





WELL COMPLETION REPORT 25 AUG 1995 PERCH-4

GIPPSLAND BASIN, VICTORIA

Compiled by: Ben Hayes August 1995

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II.	W	ELL DATA RECORD
LOCATION Surface Location		Latitude: 038° 34' 14" S Longitude: 147° 19' 16"E X= 527,991 E Y= 5,730,783 N
Primary Objective		 X= 529,169 E Y= 5,730,484 N Map Projection: UTM Zone 55 Geographical Location: Bass Strait, Victoria Field : PERCH
BLOCK	:	VIC/L15
ELEVATION	:	37.0m
WATER DEPTH	:	41.3m
TOTAL DEPTH	:	2052.0 m (Driller) 1931.0 m (Logger) 2055.0 m (Logger Extrap.)
COMPLETION:	:	Cased and Suspended as a future oil producer from the N sand
MOVE IN	:	30/01/95
SPUDDED	:	01/02/95
REACHED TD	:	11/02/95
RIG RELEASED	:	25/02/95
OPERATOR	:	Esso Australia Resources Ltd.
PERMITEE OR LICENSEE	:	BHP Petroleum (Australia) Pty Ltd and Esso Australia Resources Ltd.
ESSO INTEREST	:	50 %
OTHER INTEREST	:	BHPP 50%
CONTRACTOR	:	Reading and Bates
RIG NAME	:	Harvey H Ward.
EQUIPMENT TYPE	:	Jack Up
TOTAL RIG DAYS	:	29.7
DRILLING AFE NO	:	L05014007
TYPE COMPLETION	:	7-3/4" casing, oil producer.
WELL CLASSIFICATION	:	Production

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II. OPERATIONS SUMMARY

Perch 4 was drilled as a production well through the Perch Monotower by the H.H. Ward drilling rig. The rig was positioned over the monotower on January 30th, 1995.

i. 17-1/2" Hole Section

Perch 4 was spudded at 9:00 hours, February 1st 1995. A 20" conductor was driven to 89m. The conductor was then washed out with a 17-1/2" bit and the hole deepened to 140m using a seawater drilling fluid. The hammer was then picked up and the 20" conductor driven a refusal at 149m. After laying down the hammer and the landing joint the 20" casing was cut and dressed and a 21-1/4" diverter nippled onto the wellhead.

ii. 13-1/2" Hole Section

The 20" hole section was drilled with flocculated seawater mud system. A 13-1/2" directional assembly and Hycalog DS-4OH bit and a Halliburton MWD tool assembly were picked up, function tested and the 20" casing cleaned out to 149m. The rest of the BHA was then picked up and the well was deepened and deviated in 13-1/2" hole. The hole angle was built by motor drilling with slide drilling operations, from 0.17° at 148.5 m to 37.4° with a constant 104° azimuth at 505m. A wiper trip was conducted at that depth to condition the hole with the bit pumped and back reamed to the 20" casing shoe. After running back into the hole the well was motor drilled, slide drilling 70-80% of each stand to 855m with the hole angle built to 63.7° on an azimuth of 104°. From 855m to 886m, slide drilling operations were reduced to 50% to reduce the angle of build. At 876.3m the hole was at 64.3° on an azimuth of 103.4°. The well was subsequently deepened by rotary drilling from 886m to 975m taking surveys every stand. A wiper trip was conducted at 975m to condition the hole. The bit was pumped and backreamed to the casing shoe prior to being run back into the hole. Soft fill was cleaned from the hole from 960-975m and the hole circulated to condition prior to running casing. The bit was then pulled from the hole and the 9-1/2" motor laid down. Prior to running the 10-3/4" casing, the diverter was nippled down and the casing cut. laying down the stub and casing flange. During cutting operations mud in the annulus dropped and was refilled with 20 barrels of sea water. Surface casing equipment was then rigged up and 80 joints of 40.5 lb/ft K-55 casing was run. The cement head was then rigged up and the casing cemented with a 875 sxs lead slurry and 300 tail cement. The 13-5/8" BOP and riser to the well head were then nippled up.

iii. 9-7/8" Hole Section:

After nippling up, the BOP's were successfully pressure tested to 200/3000 psi and 200/1600 psi. A 9-7/8" BHA was picked up and run into the hole with a DBS QP-19L bit. After drilling out the shoe track and cleaning the hole to 975m, the seawater gel mud system was displaced with a KCL/Glycol mud system which was circulated and conditioned. 3m of new formation was then drilled prior to conducting a pressure integrity test indicating an EMW of 16.01ppg. Further circulation of the mud continued while raising the glycol concentration to 3% and PHPA was added. The well was then deepened in 9-7/8" hole from 978m to 1345m taking MWD surveys after each stand. At 1345m the bit was pumped and backreamed in a wiper trip was conducted to the 10-3/4" casing shoe. After running back to bottom, the well was then deepened from 1345m to 1573m taking MWD surveys every stand. A wiper trip was then conducted with the bit pumped and backreamed to the 10-3/4" casing shoe. After running back to bottom, the well was deepened from 1573m to 1740m prior to pulling the bit from the hole.

II. OPERATIONS SUMMARY (cont.)

After pulling the bit from the hole the PDC bit and MWD tools were laid down and the Anadrill LWD tool assembly was picked up with a new Reed HP-51A 9-7/8" rock bit. The Halliburton MWD tools were then picked up, function tested and run into the hole. After slipping and cutting drill line at the casing shoe, the bit was run to 1720m prior to precautionary reaming to 1740m. The well was then deepened from 1740m to 1784m with a constant 25-33 klbs on the bit. From 1784m to 1890m, the well was deepened by controlled drilling at no greater than 15 metres/hour in an effort to optimise Anadrill LWD data. MWD surveys were conducted after every stand. The top Latrobe Formation, Coarse Clastics and N1 Coal were drilled out, prior to conducting a wiper trip to condition the hole at 1890m. The bit was backreamed and pumped to the casing shoe prior to being run back into the hole and precautionary reamed from 1861-1890m. The well was then deepened from 1890-1969m at normal penetration rates with MWD surveys conducted every stand. At 1969m, within the fractured top of the N2 coal, lost circulation was experienced with initial losses while circulating, running at 100 bbl/hr. To counter losses, a pill containing mica and kwikseal lost circulation material was spotted on bottom and allowed to soak while the bit was pulled to 5 stands from bottom and the hole circulated.

After curing lost circulation problems, the bit was run back to bottom and the well was deepened by controlled drilling from 1969-2052m conducting MWD surveys every stand. Rates of penetration were restricted to a maximum of 15m/hr to optimise the quality of the LWD log. A total depth of 2052m was reached at 20:30 hours on 11/02/95. A wiper trip to the casing shoe at 962m was conducted at that depth and the bit pulled from the hole. Tight hole and bridges were encountered during the course of the wiper trip.

At surface, the Anadrill tools were laid down and the data downloaded, and the Sperry Sun adjustable stabiliser and Halliburton MWD tool assembly laid down, prior to rigging up Schlumberger tools for logging suite #1. Logs attempted were; DLL-MSFL-AS-GR-CNL-LDL-AMS. In the event, the tools would not pass below the high angle hole within the casing at 860 m and after attempts at working them lower, they were pulled from the hole for assessment of the tool configuration. Three CMEZ centralisers were removed and the tool string was run back into the hole. On the second attempt, the tool string was unable to pass below 850m, and after attempting to work it deeper, was pulled from the hole and Schlumberger rigged down.

Anadrill's CDN and CDR tools were picked up and run into the hole in the BHA above the re-run Reed HP-51A bit and logging operations were conducted during reaming operations by that company. The logged interval was 1600-2052m with reaming speeds maintained below 60 m/hr in the main hole section and below 15 m/hr in the zones of interest from 1800-1850m, and 1935-2000m. On completion of logging operations the bit and LWD tools were puled from the hole, laid down and the data downloaded. The surface casing equipment was rigged up prior to running 7-5/8" casing which comprised a total of 169 joints of 26.4# L-80 LTC grade. The cement head and surface lines were then rigged up, pressure tested, the cross over tightened and re pressure tested to 3000 psi and the casing cemented with 750 sacks of neat cement with 0.223 gallons/ sack of Halad 322 LS for lost circulation control. Surface pressures indicated possible lost circulation problems during displacement of the cement with seawater and subsequent attempts to bump the plug. Surface cementing equipment was rigged down, the well head cleaned and drillpipe laid down prior to commencing Schlumberger cased hole logs.

II. OPERATIONS SUMMARY (cont.)

Schlumberger cased hole logs comprised; AS-GR-CCL-AMS/ VSP. The top of the cement inside the 7-5/8" casing was tagged at 1572m and the Array sonic logged from that depth to 150m. There was no indication from the AMS temperature log of cement outside the casing above that depth. It was deemed necessary to drill out the cement and the drillpipe on deck had couplings with an OD in excess of the ID of the casing. Whilst waiting on replacement drillpipe. 112 stands of 5" drillpipe were laid down and the 4-1/2" tubing joints picked up and made into stands.

The BOPs were then tested to 200/3000 psi prior to making up a 6-1/2" PDC bit with a 7-5/8" casing scraper, 3-1/2" heavy weight drillpipe and 3-1/2" drillpipe and running into the hole. The top of the ratty cement was intersected at 1580 and drilled to 1592 m where hard cement was intersected. The seawater in the hole was displaced with mud at this point. Hard cement was then drilled from 1592-1930 m, prior to displacing the hole with seawater and pulling the bit from the hole for a second attempt at acquiring cased hole logs. Logs run were CET-CBL-GR-AMS. No cement was seen outside the casing above 1931m and logs were run up to 1700m. A gyro survey was then conducted by gyrodata on Schlumberger's wireline prior to rigging down. In the absence of cement bond no array sonic or seismic survey were conducted over this interval.

III. CASING DATA

SIZE (in)	WEIGHT (lb/ft)	GRADE	CONNECTION	INTERVAL (m MDRT)	SHOE DEPTH (m MDRT)
20	129	X-56	RL-45	24 - 149	149
10.75	40.5	K-55	BTC	23 - 962	962
7.625	26.4	L-80	LTC	23 - 2039	2039

CASING (OD)	10.75''	7.625'' Primary	7.625'' Remedial
SETTING DEPTH (mMDRT)	962	2039	1854
LEAD SLURRY			
Volume Pumped (sx)	875		
Weight (ppg) Additives	12.5		
Econolite (gal/sk)	0.55		
Mixwater (FW) (gal/sk)	11.8		
Yield (ft ³ /sk)	2.05		
TAIL SLURRY		· · · · · · · · · · · · · · · · · · ·	
Volume Pumped (sx)	300	750	500
Weight (ppg)	15.8	15.8	15.8
Additives			
Halad 322L (Fluid Loss) (gal/10bbl)		18	16
Mixwater (gal/sk)	5	5	5
Yield (ft ³ /sk)	1.15	1.15	1.15
BUMP PLUG?	Yes	No	
CALCULATED TOC (mMDRT)	Surface	1968	1500
GROUT			
Volume (sx)	150		
Weight (ppg)	15.8		
CaCl (% BWOC)	2		

IV. CEMENTING DATA

V. SAMPLES

Cuttings

Three Sets of washed and dried cuttings samples were collected at 10 metre intervals from 150 to 1650m MDRT and 5 metre intervals from 1650 to 2052m MDRT. Cuttings descriptions are contained in Appendix 4.

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VI. LOGS AND SURVEYS

Due to high angle hole, wireline logging tools were unable to pass below the casing shoe and therefore no open hole wireline logs were acquired. Logging while drilling (LWD) and cased hole logs were run as follows;

Survey	Company	Top (m MDRT)	Bottom (m MDRT)						
LWD									
MWD (Directional)	Halliburton	170.5	2007.7						
CDR-CDN (Reaming)	Schlumberger/Anadrill	1600.0 2052.0							
	Cased Hole								
AS-GR-AMS	Schlumberger	150.0	1572.0						
CET-CBL-GR-AMS	Schlumberger	1700.0	1931.0						
Gyro (Directional)	Gyrodata	110.0	1915.0						

No temperature plot was possible due to the inability to get wireline logging tools into the open hole.

V. FORMATION RESERVOIR TOPS

Formation/ Zone				m MDRT	m TVT Net Oil Sand		
	Predicted	Actual*	Difference		Predicted	Actual	
Top of Lakes Entrance	976	975.3	0.7 high	1510.0			
Top of Latrobe Group (TOL)	1094	1097.0	3.0 low	1768.0	11.5	10.5	
Top of Coarse Clastics (TCC)	1120	1120.7	0.7 low	1814.5			
Original OWC	1132	1132.0		1835.9			
Total Depth		1256.5		2052.0			

VI. GEOLOGICAL ANALYSIS

Objectives

The proposed Perch-4 was a longreach well, located 1206m ESE of Perch-3 & Perch monotower and 171m ESE of Perch-2. The well was designed to produce from the N1 reservoir in the eastern fault block of Perch in a crestal position approximately 3m updip from Perch-2. Perch-2 intersected 12.5m gross sand with 8.8m net oil column and an original OWC of 1132mTVDSS, which is interpreted as the field OOWC common with the western fault block (encountered in Perch-1).

Cored N1 Sand in Perch-1 and 2 is quartzose, medium-very coarse grained, massive and containing glauconite. It is interpreted to be of upper shoreface facies and is of consistent quality and similar thickness in Perch-1, 2 and 3 with a slight thickening from Perch-3 and 2 off flank to Perch-1.

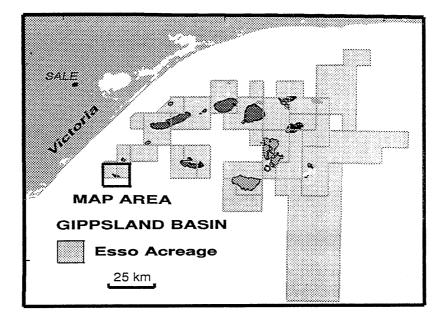
Results

Perch-4 intersected the TCC (top N1 Reservoir) 1120.5mTVDSS, 2.5m TVD updip of Perch-2, and 0.7m TVD low to prognosis. The well intersected 10.5m TVT gross sand with 10.5m TVT net oil column in the N1 reservoir. The upper 2.3m TVT is of poorer quality due to pyritisation and mixing of iron-rich glauconitic, silty Gurnard Fm, possibly due to localised subaerial exposure and bioturbation at the crest of the palaeo-high. The current OWC is within a 1m siltstone between a LPO at 1131.0m TVDSS and a HPW at 1132.0m TVDSS. The up to 1m rise in current OWC from the original OWC at 1132.0m TVDSS confirms that some oil from east Perch has been produced at Perch 3 via fault leak, as prognosed.

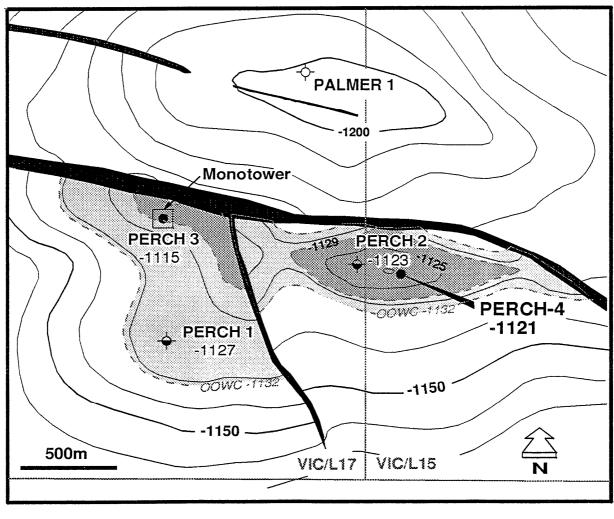
Reservoir quality was good with an average porosity of 31.0% below the upper mineralised zone and an Sw of 13.6%. The upper 2.3m thick, mineralised zone has an average porosity of 20.5% and an Sw of 39.9%.

Perch-4 was initially perforated over the interval 1811.5m to 1821.5mMDRT (1120.5m to 1125.2m TVDSS) and flowed at an initial rate of 8178 BOPD with 0% water cut and a THP of 167psi. Due to the comingling of produced oil from both Dolphin and Perch fields in the one flowline,the minimum pressure requirements for dual flowing of oil from both fields was not met by this initial flow pressure. Therefore, the N1 reservoir was re-perforated over a larger interval of the 31% porosity sand to increase PI and flowing pressure. Re-perforation over the interval 1815.5-1825.5mMD (1122.2-1127.2mTVDSS) resulted in a final flow rate of 6473BOPD at 19% water cut and 199psi THP, which met the flowline minimum requirements.



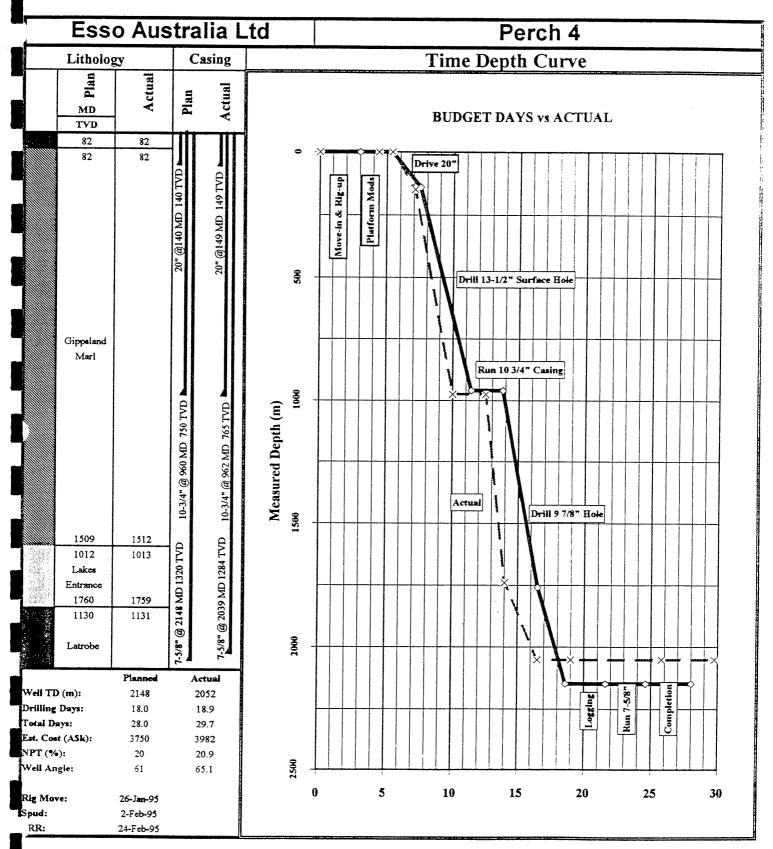


PERCH-4 Location Map Depth Structure @ Top of Coarse Clastics

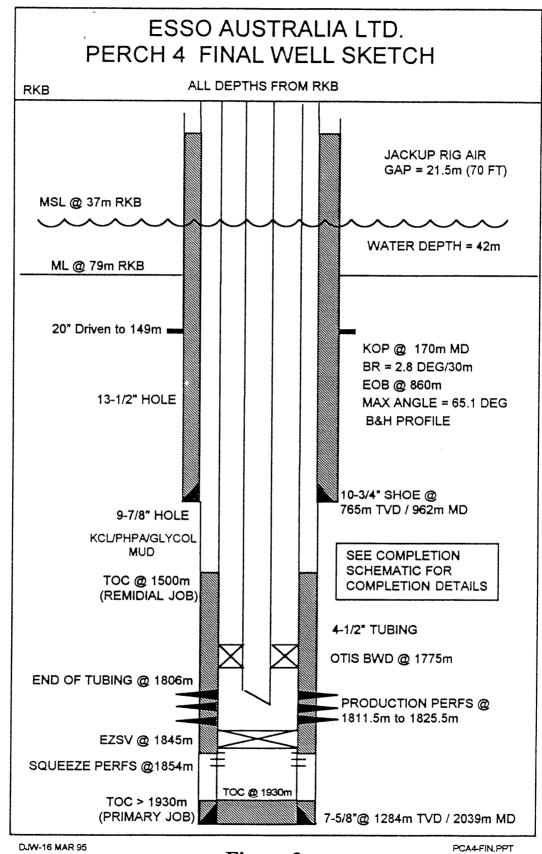


GPV01426 21/8/95

Figure 1









SCHEMATIC	DESCRIPTION	OD	MIN ID	LENGTH	1	
	Tubing Conn.: EUE unless marked other	(in)	(in)	(m)	TOP(m)	TOP(n
	RT to top of tubinghead flange			23.00		
	1 Cooper 13-5/8" MC-2 Snapring Tubing Hanger, 645256-32-46	13.292	3.900	0.36	23.00	
	2 X-over pup joint 4-1/2" VAM ACE to 4-1/2" 12.75# EUE, J-55, PxP	4.500	3.958	1.71	23.36	
	3 2 Pup joints, 2.48m and 2.47m, 4-1/2" 12.75# J-55	4.500	3.958	4.95	25.07	
	4 Tubing, 4-1/2" 12.75#, J-55	4.500		266.04	30.02	
17. E. J.	5 2 Pup joints, 1.86m and 1.86m, 4-1/2" 12.75# J-55	4.500		3.72	296.06	
(1) x ≠ (1)	6 Flow Coupling, 6ft, 4-1/2", 811FN38105	5.614		1.83	299.78	
	7 SSV Landing Nipple 4-1/2" Otis XXO, 711XXO38115 8 Flow Coupling, 6ft, 4-1/2", 811FN38105	5.619	4	0.70	301.61	300
	9 Pup joint, 6ft, 4-1/2" 12.75# J-55	4.500		1.83 1.86	302.31 304.14	
A , k	10 Tubing, 4-1/2" 12.75#, J-55	4.500	1	364.35	306.00	1
:	11 Pup joint, 6ft, 4-1/2" 12.75# J-55	4,500		1.85	670.35	
a contraction of the contraction	12 Blast Joint, 10ft, 4-1/2", 811BN38101	5.560		2.98	672.20	
b	13 Side Pocket Mandrei, Camco MMRG-2, 1-1/2" GLV, RK latch	6.625	3.833	2.81	675.18	614
	14 Pup joint, 6ft, 4-1/2" 12.75# J-55	4.500	3.958	1.70	677.99	
	15 Tubing, 4-1/2" 12.75#, J-55	4.500	3.958	451.16	679.69	
	16 Pup joint, 6ft, 4-1/2" 12.75# J-55	4.500	3.958	1.85	1130.85	
	17 Blast Joint, 10ft, 4-1/2", 811BN38101	5.560	3.970	2.98	1132.70	
(18) E	18 Side Pocket Mandrel, Camco MMRG-2, 1-1/2" GLV, RK latch	6.625	3.833	2.81	1135.68	841
	19 Pup joint, 6ft, 4-1/2" 12.75# J-55	4.500	3.958	1.71	1138.49	
	20 Tubing, 4-1/2" 12.75#, J-55	4.500	3.958	326.33	1140.20	
	21 Pup joint, 6ft, 4-1/2" 12.75# J-55	4.500	3.958	1.87	1466.53	
	22 Blast Joint, 10ft, 4-1/2", 811BN38101	5.560	3.970	2.98	1468.40	İ
	23 Side Pocket Mandrel, Camco MMRG-2, 1-1/2" GLV, RK latch	6.625	3.833	2.81	1471.38	995
	24 Pup joint, 6ft, 4-1/2" 12.75# J-55	4.500	3.958	1.72	1474.19	
	25 Tubing, 4-1/2" 12.75#, J-55, 1 joint	4.500	3.958	9.60	1475.91	
	26 Landing Nipple, "R" , 4-1/2", 3.688 pkg bore, 11R36826	5.619	3.688	0.33	1485.51	1001
38 - 1	27 Tubing, 4-1/2" 12.75#, J-55	4.500	3.958	287.11	1485.84	
26 R	28 Xover 4-1/2" EUE box to 3-1/2" EUE pin	4.500	2.992	0.16	1772.95	
	29 Pup joint, 6ft, 3-1/2" 9.3.# J-55 EUE	3.500	2.992	1.85	1773.11	
	30 X-over 3-1/2" EUE box to 3-1/2" VAM ACE pin	3.500	2.992	0.28	1774.96	
	31 BWD Packer Seal Stinger	4.470	2.970	0.18	1775.24	
	31A Straight Slot Locator, 212S40008-A	4.470	2.970	(0.5)		
	31B Seal Unit 212RTR40004-A, Seal Unit Extension 212X40000-A, Two Seal Units, Muleshoe Guide 212G40000-A	4.018	2.970	(2.38)		
	32 Wireline Set Packer, Otis BWD 7-5/8" by 3-1/2", 212BWD7540-A	6.375	4.000	0.94	1775.42	1138
	33 Seal Bore Extension 4-3/4" 8 UN Pin by Pin, 212C7060	5.032	4.000	2.28	1776.36	1150
	34 Millout extension 4-3/4" 8 UN Box by Box, 812MOE40002	5.600	4.350	2.44	1778.64	
	35 Xover, 4-3/4" UN Pin by 3-1/2" EUE Pin, 892PPC43002	4.772	3.003	0.11	1781.08	
	36 Pup joint, 6ft, 3-1/2" 9.3.# J-55 EUE	3.500	2,992	1.86	1781.19	
	37 Joint of tubing, 3-1/2" 9.3# J-55 EUE	3.500	2.992	9.62	1783.05	
.a	38 Landing Nipple, "XN", 2.75" pkg bore with 2.635" nogo		2.635	0.44	1792.67	1146
	39 12 foot Perforated Pup Joint, 3-1/2" 9.3# J-55 EUE	3.500	2.992	3.70	1793.11	
	40 Joint of tubing, 3-1/2" 9.3# J-55 EUE	3.500	2.992	9.59	1796.81	
	41 Xover, 3-1/2" EUE Box by 4-1/2" EUE Pin	4.500	2.992	0.23	1806.40	
(38) XN	42 Pup joint, 6ft, 4-1/2" 12.75# J-55	4,500	3.958	1.87	1806.63	
0 0	43 Top of Schlumberger SAXR automatic gun release	5.200	4.000	0.70	1808.50	1155
3	Bottom of completion				1809.20	
	A PERFORATIONS 1811.5 to 1821.5 mdkb, Schlumberger 4-1/2" 5 spf				1811.50	1156
	TCP and 1815.5 to 1825.5 mdkb with 2-1/8" 6 spf Enerjets. 44 Schlumberger TCP gun fish 15.01m. Bottom SAXR 2.21, 4-1/2" Spacer	5.200		15.01		
1	2.56m, 4-1/2" Gun 10m, Roller/builnose 0.24. 45 Halliburton 7-5/8" EZSV Cement Retainer 0.804 m long, 802.351				1845.00	1174
	B Perforations for remedial cementing of production casing 1854 to 1854.6				1854.00	
	mdkb, 3-3/8" 6 spf 60 deg. phasing Schlumberger HSD	10.755	10.050			765
	Surface Casing, 10 3/4", 40.5 lb/ft, K-55 Butt 61 jts	10.750	10.050	939.00	962.00	765 1286
	Production Casing, 7 5/8", 26.4lb/ft, N-80.	7.625	6.875	2016.00	2039.00	1200
	Top of cement outside production casing, 1500 metres. PBTD 1930 mdkb					
ESSO	PERCH 4 Completion.	Appr.	No. Date 0 9/94			
				COMP	ENTO	
	Wellhead			COMM		
	Type: Cooper, MC-2 Compact Wellhead		•	23rd Februa	ary 1995.	
	Xmas Tree Cap: 7-1/16" API 3000 psi WP R45 Xmas Tree Bore: 4-1/8"	Average Max. ang	-	50.7 65.11 at 95) mdkb	

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Figure 4

APPENDIX 1

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APPENDIX 1

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PERCH-4

Survey Data

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for

ESSO AUSTRALIA LIMITED

HARVEY H. WARD, BLOCK VIC/L15, WELL PERCH 4

7 5/8" CASING SURVEY - DEFINITIVE RESULTS

te Run: 19-FEB-95 00:51:24

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Job Number: AU02956269

Iculation Method: MINIMUM CURVATURE

Survey Latitude: 38.5700deg S

imuths Corrected .2010deg EAST to Grid North

Proposed Well Aziauth: 104.3600deg

mrtical Section Calculated from Well Head Location

osure Calculated from Well Head Location

Horizontal Coordinates Calculated from Local Horizontal Reference

- AUSTRALIA LIMITED VEY H. WARD, BLOCK VIC/L15, WELL PERCH 4 3" CASING SURVEY - DEFINITIVE RESULTS Number: AU02956269

MEAS	INCL	AZIMUTH	VERT	HORIZO				VERT	DOG-LEG
DEPTH			DEPTH	COORDIN				SECTION	SEVERITY
	deg	deg	2	aeters		<u>0</u>	deg	8	deg/30a
79.0	. 00	. 00	79.0	.00 N	.00 E	.0	.0	. 0	. 00
			ASSUMED VE	RTICAL TO SEABED	AT 79.0 METRE	S B.R.T.			
110.0	.03	64.62	110.0	.00 N	.01 E	.0	64.6	.0	.03
140.0	. 08	114.86	140.0	.00 S	.04 E	.0	93.0	.0	.07
170.0	.28	140.21	170.0	.07 S	.10 E	.1	123.5	.1	.21
200.0	2.39	120.26	200.0	.44 S	.69 E	.8	122.5	.8	2.13
230.0	5.64	111.90	229.9	1.31 S	2.60 E	2.9	116.6	2.8	3.29
260.0	9.48	110.47	259.6	2.72 5	6.28 E		113.4	6.8	3.85
290.0	13.50	107.40	289.0	4.63 S	11.94 E		111.2	12.7	4. Đồ
320.0	16.27	103.67	318.0	6.67 S	19.36 E		109.0	20.4	2.94
350.0	18.87	103.00	346.6	8.76 S	28.18 E	29.5	107.2	29.5	2.60
380.0	21.82	102.45	374.8	11.05 S	38.35 E	39.9	106.0	39.9	2.96
410.0	26.17	103.04	402.2	13.75 S	50.25 E	52.1	105.3	52.1	4.35
440.0	30.16	102.46	428.6	16.87 S	64.05 E	66.2	104.7	66.2	4.01
470.0	33.14	101.42	454.1	20.12 S	79.45 E	82.0	104.2	82.0	3.03
500.0	36.82	101.48	478.7	23 . 53 S	96.31 E		103.7	99.1	3.68
530.0	39.35	102.63	502.3	27.40 S	114.40 E	117.6	103.4	117.6	2.63
560.0	38.72	103.67	525.6	31.70 S	132.80 E	136.5	103.4	136.5	.91
590.0	38.36	102.98	549.1	36.00 S	150.99 E	155.2	103.4	155.2	.56
620.0	38.36	102.32	572.6	40.08 S	169.15 E	173.8	103.3	173.8	. 41
650.0	41.11	102.02	595.7	44.12 S	187.90 E	193.0	103.2	193.0	2.75
680.0	46.09	102.07	617.4	48.44 S	208.13 E	213.7	103.1	213.6	4.98
710.0	47.77	103.96	637.9	53.38 5	229.48 E	235.6	103.1	235.5	2.17
740.0	50.75	103.03	657.5	58.68 S	251.58 E	258.3	103.1	258.3	3.06
770.0	54.54	102.03	675.7	63.85 S	274.85 E	282.2	103.0	282.1	3.86
800.0	58.01	102.00	692.3	69.04 S	299.25 E	307.1	102.9	307.0	3.47

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SSOLUSTRALIA LIMITED PEY H. WARD, BLOCK VIC/L15, WELL PERCH 4 CASING SURVEY - DEFINITIVE RESULTS Defen: AU02956269

MEAS	INCL	AZIMUTH	VERT	HORIZO	NTAL	CLOS	URE	VERT	DOG-LEG
DEPTH			DEPTH	COORDI	NATES	DISTANCE	AZIMUTH	SECTION	SEVERITY
	deg	deg		∎eter	5		deg	1	deg/30 s
830.0	61.48	102.13	707.4	74.46 S	324.59 E	777 B	102.9	332.9	3.47
860.0	64.42	101.63	721.1	79.96 S	350.73 E	359.7		359.6	2.98
890.0	63.89	102.08	734.1	85.50 5	377.16 E	386.7	102.7	386.6	.67
920.0	64.43	101.67	747.2	91.06 S	403.58 E	413.7	102.7	413.6	.66
950.0	65.11	101.23	760.0	96.44 S	430.18 E	440.9	102.6	440.7	.78
980.0	64.80	101.74	772.7	101.85 S	456.81 E	468.0	102.5	467.8	.55
1010.0	64.17	102.42	785.6	107.52 S	483.29 E	495.1	102.5	494.9	.88
1040. 0	63.39	102.15	798.9	113.24 S	509.58 E	522.0	102.5	521.7	.81
1070.0	63.65	102.61	812.3	119.00 S	535.81 E	548.9	102.5	548.6	. 48
1100.0	63.77	102.78	825.6	124.91 S	562.05 E	575.8	102.5	575.5	.20
1130.0	63.60	103.09	838.9	130.93 5	588.26 E	602.7	102.5	602.4	. 33
1160.0	62.98	103.28	852.3	137.05 S	614.35 E	629.5	102.5	629.1	.64
1190.0	63.47	103.72	865.9	143.30 S	640.40 E	656.2	102.6	655.9	.62
1220.0	63.09	103.49	879.3	149.60 S	666.44 E	683.0	102.6	682.7	.43
1250.0	62.75	103.72	893.0	155.88 S	692.40 E	709.7	102.6	709.4	. 39
1280.0	62.96	103.69	906.7	162.20 S	718.34 E			736.1	.21
1310.0	62.72	103.59	920.4	168.50 S	744.28 E	763.1	102.7	762.8	.26
1340.0	62.56	103.74	934.2	174.90 S	770.17 E	789.8	102.7	789.5	.21
1370.0	63.08	104.06	947.9	181.21 S	796.07 E	816.4	102.8	816.1	. 59
1400.0	63.10	104.25	961.5	187.75 S	822.01 E	843.2	102.8	842.9	. 17
1430.0	62.41	104.02	975.2	194.26 S	847.88 E	869.8	102.9	869.6	.72
1460.0	62.13	104.32	989.1	200.76 S	873.62 E	896.4	102.9	896.1	. 39
1490.0	62.43	104.40	1003.1	207.34 S	899.35 E	922.9	102.9	922.7	.31
1520.0	62.79	104.47	1016.9	213.99 S	925.14 E	949.6	103.0	949.3	.37
1550.0	62.44	104.68	1030.7	220.69 S	950.93 E	976.2	103.0	975.9	. 40

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D AUSTRALIA LIMITED
#EY H. WARD, BLOCK VIC/L15, WELL PERCH 4
B" CASING SURVEY - DEFINITIVE RESULTS
Number: AU02956269

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MERS DEPTH	INCL	AZIMUTH	VERT DEPTH	HORIZO COORDI areter	NATES	C L O S DISTANCE ₽		VERT SECTION	DOG-LEG SEVERITY deg/30∎
	deg	deg		# C U C 1	3	•	059	•	013,005
1580.0	62.09	104.54	1044.7	227.39 S	976.62 E	1002.7	103.1	1002.5	.37
1610.0	62.49	104.98	1058.6	234.15 S	1002.30 E	1029.3	103.1	1029.1	.56
1640.0	62.37	104.95	1072.5	241.02 S	1027.99 E	1055.9	103.1	1055.7	.12
1670.0	61.93	104.97	1086.5	247.87 S	1053.62 E	1082.4	103.2	1082.2	.44
1700.0	61.11	105.08	1100.8	254.70 S	1079.09 E	1108.7	103.2	1108.5	.83
1730.0	61.02	105.09	1115.3	261.54 S	1104.44 E	1135.0	103.3	1134.8	. 09
1760.0	60.21	105.60	1130.1	268.45 S	1129.64 E	1161.1	103.3	1160.9	.92
1790.0	59.61	106.02	1145.1	275.52 S	1154.62 E	1187.0	103.4	1186.9	.71
1820.0	58.36	106.22	1160.6	282.66 S	1179.32 E	1212.7	103.4	1212.6	1.26
1850.0	56.56	106.67	1176.7	289.82 S	1203.57 E	1238.0	103.5	1237.8	1,83
1880.0	55.72	107.17	1193.4	297.08 S	1227.40 E	1262.8	103.6	1262.7	.94
1910.0	55.32	107.36	1210.4	304.42 S	1251.02 E	1287.5	103.6	1287.4	.43
1915.0	55.17	107.39	1213.2	305.64 S	1254.94 E	1291.6	103.6	1291.5	. 88

Final Station Closure: 1291.6 meters 103.6880 degrees

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GYRODATA FINAL REPORT JOB NO.AU0295G269

EQUIPMENT REPORT

CLIENT

ESSO AUSTRALIA LIMITED LOCATION: HARVEY H. WARD WELL NO : PERCH 4, 7 5/8" CASING SURVEY DATE : 19 FEBRUARY 1995

GRID CORRECTION : 0.2010 E TO GRID NORTH REF. CO-ORDINATES : N = 0.00 Metres E = 0.00 Metres

General Remarks

A Gyro Multi-shot Survey was performed in Well PERCH 4 in the 7 5/8" Casing. The survey was performed from a depth of 1915.0 metres RKB Harvey H. Ward and tied onto seabed at 79.0 metres.

Downhole Electronics

Surface Electronics

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Primary

Tool No. 934

Gyro Section	:	A0005	Compaq :	:	A0052
Data Section	:	C0017	Power Supply :	:	A0057
Power Section	:	C0010	Printer :	:	A0043

Backup

Tool No. 702

Gyro Section	:	A0016	Compaq	:	A0066
Data Section	:	C0004	Power Supply	:	A0059
Power Section	:	C0002	Printer	:	A0106

Running Gear

Pressure barrel, Heatshield, Sinker bars, Roller bars, Springbow, Wear bushings.

Total Length of Tool : 11.00 METRES

Maximum O.D. : 3.70 INCHES

GYRODATA FINAL REPORT JOB NO.AU0295G269

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WELL DETAILS

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OPERATOR	.ESSO AUSTRALIA LIMITED
INSTALLATION	.HARVEY H. WARD
WELL NO	.PERCH 4
CASING SIZE	.7 5/8" CASING SURVEY

SURVEY DETAILS

DATE OF SURVEY	19 FEBRUARY 1995
ENGINEER	A.LINDIE/J.COLLINS
OUTRUN SURVEY INTERVAL	30 Metres
MAXIMUM GYRO TEMPERATURE	78.30 Deg. C
MAXIMUM AMBIENT TEMPERATURE	
MAXIMUM INCLINATION	
AVERAGE AZIMUTH	
SURVEY DEPTH	
SURVEY TIED ONTO	SEABED at 79.0 metres RKB
	Harvey H. Ward

WIRELINE DETAILS

WIRELINE COMPANY	SCHLUMBERGER
CABLE TYPE	MULTI-CONDUCTOR
CABLE SIZE	15/32"
WIRELINE COUNTER READING AT END	-
OF SURVEY	1.5 METRES

CALIBRATION DETAILS

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BOTTOM LINE COMPARISONS

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	M.D.	INCL.	AZ.	TVD	N	E
GYRODATA HES MWD (Interplted)				1213.20 1211.12		

LATERAL	DIFFERENCE	=	5.55	metres	(2.89	M/K)
TVD	DIFFERENCE	=	2.08	metres	(1.09	M/K)

APPENDIX 2

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APPENDIX 2

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PERCH-4

MD - TVD Data Listing

Perch-4 MD-TVD Survey Data Listing

and the second
MD 0.0	Angle 0.0	Direction	TVDRT	TVDSS	DNorth	DEast	Northing	Easting
5.0 10.0	0.0 0.0 0.0	0.0 0.1 0.3	0.0 5.0 10.0	-37.0 -32.0 -27.0	0.0 0.0 0.0	0.0 0.0 0.0	5730813.9 5730813.9 5730813.9	527973.0 527973.0 527973.0
15.0 20.0	0.0 0.0	• 0.4 0.6	15.0 20.0	-22.0 -17.0	0.0 0.0	0.0 0.0	5730813.9 5730813.9	527973.0 527973.0
25.0 30.0	0.0 0.1	0.7 0.9	25.0 30.0	-12.0 -7.0	0.0 0.0	0.0 0.0	5730813.9 5730813.9	527973.0 527973.0
35.0 40.0	0.1 0.1	1.0 1.2	35.0 40.0	-2.0 3.0	0.0 0.0	0.0 0.0	5730813.9 5730813.9	527973.0 527973.0
45.0 50.0 55.0	0.1 0.1 0.1	1.3 1.4 1.6	45.0 50.0 55.0	8.0 13.0 18.0	0.0 0.0 0.0	0.0 0.0 0.0	5730814.0 5730814.0	527973.0 527973.0 527973.0
60.0 65.0	0.1 0.1	1.0 1.7 1.9	60.0 65.0	23.0 28.0	0.0 0.1 0.1	0.0 0.0	5730814.0 5730814.0 5730814.0	527973.0 527973.0 527973.0
70.0 75.0	0.1 0.1	2.0 2.2	70.0 75.0	33.0 38.0	0.1 0.1	0.0 0.0	5730814.0 5730814.0	527973.0 527973.0
80.0 85.0	0.1 0.2	33.8 191.1	80.0 85.0	43.0 48.0	0.1 0.1	0.0 0.0	5730814.0 5730814.0	527973.0 527973.0
90.0 95.0 100.0	0.2 0.1 0.1	348.5 176.5 4.6	90.0 95.0 100.0	53.0 58.0 63.0	0.1 0.1 0.1	0.0	5730814.0 5730814.0	527973.0 527973.0
105.0 110.0	0.1 0.0	34.6 64.6	100.0 105.0 110.0	68.0 73.0	0.1 0.2	0.0 0.0 0.0	5730814.1 5730814.1 5730814.1	527973.0 527973.0 527973.0
115.0 120.0	0.0 0.1	73.0 81.4	115.0 120.0	78.0 83.0	0.2	0.0 0.0	5730814.1 5730814.1	527973.0 527973.0
125.0 130.0	0.1 0.1	89.7 98.1	125.0 130.0	88.0 93.0	0.2 0.2	0.0 0.0	5730814.1 5730814.1	527973.0 527973.0
135.0 140.0 145.0	0.1 0.1 0.1	106.5 114.9 119.1	135.0 140.0 145.0	98.0 103.0 108.0	0.2 0.1 0.1	0.0 0.0 0.0	5730814.1 5730814.1	527973.0 527973.0
150.0 155.0	0.2 0.2	123.3 127.5	150.0 155.0	113.0 118.0	0.1 0.1	0.0 0.0 0.1	5730814.1 5730814.1 5730814.0	527973.0 527973.0 527973.1
160.0 165.0	0.2 0.3	131.8 136.0	160.0 165.0	123.0 128.0	0.1 0.1	0.1 0.1	5730814.0 5730814.0	527973.1 527973.1
170.0 175.0	0.3 0.6 1.0	140.2 136.9	170.0 175.0	133.0 138.0	0.1 0.1	0.1 0.1	5730814.0 5730814.0	527973.1 527973.1
180.0 185.0 190.0	1.3 1.7	133.6 130.2 126.9	180.0 185.0 190.0	143.0 148.0 153.0	0.0 -0.1 -0.1	0.2 0.3 0.4	5730813.9 5730813.9 5730813.8	527973.2 527973.3 527973.4
195.0 200.0	2.0 2.4	123.6 120.3	195.0 200.0	158.0 163.0	-0.2 -0.3	0.5 0.7	5730813.7 5730813.6	527973.5 527973.7
205.0 210.0	2.9 3.5	118.9 117.5	205.0 210.0	168.0 173.0	-0.4 -0.5	0.9 1.1	5730813.5 5730813.4	527973.9 527974.1
215.0 220.0 225.0	4.0 4.6	116.1 114.7	215.0 220.0	178.0 183.0	-0.7 -0.8	1.4 1.8	5730813.2 5730813.1	527974.4 527974.8
230.0 235.0 235.0	5.1 5.6 6.3	113.3 111.9 111.7	224.9 229.9 234.9	187.9 192.9 197.9	-1.0 -1.2 -1.4	2.2 2.6 3.1	5730812.9 5730812.8 5730812.6	527975.2 527975.6 527976.1
240.0 245.0	6.9 7.6	111.4 111.2	239.9 244.8	202.9 207.8	-1.6 -1.8	3.6 4.2	5730812.4 5730812.1	527976.6 527977.2
250.0 255.0	8.2 8.8	111.0 110.7	249.8 254.7	212.8 217.7	-2.0 -2.3	4.8 5.5	5730811.9 5730811.6	527977.8 527978.5
260.0 265.0 270.0	9.5 10.2 10.8	110.5 110.0 109.5	259.7 264.6 269.5	222.7 227.6 232.5	-2.6 -2.9 -3.2	6.3 7.1	5730811.3 5730811.1	527979.3 527980.1
275.0 280.0	11.5 12.2	103.5 108.9 108.4	209.5 274.4 279.3	232.5 237.4 242.3	-3.2 -3.5 -3.8	7.9 8.8 9.8	5730810.7 5730810.4 5730810.1	527980.9 527981.8 527982.8
285.0 290.0	12.8 13.5	107.9 107.4	284.2 289.0	247.2 252.0	-4.2 -4.5	10.8 11.9	5730809.8 5730809.4	527983.8 527984.9
295.0 300.0 305.0	14.0 14.4 14.9	106.8 106.2	293.9 298.7	256.9 261.7	-4.8 -5.2	13.1 14.2	5730809.1 5730808.7	527986.1 527987.2
310.0 315.0	15.4 15.8	105.5 104.9 104.3	303.6 308.4 313.2	266.6 271.4 276.2	-5.5 -5.9 -6.2	15.5 16.7 18.0	5730808.4 5730808.1 5730807.7	527988.5 527989.7 527991.0
320.0 325.0	16.3 16.7	103.7 103.6	318.0 322.8	281.0 285.8	-6.5 -6.9	19.4 20.7	5730807.4 5730807.1	527991.0 527992.4 527993.7
330.0 335.0	17.1 17.6	103.5 103.3	327.6 332.4	290.6 295.4	-7.2 -7.6	22.2 23.6	5730806.7 5730806.4	527995.2 527996.6

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Appendix 2

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MD	Angle	Direction	TVDRT	TVDSS	DNorth	DEast	Northing	Easting
340.0	18.0	103.2	337.1	300.1	-7.9	25.1	Northing 5730806.0	Easting 527998.1
345.0	18.4	103.1	341.9	304.9	-8.3	26.6	5730805.7	527999.6
350.0	18.9	103.0	346.6	309.6	-8.6	28.2	5730805.3	528001.2
355.0 360.0	19.4 19.9	102.9 102.8	351.4 356.1	314.4 319.1	-9.0 -9.4	29.8 31.4	5730804.9 5730804.6	528002.8 528004.4
365.0	20.4	102.7	360.8	323.8	-9.7	33.1	5730804.0	528004.4
370.0	20.8	` 102.6	365.4	328.4	-10.1	34.8	5730803.8	528007.8
375.0	21.3	102.5	370.1	333.1	-10.5	36.6	5730803.4	528009.5
380.0 385.0	21.8 22.6	102.5 102.6	374.8 379.4	337.8 342.4	-10.9 -11.3	38.3 40.2	5730803.0 5730802.6	528011.3
390.0	23.3	102.7	384.0	347.0	-11.7	42.1	5730802.2	528013.2 528015.1
395.0	24.0	102.8	388.6	351.6	-12.2	44.0	5730801.7	528017.0
400.0 405.0	24.7 25.5	102.8 102.9	393.1 397.7	356.1	-12.6	46.1	5730801.3	528019.1
405.0	26.2	102.9	402.2	360.7 365.2	-13.1 -13.6	48.1 50.2	5730800.8 5730800.3	528021.1 528023.2
415.0	26.8	102.9	406.6	369.6	-14.1	52.4	5730799.8	528025.4
420.0	27.5	102.9	411.1	374.1	-14.6	54.6	5730799.3	528027.6
425.0 430.0	28.2 28.8	102.8 102.7	415.5 419.9	378.5 382.9	-15.1 -15.7	56.9 59.2	5730798.8 5730798.3	528029.9 528032.2
435.0	29.5	102.6	424.3	387.3	-16.2	61.6	5730797.7	528032.2
440.0	30.2	102.5	428.6	391.6	-16.7	64.1	5730797.2	528037.0
445.0 450.0	30.7 31.2	102.3 102.1	432.9 437.2	395.9 400.2	-17.3	66.5	5730796.7	528039.5
455.0	31.7	102.1	437.2	400.2	-17.8 -18.4	69.0 71.6	5730796.1 5730795.6	528042.0 528044.6
460.0	32.2	101.8	445.7	408.7	-18.9	74.2	5730795.0	528047.2
465.0 470.0	32.6 33.1	101.6	449.9	412.9	-19.4	76.8	5730794.5	528049.8
475.0	33.8	101.4 101.4	454.1 458.3	417.1 421.3	-20.0 -20.5	79.5 82.2	5730794.0 5730793.4	528052.4 528055.1
480.0	34.4	101.4	462.5	425.5	-21.1	84.9	5730792.8	528057.9
485.0	35.0	101.5	466.6	429.6	-21.6	87.7	5730792.3	528060.7
490.0 495.0	35.6 36.2	101.5 101.5	470.6 474.7	433.6 437.7	-22.2 -22.8	90.5 93.4	5730791.7	528063.5
500.0	36.8	101.5	478.7	441.7	-22.8	93.4 96.3	5730791.1 5730790.5	528066.4 528069.3
505.0	37.2	101.7	482.7	445.7	-24.0	99.3	5730789.9	528072.3
510.0 515.0	37.7 38.1	101.9	486.7	449.7	-24.6	102.2	5730789.3	528075.2
520.0	38.5	102.1 102.3	490.6 494.5	453.6 457.5	-25.3 -25.9	105.2 108.3	5730788.7 5730788.0	528078.2 528081.3
525.0	38.9	102.4	498.4	461.4	-26.6	111.3	5730787.4	528084.3
530.0	39.4 39.2	102.6	502.3	465.3	-27.3	114.4	5730786.7	528087.4
535.0 540.0	39.2 39.1	102.8 103.0	506.2 510.1	469.2 473.1	-28.0 -28.7	117.5 120.6	5730786.0 5730785.3	528090.5 528093.6
545.0	39.0	103.2	514.0	477.0	-29.4	123.6	5730784.6	528096.6
550.0	38.9	103.3	517.8	480.8	-30.1	126.7	5730783.8	528099.7
555.0 560.0	38.8 38.7	103.5 103.7	521.7 525.6	484.7 488.6	-30.8 -31.6	129.8 132.8	5730783.1	528102.7 528105.8
565.0	38.7	103.6	529.5	492.5	-32.3	132.8	5730782.4 5730781.6	528105.8
570.0	38.6	103.4	533.4	496.4	-33.0	138.9	5730780.9	528111.9
575.0 580.0	38.5 38.5	103.3 103.2	537.3 541.3	500.3	-33.7	141.9	5730780.2	528114.9
585.0	38.4	103.2	541.3	504.3 508.2	-34.5 -35.2	144.9 148.0	5730779.5 5730778.8	528117.9 528121.0
590.0	38.4	103.0	549.1	512.1	-35.9	151.0	5730778.1	528124.0
595.0	38.4	102.9	553.0	516.0	-36.6	154.0	5730777.4	528127.0
600.0 605.0	38.4 38.4	102.8 102.7	556.9 560.9	519.9 523.9	-37.2 -37.9	157.0 160.1	5730776.7 5730776.0	528130.0 528133.1
610.0	38.4	102.5	564.8	527.8	-38.6	163.1	5730775.3	528136.1
615.0	38.4	102.4	568.7	531.7	-39.3	166.1	5730774.6	528139.1
620.0 625.0	38.4 38.8	102.3 102.3	572.6 576.5	535.6 539.5	-39.9 -40.6	169.2 172.2	5730774.0 5730773.3	528142.1 528145.2
630.0	39.3	102.2	580.4	543.4	-41.3	175.3	5730772.7	528148.3
635.0	39.7	102.2	584.3	547.3	-41.9	178.4	5730772.0	528151.4
640.0 645.0	40.2 40.7	102.1 102.1	588.1 591.9	551.1 554.9	-42.6 -43.3	181.5 184.7	5730771.3 5730770.6	528154.5 528157.7
650.0	41.1	102.0	595.7	558.7	-43.3	187.9	5730769.9	528160.9
655.0	41.9	102.0	599.4	562.4	-44.7	191.1	5730769.3	528164.1
660.0 665.0	42.8 43.6	102.0 102.1	603.1 606.8	566.1 569.8	-45.4 -46.1	194.4	5730768.6	528167.4
670.0	43.0	102.1	610.8	569.8 573.4	-46.1 -46.8	197.8 201.2	5730767.8 5730767.1	528170.8 528174.2
675.0	45.3	102.1	613.9	576.9	-47.6	204.6	5730766.4	528177.6
680.0 685.0	46.1 46.4	102.1 102.4	617.4 620.9	580.4 583.9	-48.3 -49.1	208.1	5730765.6	528181.1
690.0	46.4	102.4	620.9 624.3	583.9 587.3	-49.1 -49.9	211.7 215.2	5730764.9 5730764.1	528184.6 528188.2
			•• •					

 $\frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2} \right) + \frac{1}{2} \left(\frac{1}{2} \right) \right) = \frac{1}{2} \left(\frac{1}{2} \left(\frac{1}{2} \right) + \frac{1}{2} \left(\frac{1}{2} \right) \right) + \frac{1}{2} \left(\frac{1}{2} \right) \left(\frac{1}{2} \right) + \frac{1}{2} \left(\frac{1}{2} \right) \left(\frac{1}{2} \right) + \frac{1}{2} \left(\frac{1}{2} \right) \left(\frac{1}{2} \right) \left(\frac{1}{2} \right) + \frac{1}{2} \left(\frac{1}{2} \right) \left(\frac{1}{2} \right) \left(\frac{1}{2} \right) + \frac{1}{2} \left(\frac{1}{2} \right) + \frac{1}{2} \left(\frac{1}{2} \right)

Appendix 2

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			TIDCC		DE	NT	F = - ('
MD Ang 695.0 46	de Direction	TVDRT 627.7	TVDSS 590.7	DNorth -50.7	DEast 218.7	Northing 5730763.3	Easting 528191.7
700.0 47		631.1	594.1	-51.5	222.3	5730762.4	528195.3
705.0 47		634.5	597.5	-52.4	225.9	5730761.6	528198.9
	'.8 104.0	637.9	600.9	-53.2	229.5	5730760.7	528202.5
	3.3 103.8	641.2	604.2	-54.1	233.1	5730759.8	528206.1
	8.8 103.7	644.5	607.5	-55.0	236.7	5730758.9	528209.7
725.0 49 730.0 49	0.3 ` 103.5 0.8 103.3	647.8 651.1	610.8 614.1	-55.9 -56.8	240.4 244.1	5730758.0 5730757.1	528213.4 528217.1
).3 103.2	654.3	617.3	-57.7	247.8	5730756.3	528220.8
	.8 103.0	657.5	620.5	-58.5	251.6	5730755.4	528224.6
745.0 51	.4 102.9	660.6	623.6	-59.4	255.4	5730754.5	528228.4
750.0 52		663.7	626.7	-60.3	259.2	5730753.6	528232.2
	102.5 102.4	666.8 669.8	629.8 632.8	-61.1 -62.0	263.1 266.9	5730752.8 5730751.9	528236.0 528239.9
765.0 53		672.7	635.7	-62.9	270.9	5730751.1	528243.9
770.0 54		675.7	638.7	-63.7	274.8	5730750.2	528247.8
775.0 55		678.5	641.5	-64.6	278.8	5730749.4	528251.8
780.0 55		681.4	644.4	-65.4	282.9 286.9	5730748.5	528255.9
785.0 56 790.0 56		684.2 686.9	647.2 649.9	-66 <i>.</i> 3 -67.1	280.9	5730747.6 5730746.8	528259.9 528264.0
795.0 57		689.7	652.7	-68.0	295.1	5730745.9	528268.1
800.0 58	102.0	692.3	655.3	-68.9	299.2	5730745.0	528272.2
805.0 58		694.9	657.9	-69.8	303.4	5730744.1	528276.4
810.0 59 815.0 59		697.5 700.1	660.5 663.1	-70.7 -71.6	307.6 311.8	5730743.2 5730742.4	528280.6 528284.8
820.0 60		702.6	665.6	-72.5	316.0	5730741.4	528289.0
825.0 60		705.0	668.0	-73.4	320.3	5730740.5	528293.3
830.0 61		707.4	670.4	-74.3	324.6	5730739.6	528297.6
835.0 62		709.8	672.8	-75.2	328.9	5730738.7	528301.9
840.0 62 845.0 63	102.0 0.0 101.9	712.1 714.4	675.1 677.4	-76.2 -77.1	333.2 337.6	5730737.8 5730736.9	528306.2 528310.6
850.0 63		716.7	679.7	-78.0	341.9	5730735.9	528314.9
855.0 63	.9 101.7	718.9	681.9	-78.9	346.3	5730735.0	528319.3
860.0 64		721.1 723.2	684.1	-79.8 -80.7	350.7 355.1	5730734.1	528323.7 528328.1
865.0 64 870.0 64		725.2	686.2 688.4	-80.7	359.6	5730733.2 5730732.3	528332.6
875.0 64		727.6	690.6	-82.6	364.0	5730731.4	528337.0
880.0 64	.1 101.9	729.8	692.8	-83.5	368.4	5730730.4	528341.4
885.0 64		732.0	695.0	-84.4	372.8	5730729.5	528345.8
890.0 63 895.0 64		734.2 736.4	697.2 699.4	-85.4 -86.3	377.2 381.5	5730728.6 5730727.6	528350.1 528354.5
900.0 64		738.5	701.5	-87.2	385.9	5730726.7	528358.9
905.0 64	.2 101.9	740.7	703.7	-88.2	390.3	5730725.8	528363.3
910.0 64		742.9	705.9	-89.1	394.7	5730724.8	528367.7
915.0 64 920.0 64		745.1 747.2	708.1 710.2	-90.0 -90.9	399.2 403.6	5730723.9 5730723.0	528372.2 528376.6
925.0 64		749.4	712.4	-90.9	408.0	5730722.1	528381.0
930.0 64		751.5	714.5	-92.7	412.4	5730721.2	528385.4
935.0 64		753.7	716.7	-93.6	416.9	5730720.3	528389.8
940.0 64 945.0 65		755.8	718.8	-94.5 -95.4	421.3 425.7	5730719.4 5730718.5	528394.3 528398.7
945.0 65 950.0 65		757.9 760.0	720.9 723.0	-95.4	425.7	5730717.6	528403.2
955.0 65		762.1	725.1	-97.2	434.6	5730716.7	528407.6
960.0 65		764.2	727.2	-98.1	439.1	5730715.8	528412.1
965.0 65		766.3 768.5	729.3 731.5	-99.0 -99.9	443.5 447.9	5730714.9	528416.5 528420.9
970.0 64 975.0 64		708.5	733.6	-100.8	447.9	5730714.0 5730713.1	528425.4
980.0 64		772.7	735.7	-101.7	456.8	5730712.2	528429.8
985.0 64	.7 101.9	774.9	737.9	-102.6	461.2	5730711.3	528434.2
990.0 64 995.0 64		777.0 779.1	740.0 742 <i>.</i> 1	-103.6 -104.5	465.7 470.1	5730710.4 5730709.4	528438.7 528443.1
1000.0 64		781.3	742.1	-104.5	470.1	5730708.5	528447.5
1005.0 64	.3 102.3	783.5	746.5	-106.4	478.9	5730707.5	528451.9
1010.0 64		785.6	748.6	-107.4	483.3	5730706.5	528456.3
1015.0 64 1020.0 63		787.8 790.0	750.8 753.0	-108.3 -109.3	487.7 492.1	5730705.6 5730704.6	528460.7 528465.1
1025.0 63		792.2	755.2	-110.3	496.4	5730703.7	528469.4
1030.0 63	.7 102.2	794.4	757.4	-111.2	500.8	5730702.7	528473.8
1035.0 63		796.7 798.9	759.7 761.9	-112.2 -113.1	505.2 509.6	5730701.8 5730700.8	528478.2 528482.6
1040.0 63 1045.0 63		801.1	764.1	-113.1	509.8	5730699.9	528486.9
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MD Angle	Direction TVDRT		DNorth	DEast	Northing	Easting
1050.0 63.5 1055.0 63.5	102.3 803.4 102.4 805.6	5 768.6	-116.0	518.3 522.7	5730698.9 5730698.0	528491.3 528495.7
1060.0 63.6 1065.0 63.6	102.5 807.8 102.5 810.0			527.1 531.4	5730697.0 5730696.0	528500.1 528504.4
1070.0 63.7 1075.0 63.7	102.6 812.3 102.6 814.5	3 775.3	-118.9	535.8 540.2	5730695.1 5730694.1	528508.8 528513.2
1080.0 63.7	[`] 102.7 816.7	779.7	-120.8	544.6	5730693.1	528517.5
1085.0 63.7 1090.0 63.7	102.7 818.9 102.7 821.1	784.1	-122.8	548.9 553.3	5730692.1 5730691.1	528521.9 528526.3
1095.0 63.8 1100.0 63.8	102.8 823.3 102.8 825.6			557.7 562.0	5730690.1 5730689.2	528530.7 528535.0
1105.0 63.7 1110.0 63.7	102.8 827.8 102.9 830.0	790.8	-125.8	566.4 570.8	5730688.2 5730687.2	528539.4 528543.8
1115.0 63.7	102.9 832.2	2 795.2	-127.8	575.2	5730686.2	528548.2
1120.0 63.7 1125.0 63.6	103.0 834.4 103.0 836.6	5 799.6	-129.8	579.5 583.9	5730685.2 5730684.1	528552.5 528556.9
1130.0 63.6 1135.0 63.5	103.1 838.9 103.1 841.1		-130.8 -131.8	588.3 592.6	5730683.1 5730682.1	528561.3 528565.6
1140.0 63.4 1145.0 63.3	103.2 843.3 103.2 845.6			597.0 601.3	5730681.1 5730680.1	528570.0 528574.3
1150.0 63.2 1155.0 63.1		8 810.8		605.7 610.0	5730679.1 5730678.0	528578.7 528583.0
1160.0 63.0	103.3 852.3	8 815.3	-136.9	614.3	5730677.0	528587.3
1165.0 63.1 1170.0 63.1	103.4 854.6 103.4 856.9	819.9	-139.0	618.7 623.0	5730676.0 5730675.0	528591.7 528596.0
1175.0 63.2 1180.0 63.3	103.5 859.1 103.6 861.4		-140.0 -141.1	627.4 631.7	5730673.9 5730672.9	528600.4 528604.7
1185.0 63.4 1190.0 63.5		826.6	-142.1	636.0 640.4	5730671.8 5730670.8	528609.0 528613.4
1195.0 63.4 1200.0 63.3		831.1	-144.2	644.7 649.1	5730669.7 5730668.7	528617.7 528622.1
1205.0 63.3	103.6 872.6	835.6	-146.3	653.4	5730667.6	528626.4
1210.0 63.2 1215.0 63.2	103.6 874.8 103.5 877.1	840.1	-148.4	657.8 662.1	5730666.6 5730665.5	528630.8 528635.1
1220.0 63.1 1225.0 63.0	103.5 879.3 103.5 881.6			666.4 670.8	5730664.5 5730663.4	528639.4 528643.8
1230.0 63.0 1235.0 62.9		846.9	-151.5	675.1 679.4	5730662.4 5730661.3	528648.1 528652.4
1240.0 62.9 1245.0 62.8	103.6 888.4 103.7 890.7	851.4	-153.6	683.8 688.1	5730660.3 5730659.2	528656.8 528661.1
1250.0 62.8	103.7 893.0	856.0	-155.7	692.4	5730658.2	528665.4
1255.0 62.8 1260.0 62.8	103.7 897.6	860.6	-157.9	696.7 701.0	5730657.1 5730656.1	528669.7 528674.0
1265.0 62.9 1270.0 62.9	103.7 899.9 103.7 902.1		-158.9 -160.0	705.4 709.7	5730655.0 5730654.0	528678.4 528682.7
1275.0 62.9 1280.0 63.0				714.0 718.3	5730652.9 5730651.9	528687.0 528691.3
1285.0 62.9 1290.0 62.9	103.7 909.0	872.0	-163.1	722.7 727.0	5730650.8 5730649.8	528695.7 528700.0
1295.0 62.8	103.6 913.5	876.5	-165.2	731.3	5730648.7	528704.3
1300.0 62.8 1305.0 62.8		881.1	-167.3	735.6 740.0	5730647.7 5730646.6	528708.6 528712.9
1310.0 62.7 1315.0 62.7	103.6 922.7	885.7	-169.4	744.3 748.6	5730645.6 5730644.5	528717.3 528721.6
1320.0 62.7 1325.0 62.6				752.9 757.2	5730643.5 5730642.4	528725.9 528730.2
1330.0 62.6 1335.0 62.6				761.5 765.9	5730641.4 5730640.3	528734.5 528738.8
1340.0 62.6 1345.0 62.7	103.7 934.2	897.2	-174.7	770.2 774.5	5730639.3 5730638.2	528743.2 528747.5
1350.0 62.7	103.9 938.8	901.8	-176.8	778.8	5730637.1	528751.8
1355.0 62.8 1360.0 62.9	104.0 943.3	906.3		783.1 787.4	5730636.1 5730635.0	528756.1 528760.4
1365.0 63.0 1370.0 63.1	104.1 947.9	910.9	-181.1	791.7 796.1	5730633.9 5730632.9	528764.7 528769.1
1375.0 63.1 1380.0 63.1	104.1 950.1 104.1 952.4		-183.2	800.4 804.7	5730631.8 5730630.7	528773.4 528777.7
1385.0 63.1 1390.0 63.1	104.2 954.7 104.2 956.9	917.7	-184.3	809.0 813.4	5730629.6 5730628.5	528782.0 528786.4
1395.0 63.1 1400.0 63.1	104.2 959.2 104.3 961.5	922.2	-186.5	817.7 822.0	5730627.4 5730626.3	528790.7 528795.0
1700.0 00.1	10710 00110	D D	-107.0	522.0	0,00020.0	

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	MD	Angle	Direction	TVDRT	TVDSS	DNorth	DEast	Northing	Easting
	1405.0 1410.0	63.0 62.9	104.2 104.2	963.7 966.0	926.7 929.0	-188.7 -189.8	826.3 830.6	5730625.2 5730624.1	528799.3 528803.6
1	1415.0	62.8	104.1	968.3	931.3	-190.9	835.0	5730623.0	528808.0
	1420.0 1425.0	62.6 62.5	104.1 104.1	970.6 972.9	933.6 935.9	-192.0 -193.1	839.3 843.6	5730622.0 5730620.9	528812.3 528816.6
1	1430.0	62.4	104.0	975.2	938.2	-194.1	847.9	5730619.8	528820.9
	1435.0 1440.0	62.4 62.3	104.1 104.1	977.5 979.8	940.5 942.8	-195.2 -196.3	852.2 856.5	5730618.7 5730617.6	528825.2 528829.5
1	1445.0	62.3	104.2	982.1	945.1	-197.4	860.8	5730616.6	528833.8
	1450.0 1455.0	62.2 62.2	104.2 104.3	984.5 986.8	947.5 949.8	-198.4 -199.5	865.0 869.3	5730615.5 5730614.4	528838.0 528842.3
1	1460.0	62.1	104.3	989.1	952.1	-200.6	873.6	5730613.3	528846.6
	1465.0 1470.0	62.2 62.2	104.3 104.4	991.5 993.8	954.5 956.8	-201.7 -202.8	877.9 882.2	5730612.2 5730611.1	528850.9 528855.2
1	1475.0	62.3	104.4	996.1	959.1	-203.9	886.5	5730610.0	528859.5
	480.0 485.0	62.3 62.4	104.4 104.4	998.5 1000.8	961.5 963.8	-205.0 -206.1	890.8 895.1	5730608.9 5730607.8	528863.8 528868.0
1	490.0	62.4	104.4	1003.1	966.1	-207.2	899.3	5730606.7	528872.3
	495.0 500.0	62.5 62.6	104.4 104.4	1005.4 1007.7	968.4 970.7	-208.3 -209.4	903.6 907.9	5730605.6 5730604.5	528876.6 528880.9
1	505.0	62.6	104.4	1010.0	973.0	-210.5	912.2	5730603.4	528885.2
	510.0 515.0	62.7 62.7	104.5 104.5	1012.3 1014.6	975.3 977.6	-211.6 -212.7	916.5 920.8	5730602.3 5730601.2	528889.5 528893.8
1	520.0	62.8	104.5	1016.9	979.9	-213.9	925.1	5730600.1	528898.1
	525.0 530.0	62.7 62.7	104.5 104.5	1019.2 1021.5	982.2 984.5	-215.0 -216.1	929.4 933.7	5730599.0 5730597.8	528902.4 528906.7
1	535.0	62.6	104.6	1023.8	986.8	-217.2	938.0	5730596.7	528911.0
	540.0 545.0	62.6 62.5	104.6 104.7	1026.1 1028.4	989.1 991.4	-218.3 -219.4	942.3 946.6	5730595.6 5730594.5	528915.3 528919.6
	550.0	62.4	104.7	1030.7	993.7	-220.6	950.9	5730593.4	528923.9
	555.0 560.0	62.4 62.3	104.7 104.6	1033.0 1035.3	996.0 998.3	-221.7 -222.8	955.2 959.5	5730592.2 5730591.1	528928.2 528932.5
	565.0 570.0	62.3 62.2	104.6 104.6	1037.7 1040.0	1000.7 1003.0	-223.9 -225.0	963.8 968.1	5730590.0 5730588.9	528936.8 528941.1
1	575.0	62.2	104.6	1042.3	1005.3	-226.1	972.3	5730587.8	528945.3
	580.0 585.0	62.1 62.2	104.5 104.6	1044.7 1047.0	1007.7 1010.0	-227.3 -228.4	976.6 980.9	5730586.7 5730585.6	528949.6 528953.9
1	590.0	62.2	104.7	1049.3	1012.3	-229.5	985.2	5730584.4	528958.2
	595.0 600.0	62.3 62.4	104.8 104.8	1051.7 1054.0	1014.7 1017.0	-230.6 -231.7	989.5 993.7	5730583.3 5730582.2	528962.4 528966.7
1	605.0	62.4	104.9	1056.3	1019.3	-232.9	998.0	5730581.0	528971.0
	610.0 615.0	62.5 62.5	105.0 105.0	1058.6 1060.9	1021.6 1023.9	-234.0 -235.2	1002.3 1006.6	5730579.9 5730578.8	528975.3 528979.6
1	620.0	62.5	105.0	1063.2	1026.2	-236.3	1010.9	5730577.6	528983.9
	625.0 630.0	62.4 62.4	105.0 105.0	1065.5 1067.9	1028.5 1030.9	-237.5 -238.6	1015.1 1019.4	5730576.5 5730575.3	528988.1 528992.4
1	635.0	62.4	105.0	1070.2	1033.2	-239.7	1023.7	5730574.2	528996.7
	640.0 645.0	62.4 62.3	105.0 105.0	1072.5 1074.8	1035.5 1037.8	-240.9 -242.0	1028.0 1032.3	5730573.0 5730571.9	529001.0 529005.3
	650.0 655.0	62.2 62.2	105.0 105.0	1077.1	1040.1	-243.2	1036.5	5730570.8	529009.5
	660.0	62.2	105.0	1079.5 1081.8	1042.5 1044.8	-244.3 -245.5	1040.8 1045.1	5730569.6 5730568.5	529013.8 529018.1
	665.0 670.0	62.0 61.9	105.0 105.0	1084.2 1086.5	1047.2 1049.5	-246.6 -247.7	1049.4 1053.6	5730567.3 5730566.2	529022.3 529026.6
	675.0	61.8	105.0	1088.9	1051.9	-248.9	1053.0	5730565.1	529030.9
	680.0 685.0	61.7 61.5	105.0 105.0	1091.2 1093.6	1054.2 1056.6	-250.0 -251.2	1062.1 1066.4	5730563.9 5730562.8	529035.1 529039.4
1	690.0	61.4	105.0	1096.0	1059.0	-252.3	1070.6	5730561.6	529043.6
	695.0 700.0	61.3 61.1	105.1 105.1	1098.4 1100.8	1061.4 1063.8	-253.4 -254.6	1074.9 1079.1	5730560.5 5730559.4	529047.8 529052.1
1	705.0	61.1	105.1	1103.2	1066.2	-255.7	1083.3	5730558.2	529056.3
	710.0 715.0	61.1 61.1	105.1 105.1	1105.7 1108.1	1068.7 1071.1	-256.9 -258.0	1087.5 1091.8	5730557.1 5730555.9	529060.5 529064.8
1	720.0	61.1	105.1	1110.5	1073.5	-259.1	1096.0	5730554.8	529069.0
	725.0 730.0	61.0 61.0	105.1 105.1	1112.9 1115.3	1075.9 1078.3	-260.3 -261.4	1100.2 1104.4	5730553.7 5730552.5	529073.2 529077.4
1	735.0 740.0	60.9 60.8	105.2 105.3	1117.8 1120.2	1080.8 1083.2	-262.5 -263.7	1108.7 1112.9	5730551.4 5730550.2	529081.6
1	745.0	60.6	105.4	1122.6	1085.6	-264.8	1117.1	5730549.1	529085.9 529090.1
	750.0 755.0	60.5 60.3	105.4 105.5	1125.1 1127.6	1088.1 1090.6	-266.0 -267.2	1121.3 1125.5	5730547.9 5730546.8	529094.3 529098.5
		00.0	100.0		Page 5 (5,00040.0	029090.0 Append

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MD	Angle	Direction	TVDRT	TVDSS	DNorth	DEast	Northing	Easting
1760.0 1761.0 1762.0 1763.0 1764.0 1765.0 1766.0 1767.0 1777.0 1777.0 1777.0 1777.0 1778.0 1778.0 1780.0 1782.0 1783.0 1784.0 1785.0 1784.0 1785.0 1785.0 1785.0 1785.0 1790.0 1791.0 1792.0 1793.0 1795.0 1795.0 1795.0 1795.0 1795.0 1795.0 1795.0 1797.0 1795.0 1797.0 1795.0 1801.0 1802.0 1803.0 1803.0 1803.0 1803.0 1805.0 1805.0 1805.0 1811.0 1815.0 1815.0 1815.0 1815.0 1815.0 1821.0 1822.0 1822.0 1822.0 1822.0 1823.0 1825.0 18	Ange 222221111110000009999999999999999999999	IO5.6 105.6 105.7 105.7 105.7 105.7 105.7 105.7 105.7 105.7 105.7 105.7 105.7 105.7 105.7 105.7 105.8 105.8 105.9 105.9 105.9 105.9 105.9 105.9 105.9 105.9 106.0 106.0 106.0 106.1 106.1 106.1 106.1 106.1 106.1 106.1 106.1 106.1 106.1 106.2 106.2 106.2 106.2 106.2 106.2 106.2 106.2 106.2 106.2 </td <td>$\begin{array}{c} \textbf{VDR1} \\ \textbf{1130.15} \\ \textbf{1130.50} \\ \textbf{11331.50} \\ \textbf{11332.50} \\ \textbf{11332.50} \\ \textbf{11335.50} \\ \textbf{11444.50} \\ \textbf{11445.60} \\ \textbf{11445.60} \\ \textbf{11445.50} \\ \textbf{11555.22} \\ \textbf{33.83} \\ \textbf{33.83} \\ \textbf{33.99} \\ \textbf{49.49} \\ \textbf{49.55} \\ \textbf{11555.50} \\ \textbf{55.50} \\$</td> <td>1093.1 1093.5 1094.0 1094.5 1095.0 1095.5 1096.0 1097.0 1097.5 1098.5 1099.0 1099.5 1100.0 1101.5 1102.5 1102.5 1103.6 1104.1 1105.6 1107.1 1105.6 1107.1 1108.6 1107.1 1108.6 1107.1 1108.6 1109.1 1109.6 110.1 1109.6 1111.1 1102.5 1103.6 1107.1 1108.6 1107.1 1108.6 1107.1 1108.6 1109.1 110.1 110.5 1102.5 1103.6 1107.1 1108.6 1107.1 1108.6 1107.1 1108.6 1109.1 110.1 110.6 1111.1 1112.2 112.7 113.7</td> <td>-268.3 -268.6 -268.8 -269.0 -269.3 -269.5 -269.7 -270.0 -270.2 -270.4 -270.7 -270.9 -271.1 -271.4 -271.6 -271.8 -272.1 -272.3 -272.5 -272.8 -273.0 -273.3 -273.5 -273.7 -274.0 -274.2 -274.4 -274.7 -274.9 -275.2 -275.4 -275.9 -275.4 -275.9 -275.5 -275.9 -276.1 -276.3 -276.6 -275.9 -276.1 -276.8 -275.9 -276.1 -276.8 -275.9 -276.1 -276.8 -275.9 -276.1 -276.8 -275.8 -277.3 -277.5 -277.8 -277.8 -277.8</td> <td>$\begin{array}{l} \textbf{DEast}\\ 1129.6\\ 1130.5\\ 1131.3\\ 1132.0\\ 1133.3\\ 1132.0\\ 1133.3\\ 1135.5\\ 1136.2\\ 1135.3\\ 1135.5\\ 1136.2\\ 1137.0\\ 1135.3\\ 1137.0\\ 1138.8\\ 1139.5\\ 1137.0\\ 1138.8\\ 1139.5\\ 1137.0\\ 1141.3\\ 1144.5\\ 1155.3\\ 1155.$</td> <td>Nortning 5730545.6 5730545.1 5730545.1 5730544.9 5730544.7 5730544.2 5730544.2 5730543.7 5730543.7 5730543.7 5730543.7 5730543.3 5730542.8 5730542.8 5730542.1 5730542.3 5730542.1 5730542.1 5730542.1 5730542.1 5730542.1 5730542.1 5730541.4 5730540.7 5730540.7 5730539.7 5730539.7 5730539.7 5730539.7 5730539.7 5730539.7 5730539.7 5730538.1 5730537.3 5730537.1 5730537.1 5730535.7 5730535.7 5730535.7 5730535.7 5730535.7 5730535.7 5730535.7 5730535.7 5730533.1</td> <td>529102.6 529103.5 529104.3 529105.1 529106.0 529106.8 529107.6 529108.5 529109.3 529110.2 529110.2 529111.0 529111.8 529112.7 529114.3 529114.3 529115.2 529114.3 529114.3 529114.3 529114.3 529114.3 529114.3 529114.3 529114.3 529114.3 529114.3 529112.7 529114.3 529112.0 529122.0 529122.0 529122.0 529122.0 529122.0 529122.0 529122.0 529124.3 529122.6 529124.3 529126.0 529126.0 529128.4 529127.6 529129.3 529130.1 529130.1 529133.4 529135.1 529135.1 529135.1 529135.7</td>	$\begin{array}{c} \textbf{VDR1} \\ \textbf{1130.15} \\ \textbf{1130.50} \\ \textbf{11331.50} \\ \textbf{11332.50} \\ \textbf{11332.50} \\ \textbf{11335.50} \\ \textbf{11444.50} \\ \textbf{11445.60} \\ \textbf{11445.60} \\ \textbf{11445.50} \\ \textbf{11555.22} \\ \textbf{33.83} \\ \textbf{33.83} \\ \textbf{33.99} \\ \textbf{49.49} \\ \textbf{49.55} \\ \textbf{11555.50} \\ \textbf{55.50} \\$	1093.1 1093.5 1094.0 1094.5 1095.0 1095.5 1096.0 1097.0 1097.5 1098.5 1099.0 1099.5 1100.0 1101.5 1102.5 1102.5 1103.6 1104.1 1105.6 1107.1 1105.6 1107.1 1108.6 1107.1 1108.6 1107.1 1108.6 1109.1 1109.6 110.1 1109.6 1111.1 1102.5 1103.6 1107.1 1108.6 1107.1 1108.6 1107.1 1108.6 1109.1 110.1 110.5 1102.5 1103.6 1107.1 1108.6 1107.1 1108.6 1107.1 1108.6 1109.1 110.1 110.6 1111.1 1112.2 112.7 113.7	-268.3 -268.6 -268.8 -269.0 -269.3 -269.5 -269.7 -270.0 -270.2 -270.4 -270.7 -270.9 -271.1 -271.4 -271.6 -271.8 -272.1 -272.3 -272.5 -272.8 -273.0 -273.3 -273.5 -273.7 -274.0 -274.2 -274.4 -274.7 -274.9 -275.2 -275.4 -275.9 -275.4 -275.9 -275.5 -275.9 -276.1 -276.3 -276.6 -275.9 -276.1 -276.8 -275.9 -276.1 -276.8 -275.9 -276.1 -276.8 -275.9 -276.1 -276.8 -275.8 -277.3 -277.5 -277.8 -277.8 -277.8	$\begin{array}{l} \textbf{DEast}\\ 1129.6\\ 1130.5\\ 1131.3\\ 1132.0\\ 1133.3\\ 1132.0\\ 1133.3\\ 1135.5\\ 1136.2\\ 1135.3\\ 1135.5\\ 1136.2\\ 1137.0\\ 1135.3\\ 1137.0\\ 1138.8\\ 1139.5\\ 1137.0\\ 1138.8\\ 1139.5\\ 1137.0\\ 1141.3\\ 1144.5\\ 1155.3\\ 1155.$	Nortning 5730545.6 5730545.1 5730545.1 5730544.9 5730544.7 5730544.2 5730544.2 5730543.7 5730543.7 5730543.7 5730543.7 5730543.3 5730542.8 5730542.8 5730542.1 5730542.3 5730542.1 5730542.1 5730542.1 5730542.1 5730542.1 5730542.1 5730541.4 5730540.7 5730540.7 5730539.7 5730539.7 5730539.7 5730539.7 5730539.7 5730539.7 5730539.7 5730538.1 5730537.3 5730537.1 5730537.1 5730535.7 5730535.7 5730535.7 5730535.7 5730535.7 5730535.7 5730535.7 5730535.7 5730533.1	529102.6 529103.5 529104.3 529105.1 529106.0 529106.8 529107.6 529108.5 529109.3 529110.2 529110.2 529111.0 529111.8 529112.7 529114.3 529114.3 529115.2 529114.3 529114.3 529114.3 529114.3 529114.3 529114.3 529114.3 529114.3 529114.3 529114.3 529112.7 529114.3 529112.0 529122.0 529122.0 529122.0 529122.0 529122.0 529122.0 529122.0 529124.3 529122.6 529124.3 529126.0 529126.0 529128.4 529127.6 529129.3 529130.1 529130.1 529133.4 529135.1 529135.1 529135.1 529135.7

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$\begin{array}{c} 1830.0 \\ 1831.0 \\ 1831.0 \\ 1831.0 \\ 1832.0 \\ 1832.0 \\ 1833.0 \\ 1833.0 \\ 1835.0 \\ 1835.0 \\ 1835.0 \\ 1837.0 \\ 1840.0 \\ 1841.0 \\ 1842.0 \\ 1844.0 \\ 1845.0 \\ 1846.0 \\ 1847.0 \\ 1846.0 \\ 1847.0 \\ 1846.0 \\ 1855.0 \\ 1855.0 \\ 1855.0 \\ 1855.0 \\ 1855.0 \\ 1855.0 \\ 1855.0 \\ 55 \\ 1856.0 \\ 55 \\ 1856.0 \\ 55 \\ 1856.0 \\ 55 \\ 1856.0 \\ 55 \\ 1856.0 \\ 55 \\ 1866.0 \\ 55 \\ 1866.0 \\ 55 \\ 1866.0 \\ 55 \\ 1866.0 \\ 55 \\ 1866.0 \\ 55 \\ 1866.0 \\ 55 \\ 1866.0 \\ 55 \\ 1866.0 \\ 55 \\ 1866.0 \\ 55 \\ 1866.0 \\ 55 \\ 1866.0 \\ 55 \\ 1866.0 \\ 55 \\ 1866.0 \\ 55 \\ 1866.0 \\ 55 \\ 1866.0 \\ 55 \\ 1866.0 \\ 55 \\ 1866.0 \\ 55 \\ 1866.0 \\ 55 \\ 1867.0 \\ 55 \\ 1874.0 \\ 1874.0 \\ 1874.0 \\ 1874.0 \\ 1874.0 \\ 1874.0 \\ 1874.0 \\ 18$	ngle Direction 57.8 106.4 57.6 106.4 57.6 106.4 57.6 106.4 57.6 106.4 57.6 106.4 57.6 106.5 57.1 106.5 57.2 106.5 57.2 106.5 57.2 106.5 57.2 106.5 57.2 106.5 57.1 106.6 57.2 106.6 57.0 106.6 57.0 106.6 57.0 106.6 56.7 106.6 56.7 106.6 56.7 106.6 56.7 106.7 56.5 106.7 56.5 106.7 56.5 106.7 56.5 106.7 56.5 106.7 56.5 106.7 56.5 106.7 56.5 106.7 56.6 106.7	TVDRT 1165.8 1166.4 1166.9 1167.4 1168.0 1168.5 1169.1 1170.7 1171.2 1171.8 1172.3 1172.8 1173.9 1174.5 1175.6 1176.7 1175.6 1176.7 1177.2 1177.8 1175.6 1176.7 1177.2 1177.8 1178.3 1178.9 1174.5 1176.7 1177.2 1177.8 1178.3 1178.3 1178.9 1174.5 1176.7 1177.2 1180.6 1181.1 1183.3 1183.9 1184.4 1185.6 1186.1 1186.7 1185.6 1186.1 1186.7 1187.2 1187.8 1189.5 1190.0 1191.2 1191.7 1192.3 1194.5 1195.1 1195.7 1195.7	TVDSS 1128.8 1129.4 1129.9 1130.4 1131.0 1131.5 1132.1 1132.6 1133.7 1134.8 1135.8 1136.9 1137.5 1138.6 1139.7 1140.2 1140.8 1143.6 1139.7 1140.2 1140.8 1144.7 1145.8 1144.7 1145.8 1144.7 1145.8 1144.7 1145.8 1144.7 1145.8 1144.7 1145.8 1144.7 1150.8 1151.9 1152.5 1153.6 1154.7 1155.8 1155.8 1155.7 1158.7 1158.7	DNorth -284.9 -285.2 -285.4 -285.6 -285.9 -286.3 -286.3 -286.3 -287.3 -287.3 -287.3 -287.3 -287.3 -288.3 -288.7 -289.2 -289.7 -289.2 -289.7 -289.2 -289.7 -290.4 -290.9 -290.4 -290.9 -291.1 -291.4 -291.9 -292.3 -293.3 -293.5 -293.3 -293.5 -295.7	DEast 1187.5 1188.3 1189.1 1189.9 1190.7 1191.5 1192.3 1193.1 1193.9 1194.7 1195.5 1196.4 1197.2 1298.0 1202.8 1200.4 1201.2 1202.0 1202.8 1203.6 1204.4 1205.2 1206.8 1207.6 1208.4 1207.6 1208.4 1207.6 1208.4 1207.6 1208.4 1207.6 1208.4 1207.5 1210.3 1211.5 1213.1 1213.9 1214.7 1215.5 1216.3 1217.9 1218.7 1225.0 1225.8 1226.6 1227.4 1229.0 1229.8 1220.6	Northing 5730529.0 5730528.8 5730528.3 5730528.3 5730528.1 5730527.8 5730527.8 5730527.3 5730527.1 5730526.9 5730526.4 5730526.4 5730526.2 5730525.7 5730525.7 5730525.7 5730525.2 5730524.2 5730524.2 5730524.5 5730524.2 5730522.3 5730522.3 5730522.3 5730522.3 5730522.1 573052	Easting 529160.5 529162.1 529162.9 529162.9 529163.7 529164.5 529166.1 529166.9 529167.7 529168.5 529170.2 529177.0 529177.0 529177.6 529177.6 529177.4 529175.0 529175.8 529175.8 529177.4 529175.0 529175.8 529177.4 529175.8 529177.4 529175.8 529177.4 529175.8 529175.8 529175.8 529175.8 529175.8 529175.8 529175.8 529175.8 529175.8 529175.8 529175.8 529175.8 529175.8 529175.8 529175.8 529177.4 529179.0 529179.8 529183.7 529184.5 529184.5 529185.3 529187.7 529187.7 529187.7 529187.7 529190.1 529190.1 529190.1 5291917.2 529194.1 529194.1 529194.1 529194.2 529194.1 529194.1 529194.2 529194.1 529194.2 52914.2 52914.2 52914.2 52914.2
1874.0 5 1875.0 5 1876.0 5 1877.0 5 1878.0 5 1879.0 5 1879.0 5 1880.0 5 1881.0 5 1882.0 5 1883.0 5 1885.0 5 1886.0 5 1887.0 5 1889.0 5 1891.0 5 1892.0 5 1893.0 5 1894.0 5 1895.0 5 1896.0 5 1897.0 5 1898.0 5 1899.0 5 1899.0 5 1899.0 5 1898.0 5 1898.0 5 1898.0 5 1898.0 5 1898.0 5 1898.0 5 1898.0 5 1899.0 5	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	1190.0 1190.6 1191.2 1191.7 1192.3 1192.8 1193.4 1194.0 1194.5 1195.1 1195.7 1196.2 1196.8 1197.3 1197.9 1198.5 1199.0 1200.2 1200.7 1201.3 1201.9 1202.4 1203.6 1204.1	$\begin{array}{c} 1153.0\\ 1153.6\\ 1154.2\\ 1154.7\\ 1155.3\\ 1155.8\\ 1156.4\\ 1157.0\\ 1157.5\\ 1158.7\\ 1159.2\\ 1159.8\\ 1160.3\\ 1160.9\\ 1161.5\\ 1162.0\\ 1162.6\\ 1163.2\\ 1164.3\\ 1164.3\\ 1164.9\\ 1165.4\\ 1166.0\\ 1167.1 \end{array}$	-295.5 -295.7 -296.0 -296.2 -296.5 -296.7 -296.9 -297.2 -297.4 -297.7 -297.9 -298.2 -298.4 -298.6 -298.9 -299.1 -299.4 -299.4 -299.6 -299.9 -300.1 -300.4 -300.6 -301.8	1222.7 1223.5 1224.2 1225.0 1225.8 1226.6 1227.4 1228.2 1229.0 1229.8	5730518.4 5730518.2 5730518.0 5730517.7 5730517.5 5730517.2 5730517.0 5730516.7 5730516.5 5730516.3	529194.9 529195.7 529196.4 529197.2 529198.0 529198.8 529199.6 529200.4 529201.2 529201.2 529202.0 529202.8

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Appendix 2

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MDAngle1901.055.41902.055.41903.055.4	Direction TVDRT	TVDSS	DNorth	DEast	Northing	Easting
	107.3 1205.3	1168.3	-302.1	1244.0	5730511.9	529216.9
	107.3 1205.8	1168.8	-302.3	1244.7	5730511.6	529217.7
	107.3 1206.4	1169.4	-302.6	1245.5	5730511.4	529218.5
1904.0 55.4	107.3 1207.0	1170.0	-302.8	1246.3	5730511.1	529219.3
1905.0 55.4	107.3 1207.5	1170.5	-303.1	1247.1	5730510.9	529220.1
1906.0 55.4	107.3 1208.1	1171.1	-303.3	1247.9	5730510.6	529220.9
1907.0 55.4	107.3 1208.7	1171.7	-303.5	1248.7	5730510.4	529221.7
1908.0 55.4 1909.0 55.3 1910.0 55.3 1911.0 55.3 1912.0 55.3	107.4 1209.2 107.4 1209.8 107.4 1210.4 107.4 1211.0 107.4 1211.5	1172.2 1172.8 1173.4 1174.0	-303.8 -304.0 -304.3 -304.5	1249.5 1250.2 1251.0 1251.8	5730510.1 5730509.9 5730509.6 5730509.4	529222.4 529223.2 529224.0 529224.8
1912.055.31913.055.21914.055.21915.055.21916.055.2	107.4 1211.5	1174.5	-304.8	1252.6	5730509.2	529225.6
	107.4 1212.1	1175.1	-305.0	1253.4	5730508.9	529226.4
	107.4 1212.7	1175.7	-305.3	1254.2	5730508.7	529227.2
	107.4 1213.2	1176.2	-305.5	1254.9	5730508.4	529227.9
	107.3 1213.8	1176.8	-305.8	1255.7	5730508.2	529228.7
1917.055.21918.055.21919.055.21920.055.2	107.2 1214.4	1177.4	-306.0	1256.5	5730507.9	529229.5
	107.2 1214.9	1177.9	-306.2	1257.3	5730507.7	529230.3
	107.1 1215.5	1178.5	-306.5	1258.1	5730507.4	529231.1
	107.0 1216.1	1179.1	-306.7	1258.9	5730507.2	529231.9
1921.055.21922.055.21923.055.21924.055.2	106.9 1216.7	1179.7	-307.0	1259.6	5730507.0	529232.6
	106.8 1217.2	1180.2	-307.2	1260.4	5730506.7	529233.4
	106.8 1217.8	1180.8	-307.4	1261.2	5730506.5	529234.2
	106.8 1218.4	1181.4	-307.7	1262.0	5730506.3	529235.0
1925.0 55.1 1926.0 55.1 1927.0 55.1 1928.0 55.1 1929.0 55.1	106.8 1218.9 106.8 1219.5 106.8 1220.1 106.8 1220.7 106.8 1221.2	1181.9 1182.5 1183.1 1183.7 1184.2	-307.9 -308.1 -308.4 -308.6 -308.9	1262.8 1263.6 1264.4 1265.1 1265.9	5730506.0 5730505.8 5730505.5 5730505.3	529235.8 529236.6 529237.4 529238.1
1929.0 55.1 1930.0 55.0 1931.0 55.0 1932.0 55.0 1933.0 55.0	106.8 1221.2 106.8 1221.8 106.8 1222.4 106.8 1223.0 106.8 1223.5	1184.2 1184.8 1185.4 1186.0 1186.5	-309.1 -309.3 -309.6 -309.8	1265.9 1266.7 1267.5 1268.3 1269.1	5730505.1 5730504.8 5730504.6 5730504.4 5730504.1	529238.9 529239.7 529240.5 529241.3 529242.1
1934.055.01935.054.91936.054.91937.054.9	106.8 1224.1	1187.1	-310.0	1269.9	5730503.9	529242.8
	106.8 1224.7	1187.7	-310.3	1270.6	5730503.7	529243.6
	106.8 1225.2	1188.2	-310.5	1271.4	5730503.4	529244.4
	106.8 1225.8	1188.8	-310.8	1272.2	5730503.2	529245.2
1938.054.91939.054.91940.054.81941.054.81942.054.8	106.8 1226.4 106.8 1227.0 106.8 1227.6 106.8 1228.1 106.8 1228.7	1189.4 1190.0 1190.6 1191.1 1191.7	-311.0 -311.2 -311.5 -311.7 -311.9	1273.0 1273.8 1274.6 1275.3 1276.1	5730502.9 5730502.7 5730502.5 5730502.2	529246.0 529246.8 529247.5 529248.3
1943.0 54.8 1944.0 54.8 1945.0 54.7 1946.0 54.7	106.8 1229.3 106.8 1229.3 106.8 1229.9 106.8 1230.4 106.8 1231.0	1192.3	-312.2 -312.4 -312.6 -312.9	1276.9 1277.7 1278.5 1279.2	5730502.0 5730501.8 5730501.5 5730501.3 5730501.3	529249.1 529249.9 529250.7 529251.5 529252.2
1947.054.71948.054.71949.054.71950.054.6	106.8 1231.6	1194.6	-313.1	1280.0	5730500.8	529253.0
	106.8 1232.2	1195.2	-313.3	1280.8	5730500.6	529253.8
	106.8 1232.7	1195.7	-313.6	1281.6	5730500.3	529254.6
	106.8 1233.3	1196.3	-313.8	1282.4	5730500.1	529255.4
1951.0 54.6 1952.0 54.6 1953.0 54.6 1954.0 54.6 1955.0 54.6	106.8 1233.9 106.8 1234.5 106.8 1235.1 106.8 1235.6 106.8 1236.2	1196.9 1197.5 1198.1 1198.6 1199.2	-314.1 -314.3 -314.5 -314.8 -315.0	1283.1 1283.9 1284.7 1285.5 1286.3	5730499.9 5730499.6 5730499.4 5730499.2 5730499.2 5730498.9	529256.1 529256.9 529257.7 529258.5 529259.3
1956.054.61957.054.61958.054.61959.054.5	106.8 1236.8	1199.8	-315.2	1287.0	5730498.7	529260.0
	106.8 1237.4	1200.4	-315.5	1287.8	5730498.5	529260.8
	106.9 1238.0	1201.0	-315.7	1288.6	5730498.2	529261.6
	106.9 1238.5	1201.5	-315.9	1289.4	5730498.0	529262.4
1960.054.51961.054.51962.054.51963.054.51964.054.5	106.9 1239.1 106.9 1239.7 106.9 1240.3 106.9 1240.9 106.9 1241.4	1202.1 1202.7 1203.3 1203.9 1204.4	-316.2 -316.4 -316.7 -316.9 -317.1	1290.2 1290.9 1291.7 1292.5 1293.3	5730497.7 5730497.5 5730497.3 5730497.0 5730497.0 5730496.8	529263.2 529263.9 529264.7 529265.5 529266.3
1965.054.51966.054.51967.054.51968.054.5	106.9 1242.0	1205.0	-317.4	1294.1	5730496.6	529267.1
	106.9 1242.6	1205.6	-317.6	1294.8	5730496.3	529267.8
	106.9 1243.2	1206.2	-317.8	1295.6	5730496.1	529268.6
	106.9 1243.8	1206.8	-318.1	1296.4	5730495.9	529269.4
1969.0 54.5	106.9 1244.3	1207.3	-318.3	1297.2	5730495.6	529270.2
1970.0 54.5	106.9 1244.9	1207.9	-318.5	1298.0	5730495.4	529271.0
1971.0 54.5	106.9 1245.5	1208.5	-318.8	1298.7	5730495.1	529271.7

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Appendix 2

1972.0 1973.0 1974.0 1975.0 1976.0 1977.0 1978.0 1980.0 1981.0 1982.0 1982.0 1983.0 1984.0 1985.0 1986.0 1987.0 1987.0 1990.0 1991.0 1992.0 1994.0 1994.0 1994.0 1995.0 1994.0 1995.0 1994.0 1995.0 1995.0 1995.0 1996.0 1997.0 1996.0 1997.0 1998.0 1997.0 1998.0 1997.0 2000.0 5 2000.0 5 2005.0 5 2010.0 5 5 5 5 5 5 5 5 5 5 5 5 5	54.4 10 54.4 10 54.4 10 54.4 10 54.4 10 54.4 10 54.4 10 54.4 10 54.4 10 54.4 10 54.4 10 54.4 10	7.0 1246.1 7.0 1246.7 7.0 1247.8 7.0 1247.8 7.0 1247.8 7.0 1249.6 7.0 1249.6 7.0 1250.2 7.0 1250.2 7.0 1250.2 7.1 1251.3 7.1 1252.5 7.2 1253.1 7.3 1254.2 7.3 1254.2 7.3 1254.2 7.3 1255.4 7.4 1256.6 7.5 1257.2 7.5 1257.8 7.6 1259.5 7.7 1260.17 7.7 1260.17 7.7 1263.7 7.8 1262.5 7.9 1263.7 7.9 1266.13 7.9 1264.3 8.0 1265.5 8.0 1266.7 8.1 1267.2 8.1 1267.2 8.1 1269.6 7.1 1267.2 8.1 1269.6 7.1 1270.2 8.1 1269.6 7.1 1270.2 7.1 1270.8	 1209.7 1210.3 1210.8 1211.4 1212.0 1212.6 1213.2 1213.7 1214.3 1214.9 1215.5 1216.7 1217.2 1217.2 1217.8 1218.4 1219.0 1219.6 1220.2 1220.8 1221.4 	DNorth -319.0 -319.3 -319.5 -319.7 -320.0 -320.2 -320.4 -320.7 -320.9 -321.2 -321.4 -321.6 -322.8 -322.8 -322.8 -322.8 -322.8 -322.8 -322.8 -323.6 -322.8 -322.8 -322.8 -322.5 -324.5 -325.5 -325.8 -325.5 -326.0 -325.5 -326.5 -326.5 -326.5 -326.5 -326.5 -326.5 -326.5 -326.5 -326.5 -326.5 -326.5 -326.5 -326.5 -326.5 -326.5 -326.5 -326.5 -327.7 -328.7 -328.7 -329.5 -329.5	DEast 1299.5 1300.3 1301.1 1301.8 1302.6 1303.4 1304.2 1305.0 1305.7 1306.5 1307.3 1308.1 1308.8 1309.6 1310.4 1310.2 1312.7 1313.5 1314.3 1315.0 1315.8 1316.6 1317.3 1318.1 1318.9 1320.4 1321.2 1322.7 1323.5 1324.2 1325.8 1326.5 1327.3 1328.8 1326.5 1327.3 1328.8 1329.6 1330.4 1331.1 1331.9 1332.6	Northing 5730494.9 5730494.7 5730494.2 5730494.2 5730493.7 5730493.2 5730493.2 5730493.2 5730492.3 5730492.3 5730492.3 5730492.3 5730492.3 5730492.3 5730491.6 5730491.6 5730491.6 5730491.3 5730491.6 5730490.6 5730490.6 5730490.4 5730490.4 5730490.4 5730489.9 5730489.9 5730489.4 5730489.1 5730488.4 5730488.7 5730488.4 5730487.7 5730487.4 5730487.4 5730487.4 5730487.4 5730486.7 5730486.7 5730485.2 5730485.4 5730485.4 5730484.4	Easting 529272.5 529273.3 529274.1 529274.8 529275.6 529276.4 529277.2 529278.0 529278.7 529280.3 529281.1 529281.8 529282.6 529283.4 529284.2 529284.2 529284.2 529284.3 529284.5 529285.7 529288.0 529288.0 529288.0 529288.0 529288.0 529288.0 529289.6 529290.3 529291.1 529291.1 529292.6 529293.4 529294.2 529294.2 529294.2 529294.2 529294.2 529294.2 529294.2 529294.2 529294.2 529294.2 529294.2 529295.7 529295.
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2040.0 5 2041.0 5	3.4 108 3.4 108 3.4 108 3.4 108	.1 1286.3 .1 1286.9	1248.7 1249.3 1249.9 1250.5 Page 9 c	-335.7 -336.0 -336.2	1351.0 1351.7 1352.5 1353.2	5730478.5 5730478.2 5730478.0 5730477.7	529324.0 529324.7 529325.5 529326.2 Append
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Appendix 2

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MD	Angle	Direction	TVDRT	TVDSS	DNorth	DEast	Northing	Easting
2043.0	5Š.4	108.1	1288.1	1251.1	-336.5	1354.0	5730477.5	529327.0
2044.0	53.4	108.1	1288.7	1251.7	-336.7	1354.8	5730477.2	529327.8
2045.0	53.4	108.1	1289.3	1252.3	-337.0	1355.5	5730477.0	529328.5
2046.0	53.4	108.1	1289.9	1252.9	-337.2	1356.3	5730476.7	529329.3
2047.0	53.4	108.1	1290.5	1253.5	-337.5	1357.1	5730476.5	529330.1
2048.0	53.4	108.1	1291.1	1254.1	-337.7	1357.8	5730476.2	529330.8
2049.0	53.4	108.1	1291.7	1254.7	-338.0	1358.6	5730476.0	529331.6
2050.0	53.4	108.1	1292.3	1255.3	-338.2	1359.4	5730475.7	529332.3
2051.0	53.4	108.1	1292.9	1255.9	-338.5	1360.1	5730475.5	529333.1
2052.0	53.4	108.1	1293.5	1256.5	-338.7	1360.9	5730475.2	529333.9

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APPENDIX 3

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APPENDIX

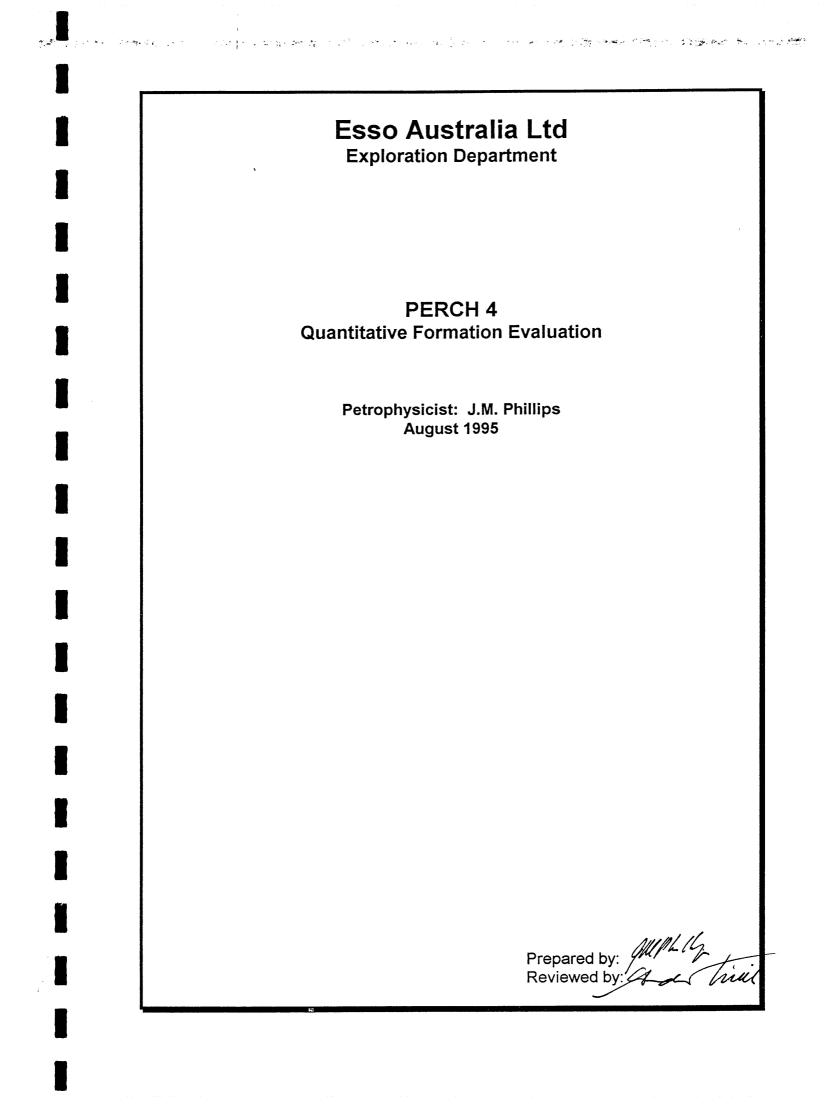
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APPENDIX 3

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PERCH-4

Petrophysics Evaluation Summary



PERCH 4 QUANTITATIVE FORMATION EVALUATION

The Perch 4 well is an oil development well designed to access the Perch N-1 reservoir in a crestal location within the eastern fault block of the Perch field (Vic/L17 - Vic/L15). The N-1 reservoir was proposed to be intersected some 3m structurally higher than the adjacent Perch 2 well.

Perch 1 (drilled in 1968) and Perch 2 (drilled 1985) are plugged and abandoned exploration wells whilst the Perch 3 well was drilled from the Perch monotower facility in 1989, and until now has been the only producing well in the Perch field. Perch 3 lies some 1.2km to the northwest of the Perch 4 N-1 reservoir penetration.

Perch 2 provides the nearest correlation point (some 190m to the NW) at the target horizon and wireline log data from this well has been used as a check of the Perch 4 log data and subsequent analysis.

The top of Latrobe Group was intersected in Perch 4 at 1769m MDKB (1097.5m TVDSS), some 9m high to prognosis, whilst the primary objective N-1 reservoir sand was encountered at 1814.4m MDKB (1120.6m TVDSS), some 2.7m updip of the Perch 2 well, and is 10.5m (True Vertical Thickness) thick.

Perch 4 was drilled from the Perch Monotower Facility using the Harvey Ward jack up drilling rig. The well was deviated (59°@ 106°T) to reach the primary target within the eastern fault block.

<u>DATA</u>

Logs Acquired

Anadrill LWD:	CDR, 1740m to 2070m MDKB
	CDN, 1600m to 2052m MDKB

Schlumberger CSU: GR-CBL-VDL-CCL to 1930m MDKB

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Log Quality

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Attempts to run an openhole suite of wireline logs proved unsuccessful due to an inability to pass 860m MDKB in the 59° well bore. Consequently the only wireline logs in Perch 4 were obtained in cased hole (GR, CBL, VDL, CCL) and only down to 1930m MDKB (This was due to operational cementing problem leaving cement inside casing which was subsequently drilled out down to 1930m MDKB). LWD measurements were, however, obtained from Anadrill CDR and CDN tools which were run in two modes. Firstly, the CDR (Compensated Dual Resistivity) was used to record data whilst drilling the section from 1740m MDKB to 2070m MDKB. (ie gamma ray and resistivity data available for this section of hole). Once it was established that no open hole wireline logs could be acquired a second pass of the LWD tools was made. This run included the CDR and CDN (Compensated Density Neutron) in a reaming pass from 1600m to 2052m MDKB at a speed of less than 15m/hr over the objective N-1 Reservoir interval (1800-1850m MDKB).

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Log Processing

The wireline Gamma Ray, recorded in cased hole with the CCL-CBL-VDL-GR run was considered to represent; the correct depth measurement down to 1930m MDKB. Consequently the LWD gamma ray (which covered the section from TOL to TD was depth aligned (by 2m) to match the wireline gamma ray and was used in this analysis.

The two passes of LWD resistivity curves were spliced below the N-1 reservoir to provide a curve composed of maximum real time data over the zone of interest and bottom hole section. No correction was made to the composite resistivity curve. As both phase shift resistivity (PSR) and attenuation resistivity (ATR) obtained with the LWD were strongly affected by invasion the ATR, which was the highest resistivity measurement, was used to represent Rt (despite this, saturations are recognised as probably being pessimistic).

Comparison of bulk density logs from the Perch 2 (wireline logs) and Perch 4 (LWD logs) wells over the N-1 reservoir section revealed the LWD density measurements in Perch 4 to be consistently lower in similar facies/quality section as a result of tool calibration error. Accordingly a bulk shift of +0.1gm/cc was applied to the Perch 4 density measurements to gain a good match with the Perch 2 wireline data, over the main reservoir interval (see Figure 1).

A two porosity unit negative bulk shift correction was applied to the LWD neutron data in Perch 4 to better fit the clean nature of the N-1 reservoir sand observed in Perch 2.

INTERPRETATION

Logs Used

GR, RHOB, NPHI, ATR, PSR (Anadrill LWD)

Analysis Parameters

1 а 1.85 m 2 n 0.25 Apparent Shale Porosity (PHISH) Shale Resistivity (RSH) 15 ohmm Formation Water Resistivity (RW) 0.14 ohmm above 1835m MDKB Formation Water Resistivity (RW) 0.8 ohmm below 1835m MDKB 80 DEGC Bottom Hole Temperature

Porosity

Total porosity was derived from the density-neutron using the LOGIC program XPL. Effective porosity was derived from total porosity using a gamma ray derived VSH.

Shale Volume

Shale volume was derived from the gamma ray using the LOGIC program VSH with the Clavier option and a gamma ray minimum and maximum of 60 API and 180 API respectively.

Free Formation Water Resistivity

In the N-1 oil zone Rw has been based on regional data as it is interpreted to be more saline than the underlying aquifer which has been flushed by fresh water. Below the N-1 oil, free formation water resistivity was derived from RWA calculations in clean water sands.

Water Saturations

Total water saturation was calculated using density-neutron total porosity in the Dual Water programme DWGP. Effective porosity and effective water saturation were calculated using gamma ray VSH.

Water saturation was set to 1 and porosity set to 0 in coals and carbonaceous shales.

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RESULTS

- 1. The top of the primary objective (N-1 reservoir) was intersected at 1814.4m MDKB (1120.6m TVDSS) 1m low to prognosis. The sand was described from cuttings as coarse to very coarse grained, well sorted loose and of fair to good visual porosity. A total gross sand thickness of 19.8m measured thickness was intersected. The upper 4.6m (measured thickness) of the N-1 reservoir displayed relatively poorer average porosity than the lower 15.1m (measured thickness).
- 2. The base of porosity within the N-1 reservoir at Perch 4 is interpreted to be 1834.2m MDKB, immediately above a probable thin coal interval. This indicates a level of lowest known oil of 1834.2m MDKB (1131.1m TVDSS) in this well which is 0.9m TVD above the Original Oil Water Contact for the Perch field.
- 3. A total of 19.6m (measured thickness) (10.5m TVT) of net pay with average porosity of 29% and average Sw of 19% is calculated for the N-1 Perch 4 reservoir.
- 4. A thin sand below the Field OOWC from 1836.5m MDKB to 1837.9m MDKB exhibits an average porosity of 27% and an average Sw of 79% but is not considered to be net pay.
- 5. All other reservoir section below 1837.9m MDKB is interpreted to be water saturated.

Attached are the following presentations of results:

Table 1 - Summary of ResultsTable 2 - Log Analysis ListingFigure 1 - Density-Neutron CrossplotAttachment 1 - Log Analysis Depthplot

TABLE 1

PERCH_4

ANALYSIS SUMMARY (Depths are Measured Depth KB)

Net porosity cut-off..... 0.120 volume per volume t water saturation cut-off..: 0.500 volume per volume

Net Porous Interval based on Porosity cut-off only.

l	ROSS INTERVA	L	NET PO	OROUS INT	ERVAL						
ł	(metres MDKB)	Gross	Net	Net to	Mean	(Std.)	Mean	(Std.)	Mode	Mean	
((top) -(base)	Metres	Metres	Gross	Vsh	(Dev.)	Porosity	(Dev.)	Porosity	Sw	
1	4.4-1819.0	4.6	4.5	97 %	0.08	(0.062)	0.210	(0.022)	0.200	0.39	OIL ZONE
1	1819.1-1834.2	15.1	15.1	100 %	0.00	(0.002)	0.310	(0.014)	0.310	0.13	OIL ZONE
1	6.5-1837.9	1.4	1.4	100 %	0.19	(0.099)	0.270	(0.041)	0.280	0.79	WATER ZONE
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** Lowest Known Oil calculated at 1834.2 m MDKB (-1132m TVDSS)**

Total Net Pay = 19.6m Measured Thickness (10.5m True Vertical Thickness) Av Porosity = 29% Av Sw = 19%

PERCH 4

WELL DATA LISTING

(Table 2)

PERCH_4

Well Data Listing

DEPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE frac
(mRKB)	api	ohmm	g/cc	frac	frac	frac	IIac
1800.0	141	1.6	2.060	0,528	0.477	0.000	1.000
1800.2	137	1.6	1.927	0.535	0.446	0.000	1.000
1800.4	136	1.7	1.898	0.566	0.433	0.000	1.000
1800.6	138	1.8	1.909	0.539	0.449		1.000
1800.8	138	1.7	1.955	0.503	0.456	0.000	1.000
1801.0	136	1.8	1.970	0.482	0.432	0.000	1.000
1801.2	134	1.8	1.987	0.460	0.413	0.000	1.000
1801.4	131	1.8	2.013	0.426	0.394	0.000	1.000
1801.6	131	1.7	2.090	0.414	0.390	0.000	1.000
1801.8	137	1.7	2.185	0.413	0.442	0.000	1.000
1802.0	138	1.8	2.260	0.404	0.449	0.000	1.000
1802.2	133	1.8	2.321	0.381	0.407	0.000	1.000
1802.4	127	1.7	2.390	0.370	0.361	0.000	1.000
1802.6	123	1.7	2.473	0.351	0.331	0.000	1.000
1802.8	119	1.6	2.521	0.319	0.300	0.000	1.000
1803.0	115	1.7	2.511	0.308	0.269	0.000	1.000
1803.2	114	1.8	2.505	0.308	0.263	0.000	1.000
1803.4	114	1.9	2.511	0.308	0.263	0.000	1.000
1803.6	114	2.0	2.500	0.296	0.267	0.000	1.000
1803.8	113	2.1	2.497	0.288	0.257	0.000	1.000
1804.0	110	2.0	2.503	0.296	0.242	0.000	1.000
1804.2	110	2.0	2.497	0.313	0.238	0.000	1.000
1804.4	114	1.9	2.484	0.333	0.265	0.000	1.000
1804.6	118	1.9	2.467	0.353	0.293	0.000	1.000
1804.8	119	1.9	2.436	0.367	0.302	0.000	1.000
1805.0	120	1.9	2.422	0.369	0.305	0.000	1.000
1805.2	123	1.9	2.445	0.354	0.328	0.000	1.000
1805.4	132	1.9	2.485	0.342	0.396	0.000	1.000
1805.6	138	1.8	2.509	0.342	0.453	0.000	1.000
1805.8	134	1.8	2.514	0.352	0.418	0.000	1.000
1806.0	124	1.8	2.522	0.372	0.339	0.000	1.000
1806.2	122	1.7	2.531	0.367	0.321	0.000	1.000
1806.4	124	1.7	2.491	0.345	0.337	0.000	1.000
1806.6	129	1.6	2.419	0.328	0.378	0.000	1.000
1806.8	130	1.7	2.394	0.338	0.385	0.000	1.000
1807.0	127	1.9	2.389	0.343	0.358	0.000	1.000
1807.2	129	2.0	2.384	0.318	0.374	0.000	1.000
1807.4	132	2.2	2.360	0.297	0.403	0.000	1.000
1807.6	134	2.3	2.323	0.293	0.420	0.000	1.000
1807.8	134	2.7	2.314	0.293	0.417	0.000	1.000
1808.0	133	2.9	2.318	0.297	0.409	0.000	1.000
1808.2	135	3.2	2.294	0.303	0.425	0.000	1.000
1808.4	138	3.6	2.252	0.325	0.449	0.000	1.000
1808.6	142	3.9	2.260	0.347	0.485	0.000	1.000
1808.8	146	4.3	2.272	0.336	0.525	0.000	1.000
1809.0	148	4.6	2.268	0.325	0.548	0.000	1.000
1809.2	152	4.6	2.287	0.316	0.586	0.000	1.000
1809.4	158	4.7	2.306	0.305	0.660	0.000	1.000
1809.6	161	4.9	2.309	0.299	0.704	0.000	1.000
1809.8	162	5.0	2.323	0.289	0.716	0.000	1.000
1810.0	160	5.1	2.357	0.288	0.689	0.000	1.000
1810.2	154	5.0	2.394	0.281	0.616	0.000	1.000
1810.4	150	4.9	2.394	0.268	0.573	0.000	1.000
1810.6	156	4.8	2.372	0.272	0.632	0.000	1.000

		PERCH	4 (pag	e 2 of	data list	ing)	
DEPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE
(mRKB)	api	ohmm	g/cc	frac	frac	frac	frac
1810.8	167	5.1	2.361	0.302	0.776	0.000	1.000
1811.0	175	5.0	2.358	0.320	0.909	0.000	1.000
1811.2	180	5.0	2.378	0,325	1.000	0.000	1.000
1811.4	185	4.9	2.379	0.340	1.000	0.000	1.000
1811.6	194	4.6	2.360	0.339	1.000	0.000	1.000
1811.8	202	4.2	2.351	0.322	1.000	0.000	1.000
1812.0	209	4.0	2.338	0.328	1.000	0.000	1.000
1812.2	210	3.9	2.336	0.357	1.000	0.000	1.000
1812.4	204	4.1	2.340	0.375	1.000	0.000	1.000
1812.6	196	3.8	2.346	0.388	1.000	0.000	1.000
1812.8	193	3.8	2.361	0.399	1.000	0.000	1.000
1813.0	194	4.0	2.378	0.391	1.000	0.000	1.000
1813.2	192	4.0	2.404	0.368	1.000	0.000	1.000
1813.4	187	4.0	2.394	0.360	1.000	0.000	1.000
1813.6	183	4.0	2.360	0.364	1.000	0.000	1.000
1813.8	177	4.1	·2.360	0.366	0.951	0.000	1.000
1814.0	166	4.5	2.371	0.345	0.765	0.000	1.000
1814.2	152	4.8	2.384	0.312	0.594	0.000	1.000
1814.4	139	5.0	2.402	0.284	0.457	0.054	0.874
1814.6	121	5.2	2.403	0.262	0.318	0.141	0.698
1814.8	106	5.7	2.395	0.256	0.213	0.167	0.633
1815.0	95	6.4	2.388	0.269	0.153	0.190	0.559
1815.2	. 87	7.5	2.372	0.264	0.109	0.203	0.505
1815.4	83	8.1	2.375	0.253	0.092	0.201	0.497
1815.6	82	8.4	2.360	0.252	0.088	0.206	0.481
1815.8	80	9.3	2.334	0.251	0.077	0.216	0.441
1816.0	78	9.8	2.342	0.242	0.069	0.211	0.442
1816.2	78	10.4	2.358	0.236	0.068	0.204	0.442
1816.4	76	11.3	2.364	0.230	0.060	0.201	0.433
1816.6	77	11.6	2.374	0.235	0.067	0.199	0.426
1816.8	79	13.4	2.381	0.239	0.073	0.198	0.392
1817.0	77	13.8	2.379	0.229	0.067	0.195	0.394
1817.2	76	15.8	2.358	0.205	0.062	0.190	0.377
1817.4	75	16.6	2.359	0.209	0.057	0.193	0.364
1817.6	73	19.2	2.370	0.230	0.049	0.202	0.328
1817.8	70	21.2	2.352	0.242	0.039	0.216	0.299
1818.0	69	24.7	2.327	0.240	0.035	0.223	0.269
1818.2	69	24.9	2,319	0.236	0.032	0.224	0.268
1818.4	68	30.3	2.315	0.242	0.031	0.228	0.238
1818.6	67	31.7	2.319	0.242	0.025	0.229	0.236
1818.8	66	39.2	2.301	0.246	0.022	0.237	0.206
1819.0	65	40.7	2.249	0.252	0.018	0.258	0.189
1819.2	62	49.1	2.195	0.262	0.008	0.285	0.161
1819.4	59	53.5	2.163	0.266	0.000	0.301	0.151
1819.6	58	52.2	2.167	0.260	0.000	0.297	0.154
1819.8	60	61.7	2.187	0.258	0.000	0.289	0.146
1820.0	61	63.1	2.182	0.262	0.002	0.292	0.142
1820.2	60	73.0	2.161	0.270	0.001	0.303	0.128
1820.4	61	65.9	2.153	0.269	0.002	0.306	0.133
1820.6	62	72.5	2.147	0.262	0.006	0.304	0.126
1820.8	61	80.3	2.152	0.266	0.002	0.305	0.121
1821.0	61	77.7	2.164	0.270	0.003	0.301	0.123
1821.2	62	75.2	2.156	0.264	0.007	0.301	0.124
1821.4	60	70.4	2.139	0.259	0.001	0.308	0.128
1821.6	59	67.7	2.135	0.271	0.000	0.314	0.129
1821.8	60	71.0	2.128	0.283	0.000	0.321	0.124
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					data lis		
DEPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE
(mRKB)	api	ohmm	g/cc	frac	frac	frac	frac
1822.0	61	74.4	2.124	0.278	0.004	0.320	0.119
1822.2	60	79.8	2.139	0.278	0.001	0.315	0.118
1822.4	59	82.1	2.144	0.286	0.000	0.316	0.117
1822.6	59	83.3	2.151	0.290	0.000	0.314	0.116
1822.8	62	91.1	2.162	0.291	0.006	0.309	0.110
1823.0	62	101.2	2.168	0.288	0.007	0.305	0.105
1823.2	60	86.2	2.168	0.283	0.002	0.305	0.117
1823.4	61	87.2	2.161	0.280	0.002	0.306	0.115
1823.6	61	110.1	2.158	0.278	0.002	0.307	0.102
1823.8	60	120.9	2.148	0.275	0.000	0.310	0.098
1824.0	59	114.7	2.147	0.278	0.000	0.312	0.100
1824.2	58	113.7	2.158	0.293	0.000	0.312	0.100
1824.4	57	113.8	2.156	0.298	0.000	0.315	0.099
1824.6	57	145.0	2.153	0.284	0.000	0.312	0.089
1824.8	56	120.7	2.167	0.274	0.000	0.302	0.100
1825.0	58	109.0	2.165	0.263	0.000	0.299	0.106
1825.2	60	136.8	2.152	0.257	0.000	0.302	0.094
1825.4	61	123.5	2.143	0.269	0.003	0.310	0.096
1825.6	59	115.5	2.139	0.283	0.000	0.316	0.098
1825.8	59	142.7	2.140	0.287	0.000	0.317	0.088
1826.0	59	112.6	2.137	0.291	0.000	0.320	0.098
1826.2	59	105.2	2.139	0.296	0.000	0.321	0.102
1826.4	58	109.6	2.153	0.296	0.000	0.315	0.101
1826.6	56	100.2	2.158	0.285	0.000	0.310	0.107
1826.8	54	98.1	2.168	0.286	0.000	0.306	0.110
1827.0	55	103.8	2.176	0.298	0.000	0.307	0.106
1827.2	55	110.5	2.166	0.300	0.000	0.312	0.102
1827.4	54	116.1	2.159	0.284	0.000	0.309	0.100
1827.6	55	107.2	2.147	0.288	0.000	0.315	0.102
1827.8	55	106.0	2.124	0.303	0.000	0.329	0.099
1828.0	57	115.0	2.130	0.300	0.000	0.326	0.096
1828.2	60	118.4	2.140	0.304	0.000	0.323	0.095
1828.4	62	133.2	2.123	0.307	0.006	0.330	0.086
1828.6	62	144.3	2.102	0.299	0.006	0.335	0.081
1828.8	61	115.4	2.101	0.284	0.003	0.331	0.093
1829.0	60	112.7	2.104	0.285	0.001	0.331	0.095
1829.2	59	116.3	2.123	0.300	0.000	0.329	0.095
1829.4	58	108.8	2.137	0.306	0.000	0.325	0.099
1829.6	58	113.2	2.138	0.291	0.000	0.320	0.098
1829.8	57	117.3	2.149	0.272	0.000	0.309	0.100
1830.0	57	121.2	2.147	0.272	0.000	0.310	0.098
1830.2	56	109.2	2.124	0.287	0.000	0.324	0.099
1830.4	55	123.4	2.114	0.307	0.000	0.335	0.091
1830.6	56	93.1	2.110	0.310	0.000	0.337	0.103
1830.8 1831.0	57 58	92.1 105.5	2.116 2.126	0.310 0.323	0.000 0.000	0.335 0.335	0.104 0.098
1831.2	58	82.9	2.120	0.323	0.000	0.335	0.107
1831.4	58	53.8	2.102	0.336	0.000	0.349	0.132
1831.6	58	51.5	2.120	0.318	0.000	0.336	0.132
1831.8	56	63.9	2.120	0.310	0.000	0.324	0.129
1832.0	54	49.2	2.143	0.279	0.000	0.313	0.152
1832.2	53	43.4	2.162	0.255	0.000	0.297	0.169
1832.4	53	34.9	2.169	0.235	0.000	0.287	0.194
1832.6	52	26.9	2.159	0.235	0.000	0.291	0.219
1832.8	51	21.9	2.154	0.253	0.000	0.300	0.236
1833.0	52	18.7	2.163	0.264	0.000	0.301	0.255

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					data list	-	_
DEPTH (mRKB)	GR api	RT Ohmm	RHOB g/cc	NPHI frac	VSH frac	PHIE	SWE
(matrix)	abt	OIMali	y/cc	LLAC	LIAC	frac	frac
1833.2	53	15.1	2.169	0.274	0.000	0.301	0.283
1833.4	53	12.0	2.182	0.281	0.000	0.299	0.320
1833.6	53	10.8	2.192	0.269	0.000	0.291	0.345
1833.8	55	10.0	2.190	0.249	0.000	0.284	0.366
1834.0	57	10.1	2.178	0.252	0.000	0.290	0.359
1834.2	58	9.5	2.127	0.273	0.000	0.318	0.340
1834.4	69	9.7	2.056	0.297		bal	
1834.6	124	10.5	1.967	0.342		bal	
1834.8	183	11.6	1.905	0.405		oal	
1835.0	203	11.6	1.923	0.449		oal	
1835.2	201	10.9	2.018	0.501		bal	
1835.4	198	10.1	2.116	0.571		bal	
1835.6	195	9.7	2.181	0.604	1.000	0.000	0.000
1835.8 1836.0	192 183	9.8 10.0	2.216	0.553	1.000	0.000	0.000
1836.2	172	10.0	2.241 2.269	$0.470 \\ 0.448$	1.000	0.000	0.000
1836.4	151	10.4	2.209	0.440 0.415	0.857 0.580	0.000	0.000
1836.6	116	10.2	2.156	0.413	0.280	0.000 0.273	1.000 0.665
1836.8	89	9.0	2.189	0.324	0.120	0.273	0.833
1837.0	82	8.8	2.179	0.299	0.086	0.285	0.855
1837.2	84	8.8	2.142	0.298	0.099	0.205	0.828
1837.4	92	9.1	2.126	0.314	0.135	0.299	0.779
1837.6	104	8.7	2.113	0.338	0.203	0.295	0.754
1837.8	123	8.9	2.135	0.344	0.332	0.256	0.730
1838.0	148	9.4	2.163	0.364	0.544	0.006	1.000
1838.2	169	10.2	2.190	0.422	0.804	0.000	1.000
1838.4	176	10.8	2.182	0.507	0.928	0.000	1.000
1838.6	180	11.7	2.121	0.558	1.000	0.000	1.000
1838.8	189	12.0	2.051	0.560	1.000	0.000	1.000
1839.0	206	12.5	2.037	0.555	1.000	0.000	1.000
1839.2	222	12.6	2.071	0.507	1.000	0.000	1.000
1839.4	231	12.4	2.140	0.462	1.000	0.000	1.000
1839.6	231	12.4	2.197	0.439	1.000	0.000	1.000
1839.8	225	12.3	2.268	0.415	1.000	0.000	1.000
1840.0	216	11.7	2.291	0.419	1.000	0.000	1.000
1840.2	207	11.8	2.274	0.417	1.000	0.000	1.000
1840.4 1840.6	199	11.8	2.252	0.429	1.000	0.000	1.000
1840.8	199 197	12.0 12.1	2.170	0.483	1.000	0.000	1.000
1841.0	191	12.1	2.105	0.509	1.000	0.000	1.000
1841.2	189	12.3	2.087 2.057	0.490 0.501	1.000	0.000	1.000
1841.4	191	12.3	1.957	0.554		bal Dal	
1841.6	191	12.5	1.845	0.603		bal	
1841.8	184	12.8	1.780	0.623		bal	
1842.0	178	12.5	1.820	0.604		bal	
1842.2	177	12.8	1.922	0.550		bal	
1842.4	180	13.1	2.087	0.488	1.000	0.000	1.000
1842.6	183	12.8	2.244	0.465	1.000	0.000	1.000
1842.8	185	12.5	2.260	0.487	1.000	0.000	1.000
1843.0	187	12.2	2.211	0.524	1.000	0.000	1.000
1843.2	190	11.9	2.131	0.575	1.000	0.000	1.000
1843.4	191	11.7	1.992	0.577	Co	bal	
1843.6	187	12.3	1.820	0.543	Co	bal	
1843.8	182	12.5	1.802	0.560	Co	al	
1844.0	179	12.4	1.862	0.586		al	
1844.2	178	12.6	1.932	0.571	Co	al	

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					data lis				
DEPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE		
(mRKB)	api	ohmm	g/cc	frac	frac	frac	frac		
1844.4	179	11.9	1.938	0.538	C	oal			
1844.6	181	11.7	1.922	0.557		oal			
1844.8	184	11.4	1.982	0.594		oal			
1845.0	183	12.0	2.009	0.594 0.541					
1845.2	183					oal			
		11.5	1.967	0.493		oal			
1845.4	185	11.9	1.948	0.501		oal			
1845.6	181	11.0	1.939	0.518		oal			
1845.8	176	11.5	1.962	0.502		oal			
1846.0	173	11.4	2.031	0.482	0.878	0.000	1.000		
1846.2	173	12.2	2.127	0.482	0.876	0.000	1.000		
1846.4	176	12.1	2.219	0.501	0.916	0.000	1.000		
1846.6	175	12.3	2.287	0.479	0.911	0.000	1.000		
1846.8	169	13.6	2.311	0.448	0.807	0.000	1.000		
1847.0	166	14.5	2.279	0.444	0.765	0.000	1.000		
1847.2	171	12.9	2.242	0.426	0.842	0.000	1.000		
1847.4	178	12.5	2.207	0.421	0.958	0.000	1.000		
1847.6	183	12.1	2.206	0.447	1.000	0.000	1.000		
1847.8	187	11.5	2.132	0.484	1.000	0.000	1.000		
1848.0	186	12.1	1.991	0.502	Co	bal			
1848.2	184	12.4	1.989	0.504	Co	bal			
1848.4	179	12.3	2.108	0.512	0.986	0.000	1.000		
1848.6	174	11.9	2.182	0.513	0.890	0.000	1.000		
1848.8	171	11.5	2.226	0.488	0.839	0.000	1.000		
1849.0	170	11.4	2.253	0.422	0.829	0.000	1.000		
1849.2	173	11.9	2.258	0.368	0.880	0.000	1.000		
1849.4	179	11.9	2.235	0.355	0.981	0.000	1.000		
1849.6	187	11.5	2.191	0.381	1.000	0.000	1.000		
1849.8	190	11.7	2.120	0.451	1.000	0.000	1.000		
1850.0	188	11.4	2.012	0.505	Co	bal			
1850.2	185	11.2	1.869	0.519	Co	bal			
1850.4	185	11.2	1.764	0.496	Co	bal			
1850.6	179	10.8	1.736	0.530	Co	bal			
1850.8	170	10.9	1.784	0.642	Co	bal			
1851.0	166	10.9	1.842	0.734	Co	bal			
1851.2	167	10.2	1.864	0.731	Co	bal			
1851.4	171	10.2	1.899	0.643	Co	bal			
1851.6	176	10.0	1.978	0.538	Co	bal			
1851.8	177	10.1	2.071	0.508	0.941	0.000	1.000		
1852.0	175	10.6	2.076	0.519	0.898	0.000	1.000		
1852.2	171	10.7	1.989	0.532	Co	al			
1852.4	169	10.9	1.972	0.538	Co	al			
1852.6	168	10.8	2.057	0.519	0.793	0.000	1.000		
1852.8	168	10.8	2.156	0.501	0.788	0.000	1.000		
1853.0	170	11.3	2.213	0.482	0.822	0.000	1.000		
1853.2	174	11.4	2.212	0.438	0.890	0.000	1.000		
1853.4	174	11.3	2.139	0.444	0.883	0.000	1.000		
1853.6	169	11.2	2.066	0.506	0.802	0.000	1.000		
1853.8	164	11.3	2.064	0.527	0.740	0.000	1.000		
1854.0	165	11.2	2.111	0.474	0.752	0.000	1.000		
1854.2	171	11.5	2.181	0.460	0.846	0.000	1.000		
1854.4	179	12.3	2.218	0.471	0.974	0.000	1.000		
1854.6	180	12.4	2.177	0.444	1.000	0.000	1.000		
1854.8	177	12.2	2.160	0.408	0.949	0.000	1.000		
1855.0	176	11.7	2.165	0.399	0.931	0.000	1.000		
1855.2	182	11.6	2.178	0.397	1.000	0.000	1.000		
1855.4	187	11.6	2.241	0.374	1.000	0.000	1.000		

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		PERCH	4 (pa	an for	data list	ing)	
DEPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE
(mRKB)	api	ohmm	g/cc	frac	frac	frac	frac
	-		5,				
1855.6	188	11.7	2.282	0.367	1.000	0.000	1.000
1855.8	185	11.1	2.269	0.341	1.000	0.000	1.000
1856.0	182	11.5	2.258	0.316	1.000	0.000	1.000
1856.2	178	10.5	2.257	0.309	0.957	0.000	1.000
1856.4	175	10.3	2.307	0.326	0.906	0.000	1.000
1856.6	176	10.1	2.252	0.379	0.919	0.000	1.000
1856.8	179	10.4	2.224	0.446	0.978	0.000	1.000
1857.0	182	11.0	2.287	0.446	1.000	0.000	1.000
1857.2	184	10.5	2.315	0.390	1.000	0.000	1.000
1857.4	183	10.1	2.319	0.352	1.000	0.000	1.000
1857.6	182	10.1	2.309	0.360	1.000	0.000	1.000
1857.8	185	10.0	2.288	0.348	1.000	0.000	1.000
1858.0	185	9.6	2.262	0.350	1.000	0.000	1.000
1858.2	179	9.6	2.163	0.436	Co	bal	
1858.4	174	9.7	2.015	0.529		bal	
1858.6	169	9.3	1.988	0.566		0.000	1.000
1858.8	167	9.5	2.146	0.502		0.000	1.000
1859.0	172	9.7	2.243	0.407	0.848	0.000	1.000
1859.2	178	9.8	2.213	0.350	0.958	0.000	1.000
1859.4	179	10.0	2.135	0.398	0.973	0.000	1.000
1859.6	177	10.0	1.990	0.484	0.937	0.000	1.000
1859.8	175	10.1	1.842	0.530	0.910	0.000	1.000
1860.0	175	10.1	1.696	0.539		bal	
1860.2	175	10.1	1.587	0.565		bal	
1860.4	170	11.6	1.520	0.586		bal	
1860.6	160	12.2	1.480	0.595		bal	
1860.8	151	12.2	1.445	0.640		bal	
1861.0	141	13.5	1.416	0.721		bal	
1861.2	126	14.5	1.424	0.770		bal	
1861.4	110	15.7	1.445	0.805		bal	
1861.6	98	17.4	1.448	0.857		bal	
1861.8	100	18.9	1.439	0.873		bal	
1862.0	100	25.1	1.419	0.812		bal	
1862.2	94	29.3	1.409	0.740		bal	
1862.4	90	32.7	1.413	0.755		bal	
1862.6 1862.8	89	36.6	1.414	0.879		bal	
1863.0	89	42.0	1.409	1.039		bal	
1863.2	87 83	42.9 42.4	1.401 1.409	0.931 0.730		bal	
1863.4	78	50.4	1.409	0.714		bal	
1863.6	77	49.5	1.415	0.886		oal Dal	
1863.8	79	4J.5 51.5	1.407	0.962		bal	
1864.0	81	56.1	1.390	0.919		bal	
1864.2	82	66.5	1.383	0.899		bal	
1864.4	82	73.4	1.392	0.843		bal	
1864.6	81	64.5	1.396	0.827		bal	
1864.8	79	63.7	1.382	0.916		al	
1865.0	76	59.7	1.374	1.000		bal	
1865.2	74	67.6	1.383	1.006		bal	
1865.4	71	63.7	1.391	1.030		bal	
1865.6	69	62.3	1.391	1.004		bal	
1865.8	67	70.1	1.375	0.917		bal	
1866.0	65	62.9	1.345	0.821		bal	
1866.2	64	73.3	1.351	0.781		bal	
1866.4	65	69.9	1.373	0.720		bal	
1866.6	68	62.7	1.382	0.655		bal	

DEPTH GR RT RHOB NPHI VSH PHIE SWE 18666.8 70 68.6 1.384 0.681 Coal 1 1867.0 72 68.0 1.369 0.849 Coal 1 1867.4 73 77.2 1.354 0.858 Coal 1 1867.4 83 61.4 1.361 0.661 Coal 1 1867.8 102 59.1 1.381 0.669 Coal 1 1868.4 151 48.0 2.017 0.497 Coal 1 1868.4 167 40.4 2.297 0.326 0.783 0.000 1.000 1869.4 120 2.424 0.266 0.624 0.000 1.000 1869.4 120 2.424 0.266 0.639 0.303 0.001 1.000 1869.4 120 2.424 0.266 0.630 0.001 1.000 1869.4 120			PERCH	1_4 (pa	ge 7 of	data lis	ting)	
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1872.0 139 58.7 1.924 0.341 $Coal$ 1872.2 154 55.4 1.960 0.444 $Coal$ 1872.4 165 39.1 2.094 0.497 0.751 0.000 0.000 1872.6 167 27.1 2.162 0.503 0.784 0.000 1.000 1872.8 167 21.2 2.080 0.542 0.778 0.000 1.000 1873.0 167 15.4 1.942 0.587 $Coal$ 1873.2 170 11.9 1.935 0.581 $Coal$ 1873.4 171 8.4 2.023 0.548 0.845 0.000 0.000 1873.8 160 7.4 2.074 0.484 0.681 0.000 1.000 1874.0 147 6.3 2.063 0.514 0.534 0.024 1.000 1874.2 128 5.5 2.075 0.501 0.365 0.303 0.808 1874.4 105 5.7 2.262 0.444 0.211 0.286 1.000 1875.7 75 4.3 2.280 0.327 0.058 0.271 1.000 1875.8 76 4.2 2.298 0.327 0.076 0.253 1.000 1875.4 84 4.9 2.316 0.271 0.098 0.226 1.000 1875.8 85 5.8 2.293 0.231 0.102 0.213 1.000 1876.6 <				2.195	0.170	0.280	0.000	0.000
1872.2 154 55.4 1.960 0.444 $Coal$ 1872.4 165 39.1 2.094 0.497 0.751 0.000 0.000 1872.6 167 27.1 2.162 0.503 0.784 0.000 1.000 1872.8 167 21.2 2.080 0.542 0.778 0.000 1.000 1873.0 167 15.4 1.942 0.587 $Coal$ 1873.2 170 11.9 1.935 0.581 $Coal$ 1873.4 171 8.4 2.023 0.548 0.845 0.000 1.000 1873.6 168 7.1 2.051 0.496 0.791 0.000 1.000 1874.0 147 6.3 2.063 0.514 0.534 0.024 1.000 1874.2 128 5.5 2.075 0.501 0.365 0.303 0.808 1874.4 105 5.7 2.262 0.444 0.211 0.286 0.988 1874.4 105 5.7 2.262 0.444 0.211 0.269 1.000 1875.0 75 4.3 2.280 0.327 0.058 0.271 1.000 1875.4 84 4.9 2.316 0.271 0.098 0.226 1.000 1875.8 85 5.8 2.293 0.231 0.102 0.213 1.000 1875.4 84 4.9 2.316 0.277 0.066 0.212 1.000				1.994	0.243	Co	bal	
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1872.6 167 27.1 2.162 0.503 0.784 0.000 1.000 1872.8 167 21.2 2.080 0.542 0.778 0.000 1.000 1873.0 167 15.4 1.942 0.587 $Coal$ 1873.2 170 11.9 1.935 0.581 $Coal$ 1873.4 171 8.4 2.023 0.548 0.845 0.000 0.000 1873.6 168 7.1 2.051 0.496 0.791 0.000 1.000 1873.8 160 7.4 2.074 0.484 0.681 0.000 1.000 1874.0 147 6.3 2.063 0.514 0.534 0.024 1.000 1874.4 105 5.7 2.262 0.444 0.211 0.286 0.988 1874.6 87 4.5 2.346 0.397 0.110 0.269 1.000 1875.0 75 4.3 2.280 0.327 0.058 0.271 1.000 1875.4 84 4.9 2.316 0.271 0.098 0.226 1.000 1875.4 84 4.9 2.316 0.271 0.080 0.216 1.000 1875.4 86 5.3 2.306 0.250 0.108 0.216 1.000 1875.4 84 4.9 2.316 0.271 0.098 0.226 1.000 1876.6 86 5.3 2.306 0.250 0.108 <td></td> <td></td> <td></td> <td></td> <td></td> <td>Co</td> <td>bal</td> <td></td>						Co	bal	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1872.4	165	39.1	2.094	0.497	0.751	0.000	0.000
1873.0 167 15.4 1.942 0.587 $Coal$ 1873.2 170 11.9 1.935 0.581 $Coal$ 1873.4 171 8.4 2.023 0.548 0.845 0.000 0.000 1873.6 168 7.1 2.051 0.496 0.791 0.000 1.000 1873.8 160 7.4 2.074 0.484 0.681 0.000 1.000 1874.0 147 6.3 2.063 0.514 0.534 0.024 1.000 1874.2 128 5.5 2.075 0.501 0.365 0.303 0.808 1874.4 105 5.7 2.262 0.444 0.211 0.286 0.988 1874.6 87 4.5 2.346 0.397 0.110 0.269 1.000 1874.8 76 4.2 2.298 0.362 0.063 0.280 1.000 1875.0 75 4.3 2.280 0.327 0.058 0.271 1.000 1875.2 79 4.5 2.283 0.297 0.076 0.253 1.000 1875.6 86 5.3 2.306 0.250 0.108 0.216 1.000 1875.6 86 5.8 2.297 0.207 0.066 0.212 1.000 1876.4 77 5.6 2.297 0.276 0.064 0.220 1.000 1876.4 77 5.6 2.297 0.276 0.064 <t< td=""><td>1872.6</td><td></td><td>27.1</td><td>2.162</td><td>0.503</td><td>0.784</td><td>0.000</td><td>1.000</td></t<>	1872.6		27.1	2.162	0.503	0.784	0.000	1.000
1873.2 170 11.9 1.935 0.581 $Coal$ 1873.4 171 8.4 2.023 0.548 0.845 0.000 0.000 1873.6 168 7.1 2.051 0.496 0.791 0.000 1.000 1873.8 160 7.4 2.074 0.484 0.681 0.000 1.000 1874.0 147 6.3 2.063 0.514 0.534 0.024 1.000 1874.2 128 5.5 2.075 0.501 0.365 0.303 0.808 1874.4 105 5.7 2.262 0.444 0.211 0.286 0.988 1874.6 87 4.5 2.346 0.397 0.110 0.269 1.000 1875.0 75 4.3 2.280 0.327 0.058 0.271 1.000 1875.2 79 4.5 2.283 0.297 0.076 0.253 1.000 1875.4 84 4.9 2.316 0.271 0.098 0.226 1.000 1875.8 85 5.8 2.293 0.231 0.102 0.213 1.000 1876.4 77 5.6 2.297 0.207 0.066 0.212 1.000 1876.4 77 5.6 2.309 0.226 0.064 0.220 1.000 1876.8 79 6.6 2.309 0.261 0.073 0.223 1.000 1877.0 76 5.8 2.311 <td< td=""><td>1872.8</td><td>167</td><td>21.2</td><td>2.080</td><td>0.542</td><td>0.778</td><td>0.000</td><td>1.000</td></td<>	1872.8	167	21.2	2.080	0.542	0.778	0.000	1.000
1873.4 171 8.4 2.023 0.548 0.845 0.000 0.000 1873.6 168 7.1 2.051 0.496 0.791 0.000 1.000 1873.8 160 7.4 2.074 0.484 0.681 0.000 1.000 1874.0 147 6.3 2.063 0.514 0.534 0.024 1.000 1874.2 128 5.5 2.075 0.501 0.365 0.303 0.808 1874.4 105 5.7 2.262 0.444 0.211 0.286 0.988 1874.6 87 4.5 2.346 0.397 0.110 0.269 1.000 1874.8 76 4.2 2.298 0.362 0.063 0.280 1.000 1875.0 75 4.3 2.280 0.327 0.58 0.271 1.000 1875.2 79 4.5 2.283 0.297 0.076 0.253 1.000 1875.4 84 4.9 2.316 0.271 0.988 0.226 1.000 1876.0 80 5.8 2.311 0.213 0.080 0.205 1.000 1876.4 77 5.6 2.297 0.207 0.666 0.212 1.000 1876.4 77 5.1 2.294 0.226 0.064 0.220 1.000 1876.6 79 6.6 2.309 0.261 0.073 0.228 1.000 1877.0 76 <td< td=""><td>1873.0</td><td></td><td>15.4</td><td>1.942</td><td>0.587</td><td>Co</td><td>bal</td><td></td></td<>	1873.0		15.4	1.942	0.587	Co	bal	
1873.6 168 7.1 2.051 0.496 0.791 0.000 1.000 1873.8 160 7.4 2.074 0.484 0.681 0.000 1.000 1874.0 147 6.3 2.063 0.514 0.534 0.024 1.000 1874.2 128 5.5 2.075 0.501 0.365 0.303 0.808 1874.4 105 5.7 2.262 0.444 0.211 0.286 0.988 1874.6 87 4.5 2.346 0.397 0.110 0.269 1.000 1874.8 76 4.2 2.298 0.362 0.063 0.280 1.000 1875.0 75 4.3 2.280 0.327 0.058 0.271 1.000 1875.2 79 4.5 2.283 0.297 0.076 0.253 1.000 1875.4 84 4.9 2.316 0.271 0.098 0.226 1.000 1875.8 85 5.8 2.293 0.231 0.102 0.213 1.000 1876.0 80 5.8 2.311 0.213 0.080 0.205 1.000 1876.4 77 5.6 2.297 0.207 0.066 0.212 1.000 1876.6 79 6.6 2.309 0.261 0.073 0.229 1.000 1876.8 79 6.6 2.309 0.261 0.073 0.221 1.000 1877.0 76 <td< td=""><td>1873.2</td><td>170</td><td>11.9</td><td>1.935</td><td>0.581</td><td>Co</td><td>bal</td><td></td></td<>	1873.2	170	11.9	1.935	0.581	Co	bal	
1873.8 160 7.4 2.074 0.484 0.681 0.000 1.000 1874.0 147 6.3 2.063 0.514 0.534 0.024 1.000 1874.2 128 5.5 2.075 0.501 0.365 0.303 0.808 1874.4 105 5.7 2.262 0.444 0.211 0.286 0.988 1874.6 87 4.5 2.346 0.397 0.110 0.269 1.000 1874.8 76 4.2 2.298 0.362 0.063 0.280 1.000 1875.0 75 4.3 2.280 0.327 0.058 0.271 1.000 1875.2 79 4.5 2.283 0.297 0.076 0.253 1.000 1875.4 84 4.9 2.316 0.271 0.098 0.226 1.000 1875.6 86 5.3 2.306 0.250 0.108 0.216 1.000 1876.0 80 5.8 2.311 0.213 0.025 1.000 1876.2 77 5.6 2.297 0.207 0.066 0.212 1.000 1876.4 77 5.1 2.294 0.226 0.064 0.220 1.000 1876.6 79 6.6 2.309 0.261 0.073 0.229 1.000 1877.0 76 5.8 2.311 0.233 0.047 0.221 1.000 1877.4 73 4.2 2	1873.4	171	8.4	2.023	0.548	0.845	0.000	0.000
1874.0 147 6.3 2.063 0.514 0.534 0.024 1.000 1874.2 128 5.5 2.075 0.501 0.365 0.303 0.808 1874.4 105 5.7 2.262 0.444 0.211 0.286 0.988 1874.6 87 4.5 2.346 0.397 0.110 0.269 1.000 1874.8 76 4.2 2.298 0.362 0.063 0.280 1.000 1875.0 75 4.3 2.280 0.327 0.058 0.271 1.000 1875.2 79 4.5 2.283 0.297 0.076 0.253 1.000 1875.4 84 4.9 2.316 0.271 0.098 0.226 1.000 1875.8 85 5.8 2.293 0.231 0.102 0.213 1.000 1876.0 80 5.8 2.311 0.213 0.080 0.205 1.000 1876.2 77 5.6 2.297 0.207 0.066 0.212 1.000 1876.4 77 5.1 2.294 0.226 0.064 0.220 1.000 1876.8 79 6.6 2.309 0.261 0.073 0.229 1.000 1877.0 76 5.8 2.311 0.233 0.047 0.221 1.000 1877.4 73 4.2 2.311 0.236 0.055 0.221 1.000	1873.6	168	7.1	2.051	0.496	0.791	0.000	1.000
1874.2 128 5.5 2.075 0.501 0.365 0.303 0.808 1874.4 105 5.7 2.262 0.444 0.211 0.286 0.988 1874.6 87 4.5 2.346 0.397 0.110 0.269 1.000 1874.8 76 4.2 2.298 0.362 0.063 0.280 1.000 1875.0 75 4.3 2.280 0.327 0.058 0.271 1.000 1875.2 79 4.5 2.283 0.297 0.076 0.253 1.000 1875.4 84 4.9 2.316 0.271 0.098 0.226 1.000 1875.6 86 5.3 2.306 0.250 0.108 0.216 1.000 1875.8 85 5.8 2.293 0.231 0.102 0.213 1.000 1876.0 80 5.8 2.311 0.213 0.080 0.205 1.000 1876.2 77 5.6 2.297 0.207 0.066 0.212 1.000 1876.4 77 5.1 2.294 0.226 0.064 0.220 1.000 1876.8 79 6.6 2.309 0.261 0.073 0.229 1.000 1877.0 76 5.8 2.311 0.233 0.047 0.221 1.000 1877.4 73 4.2 2.311 0.236 0.055 0.221 1.000	1873.8	160	7.4	2.074	0.484	0.681	0.000	1.000
1874.41055.72.2620.4440.2110.2860.9881874.6874.52.3460.3970.1100.2691.0001874.8764.22.2980.3620.0630.2801.0001875.0754.32.2800.3270.0580.2711.0001875.2794.52.2830.2970.0760.2531.0001875.4844.92.3160.2710.0980.2261.0001875.6865.32.3060.2500.1080.2161.0001875.8855.82.2930.2310.1020.2131.0001876.0805.82.3110.2130.0800.2051.0001876.2775.62.2970.2070.0660.2121.0001876.4775.12.2940.2260.0640.2201.0001876.8796.62.3090.2610.0730.2291.0001877.0765.82.3110.2480.0600.2251.0001877.2734.92.3130.2330.0470.2211.0001877.4734.22.3110.2310.0480.2211.0001877.6743.42.3090.2360.0550.2211.000	1874.0	147	6.3	2.063	0.514	0.534	0.024	1.000
1874.6874.52.3460.3970.1100.2691.0001874.8764.22.2980.3620.0630.2801.0001875.0754.32.2800.3270.0580.2711.0001875.2794.52.2830.2970.0760.2531.0001875.4844.92.3160.2710.0980.2261.0001875.6865.32.3060.2500.1080.2161.0001875.8855.82.2930.2310.1020.2131.0001876.0805.82.3110.2130.0800.2051.0001876.2775.62.2970.2070.0660.2121.0001876.4775.12.2940.2260.0640.2201.0001876.8796.62.3090.2610.0730.2291.0001877.0765.82.3110.2480.0600.2251.0001877.4734.22.3130.2330.0470.2211.0001877.6743.42.3090.2360.0550.2211.000	1874.2	128	5.5	2.075	0.501	0.365	0.303	0.808
1874.8764.22.2980.3620.0630.2801.0001875.0754.32.2800.3270.0580.2711.0001875.2794.52.2830.2970.0760.2531.0001875.4844.92.3160.2710.0980.2261.0001875.6865.32.3060.2500.1080.2161.0001875.8855.82.2930.2310.1020.2131.0001876.0805.82.3110.2130.0800.2051.0001876.2775.62.2970.2070.0660.2121.0001876.4775.12.2940.2260.0640.2201.0001876.6796.02.3060.2570.0720.2281.0001876.8796.62.3090.2610.0730.2291.0001877.0765.82.3110.2480.0600.2251.0001877.2734.92.3130.2330.0470.2211.0001877.4734.22.3110.2310.0480.2211.0001877.6743.42.3090.2360.0550.2211.000	1874.4	105	5.7	2.262	0.444	0.211	0.286	0.988
1874.8764.22.2980.3620.0630.2801.0001875.0754.32.2800.3270.0580.2711.0001875.2794.52.2830.2970.0760.2531.0001875.4844.92.3160.2710.0980.2261.0001875.6865.32.3060.2500.1080.2161.0001875.8855.82.2930.2310.1020.2131.0001876.0805.82.3110.2130.0800.2051.0001876.2775.62.2970.2070.0660.2121.0001876.4775.12.2940.2260.0640.2201.0001876.6796.02.3060.2570.0720.2281.0001876.8796.62.3090.2610.0730.2291.0001877.0765.82.3110.2480.0600.2251.0001877.2734.92.3130.2330.0470.2211.0001877.4734.22.3110.2310.0480.2211.0001877.6743.42.3090.2360.0550.2211.000	1874.6	87	4.5	2.346	0.397	0.110	0.269	1.000
1875.0754.32.2800.3270.0580.2711.0001875.2794.52.2830.2970.0760.2531.0001875.4844.92.3160.2710.0980.2261.0001875.6865.32.3060.2500.1080.2161.0001875.8855.82.2930.2310.1020.2131.0001876.0805.82.3110.2130.0800.2051.0001876.2775.62.2970.2070.0660.2121.0001876.4775.12.2940.2260.0640.2201.0001876.6796.02.3060.2570.0720.2281.0001876.8796.62.3090.2610.0730.2291.0001877.0765.82.3110.2480.0600.2251.0001877.4734.22.3130.2330.0470.2211.0001877.6743.42.3090.2360.0550.2211.000	1874.8	76		2.298				
1875.2794.52.2830.2970.0760.2531.0001875.4844.92.3160.2710.0980.2261.0001875.6865.32.3060.2500.1080.2161.0001875.8855.82.2930.2310.1020.2131.0001876.0805.82.3110.2130.0800.2051.0001876.2775.62.2970.2070.0660.2121.0001876.4775.12.2940.2260.0640.2201.0001876.6796.02.3060.2570.0720.2281.0001876.8796.62.3090.2610.0730.2291.0001877.0765.82.3110.2480.0600.2251.0001877.4734.22.3130.2330.0470.2211.0001877.6743.42.3090.2360.0550.2211.000	1875.0							
1875.4844.92.3160.2710.0980.2261.0001875.6865.32.3060.2500.1080.2161.0001875.8855.82.2930.2310.1020.2131.0001876.0805.82.3110.2130.0800.2051.0001876.2775.62.2970.2070.0660.2121.0001876.4775.12.2940.2260.0640.2201.0001876.6796.02.3060.2570.0720.2281.0001876.8796.62.3090.2610.0730.2291.0001877.0765.82.3110.2480.0600.2251.0001877.4734.22.3110.2310.0480.2211.0001877.6743.42.3090.2360.0550.2211.000	1875.2							
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1876.0805.82.3110.2130.0800.2051.0001876.2775.62.2970.2070.0660.2121.0001876.4775.12.2940.2260.0640.2201.0001876.6796.02.3060.2570.0720.2281.0001876.8796.62.3090.2610.0730.2291.0001877.0765.82.3110.2480.0600.2251.0001877.2734.92.3130.2330.0470.2211.0001877.4734.22.3110.2310.0480.2211.0001877.6743.42.3090.2360.0550.2211.000		85		2.293				
1876.2775.62.2970.2070.0660.2121.0001876.4775.12.2940.2260.0640.2201.0001876.6796.02.3060.2570.0720.2281.0001876.8796.62.3090.2610.0730.2291.0001877.0765.82.3110.2480.0600.2251.0001877.2734.92.3130.2330.0470.2211.0001877.4734.22.3110.2310.0480.2211.0001877.6743.42.3090.2360.0550.2211.000	1876.0	80	5.8	2.311				
1876.4775.12.2940.2260.0640.2201.0001876.6796.02.3060.2570.0720.2281.0001876.8796.62.3090.2610.0730.2291.0001877.0765.82.3110.2480.0600.2251.0001877.2734.92.3130.2330.0470.2211.0001877.4734.22.3110.2310.0480.2211.0001877.6743.42.3090.2360.0550.2211.000	1876.2	77						
1876.6796.02.3060.2570.0720.2281.0001876.8796.62.3090.2610.0730.2291.0001877.0765.82.3110.2480.0600.2251.0001877.2734.92.3130.2330.0470.2211.0001877.4734.22.3110.2310.0480.2211.0001877.6743.42.3090.2360.0550.2211.000								
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1877.0765.82.3110.2480.0600.2251.0001877.2734.92.3130.2330.0470.2211.0001877.4734.22.3110.2310.0480.2211.0001877.6743.42.3090.2360.0550.2211.000								
1877.2734.92.3130.2330.0470.2211.0001877.4734.22.3110.2310.0480.2211.0001877.6743.42.3090.2360.0550.2211.000								
1877.4734.22.3110.2310.0480.2211.0001877.6743.42.3090.2360.0550.2211.000								
1877.6 74 3.4 2.309 0.236 0.055 0.221 1.000								

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					data list	-	
DEPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE
(mRKB)	api	ohmm	g/cc	frac	frac	frac	frac
1878.0	80	2.9	2.318	0.231	0.077	0.211	1.000
1878.2	86	3.2	2.306	0.227	0.105	0.206	1.000
1878.4	92	4.0	2.262	0.234	0.138	0.217	1.000
1878.6	96	4.9	2.271	0.241	0.156	0.212	1.000
1878.8	96	5.5	2.332	0.242	0.156	0.192	1.000
1879.0	95	5.4	2.325	0.248	0.151	0.198	1.000
1879.2	95	5.1	2.287	0.256	0.151	0.214	1.000
1879.4	95	4.6	2.288	0.247	0.151	0.209	1.000
1879.6	94	4.8	2.300	0.239	0.149	0.202	1.000
1879.8	96	5.2	2.273	0.251	0.155	0.202	1.000
1880.0	100	5.4	2.255	0.260	0.133	0.220	1.000
1880.2	105	6.1	2.277	0.259	0.208	0.220	1.000
1880.4	107	7.0	2.324	0.239	0.200	0.193	1.000
1880.6	107	6.7	2.371	0.296	0.223	0.190	1.000
1880.8	106	6.5	2.371	0.304	0.215	0.193	1.000
1881.0	104	6.4	2.341	0.304	0.210	0.207	1.000
1881.2	98	6.1	2.341	0.280	0.167	0.207	1.000
1881.4	98 89	6.3		0.280	0.187	0.212	1.000
1881.6			2.312				
	83	7.1	2.298	0.227	0.093	0.212	1.000
1881.8	81	7.7	2.328	0.218	0.083	0.201	1.000
1882.0	81	8.1	2.374	0.203	0.082	0.179	1.000
1882.2	81	8.1	2.418	0.189	0.082	0.160	1.000
1882.4	81	8.0	2.461	0.175	0.082	0.141	1.000
1882.6	81	7.9	2.410	0.163	0.082	0.150	1.000
1882.8	81	7.4	2.343	0.176	0.082	0.178	1.000
1883.0	81	7.1	2.352	0.189	0.082	0.181	1.000
1883.2	81	6.5	2.346	0.180	0.082	0.179	1.000
1883.4	81	5.5	2.304	0.172	0.082	0.191	1.000
1883.6	81	5.7	2.291	0.170	0.081	0.195	1.000
1883.8	77	6.5	2.269	0.172	0.067	0.208	1.000
1884.0	76	6.6	2.261	0.176	0.059	0.214	1.000
1884.2	77	6.5	2.271	0.180	0.064	0.211	1.000
1884.4	77	5.6	2.260	0.179	0.066	0.214	1.000
1884.6	77	5.6	2.250	0.178	0.065	0.218	1.000
1884.8	83	6.1	2.219	0.190	0.092	0.228	1.000
1885.0	89	6.3	2.246	0.204	0.119	0.216	1.000
1885.2	87	6.4	2.252	0.208	0.110	0.217	1.000
1885.4	83	6.6	2.240	0.227	0.091	0.234	1.000
1885.6	78	6.7	2.206	0.253	0.070	0.262	1.000
1885.8	75	6.9	2.203	0.264	0.056	0.271	1.000
1886.0	75	7.0	2.210	0.259	0.059	0.265	1.000
1886.2	82	7.2	2.222	0.242	0.088	0.247	1.000
1886.4	89	7.3	2.237	0.232	0.119	0.231	1.000
1886.6	89	7.5	2.229	0.239	0.120	0.236	1.000
1886.8	86	7.6	2.209	0.241	0.105	0.248	1.000
1887.0	81	6.3	2.198	0.250	0.085	0.261	1.000
1887.2	76	5.4	2.200	0.263	0.061	0.270	1.000
1887.4	72	5.0	2.223	0.257	0.044	0.264	1.000
1887.6	73	5.1	2.235	0.261	0.048	0.260	1.000
1887.8	74	5.3	2.207	0.275	0.053	0.274	1.000
1888.0	74	5.4	2.197	0.274	0.052	0.278	1.000
1888.2	73	5.4	2.222	0.260	0.050	0.264	1.000
1888.4	73	5.4	2.227	0.257	0.050	0.261	1.000
1888.6	73	5.8	2.215	0.251	0.050	0.263	1.000
1888.8	73	6.4	2.200	0.246	0.048	0.267	1.000
1889.0	72	6.9	2.209	0.244	0.043	0.265	1.000

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		DEDCL	I ())	an 9 of	data lis	ting)	
DEPTH	GR	RT	RHOB	NPHI		PHIE	CMF
					VSH		SWE
(mRKB)	api	ohmm	g/cc	frac	frac	frac	frac
1889.2	70	7.2	2.243	0.244	0.035	0.254	1.000
1889.4	68	7.3	2.263	0.244	0.029	0.248	1.000
1889.6	67	7.9	2.259	0.244	0.026	0.250	1.000
1889.8	68	9.5	2.264	0.243	0.028	0.247	0.994
1890.0	68	7.7	2.262	0.235	0.030	0.244	1.000
1890.2	68	5.7	2.255	0.224	0.028	0.243	1.000
1890.4	67	5.9	2.257	0.223		0.243	1.000
1890.6	67	6.1	2.277	0.232	0.026	0.239	1.000
1890.8	66	6.2	2.307	0.238	0.023	0.231	1.000
1891.0	65	6.0	2.305	0.248	0.020	0.237	1.000
1891.2	66	5.3	2.277	0.261	0.021	0.251	1.000
1891.4	67	4.8	2.231	0.264	0.025	0.268	1.000
1891.6	69	4.0	2.185	0.261	0.033	0.282	1.000
1891.8	73	4.0	2.176	0.249	0.048	0.278	1.000
1892.0	77	4.5	2.181	0.245	0.064	0.270	1.000
1892.2	78	4.4	2.189	0.246	0.072	0.266	1.000
1892.4	77	3.9	2.182	0.241	0.064	0.268	1.000
1892.6	74	4.9	2.219	0.238	0.052	0.256	1.000
1892.8	73	5.8	2.262	0.235	0.049	0.240	1.000
1893.0	75	5.7	2.278	0,225	0.055	0.228	1.000
1893.2	75	5.5	2.295	0.203	0.055	0.214	1.000
1893.4	72	5.2	2.306	0.187	0.043	0.206	1.000
1893.6	71	4.7	2.296	0.184	0.042	0.209	1.000
1893.8	75	5.4	2.316	0.182	0.059	0.197	1.000
1894.0	80	5.7	2.324	0.181	0.078	0.189	1.000
1894.2	82	5.9	2.309	0.188	0.086	0.195	1.000
1894.4	80	5.7	2.304	0.200	0.079	0.203	1.000
1894.6	79	5.4	2.326	0.207	0.073	0.199	1.000
1894.8	77	5.2	2.272	0.204	0.067	0.220	1.000
1895.0	76	5.3	2.128	0.190	Co	bal	
1895.2	74	5.4	2.015	0.178	Co	bal	
1895.4	73	5.4	1.977	0.187	Co	bal	
1895.6	71	5.2	1.981	0.201	Co	bal	
1895.8	69	5.0	2.036	0.206	Co	bal	
1896.0	70	5.1	2.083	0.236	0.037	0.000	0.000
1896.2	67	6.2	2.133	0.280	0.025	0.311	1.000
1896.4	62	6.7	2.167	0.321	0.006	0.318	0.964
1896.6	60	5.9	2.179	0.343	0.001	0.324	1.000
1896.8	62	5.9	2.173	0.327	0.008	0.318	1.000
1897.0	62	6.1	2.170	0.311	0.007	0.312	1.000
1897.2	61	5.0	2.182	0.290	0.005	0.301	1.000
1897.4	60	5.0	2.199	0.269	0.000	0.288	1.000
1897.6	58	5.3	2.190	0.243	0.000	0.282	1.000
1897.8	57	5.3	2.200	0.237	0.000	0.276	1.000
1898.0	59	5.1	2.224	0.255	0.000	0.274	1.000
1898.2	61	5.1	2.228	0.276	0.003	0.279	1.000
1898.4	62	4.4	2.227	0.278	0.007	0.279	1.000
1898.6	60	3.9	2.269	0.265	0.000	0.261	1.000
1898.8	56	3.7	2.274	0.257	0.000	0.256	1.000
1899.0	56	3.7	2.261	0.264	0.000	0.263	1.000
1899.2	56	3.8	2.272	0.272	0.000	0.264	1.000
1899.4 1800 6	55	3.7	2.260	0.279	0.000	0.271	1.000
1899.6 1899.8	54 56	3.6	2.230	0.294	0.000	0.287	1.000

1899.8

1900.0

1900.2

56

60

64

3.7

3.8

3.8

2.223

2.215

2.230

0.289

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PERCH_4 (page 10 of data listing) DEPTH (mRKB) GR api RT ohum R/CC Frac Frac Frac Frac 1900.4 69 4.0 2.246 0.258 0.032 0.259 1.000 1900.8 71 4.1 2.221 0.262 0.042 0.264 1.000 1901.0 74 4.9 2.212 0.233 0.052 0.264 1.000 1901.4 83 4.5 2.232 0.293 0.094 0.262 1.000 1901.6 88 5.0 2.231 0.287 0.114 0.225 1.000 1902.0 85 5.6 2.173 0.267 0.074 0.274 1.000 1902.4 79 4.0 2.172 0.267 0.064 0.273 1.000 1902.6 77 3.8 2.155 0.267 0.064 0.273 1.000 1903.0 77 4.0 2.103 0.282 0.263 1.000 <th></th> <th></th> <th>PERCH</th> <th>4 (pa</th> <th>re 10 of</th> <th>data li</th> <th>sting)</th> <th></th>			PERCH	4 (pa	re 10 of	data li	sting)	
(mRKB) api ohumm g/cc frac frac frac frac 1900.4 69 4.0 2.246 0.258 0.032 0.259 1.000 1900.8 71 4.1 2.221 0.262 0.042 0.267 1.000 1901.0 74 4.9 2.212 0.253 0.052 0.264 1.000 1901.4 83 4.5 2.221 0.233 0.094 0.262 1.000 1901.6 88 5.0 2.231 0.282 0.103 0.277 1.000 1902.0 85 5.6 2.173 0.282 0.103 0.277 1.000 1902.4 79 4.0 2.175 0.267 0.074 0.223 1.000 1902.6 77 3.8 2.151 0.271 0.664 0.291 1.000 1903.2 83 4.4 2.213 0.280 0.148 0.262 1.000 1903.6 94	DEPTH	GR			-		-	SWE
1900.67I4.12.2210.2620.0420.2671.0001901.0744.32.2020.2470.0450.2681.0001901.2784.92.2120.2330.0940.2621.0001901.4834.52.2320.2330.0940.2621.0001901.6885.02.2310.2870.1140.2551.0001902.8885.62.1730.2820.1030.2741.0001902.4794.02.1720.2670.0740.2731.0001902.8753.92.1550.2670.0660.2911.0001903.0774.02.2000.2710.0640.2731.0001903.4915.12.1880.2750.1290.2631.0001903.4915.12.1880.2810.1480.2611.0001903.8955.42.2050.3040.1540.2611.0001904.0955.22.1880.3280.1480.2621.0001904.4895.12.1440.2710.1210.2801.0001904.4895.12.1480.3220.1260.2711.0001904.6865.12.1770.2910.1080.2781.0001904.6877.22.1530.2840.1110.2840.9461905.6787.82.	(mRKB)	api	ohmm					
1900.67I4.12.2210.2620.0420.2671.0001901.0744.32.2020.2470.0450.2681.0001901.2784.92.2120.2330.0940.2621.0001901.4834.52.2320.2330.0940.2621.0001901.6885.02.2310.2870.1140.2551.0001902.8885.62.1730.2820.1030.2741.0001902.4794.02.1720.2670.0740.2731.0001902.8753.92.1550.2670.0660.2911.0001903.0774.02.2000.2710.0640.2731.0001903.4915.12.1880.2750.1290.2631.0001903.4915.12.1880.2810.1480.2611.0001903.8955.42.2050.3040.1540.2611.0001904.0955.22.1880.3280.1480.2621.0001904.4895.12.1440.2710.1210.2801.0001904.4895.12.1480.3220.1260.2711.0001904.6865.12.1770.2910.1080.2781.0001904.6877.22.1530.2840.1110.2840.9461905.6787.82.				-				
1900.8 72 4.3 2.202 0.247 0.045 0.268 1.000 1901.2 78 4.9 2.212 0.253 0.052 0.264 1.000 1901.4 83 4.5 2.232 0.293 0.094 0.262 1.000 1901.6 88 5.0 2.231 0.287 0.114 0.255 1.000 1902.2 82 4.9 2.173 0.282 0.103 0.277 1.000 1902.4 79 4.0 2.172 0.267 0.056 0.291 1.000 1902.6 77 3.8 2.151 0.274 0.063 0.223 1.000 1903.0 77 4.0 2.200 0.271 0.064 0.263 1.000 1903.4 91 5.1 2.188 0.308 0.152 0.263 1.000 1903.4 91 5.1 2.133 0.281 0.100 1.000 1904.8 95 5.4	1900.4	69	4.0	2.246	0.258	0.032	0.259	1.000
1901.0 74 4.9 2.212 0.253 0.062 0.264 1.000 1901.4 83 4.5 2.232 0.289 0.069 0.271 1.000 1901.4 83 4.5 2.232 0.287 0.114 0.255 1.000 1901.8 88 5.5 2.209 0.304 0.118 0.268 1.000 1902.2 82 4.9 2.170 0.258 0.867 0.274 1.000 1902.4 79 4.0 2.172 0.267 0.074 0.273 1.000 1902.8 75 3.9 2.155 0.267 0.074 0.273 1.000 1903.7 73 4.4 2.213 0.282 0.094 0.264 1.000 1903.6 94 5.4 2.175 0.280 0.148 0.265 1.000 1903.8 95 5.4 2.205 0.304 0.154 0.261 1.000 1904.4 89 5.1 2.144 0.271 0.212 1.026 1.000 19	1900.6	71°	4.1	2.221	0.262	0.042	0.267	1.000
1901.2 78 4.9 2.218 0.289 0.069 0.271 1.000 1901.6 88 5.5 2.232 0.293 0.094 0.262 1.000 1901.6 88 5.5 2.231 0.287 0.114 0.255 1.000 1902.0 85 5.6 2.173 0.282 0.103 0.277 1.000 1902.4 79 4.0 2.172 0.267 0.064 0.273 1.000 1902.8 77 3.8 2.151 0.274 0.063 0.293 1.000 1903.0 77 4.0 2.200 0.271 0.064 0.263 1.000 1903.4 91 5.1 2.188 0.308 0.152 0.263 1.000 1903.4 91 5.1 2.188 0.308 0.152 0.261 1.000 1904.4 94 5.4 2.218 0.308 0.152 0.261 1.000 1904.4 89 5.2 2.188 0.308 0.152 0.261 1.000 19	1900.8	72	4.3	2.202	0.247	0.045	0.268	1.000
1901.4834.52.2320.2930.0940.2621.0001901.6885.02.2310.2870.1140.2551.0001902.0855.62.1730.2820.1030.2771.0001902.2824.92.1700.2580.0870.2741.0001902.4794.02.1720.2670.0740.2791.0001902.6773.82.1510.2740.0630.2931.0001902.8753.92.1550.2670.0560.2731.0001903.0774.02.2000.2710.0640.2731.0001903.4915.12.1880.2820.0940.2641.0001903.8955.42.2050.3040.1540.2611.0001904.9955.22.1880.3080.1520.2691.0001904.4895.12.1440.2710.1210.2801.0001904.6865.12.1770.2910.1080.2781.0001905.0945.42.2280.3190.1450.2621.0001905.6787.82.1650.2440.1110.2840.9461905.6787.82.1650.2460.0710.2750.9921906.7758.02.1850.2210.0620.2610.9921906.7768.32.	1901.0	74	4.9	2.212	0.253	0.052	0.264	1.000
1901.6885.02.2310.2870.1140.2551.0001902.0855.62.2090.3040.1180.2681.0001902.2824.92.1700.2820.0370.2711.0001902.4794.02.1720.2670.0740.2731.0001902.6773.82.1510.2740.0630.2931.0001903.8753.92.1550.2670.0640.2731.0001903.4915.12.1880.2750.1290.2631.0001903.6945.42.1750.2800.1480.2651.0001903.6945.42.2150.3040.1540.2611.0001904.0955.22.1880.3080.1520.2611.0001904.4895.12.1770.2910.1080.2711.0001904.585.42.2280.3190.1450.2621.0001904.6865.12.1770.2910.1080.2711.0001905.7945.42.2280.3190.1450.2621.0001905.8768.32.1850.2210.0670.2750.9921906.0778.42.1910.3060.1380.2680.9891906.2758.02.1850.2210.0660.2860.9921905.6787.82.1	1901.2	78	4.9	2.218	0.289	0.069	0.271	1.000
1901.8 88 5.5 2.209 0.304 0.118 0.268 1.000 1902.2 82 4.9 2.170 0.282 0.103 0.277 1.000 1902.4 79 4.0 2.172 0.267 0.074 0.279 1.000 1902.6 77 3.8 2.151 0.267 0.063 0.293 1.000 1903.0 77 4.0 2.200 0.271 0.064 0.273 1.000 1903.4 91 5.1 2.188 0.325 0.094 0.263 1.000 1903.6 94 5.4 2.175 0.280 0.148 0.265 1.000 1903.8 5 5.4 2.205 0.304 0.152 0.269 1.000 1904.4 89 5.1 2.144 0.271 0.121 0.281 1.000 1905.2 92 6.4 2.228 0.319 0.145 0.262 1.000 1904.4 89	1901.4	83	4.5	2.232	0.293	0.094	0.262	1.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1901.6	88	5.0	2.231	0.287	0.114	0.255	1.000
1902.2824.92.1700.2580.0870.2741.0001902.4794.02.1720.2670.0740.2791.0001902.6773.82.1550.2670.0560.2931.0001903.0774.02.2000.2710.0640.2731.0001903.2834.42.2130.2820.0940.2641.0001903.4915.12.1880.2750.1290.2631.0001903.6945.42.1750.2800.1480.2651.0001904.0955.22.1880.3080.1520.2691.0001904.4895.12.11440.2710.1281.0001904.4895.12.1770.2910.1080.2781.0001904.8905.22.2180.3220.1260.2711.0001905.9945.42.1770.2910.1080.2781.0001905.4877.22.1530.2840.1110.2861.0001905.5768.32.1850.2210.6620.2610.9921906.0778.42.1910.3060.1380.2681.0001905.6788.02.1850.2370.0620.2610.9921906.6748.02.1660.2480.5930.2770.9671906.6748.02.1650	1901.8	88	5.5	2.209	0.304	0.118	0.268	1.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1902.0	85	5.6	2.173	0.282	0.103	0.277	1.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1902.2	82	4.9	2.170	0.258	0.087	0.274	1.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1902.4	79	4.0	2.172	0.267	0.074	0.279	1.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1902.6	77	3.8	2.151	0.274	0.063	0.293	1.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1902.8	75	3.9	2.155	0.267	0.056	0.291	1.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1903.0	77	4.0	2.200	0.271	0.064	0.273	1.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1903.2	83	4.4	2.213	0.282	0.094	0.264	1.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1903.4	91	5.1	2.188	0.275	0.129	0.263	1.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1903.6	94	5.4	2.175	0.280	0.148	0.265	1.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1903.8	95	5.4	2.205	0.304	0.154	0.261	1.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		95	5.2	2.188	0.308	0.152	0.269	1.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1904.2		5.1	2.133	0.281	0.147	0.281	1.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1904.4			2.144	0.271	0.121	0.280	1.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$					0.291	0.108	0.278	1.000
$\begin{array}{cccccccccccccccccccccccccccccccccccc$								1.000
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1910.61094.82.1690.3160.2360.2571.0001910.81074.72.1630.2940.2210.2561.0001911.01074.12.1820.2690.2190.2401.0001911.21093.42.1850.2670.2350.2341.000	1910.2	112	5.5	2.179	0.308	0.253	0.246	1.000
1910.81074.72.1630.2940.2210.2561.0001911.01074.12.1820.2690.2190.2401.0001911.21093.42.1850.2670.2350.2341.000	1910.4	112	5.2	2.170	0.314	0.250	0.253	1.000
1911.01074.12.1820.2690.2190.2401.0001911.21093.42.1850.2670.2350.2341.000					0.316	0.236	0.257	1.000
1911.2 109 3.4 2.185 0.267 0.235 0.234 1.000						0.221	0.256	
1911.4 114 4.5 2.205 0.281 0.265 0.224 1.000								
	1911.4	114	4.5	2.205	0.281	0.265	0.224	1.000

		PERCH	1_4 (pa	ge 11 of	data li	sting)	
DEPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE
(mRKB)	api	ohmm	g/cc	frac	frac	frac	frac
1911.6	116	5.4	2.228	0.296	0.280	0.218	1.000
1911.8	117	4.8	2.180	0.290	0.287	0.210	1.000
1912.0	119	4.1	2.138	0.205	0.299	0.231	1.000
1912.2	121	3.6	2.140	0.316	0.299	0.247	
1912.4	119			0.318			1.000
1912.4	115	3.6	2.159		0.297	0.241	1.000
	115	3.9	2.175	0.264	0.275	0.227	1.000
1912.8		5.5	2.205	0.255	0.310	0.203	1.000
1913.0	129	5.7	2.246	0.269	0.375	0.154	1.000
1913.2	135	5.8	2.285	0.287	0.423	0.102	1.000
1913.4	140	6.2	2.241	0.295	0.466	0.070	1.000
1913.6	146	6.7	2.241	0.307	0.528	0.017	1.000
1913.8	153	7.1	2.262	0.336	0.603	0.000	1.000
1914.0	159	6.0	2.272	0.326	0.671	0.000	1.000
1914.2	169	5.6	2.271	0.303	0.804	0.000	1.000
1914.4	178	5.9	2.257	0.310	0.957	0.000	1.000
1914.6	181	6.0	2.240	0.333	1.000	0.000	1.000
1914.8	185	6.3	2.236	0.321	1.000	0.000	1.000
1915.0	190	6.8	2.281	0.295	1.000	0.000	1.000
1915.2	188	7.5	2.376	0.301	1.000	0.000	1.000
1915.4	184	7.6	2.426	0.327	1.000	0.000	1.000
1915.6	179	7.4	2.449	0.333	0.978	0.000	1.000
1915.8	178	7.4	2.444	0.320	0.952	0.000	1.000
1916.0	182	7.7	2.430	0.324	1.000	0.000	1.000
1916.2	187	7.5	2.419	0.336	1.000	0.000	1.000
1916.4	183	7.3	2.429	0.352	1.000	0.000	1.000
1916.6	175	7.5	2.408	0.355	0.903	0.000	1.000
1916.8	169	7.9	2.380	0.336	0.806	0.000	1.000
1917.0	170	8.2	2.377	0.352	0.818	0.000	1.000
1917.2	171	8.2	2.376	0.422	0.832	0.000	1.000
1917.4	167	8.3	2.379	0.482	0.785	0.000	1.000
1917.6	167	8.4	2.367	0.509	0.779	0.000	1.000
1917.8	171	8.3	2.212	0.560		bal	
1918.0	176	8.6	1.965	0.609		bal	
1918.2	180	8.9	1.891	0.610		bal	
1918.4	182	8.6	1.949	0.582		bal	
1918.6	176	8.0	2.003	0.546		bal	
1918.8	168	7.1	1.833	0.528		bal	
1919.0	165	6.7	1.631	0.527		bal	
1919.2	166	6.4	1.556	0.539		bal	
1919.4	160	6.3	1.551	0.566		bal	
1919.6	147	5.5	1.586	0.590		bal	
1919.8	142	5.2	1.640	0.602		bal	
1920.0	138	6.6	1.722	0.600		bal	
1920.2	121	9.4	1.853	0.569		bal	
1920.4	105	13.4	1.992	0.518	Co	bal	
1920.6	110	18.5	2.079	0.479	Co	bal	
1920.8	139	19.3	2.116	0.468	0.458	0.128	0.661
1921.0	169	9.8	2.123	0.471	0.812	0.000	1.000
1921.2	196	7.9	2.127	0.477	1.000	0.000	1.000
1921.4	216	7.1	2.133	0.488	1.000	0.000	1.000
1921.6	225	9.6	2.139	0.503	1.000	0.000	1.000
1921.8	217	9.9	2.155	0.511	1.000	0.000	1.000
1922.0	205	7.3	2.179	0.514	1.000	0.000	1.000
1922.2	192	6.0	2.195	0.530	1.000	0.000	1.000
1922.4	172	6.0	2.186	0.536	0.850	0.000	1.000
1922.6	155	6.7	2.167	0.550	0.623	0.000	1.000

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		PERCH	_4 (pag	e 12 of	data lis	ting)	
DEPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE
(mRKB)	api	ohmm	g/cc	frac	frac	frac	frac
1922.8	151	10.0	2.164	0.611	0.576	0.000	1.000
1923.0	157	9.8	2.184	0.689	0.654	0.000	1.000
1923.2	163	14.2	2.201	0.677	0.724	0.000	1.000
1923.4	166	14.8	2.207	0.617	0.762	0.000	1.000
1923.6	155	13.8	2.218	0.549	0.625	0.000	1.000
1923.8	140	14.9	2.229	0.502	0.469	0.103	0.746
1924.0	134	15.7	2.230	0.469	0.420	0.165	0.607
1924.2	140	15.4	2.226	0.467	0.466	0.102	0.738
1924.4	147	12.0	2.230	0.483	0.538	0.014	1.000
1924.6	153	10.5	2.229	0.491	0.605	0.000	1.000
1924.8	159	12.1	2.203	0.516	0.669	0.000	1.000
1925.0	163	17.9	2.124	0.564	0.729	0.000	1.000
1925.2	165	16.0	2.052	0.575	Co	al	
1925.4	161	16.7	2.030	0.536	Cc	al	
1925.6	157	18.7	2.083	0.538	Co	al	
1925.8	153	18.7	2.115	0.556	Co	al	
1926.0	147	20.6	1.994	0.547	Co	al	
1926.2	141	22.4	1.762	0.534		al	
1926.4	136	22.7	1.560	0.568		al	
1926.6	131	14.9	1.441	0.625		al	
1926.8	126	9.0	1.379	0.631		al	
1927.0	122	6.8	1.403	0.626		al	
1927.2	118	6.2	1.542	0.648		al	
1927.4	114	6.6	1.731	0.597		al	
1927.6	110	7.1	1.984	0.493		al	
1927.8	108	6.9	2.207	0.413		al	1 000
1928.0	109	6.4	2.244	0.364	0.232	0.255	1.000
1928.2	112	6.0	2.204	0.330	0.251	0.248	1.000 1.000
1928.4	115	6.1	2.210	0.290 0.262	0.271 0.292	0.224 0.194	1.000
1928.6 1928.8	118 121	6.6 7.1	2.248 2.288	0.282	0.292	0.194	1.000
1929.0	121	7.4	2.319	0.243	0.340	0.146	1.000
1929.2	131	7.3	2.320	0.243	0.389	0.111	1.000
1929.4	138	7.1	2.295	0.243	0.451	0.071	1.000
1929.6	145	6.9	2.268	0.293	0.517	0.024	1.000
1929.8	155	6.8	2.247	0.300	0.627	0.000	1.000
1930.0	165	6.5	2.232	0.295	0.756	0.000	1.000
1930.2	169	5.8	2.247	0.306	0.812	0.000	1.000
1930.4	172	5.4	2.292	0.331	0.859	0.000	1.000
1930.6	183	5.0	2.351	0.355	1.000	0.000	1.000
1930.8	201	4.6	2.386	0.352	1.000	0.000	1.000
1931.0	214	4.4	2.403	0.334	1.000	0.000	1.000
1931.2	209	4.6	2.379	0.296	1.000	0.000	1.000
1931.4	180	4.9	2.373	0.253	0.999	0.000	1.000
1931.6	145	5.2	2.368	0.221	0.517	0.013	1.000
1931.8	116	5.6	2.316	0.201	0.282	0.148	1.000
1932.0	97	6.0	2.269	0.197	0.162	0.194	1.000
1932.2	86	6.5	2.268	0.198	0.105	0.209	1.000
1932.4	80	7.1	2.279	0.207	0.080	0.215	1.000
1932.6	76	7.8	2.273	0.210	0.063	0.222	1.000
1932.8	73	8.2	2.262	0.199	0.049	0.226	1.000
1933.0	76	9.0	2.253	0.197	0.060	0.225	1.000
1933.2	79	9.6	2.290	0.203	0.075	0.210	1.000
1933.4	82	9.7	2.345	0.206	0.089	0.188	1.000
1933.6	89 102	9.2	2.400	0.215 0.233	0.123 0.188	0.168 0.162	1.000 1.000
1933.8	102	5.9	2.397	0.233	Ŷ.TOO	0.104	±. 000

		PERCH	(4 (pa	ge 13 of	data li	sting)	
DEPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE
(mRKB)	api	ohmm	g/cc	frac	frac	frac	frac
1934.0	120	6.5	2.350	0.249	0.304	0.153	1.000
1934.2	137	9.2	2.301	0.258	0.439	0.077	1.000
1934.4	141	8.3	2.300	0.272	0.479	0.048	1.000
1934.6	141	5.7	2.346	0.284	0.479	0.046	1.000
1934.8	140	5.9	2.409	0.292	0.468	0.048	1.000
1935.0	144	7.8	2.462	0.307	0.508	0.020	1.000
1935.2	152	11.9	2.494	0.304	0.590	0.000	1.000
1935.4	155	13.7	2.509	0.279	0.626	0.000	1.000
1935.6	151	13.4	2.487	0.249	0.579	0.000	1.000
1935.8	148	13.1	2.448	0.240	0.546	0.001	1.000
1936.0	149	12.2	2.426	0.246	0.563	0.000	1.000
1936.2	152	11.9	2.409	0.247	0.589	0.000	1.000
1936.4	151	11.3	2.380	0.248	0.582	0.000	1.000
1936.6	148	9.5	2.338	0.253	0.548	0.001	1.000
1936.8	140	7.1	2.297	0.252	0.471	0.051	1.000
1937.0	131	6.1	2.277	0.252	0.395	0.120	1.000
1937.2	127	6.7	2.268	0.271	0.357	0.170	1.000
1937.4	132	8.5	2.221	0.305	0.396	0.151	0.912
1937.6	141	11.0	2.200	0.358	0.477	0.075	0.853
1937.8	147	12.8	2.223	0.415	0.536	0.015	1.000
1938.0	145	13.4	2.237	0.404	0.518	0.032	0.991
1938.2	136	12.0	2.276	0.343	0.432	0.110	0.797
1938.4	123	10.2	2.287	0.302	0.327	0.191	0.865
1938.6	115	8.2	2.261	0.285	0.269	0.206	1.000
1938.8	108	7.2	2.257	0.278	0.230	0.213	1.000
1939.0	102	7.4	2.237	0.274	0.193	0.227	1.000
1939.2	101	7.7	2.204	0.270	0.186	0.240	0.991
1939.4	102	7.1	2.196	0.275	0.191	0.244	1.000
1939.6	103	6.0	2.210	0.296	0.198	0.245	1.000
1939.8	105	5.3	2.237	0.286	0.207	0.229	1.000
1940.0	107	6.2	2.277	0.253	0.223	0.197	1.000
1940.2	110	8.2	2.321	0.226	0.237	0.168	1.000
1940.4	113	8.9	2.350	0.201	0.261	0.142	1.000
1940.6	120	9.0	2.375	0.180	0.304	0.113	1.000
1940.8	124	10.0	2.394	0.172	0.337	0.095	1.000
1941.0	126	10.2	2.415	0.171	0.351	0.084	1.000
1941.2	129	9.5	2.423	0.168	0.374	0.065	1.000
1941.4	133	9.7	2.412	0.163	0.412	0.046	1.000
1941.6	143	10.6	2.395	0.156	0.497	0.013	1.000
1941.8	152	11.0	2.406	0.144	0.592	0.000	1.000
1942.0	154	13.3	2.435	0.134	0.611	0.000	1.000
1942.2	140		2.425	0.123	0.468	0.013	1.000
1942.4	123	15.1	2.452	0.116	0.331	0.053	1.000
1942.6	109	15.5	2.507	0.105	0.232	0.055	1.000
1942.8	98	15.4	2.522	0.086	0.166	0.058	1.000
1943.0	90	15.6	2.531	9.074	0.127	0.059	1.000
1943.2	87	18.0	2.580	0.064	0.114	0.042	1.000
1943.4	86	22.4	2.608	0.051	0.105	0.029	1.000
1943.6	83	33.0	2.626	0.040	0.093	0.022	1.000
1943.8	81	39.3	2.644	0.033	0.081	0.015	1.000
1944.0	80	45.5	2.657	0.028	0.077	0.010	1.000
1944.2	81	74.8	2.673	0.025	0.083	0.003	1.000
1944.4	82	94.3	2.673	0.024	0.089	0.001	1.000
1944.6	80	98.1	2.662	0.026	0.077	0.008	1.000
1944.8	77	99.7	2.671	0.025	0.066	0.008	1.000
1945.0	75	87.4	2.677	0.021	0.057	0.006	1.000

	PERCH_4 (page 14 of data listing)										
DEPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE				
(mRKB)	api	ohmm	g/cc	frac	frac	frac	frac				
							1 000				
1945.2	76	149.0	2.692	0.018	0.059	0.001	1.000				
1945.4	76	151.5	2.732	0.018	0.063	0.001	1.000				
1945.6	76	129.2	2.741	0.017	0.059	0.001	1.000				
1945.8	74	128.4	2.717	0.015	0.051	0.001	1.000				
1946.0	72	145.2	2.709	0.014	0.043	0.001	1.000				
1946.2	71	184.1	2.711	0.013	0.040	0.001	1.000				
1946.4	70	146.2	2.744	0.013	0.038	0.001	1.000				
1946.6	71	163.1	2.787	0.013	0.041	0.001	1.000				
1946.8	73	186.7	2.757	0.014	0.049	0.001	1.000				
1947.0	74	226.3	2.730	0.014	0.051	0.001	1.000				
1947.2	72	168.3	2.734	0.013	0.045	0.001	1.000				
1947.4	71	224.6	2.716	0.012	0.041	0.001	1.000				
1947.6	69	217.2	2.714	0.012	0.032	0.001	1.000				
1947.8	66	167.4	2.726	0.014	0.021	0.001	1.000				
1948.0	63	163.1	2.723	0.018	0.011	0.006	1.000				
1948.2	63	233.5	2.717	0.027	0.010	0.013	1.000				
1948.4	66	239.8	2.673	0.040	0.021	0.028	1.000				
1948.6	71	145.3	2.610	0.051	0.040	0.045	1.000				
1948.8	74	121.1	2.617	0.053	0.053	0.040	1.000				
1949.0	76	101.1	2.646	0.050	0.062	0.030	1.000				
1949.2	77	96.0	2.631	0.044	0.065	0.029	1.000				
1949.4	74	82.7	2.620	0.039	0.053	0.033	1.000				
1949.6	71	72.7	2.635	0.038	0.041	0.031	1.000				
1949.8	69	66.2	2.638	0.044	0.033	0.035	1.000				
1950.0	71	66.1	2.601	0.052	0.042	0.048	1.000				
1950.2	77	65.7	2.570	0.057	0.066	0.054	1.000				
1950.4	83	77.6	2.588	0.061	0.090	0.044	1.000				
1950.6	84	82.9	2.593	0.057	0.096	0.039	1.000				
1950.8	83	62.7	2.612	0.050	0.091	0.031	1.000				
1951.0	79	44.3	2.634	0.048	0.075	0.028	1.000				
1951.2	76	31.9	2.605	0.052	0.060	0.042	1.000				
1951.4	75	30.5	2.540	0.064	0.058	0.069	1.000				
1951.6	79	34.1	2.450	0.093	0.072	0.108	0.990				
1951.8	85	35.6	2.376	0.132	0.102	0.144	0.700 0.611				
1952.0	96	27.2	2.289	0.172	0.156	0.178	0.666				
1952.2	104	18.0	2.234	0.206	0.203	0.201	0.000				
1952.4	103	12.2	2.200	0.226	0.195	0.223 0.243	0.747				
1952.6	98	12.5	2.183	0.245	0.169 0.131	0.243	0.727				
1952.8	91	13.8	2.203	0.250 0.242	0.131	0.238	0.774				
1953.0	90	13.4	2.224	0.242	0.125	0.233	0.755				
1953.2	92	14.1 13.1	2.236 2.257	0.248	0.133	0.233	0.812				
1953.4	93	11.0	2.237	0.233	0.133	0.209	0.963				
1953.6	91	9.1	2.203	0.233	0.121	0.202	1.000				
1953.8 1954.0	89 88	7.9	2.303	0.223	0.116	0.193	1.000				
1954.0	87	7.0	2.321	0.202	0.113	0.189	1.000				
1954.2	89	5.5	2.321	0.199	0.120	0.190	1.000				
1954.4	90	4.3	2.312	0.213	0.128	0.195	1.000				
1954.8	90 90	4.4	2.276	0.219	0.124	0.209	1.000				
1954.8	90 88	4.6	2.278	0.215	0.116	0.228	1.000				
1955.0	85	4.6	2.220	0.213	0.100	0.240	1.000				
1955.4	81	4.8	2.209	0.234	0.084	0.252	1.000				
1955.6	80	5.2	2.191	0.259	0.080	0.268	1.000				
1955.8	80	5.9	2.191	0.279	0.085	0.274	1.000				
1955.0	82	6.8	2.105	0.267		0.269	1.000				
1956.2	81	7.2	2.191	0.248	0.082	0.267	1.000				
4	<u></u>				· · · • • •	-					

Example and the second seco

		PERC			data li	sting)		
DEPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE	
(mRKB)	api	ohmm	g/cc	frac	frac	frac	frac	
1056 (<u> </u>		0					
1956.4	81	7.5	2.185	0.242	0.085	0.263	1.000	
1956.6	87	7.6	2.211	0.238	0.111	0.245	1.000	
1956.8	95	6.7	2.248	0.224	0.149	0.216	1.000	
1957.0	101	5.1	2.294	0.214	0.187	0.186	1.000	
1957.2	106	4.3	2.331	0.212	0.215	0.164	1.000	
1957.4	103	3.3	2.357	0.209	0.199	0.158	1.000	
1957.6	94	2.3	2.324	0.202	0.147	0.180	1.000	
1957.8	85	3.6	2.276	0.208	0.101	0.211	1.000	
1958.0	81	5.0	2.260	0.224	0.081	0.228	1.000	
1958.2	80	4.9	2.268	0.228	0.080	0.227	1.000	
1958.4	82	4.7	2.299	0.205	0.088	0.205	1.000	
1958.6	84	4.8	2.318	0.194	0.096	0.191	1.000	
1958.8	85	5.3	2.320	0.192	0.103	0.188	1.000	
1959.0	85	5.3	2.311	0.186	0.103	0.189	1.000	
1959.2	88	5.0	2.298	0.189	0.114	0.192	1.000	
1959.4	87	5.3	2.289	0.205	0.109	0.203	1.000	
1959.6	84	6.9	2.288	0.212	0.097	0.209	1.000	
1959.8	81	10.9	2.319	0.207	0.084	0.199	1.000	
1960.0	80	14.2	2.378	0.195	0.077	0.175	1.000	
1960.2	82	15.7	2.338	0.180	0.089	0.180	0.946	
1960.4	85	16.2	2.272	0.175	0.099	0.200	0.835	
1960.6	85	15.5	2.264	0.174	0.101	0.202	0.846	
1960.8	82	14.0	2.345	0.174 0.171	0.088	0.174	1.000	
1961.0	79	12.3	2.431	0.168	0.074	0.174 0.148	1.000	
1961.2	81	10.6	2.431	0.155	0.074	0.148	1.000	
1961.4	83	9.5	2.447	0.135	$0.084 \\ 0.094$	$0.134 \\ 0.129$	1.000	
1961.4	82	9.3	2.427	0.138	0.094 0.090	0.129	1.000	
1961.8	80	8.3	2.423	0.132	0.090	0.130	1.000	
1962.0	81	8.6	2.429	0.137	0.078			
1962.0	82	8.8 9.8	2.422 2.434	0.135		0.134	1.000	
1962.2	82 81	9.8 12.1	2.434 2.436		0.087	0.130	1.000	
1962.4	81	12.1		0.140	0.085	0.130	1.000	
1962.8	81		2.449	0.141	0.084	0.127	1.000	
		17.3	2.500	0.139	0.080	0.112	1.000	
1963.0	78	17.7	2.526	0.125	0.068	0.101	1.000	
1963.2	78	21.1	2.439	0.113	0.070	0.122	1.000	
1963.4	80 76	24.8	2.196	0.113	0.077		0.000	
1963.6	76	28.1	1.908	0.128		bal		
1963.8	69 61	34.3	1.658	0.170		bal		
1964.0	61 54	40.0	1.469	0.244		bal		
1964.2	54	48.5	1.369	0.362		bal		
1964.4	49	43.6	1.340	0.473		bal		
1964.6	47	38.6	1.324	0.548		bal		
1964.8	45	55.7	1.313	0.630		bal		
1965.0	43	53.3	1.308	0.724		bal		
1965.2	43	44.3	1.309	0.720		bal		
1965.4	43	48.0	1.311	0.653		oal		
1965.6	42	48.2	1.312	0.615		bal		
1965.8	42	55.4	1.318	0.628		bal		
1966.0	44	75.3	1.321	0.679		bal		
1966.2	45	94.3	1.321	0.756		bal		
1966.4	49	36.9	1.322	0.775		bal		
1966.6	56	15.6	1.321	0.769		bal		
1966.8	62	30.4	1.330	0.810	Co	bal		
1967.0	65	309.1	1.346	0.758	Co	bal		
1967.2	68	673.0	1.361	0.665		bal		
1967.4	76	28.0	1.362	0.728	Co	bal		

		PERCH	_4 (pag	re 16 of	data	listing)		
DEPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE	
(mRKB)	api	ohmm	g/cc	frac	frac	frac	frac	
1967.6	84	13.2	1.368	0.818		Coal		
1967.8	87	15.4	1.386	0.828		Coal		
1968.0	82	9.2	1.405	0.777		Coal		
1968.2	76	161.5	1.413	0.779		Coal		
1968.4	71	676.4	1.410	0.677		Coal		
1968.6	68	14.8	1.401	0.664		Coal		
1968.8	65	30.0	1.389	0.680		Coal		
1969.0	62	26.2	1.381	0.626		Coal		
1969.2	63	7.8	1.375	0.581		Coal		
1969.4	65	8.4	1.366	0.638		Coal		
1969.6	67	7.8	1.371	0.786		Coal		
1969.8	66	5.9	1.383	0.967				
1970.0	70	38.0	1.389	0.961		Coal Coal		
1970.2	81	851.1						
1970.4	85	946.2	1.399 1.411	0.714		Coal		
1970.6	85			0.642		Coal		
1970.8		294.6	1.417	0.671		Coal		
	86	147.7	1.403	0.691		Coal		
1971.0	88	965.2	1.416	0.710		Coal		
1971.2	86	1000.0	1.429	0.739		Coal		
1971.4	78	886.3	1.426	0.760		Coal		
1971.6	73	90.1	1.414	0.773		Coal		
1971.8	75	28.0	1.397	0.761		Coal		
1972.0	74	16.4	1.373	0.757		Coal		
1972.2	71	8.2	1.371	0.700		Coal		
1972.4	70	5.6	1.382	0.654		Coal		
1972.6	70	5.6	1.383	0.660		Coal		
1972.8	73	13.1	1.380	0.718		Coal		
1973.0	76	17.0	1.384	0.735		Coal		
1973.2	77	675.0	1.391	0.746		Coal		
1973.4	75	213.6	1.392	0.812		Coal		
1973.6	74	19.2	1.387	0.715		Coal		
1973.8	72	16.5	1.381	0.633		Coal		
1974.0	71	16.7	1.379	0.682		Coal		
1974.2	70	19.9	1.373	0.787		Coal		
1974.4	69	20.1	1.360	0.838		Coal		
1974.6	68	37.8	1.356	0.784		Coal		
1974.8	66	22.0	1.357	0.788		Coal		
1975.0	64	18.9	1.353	0.803		Coal		
1975.2	63	19.1	1.341	0.740		Coal		
1975.4	62	23.6	1.334	0.716		Coal		
1975.6	60	20.0	1.330	0.741		Coal		
1975.8	57	46.2	1.325	0.788		Coal		
1976.0	59	137.8	1.327	0.825		Coal		
1976.2	66	16.6	1.353	0.725		Coal		
1976.4	70	13.5	1.373	0.657		Coal		
1976.6	69	20.7	1.369	0.667		Coal		
1976.8	67	19.3	1.358	0.704		Coal		
1977.0	67	12.2	1.359	0.725		Coal		
1977.2	69	6.9	1.371	0.764		Coal		
1977.4	70	6.3	1.375	0.786		Coal		
1977.6	71	33.1	1.370	0.733		Coal		
1977.8	74	50.9	1.369	0.738		Coal		
1978.0	76	23.9	1.377	0.825		Coal		
1978.2	75	26.8	1.388	0.836		Coal		
1978.4	73	120.5	1.395	0.818		Coal		
1978.6	71	690.3	1.408	0.941		Coal		

			PERCH	_4 (pag	e 17 of	data lis	sting)	
	DEPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE
	(mRKB)	api	ohmm	g/cc	frac	frac	frac	frac
	1978.8	72	52.8	1.406	1.048	C	bal	
	1979.0	73	21.0	1.386	0.948		bal	
	1979.2	74						
			229.6	1.369	0.726		bal	
	1979.4	73	725.4	1.359	0.685		bal	
	1979.6	72	97.8	1.349	0.874		bal	
	1979.8	69 66	22.2	1.347	1.211		bal	
	1980.0	66	30.5	1.347	0.948		bal	
	1980.2	64	20.4	1.333	0.932		bal	
	1980.4	62	60.7	1.325	1.065		al	
	1980.6	58	98.7	1.345	1.188		bal	
	1980.8	55	20.3	1.374	0.887		al	
	1981.0	59	47.1	1.388	0.682		bal	
	1981.2	66	36.9	1.394	0.624		bal	
	1981.4	69	48.2	1.388	0.611		bal	
	1981.6	69	18.3	1.381	0.611		bal	
	1981.8	70	244.8	1.402	0.597		bal	
	1982.0	71	395.0	1.401	0.574		bal	
	1982.2	73	35.6	1.394	0.555	Co	bal	
	1982.4	77	19.0	1.384	0.550		al	
	1982.6	83	14.6	1.374	0.552	Co	al	
	1982.8	86	161.3	1.377	0.565	Co	bal	
	1983.0	81	62.6	1.392	0.595	Co	al	
	1983.2	76	11.7	1.401	0.652	Co	bal	
	1983.4	75	55.5	1.397	0.727	Co	bal	
	1983.6	77	38.1	1.387	0.779	Co	al	
	1983.8	82	25.0	1.384	0.766	Cc	al	
	1984.0	105	27.4	1.388	0.722	Co	al	
	1984.2	151	24.8	1.392	0.674	Co	al	
	1984.4	190	27.2	1.393	0.653	Co	al	
	1984.6	209	21.4	1.394	0.604	Co	al	
	1984.8	216	15.6	1.394	0.535	Co	al	
	1985.0	219	14.8	1.393	0.493	Co	al	
	1985.2	215	16.3	1.508	0.453	Co	al	
	1985.4	202	15.4	2.005	0.389	Co	al	
	1985.6	189	13.4	2.434	0.361	1.000	0.000	0.000
	1985.8	181	12.6	2.511	0.348	1.000	0.000	1.000
	1986.0	171	12.2	2.509	0.325	0.844	0.000	1.000
	1986.2	161	11.1	2.472	0.293	0.695	0.000	1.000
	1986.4	157	8.1	2.431	0.268	0.651	0.000	1.000
	1986.6	154	7.8	2.413	0.264	0.615	0.000	1.000
	1986.8	145	9.7	2.367	0.269	0.518	0.017	1.000
	1987.0	138	9.2	2.325	0.270	0.454	0.064	1.000
	1987.2	136	8.3	2.315	0.270	0.431	0.084	1.000
	1987.4	134	8.7	2.304	0.261	0.414	0.099	1.000
	1987.6	132	9.5	2.297	0.245	0.398	0.110	1.000
	1987.8	130	10.2	2.303	0.229	0.385	0.114	1.000
	1988.0	128	9.8	2.291	0.238	0.370	0.135	1.000
	1988.2	127	8.6	2.264	0.248	0.356	0.162	1.000
	1988.4	123	8.0	2.261	0.249	0.332	0.175	1.000
	1988.6	119	6.6	2.274	0.253	0.301	0.179	1.000
	1988.8	115	5.0	2.289	0.261	0.272	0.185	1.000
	1989.0	111	3.8	2.290	0.257	0.245	0.190	1.000
•	1989.2	107	1.8	2.307	0.263	0.222	0.193	1.000
	1989.4	105	1.4	2.280	0.300	0.207	0.222	1.000
	1989.6	103	1.4	2.229	0.344	0.198	0.260	1.000
	1989.8	102	1.5	2.139	0.345	0.190	0.291	1.000

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		PERCH	4 (pad	ge 18 of	data li	sting)	
DEPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE
(mRKB)	api	ohmm	g/cc	frac	frac	frac	frac
1990.0	101	1.7	2.127	0.358	0.184	0.302	1.000
1990.2	98	1.7	2.234	0.335	0.167	0.262	1.000
1990.4	86	1.7	2.260	0.295	0.107	0.251	1.000
1990.6	74	1.9	2.259	0.275	0.052	0.256	1.000
1990.8	68	2.3	2.248	0.270	0.030	0.263	1.000
1991.0	67	2.4	2.267	0.269	0.025	0.203	1.000
1991.2	67	2.4	2.276	0.262	0.025	0.251	1.000
1991.4	68	2.5	2.283	0.250	0.020	0.242	1.000
1991.6	69	2.5	2.323	0.243	0.035	0.226	1.000
1991.8	70	2.6	2.339	0.255	0.038	0.226	1.000
1992.0	72	2.6	2.330	0.270	0.045	0.234	1.000
1992.2	74	2.6	2.335	0.261	0.052	0.227	1.000
1992.4	77	2.6	2.355	0.233	0.065	0.204	1.000
1992.6	80	2.6	2.383	0.227	0.081	0.189	1.000
1992.8	83	2.6	2.388	0.239	0.094	0.190	1.000
1993.0	87	2.6	2.381	0.257	0.110	0.197	1.000
1993.2	88	2.6	2.349	0.266	0.117	0.209	1.000
1993.4	87	3.0	2.327	0.263	0.112	0.215	1.000
1993.6	87	5.9	2.334	0.256	0.109	0.210	1.000
1993.8	85	8.5	2.393	0.251	0.101	0.193	1.000
1994.0	82	8.7	2.457	0.222	0.087	0.165	1.000
1994.2	81	8.1	2.452	0.186	0.081	0.149	1.000
1994.4	80	6.6	2.418	0.172	0.081	0.152	1.000
1994.6	83	6.1	2.392	0.180	0.092	0.160	1.000
1994.8	91	6.6	2.349	0.194	0.132	0.171	1.000
1995.0	96	6.4	2.327	0.201	0.157	0.176	1.000
1995.2	95	6.5	2.315	0.195	0.153	0.179	1.000
1995.4	96	7.5	2.342	0.188	0.157	0.165	1.000
1995.6	99	7.6	2.406	0.190	0.171	0.141	1.000
1995.8	98	7.2	2.429	0.191	0.169	0.136	1.000
1996.0	97	6.2	2.371	0.182	0.162	0.151	1.000
1996.2	102	5.3	2.387	0.175	0.188	0.136	1.000
1996.4	111	4.4	2.467	0.177	0.249	0.098	1.000
1996.6	122	3.9	2.423	0.185	0.323	0.096	1.000
1996.8	127	4.6	2.232	0.242	0.361	0.165	1.000
1997.0	129	6.3	1.954	0.338		bal	
1997.2	135	9.4	1.660	0.377		bal	
1997.4	148	10.4	1.563	0.354		bal	
1997.6	163	10.8	1.667	0.458		oal	
1997.8	177	14.0	1.983	0.569		bal	
1998.0	186	17.0	2.292	0.488		bal	
1998.2	188	11.4	2.383	0.425	1.000	0.000	1.000
1998.4	191	10.9	2.416	0.383	1.000	0.000	1.000
1998.6	195	9.9	2.456	0.370	1.000	0.000	1.000
1998.8	198	8.8	2.479	0.415	1.000	0.000	1.000
1999.0 1999.2	193	10.8	2.443	0.470	1.000	0.000	1.000
1999.4	190	11.7 7.7	2.347	0.560	1.000	0.000	1.000
1999.4 1999.6	191 188	6.1	2.268 2.142	0.696 0.661	1.000	0.000 Dal	1.000
1999.8	177	5.2	2.012	0.649		bal	
2000.0	169	4.9	1.849	0.641		bal	
2000.2	166	4.9	1.767	0.639		bal	
2000.2	171	4.6	1.825	0.619		bal	
2000.6	181	4.5	1.926	0.531		bal	
2000.8	191	4.5	1.972	0.466		bal	
2001.0	196	5.5	2.087	0.507		bal	
		- / -				-	

		PERCH	_4 (pag	e 19 of	data lis	ting)	
DEPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE
(mRKB)	api	ohmm	g/cc	frac	frac	frac	frac
2001.2	194	6.5	2.278	0.548	1.000	0.000	1.000
2001.4	189	7.1	2.382	0.506	1.000	0.000	1.000
2001.6	189	9.0	2.448	0.426	1.000	0.000	1.000
2001.8	195	9.1	2.487	0.378	1.000	0.000	1.000
2002.0	201	8.5	2.509	0.354	1.000	0.000	1.000
2002.2	200	8.7	2.500	0.332	1.000	0.000	1.000
2002.2	202	9.6	2.447	0.311	1.000	0.000	1.000
2002.4	202	9.0 9.2	2.447	0.290	1.000	0.000	1.000
2002.8	200	9.3					
2002.8	206		2.376	0.281	1.000	0.000	1.000
		8.9	2.336	0.284	1.000	0.000	1.000
2003.2	196	8.2	2.271	0.294	1.000	0.000	1.000
2003.4	186	6.1	2.213	0.320	1.000	0.000	1.000
2003.6	173	5.8	2.177	0.337	0.871	0.000	1.000
2003.8	155	7.4	2.168	0.307	0.624	0.000	1.000
2004.0	130	8.4	2.194	0.275	0.381	0.166	0.925
2004.2	108	8.9	2.226	0.267	0.224	0.221	0.943
2004.4	110	8.5	2.253	0.254	0.242	0.202	1.000
2004.6	126	7.7	2.297	0.233	0.348	0.151	1.000
2004.8	114	7.5	2.313	0.223	0.267	0.162	1.000
2005.0	87	6.5	2.281	0.234	0.114	0.216	1.000
2005.2	86	4.6	2.255	0.259	0.108	0.236	1.000
2005.4	84	3.2	2.307	0.275	0.098	0.230	1.000
2005.6	82	2.6	2.350	0.283	0.086	0.224	1.000
2005.8	81	2.2	2.334	0.275	0.085	0.225	1.000
2006.0	82	1.8	2.303	0.261	0.087	0.227	1.000
2006.2	82	1.5	2.299	0.253	0.087	0.225	1.000
2006.4	81	1.5	2.310	0.249	0.083	0.220	1.000
2006.6	82	1.5	2.283	0.246	0.087	0.227	1.000
2006.8	85	1.3	2.260	0.253	0.104	0.233	1.000
2007.0	88	1.1	2.282	0.263	0.116	0.227	1.000
2007.2	86	0.9	2.269	0.265	0.106	0.235	1.000
2007.4	82	1.1	2.260	0.250	0.090	0.236	1.000
2007.6	85	1.6	2.280	0.244	0.101	0.223	1.000
2007.8	89	4.4	2.326	0.239	0.119	0.202	1.000
2008.0	89	2.2	2.334	0.244	0.121	0.202	1.000
2008.2	86	2.2	2.304	0.252	0.106	0.218	1.000
2008.4	80	2.9	2.255	0.251	0.080	0.241	1.000
2008.6	79	4.0	2.226	0.255	0.075	0.254	1.000
2008.8	83	5.0	2.216	0.262	0.094	0.256	1.000
2009.0	82	5.1	2.231	0.266	0.090	0.253	1.000
2009.2	77	5.2	2.255	0.264	0.066	0.249	1.000
2009.4	77	5.1	2.268	0.255	0.065	0.241	1.000
2009.6	76	4.7	2.278	0.255	0.062	0.239	1.000
2009.8	75	4.5	2.274	0.254	0.058	0.240	1.000
2010.0	76	3.5	2.307	0.241	0.060	0.223	1.000
2010.2	77	3.0	2.296	0.232	0.066	0.222	1.000
2010.4	78	2.7	2.241	0.229	0.070	0.240	1.000
2010.6	82	2.5	2.219	0.244	0.088	0.250	1.000
2010.8	83	2.3	2.227	0.266	0.094	0.253	1.000
2011.0	80	2.2	2.243	0.264	0.081	0.249	1.000
2011.2	81	2.3	2.228	0.249	0.084	0.249	1.000
2011.4	85	2.4	2.253	0.241	0.102	0.232	1.000
2011.6	84	2.3	2.275	0.244	0.095	0.227	1.000
2011.8	78	2.2	2.249	0.244	0.069	0.243	1.000
2012.0	77	2.1	2.283	0.238	0.066	0.229	1.000
2012.2	81	1.8	2.295	0.233	0.082	0.219	1.000

			PERCH	[_4 (pag	re 20 of	data lis	sting)	
	DEPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE
	(mRKB)	api	ohmm	g/cc	frac	frac	frac	frac
	2012.4	85	1.2	2.284	0.240	0.100	0.221	1.000
	2012.6	85	0.9	2.308	0.246	0.103	0.215	1.000
	2012.8	85	0.7	2.301	0.239	0.100	0.214	1.000
	2013.0	83	0.6	2.223	0.247	0.091	0.248	1.000
	2013.2	80	0.7	2.145	0.269	0.077	0.290	1.000
	2013.4	77	0.9	2.147	0.298	0.064	0.303	1.000
	2013.6	75	1.7	2.221	0.341	0.057	0.296	1.000
	2013.8	77	2.6	2.246	0.356	0.066	0.292	1.000
	2014.0	83	3.2	2.268	0.316	0.093	0.262	1.000
ň	2014.2	89	3.7	2.265	0.268	0.120	0.234	1.000
	2014.4	92	4.0	2.240	0.243	0.138	0.229	1.000
	2014.6	96	4.5	2.250	0.233	0.157	0.216	1.000
	2014.8	99	5.3	2.242	0.234	0.174	0.215	1.000
	2015.0	101	5.5	2.228	0.239	0.182	0.221	1.000
	2015.2	96	4.2	2.230	0.237	0.156	0.226	1.000
	2015.4	88	3.7	2.252	0.243	0.117	0.230	1.000
	2015.6	84	3.0	2.284	0.255	0.099	0.228	1.000
	2015.8	85	2.4	2.298	0.256	0.101	0.223	1.000
	2016.0	87	1.9	2.317	0.234	0.110	0.204	1.000
	2016.2	88	1.4	2.329	0.222	0.114	0.194	1.000
	2016.4	85	1.5	2.352	0.228	0.101	0.193	1.000
	2016.6	83	1.9	2.345	0.228	0.091	0.198	1.000
	2016.8	87	3.7	2.299	0.212	0.112	0.201	1.000
	2017.0	92	7.0	2.272	0.200	0.138	0.201	1.000
	2017.2	90	10.3	2.072	0.237		0.200	1.000
	2017.4	86	12.1	1.906	0.301		al	
	2017.6	80	12.4	1.969	0.333		al	
	2017.8	73	15.4	2.050	0.390		al	
	2018.0	66	21.9	1.692	0.440		al	
	2018.2	59	19.0	1.349	0.440		al	
	2018.4	55	21.6	1.303	0.401		al	
	2018.6	57	29.9	1.322	0.563		al	
	2018.8	66	33.6	1.339	0.572		al	
	2019.0	77	20.8	1.348	0.630		al	
	2019.2	88	15.5	1.340	0.685		al	
	2019.4	103	15.1	1.397	0.677		al	
	2019.6	120	12.9	1.450	0.769		al	
	2019.8	139	11.5	1.528	0.888		al	
	2020.0	152	8.3	1.640	0.791		al	
	2020.2	160	7.2	1.719	0.654		al	
	2020.4	166	8.2	1.809	0.596		al	
	2020.6	177	9.1	1.932	0.544		al	
	2020.8	185	9.8	2.051	0.524		al	
	2021.0	185	10.7	2.183	0.525		al	
	2021.2	186	11.2	2.319	0.498	1.000	0.000	1.000
	2021.4	191	10.1	2.410	0.490	1.000	0.000	1.000
	2021.6	195	9.9	2,498	0.440	1.000	0.000	1.000
	2021.8	200	10.9	2.544	0.4407	1.000	0.000	1.000
	2022.0	205	10.9	2.544	0.376	1.000	0.000	1.000
	2022.2	206	10.4	2.525	0.353		0.000	
	2022.2	208	10.4	2.528	0.335	1.000 1.000	0.000	1.000 1.000
:	2022.4	205	10.8	2.577	0.335	1.000	0.000	1.000
	2022.8	205	10.1	2.527	0.320	1.000	0.000	1.000
	2023.0	198	9.1	2.527	0.333	1.000	0.000	1.000
	2023.2	174	7.8	2.525	0.336	0.896	0.000	1.000
	2023.4	141	6.8	2.303	0.332	0.479	0.042	1.000
		~ * *	0.0	~. - UJ	0.002	0.7/2	0.042	T.000

			PERCH	4_4 (pa	.ge 21 of	data li	sting)	
	DEPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE
	(mRKB)	api	ohmm	g/cc	frac	frac	frac	frac
	2023.6	112	6.1	2.415	0.318	0.251	0.180	1.000
	2023.8	96	5.7	2.363	0.278	0.160	0.200	1.000
	2024.0	90	5.6	2.325	0.249	0.128	0.205	1.000
	2024.2	85	6.4	2.280	0.241	0.103	0.222	1.000
	2024.4	84	7.1	2.263	0.242	0.099	0.229	1.000
	2024.6	89	7.6	2.270	0.253	0.122	0.225	1.000
	2024.8	96	8.0	2.266	0.267	0.155	0.225	1.000
	2025.0	98	8.1	2.259	0.263	0.169	0.223	1.000
	2025.2	94	7.5	2.223	0.278	0.146	0.221	1.000
	2025.2	88	7.3	2.222	0.278	0.140 0.114		
							0.277	0.962
	2025.6	86	7.7	2.168	0.291	0.104	0.282	0.927
	2025.8	88	7.7	2.177	0.296	0.114	0.278	0.930
	2026.0	90	8.4	2.211	0.311	0.126	0.269	0.905
	2026.2	88	10.4	2.228	0.314	0.118	0.267	0.810
	2026.4	84	9.4	2.192	0.289	0.099	0.273	0.855
	2026.6	83	9.7	2.161	0.254	0.091	0.275	0.847
	2026.8	84	10.2	2.151	0.247	0.099	0.274	0.817
	2027.0	83	10.0	2.162	0.257	0.094	0.275	0.828
	2027.2	81	9.7	2.171	0.264	0.084	0.276	0.845
	2027.4	83	8.6	2.145	0.276	0.093	0.289	0.861
	2027.6	85	8.5	2.167	0.273	0.102	0.277	0.893
	2027.8	85	8.0	2.232	0.254	0.101	0.245	1.000
	2028.0	86	4.6	2.247	0.258	0.104	0.240	1.000
	2028.2	86	2.4	2.262	0.294	0.108	0.250	1.000
	2028.4	87	1.3	2.184	0.327	0.109	0.289	1.000
	2028.6	83	0.9	2.107	0.337	0.092	0.324	1.000
	2028.8	79	0.8	2.094	0.310	0.075	0.325	1.000
	2029.0	80	0.9	2.174	0.291	0.077	0.286	1.000
	2029.2	83	1.6	2.247	0.250	0.093	0.240	1.000
	2029.4	85	3.5	2.254	0.234	0.100	0.229	1.000
	2029.6	86	4.5	2.237	0.235	0.109	0.234	1.000
	2029.8	88	4.7	2.232	0.235	0.118	0.234	1.000
	2030.0	86	5.0	2.232	0.209	0.107	0.234	1.000
	2030.2	81	4.7					
	2030.2			2.252	0.188	0.084	0.216	1.000
		79	4.3	2.299	0.195	0.073	0.204	1.000
	2030.6	77	4.4	2.325	0.203	0.068	0.200	1.000
	2030.8	77	4.7	2.312	0.198	0.064	0.203	1.000
	2031.0	77	5.2	2.281	0.197	0.064	0.214	1.000
	2031.2	79	5.9	2.250	0.202	0.076	0.225	1.000
	2031.4	83	6.4	2.221	0.208	0.092	0.234	1.000
	2031.6	82	6.9	2.213	0.211	0.088	0.239	1.000
	2031.8	80	7.6	2.197	0.208	0.078	0.247	1.000
	2032.0	79	8.8	2.216	0.201	0.075	0.238	1.000
	2032.2	77	9.3	2.279	0.196	0.066	0.214	1.000
	2032.4	75	9.5	2.282	0.198	0.056	0.216	1.000
	2032.6	78	9.5	2.243	0.211	0.068	0.233	1.000
	2032.8	82	9.6	2.217	0.228	0.086	0.245	0.946
	2033.0	81	9.8	2.210	0.237	0.084	0.251	0.917
	2033.2	79	10.0	2.206	0.254	0.072	0.262	0.884
	2033.4	78	10.2	2.223	0.267	0.070	0.261	0.880
	2033.6	79	10.1	2.248	0.258	0.075	0.247	0.926
į	2033.8	81	10.0	2.241	0.247	0.081	0.244	0.936
•	2034.0	80	9.9	2.247	0.239	0.078	0.240	0.955
	2034.2	80	10.0	2.266	0.218	0.077	0.225	1.000
	2034.4	81	9.5	2.270	0.205	0.082	0.217	1.000
	2034.6	84	9.5	2.222	0.213	0.096	0.234	0.981
			-					

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			PERCH	4 (page	e 22 of	data lis	ting)	
DI	EPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE
(1	mRKB)	api	ohmm	g/cc	frac	frac	frac	frac
	034.8	89	9.1	2.185	0.226	0.121	0.247	0.935
	035.0	94	8.4	2.156	0.239	0.148	0.257	0.918
	035.2	94	8.4	2.173	0.246	0.148	0.253	0.932
	035.4	88	8.3	2.169	0.270	0.118	0.270	0.913
	035.6	83	8.2	2.134	0.295	0.090	0.300	0.855
	035.8	83	8.6	2.180	0.278	0.094	0.275	0.898
	036.0 036.2	88 90	5.8	2.240	0.255	0.114	0.239	1.000
	036.4	90 93	4.7 5.1	2.255 2.241	0.239 0.235	0.124	0.225	1.000
	036.6	96	4.8	2.221	0.235	0.140 0.159	0.225 0.228	1.000
	036.8	99	4.6	2.224	0.237	0.139	0.223	1.000 1.000
	037.0	101	4.6	2.263	0.238	0.183	0.207	1.000
	037.2	99	5.0	2.216	0.235	0.175	0.226	1.000
	037.4	95	5.2	2.215	0.227	0.154	0.228	1.000
20	037.6	92	4.9	2.230	0.219	0.135	0.224	1.000
20	037.8	92	4.7	2.203	0.216	0.136	0.233	1.000
20	038.0	97	3.9	2.192	0.221	0.162	0.233	1.000
	038.2	105	3.4	2.242	0.237	0.208	0.208	1,000
	038.4	112	3.6	2.274	0.252	0.249	0.192	1.000
	038.6	115	4.3	2.282	0.251	0.271	0.183	1.000
	038.8	111	5.7	2.294	0.258	0.244	0.190	1.000
	039.0	102	8.0	2.291	0.269	0.191	0.209	1.000
	039.2 039.4	90 78	9.6	2.272	Nul	0.127	0.968	0.266
	039.4	70	10.1 9.4	2.269 2.285	Nul Nul	0.070	0.982	0.268
	039.8	70	9.0	2.295	Nul	0.038 0.038	0.990 0.991	0.285 0.292
	040.0	73	7.8	2.290	Nul	0.050	0.991	0.312
	040.2	76	6.8	2.269	Nul	0.063	0.984	0.333
	040.4	79	5.8	2.248	Nul	0.074	0.982	0.361
20	040.6	86	5.2	2.227	Nul	0.104	0.974	0.376
	040.8	101	4.9	2.213	Nul	0.185	0.954	0.378
	041.0	129	6.7	Nul	Nul	0.375	0.793	0.370
	041.2	160	9.7	Nul	Nul	0.690	0.000	1.000
	041.4 041.6	181	11.4	Nul	Nul	1.000	0.000	1.000
	041.8 041.8	195 201	12.3 11.9	Nul	Nul	1.000	0.000	1.000
	042.0	201	11.9	Nul Nul	Nul Nul	1.000 1.000	0.000 0.000	1.000
	042.2	201	12.6	Nul	Nul	1.000	0.000	1.000 1.000
	042.4	195	11.8	Nul	Nul	1.000	0.000	1.000
20	042.6	187	10.5	Nul	Nul	1.000	0.000	1.000
20	042.8	182	9.8	Nul	Nul	1.000	0.000	1.000
20	043.0	179	9.0	Nul	Nul	0.987	0.000	1.000
	043.2	175	9.6	Nul	Nul	0.914	0.000	1.000
	043.4	172	10.0	Nul	Nul	0.860	0.000	1.000
	043.6	171	9.5	Nul	Nul	0.843	0.000	1.000
	043.8	172	9.3	Nul	Nul	0.849	0.000	1.000
)44.0)44.2	171 168	8.8	Nul	Nul	0.844	0.000	1.000
)44.4	163	9.3 9.7	Nul	Nul	0.793	0.000	1.000
)44.6	159	9.7 9.2	Nul Nul	Nul Nul	0.724 0.669	0.000 0.000	1.000
)44.8	153	8.9	Nul	Nul	0.600	0.000	1.000 1.000
	045.0	141	8.8	Nul	Nul	0.478	0.000	0.714
	045.2	125	8.8	Nul	Nul	0.345	0.000	0.236
)45.4	113	9.0	Nul	Nul	0.260	0.000	0.251
	045.6	102	9.2	Nul	Nul	0.193	0.000	0.260
20	045.8	92	9.4	Nul	Nul	0.134	0.000	0.268

			PERCH	4 (pa	ne 23 of	data lis	sting)	
	DEPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE
	(mRKB)	api	ohmm	g/cc	frac	frac	frac	frac
		-		2				
	2046.0	83	9.4	Nul	Nul	0.091	0.000	0.276
	2046.2	80	9.4	Nul	Nul	0.079	0.000	0.277
	2046.4		9.6	Nul	Nul	1.000	0.000	1.000
	2046.6		9.7	Nul	Nul	1.000	0.000	1.000
	2046.8		8.9	Nul	Nul	1.000	0.000	1.000
	2047.0		8.3	Nul	Nul	1.000	0.000	1.000
	2047.2		7.8	Nul	Nul	1.000	0.000	1.000
	2047.4		7.4	Nul	Nul	1.000	0.000	1.000
	2047.6		7.1	Nul	Nul	1.000	0.000	1.000
	2047.8		6.8	Nul	Nul	1.000	0.000	1.000
	2048.0		6.8	Nul	Nul	1.000	0.000	1.000
	2048.2		7.2	Nul	Nul	1.000	0.000	1.000
	2048.4		7.6	Nul	Nul	1.000	0.000	1.000
	2048.6		8.0	Nul	Nul	1.000	0.000	1.000
	2048.8		8.7	Nul	Nul	1.000	0.000	1.000
	2049.0		9.6	Nul	Nul	1.000	0.000	1.000
	2049.2		13.9	Nul	Nul	1.000	0.000	1.000
	2049.4		18.1	Nul	Nul	1.000	0.000	1.000
	2049.6		N	Nul	Nul	1.000	0.000	0.000
	2049.8		N	Nul	. Nul	1.000	0.000	0.000
	2050.0		N	Nul	Nul	1.000	0.000	0.000
	2050.2		N	Nul	Nul	1.000	0.000	0.000
	2050.4		N	Nul	Nul	1.000	0.000	0.000
	2050.6		N	Nul	Nul	1.000	0.000	0.000
	2050.8		N	Nul	Nul	1.000	0.000	0.000
	2051.0		N	Nul	Nul	1.000	0.000	0.000
	2051.2		N	Nul	Nul	1.000	0.000	0.000
	2051.4		N	Nul	Nul	1.000	0.000	0.000
	2051.4		N	Nul	Nul	1.000	0.000	0.000
	2051.0		N	Nul	Nul	1.000	0.000	0.000
	2052.0		N	Nul	Nul	1.000	0.000	0.000
	2052.0		N	Nul	Nul	1.000	0.000	0.000
	2052.2		N	Nul	Nul	1.000	0.000	0.000
	2052.4		N	Nul	Nul	1.000	0.000	0.000
	2052.8		N	Nul	Nul	1.000	0.000	0.000
	2052.0		N	Nul	Nul	1.000	0.000	0.000
	2053.2		N	Nul	Nul	1.000	0.000	0.000
	2053.4		N	Nul	Nul	1.000	0.000	0.000
	2053.6		N	Nul	Nul	1.000	0.000	0.000
	2053.8		N	Nul	Nul	1.000	0.000	0.000
	2054.0		N	Nul	Nul	1.000	0.000	0.000
	2054.2		N	Nul	Nul	1.000	0.000	0.000
	2054.4		N	Nul	Nul	1.000	0.000	0.000
	2054.6		N	Nul	Nul	1.000	0.000	0.000
	2054.8		N	Nul	Nul	1.000	0.000	0.000
	2055.0		N	Nul	Nul	Nul	0.000	0.000
	2055.2		N	Nul	Nul	Nul	0.000	0.000
	2055.4		N	Nul	Nul	Nul	0.000	0.000
	2055.6		N	Nul	Nul	Nul	0.000	0.000
	2055.8		N	Nul	Nul	Nul	0.000	0.000
	2055.0		N	Nul	Nul	Nul	0.000	0.000
3	2056.2		N	Nul	Nul	Nul	0.000	0.000
•	2056.4		N N	Nul	Nul	Nul	0.000	0.000
	2056.6		N	Nul	Nul	Nul	0.000	0.000
	2056.8		N N	Nul	Nul	Nul	0.000	0.000
	2050.0		N	Nul	Nul	Nul	0.000	0.000
	2007.0		TA	NUL	ицт	11 (4.1	0.000	0.000

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	data listing)						
DEPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE
(mRKB)	api	ohmm	g/cc	frac	frac	frac	frac
2057 2			NT - 1	N. 1		0 000	0 000
2057.2 2057.4	•	N	Nul	Nul	Nul	0.000	0.000
2057.4		N	Nul	Nul	Nul	0.000	0.000
2057.8		N	Nul	Nul Nul	Nul	0.000	0.000
2058.0		N	Nul		Nul	0.000	0.000
2058.2		N N	Nul Nul	Nul	Nul Nul	0.000	0.000
2058.4		N	Nul	Nul Nul	Nul	0.000 0.000	0.000 0.000
2058.6		N	Nul	Nul	Nul	0.000	0.000
2058.8		N	Nul	Nul	Nul	0.000	0.000
2059.0		N	Nul	Nul	Nul	0.000	0.000
2059.2		N	Nul	Nul	Nul	0.000	0.000
2059.4		N	Nul	Nul	Nul	0.000	0.000
2059.6		N	Nul	Nul	Nul	0.000	0.000
2059.8		N	Nul	Nul	Nul	0.000	0.000
2060.0		N	Nul	Nul	Nul	0.000	0.000
2060.2		N	Nul	Nul	Nul	0.000	0.000
2060.4		N	Nul	Nul	Nul	0.000	0.000
2060.6		N	Nul	Nul	Nul	0.000	0.000
2060.8		N	Nul	Nul	Nul	0.000	0.000
2061.0		N	Nul	Nul	Nul	0.000	0.000
2061.2		N	Nul	Nul	Nul	0.000	0.000
2061.4		N	Nul	Nul	Nul	0.000	0.000
2061.6		N	Nul	Nul	Nul	0.000	0.000
2061.8		N	Nul	Nul	Nul	0.000	0.000
2062.0		N	Nul	Nul	Nul	0.000	0.000
2062.2		N	Nul	Nul	Nul	0.000	0.000
2062.4		N	Nul	Nul	Nul	0.000	0.000
2062.6		N	Nul	Nul	Nul	0.000	0.000
2062.8		N	Nul	Nul	Nul	0.000	0.000
2063.0		N	Nul	Nul	Nul	0.000	0.000
2063.2		N	Nul	Nul	Nul	0.000	0.000
2063.4		N	Nul	Nul	Nul	0.000	0.000
2063.6		N	Nul	Nul	Nul	0.000	0.000
2063.8		N	Nul	Nul	Nul	0.000	0.000
2064.0		N	Nul	Nul	Nul	0.000	0.000
2064.2		N	Nul	Nul	Nul	0.000	0.000
2064.4		N	Nul	Nul	Nul	0.000	0.000
2064.6		N	Nul	Nul	Nul	0.000	0.000
2064.8		N	Nul	Nul	Nul	0.000	0.000
2065.0		N	Nul	Nul	Nul	0.000	0.000
2065.2		N	Nul	Nul	Nul	0.000	0.000
2065.4		N	Nul	Nul	Nul	0.000	0.000
2065.6		N	Nul	Nul	Nul	0.000	0.000
2065.8		N	Nul	Nul	Nul	0.000	0.000
2066.0 2066.2		N	Nul	Nul	Nul	0.000	0.000
2066.4		N	Nul	Nul	Nul	0.000	0.000
		N	Nul	Nul	Nul	0.000	0.000
2066.6 2066.8		N	Nul	Nul	Nul	0.000	0.000
2068.8		N	Nul	Nul	Nul	0.000	0.000
2067.0		N	Nul	Nul	Nul	0.000	0.000
2067.2		N	Nul	Nul	Nul	0.000	0.000
2067.4		N N	Nul	Nul	Nul	0.000	0.000
2067.8		N N	Nul Nul	Nul Nul	Nul Nul	0.000	0.000
2068.0		N	Nul	Nul	Nul	0.000 0.000	0.000 0.000
2068.2		N	Nul	Nul	Nul	0.000	0.000
		11	14 12	I UL	1941	0.000	0.000

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		PERCH	14 (pad	re 25 of	data li:	sting)	
DEPTH	GR	RT	RHOB	NPHI	VSH	PHIE	SWE
(mRKB)	api	ohmm	g/cc	frac	frac	frac	frac
2068.4		N	Nul	Nul	Nul	0.000	0.000
2068.6	•	N	Nul	Nul	Nul	0.000	0.000
2068.8		N	Nul	Nul	Nul	0.000	0.000
2069.0		N	Nul	Nul	Nul	0.000	0.000
2069.2		N	Nul	Nul	Nul	0.000	0.000
2069.4		N	Nul	Nul	Nul	0.000	0.000
2069.6		N	Nul	Nul	Nul	0.000	0.000
2069.8		N	Nul	Nul	Nul	0.000	0.000
2070.0		N	Nul	Nul	Nul	0.000	0.000

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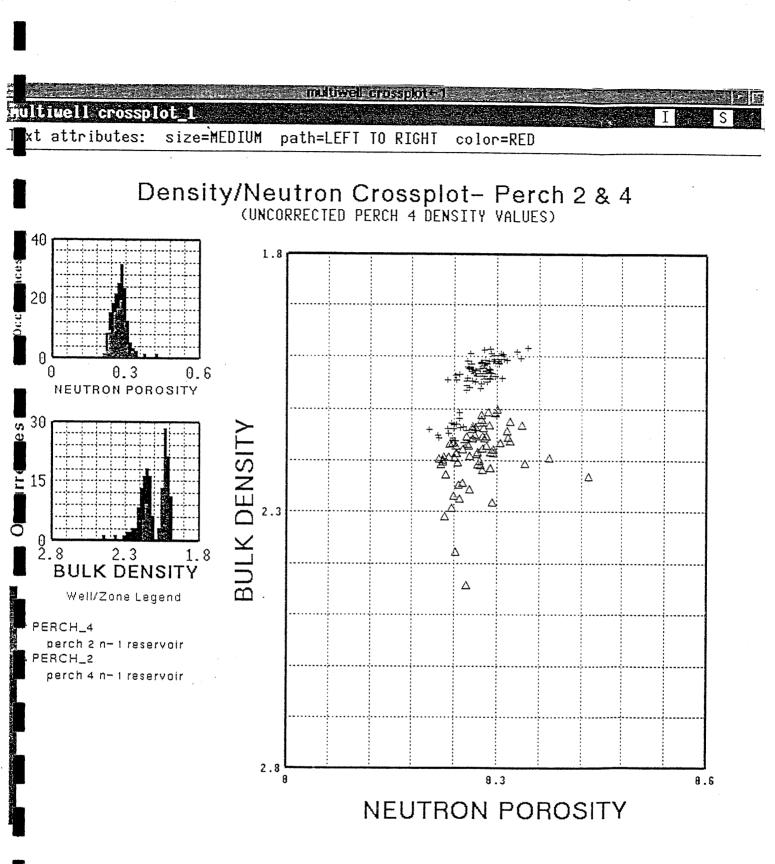


Figure 1

PE600736

This is an enclosure indicator page. The enclosure PE600736 is enclosed within the container PE900924 at this location in this document.

The enclosure PE600736 has the following characteristics: ITEM_BARCODE = PE600736 $CONTAINER_BARCODE = PE900924$ NAME = CBL-VDL-GR Log BASIN = GIPPSLAND PERMIT = TYPE = WELLSUBTYPE = WELL_LOG DESCRIPTION = CBL-VDL-GR Log 1:200 for Perch-4 REMARKS = DATE_CREATED = 19/02/95DATE_RECEIVED = 15/03/95W_NO = W1115 WELL_NAME = Perch-4CONTRACTOR = Schlumberger CLIENT_OP_CO = ESSO

(Inserted by DNRE - Vic Govt Mines Dept)

PE600737

This is an enclosure indicator page. The enclosure PE600737 is enclosed within the container PE900924 at this location in this document.

	00737 has the following characteristics:
ITEM_BARCODE =	
CONTAINER_BARCODE =	= PE900924
NAME =	= Reservoir Evaluation Log (CPI)
BASIN =	= GIPPSLAND
PERMIT =	=
TYPE =	= WELL
SUBTYPE =	= WELL_LOG
DESCRIPTION =	= CPI/Reservoir Evaluation Log (enclosure
	from WCR) for Perch-4
REMARKS =	=
DATE_CREATED =	= 24/08/95
DATE_RECEIVED =	= 25/08/95
W_NO =	= W1115
WELL_NAME =	= Perch-4
CONTRACTOR =	SOLAR
CLIENT_OP_CO =	= ESSO

(Inserted by DNRE - Vic Govt Mines Dept)

APPENDIX 4

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APPENDIX

PERCH-4

Lithology/Show Descriptions

Geologist: Jon Elliott

Wirth .

Perch-4 Lithology/Show Descriptions

<u>Depth (mMD)</u> 1320	<u>%</u> 100	Description <u>LIMESTONE</u> : pale grey, pale grey brown, occasionally off white, micritic to predominantly calc-silty, locally micro-crystalline, firm, blocky, occasional crystalline calcite fossil fragments, trace visual porosity, locally very argillaceous and grading in part to siltstone	
1350	100	LIMESTONE: as above, generally grading to calcareous siltstone.	
1380	100	<u>LIMESTONE</u> : pale grey, occasionally pale grey brown and off white, firm, blocky, predominantly and generally grading to marl, locally calcarenitic, rare calcareous fossil fragments, rare glauconite.	
1410	100	LIMESTONE: as above.	
1440	100	<u>LIMESTONE</u> : pale grey to pale grey brown, occasionally off white, firm, blocky, silty to micritic and generally as marl, locally calcarenitic with common glauconite, occasional calcite fossil fragments, trace visual porosity.	
1470	100	LIMESTONE: as above.	
1500	100	LIMESTONE: generally as above, also occasionally chalky.	
1530	100	<u>LIMESTONE</u> : pale grey, occasionally off white, pale grey brown, firm, massive, micritic to calcisiltitic, rarely calcarenitic, rare pyrite, glauconite, no visual porosity.	
1560	100	LIMESTONE: as above.	
1590	100	<u>LIMESTONE</u> : pale grey, rarely pale grey brown, moderately firm, massive, calcilutitic to calcisiltitic, generally as marl, common microfossils including forams and ostracods, trace glauconite, no visual porosity.	
1620	100	<u>LIMESTONE:</u> pale grey, pale brown, occasionally off white, becoming commonly calcarenitic, generally as marl, locally common glauconite, common microfossils including gastropods and forams, no visual porosity.	
1650	100	<u>LIMESTONE</u> : pale grey, occasionally pale grey brown, pale blue green, firm, massive, calcilutitic to calcisiltitic, rarely calcarenitic, common clastic detritus, trace glauconite, carbonaceous flecks, calcareous fossil fragments, no visual porosity.	
1655	100	LIMESTONE: as above.	
1660	100	LIMESTONE: generally as above, grading increasingly to calcareous claystone in part.	
1665	80 20	<u>LIMESTONE</u> : as above. <u>CLAYSTONE</u> : pale to mid grey, occasionally pale grey brown, moderately firm, subfissile, micromicaceous, very calcareous and generally grading to argillaceous limestone, trace glauconite and carbonaceous flecks.	
1670	80 20	<u>LIMESTONE:</u> as above. <u>CLAYSTONE:</u> as above.	
1675 <i>f</i>	70 30	<u>LIMESTONE</u> : as above. <u>CLAYSTONE</u> : as above, becoming more silty and locally grading to calcareous siltstone.	

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Page 1

<u>Depth (mMD)</u>	<u>%</u>	Description
1680	60	<u>LIMESTONE</u> : pale brown grey, pale grey, soft to moderately firm, massive to subfissile, becoming increasingly argillaceous, common glauconite, locally micromicaceous, rare crystalline calcite possibly from fossil fragments, no visual porosity.
	40	<u>CLAYSTONE:</u> as above.
1685	60	LIMESTONE: as above.
	40	<u>CLAYSTONE</u> : as above with very common forams and occasional gastropods and ostracods.
1690	60	LIMESTONE: as above.
	40	<u>CLAYSTONE:</u> as above.
1695	70	<u>LIMESTONE</u> : pale grey to pale grey brown, moderately firm, massive, calcilutitic grading to calcisilititic, occasional hard limestone clasts, trace glauconite and forams, no visual porosity.
	30	<u>CLAYSTONE:</u> as above.
1700	50	LIMESTONE: as above.
· · · · ·	50	<u>CLAYSTONE</u> : pale brown grey, rare pale grey and green, moderately firm, plastic, moderately to very calcareous, generally grading to argillaceous limestone, trace glauconite, carbonaceous material, very fine mica and rare fossils.
1705	40	LIMESTONE: as above.
	60	<u>CLAYSTONE</u> : as above.
1710	50	LIMESTONE: as above.
	50	<u>CLAYSTONE:</u> as above.
1715	50	LIMESTONE: pale grey brown, occasionally pale brown, off white, firm, massive, very argillaceous, generally grading to calcareous claystone, trace glauconite.
	50	<u>CLAYSTONE</u> : as above.
1720	60	LIMESTONE: as above.
	40	CLAYSTONE: as above.
1725	40	LIMESTONE: as above.
	60	<u>CLAYSTONE</u> : generally as above, becoming increasingly silty and occasionally mid brown in colour.
1730	40	LIMESTONE: as above.
	60	<u>CLAYSTONE</u> : pale to occasionally mid brown, pale brown grey, pale grey, occasionally pale green, firm, massive to subfissile, silty in part, moderate to very calcareous.
1735	50	LIMESTONE: as above.
	50	CLAYSTONE: as above.
1740	40	LIMESTONE: pale grey, pale brown grey, firm, argillaceous, generally grading to calcilutite or calcisilitite, trace glauconite, no visual porosity.
	60	<u>CLAYSTONE:</u> as above.
1745	40	LIMESTONE: as above.
ł	60	CLAYSTONE: as above.
1750	30	LIMESTONE: as above, generally becoming increasingly argillaceous.

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<u>Depth (mMD)</u>	<u>%</u>	Description
. :	70	<u>CLAYSTONE</u> : pale grey, pale grey brown, occasionally pale green grey, firm, subfissile, very calcareous and grading to argillaceous limestone, trace glauconite, and coal.
1755	30 70	LIMESTONE: as above. CLAYSTONE: as above.
1760	30 70	LIMESTONE: as above. CLAYSTONE: as above.
1765	10 90	<u>LIMESTONE</u> : as above becoming slowly more argillaceous. <u>CLAYSTONE</u> : pale brown grey, pale grey, occasionally pale green grey, moderately firm, massive to locally subfissile, moderately to very calcareous, occasional coal and glauconite, silty in part and occasionally grading to siltstone.
1770	10 90	<u>LIMESTONE</u> : pale grey to pale grey brown, firm, massive, very argillaceous and generally grading to calcareous claystone, trace glauconite, occasional hard microcrystalline calcite. <u>CLAYSTONE</u> : as above.
1775	90 10	<u>CLAYSTONE</u> : pale grey to pale grey brown, moderately firm, blocky to subfissile, moderate to very calcareous, common finely disseminated glauconite and coal fragments, occasional crystalline calcite microfossils, generally silty and grading to siltstone in part. <u>SILTSTONE</u> : pale to mid grey brown, mid green, firm, blocky, abundant argillaceous matrix, common to abundant glauconite, moderate to very calcareous.
1780	90 10	<u>CLAYSTONE:</u> as above. <u>SILTSTONE:</u> as above
1785	90 10	<u>CLAYSTONE</u> : as above with increasing dark green fresh glauconite. <u>SILTSTONE</u> : as above.
1790	80 20	<u>CLAYSTONE:</u> as above. <u>SILTSTONE:</u> as above.
1795	70	<u>CLAYSTONE</u> : pale to mid grey brown, occasionally pale brown, pale grey and pale green grey, moderately firm, massive to subfissile, locally common glauconite, very calcareous, silty.
	30	<u>SILTSTONE:</u> mid green, pale to mid grey brown, firm, massive, moderate to very calcareous, locally abundant glauconite, trace carbonaceous material.
1800	70 30	<u>CLAYSTONE:</u> as above. <u>SILTSTONE:</u> as above.
1805	70 30	<u>CLAYSTONE:</u> pale to mid grey brown, pale grey, firm, massive to subfissile, locally splintery, moderate to very calcareous, common medium to coarse well rounded sand grains, locally common glauconite. <u>SILTSTONE:</u> as above with local floating sand grains.
1810	50 60 40	<u>CLAYSTONE</u> : as above with increasing floating sand grains. <u>SILTSTONE</u> : as above.
1815 	40 60	<u>CLAYSTONE</u> : as above. <u>SANDSTONE</u> : off white to pale grey, medium to very coarse grained, generally coarse grained with fair to good sorting, subangular to well rounded, local weak silica cement,

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<u>Depth (mMD)</u>	<u>%</u>	Description	
		trace hard pyrite cement, no matrix, trace glauconite, rare lithics, loose, good inferred porosity, 5% very dull to occasionally moderately bright yellow patchy fluorescence with 'no disenable cut and a trace pale yellow residue. Trace pin point yellow live oil fluorescence in mud.	
1820	20 80	<u>CLAYSTONE:</u> as above. <u>SANDSTONE:</u> as above with 10% very dull yellow fluorescence with cut as above. Rare trace of moderately bright yellow pin point fluorescence in mud.	
1825	20 80	<u>CLAYSTONE</u> : as above <u>SANDSTONE</u> : off white, medium to coarse, occasionally very coarse, fair sorting, subrounded, trace weak silica and moderate pyrite cement, local mid brown silty matrix, occasional glauconite, loose, good inferred porosity, 10% very dull yellow to cream fluorescence with a rare diffuse slow streaming cut and a trace pale yellow residue.	
1830	10 90	<u>CLAYSTONE</u> : as above. <u>SANDSTONE</u> : as above, 10% fluorescence as above. Trace pin point oil fluorescence in mud.	
1835	30 70	<u>CLAYSTONE</u> : mid brown, soft to moderately firm, massive, non to slightly calcareous, silty in part, local brown coal lenses and stringers. <u>SANDSTONE</u> : as above.	
1840	90 10	<u>CLAYSTONE:</u> as above. <u>SANDSTONE:</u> as above.	
1845	100	<u>CLAYSTONE</u> : mid brown, occasionally mid grey brown, non to very slightly calcareous, soft, generally amorphous to soluble, occasionally subfissile, common lignite, locally silty and grading to siltstone.	
1850	100	CLAYSTONE: as above.	
1855	90 10	<u>CLAYSTONE</u> : as above with occasional forams and loose floating sand grains, locally common glauconite. <u>SANDSTONE</u> : off white, green, fine to coarse, generally medium grained with fair sorting, subrounded, trace weak silica cement, common glauconite, loose to friable, fair inferred porosity, no show.	
1860	100	COAL: dark brown, black, firm, massive, rare subconchoidal fracture, earthy, lignitic.	
1865	100	COAL: as above.	
1870	10 90	<u>COAL</u> : as above. <u>SILTSTONE</u> : pale to mid brown, occasionally cream, pale grey, firm, slightly to occasionally moderately calcareous, local moderate silica cement, trace carbonaceous material, argillaceous in part.	
1875	30 60 10	<u>COAL</u> : dark brown to black, firm, massive, lignitic, earthy, locally very silty. <u>SILTSTONE</u> : as above. SANDSTONE: off white, medium to coarse, fair sorting, subrounded, no cement, no matrix, trace glauconite, loose, good inferred porosity, trace pin point dull to moderately bright yellow fluorescence with no cut and no residue.	
1880	60	SILTSTONE: as above.	
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<u>Depth (mMD)</u>	<u>%</u>	Description
`. ;	40	SANDSTONE: as above becoming predominantly coarse to very coarse, no fluorescence.
1885	60 40	[•] <u>SILTSTONE</u> : as above. <u>SANDSTONE</u> : as above with no show.
1890	20 80	<u>SILTSTONE:</u> as above <u>SANDSTONE:</u> off white, coarse to very coarse, fair sorting, subrounded, no cement, local cream silty matrix, rare lithics, pyrite, loose, good inferred porosity, trace very dull yellow patchy fluorescence in matrix with no cut.
1895	60 40	<u>CLAYSTONE</u> : pale grey firm, subfissile, very calcareous and grading to limestone, possibly cavings from above Latrobe Fm after wiper trip. <u>SANDSTONE</u> : as above.
1900	30 70	<u>SILTSTONE</u> : pale to mid grey, pale to dark grey brown, firm, massive to subfissile, non to moderately calcareous, trace pyrite, trace carbonaceous material, occasional forams. <u>SANDSTONE</u> : as above.
1905	20	SILTSTONE: as above.
1905	20 80	<u>SANDSTONE</u> : off white, medium to very coarse, predominantly coarse, fair sorting, subangular to subrounded, local moderate silica cement, locally common white argillaceous matrix, rare lithics, generally loose, fair inferred porosity, no show.
1910	40	<u>SILTSTONE</u> : pale to mid grey brown, pale grey, moderately firm, amorphous and very argillaceous to massive, moderately calcareous, trace disseminated pyrite, and carbonaceous material, occasional micro-fossils.
	60	SANDSTONE: as above.
1915	50 50	<u>SILTSTONE:</u> as above. <u>SANDSTONE:</u> as above.
1920	20	<u>COAL</u> : dark brown, black, firm to moderately hard, local subvitreous lustre and grading from lignite to subbituminous, commonly silty.
	80	SILTSTONE: as above, becoming mid brown to mid grey brown.
1925	40 60	<u>COAL:</u> as above. <u>SILTSTONE:</u> as above.
1930	50 50	<u>SILTSTONE</u> : as above. <u>SANDSTONE</u> : off white, pale brown, fine to occasionally coarse, fair sorting, subangular, weak silica cement, occasional quartz overgrowths, local pale brown argillaceous matrix, generally loose, trace to fair inferred porosity, no show.
1935	70 30	<u>SILTSTONE:</u> as above. <u>SANDSTONE:</u> as above.
1940	30	SILTSTONE: mid brown, pale to mid grey brown, massive, non to slightly calcareous, very argillaceous, trace finely disseminated carbonaceous material.
f jt	70	SANDSTONE: as above, becoming predominantly coarse to very coarse grained.
1945	30 70 Tr	<u>SILTSTONE:</u> as above. <u>SANDSTONE:</u> as above. <u>LIMESTONE:</u> white, soft, massive, chalky, micritic, clean, appears similar to rock flour, is possible calcareous argillaceous matrix from sandstone.

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Depth (mMD) % Description

1950	• _ ·	30 70	SILTSTONE: as above. • <u>SANDSTONE</u> : off white to pale grey, medium to very coarse, angular to well rounded, angular grains are probably fragments from conglomeratic grains, fair sorting, weak silica cement, possible common white chalky micritic matrix, rare lithics and pyrite, loose, fair to good inferred porosity, no show. The matrix has dull yellow natural mineral fluorescence.
1955		10 90	<u>SILTSTONE:</u> as above. <u>SANDSTONE:</u> as above.
1960		10 90	<u>SILTSTONE:</u> as above. <u>SANDSTONE:</u> as above.
1965		70 30	<u>COAL:</u> black to dark brown, firm, massive to subfissile, silty, lignitic, earthy. <u>SANDSTONE:</u> as above.

Lost circulation material added at 1969 m, including mica and kwikseal.

1970	100	<u>COAL:</u> as above.	
1975	100	COAL: as above.	
1980	100	COAL: as above.	
1985	30 20 50	<u>COAL</u> : as above, <u>CLAYSTONE</u> : pale grey brown, soft, soluble, slightly to moderately calcareous, silty, trace carbonaceous material. <u>SANDSTONE</u> : off white, coarse to very coarse grained, angular to subrounded, angular grains may be fragments from very coarse to conglomeratic grains, no cement, off white argillaceous matrix, rare glauconite, loose, good inferred porosity no fluorescence.	
1990	100	SANDSTONE: as above.	
1995	90 10	<u>SANDSTONE:</u> as above. <u>COAL:</u> dark grey, black, dark brown, firm, subconchoidal, subbituminous.	
2000	100	SANDSTONE: off white, coarse to very coarse grained, fair sorting, subangular to subrounded, trace weak silica cement, common off white argillaceous matrix, rare lithics, loose, good inferred porosity no show.	
2005	90 10	SANDSTONE: as above. COAL: as above.	
2010	100	SANDSTONE: as above.	
2015	100	SANDSTONE: as above, generally medium to very coarse grained, good inferred porosity.	
2020	100	SANDSTONE: as above.	
2025	100	SANDSTONE: as above.	
2030	100	SANDSTONE: as above.	
2035	100	SANDSTONE: as above.	

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<u>Depth (mMD)</u>	<u>%</u>	Description
2040	100	<u>SANDSTONE:</u> off white, coarse to very coarse grained, fair sorting, subangular to 'subrounded, rare weak quartz overgrowth cement, local off white argillaceous matrix, occasional lithics, loose, good inferred porosity, no show.
2045	100	SANDSTONE: as above.
2050	100	SANDSTONE: as above.
2052	90 10	<u>SANDSTONE</u> : as above. <u>CLAYSTONE</u> : mid brown, soft, amorphous, moderately calcareous, common very finely disseminated carbonaceous material.

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A total depth of 2052 m was reached at 20:30 hours, 11/02/95.

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APPENDIX 5

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PERCH-4

Mud Log

PE600738

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This is an enclosure indicator page. The enclosure PE600738 is enclosed within the container PE900924 at this location in this document.

The enclosure PE6	00	0738 has the following characteristics:
ITEM_BARCODE :	=	PE600738
CONTAINER_BARCODE :	-	PE900924
NAME :	=	Drilling Data Log (Mud Log)
BASIN :	=	GIPPSLAND
PERMIT :	=	
TYPE :	=	WELL
SUBTYPE :	=	MUD_LOG
DESCRIPTION :	=	Drilling Data Log/Mud Log (enclosure
		from WCR) for Perch-4
REMARKS =	=	
DATE_CREATED =	=	23/02/95
DATE_RECEIVED =	=	25/08/95
W_NO =	=	W1115
WELL_NAME =	=	Perch-4
CONTRACTOR =	=	HALLIBURTON
CLIENT_OP_CO =	=	ESSO

(Inserted by DNRE - Vic Govt Mines Dept)

PERCH-4

Well Completion Log

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PE600739

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This is an enclosure indicator page. The enclosure PE600739 is enclosed within the container PE900924 at this location in this document.

The enclosure PE600739 has the following characteristics: ITEM_BARCODE = PE600739 CONTAINER_BARCODE = PE900924 NAME = Well Completion Log BASIN = GIPPSLAND PERMIT = TYPE = WELLSUBTYPE = COMPLETION_LOG DESCRIPTION = Well Completion Log REMARKS = DATE_CREATED = 23/02/95DATE_RECEIVED = 25/08/95 $W_NO = W1115$ WELL_NAME = Perch-4 CONTRACTOR = ESSO $CLIENT_OP_CO = ESSO$

(Inserted by DNRE - Vic Govt Mines Dept)