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BEACH PETROLEUM N.L.

(Incorporated in South Australia)

PEP 108 OTWAY BASIN

"NA NO. 1

WELL COMPTUTION ESPORT

BY A. BUFFIN OCTOBER 1988 E.C.R. Your Port

APPENDIX 6

VITRINITE REFLECTANCE - TOC

IONA NO. 1

KK No.	Depth (m)	TOC
x8277	1240	1.10%
x8278	1287	0.73%
x8279	1383	0.30%
x8280	1423	0.34%
x8281	1481	0.24%

A1/1 K.K. Depth Description Including Ř, max No. (m) Range Exinite Fluorescence Belfast Mudstone x8277 1240 0.43 0.30-0.54 Sparse phytoplankton and liptodetrinite, greenish yellow and yellow to orange, rare ?Botryococcus related telalginite, bright yellow. (Glauconitic claystone. Dom abundant, I>E>V. Inertinite common, exinite and **SWC 22** vitrinite sparse. Diffuse organic matter common. Glauconite dominant. Iron oxide rare. Pyrite abundant, mostly framboidal.) Waarre Formation 1287 x8278 0.44 0.32-0.56 26 Rare phytoplankton, greenish yellow and yellow to orange, rare sporinite, yellow. (Carbonate>calcareous claystone>>glauconitic claystone. Dom common, I>V>E. SWC 18 Inertinite common, vitrinite sparse, exinite rare. Glauconite rare. Iron oxide common. Carbonate has isolated saccharoidal texture. Pyrite sparse to common.) Eumeralla Formation x8279 0.42 0.40-0.46 1383 Rare to spare phytoplankton and liptodetrinite, greenish yellow and yellow to orange, rare sporinite, yellow, SWC 8 rare resinite, green. (Claystone>calcareous sandstone>coal. Coal rare, V. Vitrite. Dom spare to common, I>E>V. Inertinite and eximite sparse, vitrinite rare. Inertinite consists of very fine inertodetrinite. Iron oxide rare. Pyrite major.) x8280 0.41 0.33-0.48 27 Rare phytoplankton and liptodetrinite, greenish yellow 1423 SWC 4 and yellow to orange, rare cutinite, yellow. (Siltstone>>coal. Coal sparse, V. Vitrite. Dom commo V>I>E. Vitrinite sparse to common, inertinite sparse, exinite rare to sparse. Rare canneloid shale grains in siltstone, probably reworked. Rare thucholites. Weak brown fluorescence from desmocollinite. Rare yellow oil droplets. Iron oxide rare. Pyrite sparse.) 4 Rare phytoplankton and liptodetrinite, greenish yellow and yellow to orange. (Calcareous claystone>siltstone. x8281 1481 0.47 0.37-0.53 SWC 1 Dom common, I>E>V. Inertinite common, exinite rare to 0.95 0.84-1.04 sparse, vitrinite rare. Dom mainly consists of very fine inertodetrinite. Rare thucholites. Iron oxide

rare to sparse. Pyrite rare.)

VITRINITE RELECTANCE NORKSHEET

WELL WARE JOING # 1

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SAMPLE NO.X 8277

DEPTH

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Keiraville Konsultants Pty Ltd.

VITRINITE REFLECTANCE NORKSHEET

WELL NAME TONG # 1

FGV = First Generation Vitrinite :

SAMPLE NO. X 8278

DEPTH. 127

TYPE SUSC.

8<u>8</u> Organic matter Comp.(%) Alginite. 25 0 . S. - 0> Exinite 8 1.90 1.92 8. .. B. **z** 1.95 1.96 1.98 2.00 Roge Pop Roge Type Read 80 **≤** 1.55 3.2 **3.** 35 2.60 2.65 1.62 2 1.68 1.70 1.67 1.2 1.7 1.75 1.76 1.7 1.78 1.79 1,80 1.81 1.82 1.83 86. 46. ခွင့် 2.0 0.0 0.0 80 € 1.21 1.22 1.24 1.25 1.26 1.28 1.30 1.27 1.3 1.32 1.33 1.35 7.7 1.36 1.38 1.40 .39 1.45 1.41 7: 7. 1.46 1.47 28 2× နှင့် ကို \$. 8. 8. 8 8 3 ¥. .85 .86 .88 .89 8 1 = Inertinite 6. 8 8 8 8 20.0 .08 1.10 1.07 90.1 8 1, 11 8<u>%</u> 200 8.50 8.00 8 .46 .47 49 [2] 19. 3 3 3 3 6 69 ۱۲. 5 5 2 5 Pop Pop Ruge Type Se ad 8 의= .13 51. 61. . 12 = .20 .22 .24 .25 .25 .25 . 18 61. 2 8 8 5 .32 R ٦, 36 .38 .39 35

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38. 1,87 1.88 1.89

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1,51

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VITRINITE RELECTANCE NORKSHEET

WELL WARE JOHO # 1

SAMPLE NO. X 8279

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VITRINITE RELECTANCE NORKSHEET

WELL WARE JOHO # 1

SAMPLE NOX 8780

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Keiraville Konsultants Pty Ltd.

VITRINITE RELECTANCE NORKSHEE

SAMPLE NO. X 8281

NELL MAYE, TONA - I

Pope Organic matter Comp. (%) 25 Itr in ite | inertinite TYPE SLYC. 9 0 80 % x In Ite 8. 1.91 1.92 2.3 3 1.95 .8 1.97 1.98 . 0 Pop ခိုင် DEPTH 1481 W Ro S 3.1.52 1.59 1.60 - . 63 - . 63 1.61 3. 39. 1.67 1.68 1.69 1.70 1.75 1.76 1.7 1.79 .80 1.81 -. B 1.83 1.85 <u>.</u> 1.86 1,87 1.88 1.89 Roge Pype Ro % 1.29 1.21 1.23 1.24 1.25 1.26 1.27 1.33 7. 1.35 1.38 1.39 3, 1.40 1.42 1.43 = 1.44 1.45 1.46 1.47 1.48 1.49 3. 7 1, 51 3. Age Age RIN ITE 95 55 55 Re so INE 2 1 = Inertinite 8 3 8. 28 .86 .88 8 8 6 8.6 8 8 8 8 98. 66. 8. 1.8 9 <u>-</u> 2 8 ..05 .8 1.07 98. 1.10 1,11 1.12 .13 1.17 ₹ X Pay Resid FGV = First Generation Vitrinite .. 8 .47 49 3 2 ษ 3 2 3 8 8 2 3 2 3 8 6 2 3 3 .68 69. 5. ۲. u. 5. .75 .76 .77 .78 2 8 Lybe Ype 18. Sop Sop 9: = 51. 61. . 12 = . 18 .20 .30 .30 .32 7 × .35 .36 .38 .39 40 .42 \$.45

Keiraville Konsultants Pty Ltd.

APPENDIX 13

ROUTINE CORE ANALYSIS

CPWITE



technology and enterprise

Amdel Limited

(Incorporated in S.A.) 31 Flemington Street, Frewville, S.A. 5063

Telephone: (08) 372 2700

P.O. Box 114, Eastwood, S.A. 5063

Telex: AA82520

Facsimile: (08) 79 6623

25 March 1988

F 3/0/0 F 5179/88

Beach Petroleum NL PO Box 360

CAMBERWELL VIC

Attention: Mr J. Foster

REPORT F 5179/88

YOUR REFERENCE:

Verbal request

TITLE:

Routine core analysis

MATERIAL:

Core plugs

IDENTIFICATION:

IONA-1

3124

DATE RECEIVED:

18 March 1988

WORK REQUIRED:

Porosity, air permeability, grain density

Investigation and Report by: Russell R. Martin

Manager, Petroleum Services Section: Dr Brian G. Steveson

for Dr William G. Spencer

General Manager

Applied Sciences Group

cap '

1. INTRODUCTION

On 18 March 1988 a conventional core (1305.5 m-1314.5 m) from Beach Petroleum's Iona-1 well was received at Amdel Limited's Adelaide Laboratory. A verbal request from Beach Petroleum's representative was received concerning the nature of analysis to be performed. The analysis included:

Porosity - ambient conditions only Air Permeability - ambient conditions only Grain Density - calculated

2. SAMPLE PREPARATION

The core was laid out according to depth and the core examined. After attempting to drill one-and-one-half-inch diameter plugs in the conventional manner, i.e. tap water as the bit lubricant, it was found that representative samples could not be taken.

Sections of core were packed in dry ice for a period of twelve hours. At which time individual samples were removed and one-and-one-half-inch diameter samples taken using liquid nitrogen as the bit lubricant. Samples were trimmed and faced square while still frozen and mounted in lead sleeves. Weights of the encapsulating lead and screens were recorded.

The samples were then placed in a hassler type cell and pressured to 500 psig to squeeze the lead sleeve to conform to the shape of the sample.

Samples were then placed in a soxhlet extraction apparatus with a 3:1 chloroform/methanol mix to leach any residual hydrocarbons and salts.

Upon completion the extraction samples were placed in a conventional dry oven at 110°C.

3. HELIUM INJECTION POROSITY

Porosity is determined using the Boyles Law helium injection technique to determine sample grain volume. Sample pore volume, in the case of lead sleeve, is determined by loading the samples into a hassler type cell and confining the sample with an external pressure of 400 psig. Helium is again injected and pore volume recorded.

Porosity is then calculated and expressed as a percentage value.

4. PERMEABILITY TO AIR

Permeability to air is also determined whilst the sample is confined in the hassler type cell at 400 psig. A known air pressure is passed through the sample and the differential pressure at the outlet face of the sample is monitored utilising a calibrated orifice and straight tube manometer.

In the majority of cases the samples exceeded the maximum accurate operating limits of the permeameter and are expressed as greater than 8000 millidarcys.

Sample offcuts were retained and a brief lithological description concludes this report.

Amdel Limited would like to thank Beach Petroleum for the opportunity to have been of service with this study. Should you have any questions, or if Amdel Limited can be of further service please do not hesitate to contact us.

LITHOLOGICAL DESCRIPTION

Company: Well: Field:	Beach Petroleum IONA-1 IONA
1	No offcut
2	Sst: Lt gry, med-v.crs. gr, cln, p. cmt, sbang-ang, p. srt, v. fri, v. rr cl mtrx, no vis fluor, no cut, pale wh ring.
3	No offcut
4	Sst: Lt gry, med-occ. v.crs. gr, cln, p. cmt, sbang-ang w. crs, p. srt, v. fri, sps cl mtrx, fluor and cut a/a.
5	Sst: lt gry, dom. med-rr crs gr, cln, p. cmt, sbrnd-sbang, p. srt, v. fri, v. sps cl mtrx, fluor and cut a/a.
6	As above.
7	Sst: Lt gry, rr f-occ. crs gr, cln, p. cmt, sbang, p. srt, v. fri rr qtz ovgth, carb spk, fluor and cut a/a.
8	Sst: Lt gry, rr f-occ crs gr, cln, p. cmt, sbang, p. srt, fri, rr qtz ovgth, carb spk, tr pyr carb mat, fluor and cut a/a.
9	Sst: Lt gry, dom med-v. crs grn, cln, p. cmt, sbang, p. srt, v. fri, sps cl mtrx, fluor and cut a/a.
10	Sst: As above. dom crs gr.
11	Sst: As above. dom crs-v. crs gr.
12	Sst: As above. no vis fluor, v. slow milky wh cut.
13	Sst: Lt gry, dom crs-v.crs gr, cln, p. cmt, sbang, v. fri, p. srt, v. sps mtrx, no vis fluor, v. slow milky wh cut.
14	Sst: Lt gry, f-med intbd, crs gr, cln, p. cmt, sbrnd-sbang, mod srt, fri, sps mtrx, carb spk, fluor and cut a/a.
15	Sst: As above.
16	Sst: Lt gry, dom med-occ crs gr, cln, p. cmt, sbrnd, mod srt, v. fri, sps mtrx, fluor and cut a/a.

17	Sst: wh-lt gry, fn med gr, mod cmt, sbrnd, mod srt, fri, sps mtrx, abd carb lam, dull yell fluor along carb lam, instant bright wh cut.
18	Sst: Lt gry, med-dom crs gr, p. cmt, sbang, p. srt, v. fri, v. sps mtrx, carb lam, dull yell fluor along carb lam, instant bright wh cut.
19	Sst: Lt gry, med-dom crs v. crs gr, p. cmt, sbang, p. srt, v. fri, v. sps mtrx, carb spk, rr dull yell p.p. fluor, slow milky cut.
20	Sst: As above.
21	Sst: As above.
22	Sst: As above.
23	Sst: As above.
24	Slst dk gry, v. f gr. sst intbd, pyr lam, no vis fluor, instant milky wh cut.

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Table 1

AMDEL CORE ANALYSIS

IONA No. 1

Ambient

Sample		Permeability (md)	Porosity (%)
	1305.81	7216	23.0
2		>8000	24.4
		>8000	24.3
		>8000	23.4
5	1306.71	>8000	25.7
6	1307.23	>8000	27.1
7	1307.54	>8000	27.2
8	1307.84	>8000	26.4
9	1308.20	>8000	23.3
10	1308.45	>8000	28.7
1. 1.	1308.80	>8000	25.9
12	1309.10	>8000	27.5
13	1309.40	>8000	26.6
14	1309.70	7407	26.6
15	1310.00	>8000	26.8
16	1310.3	>8000	25.0
1.7	1310.60	5149	28.6
18	1310.90	>8000	23.5
19	1311.20	>8000	24.6
20	1311.50	>8000	24.7
21	1311.80	>8000	25.5
22	1312.02	6264	21.0
23	1312.40	>8000	23.0
24	1312.70	6.13	10.7



Table 2

AMDEL CORE ANALYSIS

IONA No. 1

Ambient

		Bulk	Apparent	Absolute
Sample 	Bulk Volume	Dry Density	Grain Density	Grain Density
1	49.81	2.10	2.72	
y .st.	57.99	2.09	2.76	
3		2.03	2.68	
4	52.64	2.05	2.67	
5	56.30	1.98	2.66	
ć.	48.75	1.95	2.68	
. 7	56.73	1.95	2.68	
ε	55.72	1.97	2.67	
9	58.32	2.05	2.67	
1 C	57.15	1.90	2.67	
1 1	57.48	1.98	2.67	
12	57.73	1.95	2.68	
13	57.63	1.96	2.67	
1.4	63.64	1.96	2.67	
15	61.81	1.95	2.67	`y
1 6	58.07	1.99	2.65	
17	52.07	1.77	2.48	
1 8	62.86	2.05	2.67	
19	65.13	2.01	2.67	
20		2.01	2.67	
21		1.99	2.67	
22	59.51	2.11	2.67	
23	52.65	2.05	2.67	
24	58.11	2.44	2.73	

APPENDIX 15

FORMATION RESISTIVITY FACTOR
RESISTIVITY INDEX

27 May 1988

technology and enterprise

Amdel Limited

(Incorporated in S.A.)
31 Flemington Street,
Frewville, S.A. 5063

Telephone: (08) 372 2700

P.O. Box 114, Eastwood, S.A. 5063

Telex: AA82520

Facsimile: (08) 79 6623

Beach Petroleum NL

PO Box 360

CAMBERWELL VIC 3124

Attention: Mr J. Foster

REPORT F 7197/88

YOUR REFERENCE:

Fax No. 72/4, 19 April 1988

TITLE:

Special core analysis

SAMPLE IDENTIFICATION:

IONA-1

MATERIAL:

Core plugs

WORK REQUIRED:

Formation resistivity

factor

and

resistivity index

Investigation and Report by: Russell R. Martin

Manager, Petroleum Services Section: Dr Brian G. Steveson

for Dr William G. Spencer

General Manager

Applied Sciences Group

Brain Blevera.

cap

1. INTRODUCTION

Correspondence was received by Amdel Limited on 19 April 1988 (your ref.: facsimile no. 72/4 19 April 1988) requesting the following analyses be performed:

- Formation resistivity factor
- Formation resistivity index

on selected samples from Iona-1 well.

The three samples selected had previously undergone routine core analysis conducted by Amdel Limited and porosity at a net overburden pressure of 13,800 kPa (2000 psi).

2. PROCEDURES AND RESULTS

The samples were frozen prior to removing the encapsulating lead sleeve and screens, then wrapped in teflon tape and encapsulated in a rubber sleeve before loading into the electrical properties cells. The required overburden pressure of 13,800 kPa (2000 psi) was then applied using a mineral oil to the outside of the sample.

Samples were then evacuated and the simulated formation brine consisting of 80% NaCl, 10% CaCl₂ and 10% KCl was introduced to the sample. Brine was slowly flushed through the sample until a stable resistivity reading was obtained indicating ionic equilibrium had been achieved.

Samples were allowed to stand for approximately 24 hours to ensure equilibrium had been attained.

Humidified air was then introduced to the sample to displace some of the brine and establish the first saturation point from which to commence resistivity index measurements.

Resultant plots of formation resistivity factor versus porosity fraction yield a value for `m', the cementation exponent of 1.74.

Archie reported that the cementation exponent probably ranged from 1.8 to 2.0 for clean consolidated sandstones and as low as 1.3 for clean unconsolidated sands.

Pirson⁽¹⁾ adapted Archie's work to produce a family of curves for formation factor versus porosity percent for various reservoir characteristics or cementation classes.

From Pirson's work slightly cemented sands fall in the range of 1.55 to approximately 1.75 for `m', the cementation exponent.

The samples from Iona-1 range from very slightly cemented to moderately cemented across the cored interval and the measured value of `m' for this formation falls within the slightly cemented class as described by Pirson.

Resultant plots of formation resistivity index yield values for `n', the saturation exponent of between 1.99 and 2.17. The composite plot yields a value for `n' of 2.08.

Cation exchange capacity measurements are generally performed on shaly sand formations to refine electric log data and provide values of F*, m* and a*. Cation exchange capacity values can also be used for better correlation with Rw data. Bearing in mind that the brine used to determine `m', `n' and `a' for Iona is not the actual brine concentration present in the reservoir but of one close by, values may need to be adjusted slightly. However, as Iona is a relatively homogeneous clean sand the adjustment in `m' and `n' because of a different brine concentration will in all probability be minimal.

As Iona is a very clean sand and based on the petrographic work carried out, very low values for cation exchange capacity would be expected for this reservoir sand which would not influence the calculation of F^* , m^* and a^* to any significant extent. Therefore, cation exchange capacity determinations in this case are probably unnecessary.

3. REFERENCES

(1) PIRSON, S.J. "Oil Reservoir Engineering". McGraw Hill Book Company.

Page 1 of 7 File: F7197/88

FORMATION RESISTIVITY FACTOR AS A FUNCTION OF OVERBURDEN

Company: Beach Petroleum

Formation:

Well: Iona-1 Field:

Iona

Location:

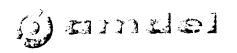
Overburden pressure:

Rw of saturant:

2000 psi 25000 ppm 0.26 ohm.m @ 25°

Sample ID	Depth m	Permeability to Air millidarcys	Porosity %	Formation Resistivity Factor
1	1305.81	7216	21.0	14.7
10	1308.45	>8000	27.1	10.1
22	1312.02	6264	19.5	16.5

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Company:

Beach Petroleum

Iona-1

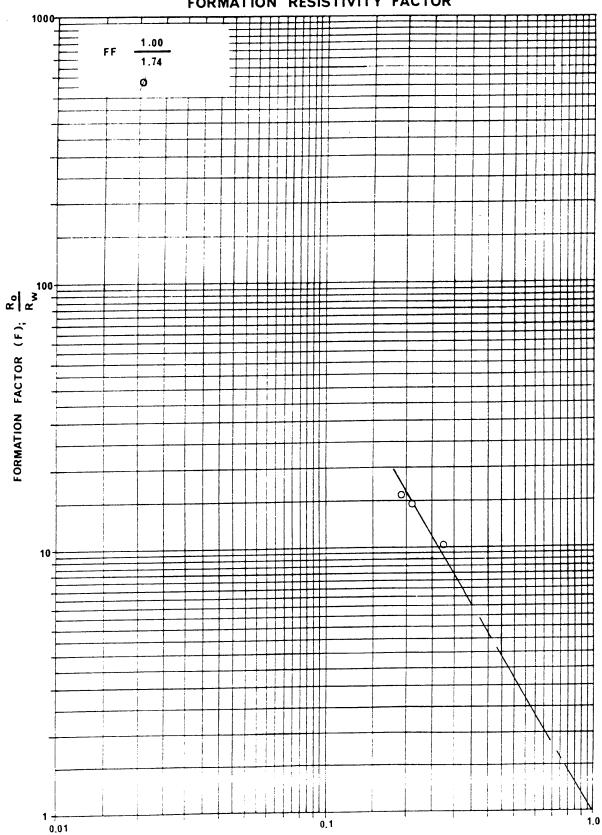
Well: Field:

Iona

Formation: Location:

Saturant: 25,000 ppm Overburden Pressure: 2000 psi

FORMATION RESISTIVITY FACTOR



POROSITY: Fraction

Page 3 of 7 File: F7197/88

FORMATION RESISTIVITY INDEX AS A FUNCTION OF OVERBURDEN

Company: Well:

Beach Petroleum

Formation:

Field:

Iona-1 Iona

Location:

Overburden pressure: 2000 psi Saturant: 25000 ppm Rw of saturant: 0.26 ohm.m @ 25°

Sample ID	Depth m	Permeability to Air, millidarcys	Porosity %	Formation Resistivity Factor	Brine Saturation % Pore Space	Formation Resistivity Index
1	1305.81	7216	21.0	14.7	100.0 75.1 63.8 56.7 45.6	1.00 1.89 2.47 3.16 4.84
10	1308.45	>8000	27.1	10.1	100.0 75.3 65.9 58.8 48.7	1.00 2.01 2.37 3.02 4.40
22	1312.02	6264	19.5	16.5	100.0 75.2 64.0 54.3 42.1	1.00 1.90 2.35 3.19 5.21

Page 5 of 7 File: F7197/88

Company: Beach Petroleum

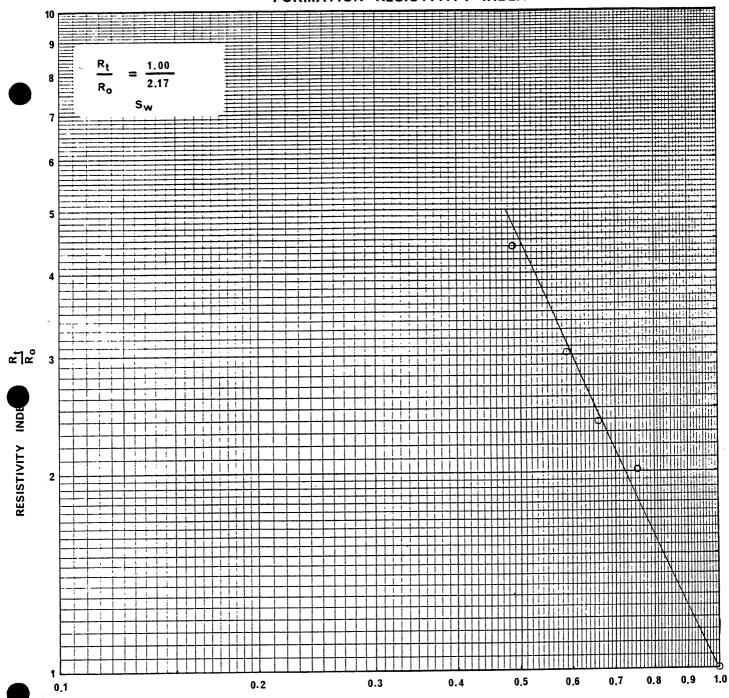
Well: Iona-1 Field: Iona

Formation: Location:

Sample No. 10

Saturant: 25,000 ppm Overburden Pressure: 2000 psi

FORMATION RESISTIVITY INDEX



BRINE SATURATION; Fraction of Pore Space

Page 6 of 7 File: F7197/88

Company: Beach Petroleum

Well: Iona-1 Field: Iona

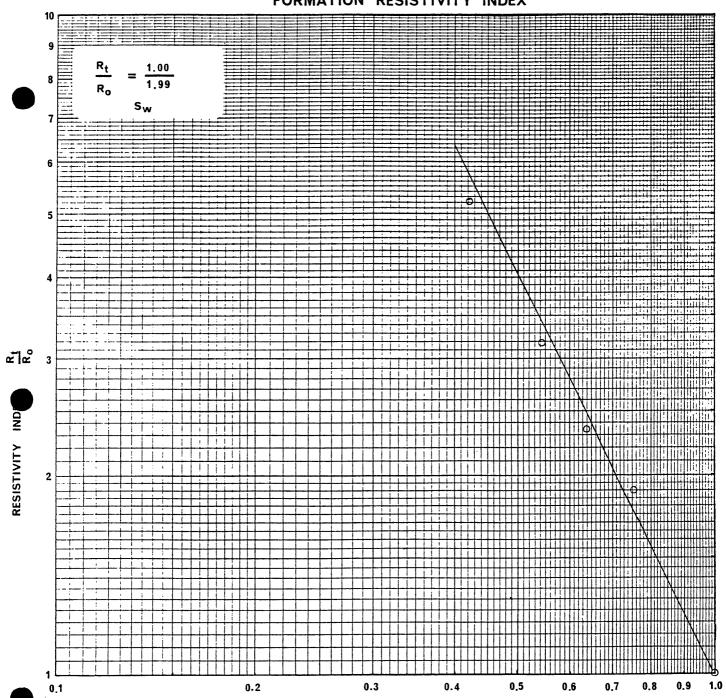
Sample No. 22

Saturant: 25,000 ppm

Overburden Pressure: 2000 psi

Formation: Location:

FORMATION RESISTIVITY INDEX



BRINE SATURATION; Fraction of Pore Space

Page 7 of 7 File: F7197/88

Company:

Beach Petroleum

Well:

Iona-1

Formation: Location:

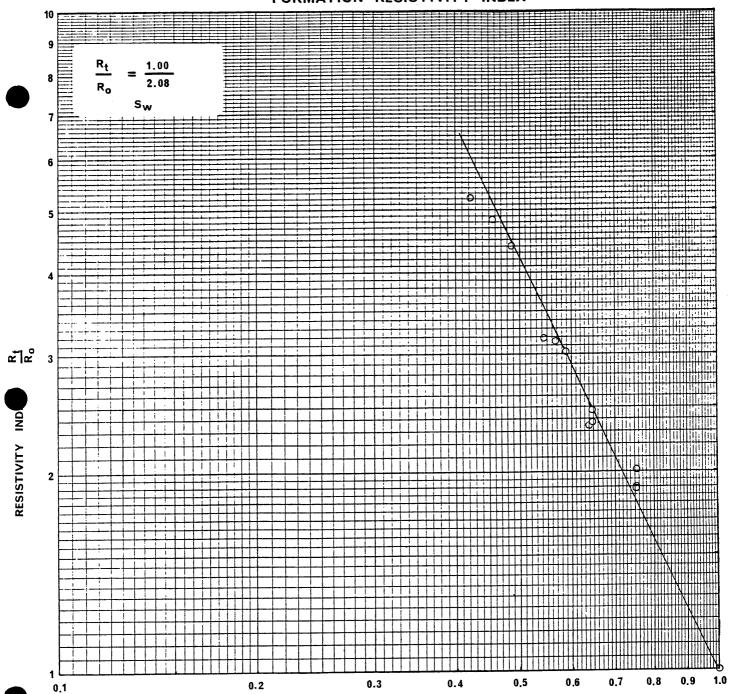
Field:

Iona

Composite

Saturant: 25,000 ppm Overburden Pressure: 2000 psi

FORMATION RESISTIVITY INDEX



BRINE SATURATION; Fraction of Pore Space

APPENDIX 16

RESIDUAL GAS ANALYSIS



BEACH PETROLEUM

IONA #1

SPECIAL CORE ANALYSIS

hese analyses, opinions or interpretations are based on observations and materials supplied by the client to whom; and for whose exclusive and confidential use; this report is made. The interpretations or opinions expressed represent the best judgment of Core Laboratories, (all errors and omissions excepted); but Core Laboratories, and its officers and employees, assume no responsibility and make no warranty or representations, as to the productivity, proper operations, or profitableness of any oil gas or other mineral well or sand in connection with which such report is used or relied upon.



July 13, 1989

Beach Petroleum GPO Box 7096 Sydney NSW 2001

Attention: Mr. A. Buffin

Subject : Special Core Analysis

Well : Iona #1 File : 318-88004

Dear Sir,

Core Laboratories was requested by Mr. A. Buffin of Beach Petroleum to perform residual gas determination on samples from the subject well.

Preliminary data was sent via telex on the 19th July 1988. This report finalizes all data.

Core Laboratories thanks you for the opportunity to have been of service with this study. If you have any questions, please feel free to call.

Yours sincerely CORE LABORATORIES

Peter Lane

Petrophysical Laboratory Supervisor

PRL:jc

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Summary of Data	2	
Discussion of Laboratory Procedures and Results	3	
Residual Gas Saturation	4	

<u>SUMMARY</u>

Residual gas saturations determined tend to have a relationship with initial gas saturation. The highest residual gas saturation recorded corresponded to the highest initial gas saturation.

RECOMMENDATIONS

 $\underline{\text{Capillary Pressure}}$: Drainage capillary pressure tests will help in determining the water saturation profile in the reservoir.

 ${\underline{\sf Water-Gas}}$ Relative permeability : Relative permeability data is necessary to properly model the reservoir performance.

SUMMARY OF DATA

IONA #1

		<u>Max</u>	<u>Min</u>	<u>Ave.</u>
Porosity, percent	ø	24.6	21.0	22.7
Permeability to air, millidarcies	Ka 10	0,000	7,000	8,930
Residual Gas Saturation, percent pore volume	Sgr	38.6	28.9	32.4
Gas Recovered, percent pore space	Sgm	61.9	55.2	59.6

DISCUSSION OF LABORATORY PROCEDURES AND RESULTS

SAMPLE PREPARATION

Three one-and-one-half inch diameter samples were received at our laboratory in Perth for testing. Two were enclosed in lead sleeves and the third wrapped in teflon tape. The teflon tape was removed from the sample prior to cleaning in hot toluene and methanol with the other two samples. The samples were then dried at 115°C to constant weight. Permeability to air and porosity were determined.

REDISUAL GAS SATURATION: COUNTER CURRENT IMBIBITION METHOD (Page 4)

After the initial room conditions permeability and porosity were determined, the samples were evacuated under toluene and then reduced to the desired "irreducible water saturation" by controlled drying. Each of the samples was then suspended under toluene and weight gain monitored as a function of time. Each test was terminated when there was negligible change in weight versus time. The residual gas saturations were calculated from these data and are tabulated on page 4.

The residual gas saturation obtained for the samples show a trend. The sample with the most initial gas in place has the greatest residual gas saturation.

Page : 4 File : 88004

RESIDUAL GAS SATURATION BY COUNTER CURRENT IMBIBITION

Company : Beach Petroleum Well : Iona #1

Gas Recovered	percent percent gas lore space in place	67.6	58.8	67.4
	percent pore space	61.7	55.2	61.9
Residual Gas Saturation, percent pore space		29.6	38.6	28.9
Initial Liquid Saturation, percent pore space		8.7	6.2	9.2
;	Porosity, percent	21.0	24.6	22.4
Permeability to Air, millidarcys		0086	7000	10000
11	ueptn, meters	1308.45	1310.30	1312.40
Sample I.D.		10	16	23