

MARLIN-A6.

902875 001

Page 1 of 34

DEPT. NAT. RES & ENV



PE902875

WELL DATA FOLDER  
FOR MARLIN-A6  
(WS25)

# COMPOSITE

## WELL SUMMARY REPORT FOR WEEK ENDING:

Well **MARLIN A6**  
Company **Hemathite - Cas.**

902875 002

Location:

Latitude **38° 13' 56"**

Longitude **148° 13' 16" (T.M.P)**

**Conductor No. 22 of Marlin "B" Platform.**

Tenement:

**Production License No. 3.**

Logistics:

Drilling Unit **National 1320 Rig on Marlin Platform**

Water Depth

Well datum and elevation **K.B. 82 feet a.s.l.**

Programmed depth. Vertical **+6821/15,000** Measured **75,000/16821'**

✓ Direction of deviation

✓ Distance of deviation (horizontal)

} **See attachment.**

Total depth

~~Vertical~~

Measured **11068 feet.**

Depth at date of report (measured)

Status

**Suspended for Production**

Spud date

**11<sup>th</sup> August 1968**

Date of reaching total depth

Date abandoned or suspended

**1<sup>st</sup> December 1968.**

Date completed for production

Stratigraphy:

Formation Tops (depths below well datum)

~~Preliminary interpretation~~

**Tropic Valley Coal Measures 5400' (M.D.).**

**Upper Carboniferous**

**10458' (M.D.) i.e. 8924' below sea level**

Hydrocarbon Indications;

902875 003

(a) Gas detector and Chromatograph Recordings.

The following intervals contain zones with significant recordings

(b) Fluorescence and other indications.

10890'-10910' @ 1.0. white fluorescence and cut.

F.I.T. by Schlumberger

Cased Hole	RECOVERIES										MARLIN AG				WELL NAME & NUMBER				MUD PENETRATION			
	No	Depth (ft)	GAS		CONDENSATE		OIL		MUD		OTHER		K	Q	JFT	Rmt	Rw	Rnt	GOR	FSIP		
cu. ft.			cc.	API	cc.	API	cc.	API	cc.	API	cc.	API									cc.	API
1	10170	60	0		14250	40.6	60															
2	10134	117.1	700	59.9	0															3820		
3	9866	129.1	800	57	60															3300		
4	9390	119	600	60.7	60															3620		
5	9210	0	0		0															3250		
6	9205																			0		
7	6578																			0		
8	6101	88.1	300																	2500		
9	6584																			2290		
10	10140	4	0		500	39.4	60													5050		
11	10204	42.4	0		15000	39.9	60													3880		

Hydrostatic pressure = 5050 psi.

Seal valve did not seal chamber. Sample lost.

902875 004

WIRE-LINE TESTS

Conventional								
No	Interval	cut.	Rec.		No	Interval	cut.	Rec.
1	8224' - 8254'	30'	30'	✓				
2	8254' - 8314'	60'	49'	✓				
3	9200 - 9329'	28	28					
4	9328 - 9355	27	27					

Side wall cores.

Log Run	Shot	Rec.		Log Run	Shot	Rec.
1						
2						
3						
4	✓					

Casing

Size	Setting Depth.	Cemented.
13 7/8"	3324' (M.D.)	Yes.
9 5/8"	10,846' (M.D.)	256sq. ft at 6697 feet
		1st Stage 20255+ + addition
		2nd Stage 11005+
		D.V. Leaked + 2 squeeze jobs. Total 2502 sq. ft.

Electrical Logs.

Type	Interval	Logging Company
IES	433' - 3773' - 1015'	Schlumberger
SGR	433' - 3265'	"
GR/FDL	<del>6550</del> 3324 - 6520 - 10830	"
GRN	3324 - 10845	"
GR/Sonic		

Mud Logging. Core lab from 3326 feet to T-D

Velocity Survey

Palaeontology

Palynology

Petrology.

Plugs: On Top of fish (Fish 10980-11068') + side track.

Plugs for sidetracking: 4<sup>th</sup> Plug 10970'-10980' 10898'  
 10054 : 10883' - 10600' 6700 - 6420'  
 10250' - 9750'  
 9450 - 9100

Model K retainer at 6050'  
 + squeeze proof at 6101'  
 20 225 5+ Cop. of "K"

# Notes

902875 007

or Weekly reports.

Top of Lutroba sequence at 547 (4624) on drilling form, samples + gas readings.

Wet gas reservoir.

Drilled from 8596' to 9442' of week end in the Paleocene section.

" " " " " " " " " " " "

Correlation with Marlin 1 suggests that 10367' drilled in this well is some 260' low to Marlin 1, although the interpreted top of the Paleocene in A-6 appears to be about 120' high to Marlin 1, as predicted. A fault may have been crossed + now drilled on low side. (at 10479')

Top of Upper Cretaceous section from log correlation with Marlin 2 is at 10458' MD (-8724 ss).

<u>Predicted Tops</u>		<u>Actual Tops</u>
Lakes Entrance	4300' TVD.	
Lutroba (Eocene)	4600' TVD	4624' TVD.
" (Paleocene)	6900' TVD	
" (Upper Cretaceous)	8500' TVD	8724' TVD ss.
Strzelecki.	14,500' TVD.	
	Attended to slightly higher.	



Surveyed positions of log 75 008

Mark A.G.

Tangential Method.  
Radius of Curvature to same center

Measured Depth.	Vertical Depth.	Angle	Direction.	S. Course.	E. Course.	
500	500	$3\frac{1}{4}^{\circ}$	S45°E	1	1	✓
592	592	$3\frac{1}{4}^{\circ}$	N72°E	0	5	
748	747	$6\frac{1}{4}^{\circ}$	S80°E	3	21	
872	870	$8\frac{1}{2}^{\circ}$	S77°E	7	39	
1028	1023	10°	S77°E	13	63	
1183	1175	$13\frac{1}{2}^{\circ}$	S74°E	22	95	
1277	1265	$15\frac{1}{2}^{\circ}$	S72°E	30	118	
1400	1382	$18\frac{1}{4}^{\circ}$	S67°E	45	153	
1525	1499	$20\frac{3}{4}^{\circ}$	S65°E	60	194	
1682	1644	24°	S67°E	88	250	✓
1837	1781	$27\frac{3}{4}^{\circ}$	S64°E	117	313	
1992	1915	32°	S63°E	153	380	
2107	2011	$33\frac{1}{4}^{\circ}$	S63°E	171	440	
2294	2164	$34\frac{3}{4}^{\circ}$	S64°E	218	535	✓
2576	2395	$35\frac{1}{4}^{\circ}$	S62°E	293	679	✓
2827	2598	36°	S61°E	364	808	✓
3136	2848	$36\frac{1}{4}^{\circ}$	S58°E	469	969	✓
3326	3001	$36\frac{1}{2}^{\circ}$	S58°E	529	1064	✓
3441	3094	36°	S57°E	565	1121	
3751	3347	$35\frac{1}{4}^{\circ}$	S55°E	668	1268	✓
3949	3510	$34\frac{3}{4}^{\circ}$	S54°E	734	1359	
4060	3599	$36\frac{1}{4}^{\circ}$	S52°E	775	1411	✓
4171	3687	$37\frac{3}{4}^{\circ}$	S50°E	818	1463	
4304	3789	40°	S49°E	875	1527	
4429	3885	40°	S49°E	927	1588	✓
4647	4049	41°	S49°E	1021	1696	✓
4864	4211	41°30'	S48°E	1117	1803	✓
5090	4381	41°30'	S48°E	1217	1914	
5305	4541	42°	S47°E	1316	2019	✓
5462	4656	$42\frac{3}{4}^{\circ}$	S46°E	1390	2096	
5525	4702	43°	S45°E	1420	2126	✓
5651	4794	43°	S45°E	1481	2187	
5835	4934	40°30'	S47°E	1562	2274	✓
6058	5110	38°	S46°E	1658	2373	
6182	5206	39°	S47°E	1711	2430	

Cont-



6740	5329	39 $\frac{1}{4}$ $^{\circ}$	S49E	+	1776	2505
6440	5405	40 $^{\circ}$	S48E		1819	2553
6745	5635	41 $^{\circ}$	S47E		1956	2699
7019	5839	42 $^{\circ}$	S47E		2081	2834
7285	6034	43 $^{\circ}$	S47E		2204	2966
7414	6130	41 $\frac{1}{2}$ $^{\circ}$	S47E		2263	3029
7543	6229	40 $^{\circ}$	S47E		2319	3089
7742	6385	38 $^{\circ}$	S48E		2403	3181
7992	6586	36 $^{\circ}$	S46E		2564	3349
8226	6776	34 $\frac{1}{2}$ $^{\circ}$	S46E		2600	3386
8509	7015	32 $^{\circ}$	S47E		2703	3496
8756	7229	29 $\frac{1}{2}$ $^{\circ}$	S46E		2788	3586
8917	7372	26 $\frac{3}{4}$ $^{\circ}$	S45E		2841	3639
9073	7513	24 $\frac{3}{4}$ $^{\circ}$	S44E		2889	3686
9300	7722	22 $\frac{3}{4}$ $^{\circ}$	S42E		2954	3740
9500	7907	21 $^{\circ}$	S40E		3010	3794
9690	8086	20 $^{\circ}$	S39E		3061	3835
9870	8257	18 $^{\circ}$	S37E		3106	3870
10071	8450	16 $^{\circ}$	S35E		3152	3903
10182	8557	15 $^{\circ}$	S33E		3176	3918
10300	8671	13 $\frac{3}{4}$ $^{\circ}$	S32E		3200	3933
10458	8806	12 $^{\circ}$ 30'	S29'E		3227	3948
10632	8977	10 $^{\circ}$	S27'E		3255	3962
10785	9129	8 $^{\circ}$ 30'	S25'E		3275	3972

Correlation of LES and f-Sonic logs of

Marlin No. 1 Well + Marlin A6 Well.

All depths are those printed on log.

Marlin No. 1 Well	=	Marlin A6 Well	
4522 feet ✓		5400 ✓	feet
4598 ✓		5400 ✓	lower KTD
4640 ✓		5443 ✓	
4666 ✓		5495 ✓	
4722 ✓		5563 ✓	
4792 ✓		5663 ✓	
4919 ✓		5794 ✓	
4992 ✓		5882 ✓	
5110 (I) ✓		6050 ✓	6058 <sub>1/2</sub> = 5110 TND
5290 ✓		6223 ✓	
5395 ✓		6390 (I) ✓	6340 = 5329
5527 (Poor) ✓		6515 ✓	
5684 ✓		6708 ✓	
5896 ✓		6969 ✓	
5926 ✓		6997 ✓	7019 = 5839
6015 ✓		7130 ✓	
6100 ✓		7214 ✓	
6218 ✓		7452 ✓	
6298 ✓		7490 ✓	
6510 - 18 <sup>⊕</sup> = 6492 ✓		7705 ✓	7742 = 6385
6653 - 18 = 6635 ✓		7895 ✓	
6840 - 18 = 6822 ✓		8112 ✓	
7335 - 18 = 7317 ✓		9012 ✓	9073 = 7513
7430 - 18 = 7412 ✓		9227 ✓	
7970 - 18 = 7952 ✓		9850 ✓	9870 = 8257
8041 - 18 = 8023 ✓		9930 ✓	
8257 - 18 = 8239 ✓		10162 ✓	10182 = 8557.

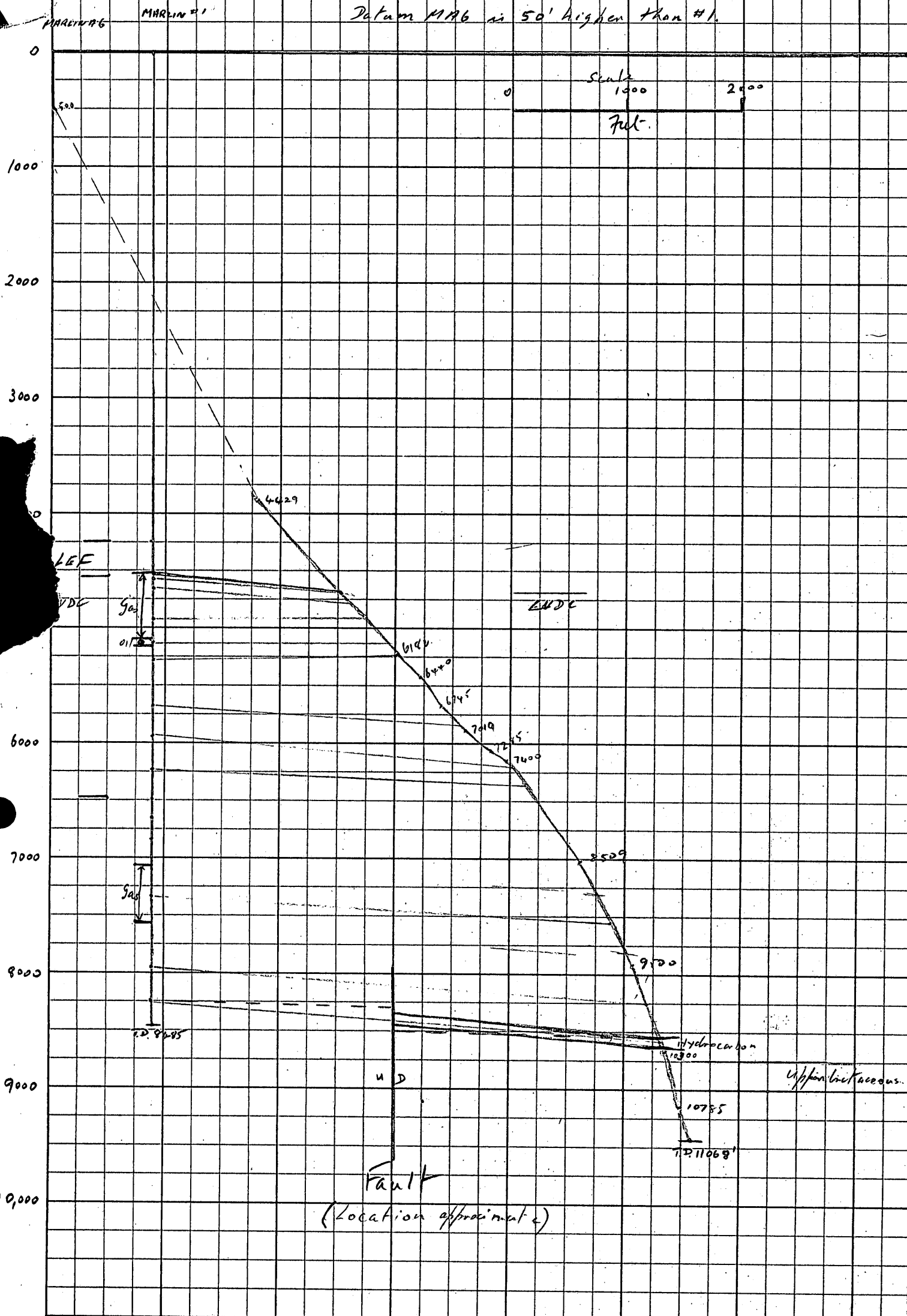
4-11-68

M. J. J.

Plan 3 of SGR - BR reads 14' low.

502875 011

Well depths used  
Datum MAR6 is 50' higher than #1.

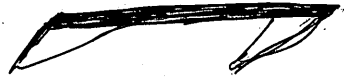


March 16.

902875 012

Plug well.

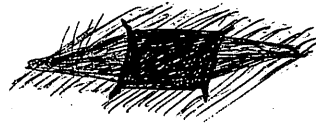
16800 M.D.



XA-1

Fitt

Preliminary depth 7 F.I.T.



10170:

FTm

10134:

9866:

9390:

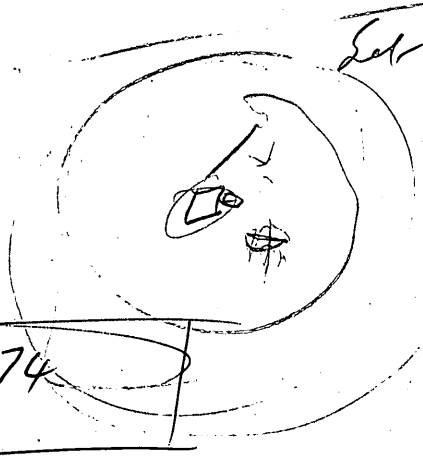
9210:

6578:

Set for 1005

10883-10600

~~10418~~

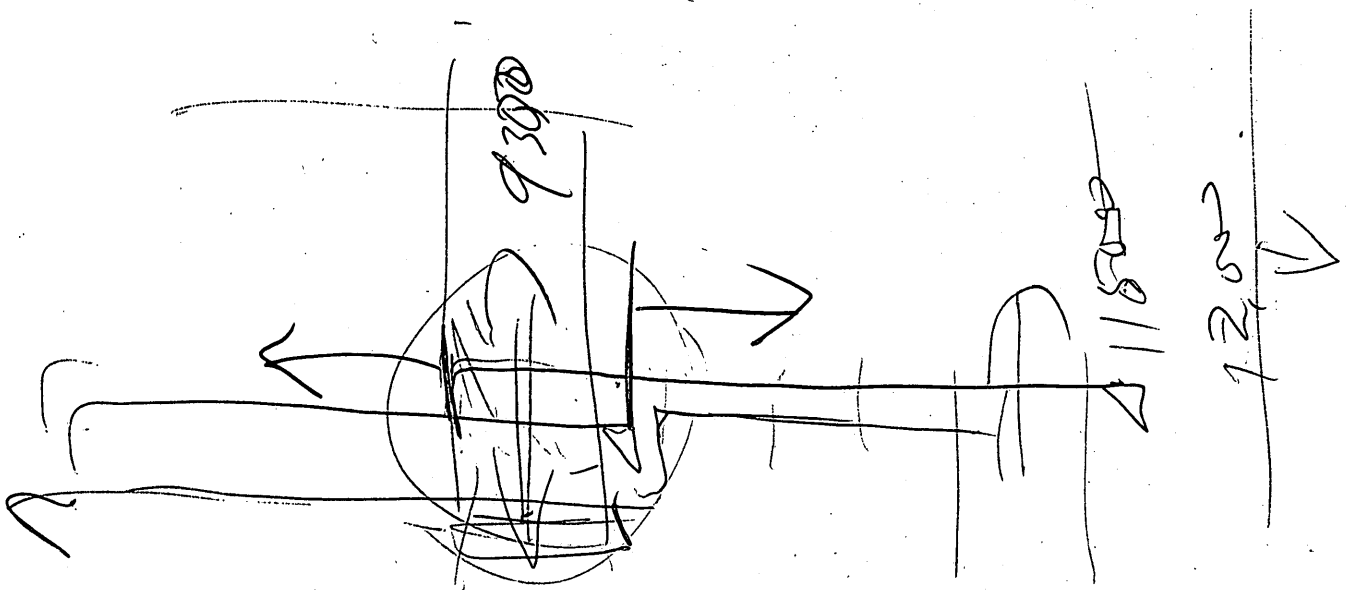


6101-6074  
at the

7 Farnham

9110-9132.

6960-7000.



In an examination of the logs from 6500' - 10849' several sands show the presence of hydrocarbon but in commercial quantities in the thickness of log in of the order of 2-5 feet. By a comparison logs they appear to mostly contain gas.

902875 013

$S_w = 100\%$  - as defined.

70% = 2 R<sub>o</sub>

50% = 4 R<sub>o</sub>

30% = 11 R<sub>o</sub>

20% = 25 R<sub>o</sub>

40% = R<sub>o</sub>

60% = R<sub>o</sub>

70% = 2 R<sub>o</sub>

80% = R<sub>o</sub>

90% = R<sub>o</sub>

$$F = \frac{1}{\phi^2}$$

$$R_c = \frac{FR_w}{S_w}$$

$$S_w = \sqrt{\frac{R_o}{R_c}}$$

MAG

GD

OH

- 6750-60 - bad
- 6800-6860 - bad
- 7030-7400 - bad
- 7480-7570 - gas
- 7710-7720 - bad
- 7900-8225 -
- 8230-8510 -
- 8610-8720 bad
- 8890-8900 bad
- 8960-8970
- 9030-9120
- 9250-9260
- 9780-9790
- 9860-9940
- 10150-10160
- 10170-10200
- 10260-10380
- 10785-10820
- 10920-10970
- 11015-11042

- 8226-8237
- 8251-4
- 8255-62 1/2
- 8275 1/2 - 79
- 9300-9301
- 9310-9327
- 10210-20
- 10600-680
- 10790-10820
- 10870-80
- 10890-10910

7475'-7490' SW 70%

7565'-7570' SW 50%

7897-7909 - SW 50%

8003-8018 - SW 75%

8110-8120 - SW 70%

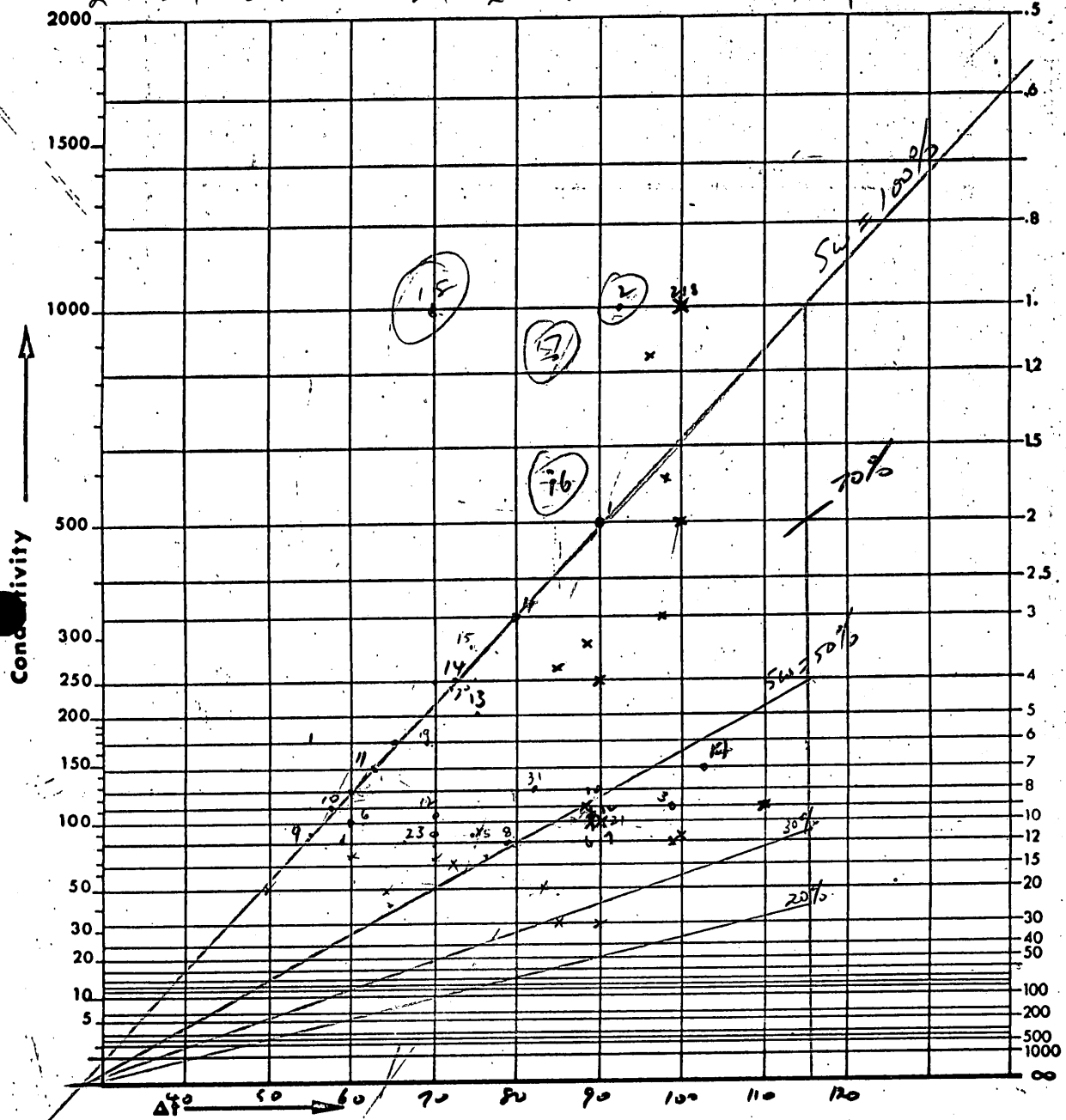
8215-8225 - SW 60%

From 8405-8530' about 9 sands with hydrocarbon.  
 Mean that 20' avg 8'

902875 014

Marlin A6 "B"

2.4 2.7 2.6 2.5 2.4 2.3 2.2 2.1 2.0 1.9 1.8



Grid for Resistivity ~~vs~~ or vs Formation Density Plot

$$F = \frac{.62}{\phi^{2.15}}$$

Depth	R <sub>1L</sub>	Δρ	R <sub>1L</sub>	Δρ
1	6490	2	2.2	100
2	6490	1	2.18	100
3	6590	9	2.11	110
4	6600	3	2.3	97
5	7160	11.5	2.35	100
6	7490	10	2.5	88
7	7565	10	2.23	90
8	7900	12	2.31	97
9	7910	11	2.55	75

Depth	R <sub>1L</sub>	Δρ	Depth	R <sub>1L</sub>	Δρ	Notes
10	8120	9	2.52	84		
11	8150	7	2.47			
12	6790	9.5	2.4	88		
13	6815	9.5	2.35	85		
14	6735	4	2.37	90		
15	6817	3.5	2.37	88		
16	6970	1.6	2.25	98		
17	6980	1.1	2.25	96		
18	6995	1.0	2.4	100		
19	6630	6.0	2.41			
20	6640	4.1	2.38			
21	7157	10	2.2			
22	7270	11				
23	7482	11	2.4			
24	7490	10	2.5			
25						
26						
27						
28						
29						
30						
31						
32						
33						
34						
35						
36						
37						
38						
39						
40						
41						
42						
43						
44						
45						
46						
47						
48						
49						
50						
51						
52						
53						
54						
55						
56						
57						
58						
59						
60						
61						
62						
63						
64						
65						
66						
67						
68						
69						
70						
71						
72						
73						
74						
75						
76						
77						
78						
79						
80						
81						
82						
83						
84						
85						
86						
87						
88						
89						
90						
91						
92						
93						
94						
95						
96						
97						
98						
99						
100						
101						
102						
103						
104						
105						
106						
107						
108						
109						
110						
111						
112						
113						
114						
115						
116						
117						
118						
119						
120						

52

OK 777 Water

shaly

Caly

SMA

9090 13 2.53 - 90

9100 15 2.4 - 60

9110 20 (2.47) - 70

9120 22 2.24 - 650

9130 20 2.2 - 650

Marlin Ab.

X

X

No	Depth.	R <sub>12</sub>	G <sub>0</sub>	ΔC			Sw%. Notes.
1	9100	15.5	2.37				60 910-1932 Ga by S+N
2	9120	30	2.25				30 Separation.
3	9200	20	2.27				40
4	9220	22	2.45				52
5	9305	21	2.45				60
6	9320	14	2.5				80
7	9380	20	2.6				100
8	9390	30	2.2				26
9	9410	14	2.34				50
10	9418	19	2.4				50
11	9505	16	2.37				50
12	9746	9.0	2.55				90+
13	9855	14	2.4				60
14	9860	20	2.26				40
15	9870	25	2.37				45
16	9890	15	2.44				70
17	9912	14	2.3				45 ? waly
18	10120	18	2.32				47
19	10130	23	2.3				40
20	10140	16	2.1				30
21	9093	13	2.4				60 See No 1+2.
22	9188	14	2.3				48 see 3+4
23	9190	18 1/2	2.3				35
24	10550	6	2.45				100 Central Point
25	10360	3.5	2.42				100 +
26	10380	6	2.55				100 + shaly
27	10300	10	2.55				100
28							
29							
30							
A							
B							
C							
D							
E							



MARLIN A6.

902875 018

No	Depth.	R <sub>IL</sub>	$\sigma_B$	$\Delta C$			Sw%. Notes.
1	10080	17	2.5				70
2	10090	11	2.42				70
3	10120	18	2.32				45
4	10130	23	2.3				36
5	10140	16	2.3				45 Coaly?
6	10172	16	2.37				50
7	10180	30	2.4				28
8	10188	18	2.22				32
9	10200	10	2.4				70
10	10215	5	2.45				100
11	10220	5	2.47				100+
12	10230	3	2.42				100+
13	10240	3	2.4				100+
14							
15							
16							
17							
18							
19							
20							
21							
22							
23							
24							
25							
26							
27							
28							
29							
30							
A							
B							
C							
D							
E							

MARLIN A6

"A"

902875 017

Marlin A6  
(Measured Depth)

Gas (High Resistivity + Sand or Gamma + High Neutron)

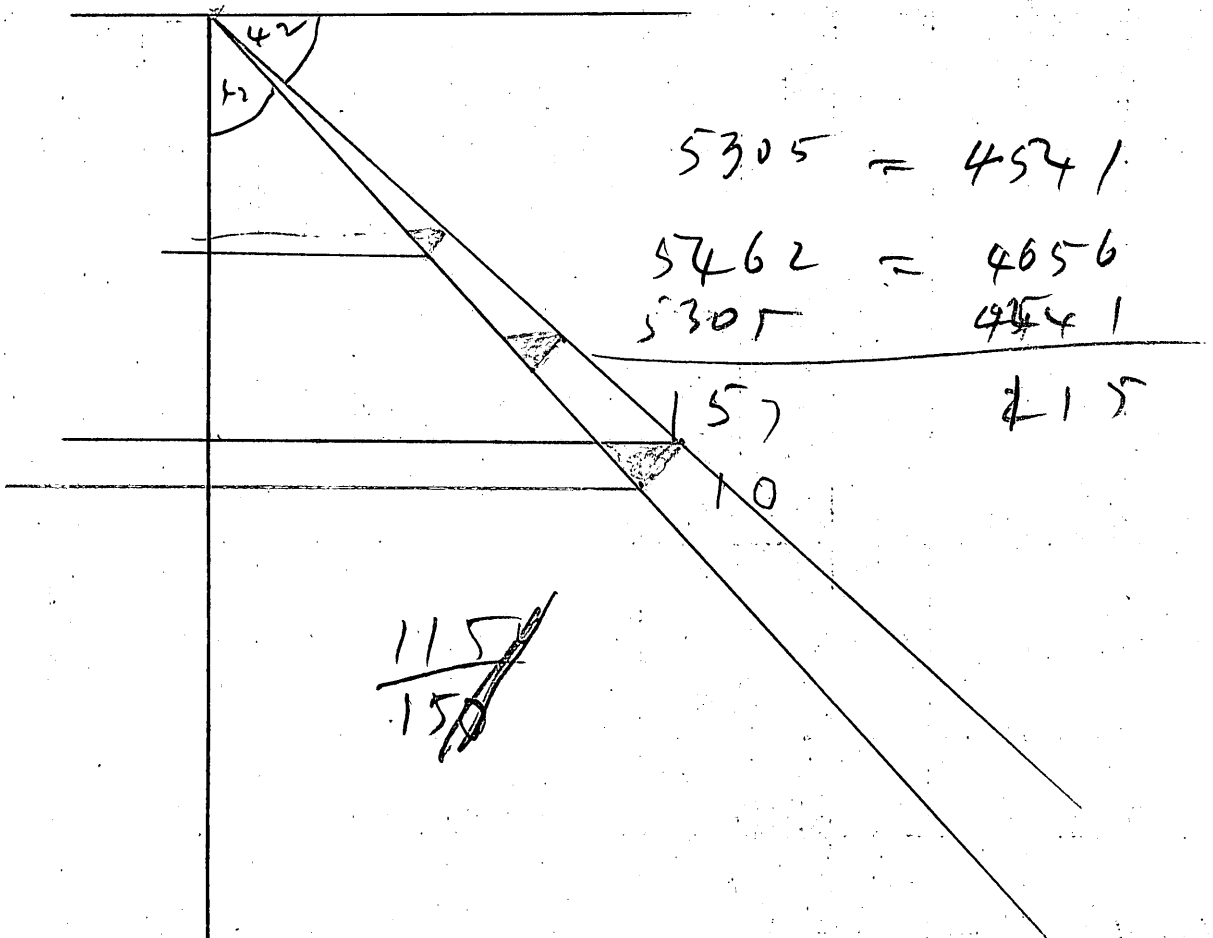
~~5400~~

From 5418 - 5750 = ~~330~~ 332 = 2450D

Nett	5418 - 5444	=	26
	5497 - 5549	=	48
	5551 - 5563	=	12
	5667 - 5750	=	83
			<u>1</u>

169 feet MD = 120' VD

97  
 34  
 18  
 26  
 63  
 51  
 12  
 850  
 667  
 83



5750' - 5800' :- Coal

Base of Hydrocarbon Column

6112 - Hydrocarbon/Water Contact

Petrography:

902875 018

Well: Marlin AB

Sample No.: 75686

Depth: 8230'

HANDSPECIMEN DESCRIPTION: fine grained arenite

THINSECTION DESCRIPTION:

Detrital Mineralogy:

Monocrystalline quartz 80%

Polycrystalline quartz 15%

Feldspar < 5%

Metasediments < 5%

Textural Characteristics:

Angular grains, although equigranular  
fine-grained

Concavo-convex grain relations

Moderate sorting

Abundant undifferentiated matrix

Post-depositional Adjustments:

Severe compaction, minor grain fracture

Products - kaolinite, siderite, quartz cement  
(illite?)

Paragenetic Relations:

1. compaction

2. siderite replacement of framework + matrix

3. Qtz cement + overgrowths

4. kaolinite filling in pores

Key Features:

\* Sporadic  $\phi$  distribution due to framework dissolution  
and subsequent infilling by kaolinite.

Petrography:Well: Marlin A6Sample No.: 75785Depth: 8226'

HANDSPECIMEN DESCRIPTION: v. fine arenite

THINSECTION DESCRIPTION:

## Detrital Mineralogy:

Polycrystalline Qtz 10%  
 Monocrystalline Qtz 75%  
 Metasediments 10%  
 K-feldspar 5%

## Textural Characteristics:

v. fine grained  
 irregular grain shapes/boundaries - this may not be a  
 depositional feature.  
 concavo-convex relations  
 moderate sorting, abundant undifferentiated matrix

## Post-depositional Adjustments:

Compaction w/out fracturing  
 Hydrocarbon pore linings  
 siderite replacement of biotite  
 Quartz overgrowths and cement  
 kaolinite replacement of framework.

## Paragenetic Relations:

1. Compaction
2. Siderite replacement
3. Qtz overgrowths + cement
4. Dissolution of framework grains
5. Kaolinite replacement of lithics
6. Hydrocarbon emplacement.

## Key Features:

\* 2°  $\phi$  production due to framework dissolution.

Petrography:Well: Markin A6Sample No.: 75691Depth: 8275'

HANDSPECIMEN DESCRIPTION: extremely fine grained sandstone

THINSECTION DESCRIPTION:

Detrital Mineralogy:

Polycrystalline quartz 25%  
 Monocrystalline quartz 45%  
 K-feldspar 10%  
 Rock fragments 20%

Textural Characteristics:

Angular, poorly rounded grains  
 Compaction is severe  
 Moderate sorting  
 v. fine grained

Post-depositional Adjustments:

Siderite replaces matrix + rock fragments  
 Kaolinite replacement of metaseds  
 Compaction w/out fracture  
 Kaolinite infilling pores.

Paragenetic Relations:

1. Compaction
2. Siderite ppt<sup>n</sup>
3. Kaolinite replacement of metaseds
4. Kaolinite ppt<sup>n</sup> in  $\phi$

Key Features:

\* 2° porosity is absent, infilled by  
 kaolinite

Petrography:Well: Marvin #6Sample No.: 75688Depth: 8260'

HANDSPECIMEN DESCRIPTION: fine grained arenite

THINSECTION DESCRIPTION:

Detrital Mineralogy:

monocrystalline quartz 70%

Feldspar 10%

Rock fragments ~20%

Textural Characteristics:

v. fine grained

angular grains

Moderate to good sorting

Concave-convex boundaries

Post-depositional Adjustments:

Kaolinite and illite replacement of framework + matrix  
quartz overgrowths.

Compaction to out fracturing

Siderite replacement of lithics

Paragenetic Relations:

1. compaction

2. Quartz overgrowths

3. Siderite replacement

4. Kaolinite replacement of lithics

Key Features:

\* No 2°  $\phi$

Petrography:

902875 022

Well: Marlin A6

Sample No.: 75092

Depth: 8279'

HANDSPECIMEN DESCRIPTION: fine grained arenite

THINSECTION DESCRIPTION:

Detrital Mineralogy:

monocrystalline quartz 70%

Polycrystalline quartz 5%

Feldspar 10%

Rock fragments 15%

Textural Characteristics:

Extremely fine grained sandstone

angular grains

Moderate sorting

Post-depositional Adjustments:

Illite replacement of rock fragments

Siderite replacement of " "

quartz cement + o.g. growths

Kaolinite ppt<sup>n</sup>

Compaction

Paragenetic Relations:

1. Compaction - metaseds are molded around qtz.

2. Qtz o.g. + cement.

3. Siderite replacement

4. Illite replacement

5. Kaolinite ppt<sup>n</sup> in  $\phi$

Key Features:

\* minor, sporadic  $\phi$  distribution



**Petrography:**Well: *Marlin A6*Sample No.: *75695*Depth: *9306'*HANDSPECIMEN DESCRIPTION: *fine grained, organic layering*

THINSECTION DESCRIPTION:

Detrital Mineralogy:

*Metasands 20%**Pyrite 5%**Quartz 75%*

Textural Characteristics:

*Extremely fine grained**Angular grains**severely compacted**Good sorting*

Post-depositional Adjustments:

*Siderite replacement of lithics**Kaolinite replacement of metasands**2°  $\phi$  minor development*

Paragenetic Relations:

*1. Compaction**2. Siderite replacement**3. Kaolinite replacement*

Key Features:

Petrography:

Well: Marlin A6

Sample No.: 75700

Depth: 9340'

HANDSPECIMEN DESCRIPTION: fine grained sandstone.

THINSECTION DESCRIPTION:

Detrital Mineralogy:

Monocrystalline qtz 55%

Polycrystalline qtz 10%

Micas 20%

Feldspar 15%

Textural Characteristics:

fine grained arenite

angular grains compaction is not severe

apparent open framework

Moderate sorting.

Post-depositional Adjustments:

Extensive dolomite cement

siderite replacement of lithics

Quartz overgrowths

Kaolinite replacement of lithics

Kaolinite ppt<sup>n</sup> in  $\phi$ 

Paragenetic Relations:

1. Minor compaction

2. coincident dolomite and siderite

3. Quartz overgrowth

4. Kaolinite replacement of lithics

5. kaolinite ppt<sup>n</sup> in pore space.

Key Features:

\* 2°  $\phi$  absent due to kaolinite ppt<sup>n</sup> in pore space

TURRUM-2      MARLIN-A6      TURRUM-1      MARLIN-A18

	75675	75686	75700	75731	75733	75737	75751	75755
Monocrystalline quartz	36.4	33.2	35.2	32.0	38.0	48.7	50.6	48.06
Polycrystalline quartz	16.6	18.0	5.2	5.33	12.6	9.6	10.0	21.2
Feldspar	2.8	2.8	3.0	2.0	2.6	4.7	1.2	0.52
Lithics	2.2	15.6	6.2	1.33	9.2	5.8	2.4	1.04
Carbonate	—	16.8	31.6	0.66	—	—	27.2	13.17
Mica	1.33	1.6	3.4	1.33	1.4	—	—	0.26
∅	8.6	1.4	0.8	2.67	12.4	—	8.4	12.14
Undifferent <sup>d</sup> -matrix	23.4	8.0	13.4	40.67	20.0	27.33	0.20	0.52
Hydrocarbon	—	0.4	1.2	—	3.4	3.2	—	3.1
Accessories	8.67	0.2	—	14.0	0.4	0.67	—	—

Table 1: Compositions of Latrobe Group Sediments.

SAMPLE LIST. *of what?*

<u>SAMPLE NO.</u>	<u>NAME</u>	<u>DEPTH</u>	
75670	Turrum 2	1569.7 m.	5149 ft.
75671	Turrum 2	1570.9 m.	5153 ft.
75672	Turrum 2	1751.7 m.	5746 ft.
75673	Turrum 2	2315.3 m.	7596 ft.
75674	Turrum 2	2316.2 m.	7598 ft.
75675	Turrum 2	2318.0 m.	7604 ft.
75676	Turrum 2	2320.8 m.	7614 ft.
75677	Turrum 2	2326.3 m.	7632 ft.
75678	Turrum 2	2329.0 m.	7640 ft.
75679	Turrum 2	2332.7 m.	7653 ft.
75680	Turrum 2	2318.3 m.	7605 ft.
75681	Turrum 2	2554.9 m.	8382 ft.
75682	Turrum 2	2599.1 m.	8527 ft.
75683	Turrum 2	2602.1 m.	8536 ft.
75684	Turrum 2	2612.8 m.	8572 ft.
75685	Marlin A 6	2507.6 m.	8226 ft.
75686	Marlin A 6	2508.8 m.	8230 ft.
75687	Marlin A 6	2514.0 m.	8247 ft.
75688	Marlin A 6	2517.7 m.	8260 ft.
75689	Marlin A 6	2518.6 m.	8263 ft.
75690	Marlin A 6	2520.7 m.	8269 ft.
75691	Marlin A 6	2522.3 m.	8275 ft.
75692	Marlin A 6	2523.5 m.	8279 ft.
75693	Marlin A 6	2525.3 m.	8285 ft.
75694	Marlin A 6	2527.4 m.	8291 ft.
75695	Marlin A 6	2836.5 m.	9305 ft.
75696	Marlin A 6	2836.8 m.	9306 ft.
75697	Marlin A 6	2839.6 m.	9316 ft.
75698	Marlin A 6	2841.4 m.	9322 ft.
75699	Marlin A 6	2843.2 m.	9327 ft.
75700	Marlin A 6	2846.9 m.	9340 ft.
75701	Marlin A 6	2847.5 m.	9342 ft.
75702	Marlin A 6	2849.0 m.	9346 ft.
75703	Marlin A 6	2850.8 m.	9352 ft.
75728	Turrum 1	936.7 m.	3073 ft.
75729	Turrum 1	1952.6 m.	6406 ft.
75730	Turrum 1	1953.2 m.	6408 ft.
75731	Turrum 1	1955.9 m.	6416 ft.
75732	Turrum 1	2133.6 m.	6999 ft.
75733	Turrum 1	2151.6 m.	7058 ft.
75734	Turrum 1	2154.9 m.	7069 ft.
75735	Turrum 1	2157.1 m.	7077 ft.
75736	Turrum 1	2160.8 m.	7089 ft.
75737	Turrum 1	2165.3 m.	7103 ft.
75738	Turrum 1	2175.4 m.	7137 ft.
75739	Turrum 1	2179.3 m.	7149 ft.
75740	Turrum 1	2182.4 m.	7160 ft.

SAMPLE NO.NAMEDEPTH

902875 027

75741	Turrum 1	2188.5 m.	7180 ft.
75742	Turrum 1	2192.1 m.	7191 ft.
75743	Turrum 1	3051.7 m.	10012 ft.
75744	Turrum 1	3055.0 m.	10022 ft.
75745	Marlin A 18	1741.0 m.	5711 ft.
75746	Marlin A 18	1742.9 m.	5718 ft.
75747	Marlin A 18	1747.1 m.	5731 ft.
75748	Marlin A 18	1751.4 m.	5745 ft.
75749	Marlin A 18	1754.1 m.	5754 ft.
75750	Marlin A 18	1757.5 m.	5766 ft.
75751	Marlin A 18	1759.6 m.	5772 ft.
75752	Marlin A 18	1764.2 m.	5787 ft.
75753	Marlin A 18	1767.6 m.	5799 ft.
75754	Marlin A 18	1769.1 m.	5804 ft.
75755	Marlin A 18	1771.8 m.	5812 ft.
75756	Marlin A 18	1775.2 m.	5824 ft.
75757	Marlin A 18	1729.5 m.	5674 ft.
75758	Marlin A 18	1735.6 m.	5694 ft.
75759	Marlin A 18	1776.1 m.	5827 ft.
75760	Marlin A 18	1784.6 m.	5854 ft.
75761	Marlin A 18	1826.1 m.	5991 ft.
75762	Marlin A 18	1829.7 m.	6002 ft.
75763	Marlin A 18	1836.1 m.	6123 ft.

PLATFORM:

MARLIN

WELL NO: A-6

OIL and GAS DIVISION

24 JAN 1983

DATE D-M-Y	COMPANY	JOB DESCRIPTION - REMARKS
27-3-69 - 29-3-69	Otis/Schlumberger	Set packer. Perforate, set ball valve (BV).
27-4-69 - 4-5-69	Otis/Schlumberger	Tag bottom at 1654 m MDKB. Ran sand bailer. Well worked over. Set packer. Re-perforate. Gradient pressure survey. Change out BV. Tag bottom at 1641 m MDKB. Ran sand bailer.
10-5-69 - 12-5-69	Otis	Well worked over and gravel packed. Set packer. Set BV.
22-5-69 - 24-5-69	Otis	Gradient pressure survey. Acidize formation.
29-5-69 - 1-6-69	Agnew	Change out BV. Test for suspected packer leak. No leak detected. Tag bottom at 1777 m MDKB. Gradient pressure survey.
15-8-69 - 16-8-69	Agnew	Tag bottom at 1750 m MDKB. Gradient pressure survey.
23-1-70	Agnew	Change out BV.
17-1-71	Agnew	Gradient pressure survey.
21-3-72	Otis	Change out BV.
25-5-72	Otis	Change out BV. Ran Eastman survey.
5-1-73	Otis	Change out BV. Set plug in sliding sidedoor at 1602 m MDKB.
26-1-73	Otis	Change out BV. Pulled plug from sliding sidedoor at 1602 m MDKB
2-2-73	Otis	Set plug in sliding sidedoor at 1602 m MDKB.
26-3-73 - 27-3-73	Otis	Change out BV. Pull plug from sliding sidedoor at 1602 m MDKB. Tag bottom at 1733 m MDKB. Set plug in sliding sidedoor at 1602 m MDKB.

PLAORM: MARLINWELL NO: A-6

DATE D-M-Y	COMPANY	JOB DESCRIPTION - REMARKS
2-5-73 - 4-5-73	Otis	Change out BV. Unsuccessful attempt to pull plug in sliding sidedoor at 1602 m MDKB. Found plug was not seated in sliding sidedoor at 1602 m MDKB. Pulled plug. Set plug in landing nipple at 1623 m MDKB.
1-7-73 - 2-7-73	Otis	Change out BV. Unsuccessful attempt to pull plug in landing nipple at 1623 m MDKB.
4-8-73	Otis	Pulled plug in landing nipple at 1623 m MDKB. Change out BV.
5-12-74	Otis	Tag bottom at 1738 m MDKB.
6-3-75	Otis	Tag bottom at 1740 m MDKB.
3-4-75	Otis	Change out BV. Ran sand bailer.
2-11-75 - 4-11-75	Agnew	Change out BV. Gradient pressure survey Take bottom hole sample.
9-11-75	Agnew	Tag bottom at 1733 m MDKB.
16-10-76	Otis	Tag bottom at 1739 m MDKB.
21-11-77	Otis	Tag bottom at 1739 m MDKB.
14-8-80	Go-International	Unsuccessful gradient pressure survey. Tag bottom at 1976 m MDKB.
17-8-80	Go-International	Gradient pressure survey. Change out BV.



OIL and GAS DIVISION

03 FEB 1983

AQUITAINE

902875 030

PROPERTIES OF COAL

WELL	SAMPLE DEPTH (FT)	VITRINITE (%)	EXINITE (%)	INERTINITE (%)	TOC (%)	CPI	PR/PH	PR/C <sub>17</sub>	PH/C <sub>18</sub>	H.I.
MARLIN A-6 (COAL)	6000-6100	86.6	7.4	4.0	66.8	1.84	4.07	0.70	0.22	161
	6450-6530	-	-	-	64.5	2.32	6.44	1.78	0.32	153
	6900-7000	79.4	10.6	10.0	63.5	2.38	6.20	2.34	0.41	127
	7400-7500	-	-	-	58.3	2.40	7.38	1.69	0.28	146
	8050-8150	84.0	10.2	5.8	63.6	2.02	5.61	1.26	0.26	156
	8600-8700	82.2	6.2	11.6	66.9	1.76	7.42	1.62	0.27	154
	9200-9300	-	-	-	64.6	1.72	5.19	1.39	0.32	163
	9800-9900	86.6	3.6	9.4	78.3	1.50	8.81	2.94	0.35	186
	10470-10550	-	-	-	64.1	1.41	4.0	1.29	0.36	266
	10750-10850	89.2	7.4	2.8	71.4	1.51	4.67	1.30	0.32	226
BARRACOUTA 3 (COAL)	5540-5610	68.0	9.8	20.6	-	-	-	-	-	-
	8590-8780	90.4	8.2	1.0	-	-	-	-	-	-

PLATFORM: MARLIN

WELL NO:

902875 031  
A-6

## OIL and GAS DIVISION

DATE D-M-Y	COMPANY	JOB DESCRIPTION - REMARKS
		18 JAN 1982
27-3-69- 29-3-69	Otis/Schlumberger	Set packer. Perforate, set ball valve (BV).
27-4-69- 4-5-69	Otis/Schlumberger	Tag bottom at 1654 m MDKB. Ran sand bailer. Well worked over. Set packer. Re-perforate. Gradient pressure survey. Change out BV. Tag bottom at 1641 m MDKB. Ran sand bailer.
10-5-69- 12-5-69	Otis	Well worked over and gravel packed. Set packer. Set BV.
22-5-69- 24-5-69	Otis	Gradient pressure survey. Acidize formation.
29-5-69- 1-6-69	Agnew	Change out BV. Test for suspected packer leak. NO leak detected. Tag bottom at 1777 m MDKB. Gradient pressure survey.
15-8-69- 16-8-69	Agnew	Tag bottom at 1750 m MDKB. Gradient pressure survey.
23-1-70	Agnew	Change out BV.
17-1-71	Agnew	Gradient pressure survey.
21-3-72	Otis	Change out BV.
25-5-72	Otis	Change out BV. Ran Eastman survey.
5-1-73	Otis	Change out BV. Set plug in sliding sidedoor at 1602 m MDKB.
26-1-73	Otis	Change out BV. Pulled plug from sliding sidedoor at 1602 m MDKB
2-2-73	Otis	Set plug in sliding sidedoor at 1602 m MDKB.
26-3-73- 27-3-73	Otis	Change out BV. Pull plug from sliding sidedoor at 1602 m MDKB. Tag bottom at 1733 m MDKB. Set plug in sliding sidedoor at 1602 m MDKB.

PLATFORM: MARLINWELL NO: A-6

DATE D-M-Y	COMPANY	JOB DESCRIPTION - REMARKS
2-5-73 - 4-5-73	Otis	Change out BV. Unsuccessful attempt to pull plug in sliding sidedoor at 1602 m MDKB. Found plug was not seated in sliding sidedoor at 1602 m MDKB. Pulled plug. Set plug in landing nipple at 1623 m MDKB.
1-7-73 - 2-7-73	Otis	Change out BV. Unsuccessful attempt to pull plug in landing nipple at 1623 m MDKB.
4-8-73	Otis	Pulled plug in landing nipple at 1623 m MDKB. Change out BV.
5-12-74	Otis	Tag bottom at 1738 m MDKB.
26-3-75	Otis	Tag bottom at 1740 m MDKB.
3-4-75	Otis	Change out BV. Ran sand bailer.
2-11-75 - 4-11-75	Agnew	Change out BV. Gradient pressure survey Take bottom hole sample.
9-11-75	Agnew	Tag bottom at 1733 m MDKB.
16-10-76	Otis	Tag bottom at 1739 m MDKB.
21-11-77	Otis	Tag bottom at 1739 m MDKB.
14-8-80	Go-International	Unsuccessful gradient pressure survey. Tag bottom at 1976 m MDKB.
17-8-80	Go-International	Gradient pressure survey. Change out BV.

ESSO STANDARD OIL (AUSTRALIA) LTD  
SUBSURFACE COMPLETION EQUIPMENT

902875 033

WELL NAME: MARLIN A-6

DATE COMPLETED: MAY 28, 1969

Schematic	Equipment Description	Length	Depth
	K.B. to 'HBA' Hanger	26.87	
	CIW 'HBA' Hanger & 'RFG' Packoff	1.13	28.00
	13 JTS Tubing 4 1/2" Butt 12.6# J-55 W/	398.46	426.46
	1/8" ID Hydraulic Line Strapped		
	externally: O.D. 4 1/2" CPLG - 5.2"		
	OD. 1/8" CPLG - 0.625"		
	Flow Coupling - 4 1/2" Butt THD, Otis 4140	4.65	431.11
	O.D. = 5.620"		
	Weldment - 4 1/2" Otis 'X' Nipple W/Butt	1.95	433.06
	THD & 'XOE' Safety Valve W/1/8"		
	Side Outlet for Control Line. O.D. =		
	5.620". I.D. of Nipple - 4.082"		
	Flow Coupling - 4 1/2" Butt THD, Otis 4140	4.65	437.71
	O.D. = 5.620"		
	X-Over 4 1/2" Butt THD Box x 7" LT & C Pin	2.77	440.48
	126 JTS Tubing 7" 23# J-55 LT & C	4777.78	5218.26
	X-Over 4 1/2" Butt THD Box x 7" LT & C Pin	3.52	5221.78
	W/7" LT & C Coupling		
	1 JT Tubing 4 1/2" Butt 12.6# J-55	30.88	5252.66
	Sliding Sleeve, 4 1/2" Otis 'XD' W/Butt	4.58	5257.24
	THDS.		
	1 JT Tubing 4 1/2" Butt 12.6# J-55	31.29	5288.53
	Packer, Otis Permatrievue 9-5/8" x	6.23	5294.76
	4 1/2" Butt W/'J' Latch Seal Unit		
	and W/Butt Adaptor Kit.		
ID = 3.875" in PKR, 4" in Seal			
1 JT Tubing 4 1/2" Butt 12.6# J-55	27.97	5322.73	
Landing Nipple, 4 1/2" Otis Type 'N' W/	1.32	5324.05	
Butt THD W/3.710" no go.			
5402'			
5432'			
5842'			
JUNK & SAND			
6041' - BAKER 'K' CMT RET.			
6045'			
JUNK			
6446'			
CMT			
6746'			
CMT - 9150'			
9450'			
CMT - 9750'			
10,250'			
CMT - 10,600'			
10,880'			
JUNK			
10 5/8" @ 10,846'			
TD - 11,068'			

MARLIN WELLS  
1977 DEPTH MEASUREMENTS

902875 034

WELL	DEPTH (FEET MDKB)			CHANGE IN DEPTH
	PREVIOUS SURVEY* (OCTOBER 1976)	AFTER BAILING (MARCH 1977)	LATEST SURVEY (NOVEMBER 1977)	
A-1	5172	-	5175	+ 3
A-2	5329	-	5329	0
A-3	5699	-	5696	- 3
A-4	5755	-	5757	+ 2
A-5	6353	-	6354	+ 1
A-6	5707	-	5707	0
A-8	7126	-	7126	0
A-9	5113	-	5113	0
A-11	6524	6539	6537	- 2**
A-12	6371	-	6370	- 1
A-13	6719	-	6718	- 1
A-15	6369	-	6369	0
A-16	6211	-	6213	+ 2
A-18	6247	-	6246	- 1
A-22	6567	6581	6567	-14**
A-23	5136	-	5138	+ 2
A-24	5805	5812	5806	- 6**

\* Reported to Department of Minerals and Energy in a letter dated October 26, 1976 (TD: 2060).

\*\* Change in depth since bailing.

M.A. SHIRBIN,  
13-2-1978