0.067</u>	EFF <u>90/-</u>	stk/min	BOTTOMS UP (min) (strk) <u>22</u>
DRILL COLLAR SIZE <u>6 1/4 B3111</u>	LENGTH <u>167.7m</u>	PRODUCTION OR LINER <u>in. @ ft.</u>	MUD TYPE <u>F.W. MUD</u>			bbl/min <u>5.13</u>	gal/min <u>215</u>		TOTAL CIRC TIME (min) (strk) <u>130</u>

Sample From	MUD PROPERTIES		MUD PROPERTY SPECIFICATIONS		
	<input type="checkbox"/> FL. <input type="checkbox"/> PIT	<input type="checkbox"/> FL. <input type="checkbox"/> PIT	WEIGHT	VISCOSITY	FILTRATE
Time Sample Taken	<u>06:00</u>	<u>20:00</u>			
Wellbore Temperature (°F)					

Depth (ft) (TVD)	Weight (ppg)	Plastic Viscosity (cp @ 10 sec/10 min)	Filtrate API (cm³/30 min)	RECOMMENDED TREATMENT	
				API @ °F	°F
<u>1</u>	<u>8.6</u>	<u>33</u>	<u>NO CONTROL</u>	<u>8.8</u>	<u>35</u>
		<u>4</u>	<u>12</u>	<u>5</u>	<u>20</u>
		<u>4 1/6</u>	<u>12 1/2</u>		

HTHP Filtrate (cm³/30 min) @ °F	Mud Thickness (32nd in. API/HTHP)	Solids Content (% by Vol)	Methylene Blue Capacity	Alkalinity (P _m)	Alkalinity Filtrate (P _f /M _f)	Chloride (mg/L)	Total Hardness as Calcium (mg/L)	Remarks
<u>-</u>	<u>+</u>	<u>2</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>2,000</u>	<u>370</u>	<u>USED WATER WITH ADDITIONAL ...</u>
<u>-</u>	<u>+</u>	<u>2</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>2,000</u>	<u>430</u>	<u>FOR GULLERBAND MUD ...</u>
<u>-</u>	<u>+</u>	<u>2</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>2,000</u>	<u>430</u>	<u>BASE OF MUD ...</u>
<u>-</u>	<u>+</u>	<u>2</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>2,000</u>	<u>430</u>	<u>HYDRATION ...</u>
<u>-</u>	<u>+</u>	<u>2</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>2,000</u>	<u>430</u>	<u>CONTAINING ...</u>
<u>-</u>	<u>+</u>	<u>2</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>2,000</u>	<u>430</u>	<u>WATER AND ...</u>
<u>-</u>	<u>+</u>	<u>2</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>2,000</u>	<u>430</u>	<u>REMARKS</u>
<u>-</u>	<u>+</u>	<u>2</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>2,000</u>	<u>430</u>	<u>RAW LEAK OFF ...</u>
<u>-</u>	<u>+</u>	<u>2</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>2,000</u>	<u>430</u>	<u>CONTINUOUS ...</u>
<u>-</u>	<u>+</u>	<u>2</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>2,000</u>	<u>430</u>	<u>TRAILER ...</u>
<u>-</u>	<u>+</u>	<u>2</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>2,000</u>	<u>430</u>	<u>PUMP WAS ...</u>
<u>-</u>	<u>+</u>	<u>2</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>2,000</u>	<u>430</u>	<u>11.0 ...</u>
<u>-</u>	<u>+</u>	<u>2</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>2,000</u>	<u>430</u>	<u>REDUCED ...</u>
<u>-</u>	<u>+</u>	<u>2</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>2,000</u>	<u>430</u>	<u>ADDITIONAL ...</u>
<u>-</u>	<u>+</u>	<u>2</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>2,000</u>	<u>430</u>	<u>DRILL ...</u>
<u>-</u>	<u>+</u>	<u>2</u>	<u>-</u>	<u>-</u>	<u>-</u>	<u>2,000</u>	<u>430</u>	<u>DRILL ...</u>

PRODUCT INVENTORY	DRILLING MUD EQUIPMENT														SOLIDS EQUIPMENT	
	72	44	122	61	81	73	22	11	33	25	10	40	9	1		
RECEIVED																SHAKER #1 <u>P4</u> , <u>B6</u> mesh
LAST																SHAKER #2 <u>P4</u> , <u>B6</u> mesh
INVENTORY	72	44	122	61	81	73	22	11	33	25	10	40	9	1		MUD CLEANER _____ mesh
COST																CENTRIFUGE _____ hours
(IADC)																DESANDER <u>7-11</u> <u>24</u> hours
																DESILTER <u>5/11</u> <u>6</u> hours

M-I REPRESENTATIVE [Signature] PHONE 054 287103 WAREHOUSE PHONE _____ DAILY COST 4,200.00 CUMULATIVE COST 1,1424.16

DRILLING MUD REPORT

M-I DISTRICT OFFICE



P.O. BOX 42842 ■ HOUSTON, TEXAS 77242 USA



DRILLING MUD REPORT NO. 5

DATE 31/3/88 19 88 DEPTH 1001m

SPUD DATE 27/5/88 PRESENT ACTIVITY Drilling

OPERATOR BRADY PERCEVALUM CONTRACTOR CRANFORD DRILLING RIG NO. 2

REPORT FOR 11 WORKER REPORT FOR C. NICOL SECTION, TOWNSHIP, RANGE Timberson

WELL NAME AND NO. COUNCIL No 1 FIELD OR BLOCK NO. P.P. 128 COUNTY, PARISH OR OFFSHORE AREA OTWAY BASIN STATE/PROVINCE VIC 3810

DRILLING ASSEMBLY			CASING		MUD VOLUME (BBL)		CIRCULATION DATA		
BIT SIZE	TYPE	JET SIZE	SURFACE	HOLE	PITS	PUMP SIZE	X IN.	ANNULAR VEL (ft/min)	
8 1/2	511	3x11	9 1/2 in. @ 299 m ft	220 bbls	420 bbls	1 1/2 x 6, 6x2		DP 102 DC 154	
DRILL PIPE SIZE	TYPE	LENGTH	INTERMEDIATE	TOTAL CIRCULATING VOLUME		PUMP MAKE, MODEL	ASSUMED EFF	CIRCULATION PRESSURE (psi)	
5 1/2	16 1/2		in. @ ft.	640 bbls		GO P28	97 %	600	
DRILL PIPE SIZE	TYPE	LENGTH	INTERMEDIATE	IN STORAGE	WEIGHT	bbl/stk	stk/min	BOTTOMS UP (min) (strk)	
4 1/2	10.00	55.4 m	in. @ ft.	80 bbl	PRC. 10			35	
DRILL COLLAR SIZE	LENGTH	PRODUCTION OR LINER	MUD TYPE			513	2.5	TOTAL CIRC TIME (min) (strk)	
6 1/2	167.7 m	in. @ ft.	FW. G. / CMC.					125	

MUD PROPERTIES			MUD PROPERTY SPECIFICATIONS		
Sample From	<input type="checkbox"/> FL <input checked="" type="checkbox"/> PIT	<input type="checkbox"/> FL <input checked="" type="checkbox"/> PIT	WEIGHT	VISCOSITY	FILTRATE
Time Sample Taken	05:00	12:00			
Downline Temperature (°F) @	31	31	RECOMMENDED TREATMENT		
Depth (ft) (TVD 1 ft)	970		USE 2% POLYMER AND 2% SODIUM CARBONATE		
Weight <input checked="" type="checkbox"/> (ppg) <input type="checkbox"/> (lb/cu ft) <input type="checkbox"/> (sp gr)	2.4	9.1	ADJUST THROUGH DRILLING FLUIDS		
Annular Viscosity (sec/qt) API @ °F	32	42	CHECK SOLIDS / 700 PHASE MUDS		
Plastic Viscosity cp @ °F	5	15	ADJUST POLYMER, ADDING COL AND POLYMER TO		
Yield Point (lb/100 ft²)	30	16	ADJUST WATER LOSS PERCENTAGE		
Shear Strength (lb/100 ft²) 10 sec/10 min	12 / 15	8 / 15	REMARKS -		
Filtrate API (cm³/30 min)	2.5	9.0	CONTINUOUSLY MONITOR THROUGH DRILLING		
API HTHP Filtrate (cm³/30 min) @ °F	-	-	SOLIDS WITH DRAIN RATE INCREASE		
Shake Thickness (32nd in. API/HTHP)	4	2 / 32	ADJUST POLYMER AND POLYMER TO MAINTAIN		
Solids Content (% by Vol) <input checked="" type="checkbox"/> calculated <input type="checkbox"/> retort	3	5	ADJUST THROUGH DRILLING FLUIDS		
Liquid Content (% by Vol) Oil/Water	- 177	- 192	ADJUST THROUGH DRILLING FLUIDS		
Sand Content (% by Vol)	TRACE	TRACE	MUDS		
Methylene Blue Capacity <input type="checkbox"/> lb/bbl equiv <input type="checkbox"/> cm³/cm³ mud	-	-	CHECK AND ADJUST THROUGH DRILLING		
Thickener <input type="checkbox"/> Strip <input type="checkbox"/> Meter @ °F	9.0	9.5	ADJUST THROUGH DRILLING FLUIDS		
Alkalinity Mud (P _m)	-	-	SODIUM		
Alkalinity Filtrate (P _f /M _f)	22 / 1	22 / 1.5	CONTINUOUSLY MONITOR THROUGH DRILLING		
Chloride (mg/L)	4,500	3,000	CHECK SOLIDS AND POLYMER THROUGH DRILLING		
Total Hardness as Calcium (mg/L)	250	30	ADJUST THROUGH DRILLING		

PRODUCT INVENTORY	BRAND	QUANTITY	UNIT	DATE	REMARKS	SOLIDS EQUIPMENT										
STARTING INVENTORY	415	22	44	122	61	21	21	22	11	20	25	-	40	9	1	SHAKER #1 800, 1000 mesh
RECEIVED																SHAKER #2 800, 1000 mesh
USED LAST	15	20	4	-	11	5	3	-	1	-	-	-	-	-	-	MUD CLEANER - mesh
CLOSING INVENTORY	415	52	40	122	50	76	18	22	10	29	25	-	40	9	1	CENTRIFUGE - hours
COST LAST	15	210	21	-	52227	1924	5000	-	2700	-	-	-	-	-	-	DESANDER 1000, 1500, 1900 mesh
USED FROM IADC																DESILTER 1000, 1500, 1900 mesh

M-I REPRESENTATIVE BRADY PERCEVALUM PHONE 281 722105 WAREHOUSE PHONE DAILY COST \$120.50 CUMULATIVE COST \$2200.00

DRILLING MUD REPORT

M-I DISTRICT OFFICE



DRILLING MUD REPORT NO. 6

DATE 1/14/1936 DEPTH 1305 m

SPUD DATE 27/3/28 PRESENT ACTIVITY DRILLING

P.O. BOX 42842 ■ HOUSTON, TEXAS 77242 USA

OPERATOR BROOK PETROLEUM CONTRACTOR GRANDER DRILLING RIG NO. 2

REPORT FOR H. WALKER REPORT FOR G. NICOT SECTION, TOWNSHIP, RANGE 11MB00N

WELL NAME AND NO. CAJALISTA No 1 FIELD OR BLOCK NO. P.P.P. 108 COUNTY, PARISH OR OFFSHORE AREA GRAND BASIN STATE/PROVINCE VICTORIA

DRILLING ASSEMBLY			CASING		MUD VOLUME (BBL)		CIRCULATION DATA			
BIT SIZE	TYPE	JET SIZE	SURFACE	HOLE	PITS	PUMP SIZE	X	IN.	ANNULAR VEL (ft/min)	
2 1/2	J11	3x11	9 5/8 in. @ 249 ft	285 bbl	420 bbl	5 1/2 x 8, 6 x 8			DP 102	DC 159
DRILL PIPE SIZE	TYPE	LENGTH	INTERMEDIATE	TOTAL CIRCULATING VOLUME		PUMP MAKE, MODEL	ASSUMED EFF	CIRCULATION PRESSURE (psi)		
4 1/2	16-6 1/2		in. @ ft	705 bbl		GO P2 B	71	650		
DRILL PIPE SIZE	TYPE	LENGTH	INTERMEDIATE	IN STORAGE	WEIGHT	bbl/stk	stk/min	BOTTOMS UP (min) (strk)		
4 1/2	17WD	66.4 m	in. @ ft	20 bbl	PREMIX	0.057/0.06	70/-	45		
DRILL COLLAR SIZE	LENGTH	PRODUCTION OR LINER	MUD TYPE		5.13		2.15	TOTAL CIRC TIME (min) (strk)		
6 1/2 BUC	16' 1-3 m	in. @ ft	F.W. / CAL / POLYMER		bbl/min		gal/min	138		

Sample From	MUD PROPERTIES		MUD PROPERTY SPECIFICATIONS	
	<input type="checkbox"/> FL. <input checked="" type="checkbox"/> PIT	<input type="checkbox"/> FL. <input type="checkbox"/> PIT	WEIGHT	VISCOSITY
me Sample Taken	05-30	24-00		
Flowline Temperature (°F)		34°C	RECOMMENDED TREATMENT	
Depth (ft) (TVD 1 ft)		1305 m	After circulating mud - 90 min.	
Weight (ppg) (lb/cu ft) (sp gr)	9.2	9.3	FRUEN ADD. REQUIRED TO INCREASE PLAN	
Annular Viscosity (sec/qt) API @ °F	45	40	GIVE THERMAL STABILITY AND PREVENT	
Plastic Viscosity cp @ °F	15	12	AND PREVENT AT 90-95°F, AND 40-45	
Yield Point (lb/100 ft²)	15	10	AND PREVENT SKIN FORM. MUDS AND PLAN	
Gel Strength (lb/100 ft²) 10 sec/10 min	10/20	7/12	PREVENT WATER LOSS.	
Filtrate API (cm³/30 min)	12	10	REMARKS	
API HTHP Filtrate (cm³/30 min) @ °F	-	-	CONTINUE RUNNING BACK TO BOTTOM FROM	
Cake Thickness (32nd in. API/HTHP)	2/32	2/32	2500 AND 4 CAS.	
Solids Content (% by Vol) (calculated) (retort)	4	5 1/2	CONTINUE DRILLING THROUGH PAROXY	
Liquid Content (% by Vol) Oil/Water	1.75	1.45	SOLIDS ARE IN MUD AND ARE	
Sand Content (% by Vol)	TRACE	TRACE	CLAY	
Methylene Blue Capacity (lb/bbl equiv) (cm³/cm³ mud)	-	-	AT 1700 RPM 7.5 MIN. 100% TAIL	
Strip Meter @ °F	9.5	10.0	HOLD WORK TIME FROM 1200 TO 1205	
Alkalinity Mud (P _m)	-	-	RIN BUT ADD HYDROLYSIS OF P _m 3	
Alkalinity Filtrate (P _f /M _f)	2.1-4.5	2.1-6	CHECK TO BE 30 CLAY AND 2000	
Chloride (mg/L)	2700	2200	CHECK AND CONTINUE DRILLING	
Total Hardness as Calcium (mg/L)	20	30	MUD SOME LOSS DURING	

PRODUCT INVENTORY	BARITE	KAOLIN	TRIP	CRUSH	GRG	CAL (MUD)	POLYMER	BICARB	SPANN	DI-CAL	LIME	SODA ASH	KCL	CALC	KAOLIN	BRG	PIPE	CLAY	SOLIDS EQUIPMENT
STARTING INVENTORY	400	52	40	122	50	76	18	22	10	24	25	-	40	9	1				SHAKER #1 P20, S60 mesh
RECEIVED																			SHAKER #2 B80, S60 mesh
USED LAST	-	32	5	-	5	11	-	-	1	-	-	-	-	-	-	-	-	-	MUD CLEANER mesh
CLOSING INVENTORY	400	20	35	122	45	65	18	22	9	24	22	-	40	9	1				CENTRIFUGE hours
POST INVENTORY	-	345	113	74	-	267	47	-	-	3705	-	-	-	-	-	-	-	-	DESANDER 7 1/2" 10-3 16 hours
USED (from IADC)																			DESILTER 10000 hours

M-I REPRESENTATIVE M. G. ... PHONE 050 72113 WAREHOUSE PHONE ... DAILY COST 2 1190.00 ✓ CUMULATIVE COST 2 6395.17 ✓

DRILLING MUD REPORT

M-I Drilling Fluids Co. OFFICE



DRILLING MUD REPORT NO. 7

DATE 2-4- 19 88 DEPTH 1475

SPUD DATE 2/3/88 PRESENT ACTIVITY DRILLING

P.O. BOX 42842 ■ HOUSTON, TEXAS 77242 USA

OPERATOR <u>BEACH PERFORM</u>	CONTRACTOR <u>GARRETT DRILLING</u>	RIG NO. <u>2</u>
REPORT FOR <u>H. WALKER</u>	REPORT FOR <u>G. NICOT</u>	SECTION, TOWNSHIP, RANGE <u>T11MB00</u>
WELL NAME AND NO. <u>CALUSA 111</u>	FIELD OR BLOCK NO. <u>F.P. 118</u>	COUNTY, PARISH OR OFFSHORE AREA <u>ORANGE BASIN</u>
		STATE/PROVINCE <u>VICTORIA</u>

DRILLING ASSEMBLY			CASING		MUD VOLUME (BBL)		CIRCULATION DATA		
BIT SIZE <u>8 1/2</u>	TYPE <u>T11</u>	JET SIZE <u>3x11</u>	SURFACE <u>9 5/8 in. @ 279'</u>	HOLE <u>330 bbl</u>	PITS <u>360 bbl</u>	PUMP SIZE <u>5 1/2 x 8, C x 2</u>		ANNULAR VEL (ft/min) DP <u>102</u> DC <u>157</u>	
DRILL PIPE SIZE <u>4 1/2</u>	TYPE <u>166/6</u>	LENGTH <u>166.4</u>	INTERMEDIATE <u>in. @ ft.</u>	TOTAL CIRCULATING VOLUME <u>690 bbl</u>		PUMP MAKE, MODEL <u>CD P28</u>		ASSUMED EFF. % <u>97</u>	
DRILL PIPE SIZE <u>4 1/2</u>	TYPE <u>114/8</u>	LENGTH <u>66.4</u>	INTERMEDIATE <u>in. @ ft.</u>	IN STORAGE <u>- 111</u>	WEIGHT <u>- 111</u>	bbl/stk <u>0.057/0.065</u>		sk/min <u>90/-</u>	
DRILL COLLAR SIZE <u>6 1/4 P.H.D.</u>		LENGTH <u>167.3</u>	PRODUCTION OR LINER <u>in. @ ft.</u>	MUD TYPE <u>1.0 GEL/PERFORM</u>		bbl/min <u>5.13</u>		gal/min <u>213</u>	
								BOTTOMS UP (min) (strk) <u>50</u>	
								TOTAL CIRC TIME (min) (strk) <u>135</u>	

MUD PROPERTIES				MUD PROPERTY SPECIFICATIONS		
Sample From	<input type="checkbox"/> FL. <input type="checkbox"/> PIT	<input type="checkbox"/> FL. <input type="checkbox"/> PIT	WEIGHT	VISCOSITY		FILTRATE
Time Sample Taken	<u>05:00</u>	<u>19:00</u>				
Downline Temperature (°F)		<u>350C</u>				
Depth (ft) (TVD)	<u>1</u> ft)	<u>1335</u>	<u>1475</u>	RECOMMENDED TREATMENT		
Weight <input checked="" type="checkbox"/> (ppg) <input type="checkbox"/> (lb/cu ft) <input type="checkbox"/> (sp gr)	<u>9.27</u>	<u>9.3</u>	<u>9.3</u>	CONTINUE TO GRADUALLY DECREASE		
Annular Viscosity (sec/qt) API @ °F	<u>44</u>	<u>45</u>	<u>45</u>	WATER LOSS BY ADDITION OF PREMIUM GEL, POLYMER, PAMIX.		
Plastic Viscosity cp @ °F	<u>14</u>	<u>14</u>	<u>14</u>	TRY TO DUMP SOME TANK ADDITIONAL GEL		
Gel Point (lb/100 ft²)	<u>13</u>	<u>13</u>	<u>13</u>	MAINTAIN REASONABLE HIGH DILUTION RATE TO		
Shear Strength (lb/100 ft²) 10 sec/10 min	<u>7121</u>	<u>7120</u>	<u>7120</u>	MAINTAIN 93 PPM MUD WT.		
Filtrate API (cm³/30 min)	<u>9.0</u>	<u>8.0</u>	<u>8.0</u>	REMARKS		
API HTHP Filtrate (cm³/30 min) @ °F	<u>-</u>	<u>-</u>	<u>-</u>	CONTINUE DRILLING INTO SLURRY		
Shake Thickness (32nd in. API/HTHP)	<u>2.132</u>	<u>2.132</u>	<u>2.132</u>	CHECK MUDSOUND - SATISFIED WITH VIB.		
Solids Content (% by Vol) <input checked="" type="checkbox"/> calculated <input type="checkbox"/> retort	<u>5</u>	<u>5 1/2</u>	<u>5 1/2</u>	STICKY SIDE ON SAMPLE AT 1342 AND		
Liquid Content (% by Vol) Oil/Water	<u>- 19%</u>	<u>- 19%</u>	<u>- 19%</u>	1372m LOOKING FOR NEW MUDSOUND. GRADUALLY		
Sand Content (% by Vol)	<u>TRAIL</u>	<u>TRAIL</u>	<u>TRAIL</u>	AT 1372m RUN WIPER TAP. 1475 TO WORK		
Methylene Blue Capacity <input type="checkbox"/> lb/bbl equiv <input type="checkbox"/> cm³/cm³ mud	<u>-</u>	<u>-</u>	<u>-</u>	TIGHTEN HOLE TO 112.1m TURN PULVERIZER		
Alkalinity (P _m)	<u>11.0</u>	<u>10.0</u>	<u>10.0</u>	TO 1067m BREAK RUNNING BACK IN. (1120)		
Alkalinity Filtrate (P _f /M _f)	<u>351.8</u>	<u>231.8</u>	<u>231.8</u>	KEY TO WASH OUT - WASH TAP 3 1/2 INCH		
Chloride (mg/L)	<u>1200</u>	<u>1600</u>	<u>1600</u>	CONTINUE DRILLING THROUGH SANDS		
Total Hardness as Calcium (mg/L)	<u>40</u>	<u>30</u>	<u>30</u>	1475 TO 1475m MUDSOUND. TRY TO 1475		
				SOUND CLAY WITH ONE SIDE ON 1475. CAUTION		
				DRILLING IN MUD GRAB 1475.		

PRODUCT INVENTORY	SOLIDS EQUIPMENT														
	FRANK	FRANK	FRANK	FRANK	FRANK	FRANK	FRANK	FRANK	FRANK	FRANK	FRANK	FRANK	FRANK	FRANK	FRANK
STARTING INVENTORY	20	20	120	45	65	120	22	1	21	25	-	40	9	1	
RECEIVED															
USED LAST	20	3	8	3	20	-	-	-	-	-	-	-	-	-	
ENDING INVENTORY	-	20	114	42	45	18	22	9	21	25	-	40	9	1	
COST	211	132	130	160	77	-	-	-	-	-	-	-	-	-	
USED FROM IADC															

M-I REPRESENTATIVE <u>MAN ...</u>	PHONE <u>737103</u>	WAREHOUSE PHONE	DAILY COST <u>91,350.04</u> ✓	CUMULATIVE COST <u>95,703.21</u> ✓
--------------------------------------	------------------------	-----------------	----------------------------------	---------------------------------------

DRILLING MUD REPORT

MAGCO DISTRICT OFFICE



DRILLING MUD REPORT NO. 8

DATE 3-4-19-88 DEPTH 1635

SPUD DATE 27/3/88 PRESENT ACTIVITY PIPE LOG TRIP

P.O. BOX 42842 ■ HOUSTON, TEXAS 77242 USA

PERATOR BROWN PERATOR CONTRACTOR GREENHILL DRILLING RIG NO. 2

REPORT FOR 11 WALKER REPORT FOR C. NICOT SECTION, TOWNSHIP, RANGE 10N09E

WELL NAME AND NO. CALCOSTON NO. 1 FIELD OR BLOCK NO. FF 108 COUNTY, PARISH OR OFFSHORE AREA OTWAL BASIN STATE/PROVINCE VICINIA

DRILLING ASSEMBLY			CASING		MUD VOLUME (BBL)		CIRCULATION DATA		
BIT SIZE	TYPE	JET SIZE	SURFACE	HOLE	PITS	PUMP SIZE	X IN.	ANNULAR VEL (ft/min)	
2 1/2"	JH	3x11	9 1/2 in. @ 277 ft.	370 bbl	430 bbl	5 1/2 x 2, 6 x 2		DP 107	DC 157
RILL PIPE SIZE	TYPE	LENGTH	INTERMEDIATE	TOTAL CIRCULATING VOLUME		PUMP MAKE, MODEL	ASSUMED EFF.	CIRCULATION PRESSURE (psi)	
4 1/2"	16.6/12		in. @ ft.	800 bbl		GO P28	97%	600	
RILL PIPE SIZE	TYPE	LENGTH	INTERMEDIATE	IN STORAGE	WEIGHT	bbl/stk	stk/min	BOTTOMS UP (min) (strk)	
2 1/2"	11.0/8	66.4	in. @ ft.			0.057/0.065	90/	55	
DRILL COLLAR SIZE	LENGTH	PRODUCTION OR LINER	MUD TYPE				bbl/min	gal/min	TOTAL CIRC TIME (min) (strk)
6 1/2" BHA	1673	in. @ ft.	F.W. GEL/FLUENT				5.13	2.5	155

MUD PROPERTIES				MUD PROPERTY SPECIFICATIONS		
Sample No.	FL. PIT	FL. PIT	WEIGHT	VISCOSITY	FILTRATE	
1	0530	1930				

RECOMMENDED TREATMENT			
Depth (ft) (TVD)	1	ft)	1635
Weight (ppg)	9.3	9.2	
Annular Viscosity (sec/qt) API @ °F	44	46	
Plastic Viscosity cp @ °F	16	18	
Yield Point (lb/100 ft²)	12	12	
Gel Strength (lb/100 ft²) 10 sec/10 min	5/18	5/20	
Filtrate API (cm³/30 min)	6.3	5.8	
API HTHP Filtrate (cm³/30 min) @ °F	-	-	
Shake Thickness (32nd in. API/HTHP)	1/32	1/32	
Solids Content (% by Vol) □ calculated □ retort	5 1/2	5	
Liquid Content (% by Vol) Oil/Water	14 1/2	19	
Sand Content (% by Vol)	Trace	Trace	
Methylene Blue Capacity (lb/bbl equiv / cm³/cm³ mud)	-	-	
H □ Strip □ Meter @ °F	9.5	9.4	
Alkalinity Mud (P _m)	-	-	
Alkalinity Filtrate (P _f /M _f)	31.8	31.8	
Chloride (mg/L)	1400	1200	
Total Hardness as Calcium (mg/L)	20	40	

REMARKS

CONTINUED DRILLING. PIPE LOG TRIP.

SAMPLE AT 1635. FOUND TO BE 1632.

RAW MUD TRIP - 100% TO SURFACE.

USED TO 1426. USED TO 1426. USED TO 1426.

USED TO 1369. USED TO 1369. USED TO 1369.

SUCCESS TO BOTTOM.

CONTINUED DRILLING TO 1635.

100% SOLIDS. SO. CAL. AND FOR PIPE.

CHANGE TRIP.

CHANGE LOG AT 1635. 6000

8.9" HOLE SIZE.

PRODUCT INVENTORY	SOLIDS EQUIPMENT														
	BHA	GR	CONCRETE	CRACK	FEEDING	BICARB	SODA	ASH	SILICA	DI. LIME	LIME	CLAY	RAVING	PIPE	CLAY
STARTING INVENTORY	400	114	32	42	45	18	25	21	9	29	40	9	1		
RECEIVED															
USED LAST	15	42	2	3	17	-	-	-	1	-	-	-	-		
CLOSING INVENTORY	385	73	30	39	28	18	25	22	8	29	40	9	1		
COST IN	100.5	30.45	45	160.75	65.25	-	-	-	37.05	-	-	-	-		
USED (from IADC)															

M-I REPRESENTATIVE ... PHONE ... WAREHOUSE PHONE ... DAILY COST \$1245.97 CUMULATIVE COST 17027.10

DRILLING MUD REPORT

M-I DISTRICT OFFICE



DRILLING MUD REPORT NO. 9

DATE 4/6/1981 DEPTH 1721m

SPUD DATE 27/3/80 PRESENT ACTIVITY Drilling

P.O. BOX 42842 ■ HOUSTON, TEXAS 77242 USA

OPERATOR BREXID PRYAGLUM CONTRACTOR GRANDWAY DRILLING RIG NO. 2

REPORT FOR H. WALKER REPORT FOR G. NICOT SECTION, TOWNSHIP, RANGE Tombow

WELL NAME AND NO. CHRISTA No 1 FIELD OR BLOCK NO. P.D.P. 108 COUNTY, PARISH OR OFFSHORE AREA OTOMI BASIN STATE/PROVINCE VICTORIA

DRILLING ASSEMBLY			CASING		MUD VOLUME (BBL)		CIRCULATION DATA		
BIT SIZE <u>2 1/2</u>	TYPE <u>35</u>	JET SIZE <u>3x11</u>	SURFACE <u>9 1/2 in. @ 279m</u>	HOLE <u>390 bbls</u>	PITS <u>430 bbls</u>	PUMP SIZE <u>5 1/2 x 8, 6 x 8</u>	X	IN.	ANNULAR VEL (ft/min) DP <u>102</u> DC <u>159</u>
DRILL PIPE SIZE <u>4 1/2</u>	TYPE <u>16-6 1/2</u>	LENGTH	INTERMEDIATE in. @ ft.	TOTAL CIRCULATING VOLUME <u>820 bbls</u>	PUMP MAKE, MODEL <u>CO P 28</u>	ASSUMED EFF <u>97 %</u>	CIRCULATION PRESSURE (psi) <u>650</u>		
DRILL PIPE SIZE <u>4 1/2</u>	TYPE <u>11-11/16</u>	LENGTH <u>66.4m</u>	INTERMEDIATE in. @ ft.	IN STORAGE	WEIGHT	bbl/stk <u>0.57/0.065</u>	stk/min <u>90/-</u>	BOTTOMS UP (min) (strk) <u>6.0</u>	
DRILL COLLAR SIZE <u>6 1/2</u>	LENGTH <u>167.3m</u>	PRODUCTION OR LINER in. @ ft.	MUD TYPE <u>F.W. Gtl/Polymer</u>	S-13 215 bbl/min gal/min		TOTAL CIRC TIME (min) (strk) <u>160</u>			

Sample From	MUD PROPERTIES		MUD PROPERTY SPECIFICATIONS		
	<input type="checkbox"/> F.L. <input type="checkbox"/> PIT	<input type="checkbox"/> F.L. <input type="checkbox"/> PIT	WEIGHT	VISCOSITY	FILTRATE
Time Sample Taken	<u>05.00</u>	<u>24.00</u>	RECOMMENDED TREATMENT		
Downline Temperature (°F)		<u>35°C</u>			
Depth (ft) (TVD <u>1</u> ft)	<u>1655m</u>	<u>1721m</u>	CONTINUE MUD MONITORING WITH		
Weight <input type="checkbox"/> (ppg) <input type="checkbox"/> (lb/cu ft) <input type="checkbox"/> (sp gr)	<u>93</u>	<u>93</u>			
Annular Viscosity (sec/qt) API @ °F	<u>4.6</u>	<u>4.8</u>	PREVENTION OF GELING / PREVENTION OF GELING		
Plastic Viscosity cp @ °F	<u>18</u>	<u>19</u>			
Yield Point (lb/100 ft²)	<u>14</u>	<u>16</u>	AT 6-7 sec, 100 cpm		
Shear Strength (lb/100 ft²) 10 sec/10 min	<u>6 / 20</u>	<u>5 / 18</u>			
Filtrate API (cm³/30 min)	<u>6.6</u>	<u>6.5</u>	REMARKS		
API HTHP Filtrate (cm³/30 min) @ °F	<u>-</u>	<u>-</u>			
Shake Thickness (32nd in. API/HTHP)	<u>1/32</u>	<u>1/32</u>	P.O. CHRISTA No 1 - 1721m		
Solids Content (% by Vol) <input type="checkbox"/> calculated <input type="checkbox"/> retort	<u>4.1%</u>	<u>5.1%</u>			
Liquid Content (% by Vol) Oil/Water	<u>- 17%</u>	<u>- 17%</u>	RUNNER 90' TO BOTTOM - THE MUD GOOD		
Sand Content (% by Vol)	<u>Trace</u>	<u>Trace</u>			
Methylene Blue Capacity ^{1 lb/bbl equiv} / _{1 cm³/cm³ mud}	<u>-</u>	<u>10</u>	CONCENTRATION OF SOLIDS IN THE MUD		
Strip <input type="checkbox"/> Meter @ °F	<u>9.5</u>	<u>9.5</u>			
Alkalinity Mud (P _m)	<u>-</u>	<u>-</u>	SOLIDS EQUIPMENT		
Alkalinity Filtrate (P _f /M _f)	<u>0.3/0.9</u>	<u>0.25/0.9</u>			
Chloride (mg/L)	<u>1200</u>	<u>1250</u>	SHAKER #1 <u>FX 1560</u> mesh		
Total Hardness as Calcium (mg/L)	<u>30</u>	<u>20</u>			

PRODUCT INVENTORY	MUD COMPONENTS														SOLIDS EQUIPMENT	
	FLUORIDE	CLAY	CEMENT	CEMENT	CEMENT	CEMENT	CEMENT	CEMENT	CEMENT	CEMENT	CEMENT	CEMENT	CEMENT	CEMENT		CEMENT
STARTING INVENTORY	300	93	30	39	28	18	25	22	8	29	0	9	1			SHAKER #1 <u>FX 1560</u> mesh
RECEIVED																SHAKER #2 <u>P 30</u> mesh
USED LAST	-	15	2	4	8	-	-	-	1	2	-	-	-			MUD CLEANER _____ mesh
CLOSING INVENTORY	300	80	28	35	20	18	25	22	7	27	0	9	1			CENTRIFUGE _____ hours
COST	-	2.32	1.65	2.10	2.10	-	-	-	3.00	9.5	-	-	-			DESANDER <u>3.11</u> hours
USED (from IADC)																DESILTER <u>3.11</u> hours

M-I REPRESENTATIVE _____ PHONE _____ WAREHOUSE PHONE _____ DAILY COST 4.20/100 CUMULATIVE COST 4.20/100

DRILLING MUD REPORT

LOCAL DISTRICT OFFICE

DRILLING MUD REPORT NO. 10

DATE 5/4/1988 DEPTH 1200

SPUD DATE 2/3/88 PRESENT ACTIVITY Logging



P.O. BOX 42842 ■ HOUSTON, TEXAS 77242 USA

OPERATOR BEACON PRODUCTION

REPORT FOR WALKER

WELL NAME AND NO. CALLISTO No. 1

CONTRACTOR GEORGE BROWN

REPORT FOR G. NICO

RIG NO. 2

SECTION, TOWNSHIP, RANGE TIMBONE

FIELD OR BLOCK NO. P.R.P. 108

COUNTY, PARISH OR OFFSHORE AREA OTWAI BASIN

STATE/PROVINCE

DRILLING ASSEMBLY			CASING		MUD VOLUME (BBL)		CIRCULATION DATA		
BIT SIZE	TYPE	JET SIZE	SURFACE	HOLE	PITS	PUMP SIZE	X IN.	ANNULAR VEL (ft/min)	
8 1/2	SIZE	3x11	9 1/2 in. @ 299 ft.	370 bbl.	400 bbl.	5 1/2 x 8	6 x 8	DP 102 DC 133	
DRILL PIPE SIZE	TYPE	LENGTH	INTERMEDIATE	TOTAL CIRCULATING VOLUME		PUMP MAKE, MODEL	ASSUMED EFF	CIRCULATION PRESSURE (psi)	
4 1/2	ILC 1b		in. @ ft.	790 bbl.		GD 828	97 %	650	
DRILL PIPE SIZE	TYPE	LENGTH	INTERMEDIATE	IN STORAGE	WEIGHT	bbl/stk	stk/min	BOTTOMS UP (min) (strk)	
6 1/2	ILC 1b		in. @ ft.	-	-	0.057/1000	90/1	60	
DRILL COLLAR SIZE	LENGTH	PRODUCTION OR LINER	MUD TYPE			bbl/min	gal/min	TOTAL CIRC TIME (min) (strk)	
6 1/2	500	in. @ ft.	F.W. GEL/POSSIBLE			513	200	150	

MUD PROPERTIES			MUD PROPERTY SPECIFICATIONS		
Sample From	<input type="checkbox"/> FL <input type="checkbox"/> PIT	<input type="checkbox"/> FL <input type="checkbox"/> PIT	WEIGHT	VISCOSITY	FILTRATE
Time Sample Taken	No Circ				
Flowline Temperature (°F)			RECOMMENDED TREATMENT		
Depth (ft) (TVD)	1 ft		OLIMPIC AND CALISTO SANDHAY		
Weight <input type="checkbox"/> (ppg) <input type="checkbox"/> (lb/cu ft) <input type="checkbox"/> (sp gr)	9.3		Mudlog Logging		
Annular Viscosity (sec/qt) API @ °F	4.2				
Plastic Viscosity cp @ °F	19				
Yield Point (lb/100 ft²)	16				
Shear Strength (lb/100 ft²) 10 sec/10 min	5.12				
Filtrate API (cm³/30 min)	6.5		REMARKS		
API HTHP Filtrate (cm³/30 min) @ °F	-		CONTINUED RUNNING TO 1200		
Cake Thickness (32nd in. API/HTHP)	2/32		RAN TO SHOWN WITH TOP OF TIGHT		
Solids Content (% by Vol) <input type="checkbox"/> calculated <input type="checkbox"/> retort	2%		MUD LOG LOGGING		
Liquid Content (% by Vol) Oil/Water	17%		MUD LOG LOGGING		
Sand Content (% by Vol)	Trace		MUD LOG LOGGING		
Methylene Blue Capacity <input type="checkbox"/> lb/bbl equiv <input type="checkbox"/> cm³/cm³ mud	1.0		MUD LOG LOGGING		
pH <input type="checkbox"/> Strip <input type="checkbox"/> Meter @ °F	9.0		MUD LOG LOGGING		
Alkalinity Mud (P _m)	-		MUD LOG LOGGING		
Alkalinity Filtrate (P _f /M _f)	22.17		MUD LOG LOGGING		
Chloride (mg/L)	2200		MUD LOG LOGGING		
Total Hardness as Calcium (mg/L)	200		MUD LOG LOGGING		

PRODUCT INVENTORY	SOLIDS EQUIPMENT																		
	SHAKER #1	SHAKER #2	MUD CLEANER	CENTRIFUGE	DESANDER	DESILTER													
TARTING INVENTORY	325	20	28	35	20	18	25	22	7	27	40	9	1						
RECEIVED																			
SED LAST 4 hr	17																		
CLOSING INVENTORY	342	20	28	35	20	18	25	22	7	27	40	9	1						
COST 1 hr	9																		
SED (from IADC)																			

MAINT REPRESENTATIVE	PHONE	WAREHOUSE PHONE	DAILY COST	CUMULATIVE COST
<u>MAINT</u>	<u>711 2700</u>	<u>711 2700</u>	<u>7 117 90</u>	<u>4 825 2500</u>

WELL SUMMARY

WELL HISTORY SHEET

MATERIALS INVENTORY

WELL HISTORY
WSP-004-C



DATE	MEAS. UREO. DEPTH (m)	TVD	MUD WT (kg/l)	V/S (°)	ANGLE (°)	FLOW RATE (lpm)	FLOW TEMP (°C)	GELS (PV)	PH	APD LOSS (lpm/100m)	HTAP LOSS (lpm/100m)	P ₁	M ₁	P _m	SALT OR CHLORIDE (lpm/100m)	F.W. GEL POLYMER (gpm)	MUD TYPE	CONDUCTOR	DEPTH (m)	MATERIALS	HOURS	DEBIT (m³/hr)	MUD COST
27.3	190	8.9	36	7	15	8/18	10.0	N.C.	-.15	.35	750	20	4	-	-	-	-	16"	5 m	PIPE LAX			
28.3	302	8.9	36	7	15	6/18	9.5	N.C.	-.1	.3	750	30	4	-	-	-	-	9 5/8"	299 m	CAL. CHL.	1	15	
29.3	308	8.5	30	2	3	1/3	11.0	N.C.	-.4	.5	8000	450	1	-	-	-	-	1800m	8 1/2"	D.I. CHL.	3	109	
30.3	737	8.8	35	215	31	4	20	12/12	9.5	N.C.	-.1	2	2	8000	400	3	-	12	10	CAUSTIC	5	2	
31.3	1001	9.1	45	215	31	15	16	8/15	9.5	N.C.	-.2	5	5	3000	30	5	-	12	10	BICARB	2	4	
1.4	1305	9.3	40	215	34	12	10	7/18	10.0	10	3	6	6	2200	30	5	-	15	20	CAUSTIC	4	3	
2.4	1495	9.3	45	215	35	14	13	7/20	10.0	10	3	8	8	1800	30	5	-	15	20	BANK THIK	5	2	
3.4	1655	9.2	46	215	18	12	5/20	9.5	5.8	-	3	8	8	1350	40	5	-	15	21	MAGCOBEL	2	3	
4.4	1781	9.3	48	215	35	19	16	5/18	9.5	6.5	-.25	.9	.9	1250	20	5	-	13	2	PIPE LAX	1	1	
5.4	1800	9.3	48	215	19	16	5/18	9.5	6.5	-.25	.9	.9	1250	20	5	-	13	2	CAUSTIC	4	2		
6.4	1800																	17		CAUSTIC	4	2	
Completed logging, plug and abandon well. Engineer released.																							



①

OPERATOR BEACH PETROLEUM

CONTRACTOR ~~GENERAL DRILLING~~

WELL CALISTA No. 1

DATE	PRODUCT	UNIT	27/5/88		28/3/88		29/3/88		30/3/88		31/3/88		1/4/88		2/4/88		TOTAL FOR WEEK		
			RECD	USED	RECD	USED	RECD	USED	RECD	USED	RECD	USED	RECD	USED	RECD	USED	RECD	USED	BAL
	MAGCOBAR	50kg			415	415			415	415					400	400	415	15	400
	MAGCOGEL	100lb			134	122			122	122					114	134	134	20	114
	SPERSENE	25kg			22	22			22	22					22	22	22	-	22
	XP 20																		
	RESINEX																		
	CAUSTIC SODA	25kg		5	44	44			44	44					35	32	49	17	32
	KWIK THIK	25kg		80	82	72			72	72					20	20	162	162	-
	BICARBONATE	40kg		23	23	23			23	18					18	23	5	18	
	SODIUM ASH	40kg		25	25	25			25	25					25	25	-	25	
	CALCIUM CHLORIDE	25kg		40	40	40			40	40					40	40	-	40	
	LIME	25kg		33	33	33			29	29					29	29	32	9	29
	POTASSIUM CHLORIDE	50kg		2	36	10			10	-					-	-	32	38	-
	CMC (BW)	25kg		61	61	61			61	61					42	42	61	19	42
	PELYSAL	25kg		81	81	81			81	81					45	45	81	36	45
	D.I. - CIDR	25L		11	11	11			11	11					9	9	11	2	9
	KWIK BLEN	5L		9	9	9			9	9					9	9	9	-	9
	PIPP LAX	20kg		1	1	1			1	1					1	1	1	-	1
	SODIUM SULFATE	50kg		1	1	1			1	1					1	1	1	-	1
	SPT	50kg		20	20	20			20	20					20	20	20	-	20
	SPT	25kg		15	15	15			15	15					15	15	15	-	15

TANRANNO 201

APPENDIX 4

Sidewall Core Descriptions

CALLISTA No.1
SIDEWALL CORE DESCRIPTIONS

<u>SWC</u>	<u>Depth</u> (m)	<u>Rec</u> (cm)	<u>Lithology</u>
1	1794	2.5	<u>SILTSTONE</u> , medium green grey, soft to firm, very dispersive, slightly calcareous, very argillaceous, trace carbonaceous detritus, no show.
2	1792	3.5	<u>SILTSTONE</u> , medium green grey, soft to firm, very dispersive, non calcareous, very common carbonaceous detritus, common very fine lithics, grades to very fine grained <u>SANDSTONE</u> , no show.
3	1788	3.2	<u>SILTSTONE</u> , medium to light grey, firm, dispersive, non calcareous, very argillaceous, common carbonaceous detritus, grades to very fine grained <u>SANDSTONE</u> , no show.
4	1737	3.0	<u>SANDSTONE</u> , lithic, light green grey, firm to friable, very fine to fine grained, subangular to subrounded, abundant argillaceous matrix, very calcareous, common creamy white feldspathic lithics, good trace carbonaceous detritus, very poor visual porosity, no show.
5	1734	3.0	<u>CLAYSTONE</u> , dark grey, soft, dispersive, non calcareous, very carbonaceous, silty, no show.
6	1731	3.0	<u>CLAYSTONE</u> , as above, no show.
7	1722	2.8	<u>SANDSTONE</u> , quartzose, patchy off-white to medium grey, friable, very fine to coarse grained, angular to subangular, poorly sorted quartz, abundant white and medium grey argillaceous matrix, non calcareous, trace black coally lithics, trace soft off-white lithics, poor visual porosity, no show.

- 8 1719.5 2.5 CLAYSTONE, dark grey, soft dispersive, non calcareous, very carbonaceous, silty, with fine grained quartz sand laminae, no show.
- 9 1715 4.0 CLAYSTONE, dark grey, firm, dispersive in part, micromicaceous, common carbonaceous laminae, silty in part, with interbedded SANDSTONE quartzose, light grey, light green grey, firm, friable in part, very fine grained, well sorted, subangular to subrounded, argillaceous matrix, non calcareous, trace lithics, poor visual porosity, no show.
- 10 1699.5 2.8 SANDSTONE, quartzose, off-white light grey, soft to firm, very friable, very fine to medium grained, dominantly fine, subangular to subrounded, moderate to well sorted quartz, abundant calcite cement, trace white argillaceous matrix, trace carbonaceous detritus, trace green lithics, fair to good visual porosity, no show.
- 11 1694 3.0 SILTSTONE, medium grey, medium grey brown, firm, dispersive in part, slightly calcareous, micromicaceous, trace fine quartz grains, no show.
- 12 1689 3.2 SILTSTONE, light grey, light brown grey, firm to moderately hard, calcareous in part, argillaceous in part, trace carbonaceous detritus, occasional green lithics, grades to very fine grained SANDSTONE, no show.
- 13 1681.5 2.7 SANDSTONE, quartzose, off white, light grey, friable, fine to medium grained, subangular to subrounded, moderate sorting, common grey white argillaceous matrix, weak calcite cement, common black carbonaceous detritus and laminae, fair visual porosity, no show.

- 14 1678 2.1 SANDSTONE, quartzose, light grey, light brown, friable, very fine to medium grained, dominantly fine grained, subangular, moderate to poorly sorted quartz, common grey white argillaceous matrix, slightly calcareous, abundant black carbonaceous laminae, fair to good visual porosity, no show.
- 15 1674 2.4 SANDSTONE, quartzose, light grey, light brown, soft, friable, very fine to medium grained, dominantly fine grained, subangular to subrounded, dominantly subangular, moderate to poorly sorted quartz, common grey white argillaceous matrix, slightly calcareous, trace carbonaceous detritus, fair visual porosity, no show.
- 16 1665 3.5 CLAYSTONE, medium to dark grey, firm, massive micromicaceous in part, silty in part, trace carbonaceous detritus, no show.
- 17 1616 3.0 SANDSTONE, lithic, dark green, black, very dark grey, loose, friable in part, medium to coarse grained, subrounded to rounded, poorly sorted, common ? carbonaceous matrix, dark grey, dispersive, argillaceous matrix in part, fair visual porosity, no show.
- 18 1605 3.2 CLAYSTONE, dark grey, firm, massive, dispersive, micromicaceous, very carbonaceous, non-calcareous, silty, no show.
- 19 1583 3.1 CLAYSTONE, as above, no show.

- 20 1370.5 2.3 SANDSTONE, quartzose, green, green olive grey, friable, medium to coarse quartz, subangular to subrounded, moderately sorted, clear, light brown, light green quartz grains, common patchy off white to medium green argillaceous and silty matrix, non-calcareous, common medium grained rounded ? chamositic pellets, fair to poor visual porosity, no show.
- 21 1153 1.8 SANDSTONE, quartzose, off white, friable, fine to very coarse grained, subangular to subrounded, poorly sorted, common white silty matrix, non-calcareous, friable, black coally lithics, fair to poor visual porosity, no show.
- 22 930 3.0 SANDSTONE, quartzose, medium brown, medium orange to brown, friable, subangular to subrounded, poorly to moderately sorted, clear, translucent and iron oxide stained quartz, moderate, very dispersive, silty, medium to dark brown, iron oxide rich matrix, non-calcareous, trace dark brown soft lithics, fair visual porosity, no show.
- 23 903 4.0 CLAYSTONE dark grey, dark grey brown, firm, dispersive, silty, micromicaceous, very carbonaceous, good trace fine quartz, very dark green rounded ? chamositic pellets, no show.

APPENDIX 5

Velocity Survey

WELL VELOCITY SURVEY

CALISTA NO. 1

PEP-104

VICTORIA

for

BEACH PETROLEUM N.L.

by

VELOCITY DATA PTY. LTD.

Brisbane, Australia

April 15, 1988.

CONTENTS

	Page
SUMMARY	1
GENERAL INFORMATION	1
EQUIPMENT	2
RECORDING	3
PROCESSING	
Elevation Data	3
Recorded Data	4
Correction for Instrument Delay and Shot Offset	4
Correction to Datum	4
Calibration of Sonic Log	
Method	5
Results	5
Trace Playouts	6

Figures

Figure 1	Well location map
Figure 2	Shot location sketch
Figure 3	Time-depth and velocity curves
Figure 4	Trace playouts

Tables

Table 1	Time-depth values
---------	-------------------

Enclosures

1.	Calculation Sheets
2.	Trace Display and First Arrival Plots

142°

143°

BALLARAT ●

VICTORIA

38°

● PORT FAIRY

● WARRNAMBOOL

CALISTA No.1

● COLAC

SOUTHERN
OCEAN

39°

CALISTA No.1
BEACH PETROLEUM N.L.
WELL LOCATION MAP

Scale 1:1000 000

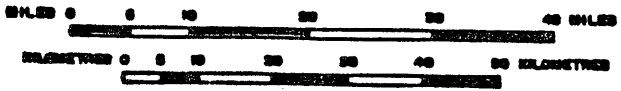
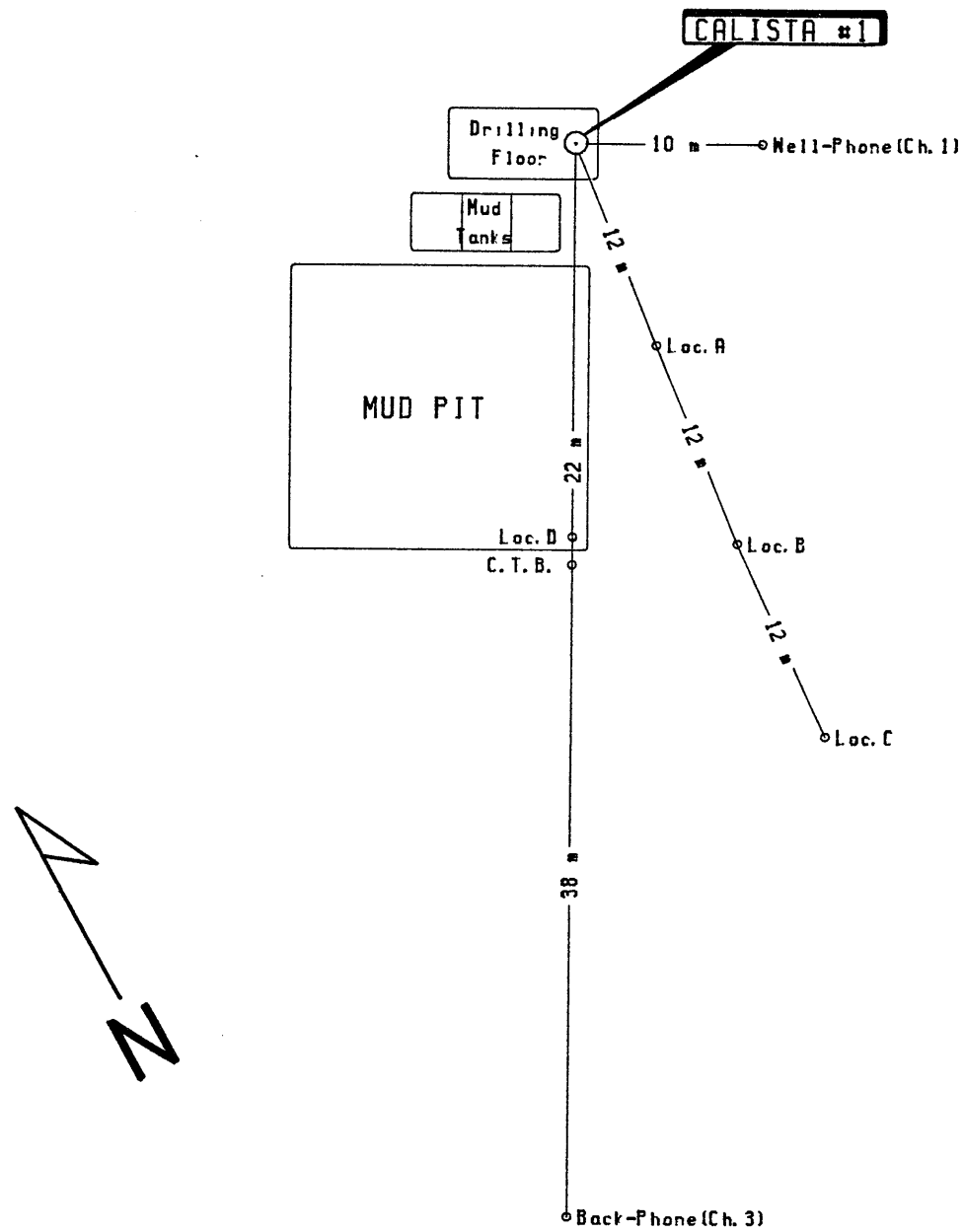


Figure 1



CALISTA #1

BEACH PETROLEUM N. L.
 SHOT POINT LOCATION SKETCH



Figure 2

SUMMARY

Velocity Data Pty. Ltd. conducted a velocity survey for Beach Petroleum N. L. in the Calista No.1 well, PEP-104 Victoria. The date of the survey was April 6, 1988.

The results of the survey, which are considered to be reliable, have been used to calibrate the sonic log.

Explosives were used as an energy source with shots being fired in the mud pit.

GENERAL INFORMATION

Name of Well	:	Calista No. 1
Location (Figure 1)	:	PEP-104 Victoria
Coordinates	:	Latitude 038 28' 00" Longitude 142 50' 13"
Date of Survey	:	April 6, 1988.
Wireline Logging	:	Gearhart
Weather	:	Fine
Operational Base	:	Brisbane
Operator	:	G. Young
Client Representative	:	B. Rayner

EQUIPMENT

Downhole Tool

Veldata Camlock 100 (90 mm)

Sensors:

6 HSI 4.5 Hz 215 ohm, high temperature (300 degrees F) detectors connected in series parallel. Frequency response 8-300 Hz within 3 dB.

Preamplifier:

48 dB fixed gain.
Frequency response 5-200 Hz within 3 dB.

Reference Geophone

Mark Products L1 4.5 Hz

Recording Instrument

VDLS 11/10 software controlled digital recording system utilising SIE OPA-10 floating point amplifiers for digital recording and SIE OPA-4 amplifiers for analog presentation. The system includes a DEC LSI-11 CPU, twin cassette tape unit and printer.

RECORDING

Energy Source : Explosive; AN-60
Shot Location : Mud pit
Charge Size : 0.5 to 2 (125 gm) sticks
Shot Depths : 0.9 to 1.5 metres
Shot Offsets : 12.0 to 36.0 metres
Recording Geometry : Figure 2

Shots were recorded on digital cassette tape and later transcribed to nine track tape (SEG-Y format) in Velocity Data's Brisbane centre. Printouts of the shots used are included with this report. (Enclosure 2)

The sample rate was 1 ms with 0.5 ms sampling over a 200 ms window encompassing the first arrivals. The scale of the graphic display varies with signal strength and is noted on each payout.

The times were picked from the printouts using the numerical value of the signal strength. (Enclosure 2)

PROCESSING**Elevation Data**

Elevation of KB : 81.9 metres above sea level
Elevation of Ground : 77.0 metres above sea level
Elevation of Seismic Datum : Sea Level
Depth Surveyed : 1797.7 metres below KB
Sonic Log Interval : 300.0 to 1798.0 metres below KB

PROCESSING**Recorded Data**

Number of Shots Used : 29
Number of Levels Recorded : 23
Data Quality : Good
Noise Level : Low
Rejected Shots : 2

Correction for Instrument Delay and Shot Offset

The 'corrected' times shown on the calculation sheet have been obtained via:

- (i) Subtraction of the instrument delay (4 ms) from the recorded arrival times
- (ii) geometric correction for non-verticality of ray paths resulting from shot offset.
- (iii) shot static correction to correct for the depth of shot below ground level at the well head using a correction velocity of 750 m/sec
- (iv) readdition of the instrument delay (4 ms).

The shot static correction velocity was determined from the surface geophone data.

Correction to Datum

The datum correction was determined directly by locking the tool at the datum and recording times from four different offsets. The datum correction used (45.6 msec) is the average of the corrected times for these shots.

PROCESSING**Calibration of Sonic Log - Method**

Sonic times were adjusted to checkshot times using a linear correction of the sonic transit times.

These differences arise as the sonic tool measures the local velocity characteristics of the formation with a high frequency signal, whereas the downhole geophone records the bulk velocity character using a signal of significantly lower frequency.

Calibration of Sonic Log - Results (Enclosure 1)

The discrepancies between shot and sonic interval velocities were generally small. The largest adjustment was 32.71 us/metre on the interval 1696.8 to 1797.7 metres below KB.

In aggregate, the shot and sonic interval times differed by -1.3 ms over the logged portion of the well.

PROCESSING

Trace Playouts (Figure 4)

Figure 4A is a plot of all traces used. No filter or gain recovery has been applied.

Figure 4B is a plot to scale in depth and time of selected traces. No filter or gain recovery has been applied.

Figure 4C is a plot to scale in depth and time of selected traces with a 5 Hz - 40 Hz filter and a gain recovery function of t^2 applied.

Figure 4D is a plot of selected surface traces. No filter or gain recovery has been applied.

Wayne Mogg
Geophysicist.

PE905709

This is an enclosure indicator page.
The enclosure PE905709 is enclosed within the
container PE902189 at this location in this
document.

The enclosure PE905709 has the following characteristics:

- ITEM_BARCODE = PE905709
- CONTAINER_BARCODE = PE902189
 - NAME = Velocity Data Table
 - BASIN = OTWAY
 - PERMIT = PEP/104
 - TYPE = WELL
 - SUBTYPE = VELOCITY_CHART
- DESCRIPTION = Velocity Data Table, Shot Calculations,
(from appendix 5 of WCR) for Calista-1
- REMARKS =
- DATE_CREATED = 6/04/88
- DATE_RECEIVED =
 - W_NO = W972
 - WELL_NAME = CALISTA-1
- CONTRACTOR = VELOCITY DATA PTY LTD
- CLIENT_OP_CO = BEACH PETROLEUM N.L.

(Inserted by DNRE - Vic Govt Mines Dept)

PE905710

This is an enclosure indicator page.
The enclosure PE905710 is enclosed within the
container PE902189 at this location in this
document.

The enclosure PE905710 has the following characteristics:

- ITEM_BARCODE = PE905710
- CONTAINER_BARCODE = PE902189
 - NAME = Velocity Data Table
 - BASIN = OTWAY
 - PERMIT = PEP/104
 - TYPE = WELL
 - SUBTYPE = VELOCITY_CHART
- DESCRIPTION = Velocity Data Table, Shot Calculations,
(from appendix 5 of WCR) for Calista-1
- REMARKS =
- DATE_CREATED = 6/04/88
- DATE_RECEIVED =
 - W_NO = W972
 - WELL_NAME = CALISTA-1
- CONTRACTOR = VELOCITY DATA PTY LTD
- CLIENT_OP_CO = BEACH PETROLEUM N.L.

(Inserted by DNRE - Vic Govt Mines Dept)

PE905711

This is an enclosure indicator page.
The enclosure PE905711 is enclosed within the
container PE902189 at this location in this
document.

The enclosure PE905711 has the following characteristics:

- ITEM_BARCODE = PE905711
- CONTAINER_BARCODE = PE902189
 - NAME = Velocity Data Table
 - BASIN = OTWAY
 - PERMIT = PEP/104
 - TYPE = WELL
 - SUBTYPE = VELOCITY_CHART
- DESCRIPTION = Velocity Data Table, Sonic Calibration
(from appendix 5 of WCR) for Calista-1
- REMARKS =
- DATE_CREATED = 6/04/88
- DATE_RECEIVED = .
 - W_NO = W972
 - WELL_NAME = CALISTA-1
 - CONTRACTOR = VELOCITY DATA PTY LTD
 - CLIENT_OP_CO = BEACH PETROLEUM N.L.

(Inserted by DNRE - Vic Govt Mines Dept)

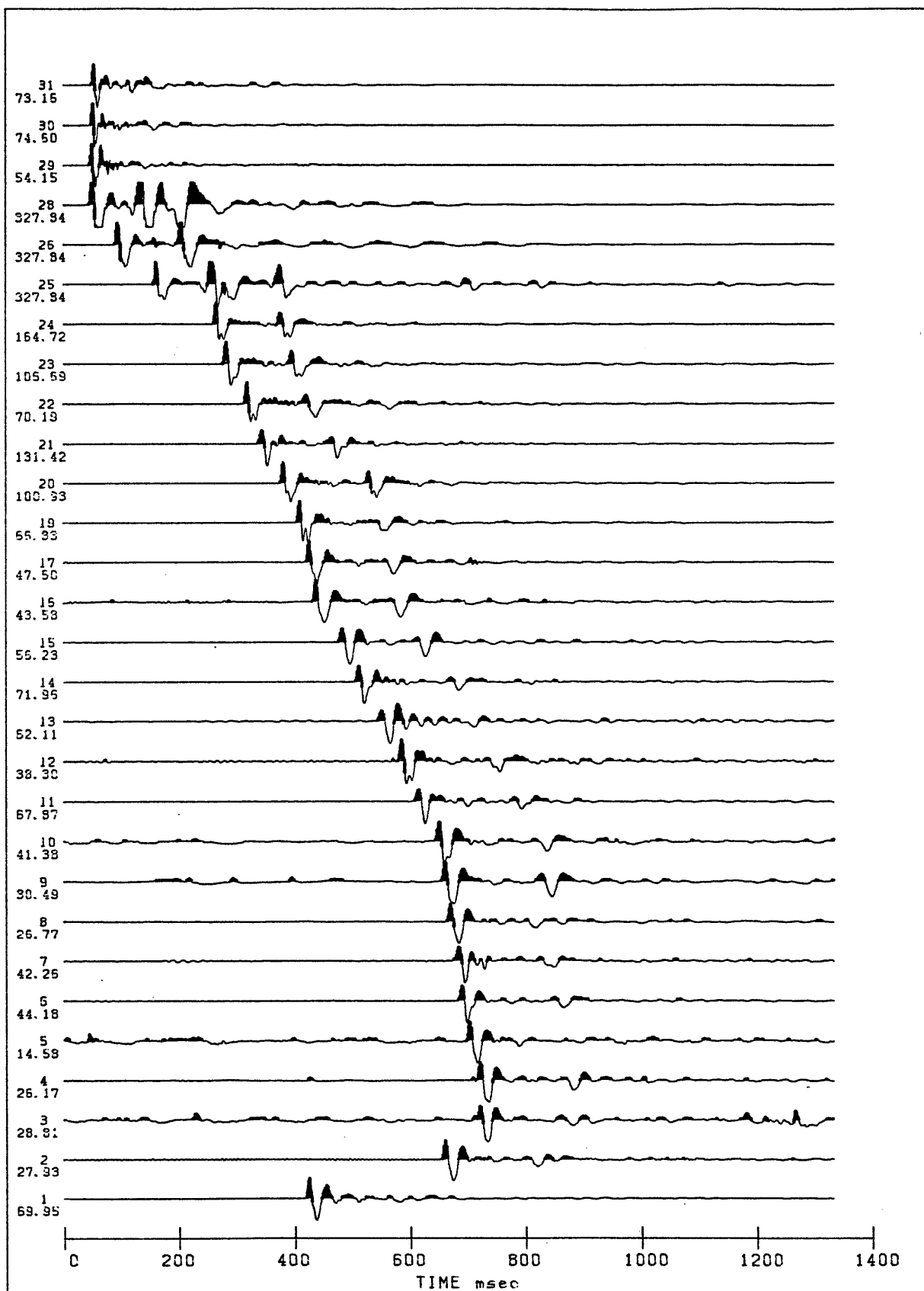
PE905712

This is an enclosure indicator page.
The enclosure PE905712 is enclosed within the
container PE902189 at this location in this
document.

The enclosure PE905712 has the following characteristics:

- ITEM_BARCODE = PE905712
- CONTAINER_BARCODE = PE902189
 - NAME = Velocity Data Table
 - BASIN = OTWAY
 - PERMIT = PEP/104
 - TYPE = WELL
 - SUBTYPE = VELOCITY_CHART
- DESCRIPTION = Velocity Data Table, Sonic drift, (from
appendix 5 of WCR) for Calista-1
- REMARKS =
- DATE_CREATED = 6/04/88
- DATE_RECEIVED =
 - W_NO = W972
 - WELL_NAME = CALISTA-1
 - CONTRACTOR = VELOCITY DATA PTY LTD
 - CLIENT_OP_CO = BEACH PETROLEUM N.L.

(Inserted by DNRE - Vic Govt Mines Dept)

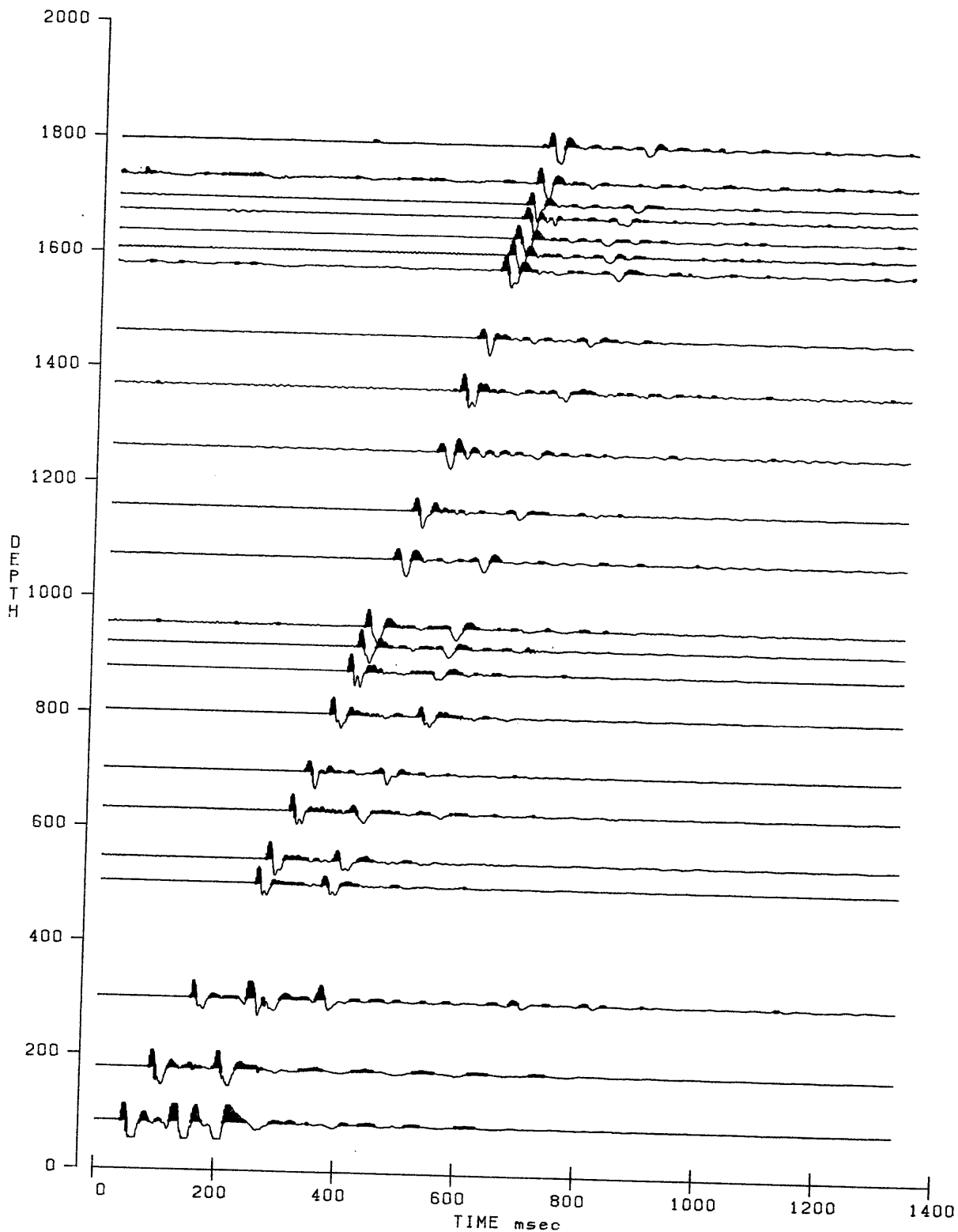


CALISTA #1

VELOCITY SURVEY TRACE DISPLAY
 Filter OUT-OUT
 No gain recovery



Figure 4A



CALISTA #1

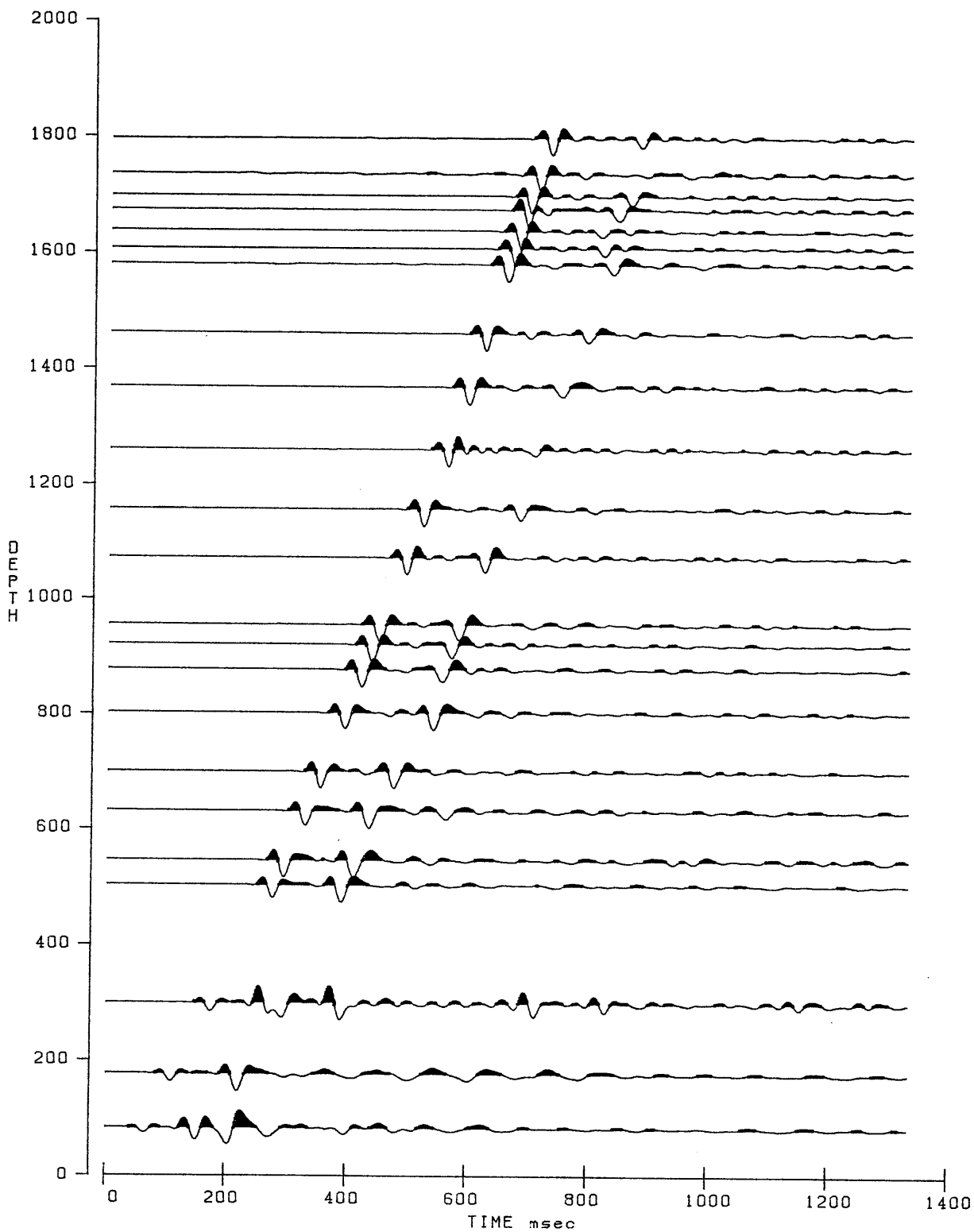
VELOCITY SURVEY TRACE DISPLAY

Filter OUT-OUT

No gain recovery



Figure 4B



CALISTA #1

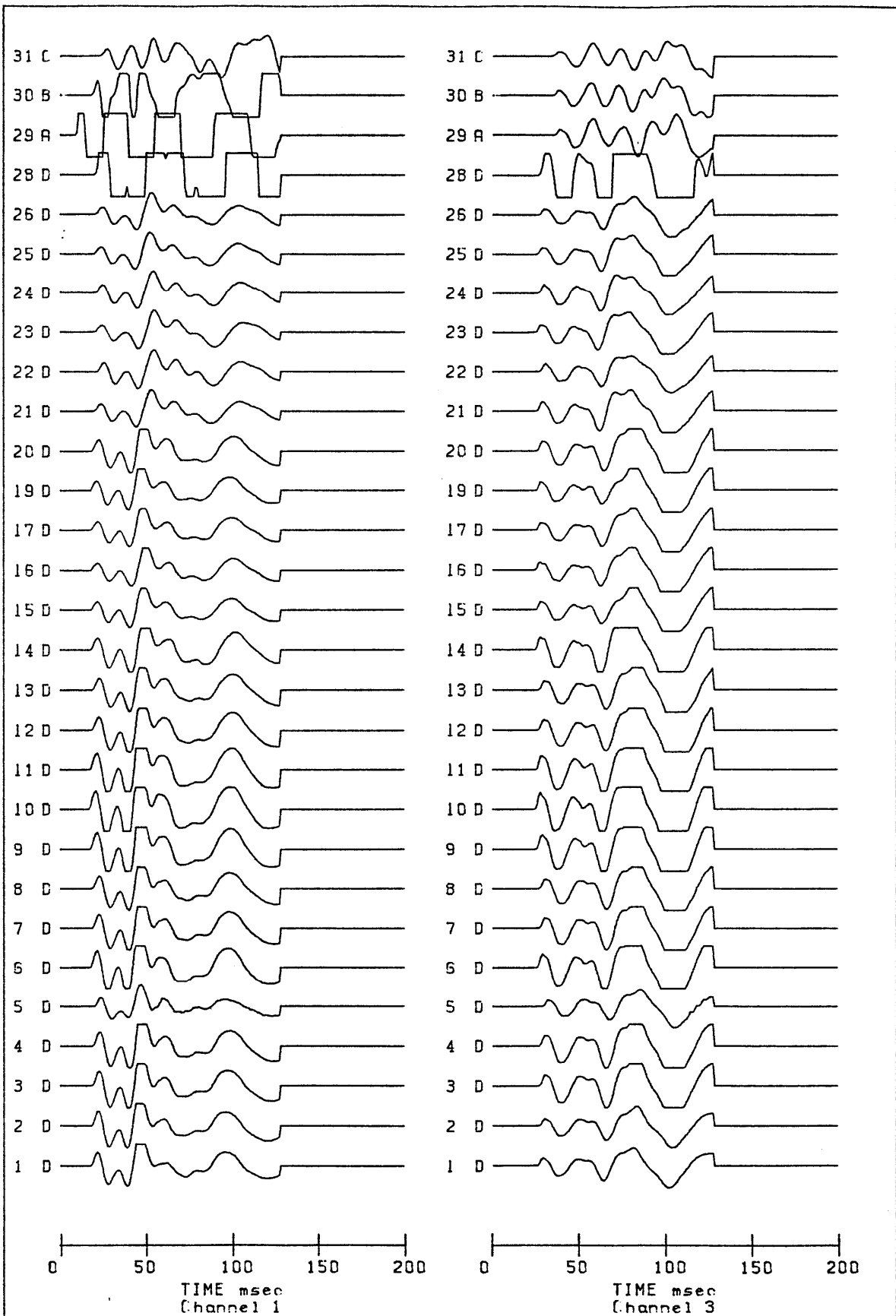
VELOCITY SURVEY TRACE DISPLAY

Filter 5-40

Gain $T^{2.0}$



Figure 4C



CALISTA #1

VELOCITY SURVEY TRACE DISPLAY
 Auxiliary channels
 Filter OUT-OUT



Figure 4D

TABLE 1. Time-Depth curve values

Well : CALISTA #1

Client : BEACH PETROLEUM N. L.

Survey units : METRES

Datum : 0.0

Calibrated sonic interval velocities used from 430.0 to 1715.0

Datum Depth	One-way time(ms)	-----VELOCITIES-----			Datum Depth	One-way time(ms)	-----VELOCITIES-----		
		Average	RMS	Interval			Average	RMS	Interval
5.0	2.4	2079	2079	2079	205.0	106.3	1929	1931	1856
10.0	4.8	2063	2063	2048	210.0	108.9	1928	1930	1863
15.0	7.3	2054	2054	2035	215.0	111.6	1927	1928	1881
20.0	9.8	2047	2048	2029	220.0	114.2	1926	1928	1919
25.0	12.2	2043	2043	2026	225.0	116.8	1927	1929	1955
30.0	14.7	2040	2040	2025	230.0	119.3	1928	1930	1972
35.0	17.2	2038	2038	2025	235.0	121.8	1929	1931	1979
40.0	19.6	2036	2036	2025	240.0	124.3	1930	1932	1982
45.0	22.1	2035	2035	2025	245.0	126.9	1931	1933	1984
50.0	24.6	2034	2034	2025	250.0	129.4	1932	1934	1984
55.0	27.1	2033	2033	2024	255.0	131.9	1933	1935	1985
60.0	29.5	2032	2032	2024	260.0	134.4	1934	1936	1985
65.0	32.0	2032	2032	2024	265.0	136.9	1935	1937	1985
70.0	34.5	2031	2031	2024	270.0	139.5	1936	1938	1985
75.0	36.9	2031	2031	2022	275.0	142.0	1937	1938	1985
80.0	39.4	2030	2030	2019	280.0	144.5	1938	1939	1985
85.0	41.9	2029	2029	2012	285.0	147.0	1938	1940	1985
90.0	44.4	2027	2027	1996	290.0	149.5	1939	1941	1985
95.0	47.0	2023	2023	1961	295.0	152.1	1940	1942	1985
100.0	49.6	2017	2017	1905	300.0	154.6	1941	1942	1985
105.0	52.2	2010	2010	1874	305.0	157.1	1941	1943	1985
110.0	54.9	2002	2003	1860	310.0	159.6	1942	1944	1985
115.0	57.6	1996	1996	1855	315.0	162.1	1943	1944	1985
120.0	60.3	1989	1990	1852	320.0	164.7	1943	1945	1985
125.0	63.0	1983	1984	1851	325.0	167.2	1944	1945	1985
130.0	65.7	1978	1979	1850	330.0	169.7	1945	1946	1985
135.0	68.4	1973	1974	1850	335.0	172.2	1945	1947	1985
140.0	71.1	1968	1970	1850	340.0	174.7	1946	1947	1985
145.0	73.8	1964	1965	1850	345.0	177.3	1946	1948	1985
150.0	76.5	1960	1961	1850	350.0	179.8	1947	1948	1985
155.0	79.2	1956	1958	1850	355.0	182.3	1947	1949	1985
160.0	81.9	1952	1954	1850	360.0	184.8	1948	1949	1985
165.0	84.6	1949	1951	1850	365.0	187.3	1948	1950	1985
170.0	87.4	1946	1948	1850	370.0	189.8	1949	1950	1985
175.0	90.1	1943	1945	1850	375.0	192.4	1949	1951	1985
180.0	92.8	1941	1942	1850	380.0	194.9	1950	1951	1985
185.0	95.5	1938	1940	1850	385.0	197.4	1950	1952	1985
190.0	98.2	1936	1937	1851	390.0	199.9	1951	1952	1986
195.0	100.9	1933	1935	1851	395.0	202.4	1951	1952	1987
200.0	103.6	1931	1933	1853	400.0	205.0	1952	1953	1989

TABLE 1.

Time-Depth curve values

Page 2.

Well : CALISTA #1
 Survey units : METRES

Client : BEACH PETROLEUM N. L.
 Datum : 0.0

Calibrated sonic interval velocities used from 430.0 to 1715.0

Datum Depth	One-way time(ms)	-----VELOCITIES-----			Datum Depth	One-way time(ms)	-----VELOCITIES-----		
		Average	RMS	Interval			Average	RMS	Interval
405.0	207.5	1952	1953	1995	605.0	287.4	2105	2124	2615
410.0	209.9	1953	1954	2009	610.0	289.1	2110	2130	2986
415.0	212.4	1954	1955	2042	615.0	291.0	2113	2134	2656
420.0	214.8	1956	1957	2121	620.0	292.9	2117	2137	2619
425.0	216.7	1962	1964	2613	625.0	295.0	2119	2139	2393
430.0	218.6	1967	1970	2618	630.0	297.0	2121	2141	2454
435.0	220.6	1972	1976	2510	635.0	299.0	2124	2145	2569
440.0	222.7	1976	1980	2371	640.0	301.2	2125	2146	2277
445.0	224.7	1980	1985	2446	645.0	303.2	2127	2148	2485
450.0	226.8	1985	1990	2458	650.0	305.3	2129	2150	2387
455.0	228.9	1988	1993	2378	655.0	307.1	2133	2154	2743
460.0	230.7	1994	2000	2694	660.0	309.2	2135	2155	2378
465.0	232.8	1997	2004	2397	665.0	311.3	2136	2157	2423
470.0	234.4	2005	2013	3080	670.0	313.0	2140	2162	2858
475.0	236.4	2009	2018	2503	675.0	315.1	2142	2163	2350
480.0	238.4	2013	2022	2476	680.0	317.5	2142	2163	2149
485.0	240.5	2017	2027	2487	685.0	319.4	2145	2166	2592
490.0	242.4	2021	2031	2524	690.0	321.5	2146	2167	2347
495.0	244.4	2025	2035	2480	695.0	323.5	2148	2169	2490
500.0	246.5	2029	2039	2481	700.0	325.5	2150	2171	2497
505.0	248.5	2032	2043	2463	705.0	327.5	2153	2174	2555
510.0	250.4	2037	2048	2660	710.0	328.8	2159	2183	3763
515.0	252.3	2041	2053	2536	715.0	330.5	2164	2188	3024
520.0	254.3	2045	2057	2557	720.0	331.6	2171	2200	4557
525.0	256.3	2048	2061	2464	725.0	333.5	2174	2202	2590
530.0	258.4	2051	2064	2473	730.0	335.5	2176	2204	2544
535.0	260.5	2054	2067	2352	735.0	337.4	2179	2207	2612
540.0	262.8	2054	2067	2116	740.0	339.3	2181	2209	2558
545.0	265.2	2055	2067	2089	745.0	341.4	2182	2211	2472
550.0	267.3	2057	2070	2384	750.0	343.7	2182	2210	2142
555.0	269.0	2063	2077	3006	755.0	345.6	2185	2213	2651
560.0	270.6	2069	2084	3050	760.0	347.5	2187	2215	2566
565.0	272.5	2074	2089	2739	765.0	349.3	2190	2219	2845
570.0	274.2	2079	2095	2855	770.0	351.1	2193	2221	2700
575.0	275.9	2084	2101	2885	775.0	353.1	2195	2224	2590
580.0	277.9	2087	2105	2581	780.0	355.1	2197	2225	2511
585.0	279.7	2091	2109	2685	785.0	356.9	2199	2228	2668
590.0	281.6	2095	2113	2668	790.0	358.8	2202	2230	2671
595.0	283.7	2098	2116	2439	795.0	360.8	2203	2232	2459
600.0	285.5	2101	2120	2690	800.0	362.8	2205	2234	2572

TABLE 1.

Time-Depth curve values

Page 3.

Well : CALISTA #1
Survey units : METRES

Client : BEACH PETROLEUM N. L.
Datum : 0.0

Calibrated sonic interval velocities used from 430.0 to 1715.0

Datum Depth	One-way time(ms)	-----VELOCITIES-----			Datum Depth	One-way time(ms)	-----VELOCITIES-----		
		Average	RMS	Interval			Average	RMS	Interval
805.0	364.6	2208	2237	2825	1005.0	438.0	2294	2326	2837
810.0	366.3	2211	2240	2886	1010.0	439.8	2296	2328	2818
815.0	368.1	2214	2244	2833	1015.0	441.6	2298	2330	2778
820.0	370.0	2216	2246	2579	1020.0	443.2	2301	2333	3040
825.0	371.9	2218	2248	2617	1025.0	445.0	2304	2336	2929
830.0	373.9	2220	2249	2554	1030.0	446.5	2307	2340	3285
835.0	375.8	2222	2251	2640	1035.0	448.2	2309	2342	2941
840.0	377.6	2225	2254	2754	1040.0	449.9	2312	2345	2897
845.0	379.2	2228	2258	2999	1045.0	451.5	2315	2348	3193
850.0	381.0	2231	2261	2876	1050.0	452.9	2318	2353	3491
855.0	382.6	2235	2265	3017	1055.0	454.7	2320	2354	2743
860.0	384.3	2238	2268	2926	1060.0	456.4	2322	2357	2953
865.0	386.1	2240	2271	2802	1065.0	458.2	2324	2359	2856
870.0	388.0	2242	2273	2643	1070.0	459.9	2326	2361	2835
875.0	389.8	2245	2276	2832	1075.0	461.7	2329	2363	2884
880.0	391.6	2247	2278	2722	1080.0	463.5	2330	2365	2741
885.0	393.4	2249	2281	2742	1085.0	465.3	2332	2366	2735
890.0	395.4	2251	2282	2499	1090.0	467.1	2333	2368	2755
895.0	397.4	2252	2283	2553	1095.0	469.0	2335	2369	2679
900.0	399.3	2254	2285	2600	1100.0	470.8	2337	2371	2827
905.0	401.1	2256	2287	2821	1105.0	472.7	2338	2372	2580
910.0	403.0	2258	2289	2568	1110.0	474.6	2339	2373	2589
915.0	405.0	2259	2290	2543	1115.0	476.6	2340	2374	2592
920.0	407.0	2261	2292	2579	1120.0	478.6	2340	2375	2506
925.0	408.9	2262	2293	2566	1125.0	480.4	2342	2376	2662
930.0	410.7	2264	2295	2788	1130.0	482.3	2343	2377	2681
935.0	412.6	2266	2297	2615	1135.0	484.2	2344	2378	2632
940.0	414.5	2268	2299	2603	1140.0	486.0	2346	2380	2788
945.0	416.4	2269	2300	2675	1145.0	487.9	2347	2381	2678
950.0	418.2	2272	2303	2845	1150.0	489.6	2349	2383	2875
955.0	420.1	2273	2304	2586	1155.0	491.5	2350	2384	2699
960.0	421.9	2275	2306	2698	1160.0	493.4	2351	2385	2622
965.0	423.8	2277	2308	2741	1165.0	495.2	2352	2386	2664
970.0	425.6	2279	2310	2676	1170.0	497.0	2354	2388	2854
975.0	427.3	2282	2313	2916	1175.0	498.7	2356	2390	2873
980.0	429.2	2283	2314	2694	1180.0	500.6	2357	2391	2663
985.0	431.0	2285	2316	2717	1185.0	502.4	2359	2393	2801
990.0	432.7	2288	2319	2949	1190.0	504.0	2361	2395	3074
995.0	434.5	2290	2322	2875	1195.0	505.7	2363	2397	2967
1000.0	436.3	2292	2324	2801	1200.0	507.4	2365	2399	2874

TABLE 1.

Time-Depth curve values

Page 4.

Well : CALISTA #1

Client : BEACH PETROLEUM N. L.

Survey units : METRES

Datum : 0.0

Calibrated sonic interval velocities used from 430.0 to 1715.0

Datum Depth	One-way time(ms)	-----VELOCITIES-----			Datum Depth	One-way time(ms)	-----VELOCITIES-----		
		Average	RMS	Interval			Average	RMS	Interval
1205.0	509.2	2366	2401	2831	1405.0	573.3	2451	2492	3335
1210.0	511.0	2368	2402	2765	1410.0	574.8	2453	2495	3310
1215.0	512.8	2369	2403	2797	1415.0	576.3	2455	2497	3347
1220.0	514.6	2371	2405	2855	1420.0	577.8	2458	2500	3385
1225.0	516.3	2373	2407	2927	1425.0	579.3	2460	2503	3423
1230.0	518.0	2375	2409	2911	1430.0	580.7	2462	2506	3464
1235.0	519.8	2376	2410	2774	1435.0	582.2	2465	2509	3468
1240.0	521.6	2377	2412	2745	1440.0	583.6	2467	2511	3427
1245.0	523.2	2379	2414	3083	1445.0	585.1	2470	2514	3460
1250.0	524.9	2381	2416	2956	1450.0	586.5	2472	2517	3482
1255.0	526.6	2383	2418	2982	1455.0	588.0	2475	2520	3449
1260.0	528.4	2385	2419	2842	1460.0	589.4	2477	2522	3416
1265.0	530.0	2387	2422	3117	1465.0	590.9	2479	2525	3334
1270.0	531.7	2389	2424	2918	1470.0	592.5	2481	2527	3195
1275.0	533.4	2390	2425	2894	1475.0	594.0	2483	2529	3250
1280.0	535.2	2392	2427	2849	1480.0	595.6	2485	2531	3174
1285.0	536.8	2394	2429	2968	1485.0	597.1	2487	2533	3434
1290.0	538.5	2396	2431	3045	1490.0	598.4	2490	2536	3587
1295.0	539.9	2399	2435	3617	1495.0	600.0	2492	2538	3161
1300.0	541.5	2401	2437	3073	1500.0	601.7	2493	2540	3063
1305.0	543.1	2403	2439	3152	1505.0	603.3	2494	2541	2966
1310.0	544.6	2405	2442	3204	1510.0	605.1	2496	2542	2915
1315.0	546.2	2408	2444	3243	1515.0	606.8	2497	2543	2957
1320.0	547.7	2410	2447	3234	1520.0	608.4	2498	2545	2960
1325.0	549.3	2412	2450	3263	1525.0	610.2	2499	2546	2862
1330.0	550.8	2415	2452	3228	1530.0	611.9	2501	2547	2963
1335.0	552.4	2417	2455	3228	1535.0	613.4	2502	2549	3283
1340.0	553.8	2419	2457	3347	1540.0	614.9	2504	2551	3237
1345.0	555.4	2422	2460	3247	1545.0	616.7	2505	2552	2898
1350.0	556.9	2424	2463	3332	1550.0	618.3	2507	2554	3157
1355.0	558.4	2427	2465	3328	1555.0	620.0	2508	2554	2783
1360.0	559.9	2429	2468	3354	1560.0	621.8	2509	2555	2844
1365.0	561.4	2431	2471	3333	1565.0	623.5	2510	2557	3038
1370.0	562.9	2434	2474	3362	1570.0	624.9	2512	2559	3356
1375.0	564.4	2436	2476	3346	1575.0	626.7	2513	2560	2851
1380.0	565.9	2438	2479	3199	1580.0	628.4	2514	2561	2928
1385.0	567.4	2441	2482	3385	1585.0	630.1	2515	2562	2945
1390.0	568.9	2443	2484	3355	1590.0	631.7	2517	2564	3160
1395.0	570.4	2446	2487	3374	1595.0	633.4	2518	2565	2996
1400.0	571.8	2448	2490	3425	1600.0	635.0	2520	2566	2978

TABLE 1.

Time-Depth curve values

Page 5.

Well : CALISTA #1
 Survey units : METRES

Client : BEACH PETROLEUM N. L.
 Datum : 0.0

Calibrated sonic interval velocities used from 430.0 to 1715.0

Datum Depth	One-way time(ms)	-----VELOCITIES-----			Datum Depth	One-way time(ms)	-----VELOCITIES-----		
		Average	RMS	Interval			Average	RMS	Interval
1605.0	636.7	2521	2567	2983	1660.0	655.1	2534	2580	3465
1610.0	638.4	2522	2568	2963	1665.0	656.7	2535	2582	3072
1615.0	640.1	2523	2569	2999	1670.0	658.2	2537	2584	3377
1620.0	641.9	2524	2570	2728	1675.0	659.8	2539	2585	3063
1625.0	643.4	2526	2572	3370	1680.0	661.5	2540	2586	2940
1630.0	645.1	2527	2573	2637	1685.0	663.2	2541	2587	3028
1635.0	646.8	2528	2574	3024	1690.0	664.8	2542	2588	3081
1640.0	648.5	2529	2575	2899	1695.0	666.4	2543	2590	3091
1645.0	650.3	2530	2576	2875	1700.0	668.1	2545	2591	3037
1650.0	652.0	2531	2577	2825	1705.0	669.7	2546	2592	3082
1655.0	653.7	2532	2578	3074	1710.0	671.4	2547	2593	2955

PE905713

This is an enclosure indicator page.
The enclosure PE905713 is enclosed within the
container PE902189 at this location in this
document.

The enclosure PE905713 has the following characteristics:

- ITEM_BARCODE = PE905713
- CONTAINER_BARCODE = PE902189
- NAME = One Way Time Graph
- BASIN = OTWAY
- PERMIT = PEP/104
- TYPE = WELL
- SUBTYPE = VELOCITY_CHART
- DESCRIPTION = One Way Time Graph (from appendix 5 of
WCR) for Calista-1
- REMARKS =
- DATE_CREATED = 5/04/88
- DATE_RECEIVED =
- W_NO = W972
- WELL_NAME = CALISTA-1
- CONTRACTOR = VELOCITY DATA PTY LTD
- CLIENT_OP_CO = BEACH PETROLEUM N.L.

(Inserted by DNRE - Vic Govt Mines Dept)

APPENDIX 6

Palynology

PALYNOLOGY OF BEACH CALLISTA-1,

OTWAY BASIN, VICTORIA

BY

ROGER MORGAN

FOR BEACH PETROLEUM

AUGUST, 1988.

PALYNOLOGY OF BEACH CALLISTA-1,

OTWAY BASIN, VICTORIA

BY

ROGER MORGAN

<u>CONTENTS</u>	<u>PAGE</u>
I SUMMARY	3
II INTRODUCTION	4
III PALYNOSTRATIGRAPHY	6
IV CONCLUSIONS	10
V REFERENCES	11

FIGURE 1. CRETACEOUS REGIONAL FRAMEWORK, OTWAY BASIN

FIGURE 2. MATURITY PROFILE, BEACH CALLISTA-1,

APPENDIX I PALYNOMORPH DISTRIBUTION DATA

I SUMMARY

930-40m (cuts) : L. balmei Zone : Paleocene : nearshore
marine : immature

940-70m (cutts) : T. longus Zone (M. druggii Dinoflagellate
Zone) : Maastrichtian : nearshore marine : immature

1665-1715m (swcs) : lower C. triplex Zone : Turonian :
nearshore to offshore marine : immature

1734m (swc) : A. distocarinatus Zone : Cenomanian :
nearshore marine : immature

1788m (swc) : Indeterminate : apparently non-marine and
therefore probably Eumeralla equivalent : marginally
mature

II INTRODUCTION

Andrew Buffin of Beach Petroleum submitted 5 swc samples and 4 cuttings samples from Callista-1 for palynological analysis for the completion report.

Palynomorph occurrence data are shown as Appendix I and form the basis for the assignment of the samples to four spore-pollen units of probably late Albian to Paleocene age. The Tertiary spore-pollen zonation is that of Stover and Evans (1973) and Stover and Partridge (1973) as modified by Partridge (1976) and shown on figure 1. The zones of Harris (1965) are not preferred as they only span part of the interval and are less widely used. The Cretaceous spore-pollen zonation is essentially that of Playford and Dettmann (1969), but has been significantly modified and improved by various authors since, and most recently discussed in Helby et. al. (1987), as shown on figure 1.

No formal dinoflagellate zonation has been published for the Tertiary of the Bass or Gippsland basins although Harris (1985) has recently published some zones for part of the Eocene of the Otway and St. Vincent Basins. Partridge (1976) published a table showing zone names in the Gippsland Basin but charts defining these zones were never published, although they are informally available. Cretaceous dinoflagellate zones are those of Helby, Morgan and Partridge (1987).

Maturity data was generated in the form of Spore Colour Index, and is plotted on figure 2 Maturity profile of Beach Callista-1. The oil and gas windows on figure 2 follow the general consensus of geochemical literature. The oil window corresponds to spore colours of light-mid brown (Staplin

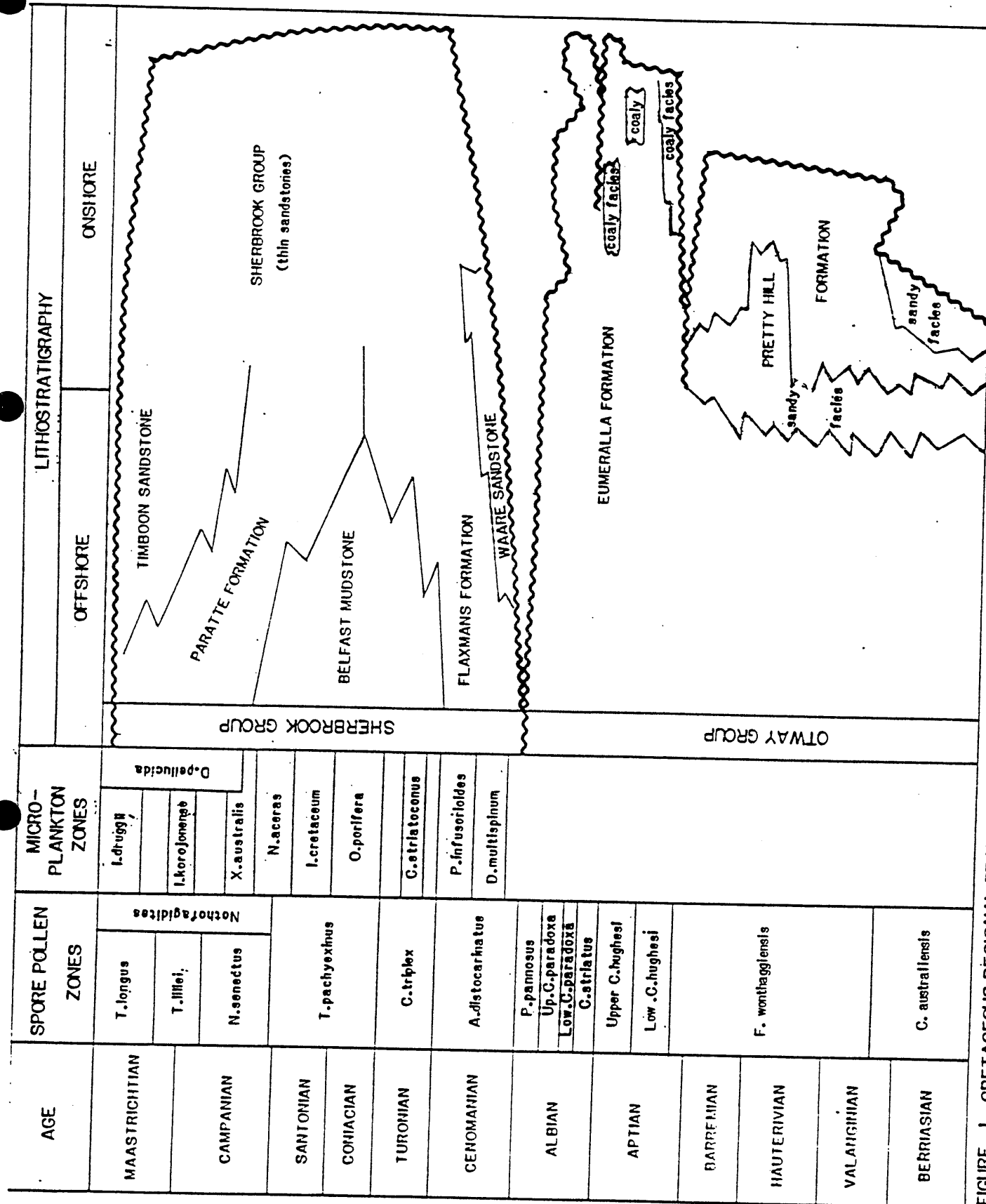


FIGURE 1. CRETACEOUS REGIONAL FRAMEWORK, OTWAY BASIN

Spore Colour Index 2.7) to dark brown (3.6). These correspond to vitrinite reflectance values of 0.6% to 1.3%. Geochemists, however, have not reached universal agreement on these values, and argue variations of kerogen type, basin type and even basin history. The maturity interpretation is therefore open to reinterpretation using the spore colours as basic data. However, the range in interpretation philosophies is not great, and probably would not move the oil window by more than 200 metres.

III PALYNOSTRATIGRAPHY

A. 930-40m (cutts) : L. balmei Zone

The presence of Gambierina rudata and Lygistepollenites balmei without older taxa, indicates assignment to the L. balmei Zone of Paleocene age. Proteacidites spp. are dominant, with frequent Cyathidites spp. Downhole caving is clearly present, with taxa such as Triporopollenites ambiguus and Nothofagidites falcatus seen. In view of these, the upper L. balmei indicators (Proteacidites grandis and P. incurvatus) may also be caved and so are disregarded.

Dinoflagellates are rare, but include Deflandrea speciosa, indicating a general Paleocene age.

The dominance of diverse spores and pollen, and scarcity of low diversity dinoflagellates, indicates very nearshore marine environments.

Colourless to yellow palynomorphs indicate immaturity for hydrocarbons.

B. 940-70m (cutts) : T. longus Zone

Assignment to the Tricolpites longus Zone is clearly indicated at the top by youngest T. longus, a downhole influx of Gambierina rudata, youngest Triporopollenites sectilis (950-60m) and Tricolporites lillei (960-70m), and confirmed by the dinoflagellates. At the base, oldest T. longus and Stereisporites punctatus indicate the zone, confirmed by the dinoflagellates. Proteacidites spp. are dominant, with frequent

Cyathidites spp. Minor Eocene caving was seen. In the cuttings sample at 940-50m, approximately equal proportions of Paleocene and Maastrichtian are seen. The unconformity therefore probably occurs in that interval.

Dinoflagellates are rare, but include Canninginopsis bretonica and Manumiella conorata, clearly indicating the M. druggii Dinoflagellate Zone, correlative with the upper T. longus Zone. Assemblages are of low diversity, but include taxa such as Alisocysta circumtabulata, Manumiella spp., Isabelidinium spp. and Areoligera senonensis.

Dominance of spores and pollen and scarcity of low diversity dinoflagellates, indicate nearshore marine environments. These assemblages can also be distinguished from the Paleocene above by high inertinite content.

Yellow spore colours indicate immaturity for hydrocarbon generation.

The T. lillei to upper C. triplex Zones are probably present but unsampled in this interval.

C. 1665m (swc)-1715m (swc) : lower C. triplex Zone

Assignment to the lower half of the Clavifera triplex Zone (=P. mawsonii Zone) is indicated at the top by youngest Appendicisporites distocarinatus and at the base by oldest Phyllocladidites mawsonii. Oldest P. eunuchus (1715m) and Clavifera triplex (1689m) confirm the assignment, as do the dinoflagellates. Common taxa

include Cyathidites spp., Falcisporites spp., and Microcachryidites antarcticus. Minor Triassic reworking was seen at 1689m only.

Dinoflagellates are fairly frequent and include consistent Cribooperidinium edwardsii up to 1689m. This event normally occurs within the lower C. triplex Zone, equivalent to a point near the top of the P. infusorioides Dinoflagellate Zone.

Dominant and diverse spores and pollen occur, with increasing dinoflagellate content upwards (2% at 1715m, 25% at 1689m, 50% at 1665m) reflecting transgression. Environments therefore range from very nearshore at the base to offshore at the top.

Yellow to yellow/brown spore colours indicate immaturity for hydrocarbons.

D. 1734m (swc) : A. distocarinatus Zone

Assignment to the Appendicisporites distocarinatus Zone is indicated by the presence of A. distocarinatus (and A. tricornitatus) without younger or older indicators. A downhole influx of Foraminisporis spp. (F. asymmetricus, F. dailyi and F. wonthaggiensis) is consistent with assignment. Cyathidites spp. are frequent.

Dinoflagellates are of low diversity and generally longranging, but do include Xenascus asperatus. This is consistent with the X. asperatus to P. infusorioides Zones. Circulodinium deflandrei is easily the most common species.

Nearshore marine environments are indicated by the dinoflagellate content (25%) and their low diversity (10 species), amongst the dominant and diverse spores and pollen.

Yellow to yellow/brown spore colours indicate immaturity for hydrocarbon generation.

E. 1788m (swc) : Indeterminate

An extremely sparse palynomorph assemblage was seen, comprising entirely longranging spores and pollen. the probably non-marine environments therefore suggest the non-marine Eumeralla Formation, and so an Early Cretaceous age. The fossils seen are insufficient to definitively confirm this deduction. Rare Botryococcus suggests some freshwater influence.

Yellow/brown spore colours indicate marginal maturity for oil generation, and immaturity for gas/condensate.

IV CONCLUSIONS

- A. Palynology suggests two unconformities. The terminal Cretaceous hiatus probably occurs in the interval 940-50m. The middle Cretaceous hiatus may occur in the gap 1734-1788m.

- B. The lower C. triplex interval shows a normal environmental pattern of transgression in time. The top common C. edwardsii may be useful for detailed correlation within this interval.

- C. The unpublished dinoflagellate C. bretonica is seen here for the second time in the Otway Basin. It may be that close sampling near the top of the Cretaceous will show that it is widely distributed. So far it is always associated with the M. druggii Dinoflagellate Zone throughout Australia, and is an excellent marker for the Late Maastrichtian.

V. REFERENCES

Harris, W.K. (1965) Basal Tertiary microfloras from the Princetown area, Victoria, Australia Palaeontographica B, 115, 75-106

Harris, W.K. (1985) Middle to Late Eocene Depositional Cycles and Dinoflagellate Zones in Southern Australia Spec. Publ., S. Aust. Dept. Mines and Energy 5 : 133-144

Helby, R.J., Morgan, R.P., and Partridge, A.D., (1987) A palynological Zonation of the Australian Mesozoic Australas. Assoc. Palaeont. Mem. 4

Partridge, A.D. (1976) The Geological Expression of eustacy in the Early Tertiary of the Gippsland Basin Aust. Pet. Explor. Assoc. J., 16 : 73-79








Stover L.E. and Evans, P.R. (1973) Upper Cretaceous - Eocene Spore Pollen Zonation, offshore Gippsland Basin, Australia Spec. Publ. Geol. Soc. Aust., 4 : 55-72

Stover, L.E. and Partridge, A.D. (1973) Tertiary and Late Cretaceous Spores and Pollen from the Gippsland Basin, South-eastern Australia Proc. R. Soc. Vict., 86 : 237-286/

CALLISTA - 1 PALYNOLOGICAL DATA (composite)

RANGE CHART OF GRAPHIC ABUNDANCES BY LOWEST APPEARANCE (By Group)

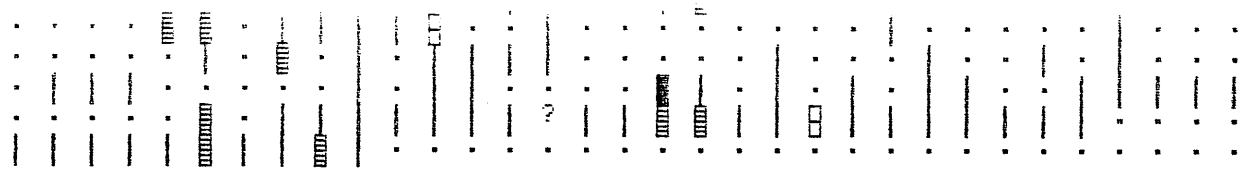
Key to Symbols

-  = Very Rare
-  = Rare
-  = Few
-  = Common
-  = Abundant
-  = Questionably Present
-  = Not Present

1	ANNULISPORITES
2	CALLIALASPORITES DAMPIERI
3	CERATOSPORITES EQUALIS
4	COROLLINA TOROSUS
5	CYATHIDITES SP.
6	FALCISPORITES SIMILIS
7	GLEICHINIDITES CIRCINIDITES
8	MICROCACHRYDITES ANTARCTICUS
9	OSMUNDACIDITES WELLMANII
10	RETITRILETES AUSTRICLAVATIDITES
11	AEQUITRIRADITES TILCHAENSIS
12	APPENDICISPORITES DISTOCARINATUS
13	APPENDICISPORITES TRICORNITATUS
14	CICATRICOSISPORITES AUSTRALIENSIS
15	CLAVIFERA TRIPLEX
16	CONTIGNISPORITES COOKSONIAE
17	COPTOSPORA SP. A
18	CYATHIDITES AUSTRALIS
19	CYATHIDITES MINOR
20	DENSOISPORITES VELATUS
21	DICTYOTOSPORITES SPECIOSUS
22	FORAMINISPORIS ASYMMETRICUS
23	FORAMINISPORIS DAILYI
24	FORAMINISPORIS WONTHAGGIENSIS
25	GLEICHENIIDITES
26	ISCHYOSPORITES PUNCTATUS
27	KLUKISPORITES SCABERIS
28	LYCOPODIACIDITES ASPERATUS
29	TRIPOROLETES RETICULATUS
30	AMOSOPOLLIS CRUCIFORMIS
31	CICATRICOSISPORITES LUDBROOKIAE
32	CYCAOOPITES FOLLICULARIS
33	LEPTOLEPIDITES VERRUCATUS

930-40 cutts

1665 S.W.C.
1689 S.W.C.
1715 S.W.C.
1734 S.W.C.
1788 S.W.C.



0930-40 cutts
 0940-50 cutts
 0950-60 cutts
 0960-70 cutts
 1665 S.W.C.
 168 S.W.C.
 1715 S.W.C.
 1734 S.W.C.
 1788 S.W.C.

34	LYGISTEPOLLENITES FLORINII
35	PEROTRILETES MORGANII/JUBATUS
36	PHYLLOCLADIDITES EUNUCHUS
37	PHYLLOCLADIDITES MAWSONII
38	SESTROSPORITES PSUEDOALVEOLATUS
39	STERIESPORITES ANTIQUASPORITES
40	AUSTRALOPOLLIS OBSCURUS
41	BALMEISPORITES HOLOICTYUS
42	CYCLOSPORITES HUGHESI
43	TRILOBOSPORITES TRIRETICULOSUS
44	CAMEROZONOSPORITES BULLATUS
45	PHIMOPOLLENITES PANNOSUS
46	CINGUTRILETES CLAVUS
47	CUPANEIDITES ORTHOTEICHUS
48	GAMBIERINA RUDATA
49	HALORAGACIDITES HARRISII
50	LATROBOSPORITES OHAIENSIS
51	LYGISTEPOLLENITES BALMEI
52	MALVACIPOLLITES SUBTILIS
53	NOTHOFAGIDITES EMARCIDUS
54	NOTHOFAGIDITES ENDURUS
55	PERIPOROPOLLENITES POLYORATUS
56	PROTEACIIDITES SPP.
57	SPINOZONOCOLPITES PROMINATUS
58	STERIESPORITES PUNCTATUS
59	TRICOLPITES LONGUS
60	TRICOLPORITES LILLIEI
61	BEAUPREADITES ELEGANSIFORMIS
62	CAMEROZONOSPORITES OHAIENSIS
63	DACRYCARPIDITES AUSTRALIENSIS
64	GAMBIERINA EDWARDSII
65	HERKOSPORITES ELLIOTTII
66	NOTHOFAGIDITES FALCATUS

BRASSUS
ALISADUS ss
FESSUS
ES SECTILIS
FLEMINGII
PANDIS
NCURVATUS
DAMARUENSIS
LILIPSII
S VERRUCOSUS
DIENANTHOIDES
RESOLABRUS
LII
ES AMBIGUUS
TIUM ASYMMETRICUM
EFLANDREI
IUM PHRAGMITES
IUM HETERACANTHUM
IUM COMPLEX
IUM PULCHERRIMUM
IUM PULCHRUM/RAMOSUS
IUM
IUM HUGUONIOTTI
IUM EDWARDSII
MEMBRANIPHORUM
IUM PULCHRUM
IUM PEPULATA
IUM
IUM
IUM CONJUNCTUM
IUM
IUM SP.

SPECIES LOCATION INDEX

Index numbers are the columns in which species appear.

INDEX NUMBER	SPECIES
11	AQUITRIRADITES TILCHAENSIS
105	ALISOCYSTA CIRCUMTABULATA
10	ALISOCYSTA MARGARITA
100	ALTERBIA ACUTULA
30	AMOSOPOLLIS CRUCIFORMIS
1	ANNULISPORITES
12	APPENDICISPORITES DISTOCARINATUS
17	APPENDICISPORITES DISTOCARINATUS

39 ABOULINIA PARVA
 40 AUSTRALOPOLLIS OBSCURUS
 96 BACCHIDIUM POLYPES
 41 BALMEISPORITES HOLODICTYUS
 61 BEAUPREADITES ELEGANSIFORMIS
 117 BOTRYOCOCCUS
 8 CALLAOSPHAERIDIUM ASYMMETRICUM
 2 CALLIALASPORITES DAMPIERI
 44 CAMEROZONOSPORITES BULLATUS
 62 CAMEROZONOSPORITES OHAIENSIS
 101 CANNINGINOPSIS BRETONICA
 3 CERATOSPORITES EQUALIS
 14 CICATRICOSISPORITES AUSTRALIENSIS
 31 CICATRICOSISPORITES LUDBROOKIAE
 46 CINGUTRILETES CLAVUS
 102 CIRCULODINIUM ATTADALICUM
 82 CIRCULODINIUM DEFLANDREI
 15 CLAVIFERA TRIPLEX
 90 CLEISTOSPHAERIDIUM HUGUONIOTI
 99 CLEISTOSPHAERIDIUM SP.
 16 CONTIGNISPORITES COOKSONIAE
 17 COPTOSPORA SP.A
 4 COROLLINA TOROSUS
 91 CRIBROPERIDINIUM EDWARDSII
 47 CUPANEIDITES ORTHOTEICHUS
 18 CYATHIDITES AUSTRALIS
 19 CYATHIDITES MINOR
 5 CYATHIDITES SP.
 32 CYCADOPIITES FOLLICULARIS
 92 CYCLONEPHELIUM MEMBRANIPHORUM
 42 CYCLOSPORITES HUGHESI
 63 DACRYCARPIDITES AUSTRALIENSIS
 110 DEFLANDREA HETEROPHLYCTA
 111 DEFLANDREA SPECIOSA
 20 DENSOSPORITES VELATUS
 21 DICTYOTOSPORITES SPECIOSUS
 83 EXOCHOSPHAERIDIUM PHRAGMITES
 6 FALCISPORITES SIMILIS
 22 FORAMINISPORIS ASYMMETRICUS
 23 FORAMINISPORIS DAILYI
 24 FORAMINISPORIS WONTHAGGIENSIS
 64 GAMBIERINA EDWARDSII
 48 GAMBIERINA RUDATA
 2 GLEICHENIIDITES
 7 GLEICHINIDITES CIRCINIDITES
 49 HALORAGACIDITES HARRISII
 65 HERKOSPORITES ELLIOTTII
 97 HETEROSPHAERIDIUM CONJUNCTUM
 84 HETEROSPHAERIDIUM HETERACANTHUM
 93 HYSTRICHODINIUM PULCHRUM
 108 ISABELDINIUM KOROJONENSE
 112 ISABELIDINIUM PELLUCUDUM
 26 ISCHYOSPORITES PUNCTATUS
 27 KLUKISPORITES SCABERIS
 50 LATROBOSPORITES OHAIENSIS
 33 LEPTOLEPIDITES VERRUCATUS
 28 LYCOPODIACIDITES ASPERATUS
 51 LYGISTEPOLLENITES BALMEI
 34 LYGISTEPOLLENITES FLORINII
 52 MALVACIPOLLITES SUBTILIS
 103 MANUMIELLA CORONATA
 104 MANUMIELLA DRUGGII
 MICROCACHRYDITES ANTARCTICUS
 98 MICRODINIUM ORNATUM
 53 NOTHOFAGIDITES EMARCIDUS
 54 NOTHOFAGIDITES ENDURUS
 66 NOTHOFAGIDITES FALCATUS

86 UCISUSPHERIDIUM FULCERRIMUM
113 OPERCULODINIUM CENTROCARPUM
9 OSMUNDACIDITES WELLMANII
109 PALAEOPERIDIUM PYROPHORUM
118 PARALECANIELLA INDENTATA
57 PERIPOROPOLLENITES POLYORATUS
30 PEROTRILETES MORGANII/JUBATUS
45 PHIMOPOLLENITES PANNOSUS
36 PHYLLOCLADIDITES EUNUCHUS
37 PHYLLOCLADIDITES MAWSONII
76 PHYLLOCLADIDITES VERRUCOSUS
77 PROTEACIDITES ADENANTHOIDES
67 PROTEACIDITES CRASSUS
72 PROTEACIDITES GRANDIS
73 PROTEACIDITES INCURVATUS
78 PROTEACIDITES OBESOLABRUS
68 PROTEACIDITES PALISADUS ss
56 PROTEACIDITES SPP.
10 RETITRILETES AUSTRICLAVATIDITES
117 SCHIZOSPORIS RETICULATA
38 SESTROSPORITES PSUEDOALVEOLATUS
115 SPINIDIINIUM SP.
87 SPINIFERITES FURCATUM/RAMOSUS
57 SPINOZONOCOLPITES PROMINATUS
30 STERIESPORITES ANTIQUASPORITES
58 STERIESPORITES PUNCTATUS
74 TETRACOLPORITES OAMARUENSIS
88 TRICHODINIUM
69 TRICOLPITES CONFESSUS
79 TRICOLPITES GILLII
59 TRICOLPITES LONGUS
75 TRICOLPITES PHILLIPSII
60 TRICOLPORITES LILLIEI
43 TRILOBOSPORITES TRIORETICULOSUS
29 TRIPOROLETES RETICULATUS
80 TRIPOROPOLLENITES AMBIGUUS
70 TRIPOROPOLLENITES SECTILIS
89 XENASCUS ASPERATUS

APPENDIX 7

X-Ray Diffraction Analysis

technology and enterprise

Amdel Limited
(Incorporated in S.A.)
31 Flemington Street,
Frewville, S.A. 5063

P.O. Box 114,
Eastwood, S.A. 5063

Telex: AA82520
Facsimile: (08) 79 6623

21 July 1988

Telephone: (08) 372 2700

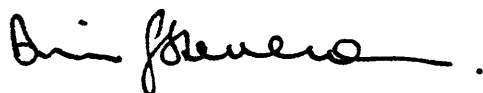
Beach Petroleum NL
Box 7096 GPO
SYDNEY NSW 2001

Attention: Mr A. Buffin

REPORT F 7266 - Part 2 (Final)

YOUR REFERENCE: Letter of 17 June 1988
SAMPLE IDENTIFICATION: 1-8
MATERIAL: SWC
LOCALITY: CALLISTA-1
WORK REQUIRED: X-ray diffraction analysis

Investigation and Report by: Dr Roger N. Brown
Manager, Petroleum Services Section: Dr Brian G. Steveson



for Dr William G. Spencer
General Manager
Applied Sciences Group

cap

1. INTRODUCTION

Eight SWC samples were received from Callista-1 for X-ray diffraction analysis.

2. PROCEDURE

Portion of each sample was powdered finely and used to prepare an X-ray diffractometer trace which was interpreted by standard procedures.

Further, weighed, lightly pre-ground subsamples were taken and dispersed in water with the aid of deflocculants and an electric blender, and allowed to sediment to produce $-2 \mu\text{m}$ e.s.d. size fractions by the pipette method. The resulting dispersions were examined by plummet balance to determine their solids contents, and were then used to produce oriented clay preparations on ceramic plates. Two plates were prepared per sample (when possible), both being saturated with Mg^{++} ions, and one in addition being treated with glycerol. When air-dry, these were examined in the X-ray diffractometer. Additional diagnostic examinations carried out consisted of examination of a glycol-treated plate and then glycerol-free plate after heating for one hour at 550°C .

3. RESULTS

The results are given in Table 1, which lists the following:

- (a) The mineralogy of the total sample, as derived from examination of the bulk material, with supporting evidence as available. The minerals found are listed in approximate order of decreasing abundance, using approximate percentage estimates. Bracketed minerals were not detected in the bulk examination but are inferred from the clay fraction.
- (b) The proportion of the sample found to separate into the $-2 \mu\text{m}$ size fraction, as determined by the plummet balance. The figure obtained applies only to the pre-treatment and dispersion conditions used.
- (c) The mineralogy of the $-2 \mu\text{m}$ fraction, given as in Section (a).

NB: Note that the percentage estimates are approximate figures.

4. REMARKS

Clay in three samples gives diffraction information which appears to originate from a triply-interstratified smectite-chlorite-illite, or at least the pattern is consistent with this interpretation. Interpretation of such clays is difficult and no estimate of the relative abundance of the larger types can be given; nor is there any suitable method for estimating the proportion of such material; an approximate estimate has been made, however.

The uncertain clay X in Core 17 gave such poorly-defined information that no proper assessment of its mineralogy could be made, except to confirm that it has a smectite component.

TABLE 1: MINERALOGY OF 8 CALLISTA-1 SAMPLES

(Figures in approximate percentages*)

	3:1788 m		6:1731 m		11:1694 m		13:1681.5 m	
Bulk Mineralogy:	Q	31	Q	35	Q	30	Q	80
	F	25	(Sm ⁺)	20	(M ⁺)	20	K	10
	M	20	C	18	K	18	F'	5
	C	15	M	10	Sid	14	M	4
	(Sm)	8	F	10	M	10	(Sm)	1
	Py?	1	K	7	F'	5		
					Py	3		
-2 μ m fraction %:	16		31		26		7	
Mineralogy:	Sm	46	Sm ⁺	58	M ⁺	64	K	80
	C	28	C	16	K	24	M	12
	M	15	K	12	M	6	Sm	4
	Q	9	M	9	Q	4	Q	4
	F	3	Q	5	C	2	F'	1
	16:1665 m		17:1616 m		18:1605 m		19:1583 m	
Bulk Mineralogy:	Q	28	(Am?)	50	(Am)	46	Q	30
	(Am?)	25	Q	15	Q	20	(Am)	25
	(TI)	20	Sid	13	(TI)	20	(TI)	25
	K	15	K	10	K	10	K	10
	M	5	F'F	5	M	3	M	5
	F	5	M	4	Py	1	Gy?	3
	Py	2	(X)	3			Py	2
-2 μ m fraction %:	25		2		16		22	
Mineralogy:	TI	60	K	44	TI	75	TI	78
	K	33	X	38	K	17	K	15
	M	4	M	16	Q	5	Q	4
	Q	3	Q	3	M	3	M	3

*NB: See text for remarks on quoted percentage figures.

Mineral Key

- Am Probable amorphous material (inferred from weak pattern)
- C Chlorite
- F Feldspar (plagioclase)
- F' K feldspar
- Gy Gypsum
- K Kaolinite
- M Mica/illite
- M⁺ Illite with minor interstratified smectite (in this instance ~20%)
- Py Pyrite
- Q Quartz
- Sid Siderite
- Sm Smectite
- Sm⁺ Smectite with minor interstratified illite (in this instance ~30%)
- TI Apparently triply-interstratified smectite-chlorite-illite clay material. See text.
- X Indeterminate smectite-related clay (not properly defined).

APPENDIX 8

Synthetic Seismogram

PE601031

This is an enclosure indicator page.
The enclosure PE601031 is enclosed within the
container PE902189 at this location in this
document.

The enclosure PE601031 has the following characteristics:

ITEM_BARCODE = PE601031
CONTAINER_BARCODE = PE902189
NAME = Synthetic Seismogram
BASIN = OTWAY
PERMIT = PEP 104
TYPE = WELL
SUBTYPE = SYNTH_SEISMOGRAM
DESCRIPTION = Synthetic Seismogram (enclosure from
WCR vol.1) for Callista-1
REMARKS =
DATE_CREATED =
DATE_RECEIVED = 2/11/88
W_NO = W972
WELL_NAME = Callista-1
CONTRACTOR = Digimap Geodata Services
CLIENT_OP_CO = Beach Petroleum NL

(Inserted by DNRE - Vic Govt Mines Dept)

PETROLEUM DIVISION

02 NOV 1988

Callista-1 W.C.R.
Vol 1.

SONSUM - WELL SONIC LOG SUMMARY PROGRAM: File: CALLISTC

Well name = CALLISTA 1

Log type = SONIC(DSC)

THIS LOG HAS BEEN CHECKSHOT CORRECTED.

KB elevation = 52.9 metres
 SRD elevation = 0.0 metres
 Replacement velocity = 2000.0 metres/s
 Time from SRD to top of sonic ... = 0.3100 seconds

2-WAY TIME FROM SRD seconds	DEPTH FROM SRD metres	DEPTH FROM KB metres	INTERVAL VELOCITY metres/s	AVERAGE VELOCITY FROM SRD metres/s	REFLECTIVITY
0.312	248.8	301.7	1622.7	1977.6	0.056247
0.314	250.6	303.5	1816.2	1996.4	-0.032208
0.316	252.3	305.2	1702.9	1994.6	0.009148
0.318	254.1	307.0	1734.3	1992.9	-0.005267
0.320	255.8	308.7	1716.1	1991.2	0.027106
0.322	257.6	310.5	1811.7	1990.1	0.008966
0.324	259.4	312.3	1844.5	1989.2	-0.028665
0.326	261.2	314.1	1738.2	1987.6	0.031306
0.328	263.0	315.9	1850.6	1986.8	-0.016449
0.330	264.8	317.7	1790.7	1985.6	-0.023553
0.332	266.5	319.4	1711.7	1984.0	0.013952
0.334	268.3	321.2	1760.1	1982.6	0.008954
0.336	270.1	323.0	1791.9	1981.5	0.017772
0.338	271.9	324.8	1856.8	1980.8	0.005504
0.340	273.8	326.7	1877.3	1980.2	0.000417
0.342	275.7	328.6	1878.9	1979.6	0.005187
0.344	277.6	330.5	1898.5	1979.1	0.009917
0.346	279.5	332.4	1936.5	1978.8	-0.011646
0.348	281.4	334.3	1891.9	1978.3	-0.017935
0.350	283.2	336.1	1825.3	1977.5	0.018604
0.352	285.1	338.0	1894.5	1977.0	0.007054
0.354	287.0	339.9	1921.4	1976.7	0.008353
0.356	289.0	341.9	1953.8	1976.6	0.005955
0.358	291.0	343.9	1977.2	1976.6	0.003529
0.360	293.0	345.9	1991.2	1976.6	-0.039601
0.362	294.8	347.7	1839.5	1975.9	0.012994
0.364	296.7	349.6	1887.9	1975.4	0.010491
0.366	298.6	351.5	1927.9	1975.1	-0.021388
0.368	300.5	353.4	1847.2	1974.4	-0.016191
0.370	302.3	355.2	1788.3	1973.4	0.019153
0.372	304.1	357.0	1858.2	1972.8	-0.002607
0.374	306.0	358.9	1848.5	1972.2	0.012846
0.376	307.9	360.8	1896.6	1971.8	-0.013384
0.378	309.7	362.6	1846.5	1971.1	-0.002375
0.380	311.5	364.4	1837.8	1970.4	0.013488
0.382	313.4	366.3	1888.0	1970.0	-0.025416
0.384	315.2	368.1	1794.4	1969.0	0.045066
0.386	317.2	370.1	1963.8	1969.0	-0.017597
0.388	319.1	372.0	1895.9	1968.6	0.001896
0.390	321.0	373.9	1903.1	1968.3	-0.028731

0.392	322.8	375.7	1796.8	1967.4	-0.006799
0.394	324.6	377.5	1772.5	1966.4	0.022217
0.396	326.4	379.3	1853.1	1965.9	0.000085
0.398	328.3	381.2	1853.4	1965.3	-0.010954
0.400	330.1	383.0	1813.2	1964.5	0.006664
0.402	331.9	384.8	1837.6	1963.9	0.020430
0.404	333.8	386.7	1914.2	1963.7	-0.005103
0.406	335.7	388.6	1894.8	1963.3	0.029576
0.408	337.7	390.6	2010.3	1963.6	-0.009155
0.410	339.7	392.6	1973.8	1963.6	0.002183
0.412	341.7	394.6	1982.4	1963.7	-0.000368
0.414	343.7	396.6	1980.2	1963.8	0.012827
0.416	345.7	398.6	2031.6	1964.1	0.009488
0.418	347.8	400.7	2070.6	1964.6	-0.014948
0.420	349.8	402.7	2009.6	1964.8	0.003380
0.422	351.8	404.7	2022.8	1965.1	-0.044809
0.424	353.7	406.6	1850.0	1964.6	0.015111
0.426	355.6	408.5	1906.8	1964.3	-0.000588
0.428	357.5	410.4	1904.6	1964.0	0.002977
0.430	359.4	412.3	1916.0	1963.8	0.002510
0.432	361.3	414.2	1925.7	1963.6	-0.007345
0.434	363.2	416.1	1897.6	1963.3	0.003734
0.436	365.1	418.0	1911.8	1963.1	-0.024833
0.438	366.9	419.8	1820.6	1962.4	0.008787
0.440	368.8	421.7	1852.8	1961.9	0.018526
0.442	370.7	423.6	1922.8	1961.7	0.012002
0.444	372.7	425.6	1969.5	1961.8	-0.010064
0.446	374.6	427.5	1930.2	1961.6	0.008700
0.448	376.6	429.5	1964.1	1961.6	-0.010771
0.450	378.5	431.4	1922.2	1961.5	0.008034
0.452	380.5	433.4	1953.4	1961.4	-0.003768
0.454	382.4	435.3	1938.7	1961.3	0.010241
0.456	384.4	437.3	1978.8	1961.4	-0.000134
0.458	386.4	439.3	1978.3	1961.5	-0.005942
0.460	388.3	441.2	1954.9	1961.5	0.021959
0.462	390.4	443.3	2042.7	1961.8	-0.025465
0.464	392.3	445.2	1941.3	1961.7	0.013856
0.466	394.3	447.2	1995.8	1961.9	-0.010820
0.468	396.2	449.1	1953.9	1961.8	0.005741
0.470	398.2	451.1	1976.4	1961.9	-0.003088
0.472	400.2	453.1	1964.3	1961.9	-0.002872
0.474	402.1	455.0	1953.0	1961.9	-0.029528
0.476	404.0	456.9	1841.0	1961.4	0.005080
0.478	405.8	458.7	1859.8	1960.9	0.000988
0.480	407.7	460.6	1863.5	1960.5	-0.001003
0.482	409.6	462.5	1859.7	1960.1	0.001490
0.484	411.4	464.3	1865.3	1959.7	-0.002396
0.486	413.3	466.2	1856.4	1959.3	-0.001823
0.488	415.1	468.0	1849.6	1958.8	0.028626
0.490	417.1	470.0	1958.6	1958.8	-0.045780
0.492	418.9	471.8	1787.1	1958.1	0.039391
0.494	420.8	473.7	1934.5	1958.0	0.058702
0.496	423.0	475.9	2175.8	1958.9	0.006822
0.498	425.2	478.1	2203.9	1959.9	-0.056860
0.500	427.2	480.1	1966.7	1959.9	0.012262
0.502	429.2	482.1	2015.6	1960.2	0.020096
0.504	431.3	484.2	2098.3	1960.7	-0.036440
0.506	433.2	486.1	1950.7	1960.7	0.106300
0.508	435.6	488.5	2414.8	1962.5	0.045183
0.510	438.3	491.2	2643.3	1965.1	-0.004306

0.512	440.9	493.8	2620.6	1967.7	0.015871
0.514	443.6	496.5	2705.1	1970.6	-0.008928
0.516	446.3	499.2	2657.3	1973.2	0.000746
0.518	448.9	501.8	2661.2	1975.9	-0.014775
0.520	451.5	504.4	2583.7	1978.2	-0.042226
0.522	453.9	506.8	2374.4	1979.7	-0.008004
0.524	456.2	509.1	2336.7	1981.1	0.014860
0.526	458.6	511.5	2407.2	1982.7	0.021065
0.528	461.1	514.0	2510.8	1984.7	-0.018590
0.530	463.6	516.5	2419.1	1986.3	-0.018665
0.532	465.9	518.8	2330.5	1987.6	-0.044964
0.534	468.1	521.0	2173.0	1988.3	0.008421
0.536	470.3	523.2	2209.9	1989.2	0.031895
0.538	472.6	525.5	2355.5	1990.5	0.001487
0.540	475.0	527.9	2362.5	1991.9	0.004791
0.542	477.4	530.3	2385.3	1993.4	-0.020625
0.544	479.7	532.6	2288.9	1994.4	-0.005669
0.546	481.9	534.8	2263.1	1995.4	-0.011869
0.548	484.1	537.0	2210.0	1996.2	0.013495
0.550	486.4	539.3	2278.6	1997.2	0.004136
0.552	488.7	541.6	2298.5	1998.3	-0.018494
0.554	490.9	543.8	2215.0	1999.1	0.033597
0.556	493.3	546.2	2369.0	2000.4	0.076478
0.558	495.1	549.0	2761.4	2003.2	0.023277
0.560	499.0	551.9	2893.0	2006.3	-0.076732
0.562	501.4	554.3	2480.7	2008.0	0.013979
0.564	504.0	556.9	2551.0	2010.0	-0.005951
0.566	506.5	559.4	2520.8	2011.8	-0.002029
0.568	509.0	561.9	2510.6	2013.5	-0.000653
0.570	511.5	564.4	2507.3	2015.3	0.030577
0.572	514.2	567.1	2655.5	2017.5	-0.025912
0.574	516.7	569.6	2530.9	2019.3	0.019500
0.576	519.4	572.3	2631.5	2021.4	0.000419
0.578	522.0	574.9	2633.7	2023.6	-0.022018
0.580	524.5	577.4	2520.3	2025.3	-0.017105
0.582	526.9	579.8	2435.5	2026.7	0.031212
0.584	529.5	582.4	2592.4	2028.6	-0.001235
0.586	532.1	585.0	2586.0	2030.5	-0.023837
0.588	534.6	587.5	2465.6	2032.0	0.007983
0.590	537.1	590.0	2505.3	2033.6	0.002073
0.592	539.6	592.5	2515.7	2035.2	0.030645
0.594	542.3	595.2	2674.8	2037.4	-0.029070
0.596	544.8	597.7	2523.7	2039.0	-0.011758
0.598	547.3	600.2	2465.0	2040.4	0.005613
0.600	549.8	602.7	2492.8	2042.0	0.024094
0.602	552.4	605.3	2415.9	2043.9	0.010436
0.604	555.0	607.9	2671.1	2045.9	0.013955
0.606	557.8	610.7	2746.7	2048.3	-0.032853
0.608	560.4	613.3	2572.0	2050.0	0.034709
0.610	563.1	616.0	2756.9	2052.3	-0.077483
0.612	565.5	618.4	2360.4	2053.3	-0.051904
0.614	567.6	620.5	2127.5	2053.5	0.000159
0.616	569.7	622.6	2128.2	2053.8	0.035003
0.618	572.0	624.9	2282.5	2054.5	-0.036810
0.620	574.1	627.0	2120.5	2054.7	-0.000716
0.622	576.3	629.2	2117.4	2054.9	0.062689
0.624	578.7	631.6	2400.7	2056.0	0.116645
0.626	581.7	634.6	3034.7	2059.2	0.036337
0.628	585.0	637.9	3263.5	2063.0	-0.094043
0.630	587.7	640.6	2702.5	2065.0	0.073482

0.632	590.8	643.7	3131.1	2068.4	-0.047505
0.634	593.6	646.5	2847.2	2070.9	-0.025733
0.636	596.3	649.2	2704.3	2072.9	0.015205
0.638	599.1	652.0	2787.8	2075.1	0.013274
0.640	602.0	654.9	2862.8	2077.6	0.014235
0.642	604.9	657.8	2945.5	2080.3	-0.012177
0.644	607.8	660.7	2874.6	2082.7	-0.042257
0.646	610.5	663.4	2641.5	2084.5	0.010909
0.648	613.2	666.1	2699.8	2086.4	0.003651
0.650	615.9	668.8	2719.6	2088.3	-0.001579
0.652	618.6	671.5	2711.0	2090.2	-0.024292
0.654	621.2	674.1	2882.4	2091.7	0.000099
0.656	623.8	676.7	2882.9	2093.2	0.000950
0.658	626.3	679.2	2578.0	2094.7	0.051144
0.660	629.2	682.1	2855.9	2097.0	-0.026493
0.662	631.9	684.8	2708.5	2098.9	0.012849
0.664	634.7	687.6	2779.0	2100.9	-0.004822
0.666	637.4	690.3	2752.4	2102.9	0.045243
0.668	640.4	693.3	3013.2	2105.6	-0.038682
0.670	643.2	696.1	2788.9	2107.6	0.025574
0.672	645.9	698.8	2639.7	2109.2	0.008152
0.674	648.5	701.4	2606.8	2110.7	-0.032712
0.676	650.9	703.8	2441.7	2111.7	-0.006417
0.678	653.3	706.2	2410.6	2112.6	0.006245
0.680	655.8	708.7	2441.0	2113.5	0.004005
0.682	658.2	711.1	2460.6	2114.6	0.009069
0.684	660.7	713.6	2805.6	2115.7	0.009476
0.686	663.3	716.2	2553.6	2117.0	0.032002
0.688	666.0	718.9	2722.4	2118.7	-0.097472
0.690	668.3	721.2	2338.9	2119.1	-0.008627
0.692	670.5	723.4	2200.5	2119.1	0.042846
0.694	672.9	725.8	2377.5	2120.1	0.021280
0.696	675.4	728.3	2801.8	2121.2	-0.011463
0.698	677.8	730.7	2485.1	2122.1	-0.015639
0.700	680.2	733.1	2369.8	2122.9	0.014923
0.702	682.6	735.5	2441.6	2123.8	-0.002733
0.704	685.0	737.9	2428.3	2124.6	0.034083
0.706	687.6	740.5	2599.6	2126.0	-0.014273
0.708	690.2	743.1	2526.5	2127.1	-0.012437
0.710	692.6	745.5	2464.4	2128.1	-0.004936
0.712	695.1	748.0	2440.2	2128.9	0.028360
0.714	697.7	750.6	2582.6	2130.2	-0.029908
0.716	700.1	753.0	2432.6	2131.0	-0.001791
0.718	702.5	755.4	2423.9	2131.9	0.002222
0.720	704.9	757.8	2434.7	2132.7	-0.034372
0.722	707.2	760.1	2722.9	2133.1	0.001284
0.724	709.5	762.4	2228.8	2133.5	0.040531
0.726	712.0	764.9	2471.3	2134.4	0.024008
0.728	714.6	767.5	2892.9	2135.7	-0.059680
0.730	716.9	769.8	2300.8	2136.1	0.035728
0.732	719.3	772.2	2471.3	2137.1	-0.024578
0.734	721.7	774.6	2352.8	2137.6	0.017003
0.736	724.1	777.0	2434.1	2138.4	0.014331
0.738	726.6	779.5	2504.9	2139.4	0.031022
0.740	729.3	782.2	2665.3	2140.9	-0.048561
0.742	731.7	784.6	2418.4	2141.6	0.025185
0.744	734.3	787.2	2513.4	2142.7	0.029947
0.746	737.0	789.9	2700.4	2144.2	-0.019331
0.748	739.6	792.5	2598.0	2145.4	-0.029923
0.750	742.0	794.9	2447.1	2146.2	0.031438

0.752	744.6	797.5	2605.9	2147.4	0.074963
0.754	747.6	800.5	3028.3	2149.8	-0.103668
0.756	750.1	803.0	2459.4	2150.6	-0.009304
0.758	752.5	805.4	2414.0	2151.3	0.019693
0.760	755.0	807.9	2511.0	2152.2	0.011349
0.762	757.6	810.5	2568.7	2153.3	-0.014817
0.764	760.1	813.0	2493.7	2154.2	0.002689
0.766	762.6	815.5	2507.1	2155.1	0.009956
0.768	765.1	818.0	2557.5	2156.2	0.000625
0.770	767.7	820.6	2560.7	2157.2	-0.021551
0.772	770.2	823.1	2452.7	2158.0	0.044317
0.774	772.8	825.7	2480.7	2159.3	-0.045077
0.776	775.3	828.2	2449.5	2160.1	-0.045195
0.778	777.5	830.4	2237.6	2160.3	0.099307
0.780	780.3	833.2	2731.1	2161.8	0.034267
0.782	783.2	836.1	2924.9	2163.7	-0.068349
0.784	785.7	838.6	2550.6	2164.7	-0.006826
0.786	788.3	841.2	2516.0	2165.6	0.010010
0.788	790.8	843.7	2566.9	2166.6	0.012140
0.790	793.4	846.3	2630.0	2167.8	0.021373
0.792	795.2	849.1	2744.9	2169.2	0.008645
0.794	799.0	851.9	2792.8	2170.8	0.101972
0.796	802.4	855.3	3427.0	2174.0	-0.11818
0.798	805.2	858.1	2737.7	2175.4	-0.054639
0.800	807.6	860.5	2454.0	2176.1	0.045240
0.802	810.3	863.2	2686.6	2177.3	0.024619
0.804	813.1	866.0	2822.2	2179.0	-0.033070
0.806	815.8	868.7	2641.5	2180.1	0.021462
0.808	818.5	871.4	2757.4	2181.5	0.079052
0.810	821.7	874.6	3230.7	2184.1	-0.090316
0.812	824.4	877.3	2695.5	2185.4	-0.052283
0.814	826.9	879.8	2427.7	2186.0	0.024664
0.816	829.4	882.3	2550.4	2186.9	0.049216
0.818	832.2	885.1	2814.5	2188.4	-0.012748
0.820	835.0	887.9	2743.6	2189.8	0.022521
0.822	837.8	890.7	2870.1	2191.4	0.003846
0.824	840.7	893.6	2892.2	2193.1	-0.021262
0.826	843.5	896.4	2771.8	2194.5	0.010047
0.828	846.3	899.2	2828.0	2196.0	-0.031381
0.830	849.0	901.9	2856.0	2197.2	0.010876
0.832	851.7	904.6	2714.4	2198.4	-0.008095
0.834	854.5	907.4	2758.7	2199.7	-0.030828
0.836	857.1	910.0	2593.7	2200.7	0.017735
0.838	859.7	912.6	2687.3	2201.8	0.010895
0.840	862.5	915.4	2746.5	2203.1	-0.023013
0.842	865.1	918.0	2623.0	2204.1	0.030608
0.844	867.7	920.8	2788.6	2205.5	0.071165
0.846	871.1	924.0	3215.9	2207.9	-0.022061
0.848	874.2	927.1	3077.1	2210.0	-0.007420
0.850	877.2	930.1	3031.7	2211.9	-0.014541
0.852	880.2	933.1	2944.8	2213.6	0.010681
0.854	883.2	936.1	3008.4	2215.5	0.020873
0.856	886.3	939.2	3136.7	2217.6	0.002889
0.858	889.5	942.4	3154.9	2219.8	-0.001941
0.860	892.6	945.5	3142.7	2222.0	-0.028076
0.862	895.6	948.5	2971.0	2223.7	-0.034357
0.864	898.4	951.3	2773.6	2225.0	-0.022795
0.866	901.0	953.9	2650.0	2225.9	0.000478
0.868	903.7	956.6	2652.5	2226.9	0.007816
0.870	906.4	959.3	2694.3	2228.0	0.056598

0.872	909.4	962.3	3017.6	2229.8	-0.027289
0.874	912.2	965.1	2857.3	2231.3	-0.025481
0.876	914.9	967.8	2715.3	2232.4	-0.023875
0.878	917.5	970.4	2588.7	2233.2	0.004270
0.880	920.1	973.0	2610.9	2234.0	-0.001817
0.882	922.7	975.6	2601.4	2234.9	-0.009139
0.884	925.3	978.2	2554.3	2235.6	0.009652
0.886	927.9	980.8	2604.1	2236.4	-0.006925
0.888	930.5	983.4	2568.3	2237.2	0.023618
0.890	933.2	986.1	2692.5	2238.2	0.012956
0.892	935.9	988.8	2763.2	2239.4	-0.045701
0.894	938.5	991.4	2521.7	2240.0	0.001498
0.896	941.0	993.9	2528.2	2240.6	-0.003772
0.898	943.5	996.4	2510.2	2241.2	-0.000854
0.900	946.0	998.9	2505.9	2241.8	-0.004412
0.902	948.5	1001.4	2483.9	2242.4	0.022339
0.904	951.1	1004.0	2597.4	2243.2	0.008690
0.906	953.7	1006.6	2643.0	2244.0	-0.009882
0.908	956.3	1009.2	2591.2	2244.8	0.024342
0.910	959.0	1011.9	2720.5	2245.8	0.004365
0.912	961.8	1014.7	2744.4	2246.9	-0.018532
0.914	964.4	1017.3	2644.5	2247.8	-0.005603
0.916	967.0	1019.9	2615.1	2248.6	0.005753
0.918	969.7	1022.6	2645.3	2249.5	-0.031175
0.920	972.2	1025.1	2485.4	2250.0	0.026218
0.922	974.8	1027.7	2619.2	2250.8	0.033909
0.924	977.4	1030.3	2803.1	2252.0	-0.014772
0.926	980.3	1033.2	2721.5	2253.0	-0.009381
0.928	983.0	1035.9	2670.9	2253.9	-0.020780
0.930	985.5	1038.4	2562.1	2254.6	0.033531
0.932	988.3	1041.2	2739.9	2255.6	0.010142
0.934	991.1	1044.0	2786.1	2256.8	0.013367
0.936	994.0	1046.9	2871.8	2258.1	-0.034835
0.938	996.6	1049.5	2678.5	2259.0	-0.007506
0.940	999.3	1052.2	2638.6	2259.8	0.014989
0.942	1002.0	1054.9	2718.9	2260.8	0.015400
0.944	1004.8	1057.7	2803.9	2261.9	-0.018136
0.946	1007.5	1060.4	2704.0	2262.8	-0.005279
0.948	1010.2	1063.1	2675.6	2263.7	0.010618
0.950	1012.9	1065.8	2733.1	2264.7	0.000210
0.952	1015.6	1068.5	2734.2	2265.7	0.044613
0.954	1018.6	1071.5	2989.6	2267.2	-0.047667
0.956	1021.3	1074.2	2717.5	2268.1	0.030425
0.958	1024.2	1077.1	2888.1	2269.4	-0.014560
0.960	1027.0	1079.9	2805.2	2270.6	0.010227
0.962	1029.9	1082.8	2863.2	2271.8	-0.015286
0.964	1032.7	1085.6	2778.9	2272.8	0.002889
0.966	1035.5	1088.4	2793.0	2273.9	0.002037
0.968	1038.3	1091.2	2804.4	2275.0	-0.002992
0.970	1041.1	1094.0	2787.7	2276.1	-0.005546
0.972	1043.8	1096.7	2756.9	2277.1	0.025842
0.974	1046.7	1099.6	2903.2	2278.3	0.007601
0.976	1049.7	1102.6	2947.7	2279.7	0.000539
0.978	1052.6	1105.5	2950.9	2281.1	0.022155
0.980	1055.7	1108.6	3084.6	2282.7	0.007229
0.982	1058.8	1111.7	3129.5	2284.4	-0.033332
0.984	1061.8	1114.7	2927.6	2285.8	0.002958
0.986	1064.7	1117.6	2945.0	2287.1	-0.007169
0.988	1067.6	1120.5	2903.1	2288.3	-0.005555
0.990	1070.5	1123.4	2871.0	2289.5	0.023156

0.992	1073.5	1126.4	3007.1	2291.0	0.025017
0.994	1076.7	1129.6	3161.4	2292.7	-0.006707
0.996	1079.8	1132.7	3119.3	2294.4	-0.051314
0.998	1082.6	1135.5	2814.8	2295.4	-0.011683
1.000	1085.3	1138.2	2749.8	2296.3	0.014802
1.002	1088.2	1141.1	2832.4	2297.4	-0.006029
1.004	1091.0	1143.9	2798.5	2298.4	-0.006080
1.006	1093.7	1146.6	2764.6	2299.3	-0.000348
1.008	1096.5	1149.4	2762.7	2300.2	0.002518
1.010	1099.3	1152.2	2804.6	2301.2	0.012338
1.012	1102.2	1155.1	2874.6	2302.4	-0.001902
1.014	1105.0	1157.9	2863.7	2303.5	0.014461
1.016	1108.0	1160.9	2947.8	2304.7	0.016586
1.018	1111.0	1163.9	3047.2	2306.2	-0.025535
1.020	1113.9	1166.8	2895.4	2307.4	-0.028134
1.022	1116.7	1169.6	2737.0	2308.2	-0.000317
1.024	1119.4	1172.3	2735.2	2309.0	-0.006946
1.026	1122.1	1175.0	2697.5	2309.8	-0.002731
1.028	1124.8	1177.7	2682.8	2310.5	0.084527
1.030	1127.5	1180.4	2707.2	2311.3	0.002951
1.032	1130.2	1183.1	2723.2	2312.1	-0.003011
1.034	1132.9	1185.8	2706.9	2312.9	-0.021009
1.036	1135.5	1188.4	2595.5	2313.4	0.003629
1.038	1138.1	1191.0	2614.4	2314.0	0.010303
1.040	1140.8	1193.7	2668.8	2314.7	-0.001640
1.042	1143.5	1196.4	2660.1	2315.3	-0.026859
1.044	1146.0	1198.9	2520.9	2315.7	-0.010055
1.046	1148.5	1201.4	2470.7	2316.0	0.022526
1.048	1151.0	1203.9	2584.6	2316.5	0.022434
1.050	1153.7	1206.6	2703.3	2317.3	-0.012419
1.052	1156.4	1209.3	2636.9	2317.9	-0.000113
1.054	1159.0	1211.9	2636.3	2318.5	0.012243
1.056	1161.7	1214.6	2701.7	2319.2	-0.017552
1.058	1164.3	1217.2	2608.5	2319.7	0.037752
1.060	1167.1	1220.0	2813.2	2320.7	-0.009036
1.062	1169.9	1222.8	2762.8	2321.5	-0.002263
1.064	1172.6	1225.5	2750.3	2322.3	-0.015935
1.066	1175.3	1228.2	2664.0	2323.0	0.005277
1.068	1178.0	1230.9	2692.3	2323.7	0.019043
1.070	1180.8	1233.7	2796.9	2324.5	-0.002092
1.072	1183.6	1236.5	2785.2	2325.4	-0.024754
1.074	1186.2	1239.1	2650.7	2326.0	-0.007482
1.076	1188.8	1241.7	2611.3	2326.5	0.006536
1.078	1191.5	1244.4	2645.7	2327.1	-0.003343
1.080	1194.1	1247.0	2628.0	2327.7	0.020086
1.082	1196.9	1249.8	2735.8	2328.4	0.013073
1.084	1199.7	1252.6	2808.3	2329.3	0.043578
1.086	1202.7	1255.6	3064.2	2330.7	-0.033898
1.088	1205.6	1258.5	2863.3	2331.7	-0.021543
1.090	1208.3	1261.2	2742.5	2332.4	0.020998
1.092	1211.2	1264.1	2860.1	2333.4	-0.031545
1.094	1213.9	1266.8	2685.2	2334.0	0.019625
1.096	1216.7	1269.6	2792.7	2334.9	0.015227
1.098	1219.6	1272.5	2879.1	2335.8	-0.009897
1.100	1222.4	1275.3	2822.6	2336.7	0.006805
1.102	1225.2	1278.1	2861.3	2337.7	-0.000821
1.104	1228.1	1281.0	2856.6	2338.6	0.006565
1.106	1231.0	1283.9	2894.4	2339.6	-0.003969
1.108	1233.9	1286.8	2871.5	2340.6	-0.004188
1.110	1236.7	1289.6	2847.5	2341.5	0.006414

1.112	1239.6	1292.5	2884.3	2342.5	0.003147
1.114	1242.5	1295.4	2902.5	2343.5	-0.016521
1.116	1245.3	1298.2	2898.2	2344.3	0.023223
1.118	1248.2	1301.1	2941.7	2345.4	-0.0004801
1.120	1251.2	1304.1	2913.6	2346.4	-0.011682
1.122	1254.0	1306.9	2846.3	2347.3	0.021106
1.124	1257.0	1309.9	2969.0	2348.4	-0.007511
1.126	1259.9	1312.8	2924.8	2349.4	-0.013385
1.128	1262.7	1315.6	2847.5	2350.3	-0.009502
1.130	1265.5	1318.4	2933.9	2351.1	-0.005378
1.132	1268.3	1321.2	2784.0	2351.8	-0.005969
1.134	1271.0	1323.9	2731.2	2352.5	0.034156
1.136	1274.0	1326.9	2824.4	2353.5	0.020384
1.138	1277.0	1329.9	3046.1	2354.7	-0.013046
1.140	1280.0	1332.9	2876.6	2355.8	0.008055
1.142	1283.0	1335.9	3015.8	2356.9	-0.000739
1.144	1286.0	1338.9	3011.4	2358.1	-0.027079
1.146	1288.9	1341.8	2852.6	2358.9	0.005299
1.148	1291.7	1344.6	2883.0	2359.9	0.039495
1.150	1294.9	1347.8	3120.1	2361.2	-0.040959
1.152	1297.7	1350.6	2874.5	2362.1	0.015729
1.154	1300.7	1353.6	2866.4	2363.1	0.004176
1.156	1303.7	1356.6	2991.3	2364.2	-0.011239
1.158	1306.6	1359.5	2924.8	2365.2	-0.006845
1.160	1309.5	1362.4	2883.0	2366.1	0.011120
1.162	1312.4	1365.3	2949.9	2367.1	0.004827
1.164	1315.4	1368.3	2978.5	2368.1	-0.011204
1.166	1318.3	1371.2	2912.5	2369.1	0.014892
1.168	1321.3	1374.2	3000.6	2370.1	0.034458
1.170	1324.6	1377.5	3244.7	2371.6	-0.017938
1.172	1327.7	1380.6	3101.4	2372.8	-0.010355
1.174	1330.7	1383.6	3037.9	2374.0	-0.022355
1.176	1333.6	1386.5	2905.0	2374.9	0.021496
1.178	1336.6	1389.5	3032.7	2376.0	0.005018
1.180	1339.7	1392.6	3063.3	2377.1	0.001053
1.182	1342.8	1395.7	3069.7	2378.3	0.006637
1.184	1345.9	1398.8	3110.7	2379.6	0.001887
1.186	1349.0	1401.9	3122.5	2380.8	0.002015
1.188	1352.1	1405.0	3135.1	2382.1	-0.000436
1.190	1355.3	1408.2	3132.4	2383.3	0.006644
1.192	1358.4	1411.3	3174.3	2384.7	0.008251
1.194	1361.7	1414.6	3227.1	2386.1	-0.007444
1.196	1364.8	1417.7	3179.4	2387.4	0.004265
1.198	1368.1	1421.0	3206.6	2388.8	-0.001489
1.200	1371.2	1424.1	3197.1	2390.1	-0.009639
1.202	1374.4	1427.3	3136.1	2391.4	0.010461
1.204	1377.6	1430.5	3202.4	2392.7	0.011655
1.206	1380.9	1433.8	3277.9	2394.2	-0.004804
1.208	1384.1	1437.0	3246.5	2395.6	0.004160
1.210	1387.4	1440.3	3273.7	2397.0	-0.000379
1.212	1390.7	1443.6	3271.2	2398.5	0.001742
1.214	1393.9	1446.8	3282.6	2399.9	0.001124
1.216	1397.2	1450.1	3290.0	2401.4	0.007898
1.218	1400.6	1453.5	3342.4	2402.9	-0.013342
1.220	1403.8	1456.7	3354.4	2404.3	-0.008634
1.222	1407.0	1459.9	3198.6	2405.6	0.070087
1.224	1410.7	1463.6	3680.8	2407.7	-0.027475
1.226	1414.2	1467.1	3484.0	2409.5	-0.025866
1.228	1417.5	1470.4	3308.3	2410.9	-0.001937
1.230	1420.8	1473.7	3295.5	2412.4	0.004392

1.232	1424.1	1477.0	3324.5	2413.9	-0.000002
1.234	1427.4	1480.3	3324.5	2415.3	-0.0003174
1.236	1430.7	1483.6	3303.5	2416.8	-0.0003190
1.238	1434.0	1486.9	3282.5	2418.2	-0.001753
1.240	1437.3	1490.2	3271.0	2419.6	-0.003278
1.242	1440.5	1493.4	3249.6	2420.9	0.004507
1.244	1443.8	1496.7	3279.1	2422.3	0.001705
1.246	1447.1	1500.0	3290.3	2423.7	-0.001588
1.248	1450.4	1503.3	3279.8	2425.0	0.007409
1.250	1453.7	1506.6	3328.8	2426.5	0.001080
1.252	1457.1	1510.0	3346.0	2427.9	0.010540
1.254	1460.5	1513.4	3407.1	2429.5	-0.002486
1.256	1463.9	1516.8	3390.2	2431.0	0.001677
1.258	1467.3	1520.2	3401.6	2432.6	-0.003522
1.260	1470.6	1523.5	3377.7	2434.1	0.000518
1.262	1474.0	1526.9	3381.2	2435.6	-0.000940
1.264	1477.4	1530.3	3374.8	2437.1	0.003497
1.266	1480.8	1533.7	3398.5	2438.6	-0.005025
1.268	1484.2	1537.1	3364.5	2440.0	-0.001224
1.270	1487.5	1540.4	3356.5	2441.5	-0.000266
1.272	1490.9	1543.8	3354.5	2442.9	-0.011493
1.274	1494.1	1547.0	3278.8	2444.2	-0.019509
1.276	1497.3	1550.2	3152.8	2445.3	0.020146
1.278	1500.6	1553.5	3282.5	2446.6	-0.008491
1.280	1503.8	1556.7	3227.3	2447.9	-0.001720
1.282	1507.0	1559.9	3216.2	2449.1	-0.006293
1.284	1510.2	1563.1	3175.9	2450.2	0.037995
1.286	1513.6	1566.5	3426.8	2451.7	-0.024816
1.288	1516.9	1569.8	3260.9	2453.0	0.021294
1.290	1520.3	1573.2	3402.8	2454.4	-0.046392
1.292	1523.4	1576.3	3101.0	2455.4	0.001760
1.294	1526.5	1579.4	3112.0	2456.5	-0.021527
1.296	1529.5	1582.4	2980.8	2457.3	0.005240
1.298	1532.5	1585.4	3012.2	2458.1	-0.006316
1.300	1535.5	1588.4	2974.4	2458.9	-0.002500
1.302	1538.4	1591.3	2959.6	2459.7	0.015877
1.304	1541.5	1594.4	3055.1	2460.6	-0.017219
1.306	1544.4	1597.3	2951.6	2461.4	0.002942
1.308	1547.4	1600.3	2969.0	2462.1	-0.004092
1.310	1550.4	1603.3	2944.8	2462.9	-0.004629
1.312	1553.3	1606.2	2917.7	2463.6	0.036333
1.314	1556.4	1609.3	3137.7	2464.6	0.029190
1.316	1559.7	1612.6	3326.4	2465.9	0.041134
1.318	1563.3	1616.2	3611.8	2467.6	0.002121
1.320	1567.0	1619.9	3627.2	2469.4	-0.007856
1.322	1570.5	1623.4	3572.0	2471.1	-0.012704
1.324	1574.0	1626.9	3482.4	2472.6	-0.028395
1.326	1577.3	1630.2	3288.8	2473.8	0.003883
1.328	1580.6	1633.5	3314.4	2475.1	-0.042088
1.330	1583.7	1636.6	3046.7	2475.9	-0.001529
1.332	1586.7	1639.6	3037.4	2476.8	0.013590
1.334	1589.8	1642.7	3121.1	2477.8	0.001870
1.336	1593.0	1645.7	3132.8	2478.7	0.008645
1.338	1596.2	1649.1	3187.4	2479.8	0.004971
1.340	1599.4	1652.3	3219.3	2480.9	-0.030981
1.342	1602.4	1655.3	3025.8	2481.7	-0.017102
1.344	1605.3	1658.2	2924.1	2482.4	0.032505
1.346	1608.4	1661.3	3120.5	2483.3	-0.004693
1.348	1611.5	1664.4	3091.4	2484.2	0.001197
1.350	1614.6	1667.5	3098.8	2485.1	0.036494

1.352	1618.0	1670.9	3333.5	2486.4	0.046095
1.354	1621.6	1674.5	3655.7	2488.1	-0.016229
1.356	1625.2	1678.1	3538.9	2489.7	-0.007419
1.358	1628.7	1681.6	3486.8	2491.1	-0.002985
1.360	1632.1	1685.0	3466.1	2492.6	0.005561
1.362	1635.6	1688.5	3504.8	2494.0	-0.000517
1.364	1639.1	1692.0	3501.2	2495.5	0.001489
1.366	1642.6	1695.5	3511.6	2497.0	-0.030432
1.368	1645.9	1698.8	3304.2	2498.2	-0.040775
1.370	1649.0	1701.9	3045.3	2499.0	0.078009
1.372	1652.5	1705.4	3560.6	2500.5	-0.016011
1.374	1656.0	1708.9	3448.4	2501.9	-0.045088
1.376	1659.1	1712.0	3150.9	2502.9	0.011402
1.378	1662.4	1715.3	3223.5	2503.9	0.016591
1.380	1665.7	1718.6	3332.3	2505.1	-0.015522
1.382	1668.9	1721.8	3230.4	2506.2	0.012928
1.384	1672.2	1725.1	3315.1	2507.3	-0.014203
1.386	1675.5	1728.4	3222.2	2508.4	-0.016822
1.388	1678.6	1731.5	3115.6	2509.2	-0.006401
1.390	1681.7	1734.6	3076.0	2510.0	0.035975
1.392	1685.0	1737.9	3305.5	2511.2	0.024058
1.394	1688.4	1741.3	3468.4	2512.6	-0.024899
1.396	1692.1	1745.0	3645.1	2514.2	-0.031546
1.398	1695.5	1748.4	3422.2	2515.5	0.033172
1.400	1699.2	1752.1	3657.0	2517.1	-0.021974
1.402	1702.7	1755.6	3499.8	2518.5	-0.006643
1.404	1706.1	1759.0	3453.6	2519.9	-0.009577
1.406	1709.5	1762.4	3388.1	2521.1	-0.001723
1.408	1712.9	1765.8	3376.4	2522.3	0.001355
1.410	1716.2	1769.1	3367.3	2523.5	0.014763
1.412	1719.7	1772.6	3464.7	2524.8	0.007862
1.414	1723.2	1776.1	3519.6	2526.2	-0.024320
1.416	1726.6	1779.5	3352.5	2527.4	-0.027515
1.418	1730.1	1783.0	3542.2	2528.8	-0.025801
1.420	1733.5	1786.4	3364.0	2530.0	0.001748
1.422	1736.9	1789.8	3375.8	2531.2	-0.018994
1.424	1740.1	1793.0	3249.9	2532.2	0.003961
1.426	1743.4	1796.3	3275.8	2533.3	-0.008750
1.428	1746.6	1799.5	3219.0	2534.2	-0.000950