W788

ATTACHMENT 1

VIC-P17

GIPPSLAND BASIN

OMEO NO. 1

FINAL TECHNICAL REPORT

(DRILLING)

ATTACHMENT 1
TO WCR
OMEO-1
(W788)

GIPPSLAND BASIN

VIC-P17

OMEO NO. 1

FINAL TECHNICAL REPORT

(DRILLING)

F3a Bis 2-78 — WELL DATA — WELL: OMEO 1

1) WELL NAME : OMEO NO. 1

2) IDENT. : OMEO NO. 1

3) GEOGRAPHICAL AREA : AUSTRALIA BASS STRAIT

4) GEOLOGICAL BASIN : GIPPSLAND

5) FIELD : VIC-P17

6) BLOCK : VIC-P17

7) PERMIT HOLDERS :
VIC-P17
AUSTRALIAN (AAP)
AQUITAINE
PETROLEUM

8) PARTNERS :

Name	%	Name	%
AUSTRALIAN OCCIDENTAL PET.	25	AUST. AQUITAINE PET P/L	25
ALLIANCE RESOURCES PTY LTD	25	CONSOLIDATED PET. (CLUFF	
AGEX PTY LTD	12.5	HARTOGEN)	12.5

9) OPERATOR : AUSTRALIAN AQUITAINE PETROLEUM PTY. LTD

11) REFERENCE WELLS :

Name	
BREAM NO. 3	EDINA NO. 1
BULLSEYE NO. 1	

10) INITIAL STATUS

- Exploration [X]
- Development [X]
- Othet [X]

12) LOCATION COORDINATES

site: Land [ ] Offshore [ ] Swamp [ ] Other [ ]

geographical coordinates: Latitude 38°36'45.01" S; Longitude 147°43'02.24" E

reference meridian: Paris [ ] Greenwich [ ]

LAMBERT coordinates: X(m) Y(m) Z(m)

SITE	LAND	OFFSHORE		SWAMP		OTHER	
Distance RKB/ REF.		92.66m	30m				
Reference	GROUND	MUD LINE	ZERO HYDRO				

13) DRILLING OBJECTIVES

Objective n°	Formation	Formation tops vertical depth	Departure	Direction
1	INTRA-LATROBE	± 2670		
2	EARLY CRETACEOUS STRZELECKI GROUP	± 3630 (NOTE: STRATIGRAPHIC & LITHOLOGICAL)		

14) WELL COURSE

Vertical [X] Deviated [X] DUE TO SIDETRACK

Normal [ ] Scourse [ ]

15) WAS THE OBJECTIVE REACHED ?

	yes	no	Formation tops vertical depth	Departure	Direction
OBJECTIVE 1	[X]	[ ]			
OBJECTIVE 2	[X]	[ ]			
OBJECTIVE 3	[ ]	[ ]			
OBJECTIVE 4	[ ]	[ ]			

16) RESULTS

- [ ] Oil production
- [ ] Gas production
- [ ] Water production
- [X] Shows but no reservoir
- [ ] Injection well
- [ ] Dry well
- [ ] Temporarily plugged
- [X] Plugged and abandonned
- [ ] Completed

17) DATES (·)

BEGINNING		END	
Well	1.11.82	Drilling	25.1.83
Drilling :	2.11.82	Well	10.2.83

18) WELL END (··)

Total depth : 3379m — Vertical depth : 3379m

Drilled footage : 3288m — Lost footage : —

Total departure : — — Direction : —

TOTAL DURATION — Drilling : 86 days — Well : 101 days

19) COSTS — CURRENCY UNIT: AUSTRALIAN $

Before drilling	277,121	"
During drilling	19,265,185	"
After drilling	--	"
Total well	19,542,306	"

Imp. 4996 SNEA(P) RGM 959.004.011

F3a' Bis 2-78	LOGISTICS	WELL: OMEO 1

Area management : AUSTRALIAN AQUITAINE PETROLEUM PTY. LTD.
99 MOUNT STREET, NORTH SYDNEY, NSW 2060
Located : P.O. BOX 725

Land Base : AQUITAINE WELSHPOOL SHORE BASE
MIDLAND HIGHWAY,
Located : WELSHPOOL, VIC, 3966
P.O. BOX 27

• SERVICE COMPANIES

- Mud	BAROID	- Under water T.V.	ODECO
- Mud logging	GEO SERVICES	- Testing	HALLIBURTON
- Production tests	FLOPETROL	- Well head	CAMERON
- Fishing	TRI-STATE	- Depollution	AAP
- Positioning	DECCA SURVEY	- Air transportation	COMMERCIAL AVIATION
- Electrical logging	SCHLUMBERGER	- Sea transportation	AOS
- Meteo	OCEANROUTES		"LADY JANE"
- Diving	OCEANEERING		"SEA SAPPHIRE"
- H.P. Pumping	DOWELL SCHLUMBERGER		STANDBY -
- Bulking	BAROID		LOMBARDO MARINE
			"CHRISTMAS CREEK"

Beginning of well = **first moving in date (if this date is known)**
Beginning of drilling = **spudding date**
End of drilling = **date of last bit pulling out or end of electrical logging operations, or pressure surge at the end of production casing cementing operation**
End of well = **end of well plugging operations laying down included or end of completion**

** - Depths ot be calculated from the rotary table
- Drilled footage: distance RKB/ground (or mud line) not included, but side tracks resulting from fishing included
- Lost footage resulting from fishing or course modification without chanaing the geological objective. Should the geological objective vary, well name or number will change, and the previous well drilled footage is not considered as a lost footage
- Except change in geological objective requiring a side track, the formula is: Drilled footage - Lost footage = Total depth - Distance RKB/ground

• AREA • LAND ☐ SEA ☒ SWAMP ☐ LAKE ☐

ALTITUDE : SEA LEVEL WATER DEPTH : 62.66m

DISTANCE FROM BASE : 105 km DISTANCE FROM SHORE : 51.5 km

• RELIEF Flat ☒ Slightly undulate ☐ Undulate ☐ Very undulate ☐

• SEA CONDITIONS Calm ☐ Medium ☐ Strong ☒ Very strong ☐

• POLLUTION RISK Low ☐ Medium ☒ High ☐ Very high ☐

• WEATHER Equatorial ☐ Hot ☐ Temperate ☐ Cold ☒ Arctic ☐

• POPULATION DENSITY Nil ☒ Low ☐ Medium ☐ High ☐ Very high ☐

MEANS USED

• NAME OF THE RIG (LAND) : _____

• SUPPORT •

• TYPE Land ☐ Artificial island ☐ Jack-up ☐ Drillship ☐ Semi-submersible ☒

Swamp barge ☐ Non assisted Platform ☐ Assisted platform ☐ Tender ☐ Other ☐

• SEA SUPPORT NAME : OCEAN DIGGER

• PROPULSION: Towed ☒ Self propelled ☐ Power : _____ Speed : _____

• POSITIONING

Mooring: Classical ☒ Dynamic ☐ Head : 262 DEG

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• DRILLING EQUIPMENT •

DRAWORK MANUFACTURER EMSCO MODEL A1500 E CONTRACTOR : ODECO

• RANGE • Light ☐ Medium ☐ Heavy ☒ Super Heavy ☐ Extra Heavy ☐

• TRANSMISSION • Mechanical ☐ Electric ☒ Hydraulic ☐

• MAIN PUMPS • Number ☒ 2 EMSCO D-1350 HP Total hydraulic power ☐

• RIG DESIGN • Normal design ☒ Compact ☐ Portable ☐ Helirig ☐

Flexorig ☐ Automatic racking ☐ Winterised ☐ ☐

• SURFACE OR SUBSEA EQUIPMENT

B.O.P. STACK	Diameter	API WP
Number 1	18 3/4" CAMERON "U"	10,000 PSI
Number 2	18 3/4" HYDRIL	5,000 PSI
Number 3		

WELL HEAD	Manufacturer	Type	Diameter	API WP
Number 1	CAMERON	TORQUE SET	18 3/4"	10,000 PSI
Number 2				
Number 3				

MUD LINE SUSPENSION: ☐ yes ☒ no Manufacturer :

RISER

Number 1		Number 2	
Diameter :	50' x 22" OD x 0.50" WALL	Diameter :	
Connector :	VETCO MR-4B	Connector :	
Buoyancy system :	no ☒ yes ☐	Buoyancy system	no ☐ yes ☐

• OPEN HOLE SECTIONS •		• CASINGS •				
DIAMETER	TOTAL DEPTH	DIAMETER	COMPOSITE STRING DIAMETERS	SHOE DEPTH	HANGER DEPTH	TOP CEMENT IN ANNULUS
26"	220m	20" 133 lbs/ft		210m	30m	SEABED
17½"	1320m	13 3/8" 68 lbs K55		1310m	89.90m	825m (TEMP LOG)
12¼"	TD - 2985 PBTD - 2674 (12¼" SIDETRACK ABROTED)	9 5/8" 68 lbs N80		2606m	91.00m	2179m (TEMP LOG)
8½"	2985m PBTD - 2674 (12¼" HOLE PLUGGED 2674 to 2985m)	7" 26 lbs N80		2984m	2498.5m	2498.5m
6"	3389m					

[redacted] Bis 2-781 [redacted]

Interval	Total footage in the interval	DRILLING			CORING			TURBODRILLING			SIMULTANEOUS PILOT DRILLING AND HOLE OPENING			HOLE OPENING		RE-DRILLING AND/OR REAMING		Abandonned footage in the interval	Drilling fluid
		Ø	m or ft	h	Ø	m or ft	h	Ø	m or ft	h	Ø	m or ft	h	m or ft	h	m or ft	h		
26"	127	26"	127	5															SEA WATER W/HI VIS PILLS
17½"	1100	17½"	1100	74												7	.5		GEL SW 1.14SG 42 VIS 14.5WL
12¼"	1665	12¼"	1647	255	8½"	18	3							18	3	972	15.5	311	GEL SW 1.14SG 42 VIS 14.5WL
8½"	311	8½	243	76.5				8½"	68	20						125	3	1	GEL POL 1.28SG
6"	394	6"	388		6	8	3									68	3	--	GEL POLYMER 1.28SG 70 VIS

F3d Bis 2-78

CORE DATA SUMMARY

WELL : OMEO 1

Core Number	DEPTH Ft or m. from	DEPTH Ft or m. to	Recovered	Formation	Core Number	DEPTH Ft or m. from	DEPTH Ft or m. to	Recovered	Formation
1	2348	2366	80	QUARTZ - SANDSTONE					
2	3032	3043	31	SHALE-SANDSTONE SOME QUARTZ					

CLABS

Run N°	DEPTH ft or m. from	DEPTH ft or m. to	Number of samples	Formation	Run N°	DEPTH ft or m. from	DEPTH ft or m. to	Number of samples	Formation
1,2,3	MISRUN	IN 6" HOLE SECTION RECOVERY FROM BELOW DEPTHS ON RUN NO. 3 - 3 SHOTS							
3	3376		1	SANDSTONE					
3	3365		1	SANDSTONE					
3	3361		1	SANDSTONE MORE SHALY					

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F3d' Bis 2-78

FORMATION TEST SUMMARY

WELL : OMEO 1
PAGE 1 OF F3D

Test N°	Date	Type of test *	Tested interval		Succeful		Reason of failure (**)	Observations
			from ft or m.	to ft or m.	Yes	No		
1	4.12.82	RFT	2849.8m		X			
2	5.12.82	RFT	2959.5m		X			
3	5.12.82	RFT	2936.5m			X	XX	RFT STUCK IN HOLE AT 2936.5m -WIRELINE BROKEN 6.5m ABOVE WEAK POINT.
4	31.1.83	RFT	3077	3125m			XX	RFT STUCK IN HOLE WHILE TAKING SAMPLE AT 3125

* TOHP - Test open hole full diameter
TOHR - Test open hole - rat hole
STOHP - Straddle test open hole full diameter
STOHR - Straddle test open hole rat hole
TCSG - Test casing
STCSG - Straddle test casing
FIT - Formation interval tester

** FP - Packer leak
BO - Tool plugged
NO - Test not opened
IN - Test interrupted
XX - Other (to be specified)

ELECTRICAL LOGGING SUMMARY

Interval	Date	Nature and Run N°	DEPTH ft or m.		Scales		
			from	to	1 20	1/200	1/500
17½"	9.11.82	+ 1 = ISF/SLS/GR	1319	210		X	X
17½"	9.11.82	+ 2 = LDL/GR/CAL	1319	210		X	X
17½-13 3/8	11.11.82	+ 1 TEMP. LOG (TOP CMT = 825m)	500	1270		X	X
12¼	3.12.82	+ 1 DLL/MSFL/GR/SP/CAL	1310	2983		X	X
12¼	3.12.82	+ 2 CNL/GR/CAL	1310	2983		X	X
12¼	3.12.82	+ 3 SONIC BHC/GR	1310	2983		X	X
6	19.1.83	+ 1 DLL/MSFL/SONIC/GR	2984	3172		X	X
6	19.1.83	+ 1 LDL/CNL/GR	2984	3172		X	X
6	19.1.83	+ 1 CBL/VDL	2498	2984		X	X
6	19.1.83	+ 1 VELOCITY SURVEY SSP-VSP	SURFACE	3172			

F3d' Bis 2-78

FORMATION TEST SUMMARY

WELL : OMEO 1

Test N°	Date	Type of test *	Tested interval		Succeful		Reason of failure (**)	Observations
			from ft or m.	to ft or m.	Yes	No		
1	31.1.83	RFT	3125		X			RUN IN 6" HOLE WITH 2 x 2 3/4 GALLONS CHAMBERS
2	5.2.83	TCSG	2918	2925	X			
"	"	"	2932	2939	X			

* TOHP - Test open hole full diameter
TOHR - Test open hole - rat hole
STOHP - Straddle test open hole full diameter
STOHR - Straddle test open hole rat hole
TCSG - Test casing
STCSG - Straddle test casing
FIT - Formation interval tester

** FP - Packer leak
BO - Tool plugged
NO - Test not opened
IN - Test interrupted
XX - Other (to be specified)

ELECTRICAL LOGGING SUMMARY

Interval	Date	Nature and Run N°	DEPTH ft or m.		Scales		
			from	to	1/20	1/200	1/500
6"	29.1.83	+ 1 - BHC/GR	2987	3378		X	X
6"	29.1.83	+ 2 DCL/MSFL	2987	3380		X	X
6"	29.1.83	+ 3 LDL/CNL/GR	2987	3378		X	X
6"	30.1.83	+ 4 HDT	2985	3379			X

F3e Bis 2-78 | TIME DISTRIBUTION | WELL : OMEO 1

		• ITEMS •	INTERVALS : Duration in hours									Duration by total duration
			D	26"	17½"	12¼"	8½"	6"	C	D		
MOVING	D1	Rigging up, transportation and tearing down	23							20.5		1.8% 43.5%
	D2	Waiting on weather										
	D3	Waiting : other										
DRILLING - CASING	F1	New hole drilling		5	74	256	82.5	179.5				24.8% 597
	F2	Drilling trips		4	5	45	37.5	91.5				7.6% 183
	F3	Miscellaneous drilling operations		2.5	15	30.5	63.5	50.5				6.7% 162
	F4	Casing and cementing		37.5	59.5		95.5					8% 192.5
FORMATION SURVEYS	G1	Coring				3		3				0.2% 6
	G2	Coring trips and miscellaneous				39		12.5				2.1% 51.5
	G3	Testing and related operations				3						0.1% 3
	G4	Electrical logging			20.5	61.5	17	172				11.2% 271
INTERRUPTIONS OF OPERATIONS UNDER F & G	A1	Sticking - Fishing				462.5	75.5	36.5				23.8% 574.5
	A2	Losses and well flowing mud treatment										
	A3	Waiting on weather										
	A4	Waiting : other				104.5	22	10				5.7% 136.5
COMPLETION AND PLUGGING	C1	Completion - Formation treatment and Production tests							114			4.7% 114
	C2	Abandon							70			2.9% 70
	C3	Waiting on weather							1.5			.06% 1.5
	C4	Waiting : other							3.5			0.1% 3.5
DURATION BY INTERVAL →			23	49	174	1005	393.5	555.5	189	20.5		2409.5 100%
			1%		7.2%	41.7%	16.3%	23.1%	7.8%	.8%		100%

OPERATIONS IN PROGRESS	DURATION \ REASONS	STICKING FISHING		LOSSES, FLOWING MUD TREATMENT		WAITING ON WEATHER		WAITING : OTHER	
		Number	Duration (h)	Number	Duration (h)	Number	Duration (h)	Number	Duration (h)
Moving (D2-D3)	Less than 24 h								
	From 1 to 5 days								
	More than 5 days								
	TOTAL →								
Drilling, casing formation surveys (A1-A2-A3-A4)	Less than 24 h							2	22
	From 1 to 5 days	2	112					4	104.5
	More than 5 days	1	462.5						
	TOTAL →	3	574.5					6	126
Completion (C3-C4)	Less than 24 h					1	1.5	1	3.5
	From 1 to 5 days								
	More than 5 days								
	TOTAL →					1	1.5	1	3.5
TOTAL →		3	574.5			1	1.5	7	130

TOTAL DURATION OF INTERRUPTIONS

During moving	0
During drilling • Casing or formation surveys	274.5
During completion and plugging	5.0
TOTAL IN HOURS →	597.5
TOTAL IN DAYS →	24.15

F3f Bis 2-78

MUD SUMMARY BY INTERVAL

WELL : OMEO 1

INTERVAL : 26" From : 91m to : 220m

Mud type used in this interval : SEAWATER/LIME FLOCCULATED GEL SLUGS

• USEFUL DATA •

CASINGS

- Diameter : 20"
- Hanger : 90m
- Shoe : 210m
- Casing 133 X56
- Lenght : 120

BALANCE OF VOLUMES bbl on m3

- Initial volume : -- 3
- Added volume : 255m3
- Jetted volume : 255m3
- Losses in formation : 0
- Final volume : 0

DRILLING

Drilled (m or ft) from : 91 to : 220 duration (date) from: 2.11.82 to : 3.11.82

Footage (m or ft) : 129m in : 2 DAYS

Average dllg rate 25.8 m/hr drilling hours : 5 HRS

Internal casing vol. : losses :

Pumping rate : 120 spm - 3950 L/min

• MUD CHARACTERISTICS •

	mini	maxi	average
Weight in flow	1.02	1.50	
Weight out flow			
Viscosity M.V.			
Viscosity A.V.			
Viscosity P.V.			
Viscosity Y.P.			
Gels 0'			
Gels 10'			
API WL API			
API WL HP-HT			
API WL Pressure			
API WL T°			
Ph			
Pf			
Pm			
Ca++ (g/l)			
SO4Ca			
Clna			
CaCl2			
% water			
% oil			
oil/water ratio			
% solids			
Solids density			
% Sand			
T °C			

• CONSUMPTIONS •

CHEMICALS	QUANTITY Total m3 or T	Kg ft or m drilled	Kg/m3	COST Unit Price	Total Cost	%
BENTONITE	11.226T	87.0	44.0	14.00	3458.00	36
CAUSTIC	0.490T	3.8	1.92	74.70	597.60	6.2
SODA ASH	0.440T	3.4	1.73	13.88	152.68	1.6
LIME	0.600T	4.6	2.35	6.75	162.00	1.7
BARITE	29.542T	229.0	115.85	8.00	5200.00	54.5

BARITE USED WAS TO MIX 32M3 OR 1.50 SG MUD TO DISPLACE CEMENT FROM CASING.

AN ADDITIONAL 390 SX OF BARITE WERE USED TO WEIGHT DOWN BASE PLATE PRIOR TO SPUDDING THIS COST OF $3120.00 HAS NOT BEEN ADDED IN DAILY REPORT COSTS. 22 SX OF CALCIUM CHLORIDE AT COST OF $252.12 USED IN CEMENT HAS NOT BEEN INCLUDED EITHER.

TOTAL	42.298				9570.28	

Depth (ft)	Lithology
91 - 220	SURFACE SANDS, SILT, CLAY

Total cost of { Interval : A$9570.28 / Drilled meter A$74.19

Currency : AUSTRALIAN DOLLARS

Conversion rate used :

F3f Bis 2-78 | **MUD SUMMARY BY INTERVAL** | **WELL :** OMEO 1

INTERVAL : 17½" From : 220m to : 1320m

Mud type used in this interval : SEAWATER/Q.MIX (PREHYDRATED GEL)

• USEFUL DATA •

CASINGS

- Diameter : 13 3/8"
- Hanger : 91.3m
- Shoe : 1310m
- Casing : 68 K55
- Lenght : 1218.7m

BALANCE OF VOLUMES (bbl on m3)

- Initial volume : 42m3
- Added volume : 786.8m3
- Jetted volume : 820.0m3
- Losses in formation : 8.8
- Final volume : 0

DRILLING

Drilled (m or ft) {from : 220 / to : 1320m} duration (date) {from : 4.11.82 / to : 11.11.82}

Footage (m or ft) : 1100m in : 8 DAYS

Average dllg rate 14.86 drilling hours : 74

Internal casing vol. : losses :

Pumping rate : 100 spm 3260 L/min

• MUD CHARACTERISTICS •

	mini	maxi	average
Weight in flow	1.09	1.16	1.15
Weight out flow	1.10	1.16	1.16
Viscosity M.V.	35	48	40
Viscosity A.V.	--	--	--
Viscosity P.V.	5	8	6
Viscosity Y.P.	8	24	20
Gels 0'	6	22	18
Gels 10'	8	35	25
API WL API	14.6	33	15
API WL HP-HT	--	--	--
API WL Pressure	--	--	--
API WL T°	--	--	--
Ph	9.0	10	9.5
Pf	0.5	0.4	0.25
Pm	0.1	0.8	0.5
Ca^{++} (g l)	250	600	300
SO4Ca	--	--	--
Clna	18000	19500	18500
CaCl2	--	--	--
% water	94	96	95
% oil	0	0	0
oil/water ratio	--	--	--
% solids	4	6	5
Solids density	--	--	--
% Sand	TR	1	TR
T °C	--	--	--

• CONSUMPTIONS •

CHEMICALS	QUANTITY Total m3 or T	Kg ft or m drilled	Kg/m3	COST Unit Price	Total Cost	%
BENTONITE	26.633T	24.20	33.85	14.00	8204.00	41.2
CAUSTIC	1.660T	1.50	2.11	74.70 53.36	1771.46	8.7
SODA ASH	3.080T	2.80	3.91	13.88 17.35	1068.76	5.0
CMC (HV)	0.750T	0.68	0.95	48.68	1460.40	7.0
Q.BROXIN	0.850T	0.77	1.08	29.50	1003.00	4.8
DEXTRID	1.543T	1.40	1.96	51.60	3508.80	17.0
PAC-R	0.200T	0.18	0.25	106.06	848.48	4.0
CONDET	410L	0.37	0.52	258.00	516	2.5
BARITE	11362	10.33	14.44	8.00	2000	9.8
TOTAL	46,488				20,380.90	100

Depth (ft)	Lithology
220	CLAY/ SAND
1320	CLAYSTONE

Total cost of { Interval : A$ 20,380.90 / Drilled meter foot A$ 18.53 }

Currency : AUSTRALIAN DOLLARS

Conversion rate used :

F3f Bis 2-78

MUD SUMMARY BY INTERVAL

WELL : OMEO 1

INTERVAL : 12¼" From : 1320m to : 2985m

Mud type used in this interval : SEA WATER POLYMER

• USEFUL DATA •

CASINGS

- Diameter : 13 3/8
- Hanger : --
- Shoe : 1310m
- Casing : 21" RISER
- Lenght : 91m

BALANCE OF VOLUMES bbl on m3

- Initial volume : 222
- Added volume : 2130
- Jetted volume : 2075
- Losses in formation : --
- Final volume : 277

DRILLING

Drilled (m or ft) {from : ____ to : ____ duration (date) {from: ____ to : ____

Footage (m or ft) : 1655 in : ____

Average dllg rate 8.4m/hr drilling hours : 198.4

Internal casing vol. : 144m³ losses : ____

Pumping rate : 66 spm (2.17 m³/min)

• MUD CHARACTERISTICS •

	mini	maxi	average
Weight in flow	1.04	1.22	1.15
Weight out flow	1.05	1.33	1.15
Viscosity M.V.	40	65	50
Viscosity A.V.	19	50	38
Viscosity P.V.	12	30	25
Viscosity Y.P.	14	40	25
Gels 0'	3	6	5
Gels 10'	5	24	18
API WL API	3.4	6.8	4.0
API WL HP-HT	--	--	--
API WL Pressure	--	--	--
API WL T°	--	--	--
Ph	9.0	11.5	9.5
Pf	0.1	0.8	0.15
Pm	--	--	--
Ca^{++} (g l)	20	500	200
SO4Ca	--	--	--
Clna	19,000	25,000	23,000
CaCl2	--	--	--
% water	87	96	92
% oil	--	--	--
oil/water ratio	--	--	--
% solids	4	13	8
Solids density	--	--	--
% Sand	0.1	1.0	0.3
T °C	28	59	50

• CONSUMPTIONS •

CHEMICALS	QUANTITY Total m³ or T	QUANTITY Kg/ft or m drilled	QUANTITY Kg/m³	COST Unit Price	COST Total Cost	%
PAC-R	10.3T	6.2	4.96	106.06	43,696.72	22.7
DEXTRID	29.6T	17.8	14.27	51.60	67,338.00	35.0
STARLOSE	5.1T	3.1	2.45	48.00	10,752.00	5.6
CAUSTIC	8.8T	5.3	4.23	74.70	9,358.94	4.9
SODA ASH	4.0T	2.4	1.93	13.88	1,388.00	0.7
BICARBONATE	2.2T	1.3	1.06	16.98	933.90	0.5
SODIUM NITRATE	3.5T	2.1	1.69	30.62	2,143.40	1.1
SURFLO W300	0.208m³	--	--	500.25	500.25	0.26
CONDET	0.83m³	--	--	258.00	1,032.00	0.54
Q.BROXIN	0.43T	0.26	0.2	29.50	501.50	0.26
AQUAGEL	2.72T	1.63	1.3	14.00	840.00	0.44
BARITE	189.6T	113.9	91.4	8.00	33,440.00	17.4
TOTAL	257.24T				192,570.21	

Depth (ft)	Lithology
TO 2250	CLYST
TO 2330	SHALE
TO 2700	SST & CLYST
TO 2985	SST W/OCC SHALE

Total cost of {Interval : A$ 192,570.21 Drilled meter/foot A$ 115.66

Currency : ____

Conversion rate used : ____

F3f Bis 2-78

MUD SUMMARY BY INTERVAL

WELL : OMEO 1

INTERVAL : 8½" HOLE From : 2674m to : 2985m

Mud type used in this interval : SEAWATER - GEL - POLYMER

• USEFUL DATA •

CASINGS

- Diameter : 9 5/8"
- Hanger :
- Shoe : 2606m
- Casing
- Lenght : 2515m

BALANCE OF VOLUMES (bbl or m3)

- Initial volume : 277m3
- Added volume : 263.3m3
- Jetted volume : 393.3m3
- Losses in formation : --
- Final volume : 147m3

DRILLING

Drilled (m or ft) { from : 2674 / to : 2985 } duration (date) { from : 23 DEC 82 / to : 3 JAN 83 }

Footage (m or ft) : 311m in : 12 DAYS

Average dllg rate 3.7 m/hr drilling hours : 84.5

Internal casing vol. : 110m3 losses : --

Pumping rate : 1.22m3/hr

• MUD CHARACTERISTICS •

	mini	maxi	average
Weight in flow	1.19	1.20	1.19
Weight out flow	1.19	1.20	1.19
Viscosity M.V.	46	75	60
Viscosity A.V.	34	40	39
Viscosity P.V.	22	33	28
Viscosity Y.P.	13	26	20
Gels 0'	4	12	7
Gels 10'	13	35	24
API WL API	5.2	6.4	5.6
API WL HP-HT	--	--	--
API WL Pressure	--	--	--
API WL T°	--	--	--
Ph	9.0	11.5	10.5
Pf	0.1	0.7	0.4
Pm	--	--	--
Ca^{++} (g l)	80	800	200
SO4Ca	--	--	--
Clna	11,000	20,000	13,000
CaCl2	--	--	--
% water	91	91	91
% oil	--	--	--
oil/water ratio	--	--	--
% solids	9	9	9
Solids density	--	--	--
% Sand	0.2	1.0	0.25
T °C	40	52	50

Depth (ft)	Lithology
TO 2985m	SANDSTONE W/SHALE

• CONSUMPTIONS •

CHEMICALS	QUANTITY Total m3 or T	Kg/ft or m drilled	Kg/m3	COST Unit Price	Total Cost	%
AQUAGEL	16.46T	53	62.6	14.00	5082.00	19.1
CAUSTIC SODA	0.21T	0.7	0.8	74.70	224.10	0.8
SODA ASH	0.64T	2.1	2.4	13.88	222.08	0.8
SODIUM BICARBONATE	0.64T	2.1	2.4	16.98	271.68	1.0
SODIUM NITRATE	0.45T	1.4	1.7	30.62	275.58	1.0
Q.BROXIN	1.20T	3.9	4.6	29.50	1416.00	5.3
SOLTEX	1.11T	3.6	4.2	78.50	3846.50	14.5
STARLOSE	0.95T	3.1	3.6	48.00	2016.00	7.6
CMC HV	1.30T	4.2	4.9	48.68	2531.36	9.5
LIME	0.10T	0.3	0.4	6.75	27.00	0.1
PAC-R	0.05T	0.2	0.2	106.06	212.12	0.8
ALUMINIUM STEARATE	0.04T	0.1	0.1	42.61	127.83	0.5
BARITE	58.51T	188.1	222.2	8.00	10,302.00	39
TOTAL	81.67T				26,572.25	

Total cost of { Interval : A$ 26,572.25 / Drilled meter foot A$ 85.44/METRE }

Currency :

Conversion rate used :

F3f Bis 2-78 | **MUD SUMMARY BY INTERVAL** | **WELL :** OMEO 1

INTERVAL : 6" HOLE From : 2985m to : 3379m

Mud type used in this interval : SEAWATER - GEL - POLYMER

• USEFUL DATA •

CASINGS

- Diameter : 7"
- Hanger : 2506m
- Shoe : 2984m
- Casing : 26+/ft
- Lenght : 478m

BALANCE OF VOLUMES (bbl on m3)

- Initial volume : 147m3
- Added volume : 420m3
- Jetted volume : 323m3
- Losses in formation : 17m3
- Final volume : 227m3

DRILLING

Drilled (m or ft) {from : 2985m / to : 3379m} duration (date) {from : 9.1.83 / to : 25.1.83}

Footage (m or ft) : 394m in : 16 DAYS

Average dllg rate 2.2 m/hr drilling hours : 161.2

Internal casing vol. : -- losses : --

Pumping rate : 0.73 m3/min

• MUD CHARACTERISTICS •

	mini	maxi	average
Weight in flow	1.09	1.28	1.11
Weight out flow	1.10	1.29	1.12
Viscosity M.V.	42	59	48
Viscosity A.V.	21.5	35.5	28.5
Viscosity P.V.	14	26	20
Viscosity Y.P.	14	20	16
Gels 0'	3	7	4
Gels 10'	13	20	16
API WL API	4.6	5.5	5.0
API WL HP-HT	--	--	--
API WL Pressure	--	--	--
API WL T°	--	--	--
Ph	8.5	11	9.5
Pf	0.05	0.3	0.2
Pm	0.1	0.2	0.1
Ca++ (g l)	80	280	240
SO4Ca	--	--	--
Clna	13,000	20,000	17,000
CaCl2	--	--	--
% water	89	95	92
% oil	0	TR	0
oil/water ratio	--	--	--
% solids	--	--	--
Solids density	--	--	--
% Sand	TR	0.4	0.2
T °C			

Depth (ft)	Lithology
2990	CLYST/SNDST
3100	SANDSTONE
3200	SAND/SILTST
3379	SHALE/SNDST

• CONSUMPTIONS •

CHEMICALS	QUANTITY Total m3 or T	Kg/ft or m drilled	Kg/m3	COST Unit Price	Total Cost	%
BARITE	124.987T	317.23	297.6	8.00	22,000.00	36.2
AQUAGEL	17.988T	45.68	42.85	14.00	5,544.00	9.1
CAUSTIC	1.260T	3.19	3.0	74.70	1,344.60	2.2
SODA ASH	1.280T	3.25	3.05	13.88	444.16	0.7
Q.BROXIN	1.000T	2.54	2.38	29.50	1,180.00	1.9
CMC HV	2.125T	5.39	5.06	48.68	4,137.80	6.8
PAC-R	1.000T	2.54	2.38	106.06	4,242.40	7.0
SOLTEX	4.608T	11.69	10.97	78.50	15,935.50	26.2
BICARB	1.240T	3.15	2.95	16.98	526.38	0.9
STARLOSE	2.247T	5.70	5.35	48.00	4,752.00	7.8
ALSTEARATE	0.062T	0.16	0.15	42.61	213.05	0.4
SOD.NITRATE	0.150T	0.38	0.36	30.62	91.86	0.2
TOTAL	157.932T				60,411.75	

Total cost of {Interval : A$ 60,411.75 / Drilled meter A$ 153.38/metre / foot}

Currency : AUSTRALIAN DOLLARS

Conversion rate used :

F3f Bis 2-78 | **MUD SUMMARY BY INTERVAL** | **WELL :** OMEO 1

INTERVAL : FORMATION/DST TEST From : 2939m to : 2918m

Mud type used in this interval : SEAWATER - GEL - POLYMER

• USEFUL DATA •

CASINGS

- Diameter : 7"
- Hanger : 2506m
- Shoe : 2984m
- Casing : 26 +/ft
- Lenght : 478m

PLUGGED AT: 2951m

BALANCE OF VOLUMES (bbl on m3)

- Initial volume : 227m3
- Added volume : 136m3
- Jetted volume : 363m3
- Losses in formation : 0
- Final volume : 0

~~DRILLING~~

TESTED (m ~~or ft~~) from : 2939 to : 2978 duration (date) from : 2.2.83 to : 6.2.83

Footage (m or ft) : -- in : 4 DAYS

Average dllg rate : -- drilling hours : --

Internal casing vol. : 111m3 losses :

Pumping rate :

• MUD CHARACTERISTICS •

	mini	maxi	average
Weight in flow	1.10	1.11	1.10
Weight out flow	1.10	1.11	1.10
Viscosity M.V.	32	41	39
Viscosity A.V.	12.5	15	15
Viscosity P.V.	10	10	10
Viscosity Y.P.	5	10	7.5
Gels 0'	1	3	2
Gels 10'	2	8	5
API WL API	6.3	15	6.5
API WL HP-HT	--	--	--
API WL Pressure	--	--	--
API WL T°	--	--	--
Ph	8.5	9.5	9.0
Pf	0.1	0.2	0.1
Pm	0.1	0.1	0.1
Ca^{++} (g l)	200	400	300
SO4Ca	--	--	--
Clna	17000	20000	18000
CaCl2	--	--	--
% water	97	97	97
% oil	--	TR	TR
oil/water ratio	--	--	--
% solids	3	3	3
Solids density	--	--	--
% Sand	TR	TR	TR
T °C			

Depth (ft)	Lithology

• CONSUMPTIONS •

CHEMICALS	QUANTITY Total m3 or T	QUANTITY Kg/ft or m drilled	QUANTITY Kg/m3	COST Unit Price	COST Total Cost	%
BARITE		--	116.9	8.00	2,800.00	26.5
AQUAGEL	12.635T	--	92.9	14.00	3,893.00	36
CAUSTIC	0.700T	--	5.1	74.70	747.00	7.1
SODA ASH	0.520T	--	3.8	13.88	180.44	1.7
Q.BROXIN	0.575T	--	4.2	29.50	678.50	6.4
CMC HV	0.775T	--	5.7	48.68	1,509.08	14.3
PAC-R	0:025T	--	0.2	106.06	106.06	1.0
MANPAC	0.150T	--	1.1	106.06	636.36	6.0
TOTAL	31,287.5				10,549.44	

Total cost of { Interval : A$ 10,549.44 / Drilled meter foot }

Currency : AUSTRALIAN DOLLARS

Conversion rate used :

Fig 3g Bis 2-78

DRILL STRING COMPOSITION AND DEVIATION SURVEYS

WELL: CAS 1

RUN NUMBER	INTERVAL	DRILL STRING	. DRILLING .			. SURVEYS .				
			Weight on bit	R.P.M.	Flow rate	Number	Date	Drilled depth (m or ft)	Inclination (°)	Direction (°)
1	26"	26" BIT+FLOAT SUB+2x9½DC+26"STAB+1x9½DC+XO+2x7 3/4DC+ +7 3/4BUMPER SUB+4x7 3/4DC+XO+5"E DP.	5/10	80/90	3400	1	2.11.82	220m	½	
2	17½"	17½"BIT+FLOAT SUB+2x9½DC+17½STAB+1x9½DC+XO+2x7 3/4DC+ BUMPER SUB+4x7 3/4DC+XO+9 HWDP+5" E DP	5/8	130/150	3200	2	5.11.82	518m	½	
3	17½"	17½"BIT+FLOAT SUB+2x9½DC+17½STAB+1x9½DC+XO+2x7 3/4DC+ BUMPER SUB+4x7 3/4DC+XO+EQ JARS+2x 7 3/4DC+XO+9 HWDP.	5/15	120/150	3200	3 4	 8.11.82	MISRUN 1320m	 ½	
4	12¼"	12¼"BIT+BIT SUB+2x7 3/4DC+12¼STAB+4x7 3/4DC+BUMPER SUB+ 6x7 3/4DC+XO+EQ JARS+XO+1 HWDP+HYDRIL SUB+8 HWDP+5" DP	15	125	2500	5 6	12.11.82 15.11.82	1572m 1847m	½ 3/4	
5	12¼"	12¼"BIT+BIT SUB+2x7 3/4DC+12¼ STAB+3x7 3/4DC+12¼STAB+ 1x7 3/4DC+BUMPER SUB+6x7 3/4DC+XO+EQ JARS+XO+1HWDP+ HYDRIL SUB+8 HWDP+5"DP GRADE E.	14	130	2300	7	19.11.82	2348m	1	
6	12¼"	8½" RC3 CORE HEAD+20m CORE BBL+2 XO+2x7 3/4DC+12¼STAB+ 2 BUMPER SUBS+6x7 3/4DC+XO+EQ JARS+XO+1 HWDP+HYDRIL SUB +8 HWDP+5" DP GRADE E.	6	100	1020					
7	12¼"	12¼BIT+NB 3 POINT REAMER+SHOCK SUB+12¼STAB+2x7 3/4DC+12¼ STAB+6x7 3/4DC+BUMPER SUB+6x7 3/4DC+XO+EQ JARS+1 HWDP+ HYDRIL SUB+ 8 HWDP+5"DP GRADE E.		NO DRILLING		DUE TO FISHING				
8	12¼"	12¼"BIT+NB 3 POINT REAMER+SHOCK SUB+2x7 3/4DC+12¼STAB+ 6x7 3/4DC+BUMPER SUB+6x7 3/4DC+XO+EQ JARS+XO+1HWDP+ HYDRIL SUB+8HWDP+5"DP GRADE E.	15/20	80/140	1950	8	25.11.82	2521m	3	
9	12¼"	12¼"BIT+NB 3 POINT REAMER+SHOCK SUB+12¼STAB+2x7 3/4DC+ 12¼STAB+6x7 3/4DC+BUMPER SUB+6x7 3/4DC+XO+EQ JARS+XO+ 1 HWDP+HYDRIL SUB+8 HWDP+5"DP GRADE E.	12/25	70	2250	9	28.11.82	2648m	2	
10	12¼"	12¼"BIT+12¼NB STAB+SHOCK SUB+2x7 3/4DC+12¼ STAB+9x7 3/4 DC+BUMPER SUB+6x7 3/4DC+XO+EQ JARS+XO+1HWDP+HYDRIL SUB +7 HWDP+5" DP GRADE E.	20	80/120	2050	10	29.11.82	2798m	2	
11	12¼"	12¼"BIT+BIT SUB+D/S ROLLER REAMER 3 POINT+SHOCK SUB+12¼ STAB+2x7 3/4DC+12¼STAB+9x7 3/4DC+BUMPER SUB+6x7 3/4DC+ XO+EQ JARS+XO+1 HWDP+HYDRIL SUB+8HWDP+5"DP GRADE E.	20	80	2050	11	2.12.82	2950m	2 3/4	
12	12¼"	12¼"BIT+BIT SUB+ROLLER REAMER+SHOCK SUB+STAB+2x 7 3/4DC+ STAB+4x7 3/4DC+BUMPER SUB+3x7 3/4DC+XO+6x6½DC+FLEX JT.+ EQ JARS+1 HWDP+HYDRIL SUB+8 HWDP.	COND. TRIP	HOLE	2050		7.12.82			
13	12¼"	BIT+REAMER+1x8"MONEL DC+1x7 3/4DC+STAB+6x7 3/4DC+BUMPER SUB+3x7 3/4DC+XO+6x6½DC+FLEX JT.+EQ JAR+1 HWDP+HYDRIL SUB+8HWDP.	MULTI SURVEY	SHOT RUN	2050	FROM MULTI SHOT	9.12.82	2678m	2	S56W
14	12¼"	SIDE TRACK BHA-BIT+9 5/8 DYNA DRILL+1½BENT SUB+8"MONEL DC+BUMPER SUB+6x7 3/4DC+XO+FLEX JT+EQ JAR+1 HWDP+HYDRIL SUB+8 HWDP.	1/3	(T) 250+	2270					
15	12¼"	SIDE TRACK BHA-BIT+DYNA DRILL+2 DEG BENT SUB+8" MONEL+ BUMPER SUB+6x7 3/4DC+XO+FLEX JT+EQ JAR+1 HWDP+HYDRIL SUB+8 HWDP.	1/3	(T) 250+	2500	(SIDE TRACK UNSUCCESSFUL)				
16	12¼"	BIT+BIT SUB+9x7 3/4DC+XO+FLEX JT+EQ JAR+ 1 HWDP+HYDRIL SUB+8 HWDP.	COND. REAMING	TRIP	2000					

[redacted] 39 [redacted] D[redacted] ST[redacted]G C[redacted]POS[redacted]N A[redacted]DE[redacted]ION [redacted]RVE[redacted] [redacted] WE[redacted]: U[redacted]

RUN NUMBER	INTERVAL	DRILL STRING	. DRILLING .			. SURVEYS .				
			Weight on bit	R.P.M.	Flow rate	Number	Date	Drilled depth (m or ft)	Inclinction (°)	Direction (°)
17	12¼"	BIT+BIT SUB+1x7 3/4DC+12¼STAB+2x7 3/4DC+12¼ STAB+6x7 3/4 DC+XO+FLEX JT+EQ JARS+1 HWDP+HYDRIL SUB+ 8 HWDP.	2/10	50/100	2000		COND. TRIP REAMING NO NEW HOLE			
18	12¼"	SIDETRACK BHA-12¼BIT+7 3/4DYNA DRILL+2 DEG BENT SUB+BUMPER SUB+3x7 3/4DC+XO+6x6½DC+FLEX JT+EQ JARS+1 HWDP+HYDRIL SUB+8 HWDP	0/1	DYNA DRILL	1640		SIDETRACK ABORTED TO RUN 9 5/8 CASING.			
19	12¼"	BIT+BIT SUB+1x7 3/4DC+STAB+2x7 3/4DC+STAB+6x7 3/4DC+XO+ FLEX JT+EQ JARS+1 HWDP+HYDRIL SUB+8 HWDP.	--	--	1900		COND. TRIP BEFORE 9 5/8 CASING.			
20	8½	BIT+BIT SUB+18x6½DC+BUMPER SUB+6x6½DC+FLEX JT+EQ JARS+1 HWDP+HYDRIL SUB+8 HWDP.	10	50/70	1184		DRILL OUT CLEAN OUT	9 5/8 FLOAT TO TD.	EQUIP & CMT.	
21	8½"	SIDETRACK BHA-BIT+POSI DRILL6½+XO+FLOAT SUB+2DEG BENT SUB +6½ BUMPER SUB+ORIENTING SUB+6½ MONEL+6x6½DC+FLEX JT+EQ JARS+1 HWDP+HYDRIL SUB+8HWDP	0/1	POSI DRILL	1316	1	START SIDETRACK 25.11.82	IN 8½ HOLE 2638m	2½	S63W
22	8½"	BIT+REAMER+CUSHION SUB+FLOAT SUB+REAMER+6½ MONEL+STAB+ 2x6½DC+STAB+15x6½DC+BUMPER SUB+6x6½DC+FLEX JT+EQ JARS+1 HWDP+HYDRIL SUB+8 HWDP.	17	70	1110	5	CONFIRMED 28.12.82	SIDETRACK 2710m	1 3/4	N12E
23	8½"	BIT+REAMER+CUSHION SUB+FLOAT SUB+REAMER+6¼ MONEL+STAB+2 x6½DC+STAB+11x6½DC+BUMPER SUB+6x6½DC+FLEX JT+EQ JAR+1 HWDP+HYDRIL SUB+8 HWDP.	15	70	1200	8	29.12.82	2791m	1	N02W
24	6"	MILL+BIT SUB+6x4 3/4BUMPER SUB+9x4 3/4DC+FLEX JT+4 3/4 EQ JAR+12 HWDP+3½DP.	1/5	70	1300					
25	6"	BIT+JUNK SUB+5 3/4STAB+1x4 3/4DC+5 3/4STAB+2x4 3/4DC+ 5 3/4STAB+3x4 3/4DC+BUMPER SUB+9x 4 3/4DC+FLEX JT+EQ JAR+12x3½ HWDP+3½ DP.	6	65	700					
26	6"	DIA BIT+NAVI DRILL+JUNK SUB+BIT SUB+1x5 3/4DC+5 3/4STAB+ 2x4 3/4DC+1x5 3/4STAB+1x4 3/4DC+4 3/4BUMPER SUB+9x4 3/4 DC+FLEX JOINT+EQ JAR+12 HWDP+3½DP.	4	--	1000/2200					
27	6"	STRATA BIT+JUNK SUB+BIT SUB+ 4x4 3/4DC+BUMPER SUB+9x4 3/4 DC+FLEX JT+EQ JAR+12x3½ HWDP-DP.	3/4	140	700					
28	6"	DRILL BIT+NEAR BIT REAMER+1x 4 3/4DC+STAB+2x4 3/4DC+STAB +9x4 3/4DC+BUMPER SUB+4x4 3/4DC+FLEX JT+EQ JARS+12x3½	10	55/75	700					
		HWDP - DPS								
29	6"	BIT+6x4 3/4DC+4 3/4BUMPER SUB+3x4 3/4DC+FLEX JT+EQ JARS+ 12x3½HWDP+3½DP+HYDRIL DROP SUB+5" DP.	USED FOR CONDITIONING TRIPS ONLY.							

Company: [redacted]

Well No.: OMEO WELL NO 1

Proposal:

Type of Survey: MAGNETIC MULTISHOT

SURVEY RECORD

Date of Survey: 9th DECEMBER 1982

Job No.:

Engineer: H. PRIESTLEY

Measured Depth	Drift Angle	True Vertical Depth	Vertical Section	Drift Direction	Rectangular Coordinates North	Rectangular Coordinates South	Rectangular Coordinates East	Rectangular Coordinates West	Dog Leg
4338	0. 75	4338 0		S 1 W		26		01	
4431	0 50	4430 99		S 41 W		1 18		28	
4525	0. 50	4524 99		S 19 W		1 87		68	
4619	0. 75	4618 98		S 53 W		2 63		1 31	
4712	0. 75	4711 98		S 56 W		3 34		2 30	
4806	1. 00	4805 97		S10 W		4 49		2 95	
4899	0 . 75	4898 96		S 56 W		5 63		3 60	
4993	0. 25	4992 95		S 85 W		5 99		4 31	
5087	0. 50	5086 95		S 40 W		6 32		4 78	
5180	0. 75	5179 95		S 50 W		7 03		5 51	
5275	1. 00	5274 94		S 83 W		7 53		6 81	
5368	1.00	5367 92		N 88 W		7 60		8 42	
5461	1.25	5460 90		S 82 W		7 71		10 24	
5555	1.00	5554 89		S 76 W		8 05		12 05	
5649	1.00	5648 87		S 75 W		8 46		13 64	
5742	1.00	5741 86		S 45 W		9 25		15 00	
5836	1.00	5835 84		S 66 W		10 16		16 32	
5930	1.25	5929 83		S 21 W		11 45		17 44	
6023	1.25	6022 80		S 16 W		13 37		18 08	
6117	1.00	6116 80		S 43 W		14 96		18 93	
6211	1.00	6210 77		S 35 W		16 23		19 96	
6304	0.75	6303 76		N 84 W		16 83		21 03	
6398	1.00	6397 76		S 6 W		17 58		21 73	

easured Depth	Drift Angle	True Vertical Depth	Vertical Section	Drift Direction	Rectangular Coordinates				Dog Leg
					North	South	East	West	
6492	0. 50	6491 75		S 43 W		18 70		22 09	
6585	0.75	6584 74		S 20 W		19 57		22 58	
6679	0.75	6678 74		S 78 W		20 27		23 39	
6773	1.00	6772 73		S 23 W		21 16		24 31	
6866	1.00	6865 71		S 20 W		22 67		24 90	
6960	0. 75	6959 70		S 49 W		23 84		25 65	
7054	0.75	7053 69		S 40 W		24 72		26 51	
7147	0.75	7146 69		S 36 W		25 67		27 26	
7241	1.25	7240 67		S 63 W		26 64		28 53	
7335	1.00	7334 65		S 61 W		27 50		30 16	
7428	0.75	7427 64		S 63 W		28 17		31 42	
7522	1.00	7521 63		N 82 W		28 33		32 78	
7615	0.75	7614 62		S 80 W		28 33		34 18	
7709	1.00	7708 61		S 81 W		28 56		35 60	
7803	1.00	7802 60		W		28 69		37 23	
7896	1.50	7895 57		S 86 W		28 78		39 25	
7990	1.75	7989 54		S 80 W		29 11		41 89	
8084	1.75	8083 49		S 77 W		29 68		44 71	
8177	2.50	8176 43		S 79 W		30 39		48 08	
8271	3.00	8270 32		S 79 W		31 25		52 51	
8365	3.00	8364 19		S 70 W		32 56		57 23	
8458	3.00	8457 06		S 67 W		34 34		61 76	
8552	3.00	8550 93		S 64 W		36 38		66 24	

sured Depth	Drift Angle	True Vertical Depth	Vertical Section	Drift Direction	Rectangular Coordinates				Dog Leg
					North	South	East	West	
646	2.75	8644 82		S 58 W		38 66		70 36	
739	2.25	8737 73		S 59 W		40 78		73 82	
789	2.00	8787 69		S 56 W		41 77		75 38	
				CLOSURE IS 86.18 Ft by S61.01°W.					

F3 h Bis 2-78 | COMPLETION STATUS | WELL: OMEO 1

1) COMPLETION (If carried out by the drilling rig)

yes ☐

no ☒

2) - CASINGS, TUBINGS AND ANNULUS STATUS

CASING AND TUBING DIAMETER	SHOE DEPTH	HANGER DEPTH	CASING CUT DEPTH (event)	CEMENT TOPS		ANNULUS FLUIDS	
				OD	ID	NATURE	SG
20"	210m	90m				CMT	1.85
13 3/8"	1310m	89m		TEMP LOG 825		POLYMER MUD	1.04
9 5/8"	2606m	91m		TEMP LOG 2179		POLYMER MUD	1.19
7" LINER	2985m	2498.5m		2498.5		POLYMER/GEL MUD	1.20

Depths of perforations : 2918 TO 2915 2932 TO 2939

Tubing anchoring device and packer depth(s) :

3) - CEMENT PLUGSAND BRIDGE PLUGS (CP and BP)

CEMENT PLUG (CP) or BRIDGE PLUG (BP)	CP #1	CP#2	CP#3	CP#4	CP#5	CP#6	CP#7		
FROM (m or ft)	3349	3220	3030	2950	2530	290	170		
TO (m or ft)	3280	3045	2960	2880	2440	200	SEABED		
TESTED	☐ yes ☒ no	☐ yes ☒ no	☒ yes ☐ no	☐ yes ☒ no	☐ yes ☐ no	☒ yes ☐ no	☐ yes ☒ no	☐ yes ☐ no	☐ yes ☐ no
BY PRESSURE OR WEIGHT			3000PSI 15'-OK			900PSI 15'-OK			

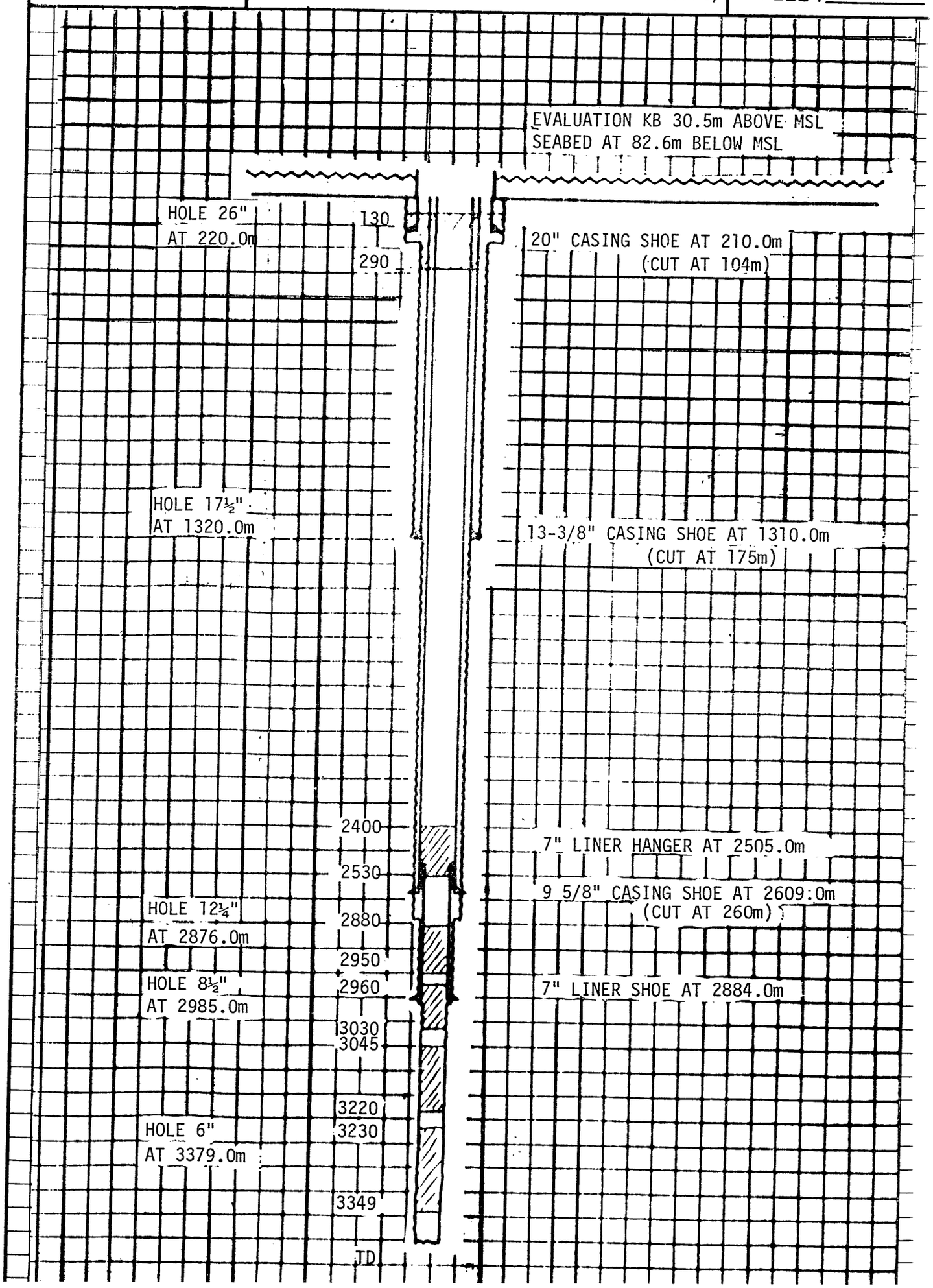
4) - WELL HEAD

Description of abandonned equipment : NOTHING - ALL BASE PLATES RECOVERED

RELOCALIZATION DEVICE { yes ☐ no ☒ TYPE :

Imp. 4996 SNEAP) RGM 959 004.011

F3h' Bis 2-78 | WELL TECHNICAL SECTION (COMPLETION STATUS) | WELL : OMEO 1



F3 i Bis 2-78 | **MAIN CONSUMPTIONS OF THE WELL** | **WELL:** OMEO 1

ROCK BITS AND CORE BITS

BIT DIAMETER	CONE BITS				DIAMOND BITS			BITS		Total by interval
	Tooth tricone bits	Insert tricone bits	Removable center	Bicone bits	Drilling bits	Core bits	Removable center	Drag bits	Special bits STRATAPAK	
26"	1U									1U
17½"	2									2
12¼"	10	6								16
8½"	4	3				1				8
6"		7			1	1			2	11
									TOTAL →	38

CASINGS

Diameter	Weight (lbs/Ft)	Thread	Grade	Length (Ft or m)	Observations
20"	133	"CC" CONN.	X56	108.47	PILE JT. 12.29m
13 3/8"	68	BUTTRESS	K55	1219.21	SET AT 1310m
9 5/8"	47	BUTTRESS	N80	2516.46	SET AT 2606.61m
7"	26	BUTTRESS	N80	486	HANGER / SHOE SET 2498.5 2985m

F3j Bis 2-78	COSTS BREAKDOWN	WELL: OMEO

	OPERATIONS	BEFORE DRILLING	DRILLING	AFTER DRILLING
I	Operation preparation	4,123	--	--
II	Access and drilling site works or sea bottom surveys	39,170	23,657	--
III	Rig mobilization and moving in - COSTS EX SINGAPORE/MOVING DOWN AUST. COAST, APPORTIONED	233,828	3,061,671	--
	SUB TOTAL	277,121	3,085,328	--
IV	Drilling Contractor	--	8,023,921	--
V	Consumables	--	2,173,644	--
VI	Rental and services	--	2,378,836	--
VII	Operator supervision	--	493,275	--
VIII	Transportation (air - land - sea)	--	2,839,610	--
IX	Insurances	--	--	--
X	Operating bases	--	270,570	--
XI	Rig demobilization and moving out	--	--	--
XII	Finalization of operations	--	--	--
	SUB TOTAL	--	16,179,857	--
	TOTAL	A 277,121	B 19,265,185	C --
	TOTAL COST OF WELL: A + B + C		19,542,306	

- **Drilled footage (meter or feet):** 3,288 m
- **Cost** { per drilled meter $\frac{B}{m}$ 5,859 / or drilled foot $\frac{B}{ft}$ }
- **Drilling duration (d):** 101 days (INCLUDING TESTIND/P&A)
- **Daily cost** $\frac{B}{d}$: 190,744

Currency: AUSTRALIAN DOLLARS **Conversion rate:** --

Imp. 4996 SNEA(P) RGM 959.004.011

F3j' Bis 2-78 | BREAKDOWN OF CONSUMABLES, RENTAL AND SERVICE COST | WELL: OMEO

CONSUMABLES (Item 5)

- Fuel and lubricants A$475,916
- Drilling bits A$133,305
- Core - Bits A$ 40,031
- Mud chemicals A$405,839
- Cements A$127,559
- Water A$ 11,932
-

- Casing and miscellaneous A$625,178
- Wellhead and miscellaneous A$283,883
- Bottom hole equipment A$ 39,745
- Surface equipment A$ 8,857
- Offshore or anchoring equipment A$16,474
- Anti-pollution products A$ 4,925
-

TOTAL : A$2,173,644

RENTAL AND SERVICES (Item 6)

- Electrical logging A$1,055,139
- Cementing and pumping A$115,760
- Fishing A$21,929
- Turbodrill A$42,831
- Testing A$225,887
- Subsea operations (diving) A$369,695
- Welding A$ 210
- Oceano-meteorological assistance A$32,126
- Velocity survey A$9,996
- Subsea television --
- Positioning / EQUITY STANDBY: A$90,372
-

- Mud logging A$149,910
- Mud services A$ 36,645
- Directional DRILLING A$ 76,565
- Tong service A$ 33,546
- Air drilling --
- Other services - LINER HANGER SETTING TOOLS A$ 28,674
- Bottom hole equipment rental A$118,576
- Surface equipment rental A$ 1,122
- Wellhead equipment rental A$ 9,023
- Anti-pollution equipment rental --
-
-

TOTAL: A$2,418,006

F3i' Bis 2-78	MAIN CONSUMPTIONS OF THE WELL	WELL: OMEO 1

• CEMENTS •

Class	QUANTITY (T)			Class	QUANTITY (T)		
	Casing	Well abandon	Plugging losses		Casing	Well abandon	Plugging losses
	296T	26T	0	"G"	6T	43T	

CHEMICALS

CHEMICAL NAME	QUANTITIES ADDED m^3 or T	CHEMICAL NAME	QUANTITIES ADDED m^3 or T
BENTONITE	88.00	CONDET	1.240M^3
CAUSTIC	13.12	BICARBONATE	4.08
SODA ASH	10.00	SODIUM NITRATE	4.10
LIME	0.70	SURFLO W300	0.208M^3
BARITE	430.00	SOLTEX	5.72
CMC HV	4.95	STARLOSE	3.20
Q.BROXIN	4.06	AL. STEARATE	0.11
DEXTRID	31.15	MANPAC	0.15
PAC-R	11.56	NB: LOSSES ARE EXCLUDED OF	ABOVE FIGURES

WATER - DIESEL/OIL (not added in mud)

FRESH WATER (m^3)	--		
DIESEL-OIL (m^3)	593T		

WELL HEADS, HANGERS (Ø - API working pressure - Type)

CIW 18 3/4" x 20" PILE JOINT 10,000 PSI

CIW DRILLING TEMPLATE (MODIFIED) & PGB

CIW 13 3/8" x 18 3/4" HANGER + LOW TORQUE SEAL ASSMY. 10,000 PSI.

CIW 9 5/8" x 18 3/4" HANGER + LOW TORQUE SEAL ASSMY, 10,000 PSI.

CIW 7" x 9 5/8" LINER HANGER WITH PACKER AND TIE BACK SLEEVE 8,500 PSI.

F3k Bis 2-78 | **MONTHLY METEOROLOGICAL SHEET** | WELL: OMEO 1

MONTH: NOVEMBER | WELL: OMEO - VIC-P17

YEAR 1982	DAILY MORNING OBSERVATIONS							UNIT MOTIONS			Temperature °C	Visibility (miles)
	Wind		Waves			Current		Roll	Pitch	Heave		
DATE	Speed	Direction	Height (Ft or m)	Period (sec.)	Direction	Speed (Knt)	Direction	(°)	(°)	(Ft or m)		
1	15	SW	1.5	6	SW			.5	.5	N/A	12.5	
2	5	S	RIPPLES					.5	.4	.2	16	
3	5	S	VARIABLE					.2	.2	.3	16	
4	10		VARIABLE					.2	.2	.4	16	
5	17	NW	RIPPLES					.2	.2	.4	21	
6	20	NNE	1	8	NE			.2	.2	.4	28	
7	27	SW	3.5	8	SW			.3	.2	.5	18	
8	30	WSW	3	8	SW			.4	.4	.5	20	
9	40	WSW	5	7	SW			.6	.5	.8	16.5	
10	45	W	7	8	SW			.7	.8	1.0	15.5	
11	20	W	3	6	SW			.4	.3	.6	16	
12	12	WSW	2.5	8	SW			.3	.2	.5	16	
13	12	SE	1.5	6	E			.2	.2	.4	15	
14	35	NNE	2	7	E			.2	.2	.5	25	
15	38	WSW	3	6	SW			.2	.2	.5	21.5	
16	38	WNW	5	6	WSW			.3	1.5	1	17	
17	40	WNW	3	7	SW			.5	.5	.8	17	
18	50	W	3	7	W			1	1.5	1.8	13	
19	30	WSW	3	7	SW			.5	.6	.6	15	
20	30	SW	4	5	SW			.4	.6	.6	15	
21	10	WSW	2	6	SW			.4	.4	.5	16	
22	15	SSE	2	4	ESE			.3	.3	.5	17	
23	23	N	1	7	E			.3	.2	.3	21	
24	25	SW	1.5	7	SW			.3	.2	.5	24	
25	35	SW	6	7	SW			1.2	1.2	1	18	
26	35	W	5	8	SW			1	1.2	1	16	
27	30	SW	5	7	SW			1	.8	1	15	
28	25	E	2.5	9	E			.6	.6	.9	19	
29	25	E	2	3	E			.6	.5	.6	18	
30	20	ENE	2	VARIABLE				.4	.3	.5	20	
31												

F3k Bis 2-78	MONTHLY METEOROLOGICAL SHEET	WELL: OMEO 1

MONTH: DECEMBER WELL: OMEO NO. 1 - VIC-P17

YEAR 1982	DAILY MORNING OBSERVATIONS							UNIT MOTIONS			Temperature °C	Visibility (miles)
	Wind		Waves			Current		Roll	Pitch	Heave		
DATE	Speed	Direction	Height (Ft or m)	Period (sec.)	Direction	Speed (Knt)	Direction	(°)	(°)	(Ft or m)		
1	35	WSW	6	6	SW			.8	.6	.6	17	
2	10	E	2	6	SW			.3	.3	.6	17	
3	25	WSW	1	4	VAR			.5	.3	.5	18	
4	25	SW	2.5	7	SW			.3	.3	.6	16	
5	26	SW	2.5	7	SW			.3	.3	.6	16	
6	18	NE	2.5	3	SW			.3	.3	.5	16	
7	40	WSW	3.5	5	WSW			.3	.4	.5	17.5	
8	50	SSW	5	5	SSW			.3	.8	1	16	
9	25	S	3	8	S			1.2	.6	1.5	17	
10	25	S	5	6	S			1.2	.5	1.5	16	
11	15	E	2.5	5	SE			.8	.3	.8	17.5	
12	18	E	2	6	SE			.2	.2	.5	17.5	
13	25	NE	2.5	VARIABLE				.2	.2	.5	21	
14	25	W	2.5	5	SW			.4	.4	.5	18.5	
15	25	W	2.5	5	SW			.4	.4	.5	18	
16	22	SSW	3	6	SW			.3	.3	.6	18	
17	35	WSW	5.5	7	SW			.5	.6	.8	18.5	
18	30	WSW	4.5	6	SW			.4	.4	.5	17.5	
19	30	WSW	5	6	SW			.5	.5	1	16	
20	40	WSW	6	7	SW			.6	.7	1	16	
21	10	ESE	1.4	6	SW			.4	.4	.5	17	
22	10	ESE	0.4	6	SW			.4	.3	.2	19.5	
23	12	NNE	-----NEG-----					.3	.3	.2	21.5	
24	22	SW	4	6	SW			.4	.5	.4	20	
25	20	E	3	6	E			.4	.5	.5	17	
26	25	E	3.5	6	E			.5	.5	.5	17	
27	25	E	3.5	6	E			.4	.4	.5	19.5	
28	20	E	----NEG----					.3	.2	.3	20	
29	20	E	1.5	5	E			.3	.4	.6	22	
30	8	ENE	1.5	5	E			.4	.4	.4	22	
31	18	E	2	5				.4	.3	.5	21	

F3k Bis 2-78 | MONTHLY METEOROLOGICAL SHEET | WELL: OMEO 1

MONTH: JANUARY | WELL: OMEO NO. 1

YEAR 1983	DAILY MORNING OBSERVATIONS							UNIT MOTIONS			Temperature °C	Visibility (miles)
	Wind		Waves			Current						
DATE	Speed	Direction	Height (Ft or m)	Period (sec.)	Direction	Speed (Knt)	Direction	Roll (°)	Pitch (°)	Heave (Ft or m)		
1	15	SW	2	6	E			.2	.2	.5	21	
2	30	WSW	5	9	SW			.5	.4	.5	20	
3	25	WSW	4.5	8	SW			.5	.5	.6	20	
4	15	WNW	2	4	SW			.4	.5	.6	18	
5	35	SWS	5	6	SW			.5	.5	.5	18	
6	20	WSW	3.5	6	SW			.3	.3	.5	18	
7	18	ENE	2	6	SW			.3	.4	.5	18	
8	18	SW	3.5	8	SW			.3	.5	.5	22.5	
9	35	W	5.5	6	W			.5	.8	1.5	20	
10	45	WSW	4.5	6	SW			.5	.8	1.5	18	
11	35	WSW	5	6	SW			.5	.8	.8	16	
12	30	W	4.5	6	SW			.5	.8	.8	16	
13	30	WSW	4	7	SW			.5	.6	.5	16	
14	35	WSW	6	7	SW			.8	.8	.6	16	
15	30	WSW	6	7	SW			.5	.7	.6	17.5	
16	35	WSW	5	6	SW			.6	.8	.8	17.5	
17	35	WSW	5	8	SW			.5	.7	.8	17	
18	15	SW	3	6	SW			.6	.4	.4	16	
19	25	SW	6	6	SW			.2	.2	.3	17	
20	10	E	1.2	6	E			.2	.3	.3	19	
21	12	ENE	1		E			.2	.2	.3	20	
22	22	E	2.5	4	E			.6	.6	.5	18.5	
23	30	WSW	5	6	WSW			.5	.6	.6	19	
24	25	W	5	7	W			.5	.6	.6	17.5	
25	25	W	5	8	W			.5	.6	.6	18	
26	32	WSW	4	7	E			.3	.6	.8	26	
27	22	W	3.5	7	SW			.4	.4	.6	18	
28	10	W	2	7	SW			.3	.3	.5	20	
29	11	SW	1.5	VARIABLE				.2	.2	.4	20	
30	8	WSW	1.5	VARIABLE				.2	.2	.4	20	
31	20	NE	1	VARIABLE				.2	.2	.4	22.8	

F3k Bis 2-78 | **MONTHLY METEOROLOGICAL SHEET** | WELL: OMEO 1

MONTH: FEBRUARY | WELL: OMEO NO. 1 - VIC-P17

YEAR 19__	DAILY MORNING OBSERVATIONS							UNIT MOTIONS			Temperature °C	Visibility (miles)
	Wind		Waves			Current						
DATE	Speed	Direction	Height (Ft or m)	Period (sec.)	Direction	Speed (Knt)	Direction	Roll (°)	Pitch (°)	Heave (Ft or m)		
1	20	SW	1.5	VARIABLE				.2	.2	.5	18.5	
2	2	SW	NIL	NIL	NIL			.2	.2	.4	19	
3	8	WSW	1	6	SW			.1	.1	.2	18	
4	2	WSW	NIL	NIL	NIL			.1	.1	.2	20	
5	6	E	1.5	2	SE			.2	.2	.3	20	
6	12	NW	1	2	VAR			.2	.2	.4	24	
7	15	ENE	1	VAR	VAR			.2	.2	.4	20	
8	35	SW	1.5	VARIABLE				.5	.5	1	19.5	
9	20	SW	1.5	VARIABLE				.5	.5	1	20	
10												
11												
12												
13												
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FORMATION TEST REPORT

F4bis 3-78

A - TECHNICAL DATA

1) GENERAL DATA

CONTRACTOR: ODECO
DRILLING RIG: OCEAN DIGGER

WELL: OMEO NO. 1

WELL STATUS	DEPTH meters or feet	DIAMETER
LAST CASING	2984	7"
OPEN HOLE	3378	6"
PLUG [Cement	3349-3280	7"
	3220-3045	7"
	3030-2960	CSG 9 5/8/7"

TEST N°: 1 CARRIED OUT BY: HALLIBURTON

FROM: 2918 TO 2938

ON SHORE ☐ OFF SHORE ☒

ALTITUDE: WATER DEPTH: 62.6m

DISTANCE RKB/GROUND: DISTANCE RKB /REFERENCE: 93.1m

REFERENCE: SEABED

REASON FOR TESTING: EVALUATION OF THE LATROBE FORMATION (QUICK TEST BEHIND 7" LINER TO DETERMINE THE NATURE OF THE FLUID)

TESTED INTERVAL
FROM 2918m
TO 2939m

HYPOTHETICAL PRODUCING LAYER(S)
from 2849 to 2952
from 3073 to 3181
from 3320 to 3372
from ____ to ____

LITHOLOGY: SANDSTONE WITH VARIABLE AMOUNTS OF CLAY

FORMATION(S): LATROBE FORMATION

2) MUD AND CUSHION FLUID CHARACTERISTICS

MUD Nature GEL/POLYMER S.G. 1.10 Water loss 7 Viscosity 38
Choride content 20000 Ph 9.5 Resistivity RMF 0.21 at 66 DEG F °C

CUSHION FLUID: Nature FRESHWATER S.G. 1.00 Chloride content NIL Resistivity -- at -- °C

CUSHION PRESSURE: 2504 PSI meters or feet in D.P., i.e. 1600 m

3) SPECIFIC TECHNICAL CONDITIONS

F I T ☐ OPEN HOLE TEST ☐ CASING TEST ☒

PACKER DEPTH: ____

CLASSICAL TEST ☒
PACKER SET AT: 2886.2m
HEIGHT UNDER PACKER AT: ____

STRADDLE TEST ☐
LOWER PACKER AT: ____
UPPER PACKER AT: ____

PERFORATED INTERVALS
from 2918 to 2938
from ____ to ____
from ____ to ____
from ____ to ____

VOLUMES: EMPTY 23.97m³ UNDER PACKER 0.878m³ DECOMPRESSION ____

WEIGHT ON PACKER WHEN SETTING: ____

DIFFERENTIAL PRESSURE ON PACKER WHEN OPENING: 140 kg/cm²

BOTTOM HOLE CHOKE ϕ: 1" (BAR CATCH SUB I.D.)

B - DETAILED COMPOSITION OF DRILL STEM STRING

WELL: OMEO NO. 1 TEST N° 1

TOOLS: NATURE, MFG, TYPE	LENGTH	OD	ID	DEPTHS
X OVER 6 3/4" x 4½" IF				-5.00
DRILL PIPE 5" - 4½" IF	87.56			
EZ TREE WITH 3½" SLICK JOINT + X OVERS	8.15			
DRILL PIPE 5" - 4½" IF	2349.39	5.0	4.27	
DRILL PIPE 3½"	286.08	3.5	2.44	
SLIP JOINT (5" STROKE)	4.01	5.0	2.25	
SLIP JOINT (5" STROKE)	4.01	5.0	2.25	
DRILL COLLARS 4 3/4"	110.50	4.75	2.31	
IMPACT REVERSE SUB	0.31	5.0	2.75	
DRILL COLLARS 4 3/4"	27.50	4.75	2.31	
BAR CATCH SUB	0.31	4.75	1.00	
AP. BT CASE	1.25	5.0	3.06	2874.07
APR A CIRCULATION VALVE	0.91	5.03	2.25	2874.98
APR M2 CIRCULATION VALVE	2.29	5.03	2.25	2877.27
APR N TESTER VALVE	3.89	5.0	2.25	2881.16
X OVER 3½ IF B x 3½ FH P	0.65	4.75	2.50	
AP BT CASE	1.25	5.0	3.06	2883.06
X OVER 3½ FH B x 3½ IF P	0.23	4.75	2.50	
FULL-FLO HYDRAULIC BY-PASS	1.93	4.68	2.25	
X OVER 3½ IF B x 2 7/8 EUE P	0.53	4.75	2.50	
7" RTT'S PACKER UP	0.42	5.50	2.25	2886.17
DOWN	0.72			
X OVER 2 7/8" EUE B x 3½ IF P	0.29	4.75	2.50	
PERFORATED ANCHOR	1.52	5.0	2.37	
PERFORATED ANCHOR	1.52	5.0	2.37	
PERFORATED ANCHOR	1.52	5.0	2.37	
BLANKED OFF SUB	0.30	4.75	0	
X OVER 3½ FH B x 3½ IF P	0.29	4.75	2.50	
FULL - FLO BUNDLE CARRIER	2.43	5.375	2.25	2894.76
X OVER 3½ IF B x 3½ FH P	0.32	4.75	2.50	
BO BT CASE	1.24	5.0	2.44	2896.32
PERFORATIONS: 2918-2915 2932-2939				

INTERPRETATION AND OBSERVATIONS:

SEE COMPLETE ANNEXE REPORT (OPERATIONS SUMMARY AND PRELIMINARY TEST REPORT)

PRESSURE EXTRAPOLATION

FIELD READINGS ON THE LAST PART OF THE BUILDUP CURVE (5 or 6 points)

	RECORDERS			
	Type	Depth	Type	Depth
	Δt	Pressure	Δt	Pressure
Initial reservoir pressure	340	3982.7	340	3995.2
	370	3990.1	370	4003.8
	400	3999.2	400	4011.6
	430	4007.2	430	4019.4
	461	4012.4	461	4025.1
Final pressure	77	3960.4	77	3972.8
	84	3964.9	84	3975.9
	91	3968.	91	3979.2
	98	3970.3	98	3982.0
	105	3974.4	105	3985.2
	108.6	3975.9	109	3986.2

C - RESULTS

1) TEST HISTORY

										Duration
1st opening period from	18	25	on	5	to	22	25	on	5	2 hr
1st close in period from	22	25	on	5	to	6	40	on	5	8:15
2nd opening period from	6	40	on	6	to	7	30	on	6	50mn
2nd close in period from	7	30	on	6	to			on	6	
3rd opening period from			on		to			on		
3rd close in period from			on		to			on		

										Duration
Reverse circulation from	7	30	on	6	to	9	30	on	6	2 hrs
Equalise pressure at	9	30	on	6						

2) OPENING PERIOD - SURFACE OBSERVATIONS

FLOW IN D.P.		FLOW AT SURFACE						
TIME	CUMULATIVE FLOW AT METER	TIME	ϕ SURFACE CHOKE	PRESSURE before CHOKE	RECORDED FLOWS OIL	GAS	WATER	OBSERVAT.
5H 20	7.5 m^3							

3) FLUIDS RECOVERY

NATURE	Sample Nb	REFERENCE ***	VOLUME	Resistivity	Temp. °C	Ph	Chloride Content	S.G.	OBSERVATIONS
WATER	5	COLLECT WHILST		0.271	74	10	14000		23000ppm EQUIV.
		REVERSE CIRCULATION		0.307	72	9.5	12000		21000ppm EQUIV.
				0.351	72	9.5	10000		18000ppm EQUIV
				0.381	72	7	9900		16000ppm EQUIV.
				0.403	74	7	9000		15000ppm EQUIV.
GAS	1	APR CHAMBER	18.25 cu ft.						P = 2350 psi
		C1 = 91.36%							
		C2 = 5.54+C3+IC4+NC4+IC5+N5							(SEE A_NEXE)

4) PRESSURES

UNITS: KILOGRAMME/cm^2 - BAR. ATMOSPHERE - PSI

	HALLIBURTON BT	HALLIBURTON BT	HALLIBURTON BT	FLOP.AMERADA RT7
RECORDER Type and N°				
RECORDER DEPTH Zero level RKB	2900m	2876.5m	2867.8m	2900m
A Initial hydrostatic pressure	4469.6	4419.6	2289.5	4616
B1 1st flow initial pressure				
C1 1st flow final pressure	3520	3476.8	3472.0	3531
D1 1st close in period final pressure	4012.9 * ST ☐ NS ☒	3968.5 * ST ☐ NS ☐	* ST ☐ NS ☒	4018 * ST ☐ NS ☐
B2 2nd flow initial pressure				
C2 2nd flow final pressure	3678	3635.9	3626	3578
D2 2nd close in period final pressure	3975 * ST ☐ NS ☒	3934 * ST ☐ NS ☒	* ST ☐ NS ☒	3970 * ST ☐ NS ☐
B3 3rd flow initial pressure				
C3 3rd flow final pressure				
D3 3rd close in period final pressure				
E Final hydrostatic pressure				4415
Calculated hydrostatic pressure				
MAXIMUM TEMPERATURE				250 DEG F

* ST = STAB. - NS = NO STAB.

5) REASON OF EVENTUAL FAILURE: ** FU ☐ BO ☐ NO ☐ IN ☐ OTHER: _____

** FU-Packer leakage. BO-plugged. NO-non opened. IN-test interrupted

*** In the tester tool, ir DP, flowing, etc...

WRITER NAME

M. PERRET

CASING AND CEMENTING REPORT

F5a Bis

WELL (Country)	RIG (Contractor)	R Ground ☐ K Height B M.L. ☒	ø Casing ☒ Liner ☐	CASING SHOE	Hanger depth (for liners) or changing ø casing depth :	OPERATION DATE
OMEO 1 (VIC-P17)	O. DIGGER (ODECO)	93M	20"	Measured depth : 210M Vertical depth : 210M		3.11.82

1 - WELL CONDITION

Open hole diameter : 26" Depth { Vertical : Measured : 220M } Deviation { Mini : ° to Maxi : 0 ½ to 220

Important caving (location - average diameter..) : NO CALIPER

Losses during drilling (levels, extent) OPEN RETURNS TO SEA BED

Reamer runs (number) ONE Reamer at 20 m from the b

Previous casing : Diameter Shoe at

Bo. Ps on well when running in (Type - equipment, test pressure) - NO -

MUD CHARACTERISTICS BEFORE INJECTING SLURRY	S.G.	W.L.	P.V.	Y.V.	VISCOSIMETER READINGS Vs R.P.M. 600	300				
	1.03									

Observations HOLE FILLED UP WITH 450 BBLS HIGH VISC. MUD (VISC 100+)

2 - GENERAL COMPOSITION OF CASING STRING

ELEMENT	MFG. type	ø	Weight (lb/ft) or thickness	Thread or joint type	Grade	Special corrosion ?	Inside volume l/m	Length (m)	Number of joints
SHOE	FLOAT TRISTATE	20")	SHOE JOINT	"CC"	X56	NO		12.80	X 1
COLLAR	FLOAT	20")							X
CASING	N.K.K	20"	133	CIW "CC"	X56	NO	177.8	95.28	8
PILE JT	CIW	24"x18"		"CC"		NO		12.29	1
Tripping joint :	5"	- DP	HW + BS					89.90	X
							TOTAL ➤	210.27 m	10

Drift diameter in the thickest joint 18" ID ON PILE JOINT

Maximum permissible tension 143T

Theoretical weight of the casing string : In air 35T in mud : 30.5T

3 - EQUIPMENT OF CASING STRING

CENTRALIZERS	SCRATCHERS	OTHER EQUIPMENT (Description - Location)
MGF :	MGF :	18 3/4" WELLHEAD HOUSING WITH
TYPE :	TYPE :	24"x3" WALL.
NUMBER :	NUMBER :	PILE JOINT EXTENSION 10m LONG
DEPTH/RKB :	DEPTH/RKB :	

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4 - RUNNING CASING

Making-up of joint : SQUNCH JOINT TYPE C.C. CAMERON
Grease type used for threads : NO-OIL
Average torque to make-up the joints : N/A
Filling frequency : EACH JOINT
Intermediate circulation (duration - depth) : BEFORE REENTERING 26" HOLE

Total running time (with circulations) 5 h 45 average rate -- joints/h
Troubles during running : BOTH SHOE JOINTS PLUGGED - HAVE TO CUT WINDOW AND CLEAN UP BETWEEN FLOAT & SHOE AND REWELD WINDOW

Bottom hole circulation : Duration 30MIN Rate 1360L/MIN Pressure 250 PSI
Reciprocating : Duration NO Rate Amplitude
M.D. indications after stop of bottom hole circulation : CASING LANDED W/TGB ON TEMPLATE
Observations : CIRCULATE CASING VOLUME BEFORE REENTRY WHILE MONITORING CIRC. AT SHOE (PARTLY PLUGGED) WITH TV.

5 - SINGLE STAGE OR FIRST STAGE CEMENTING

Service cy DOWELL SCHLUMBERGER
Mixing pump " "
Slurry injection pump DOWELL SCHLUMBERGER
Displacement pump(s) DOWELL SCHLUMBERGER

Beginning of slurry making at 17.20 h
End of slurry making at 18.35 h.
End of displacement at 19.00 h.
Pressure released in casing at 19.00 h.

	Nature or class of cements	~~Sacks or~~ bulk	Cement weight increase %	Water and additives used (nature : quantities)				TONNAGES USED
1	G	BULK	225%	F. WATER	+ 2% $CACL_2$	(200 BBLS)		72 T
2				(40 m^3)				T
3								T

CARACTERISTICS OF SLURRIES		S.G.	P.V.	Y.V.	VISCOSIMETER READINGS VS R.P.M. 600	300
	1	1.87				
	2					
	3					
SPACER PLUGS	1	SW AHEAD				
	2	SW BEHIND 10 BBLS				

Slurry injection rate 437 L/MIN Displacement rate 480 L/MIN

Displacement fluid nature HEAVY MUD S.G. 150 Pumped volume 17.5m^3
Pressure at the beginning of displacement 300 at the end 850/900 at the surge 0
Estimated losses
Casing string pressuring up at 500PSI Result OK
Residual pressure (eventual) after bleeding off NO

6 - SETTING ON SPOOL

M.D. indication at the end of displacement N/A
M.D. indication after cement betting N/A setting tension on spool →
Casing string set on spool h. after the end of displacement
Spool : MFG Nominal dimensions API WP.
Suspension and seal type CASING SET W/P.G.B. ON DRILLING TEMPLATE
Additional seal (type - dimensions)
Distance between the upper part of the spool and R.K.B. RKB TOP 18 3/4 HOUSING = 89.90m
Cut casing cm above the spool

7 - CONTROL

Temperature well logging after h. setting
Cementing log after h. setting Top cement annulus → ?
Result of these logs (or enclose a copy) NO APPARENT RETURNS TO SEA BED MONITORED ON TV

Test casing string + B.O.P.(blind and pipe rams) Test pressure → 500
Packer depth :
Test result : CASING TESTED TO 500 PSI 15 MIN (WHEN BOP LANDED) WITH AX RING & BLIND RAMS - PIPE RAMS = 300 PSI - HYDRIL = 1500 PSI.

DETAILED COMPOSITION OF THE CASING STRING

F 5 c Bis/3·79

Well site	OMEO 1	Casing diameter	20"	RKB height / ground M. L.	93	Shoe meas.d depth	210m

Joint Number	Equip.t central.	Equip.t scratch	Weight per foot, grade and thread of joints / Other equipments	Unit Length	Cumulated Length	Joint Number	Equip.t central.	Equip.t scratch	Weight per foot, grade and thread of joints / Other equipments	Unit Length	Cumulate Length
SHOE JT			133 LB	12.80	12.80						
1				11.91	24.71						
2				11.89	36.60						
3				11.90	48.50						
4				11.92	60.42						
5				11.90	72.32						
6				11.91	84.23						
7				11.91	96.14						
8				11.94	108.08						
PILE JOINT			CIW 24"ODx18"ID	12.29	120.37						
TOP 18 3/4 WELLHEAD HOUSING/RKB = 89.90M				89.90							
SHOE AT 210M											
FLOAT AT 204M											

THE DETAILED COMPOSITION OF THE CASING STRING SHOULD BE GIVEN :

- EITHER from top to bottom. For the upper joint, the length under RKB will only be considered. So, each cumulated length will be the RKB Measured Depth at the bottom of each corresponding joint.
- OR from bottom to top, beginning by the shoe. So the RKB Measured Depth at the bottom of each joint will be the difference between the shoe Measured Depth and the cumulated length at the corresponding joint. The composition of the extension string should be detailed.

Imp. 4983 A SNEA(P) 9596004023

CASING AND CEMENTING REPORT

F5a Bis

WELL (Country)	RIG (Contractor)	R Ground / K Height / B M.L.	∅ Casing / Liner	CASING SHOE	Hanger depth (for liners) or changing ∅ casing depth :	OPERAT DATE
OMEO 1 (AUST VIC-P17	O. DIGGER ODECO)	93m	13 3/8"	Measured depth : 1310m Vertical depth :		11.11.

1 - WELL CONDITION

Open hole diameter : 17½ Depth { Vertical : / Measured : 1320 } Deviation { Mini : ° to / Maxi : ½ ° to 132

Important caving (location - average diameter.) :
AVER HOLE DIAMETER 18 1/8 UP TO 318M - HOLE WASHED OUT FROM 318M UP TO 20" SHOE.

Losses during drilling (levels, extent) NONE

Reamer runs (number) 1 Reamer at 20 m from th

Previous casing : Diameter 20" Shoe at 210m

Bo. Ps on well when running in (Type - equipment, test pressure)
18 3/4" x 10,000PSI BOP STACK - 2 P. RAMS - 1 B/S - HYDRIL 5000 PSI.

MUD CHARACTERISTICS BEFORE INJECTING SLURRY	S.G.	W.L.	P.V.	Y.V.	VISCOSIMETER READINGS Vs R.P.M. 600	300				
	1.15	14.6	8	24						

Observations VERY HIGH DILUTION UP TO 12.8m³/HOUR OF SEAWATER TO CONTROL MUD S.G. AND MIXING DEXTRID AND PAC-R TO RES TRICT BORE HOLE HYDRATION MOSTLY ON CLAYSTONE.

2 - GENERAL COMPOSITION OF CASING STRING

ELEMENT	MFG. type	∅	Weight (lb/ft) or thickness	Thread or joint type	Grade	Special corrosion ?	Inside volume l/m	Length (m)	Num of jo
SHOE	DOWELL FLOAT	13 3/8						0.80	>
COLLAR	JOINT								>
	DOWELL	13 3/8	68lb/ft	BTC	K55	--	78.08	35.56	
	DOWELL							0.50	
JOINTS	"	13 3/8	68lb/ft	BTC	K55	--	78.08	1181.64	99
18 3/4x13 3/8 FLOW THRU CASING HANGER								0.71	1
Tripping joint : LANDING STRING = R. TOOL + B.SUB + 5" HWDP							4.56	90.79	>
							TOTAL ➤	1310 m	

Drift diameter in the thickest joint 311.4mm

Maximum permissible tension 475T

Theoretical weight of the casing string : 122T In air ____ in mud : 104T

3 - EQUIPMENT OF CASING STRING

CENTRALIZERS
MGF : WEATHERFORD
TYPE : STIII
NUMBER : 4
DEPTH/RKB : 1286, 1215, 1148, 1047

SCRATCHERS
MGF :
TYPE :
NUMBER :
DEPTH/RKB :

OTHER EQUIPMENT (Description - Location)
CIW 13 3/8 SEAL ASSEMBLY L
TORQUE SCREWED INTO 13 3/8
HANGER
(TOP SEAL ASSY = 90.40m)

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4 - RUNNING CASING

Making-up of joint : UP TO TRIANGLE AVER. TORQUE 11000 lb/ft
Grease type used for threads : WEATHERFORD SEAL LUBE
Average torque to make-up the joints 11,000 lb/ft
Filling frequency EVERY 5 JOINTS
Intermediate circulation (duration - depth) AT 20" SHOE (210m) TO TAKE SLOW CONTROL RATE AT 25 AND 55 SPM

Total running time (with circulations) 14 h average rate 7.2 joints/h
Troubles during running -NO-

Bottom hole circulation : Duration 1H 05MIN Rate 1800 Pressure 370 PSI
Reciprocating : Duration Rate Amplitude
M.D. indications after stop of bottom hole circulation :
Observations : RUNNING TIME AFFECTED BY BAD WEATHER CONDITIONS (WINDS 40/45 KTS W/GUSTS UP TO 50 KTS)
FIRST 3 JOINTS BETWEEN SHOE AND FLOAT MADE UP TO 16,000 LB/FT WITH THREAD LOCKING COMPOUND.

5 - SINGLE STAGE OR FIRST STAGE CEMENTING

Service cy DOWELL SCHLUMBERGER
Mixing pump DOWELL SCHLUMBERGER
Slurry injection pump
Displacement pump(s) RIG PUMP EMSCO D1350

Beginning of slurry making at 22.05 (10.11.82) h
End of slurry making at 23.20 (10.11.82) h.
End of displacement at 00.35 (11.11.82) h.
Pressure released in casing at 01.00 (11.11.82) h.

	Nature or class of cements	Sacks or bulk	Cement weight increase %	Water and additives used (nature : quantities)	TONNAGES USED
1	"G"	BULK	CAL +	F.W. + 0.1 GAL/SXD80 + 0.03 GAL/SX D81	80T T
2			20% EXCESS		T
3					T

CARACTERISTICS OF SLURRIES		S.G.	P.V.	Y.V.	VISCOSIMETER READINGS VS R.P.M. 600	300
	1	1.89				
	2					
	3					
SPACER PLUGS	1	AHEAD = 10 BBLS/F.W.				
	2	BEHIND = 12 BBLS/F.W.				

Slurry injection rate 760 L/MIN LAST 21.4 M^3 AT 825 L/MIN Displacement rate 68 M^3 AT 1800 L

Displacement fluid nature MUD S.G. 1.15 Pumped volume 91.83M^3

Pressure at the beginning of displacement 400PSI at the end 1400PSI at the surge 0
Estimated losses PARTIAL LOSSES THEN NO RETURNS AFTER 85M^3 PUMPED
Casing string pressuring up at 2000 PSI Result OK
Residual pressure (eventual) after bleeding off NO

6 - SETTING ON SPOOL

M.D. indication at the end of displacement N/A
M.D. indication after cement betting N/A setting tension on spool → T
Casing string set on spool N/A h. after the end of displacement
Spool : MFG Nominal dimensions API WP.
Suspension and seal type CIW CASING HANGER - LOW TORQUE SEAL ASSY 10,000 PSI
Additional seal (type - dimensions)
Distance between the upper part of the spool and R.K.B. RKB TOP 13 3/8 HANGER = 90.78M
Cut casing cm above the spool

7 - CONTROL

Temperature well logging after 8 TO 9 h. setting
Cementing log after h. setting Top cement annulus → 825M m
Result of these logs (or enclose a copy) GOOD CEMENT FROM FLOAT UP TO 825M (485M)
POLLUTED CMT F/825 UP TO 595M

Test casing string + B.O.P.(blind and pipe rams) Test pressure → 2000PSI
Packer depth :
Test result : BOP'S = PIPE RAMS, CHOKE AND KILL VALVES AT 5000 PSI
HYDRIL AT 25 PSI = 15 MIN OK.

DETAILED COMPOSITION OF THE CASING STRING

F 5 c Bis/3·79

Well site	OMEO 1	Casing diameter	13 3/8"	RKB height / ground M. L.	93	Shoe meas. depth	1310M

Joint Number	Equip.† central.	Equip.† scratch	Weight per foot, grade and thread of joints / Other equipments	Unit Length	Cumulated Length	Joint Number	Equip.† central.	Equip.† scratch	Weight per foot, grade and thread of joints / Other equipments	Unit Length	Cumulated Length
SHOE			DOWELL-FLOAT	0.80	0.80	42				12.07	502.94
1			68lbs-K55-BTC	11.44	12.24	43				11.78	514.72
2	X			12.07	24.31	44				11.92	526.64
3				12.05	36.36	45				12.06	538.70
FLOAT			DOWELL FLOAT	0.50	36.86	46				11.31	550.01
4				12.00	48.86	47				11.91	561.92
5				12.05	60.91	48				12.06	573.98
6				12.06	72.97	49				11.76	585.74
7				11.90	84.87	50				12.02	597.76
8	X			12.07	96.94	51				12.08	609.84
9				12.04	108.98	52				12.02	621.86
10				11.69	120.67	53				11.78	633.64
11				11.98	132.65	54				12.07	645.71
12				10.87	143.52	55				12.07	657.78
13				11.84	155.36	56				11.95	669.73
14	X			12.07	167.43	57				12.07	681.80
15				12.08	179.51	58				12.03	693.83
16				12.07	191.58	59				11.86	705.69
17				11.82	203.40	60				11.92	717.61
18				12.07	215.47	61				12.07	729.68
19				11.92	227.39	62				11.74	741.42
20				12.06	239.45	63				11.78	753.20
21				11.93	251.38	64				11.91	765.11
22	X			11.94	263.32	65				12.08	777.19
23				11.89	275.21	66				12.08	789.27
24				12.02	287.23	67				12.04	801.31
25				12.00	299.23	68				11.72	813.03
26				12.01	311.24	69				12.07	825.10
27				12.02	323.26	70				11.97	837.07
28				12.08	335.34	71				12.05	849.12
29				11.73	347.07	72				12.02	861.14
30				12.07	359.14	73				12.01	873.15
31				12.07	371.21	74				11.71	884.86
32				12.07	383.28	75				11.94	896.80
33				12.07	395.35	76				12.07	908.87
34				12.07	407.42	77				12.07	920.94
35				11.75	419.17	78				11.99	932.93
36				11.79	430.96	79				12.07	945.00
37				12.00	442.96	80				11.43	956.43
38				11.99	454.95	81				12.07	968.50
39				11.88	466.83	82				11.85	980.35
40				12.00	478.83	83				11.89	992.24
41				12.04	490.87	84				11.87	1004.11

THE DETAILED COMPOSITION OF THE CASING STRING SHOULD BE GIVEN :

- EITHER from top to bottom. For the upper joint, the length under RKB will only be considered. So, each cumulated length will be the RKB Measured Depth at the bottom of each corresponding joint.

- OR from bottom to top, beginning by the shoe. So the RKB Measured Depth at the bottom of each joint will be the difference between the shoe Measured Depth and the cumulated length at the corresponding joint. The composition of the extension string should be detailed.

Imp. 4863 A SNEA(P) 956004023

DETAILED COMPOSITION OF THE CASING STRING

F 5 c Bis/3·79

Well site	OMEO 1	Casing diameter	13 3/8	RKB height / ground M. L.	93	Shoe meas. depth	1310M

Joint Number	Equip.† central.	Equip.† scratch	Weight per foot, grade and thread of joints / Other equipments	Unit Length	Cumulated Length
85				12.08	1016.19
86				11.81	1028.00
87				11.95	1039.95
88				12.07	1052.02
89				11.99	1064.01
90				11.97	1075.98
91				12.07	1088.05
92				11.89	1099.94
93				12.00	1111.94
94				11.35	1123.29
95				11.81	1135.10
96				12.08	1147.18
97				11.80	1158.98
98				11.96	1170.94
99				12.00	1182.94
100				11.98	1194.92
101				11.80	1206.72
102				11.78	1218.50
			18 3/4" x 13 3/8" CIW CASING HANGER	0.71	1219.21
			C. HANGER R. TOOL	0.54	1219.75
			XOVER	0.61	1220.36
			6 S.I. BUMPER SUB	5.32	1225.68
			XOVER	0.96	1226.64
			9 HWDP 50 lbs/ft	83.50	1310.14
			1 5" GRADE "G" PUP JT	4.57	1314.71
			STICK UP	4.71	1310.00

Joint Number	Equip.† central.	Equip.† scratch	Weight per foot, grade and thread of joints / Other equipments	Unit Length	Cumulated Length

THE DETAILED COMPOSITION OF THE CASING STRING SHOULD BE GIVEN :

- EITHER from top to bottom. For the upper joint, the length under RKB will only be considered. So, each cumulated length will be the RKB Measured Depth at the bottom of each corresponding joint.
- OR from bottom to top, beginning by the shoe. So the RKB Measured Depth at the bottom of each joint will be the difference between the shoe Measured Depth and the cumulated length at the corresponding joint. The composition of the extension string should be detailed.

Imp. 4993 A SNEA(P) 9680004023

CASING AND CEMENTING REPORT

F5a Bis

WELL (Country)	RIG (Contractor)	R Ground ☐ K Height B M.L. ☒	ø Casing ☒ Liner ☐	CASING SHOE	Hanger depth (for liners) or changing ø casing depth :	OPERATI DATE
OMEO 1 AUSTRALIA (VIC-P17)	O. DIGGER (ODECO)	93M	9 5/8	Measured depth : 2606m Vertical depth :		22.12.8 23.12.8

1 - WELL CONDITION

Open hole diameter : 12¼ Depth { Vertical : / Measured : PBTD-2674m } Deviation { Mini : ½ ° to 1572 / Maxi : 3/4 ° to 2521

Important caving (location - average diameter..) :
1310-2100 16½"-2100-2275 14"-2275-2325 16"-2325-2350 15"-2350-2250 16"

Losses during drilling (levels, extent) 80m³ PARTIAL LOSSES OCCURED OVER 5 DAYS PRIOR TO RUNNING CASING.

Reamer runs (number) 5 Reamer at 9 m from the
Previous casing : Diameter 13 3/8" Shoe at 1310

Bo. Ps on well when running in (Type - equipment, test pressure) 18 3/4" CAMERON TYPE "U" 2 PIPE RAMS 5", 10,000PSI-BLIND SHEAR ARM AND HYDRIL 18 3/4" 5,000PSI

MUD CHARACTERISTICS BEFORE INJECTING SLURRY	S.G.	W.L.	P.V.	Y.V.	VISCOSIMETER READINGS Vs R.P.M. 600	300				
	1.20	3.4	27	36						

Observations ADDITION OF GEL AND SOLTEX TO POLYMER MUD IN ORDER TO CONTROL CAVING HOLE BEFORE RUNNING CASING. SIDE TRACKING HAD BEEN ATTEMPTED 1 TIME DUE TO RFT LOST IN HOLE AT 2960M - SECOND SIDE TRACK IN 12¼" HOLE IN PROGRESS WHEN ABORTED TO RUN CASING

2 - GENERAL COMPOSITION OF CASING STRING

ELEMENT	MFG. type	ø	Weight (lb/ft) or thickness	Thread or joint type	Grade	Special corrosion ?	Inside volume l/m	Length (m)	Numb of joi
SHOE	BAKER FLOAT	9 5/8"	47	BUTT.	N80			.60	X
COLLAR	BAKER	9 5/8"	47	BUTT.	N80			.60	X
JOINTS		9 5/8"	47	BUTT.	N80		38.19	2514.55	214
HANGER	CAMERON	18 3/4 x 9 5/8						0.71	1
Tripping joint : HWDP FOR RUNNING STRING							4.56	90.16	X
							TOTAL ➤	2606.61 m	

Drift diameter in the thickest joint 8.599 INCHES
Maximum permissible tension 494 TONS
Theoretical weight of the casing string : In air 176 TONS in mud : 150 TONS

3 - EQUIPMENT OF CASING STRING

CENTRALIZERS
MGF : WEATHERFORD
TYPE : ST III
NUMBER : 2
DEPTH/RKB : 2600m
2580m

SCRATCHERS
MGF :
TYPE :
NUMBER :
DEPTH/RKB :

OTHER EQUIPMENT
(Description - Location)
9 5/8x18 3/4 CIW LOW TORQUE SEAL ASSMY. SET IN TOP 9 5/ HANGER.

Imp. 4996 B SNEA(P) - RGM 969.004.013 - F5abis/2-78/11-80

4 - RUNNING CASING

Making-up of joint : TO TRIANGLE
Grease type used for threads : WEATHERFORD LUBE SEAL
Average torque to make-up the joints : 10,000ft/lbs
Filling frequency : EVERY 5 JOINTS COMPLETE FILL
Intermediate circulation (duration - depth) : 0:30MIN - 1306m

Total running time (with circulations) 10 h 54m average rate 19 joints/h
Troubles during running : NONE

Bottom hole circulation : Duration 2hr 25 min Rate 1152 lts/min Pressure 300 psi
Reciprocating : N/A Duration Rate Amplitude
M.D. indications after stop of bottom hole circulation :
Observations : NO MUD LOSS WHILE RUNNING OR CIRCULATING CASING. HOLE IN GOOD CONDITION.

5 - SINGLE STAGE OR FIRST STAGE CEMENTING

Service cy : DOWELL SCHLUMBERGER
Mixing pump : DOWELL SCHLUMBERGER 2"x3"x11"cont.
Slurry injection pump : DOWELL SCHLUMBERGER 4½"x3 3/4"
Displacement pump(s) : RIG PUMP EMSCO D-1350

Beginning of slurry making at 0538hrs. 23.12.82 h
End of slurry making at 0658hrs. 23.12.82 h
End of displacement at 0845hrs. 23.12.82 h
Pressure released in casing at 0900hrs. 23.12.82 h

	Nature or class of cements	Sacks or bulk	Cement weight increase %	Water and additives used (nature : quantities)	TONNAGES USED
1	'G'NEAT	BULK		2 GAL/SX D73+.15 GAL/SX D80+.02 GAL/SX D109	92
2				+4.60 GAL/SX FRESHWATER	
3					

CARACTERISTICS OF		S.G.	P.V.	Y.V.	VISCOSIMETER READINGS VS R.P.M. 600	300
SLURRIES	1	1.90				
	2					
	3					
SPACER PLUGS	1					
	2					

Slurry injection rate 800lts/min Displacement rate 987-855 Lts/min

Displacement fluid nature POLYMER MUD SG 1.20 Pumped volume 95m³

Pressure at the beginning of displacement 200 at the end 1100 at the surge
Estimated losses 31.79m³ PARTIAL DURING DISPLACEMENT
Casing string pressuring up at 3,000PSI Result HELD 15MIN OK
Residual pressure (eventual) after bleeding off NONE

6 - SETTING ON SPOOL

M.D. indication at the end of displacement
M.D. indication after cement betting setting tension on spool →
Casing string set on spool h. after the end of displacement
Spool : MFG Nominal dimensions API WP
Suspension and seal type
Additional seal (type - dimensions)
Distance between the upper part of the spool and R.K.B.
Cut casing cm above the spool

7 - CONTROL

Temperature well logging after 9.00 h. setting
Cementing log after h. setting Top cement annulus → 2179
Result of these logs (or enclose a copy) INDICATIONS OF CEMENT UP TO 2125M
GOOD CMT TOP AT 2179M.

Test casing string + B.O.P.(blind and pipe rams) Test pressure → 3000psi
Packer depth :
Test result :

DETAILED COMPOSITION OF THE CASING STRING

F 5 c Bis/3·79

Well site	OMEO 1	Casing diameter	9 5/8	RKB height / ground M. L.	93m	Shoe meas. depth	2606.61

Joint Number	Equip.† central.	Equip.† scratch	Weight per foot, grade and thread of joints / Other equipments	Unit Length	Cumulated Length	Joint Number	Equip.† central.	Equip.† scratch	Weight per foot, grade and thread of joints / Other equipments	Unit Length	Cumulated Length
SHOE				.60	.60	42			47-N-80-BTC	11.75	495.31
1	X		47-N80-BTC	11.93	12.53	43			"	11.78	507.09
2	X		"	11.91	24.44	44			"	11.79	518.88
FC			"	.60	25.04	45			"	11.64	530.52
3				11.92	36.96	46				11.86	542.38
4				11.84	48.80	47				11.71	554.09
5				11.82	60.62	48				11.91	566.00
6				11.83	72.45	49				11.93	577.93
7				11.78	84.23	50				11.64	589.57
8				11.54	95.77	51				11.95	601.52
9				11.83	107.60	52				11.78	613.30
10				11.81	119.41	53				11.75	625.05
11				11.94	131.35	54				11.65	636.70
12				11.72	143.07	55				11.74	648.44
13				11.75	154.82	56				11.75	660.19
14				11.85	166.67	57				11.76	671.95
15				11.64	178.31	58				11.80	683.75
16				11.73	190.04	59				11.81	695.56
17				11.92	201.96	60				11.96	707.52
18				11.83	213.79	61				11.87	719.39
19				11.64	225.43	62				11.79	731.18
20				11.80	237.23	63				11.86	743.04
21				11.75	248.98	64				11.71	754.75
22				11.81	260.79	65				11.78	766.53
23				11.91	272.70	66				11.82	778.35
24				11.72	284.42	67				11.76	790.11
25				11.84	296.26	68				11.82	801.93
26				11.76	308.02	69				11.56	813.49
27				11.72	319.74	70				11.74	825.23
28				11.68	331.42	71				11.41	836.64
29				11.72	343.14	72				11.74	848.38
30				11.85	354.99	73				11.73	860.11
31				11.71	366.70	74				11.55	871.66
32				11.77	378.47	75				11.80	883.46
33				11.90	390.37	76				11.57	895.03
34				11.84	402.21	77				11.85	906.88
35				11.15	413.36	78				11.85	918.73
36				11.80	425.16	79				11.54	930.27
37				11.95	437.11	80				11.87	942.14
38				11.55	448.66	81				11.84	953.98
39				11.40	460.06	82				11.80	965.78
40				11.68	471.74	83				11.20	976.98
41				11.82	483.56	84				11.90	988.88

THE DETAILED COMPOSITION OF THE CASING STRING SHOULD BE GIVEN :

- **EITHER** from top to bottom. For the upper joint, the length under RKB will only be considered. So, each cumulated length will be the RKB Measured Depth at the bottom of each corresponding joint.

- **OR** from bottom to top, beginning by the shoe. So the RKB Measured Depth at the bottom of each joint will be the difference between the shoe Measured Depth and the cumulated length at the corresponding joint. The composition of the extension string should be detailed.

Imp. 4983 A SNEA(P) - 958004023

DETAILED COMPOSITION OF THE CASING STRING

F 5 c Bis/3·79

Well site	OMEO 1	Casing diameter	9 5/8	RKB height/ground M. L.	93m	Shoe meas. depth	2606.61

Joint Number	Equip.† central.	Equip.† scratch	Weight per foot, grade and thread of joints / Other equipments	Unit Length	Cumulated Length	Joint Number	Equip.† central.	Equip.† scratch	Weight per foot, grade and thread of joints / Other equipments	Unit Length	Cumulate Length
85			47-N80-BTC	11.56	1000.44	128			47-N80-BTC	11.78	1505.2
86				12.04	1012.48	129				11.76	1517.0
87				11.77	1024.25	130				11.71	1528.7
88				11.80	1036.05	131				11.82	1540.5
89				11.70	1047.75	132				11.61	1552.1
90				11.02	1058.77	133				11.87	1564.0
91				11.75	1070.52	134				11.79	1575.8
92				11.82	1082.34	135				11.71	1587.5
93				11.74	1084.08	136				11.78	1599.3
94				11.91	1105.99	137				11.94	1611.2
95				11.80	1117.79	138				11.89	1623.1
96				11.76	1129.55	139				11.81	1634.9
97				11.69	1141.24	140				11.87	1646.8
98				11.71	1152.95	141				11.67	1658.5
99				11.70	1164.65	142				11.23	1669.7
100				11.91	1176.56	143				11.85	1681.6
101				11.83	1188.39	144				11.82	1693.4
102				11.16	1199.55	145				11.80	1705.2
103				11.82	1211.37	146				11.84	1717.0
104				11.88	1223.25	147				11.72	1728.7
105				11.39	1234.64	148				11.77	1740.5
106				11.89	1246.53	149				11.71	1752.2
107				11.77	1258.30	150				11.90	1764.1
108				11.50	1269.80	151				11.79	1775.9
109				11.84	1281.64	152				11.57	1787.5
110				11.77	1293.41	153				11.92	1799.4
111				11.82	1305.23	154				11.69	1811.1
112				11.77	1317.00	155				11.76	1822.8
113				11.61	1328.61	156				11.87	1834.7
114				11.81	1340.42	157				11.61	1846.3
115				11.75	1352.17	158				11.88	1858.2
116				11.70	1363.87	159				11.84	1870.0
117				11.89	1375.76	160				11.89	1881.9
118				11.87	1387.63	161				11.60	1893.5
119				11.61	1399.24	162				11.74	1905.3
120				11.66	1410.90	163				11.44	1916.7
121				11.47	1422.37	164				11.59	1928.3
122				11.87	1434.24	165				11.68	1940.0
123				12.01	1446.25	166				11.74	1951.7
124				11.77	1458.02	167				11.83	1963.6
125				11.83	1469.85	168				11.33	1974.9
126				11.84	1481.69	169				11.75	1986.6
127				11.82	1493.51	170				11.88	1998.5

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- OR from bottom to top, beginning by the shoe. So the RKB Measured Depth at the bottom of each joint will be the difference between the shoe Measured Depth and the cumulated length at the corresponding joint. The composition of the extension string should be detailed.

Imp 4893 A SNEA(P) 956004023

DETAILED COMPOSITION OF THE CASING STRING

F 5 c Bis/3·79

Well site	OMEO 1	Casing diameter	9 5/8	RKB height/ground M. L.	93m	Shoe meas. depth	2606.61

Joint Number	Equip.† central.	Equip.† scratch	Weight per foot, grade and thread of joints / Other equipments	Unit Length	Cumulated Length	Joint Number	Equip.† central.	Equip.† scratch	Weight per foot, grade and thread of joints / Other equipments	Unit Length	Cumulated Length
171			47-N80-BTC	11.83	2010.38	214			47-N80-BTC	11.72	2515.75
172			"	11.80	2022.19	9-5/8x18-3/4 CIW HANGER				.71	2516.46
173				11.37	2033.56	RKB TO TOP HANGER				90.15	2606.61
174				11.70	2045.26						
175				11.78	2057.04						
176				11.88	2068.92						
177				11.83	2080.75						
178				11.69	2092.44						
179				11.59	2104.03						
180				11.65	2115.68						
181				11.62	2127.30						
182				11.59	2138.89						
183				11.75	2150.64						
184				11.61	2162.25						
185				11.81	2174.06						
186				11.87	2185.93						
187				11.62	2197.55						
188				11.83	2209.38						
189				11.69	2221.07						
190				11.91	2232.98						
191				11.67	2244.65						
192				11.85	2256.50						
193				11.81	2268.31						
194				12.15	2280.46						
195				11.72	2292.18						
196				11.74	2303.92						
197				11.79	2315.71						
198				11.87	2327.58						
199				11.65	2339.23						
200				11.80	2351.03						
201				11.82	2362.85						
202				11.87	2374.72						
203				11.53	2386.25						
204				11.88	2398.13						
205				11.85	2409.98						
206				11.86	2421.84						
207				11.78	2433.62						
208				11.70	2445.32						
209				11.79	2457.11						
210				11.90	2469.01						
211				11.69	2480.70						
212				11.53	2492.23						
213				11.80	2504.03						

THE DETAILED COMPOSITION OF THE CASING STRING SHOULD BE GIVEN :

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- OR from bottom to top, beginning by the shoe. So the RKB Measured Depth at the bottom of each joint will be the difference between the shoe Measured Depth and the cumulated length at the corresponding joint. The composition of the extension string should be detailed.

Imp. 4983 A SNEA(P) 969004023

DATE OF OPERATION

CASING WITH LINER SURVEY

F5 d4/ (Tentati

WELL (Country)	RIG (Contractor)	Table ground ☐ Height M.L. ☒	LAST CASING (at the level of the anchor)		LINER	Vertical ☒ Directional ☐
			Ø	Grade	Ø	Anchor de
OMEO 1	OCEAN DIGGER	93m	9-5/8	N80	7"	2507
(AUSTRALIA)	(ODECO)		Shoe depth 2606 m	Thickness 47 lb/ft	Well depth 2985 m	Shoe dept 2984

1 WELL CONDITION BEFORE RUNNING IN THE LINER

Ø Of open hole drilling 12¼ AND 8½

Phase duration : 12¼ SECTION = 37 DAYS; 8½ HOLE = 5 DAYS — days :

Quality of casing cementing at the anchoring level — GOOD ☒ MEDIUM ☐ BAD ☐

INSIDE CALIPER From	To	Ø	REAMING From	To	REAMER LOCATION m. from bit
2606	2660	23"	2606	2985	1 & 9 m
2660	2985	8½"			

DEVIATION Measured depth	Vertical depth	Incl. (0°)	Az dire
At the theoretical depth of slurry			
At the liner hanger anchor 2523		3 Deg	
At the casing shoe in place 2648		2 Deg	
At the liner shoe 2984		1 Deg	N 7
Bottomhole 2984		1 Deg	N 7

MUD LOSSES DURING DRILLING From	to	m³	LCM

Formation tests Depth	equiv. d
2670	1.44

BOPS Type - Equipment - Date of last test	
18¾ CAMERON TYPE 'U' - 2 PIPE RAMS - 10,000 PSI - BLIND RAMS ARM AND HYDRIL 18¾ x 5000 PSI	5,0

2 EQUIPMENT OF THE LINER

CENTRALIZERS — Make: WEATHERFORD; Type: ST II; Number: 7

SCRATCHERS — Make: NONE; Type: ; Number:

Other equip: PACKER TIN; TIE BACK SI

N° of JOINT	NUMBER	N° of JOINT	NUMBER	N° of JOINT	NUMBER	N° of JOINT	NUMBER
40	1	4	1				
39	1	2	1				
38	1						
8							
6							

In case you have used a liner specialist service give :

Company T.I.W — Name of operator PAUL OLSEN

OBSERVATIONS

DRILLING 12¼" HOLE TO 2985m - LOST RFT TOOL - PLUGGED WELL WITH CEMENT TO 2660 - SIDE TRACKING WITH 8½" BIT TO 2985m - 12¼" OPEN HOLE PACKING OFF - STOP TO DRILL AND RUN LINER - 12¼" SECTION WASHED TO 23"

NAME OF SUPERVISOR : MICHEL — SIGNATURE

3 | LINER

SYMBOLS		SECTION	DEPTH
Receptacle	PACKER CONNECTION		
P B R			
Collar			
Packer			
Tie-back			2498.80
Receptacle	LINER		
Setting collar			2500 (PACKER SEAL)
Seal			
Hanger			2507 (SLIPS)
Swivel Casing Shoe			
			2947.70
Collar			2984
Shoe			

SETTING TOOL

Maker : TIW ø 6½

Type : "L"

Total length : 4.9 m

Tail pipe length : 2.82 m

Length between packer and wiper plug : 0.45

LINER SETTING STRING :

Setting tool length above liner 2.08

Liner total length 480.83

Length and Ø of pipes 5" DP 2506.09

TOTAL 2989.00

Length above rotary table 5,00 m

Liner shoe at : 2984 m

5 | LINER COMPOSITION

ELEMENTS	MAKE - TYPE - GRADE - WEIGHT - THREAD	O.D.	I.D.	l/m	LENGTH	JOINTS
Shoe	T.I.W				0.76	
3 CASINGS		177.8	159.4	19.95	35.54	38
LANDING COLLAR	T.I.W				0.30	
37 CASINGS	7" 26 lb/ft N80 BUTRESS	177.8	159.4	19.95	439.53	37
HANGER	T.I.W 7" 29 lb/ft N80 BUTRESS	177.8	157.1	19.38	1.62	
EXTENSION NIPPLE:	T.I.W 7" 29 lb/ft N80 BUTRESS	177.8	157.1	19.38	3.07	
PACKER +						
TIE BACK SLEEVE:	T.I.W 7" 29 lbs/ft N80 BUTRESS	177.8	157.1	19.38	4.39	
RUNNING TOOL	T.I.W 5" (ABOVE THE TIE BACK SLEEVE)	5"	3"	4.56	2.08	
5" EXTENSION BELOW ROTARY TABLE		5"	3½	9.16	2496.71	
				TOTAL	2984 m	

Ø of maximum drift CASING STRING = 153.9 mm

Maximum permissible strength 295 10^3

Theoretical liner weight in the air : 18.7 T In mud 15.8 T In slurry 14.1 T

ATE OF OPERATION

CEMENTING SURVEY

LINER PACKER TOGETHER

P3 0 4/79 (Tentatif)

WELL (Country)	RIG (Contractor)	Mud contractor (Name of operator)	LINER		
OMEO 1	OCEAN DIGGER	BAROID	Ø 7	PVT anchoring depth: 2507	PVT shoe depth: 2984
AUSTRALIA	ODECO		Well depth 2985	PMT anchoring depth: 2507	PMT shoe depth: 2984

1 RHEOLOGY OF THE FLUIDS USED

	TYPE OF FLUID	d	f	VP	YV	VISCOSIMETER READING ACCORDING TO RPM 600	300	GEL O	GEL 10	SOLID
WELL MUD	At the end of drilling	1.20	5.5	40	22			8	30	9%
	Before the liner	1.20	5.5	40.5	25			7	33	9%
	Before injecting slurry	1.19	6.4	31	18			7	24	9%
SPACER	Test									
	Top	1.30	7	34	14			4	12	10%
	Bottom									

SLURRIES		Class of cement	Pumping time								
	Lab. test	G	+5.00HRS	1.90	SLURRY=760 LIT/TON			WATER = 450 LIT/TON			
	Injection	G			IDEM LABORATORY TEST						

2 CEMENTS AND ADDITIVES

CLASS OF CEMENT	SACKS BULK	T. WEIGHT	WATER USED Nature	WATER USED Litres	SLURRY VOLUME m3	ADDITIVES IN % OF DRY CEMENT WEIGH Type	%	Type
G	BULK	28	FRESH	12610	21,3M3	D73(FLAC)	0.02	
						D80(DISPERSANT)	0,013	
						D109(RETARD)	0.002	

3 RUNNING THE LINER

Pipe make up method : LAMB TONG

Type of grease used for threads : API

Average torque to make up the joints : 1100 M-DA-N

Pipe filling frequency : EVERY 5 JOINTS - EVERY 10 STAND OF 5" DP (AUTO FLOAT S

Running velocity : in the casing : 3 MIN / JOINT min./length DONT WORK)

in the ground : 5 MIN / JOINT min./length

Total running time (with circulation)

DETAILED COMPOSITION OF THE CASING STRING

F 5 c Bis/3·79

Well site	OMEO 1	Casing diameter	LINER 7"	RKB height / ground M. L.		Shoe meas.d depth	

Joint Number	Equip.t central.	Equip.t scratch	Weight per foot, grade and thread of joints / Other equipments	Unit Length	Cumulated Length	Joint Number	Equip.t central.	Equip.t scratch	Weight per foot, grade and thread of joints / Other equipments	Unit Length	Cumulated Length
5" LANDING STRING + BUMPER SUB					2496.71	38	1			11.56	2959.35
LINER RUNNING TOOL				2.08	2498.79	39	1			11.94	2971.29
TIE BACK SLEEVE + PACKER				4.39	2503.18	40	1			11.95	2983.24
EXTENSION NIPPLE				3.07	2506.25				SHOE	0.76	2984.00
HANGER				1.62	2507.87						
1				11.38	2519.25						
2	1			12.24	2531.49						
3				11.79	2543.28						
4	1			11.76	2555.04						
5				11.50	2566.54						
6	1			11.83	2578.37						
7				11.80	2590.17						
8	1			12.12	2602.29						
9				12.03	2614.32						
10				11.91	2625.23						
11				11.92	2638.15						
12				11.98	2650.13						
13				12.10	2662.23						
14				11.69	2673.92						
15				11.65	2685.57						
16				12.18	2697.75						
17				11.44	2709.19						
18				11.47	2720.66						
19				11.57	2732.23						
20				11.92	2744.15						
21				12.05	2756.20						
22				12.03	2768.23						
23				11.74	2779.97						
24				12.14	2792.11						
25				11.99	2804.10						
26				11.66	2815.76						
27				12.34	2828.10						
28				11.60	2839.70						
29				11.60	2851.30						
30				12.16	2863.46						
31				12.15	2875.61						
32				11.99	2887.60						
33				11.93	2899.53						
34				12.02	2911.55						
35				11.91	2923.46						
36				11.95	2935.41						
37				11.99	2947.40						
			LANDING COLLAR	0.30	2947.70						

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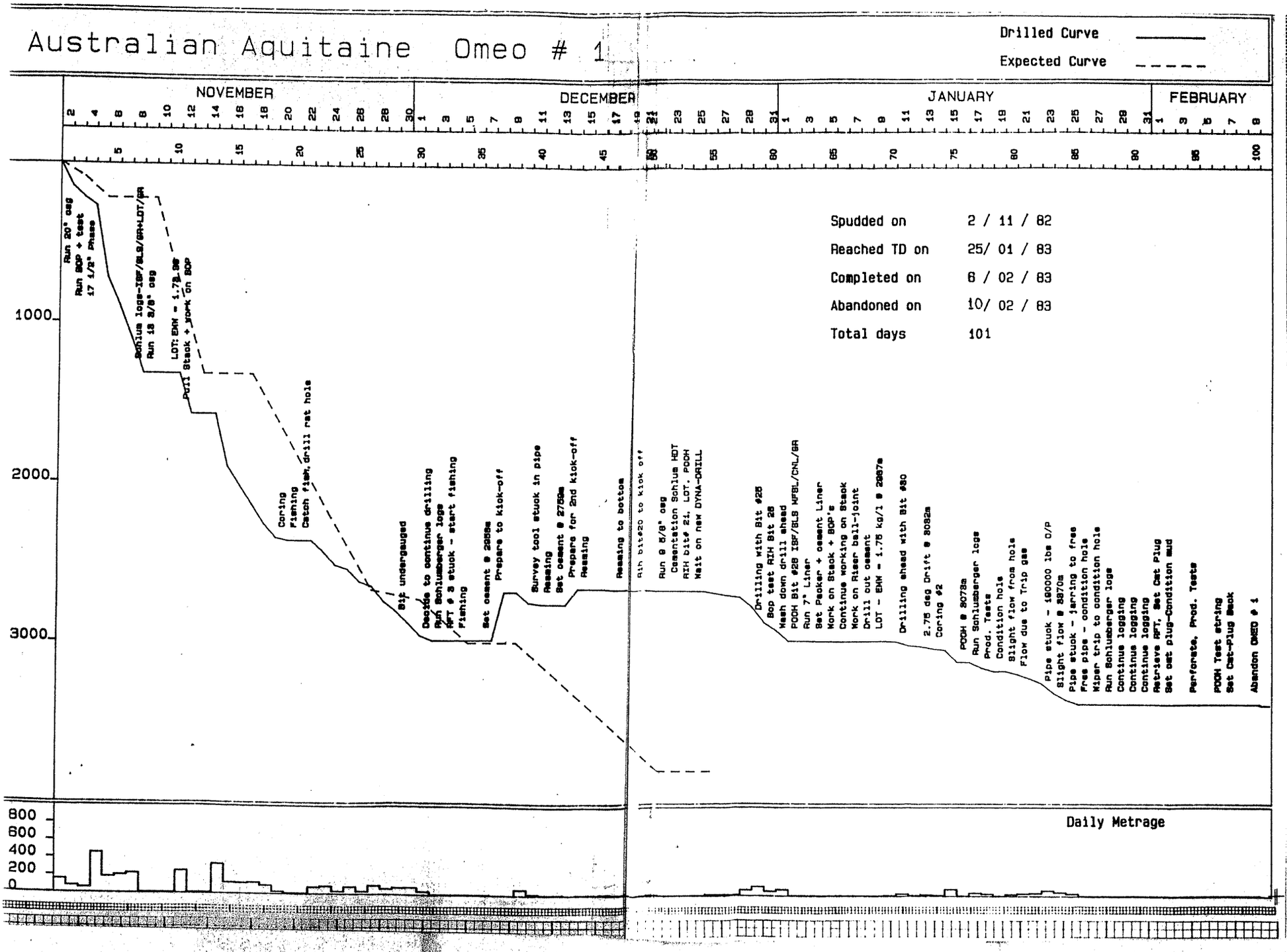
- OR from bottom to top, beginning by the shoe. So the RKB Measured Depth at the bottom of each joint will be the difference between the shoe Measured Depth and the cumulated length at the corresponding joint. The composition of the extension string should be detailed.

Imp. 4983 A SNEA(P) 968004023

Australian Aquitaine Omeo # 1



elf aquitaine

TIME DISTRIBUTION

F6 bis / 12-80

OPERATOR	COUNTRY	WELL	RIG	CONTRACTOR	MONTH/YEAR
AAP	AUSTRALIA	OMEO 1	OCEAN DIGGER	ODECO	NOVEMBER '82

DAY	Number of day from start drilling	D MOVING			F DRILLING CASING				G FORMATION SURVEYS				A INTERRUPTION OF OPERATIONS UNDER F or G				C COMPLETION AND PLUGGING			
		D_1	D_2	D_3	F_1	F_2	F_3	F_4	G_1	G_2	G_3	G_4	A_1	A_2	A_3	A_4	C_1	C_2	C_3	C_4
1	1D	3			UNDER WAY TO OMEO 1 AT 2100 HRS.															
2	1	20			2	2														
3	2				3	2	1.5	17.5					26" PHASE							
4	3				3		1	20												
5	4				19		5													
6	5				16	5	3						17½" PHASE							
7	6				19		5													
8	7				17		2					5								
9	8							8.5				15.5								
10	9							24												
11	10							24												
12	11				16		2	3								3				
13	12															24				
14	13									12¼" PHASE						24				
15	14				16.5		7.5													
16	15				8.5											15.5				
17	16				14											10				
18	17				17.5											6.5				
19	18				13.5		1.5			9										
20	19								3	17			4							
21	20												24							
22	21									10			14							
23	22				21						3									
24	23				23		1													
25	24				6.5	10	7.5													
26	25				23		1													
27	26				6.5	13	4.5													
28	27				20.5		3.5													
29	28				20	3	1													
30	29				16.5	6				1.5										
31																				
TOTAL																				

TIME OF SIDE-TRACK DRILLING				TIME OF LOGGING BY A FISHING JOB	

Causes of side-track:
- Fishing job unsolved ☐
- Accidental on Plug ☐
- Correction of drill-path ☐

N.B. : *1) Add an asterisk to each following day times :*
- *Time spent on F1, F2, F3 for technical side-tracks, until the initial depth of the old hole is reached.*
- *Time spent on G4 for logging necessitaded by a fishing job.*

2) Side-track drilling further to a change in the geological target is considered as a new-hole, whose the name changes (add .G to the old one). A new form is open up from the first day of the side track.

Imp. 4807 A SNEA(P) - 959.004.007

elf aquitaine

TIME DISTRIBUTION

F6 bis / 12-80

OPERATOR	COUNTRY	WELL	RIG	CONTRACTOR	MONTH/YEAR
AAP	AUSTRALIA	OMEO 1	OCEAN DIGGER	ODECO	DECEMBER '82

DAY	Number of day from start drilling	D MOVING			F DRILLING CASING				G FORMATION SURVEYS				A INTERRUPTION OF OPERATIONS UNDER F or G				C COMPLETION AND PLUGGING			
		D_1	D_2	D_3	F_1	F_2	F_3	F_4	G_1	G_2	G_3	G_4	A_1	A_2	A_3	A_4	C_1	C_2	C_3	C_4
1	30				22	1.5	.5													
2	31				10.5	11.5	.5			1.5										
3	32				.5							23.5								
4	33											24								
5	34											14	10							
6	35												24							
7	36												24							
8	37												24							
9	38					12¼" PHASE							24							
10	39												24							
11	40												24							
12	41												15			9				
13	42												24							
14	43												24							
15	44												24							
16	45												12.5			11.5				
17	46												24							
18	47												24							
19	48												23			1				
20	49												24							
21	50												24							
22	51												24							
23	52												24							
24	53												24							
25	54					8½" PHASE							21			3				
26	55					*8.5	*3.5						12							
27	56				*9.5	*8.5	*6													
28	57				*16.5		*7.5													
29	58				*8.5	*10.5	*4.5									.5				
30	59				*19	*.5	*4.5													
31	60				*9	*8	* 7													
TOTAL																				

TIME OF SIDE-TRACK DRILLING				TIME OF LOGGING BY A FISHING JOB	

Causes of side-track:
- Fishing job unsolved ☐
- Accidental on Plug ☐
- Correction of drill-path ☐

N.B. : *1) Add an asterisk to each following day times :*
- *Time spent on F1, F2, F3 for technical side-tracks, until the initial depth of the old hole is reached.*
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Imp. 4807 A SNEA(P) - 959.004.007

TIME DISTRIBUTION

F6 bis / 12-80

OPERATOR	AREA	WELL	RIG	CONTRACTOR	MONTH/YEAR
AAP	AUSTRALIA	OMEO 1	OCEAN DIGGER	ODECO	JANUARY '83

	DRILLING DEPTH AT 0 HOUR	D			F				G				A INTERRUPTION OF OPERATIONS UNDER F or G				C COMPLETION AND PLUGGING			
		D_1	D	D	F	F_2	F_3	F_4	G_1	G_2	G_3	G_4	A_1	A_2	A_3	A_4	C_1	C_2	C_3	C_4
1	61			-	*19.5	*1.5	*2									1				
2	62				* .5			*6.5				*17								
3	63							24												
4	64							20.5								3.5				
5	65							17								7				
6	66							17								7				
7	67						5.5						18.5							
8	68	END OF PHASE			8½		23	1												
9	69	PHASE 6"			3	10	1.5	9.5												
10	70				12	11	1													
11	71				7.5	15	1.5													
12	72				6	10	8													
13	73				12.5	7	4.5													
14	74					6	2.5		3	12.5										
15	75				18.5		5.5													
16	76				13	8.5	2.5													
17	77				9	1	4									10				
18	78				13	2						9								
19	79											24								
20	80				7							15.5	1.5							
21	81				22	2														
22	82				15	8.5	.5													
23	83				21		3													
24	84				13.5	5.5	5													
25	85				6.5	5	11						1.5							
26	86												24							
27	87											14.5	9.5							
28	88											24								
29	89											24								
30	90											24								
31	91											24								
TOTAL																				

TIME OF SIDE-TRACK DRILLING				TIME OF LOGGING BY A FISHING JOB	

Causes of side-track:
- Fishing job unsolved ☐
- Accidental on Plug ☐
- Correction of drill-path ☐

N.B. : *1) Add an asterisk to each following day times :*
- *Time spent on F1, F2, F3 for technical side-tracks, until the initial depth of the old hole is reached.*
- *Time spent on G4 for logging necessitaded by a fishing job.*

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Imp 4807 A SNEA(P) - 959.004.007

TIME DISTRIBUTION

F6 bis / 12-8

AAP	AUSTRALIA	OMEO 1	RIG OCEAN DIGGER	CONTRACTOR ODECO	MONTH/YEAR FEBRUARY '8

		D			F				G				A INTERRUPTION OF OPERATIONS UNDER F or G				C COMPLETION AND PLUGGING			
		D_1	D_2	D_3	F_1	F_2	F_3	F_4	G_1	G_2	G_3	G_4	A_1	A_2	A_3	A_4	C_1	C_2	C_3	
1	92				END 6" PHASE							13						11		
2	C1																24			
3	C2																24			
4	C3																24			
5	C4						PHASE C										24			
6	C5																18	6		
7	C6																	24		
8	C7																	19	1.5	3
9	C8	14																10		
10	C9	6.5																		
11																				
12																				
13																				
14																				
15																				
16																				
17																				
18																				
19																				
20																				
21																				
22																				
23																				
24																				
25																				
26																				
27																				
28																				
29																				
30																				
31																				
TOTAL																				

TIME OF SIDE-TRACK DRILLING

TIME OF LOGGING - BY A FISHING JOB

Causes of side-track
- Fishing job unsolved ☐
- Accidental on Plug ☐
- Correction of drill-path ☐

N.B. : *1) Add an asterisk to each following day times :*
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2) Side track drilling further to a change in the geological target is considered as a new-hole, whose the name changes (add .G to the old one). A new form is open up from the first day of the side track.

Imp. 4807 A SNEA(P) - 959 004 007

[redacted] GENERA[redacted]

[redacted] DRILLING [redacted]										[redacted] PERFORMANCES					[redacted] PARAMETERS				[redacted] MUD				[redacted] DULL BIT CONDITION				[redacted]	[redacted]	[redacted] TURBODRILLED			
Run number	Operation	Drive	Bit type	Bit Diameter	Manufacturer	Code IADC	Serial number	Nozzles 1 /32	Nozzles 2 /32	Nozzles 3 /32	Operation starting depth	Footage in this operation	Drilling time (hours)	Drilling rate	Deviation	Weight on bit	R.P.M.	Flow rate	Pressure	Density (mud weight)	Plastic Viscosity (cp)	Solid content (%)	Water loss (cc)	T	B	G	Observations on grading	GEOLOGICAL FORMATION	Reason for tripping	Type of turbodrill	Turbodrill diameter	Turbodrilled footage	Total time (hours)
1U	F	R	T	26"	SMI	DGH	SAS656	24	24	24	93	127	5	23.3	½	5/10	85	3400	1300	SEA WATER WITH HI VIS PILLS				2	2	I			EX				
2	RA	R	T	17½"	SMI	DSJ	XA7181	18	18	18	203	7	0.5	14		5/15	80	3000	1500	1.09	7	4	15	INC.				CMT.					
2	F	R	T	17½"	SMI	DSJ	XA7181	18	18	18	220	631	33	19.1	½	7/17	130	3200	2150	1.14	5	5	16.5	2	7	I		AC	AB				
3	F	R	T	17½"	HUG	OSC3AJ	3035R	18	18	18	851	496	41	11.4	½	5/17	130/150	3150	2200	1.15	8	6	14.6	3	7	I		A	EX				
4U	RA	R	T	17½"	SMI	DSJ	XA7194	OPEN										3200						1	2	IN				WIPER TRIP AFTER LOGS			
5	RA	R	T	12¼"	SMI	SDS	CH3774	12 +/32	12 C.	12 JET	1272	38	2.30		½	14	60	2420	2000	1.07	15	4	6.8					CMT		STAB @ + 20m ABOVE BIT			
5	F	R	T	12¼"	SMI	SDS	CH3774	"	"	"	1320	252	13.30	18.66	½	15	125	2500	2150	1.07	15	4	6.8	2	2	IN		A	E				
6	RA	R	T	12¼"	SMI	SDS	CH3645	"	"	"	1157	260	6	42.3		0/5	130	2300	2600	1.17	18	8	4.2										
6	F	R	T	12¼"	SMI	SDS	CH3645	"	"	"	1572	431	23	18.7	3/4	14	130	2300	2600	1.17	18	8	4.2	CENTRE JET WASHOUT A					C				
7	RA	R	T	12¼"	SMI	SDS	CH3410	12	12	12	1604	399	7	57		0/5	125	2300	2500	1.14	21	9	4					A					
7	F	R	T	12¼"	SMI	SDS	CH3410	12	12	12	2003	25	2.5	10		14	130	2300	2500	1.14	21	9	4	1	1	CENTRE JET WASHOUT			C				
8	RA	R	T	12¼"	SMI	SDS	CD9014	13	13	13	1748	280	2.5	112		0/9	80	2300	2700	1.15	21	9	4										
8	F	R	T	12¼"	SMI	SDS	CD9044	13	13	13	2028	320	44.5	7.2	1	18	110	2300	2750	1.14	11	8	3.9	7	5	5/8	W G		A ± E				
1C	C	R	C	8½"	CHR	RC4	82B0932	--	--	--	2348	18	3	6		6	100	1020	550	1.14	10	9	4						E				
9			T	12¼"	REE	HS51	94897	13	13	13	NO DRILLING - DROP IN HOLE WITH FISH									1.16	10	9	3.5	1	CONE PINCHED				G				
10	RA	R	T	12¼"	REE	HS51	339371	13	13	13	2261	87	3	29		0/5	120	2100	2500	1.16	10	9	3.5										
10	E	R	T	12¼"	REE	HS51	339371	13	13	13	2348	18	6	3		0/5	140	2300	2700	1.14	13	8	3.5										
10	F	R	T	12¼"	REE	HS51	339371	13	13	13	2366	156	47	3.3	3	16	130	2000	2350	1.15	20	8	4.2	7	8	3/8			A ± B				
11	RA	R	T	12¼"	SMI	F2	BZ1154	13	13	13	2509	13	1	13		5	100	2300	2450	1.15	20	8	4.2										
11	F	R	T	12¼"	SMI	F2	BZ1154	13	13	13	2522	101	26.5	3.8	2	15	70	2250	2650	1.15	26	8	3.6	2	2	1/16	BT		E				

OPERATION
F – Drilling
K – Coring
RA } – Redrilling (formation or cement)
} – Reaming and control trip
P – Pilot hole drilling
E – Hole opening
PE – Simultaneous piloting and hole opening

Note: Use one line for each operation

Ex.: Redrilling followed by drilling = 2 lines

DRIVE
R – Rotary
T – Turbine
M – Bottom hole motor other than turbine

BIT DESIGN
T – Tricones (rock bits)
B – Bicones
M – Other cone rock bits
F – Mill
D – Diamond bit
C – Diamond core head
A – Rock bit w/removable center
E – Diamond bit w/removable center
L – Drag bit
S – Special

MANUFACTURER
The code constitute the first three letters of the manufacturer name
HUG – Hughes
SMI – Smith
REE – Reed
SEC – Security
SMF – SMF
DIA – Diamond boart
DRI – Drilling service
CHR – Christensen

CODE
IACD code for rock bits (SEE Formulaire Foreur, p. 200 à 204).

– DULL BIT CONDITION
T1 - Tooth hight 1/8 gone
T2 - Tooth hight 1/4 gone
T3 - Tooth hight 3/8 gone
T4 - Tooth hight 1/2 gone
T5 - Tooth hight 5/8 gone
T6 - Tooth hight 3/4 gone
T7 - Tooth hight 7/8 gone
T8 - Tooth hight all gone

Bearing wear B1 to B8
B1 – 1/8 of life elapsed
B2 – 2/8 of life elapsed
B8 – Out of service

OBSERVATION ON GRADING :
Teeth and cones
CT – Chipped teeth
ET – Eroded teeth or inserts
BT – Broken teeth or inserts
BU – Bit balled up
RG – Rounded gauge teeth or inserts
WG – Worn or lost gauge teeth or inserts
FC – Flat crested
EC – Eroded cone shell
BS – Broken, worn or lost spear point

Bearings
CL – Cone(s) locked
BF – Bearing failure
SF – Seal failure
LC – Lost cone(s)
BP – Broken bearing pins or journals

Bit body
BL – Bent legs - Pinched
PN – Plugged nozzle(s)
EN – Eroded nozzle(s)
LN – Lost nozzle(s)
DB – Damaged nozzle(s)

– FORMATION
A – Clay
C – Limestone of dolomite
M – Marl or shale
D – Chalk
S – Sand
G – Sandstone
Q – Quartz
V – Chert
X – Granite
K – Conglomerate
I – Gypsum - Anhydrite
L – Saltz

The lithology drilled in the previous 24 Hrs will be defined by the codes of the last formations drilled, with a maximum of three placed in order of relative importance.

Ex. (1) Ap : Plastic clay
(2) AS : Clay and sand
(3) Mct : Marl and soltf limestone
(4) MChv: Marl and tight dolomite w/Chert

Additif necessary a small letter showing the formation characteristics : p : plastic ; h : tight ; f : laminated ; r : soft
Ex. 1) Af : laminated clay - 2) Ch : Tight dolomite

– REASON FOR TRIPPING
A – Penetration slowing down
B – Increasing torque
C – Hydraulic problems
D – Bit drill maximum hours allowed
E – Reason other than bit problems

Ex. (1) Drillstring modification
(2) Casing
(3) Test
etc...

GENERAL			BIT / DRILLING							PERFORMANCES					PARAMETERS				MUD				DULL BIT CONDITION						TURBODRILLED			
Run number	Operation	Drive	Bit type	Bit Diameter	Manufacturer	Code IADC	Serial number	Nozzles 1 /32	Nozzles 2 /32	Nozzles 3 /32	Operation starting depth	Footage in this operation	Drilling time (hours)	Drilling rate	Deviation	Weight on bit	R.P.M.	Flow rate	Pressure	Density (mud weight)	Plastic Viscosity (cp)	Solid content (%)	Water loss (cc)	T	B	G	Observations on grading	GEOLOGICAL FORMATION	Reason for tripping	Type of turbodrill	Turbodrill diameter	Turbodrilled footage	Total time (hours)
2	RA	R	T	12¼"	HUG	J22	320SK	13	13	13	2579	44	2.5	17.5		5	90	2000	2000	1.15	26	8	3.6	INC				G					
2	F	R	T	12¼"	HUG	J22	320SK	13	13	13	2623	176	48	3.7	2	10/20	130	2250	2650	1.15	24	8	4.1	6	8	3/8	BT	G	A+B				
3	RA	R	T	12¼"	HUG	J22	695FL	13	12	12	2778	21	1	21		0/4	120	2000	2800	1.15	24	8	4.1					G					
3	F	R	T	12¼"	HUG	J22	695FL	13	12	12	2799	151	38.5	3.9	2 3/4	20	80	2050	2850	1.16	27	8.5	3.9	8	8	2"	--	G	A+B				
4	RA	R	T	12¼"	SMI	F3	BT4323	13	12	12	2943	7	0.5	14		5	60	2100	2850	1.15	25	8	4.5				--	G					
4	F	R	T	12¼"	SMI	F3	BT4323	13	12	12	2950	35	11	3.2		20	80	2150	2850	1.15	35	8	4.5	1	1	0	--	G	E	DC WASHOUT IN ELEVATOR RECESS			
5U	RA	R	T	12¼"	SMI	SDS	CB7277	14	14	14	2680	6	0.5	12	2	5	125	2000	1600	1.15	22	8	4.2	1	1	I		CMT	E	DRILL OUT TOP CMT. PLUG FOR SIDE TRACK			
6	F	T	T	12¼"	SEC	M4LG	108897		OUT		2686	63	10	6.3		1/3	250÷2270		950/1400	1.15	14	8	5.2	3	6	1/8		CMT	E	ATTEMPT SIDE TRACK RUN UNDER DYNA DRILL			
7	RA	T	T	12¼"	HUG	X3A	SW343		OUT		2715	34	2.5			0/2	250	2100	1300	1.15	15	8	4.5							REAM CMT. TO BTM.			
7	F	T	T	12¼"	HUG	X3A	SW343		OUT		2749	10	2		2-2½	1/3	250÷2270		1000/1500	1.15	15	8	4.5	3	3	1/8		CMT	E	ATTEMPT KICK OFF PULLED DUE TO SURVEY HUNG IN BHA.			
8	RA	T	T	12¼"	SMI	SDS	CD831		OUT		2684	75	7.5	2	2-2½	1/3	250÷2270		650/1400	1.15	15	8	4.5							REAM CMT. TO TD.			
8	F	T	T	12¼"	SMI	SDS	CD831		OUT		2759	23	4	2	2	1/3	250÷2500		1000/1600	1.15	18	9	4.5	3	3	1/16		CMT	E	DRILLED OUT OF CMT PLUG KICK OFF NO SUCCESS.			
5U	RA	R	T	12¼"	SMI	SDS	CB7277	14	14	14	1619	529	28.5		2	3/15	80/100	1980	2000	1.20	24	11	4	3	3	0			E	REAM COND. HOLE			
9	RA	R	T	12¼"	HUG	JD3	HS522	14	14	14	2130	687	44		2	0/4	50/100	1980	2000	1.20	30	10	3.4	1	2	0				REAM COND. HOLE FOR SIDE TRACK			
10	F	T	T	12¼"	SMI	SDS	CB6084	14	14	OUT	2666	8	7			0/1	DYNA DRILL	1640	1100	1.19	27	9	3.4	2	2	0		START ABORTED		SIDE TRACK IN 12¼" HOLE TO RUN 9 5/8" CASING.			
11	RA	R	T	8½"	SMI	SDS	CC9527	12	12	12	2581	93	3			0/10	50/70	1184	1550	1.19	24	9	3.2	2	8	0	CL	CMT		FLOAT & SHOE 9 5/8"			
12	F	T	T	8½"	SMI	SDS	CH0306		OUT		2674	26	21.5		1-3/4	0/1	POSI DRILL	1316	1000	1.19	27	9	6.0	6	4	¼		MG	D	SIDETRACK SUCCESSFUL			
13	F	T	T	8½"	SMI	SDGH	BP6095		OUT		2700	9	9.5		1	0/1	POSI DRILL	1316	1000	1.19	27	9	6.2	8	8	¼		MG	D	COMPLETE SIDETRACK			
14	RA	R	T	8½"	SMI	F3	XA8788	12	12	12	2684	25	1.5			1/3	70	1200	1550	1.19	24	9	6.2		INC								
14	F	R	T	8½"	SMI	F3	XA8788	12	12	12	2709	95	25		1	15	70	1200	1600	1.19	30	9	6.2	3	5	¼		G	B				

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- T4 - Tooth hight 1/2 gone
- T5 - Tooth hight 5/8 gone
- T6 - Tooth hight 3/4 gone
- T7 - Tooth hight 7/8 gone
- T8 - Tooth hight all gone

Bearing wear B1 to B8
- B1 – 1/8 of life elapsed
- B2 – 2/8 of life elapsed
- B8 – Out of service

OBSERVATION ON GRADING :

Teeth and cones
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- B – Increasing torque
- C – Hydraulic problems
- D – Bit drill maximum hours allowed
- E – Reason other than bit problems

Ex. (1) Drillstring modification
(2) Casing
(3) Test
etc...

GENERA			DRILLING							PERFORMANCES					PARAMETERS				MUD				DULL BIT CONDITION				GEOLOGICAL FORMATION	Reason for tripping	TURBODRILLED			
Run number	Operation	Drive	Bit type	Bit Diameter	Manufacturer	Code IADC	Serial number	Nozzles 1 /32	Nozzles 2 /32	Nozzles 3 /32	Operation starting depth	Footage in this operation	Drilling time (hours)	Drilling rate	Deviation	Weight on bit	R.P.M.	Flow rate	Pressure	Density (mud weight)	Plastic Viscosity (cp)	Solid content (%)	Water loss (cc)	T	B	G	Observations on grading			Type of turbodrill	Turbodrill diameter	Turbodrilled footage	Total time (hours)
25	F	R	T	8½"	SMI	F3	XA8888	12	12	12	2804	113	28		1	16	65	1200	1250	1.19	31	9	5.8	7	3	½	RG WG	G	D				
26	RA	R	T	8½"	SMI	F3	XA8829	14	14	14	2883	34	.5		1	0/6	60	1100	1000	1.19	28	9	5.2		INC								
26	F	R	T	8½"	SMI	F3	XA8829	14	14	14	2917	68	20		1	16	65	1160	1070	1.20	29	9	5.4	6	6	¼	RG	G	B				
27	RA	R	T	8½"	SMI	SVH	CE2649	OPEN		COND. TRIP					1	COND. HOLE		900	550	1.20	29	9	5.4	1	1	0		G	E				
28	RA	R	MILL 6"		SERVCO MILL		E2465	----------			DRILL CMT+FLOAT+SHOE					6	65	1300	2100	1.11	15	5	6.8	90% WORN OUT					D				
29	F	R	T	6"	SMI	F3	CL8786	9	9	9	2987	8.5	11.5			3/4	65	700	1000 2000	1.10	14	5	5.8	3	4	1/8		GM	D				
30	F	T	D	6"	CHR	MD331	8280610	--	--	--	2994.5	2.5	2							1.10	20	5	5.4	AS NEW				GM	E	NAVI DRILL			
31	F	R	D	6"	CHR	R26	2W7147	--	--	--	2997	15.5	7											COMPLETELY WORN OUT				STRATA PACK					
30	F	R	D	6"	CHR	MD331	8280610	--	--	--	3012.5	5.5	6			3/4	140	700	2000	1.09	20	5	5.4	COMPLETELY WORN GM									
32	RA	R	T	6"	SMI	F3	CL9564	9	9	9	3003	15	1			0/1	70	700	1300	1.10	14	5	5.3					GM					
32	F	R	T	6"	SMI	F3	CL9564	9	9	9	3018	14	12.5		2 3/4	7	50	700	1300	1.10	14	5	5.3	2	2	1/8		G					
33	RA	R	C	6"	CHR	C20					3002	30	3																			
33	K	R	C	6"	CHR	C20					3032	11	3			5/6	100	500	800	1.10	18	5	5.2	40% WEAR				GM					
34	RA	R	T	6"	SMI	F3	BN7427	9	9	9	3014	26	3.5			1/2	75	700	1350	1.09	14	5	4.9					GM					
34	F	R	T	6"	SMI	F3	BN7427	9	9	9	3040	75	31.5			10	50/95	700	1350	1.09	14	5	4.9	2	4	1/8		GM					
35	RA	R	T	6"	SMI	F3	CL7267	9	9	9	3095	20	1			0/1	70	700	1350	1.09	14	5	5										
35	F	R	T	6"	SMI	F3	CL7267	9	9	9	3115	58	22			10	55	700	1350	1.10	14	5	5	4	4	1/8		GM					
36	F	R	T	6"	SMI	F3	CN054	9	9	9	3173	45	29			9/10	50/60	700	1400	1.09	16	5	4.8	4	4	1/8		GM					
37	F	R	T	6"	SMI	F3	BN7421	9	9	9	3218	135	49.5			10	60	700	1450	1.09	16	5	4.9	3	6	1/8		ASM					
38	RA	R	T	6"	SMI	F3	AT6654	9	9	9	3300	53	3			0/5	60	650	1350	1.08	16	5	5	INC									

OPERATION
F – Drilling
K – Coring
RA – Redrilling (formation or cement) / Reaming and control trip
P – Pilot hole drilling
E – Hole opening
PE – Simultaneous piloting and hole opening

Note: Use one line for each operation

Ex.: Redrilling followed by drilling = 2 lines

DRIVE
R – Rotary
T – Turbine
M – Bottom hole motor other than turbine

BIT DESIGN
T – Tricones (rock bits)
B – Bicones
M – Other cone rock bits
F – Mill
D – Diamond bit
C – Diamond core head
A – Rock bit w/removable center
E – Diamond bit w/removable center
L – Drag bit
S – Special

MANUFACTURER
The code constitute the first three letters of the manufacturer name
HUG – Hughes
SMI – Smith
REE – Reed
SEC – Security
SMF – SMF
DIA – Diamond boart
DRI – Drilling service
CHR – Christensen

CODE
IACD code for rock bits (SEE Formulaire Foreur, p. 200 à 204).

– DULL BIT CONDITION
T1 - Tooth hight 1/8 gone
T2 - Tooth hight 1/4 gone
T3 - Tooth hight 3/8 gone
T4 - Tooth hight 1/2 gone
T5 - Tooth hight 5/8 gone
T6 - Tooth hight 3/4 gone
T7 - Tooth hight 7/8 gone
T8 - Tooth hight all gone

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Ex. (1) Drillstring modification
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GENERAL DATA			DRILLING BIT					Nozzles			PERFORMANCE				PARAM				MUD			CONDITION				GEOLOGICAL FORMATION	Reason for tripp	TURBODRILL			
Run numbe	Operation	Drive	Bit type	Bit Diameter	Manufacturer	Code IADC	Serial number	1 /32	2 , 32	3 /32	Operation starting depth	Footage in this operation	Drilling time (hours)	Drilling rate	Deviation	Weight on bit	R.P.M.	Flow rate	Pressure	Density (mud weight)	Plastic Viscosity (cp)	Solid content (%)	Water loss (cc)	T	B	G	Observations on grading			Type of turbodrill	Turbodrill diameter	Turbodrilled footage	Total time (hours)
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39	RA	R	T	6"	SMI	F3	BN7430	15	15	15						0/6	50	650	800	1.28	25	9	4.8							USED FOR CONDITION TRIPS.			

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AUSTRALIAN AQUITAINE PETROLEUM PTY LTD

WELL OMEO 1

OPERATIONS SUMMARY

AND

PRELIMINARY TEST REPORT

TO: WELSHPOOL BASE

FEB 1983

SNEA (P)
EXPL / PROD / DPT PUITS

F. JACQUIER.

GENERAL INFORMATION

COMPANY	: Australian Aquitaine Petroleum
WELL NAME	: OMEO No.1
AREA - PERMIT	: Gippsland Basin - VIC / P17
CO-ORDINATES	: Lat. 38 Deg 36" 45.16' S Long. 147 Deg 43" 02.00' E
SEISMIC LOCATION	: SP 920 on line GA 81.33
ROTARY TABLE ELEVATION / MSL	: 30.5 m
WATER DEPTH	: 62.6 m
DISTANCE TO THE SHORE	: 51.5 Km
TOTAL DRILLING DEPTH	: 3379 m (Driller) 3378 m (Logger)
BEFORE TESTING TOTAL DEPTH	: 2955 m (Top cement plug)
DEVIATION	: 1 Deg average
START OF DRILLING	: 02/11/82
END OF DRILLING	: 25/01/83
START OF TESTING	: 03/02/83
END OF TESTING	: 06/02/83
NUMBER OF TESTS	: 1
NUMBER OF TESTED INTERVALS	: 1
TESTING EQUIPMENT	: Halliburton APR tool Drill pipe 3½ and 5"
WELL STATUS PRIOR TO TESTING	: 9-5/8" casing + 7" liner
WELL STATUS AT RIG RELEASE	: Plugged and Abandoned
DRILLING CONTRACTOR	: Odeco
RIG NAME AND TYPE	: Ocean Digger (semi - submersible)
REMARKS	: No motion compensator
	: A$ 180,000 average daily cost (rig and services)

I2. OBJECTIVES OF THE TEST

I2.1 RESERVOIR DATA.

The evaluation of the LATROBE formation through electrical logging, RFT's and drilling parameters analysis showed three main zones of interest:

2849 to 2952 m / RT (ref ISF log run # 3)
3073 to 3181 m / RT (ref DLL log run # 4)
3320 to 3372 m / RT (ref DLL log run # 4)

The upper interval was drilled in 8-1/2 and a 7" liner was run from 2505 to 2984 m. The lower interval was drilled with a 6" bit down to 3378 m.

Gas was proved by RFT at 2849.8 m in a forth interval (2849 to 2857 m - ISF run # 3)

LITHOLOGIE:

The Latrobe formation is mainly sandstone with variable amount of clay. The porosity is in the range 11 to 17% with an average of 13%. The water saturation varies from 50 to 70% depending upon the value of RW chosen for the calculations.

The well crossed a major fault at 3315 m and the analysis of CST's at 3361 - 3365 and 3378 m should determine whether the formation is still Latrobe or Strselecki.

From 3320 to 3378 m it was observed very good shows. However due to gas kicks the weight of the mud had to be increased to 1.28 and the drill string got stuck for 24 hours with bit at 3365 m.

PRESSURE:

A water gradient can be easily determined with RFT's pressure measurements from 2350 to 2800 m. Unfortunately all the pressures below 2850 m are not consistent with any water, gas or oil gradient.
This is mainly due to:

- the use of different pressure gauges (different calibrations)
- super charging phenomenum in some reservoirs.
- shift of some gauges as hydrostatic pressures do not aligne
- inaccurate depth measurement; one run was done without gamma ray in a badly caved hole. As a result the tool got stuck, the fishing job aborted and the well had to be sidetracked.

I2.2 GENERAL PROGRAM

- Evaluation of the interval 3073 - 3181 m with one RFT at 3126.5 m
- Plug and abandon the open hole
- Quick test over the interval 2917 to 2940 m behind the 7" liner to determine the nature of the fluid. If the effluent is oil a production test may be run.
- Plug and abandon the well.

I3 CONCLUSION

I3.1 The RFT sample at 3125.0 m proved gas in the interval 3120 to 3128.5 m.

The results are gathered in the following table.

At the end of the sampling period (2 chambers of $2\frac{3}{4}$ gallons each) the tool got stuck, the cable broke at the weak point and the tool was fished with the drill pipe on the first attempt.

RFT'S (H.P Pressure Gauge)

No.	DEPTH (m) (G.R.)	P. HYDRO (PSIA)	P. FORMATION PSIA	REMARK
1	3077.5	5642	4439.6	
2	3096.0	5680	4461.7	
3	3104.0	5692	4463.8	
4	3131.5	5740	4585.8	
5	3126.5	5730	4519.6	
6	3147.5	5766	-	MISRUN
7	3125.0	5729	4515.7	SAMPLING

SAMPLING at 3125.0 m

		LOWER CHAMBER	UPPER CHAMBER
Bottle ref. (20l Gerzat)		A 12683	A 12769
P Surface	start Transfer	1250 psi	1750 psi
	end Transfer	180 psi	460 psi
Gas vented to atmosphere		1.5 cuft	6 cuft
Liquid recovery		7500 cc	3750 cc
Water Rw (T deg,F)		.234 (82)	.245 (80)
Salinity		24500 ppm	24000 ppm
Gas	Cl (%)	90.89	91.68
	C2 "	6.73	5.21
	C3 "	1.69	2.55
	iC4 "	.38	.31
	nC4 "	.31	.26
	iC5 "	0	Tr
	nC5 "	0	Tr

Mud Filtrate Resistivity: Rmf = .21 at 66 Deg, F
Salinity 35000 ppm

I 3.2 DST from 2918 to 2939 m

The interval of interest was perforated with Enerjet 2-1/8" (13 shots/m) from 2918 to 2925 m and from 2932 to 2939 m.

The testing string was assembled as shown in appendix and the pipes were filled with a cushion of fresh water (1600 m) such as the differential pressure on the formation would be 2000 psi at the opening of the test.

The well did not flow at surface and the samples recovered during the reverse circulation showed water (filtrate + formation water ?) with decreasing salinity. No gas was noticed.

The down hole sample trapped in the APR M2 tool is gas.

DETAILS OF OPERATIONS

1. TIMING

05/02 18h15: Set packer at 2886.2 m (Driller) or 2892 m (logger)

18h25: Open APR N valve (1400 psi in annulus)
Weak air blow - Well head pressure = 0

19h30: Attempt to flow bubble hose through Schlumberger gas meter: insufficient flow to turn counters.

20h00: Air flow evaluation : 5 l of air / 10 seconds

21h00: " " " : 5 l of air / 15 seconds

22h00: Air flow evaluation : 5 l of air / 30 seconds

22h55: Shut in the well at bottom for build up

06/02 6h40: Reopen APR N valve to flow the well and to trap a fresh sample of fluid in the chamber

7h00: Air flow evaluation : 5 l of air / 20 seconds
Well head pressure = 0

7h30: Pressure up the annulus to 2250 psi to function APR M2 reverse circulating valve.

9h30: End reverse circulation - start POOH

17h30: Pressure gauges at surface

18h00: End of test

2. RECOVERY

AT SURFACE:

Mud and formation water during reverse circulation, no gas.

Five samples were collected.

No.	Cl^- (AgNO3)	PH	RW x m	T (F)	NaCl Equivalent
1	14,000	10	0.271	74	23000 ppm
2	12,000	9.5	0.307	72	21000 ppm
3	10,000	9.5	0.351	72	18000 ppm
4	9,500	7	0.381	72	16000 ppm
5	9,000	7	0.403	74	15000 ppm

Mud characteristics when drilling: S.G = 1.19
Sal = 25 000 ppm
PH = 10.5

In the APR Chamber:

18.2 cu ft of gas, no liquid. P: 2350 psi

Gas analysis on Geoservices chromatograph:

C1	:	91.36 %
C2	:	5.54
C3	:	2.07
iC4	:	0.48
nC4	:	0.45
iC5	:	0.10
nC5	:	0.06

3. PRELIMINARY INTERPRETATION

3.1 TOTAL PRODUCTION EVALUATION

During the reverce circulation the choke manifold was kept shut in until the pressure started building up in the tubing.

It took 130 strokes to fill up the tubing to surface which is 26 bbls

The initial volume of the air cushion being 73 bbls the total production during the test was;

TOTAL PRODUCTION = 73 - 26 = 47 bbl = 7.5 m3

that one can split in : 6 m3 during the 1st opening (4h30)
: 1.5 m3 during the 2nd opening (0h50)

3.2 PRESSURE

As the well did not flow at surface the classical Horner type interpretation is not valid. However the shape of the build up curve shows a very tight formation. A tentative permeability calculation, assuming a flow rate of 30 m3/day, gives K = 0.8 md. The extrapolated Initial Static Pressure is 4100 psi which does not match the one measured on RFT at 2936.5 m (4320 psi). We will consider the RFT pressure measurement as representative of the formation pressure.

3.3 TEMPERATURE:

The bottom hole temperature measured with the RT 7 from Flopetrol at 2900 m id 250 deg, F

ATTACHEMENTS

SUMMARY OF EVENTS

Feb 2nd, 1983

00.00 to 00.30 : Set cement plug # 1 from 3349 to 3280 m. Reverse out above.

00.30 to 01.30 : Pull up to 3220m, set cement plug # 2 from 3220 to 3045 m with 3 T of 'G' cement.

01.30 to 03.00 : Pull up to 3030 m, set cement plug # 3 from 3030 to 2960 m with 1.75 T of 'G' cement.

03.00 to 04.00 : Pull up to 2960 m, reverse circulate - 2 bbls in return

04.00 to 08.00 : POOH, lay out 39 joints excess 5" DP and $3\frac{1}{2}$ tubings

08.00 to 12.30 : RIH with bit and scrapper to 2950 m - Test casing to 3000 psi

12.30 to 24.00 : Circulation, conditioned mud to lower mud weight to SG = 1.1 and control water loss to 6 m3 / 30 min.
Tested all lines and valves to Flopetrol Burners to 1500 psi

Feb. 3rd, 1983

00.00 to 10.30 : Circulate and condition mud. SG = 1.1 - WL = 6.3

10.30 to 11.00 : Test casing to 3000 psi for 15 min.

11.00 to 16.30 : POOH, lay out excess $3\frac{1}{2}$ DP

16.30 to 22.00 : Pull wear bushing - test BOP RAMS to 500 and 5000 psi. Choke and kill valves to 500 and 5000 psi, hydrill to 25000 psi. C and K manifold at surface, tested to 500 and 5000 psi.

22.00 to 24.00 : Rig up Flopetrol EZE tree for dummy test run. Tested Halliburton APR tool to 5000 psi.

Feb. 4th, 1983

00.00 to 04.30 : Make up EZ tree to check out (2 runs). Slick joint properly positioned but $3\frac{1}{2}$ rams did not close. Check connection and disconnection of EZ tree. Make up control head, check out control system

04.30 to 10.00 : Rih with open end drill pipe at 2779 m.

10.00 to 17.00 : Rig up Schlumberger lubricator and test to 500 psi. Perforations with Enerjet 2-1/8 (13 h/m) from 2932 to 2939 m and 2918 to 2325 m

17.00 to 21.00 : POOH

21.00 to 24.00 : Pick up Halliburton test tools - RIH - Test string internally tested to 3000 psi from top of $4\frac{3}{4}$ DC to APR N valve (water from cushion)

Feb. 5th, 1983

00.00 to 17.00 : RIH test string with $3\frac{1}{2}$ and 5" Drill Pipe. Gatorhawk each connectior to 5000 psi. Fill up pipe with fresh water for 1600 m above APR N Run SSTT assembly. Nipple up McEvoy Flow Head.

17.00 to 18.00 : Test Well Head valves and Flopetrol choke manifold to 5000 psi test lines from C.M to tank to 3000 psi

18.00 to 18.25 : Set packer at 2892.4 m (log depth), close $3\frac{1}{2}$" pipe rams and

: pressure up the annulus to 1400 psi

18.25 to 22.25 : Flow the well : weak blow at surface.

22.25 to 24.00 : Shut in the well at bottom for build up.

Feb. 6th, 1983

00.00 to 06.40 : Well shut in for build up.

06.40 to 07.30 : Open well to trap clean sample in APR M2 chamber.

07.30 to 09.30 : Pressure up annulus to 2250 psi to open APR M2 circulation valve.
Reverse circulation and collect samples.
Clean surface lines to Flopetrol tank and rig manifold.

09.30 to 10.00 : Open $3\frac{1}{2}$ rams, pick up to unset packer, close 5" rams and squeeze volume below packer back into the formation (6 bbls at 1000 psi).

10.00 to 10.30 : Rig down Flow Head - break down flow lines.

10.30 to 18.00 : POOH test string - lay down and break Halliburton test tool and EZ tree.
Body of EZ tree was damaged due to 5" pipe rams closing by Odeco Sob. Sea Eng. - unable to unlatch.

END OF TEST.

PRESSURE GAUGE

Halliburton Recording Pressure Gauge Charts Summary.

DEPTH m (log)	INITIAL HYD. psi	FINAL 1st FLOW psi	FINAL 1st B.U psi	FINAL 2nd FLOW psi	FINAL 2nd B.U psi
2900	4469.6	3520	4012.9	3678	3975
2876.5	4419.9	3476.8	3968.5	3626 ?	3934
2867.8	2289.5	3472.0		3635.9	

Gauges at 2900 and 2876.5 are below N value
Gauges at 2867.8 m is located above N value

Final Flow and Final Build up pressures are not stabilised.

The pressure gradients that one may calculate are not accurate because the pressures are not stabilised and readings from each chart are not necessarily taken at the same time.

However the value calculated between lower and center gauges or between lower and upper gauges show liqiud production (maximum and minimum values: 1.55 and 0.92 respectively)

PRESSURE GAUGE

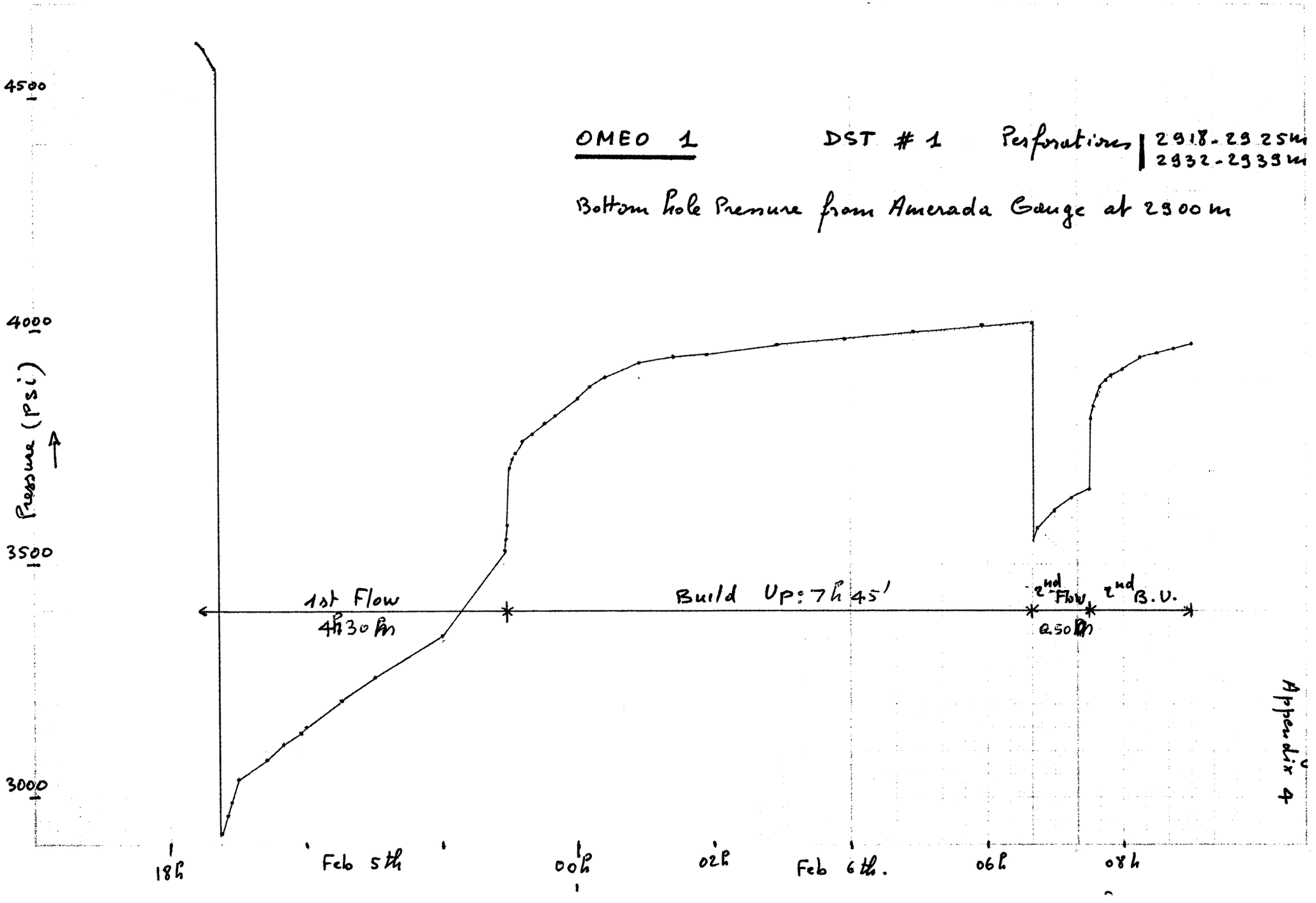
Flopetrol Recording Pressure Gauge Charts Summary

Depth; 2900 m

One gauge only worked properly, the stylus of the second one was damaged when the packer was set.

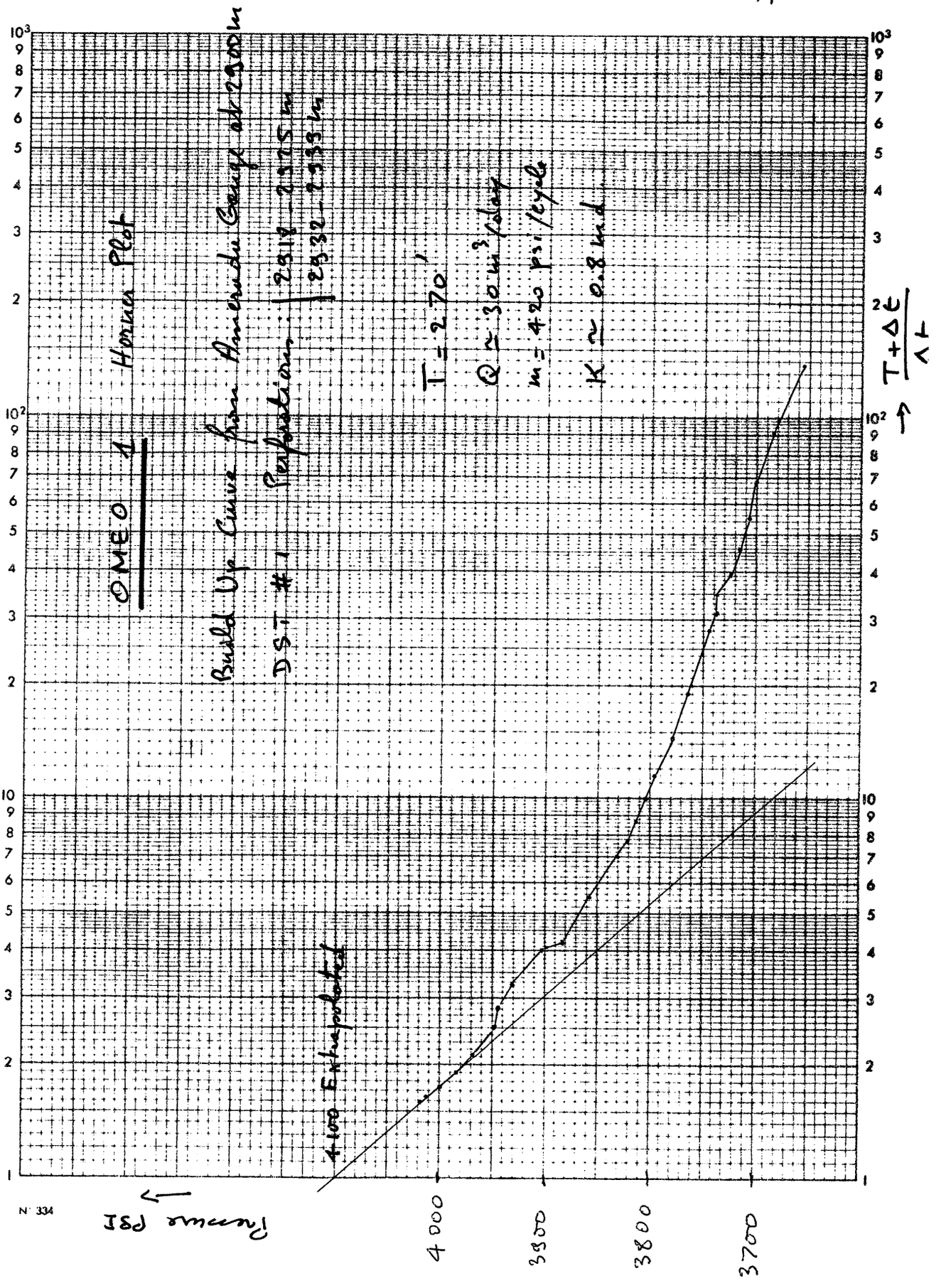
DATE TIME	TIME CUMUL	P_ (psi)
5-2-83		
18.25	0	
18.26	1	4616
18.28	3	4608
18.30	5	4605
18.40	15	4559
18.45	20	2926
18.50	25	2962
18.55	30	2992
19.00	45	3039
19.25	60	3079
19.40	75	3115
19.55	90	3141
20.00	95	3150
20.30	125	3208
21.00	155	3257
22.00	215	3345
22.55	370	3531
CLOSE APR		
22.55	0	3553
22.56	1	3584
22.57	2	3655
22.58	3	3683
22.59	4	3700
23.00	5	3707
23.01	6	3717
23,02	7	3724
23.03	8	3738
23.04	9	3737
23.05	10	3742
23.10	15	3764
23.15	20	3779
23.20	25	3796
23.25	30	3802
23.30	35	3812
23.35	40	3820
23.40	45	3830
23.55	60	3858
6-2-83		
00.10	75	3882
00.25	90	3902
00.55	120	3931

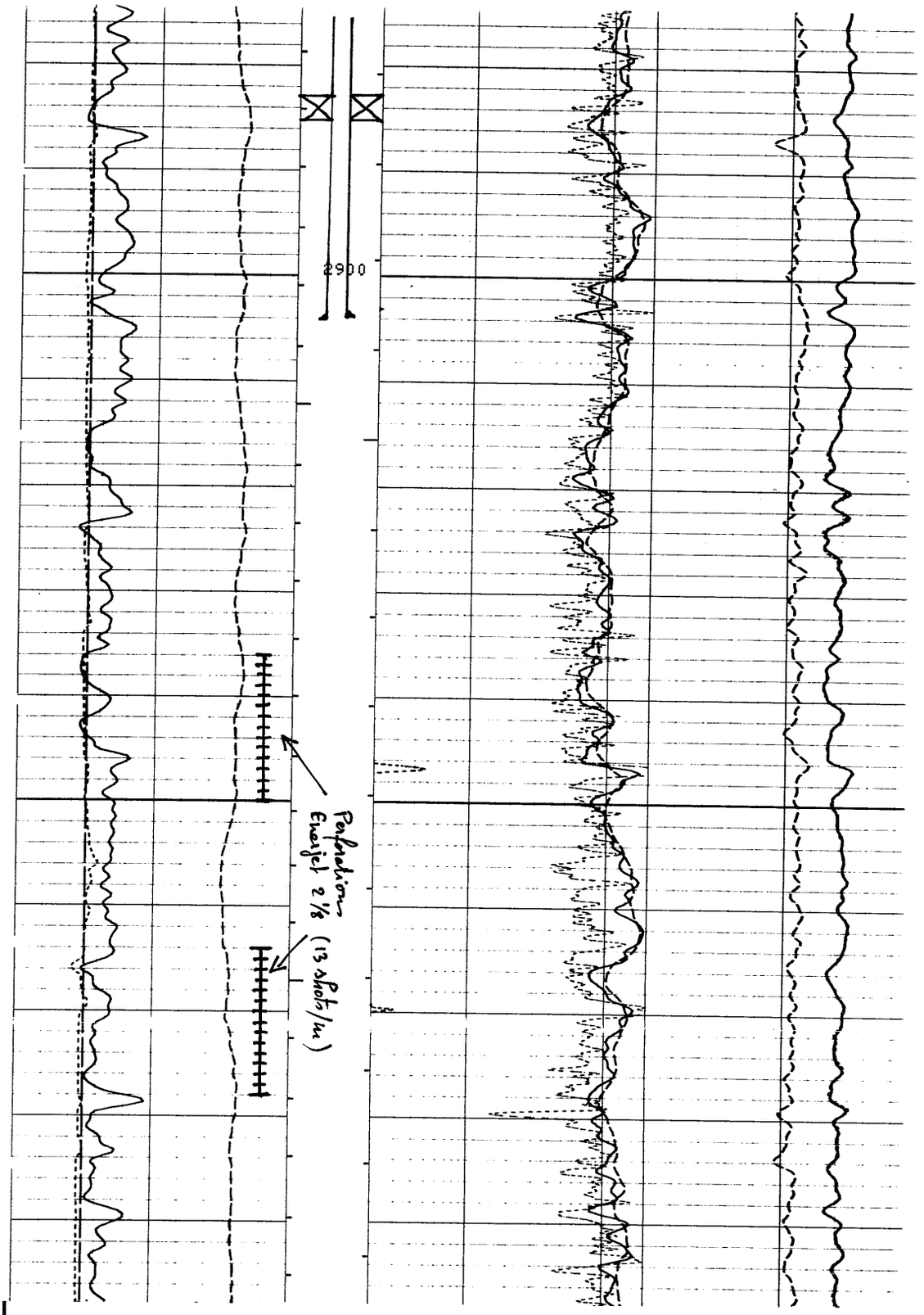
DATE TIME	TIME CUMUL	P (psi)
6-2-83		
01.25	150	3945
01.55	180	3947
02.55	240	3969
03.55	300	3983
04.55	360	3999
05.55	420	4012
06.40	455	4018
RE OPEN APR		
06.40	0	
06.45	5	3578
07.00	20	3607
07.15	35	3642
07.30	50	3660
CLOSE APRN. OPEN M VALVE		
	0	
07.31	1	3790
07.32	2	3812
07.33	3	3829
07.34	4	3839
07.35	5	3854
07.36	6	3860
07.37	7	3861
07.38	8	3869
07.39	9	3873
07.40	10	3882
07.45	15	3985
07.50	20	3906
07.55	25	3903
08.00	30	3918
08.15	45	3942
08.30	60	3951
08.45	75	3961
09.00	80	3970
UNSET PACKER		
09.30	P. Hydro	4415


OMEO 1
DST # 1
Perforations 2918-2925m
2932-2939m
Bottom Hole Pressure from Amerada Gauge at 2900 m
4500
4000
3500
3000
Pressure (psi)
1st Flow
4h30 Rn
Build Up: 7h45'
2nd Flow
0.50 Rn
2nd B.V.
18h
Feb 5th
00h
02h
Feb 6th.
06h
08h

Appendix 4

Appendix 5

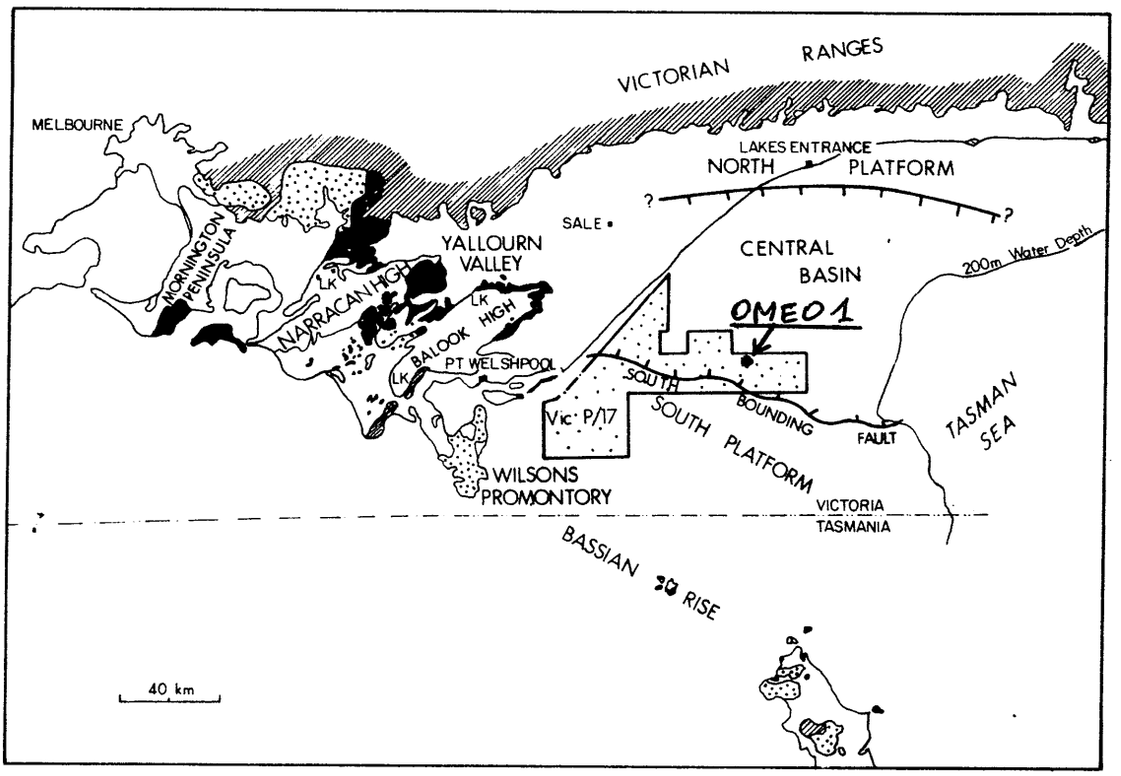

Horner Plot
OMEO 1
Build Up Curve from Interval Perforation
DST #1
2318 - 2375 m
2329 - 2333 m
T = 270°
Q ≈ 30 m³/day
m = 420 psi/cycle
K ≈ 0.8 md
4100 Extrapolated
Pressure PSI
4000
3900
3800
3700
N° 334



OMEO 1

ISF-SLS-MSFL-CNL-GR

BS (IN) 6.000 – 16.00	MSFL(OHMM) 20.00 – 2000.	
CALI(IN) 6.000 – 16.00	ILD (OHMM) 20.00 – 2000.	
GR (GAPI) 0.0 – 150.0	SFLU(OHMM) 20.00 – 2000.	
SP (MV) -80.00 – 20.00	MSFL(OHMM) 0.2000 – 20.00	DTL (US/F) 140.0 – 40.00
	ILD (OHMM) 0.2000 – 20.00	NPHI( ) 0.4500 – -0.150
	SFLU(OHMM) 0.2000 – 20.00	DT (US/F) 140.0 – 40.00



LEGEND

- PALAEOZOIC GRANITES
- PALAEOZOIC METASEDIMENTS
- VOLCANICS
- LK L CRETACEOUS - STRZELECKI GP

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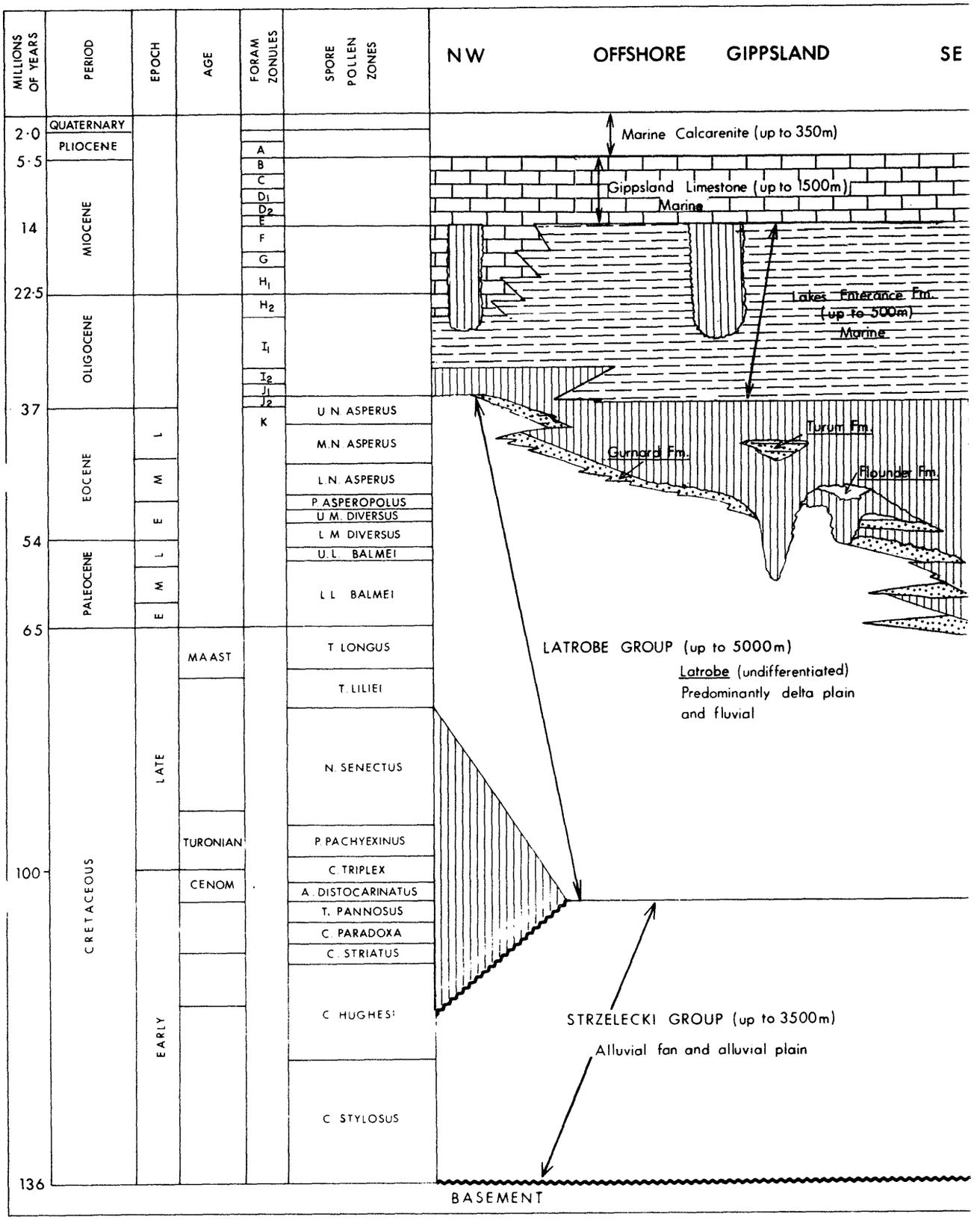
GIPPSLAND BASIN

Vic P/17

LOCATION MAP

Author KIM LY	Date DECEMBER 1981	Dwg. No 19944	FIC
Drafted by: D.H.	Report No	Base Plan	



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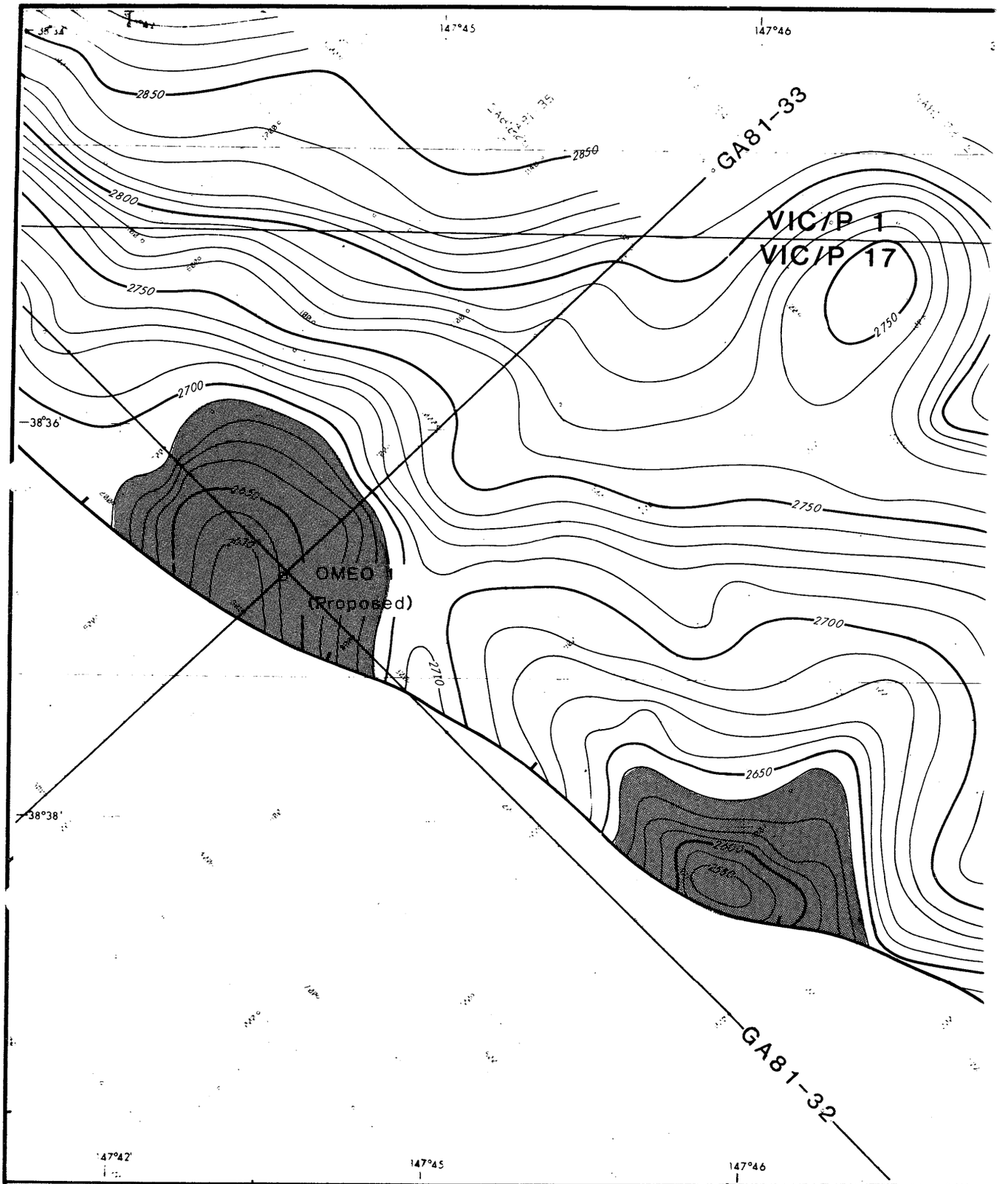
Gippsland Basin Vic/P17

STRATIGRAPHY

OFFSHORE GIPPSLAND BASIN

N.B. MODIFIED FROM THRELFALL ET AT., 1976

Dwg No: 20



OMEO PROSPECT

Contour Interval

Datum: Sea Level 10 metres

SCALE 1:50000

0 0·5 1 2 Kms

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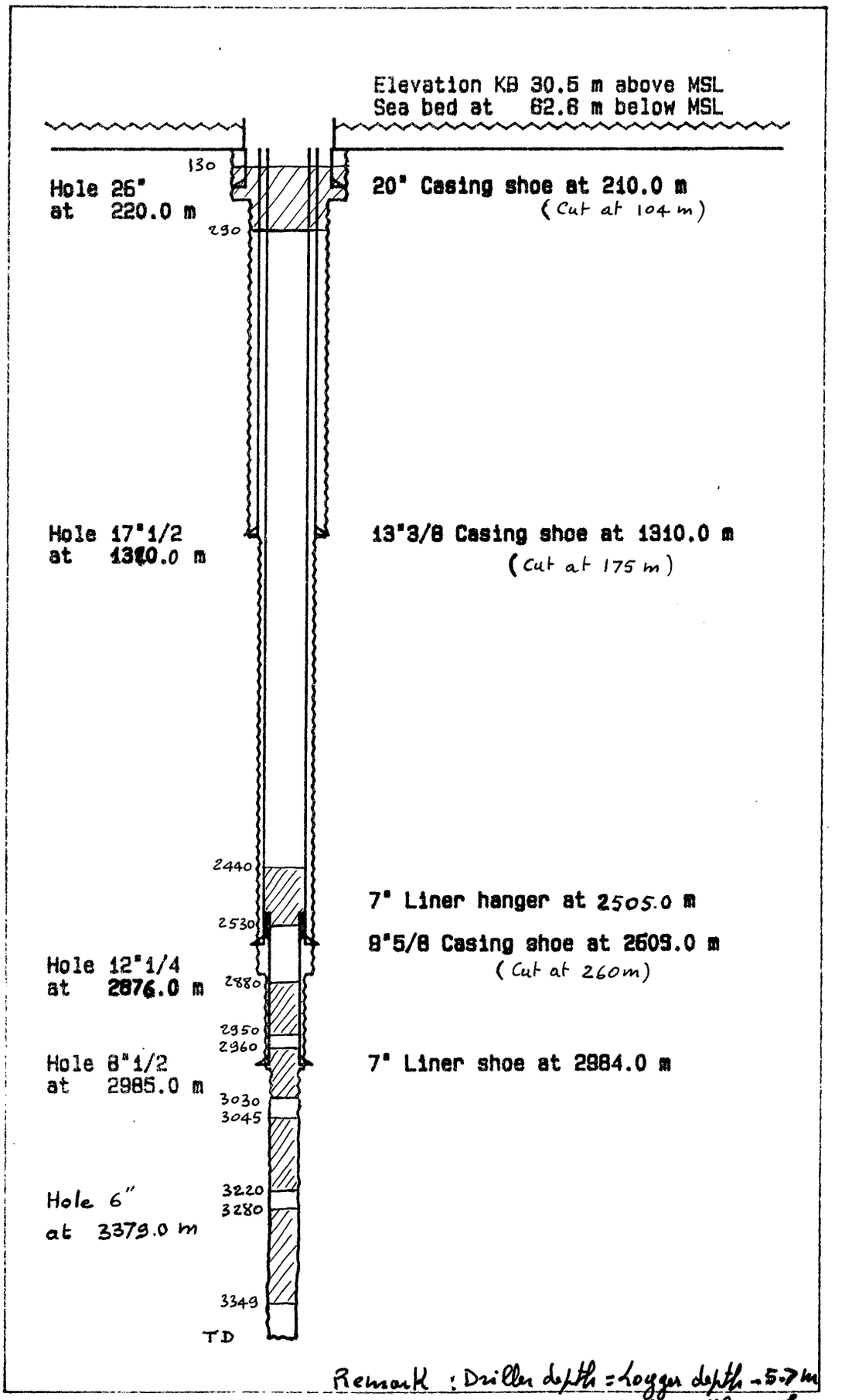
GIPPSLAND BASIN
VIC/P17

INTRA-LATROBE GREEN MARKER

Author: J. BURBURY	Date: JUNE 1982	Dwg No: 20661	Fi
Drafted by: J. PENHEY	Report No:	Base Plan: 20406	

OMEO 1

Technical Profile.



Remark : Driller depth = logger depth - 5.7 m below 7" liner shoe

OMEO 1

Perforations: 2918 - 2925 m
2932 - 2939 m

Test No. 1 Test String Composition

DESIGNATION	ID INCH	OD INCH	LENGTH METRES	DEPTH METERS / RT (DRILLER)
X Over $6\frac{3}{4}$" x $4\frac{1}{2}$" IF				- 5.00
Drill pipe 5" - $4\frac{1}{2}$" IF			87.56	
EZ Tree with $3\frac{1}{2}$" Slick joint + X overs			8.15	
Drill pipe 5" - $4\frac{1}{2}$" IF	4.27	5.0	2349.39	
Drill pipe $3\frac{1}{2}$"	2.44	3.5	286.08	
Slip joint (5" stroke)	2.25	5.0	4.01	
Slip joint (5" stroke)	2.25	5.0	4.01	
Drill collars $4\frac{3}{4}$"	2.31	4.75	110.50	
Impact reverse sub	2.75	5.0	.31	
Drill collars $4\frac{3}{4}$"	2.31	4.75	27.50	
Bar catch sub	1.00	4.75	.31	
AP. BT Case	3.06	5.0	1.25	2874.07
APR A circulation valve	2.25	5.03	.91	2874.98
APR M2 circulation valve	2.25	5.03	2.29	2877.27
APR N tester valve	2.25	5.0	3.89	2881.16
X over $3\frac{1}{2}$ IF B x $3\frac{1}{2}$ FH P	2.50	4.75	0.65	
AP. BT case	3.06	5.0	1.25	2883.06
X over $3\frac{1}{2}$ FH B x $3\frac{1}{2}$ IF P	2.50	4.75	0.23	
Full - Flo Hydraulic by-pass	2.25	4.68	1.93	
X over $3\frac{1}{2}$ IF B x 2-7/8 EUE P	2.50	4.75	0.53	
7" RTTs packer up	2.25	5.50	0.42	2886.17
7" RTTs packer down			0.72	
X over 2-7/8 EUE B x $3\frac{1}{2}$ IF P	2.50	4.75	0.29	
Perforated anchor	2.37	5.0	1.52	
Perforated anchor	2.37	5.0	1.52	
Perforated anchor	2.37	5.0	1.52	
Blanked off sub	0	4.75	0.30	
X over $3\frac{1}{2}$ FH B x $3\frac{1}{2}$ IF P	2.50	4.75	0.29	
Full - flo Bundle Carrier	2.25	5.375	2.43	2894.76
X over $3\frac{1}{2}$ IF B x $3\frac{1}{2}$ FH P	2.50	4.75	0.32	
BO BT case	2.44	5.0	1.24	2896.32

OPERATING PRESSURE:

APR N : 1390 psi

APR M2 : 2360 psi

APR A : 2750 psi

HYDROSTATIC PRESSURE:

: at APR N depth 2886.4 (logs) : 317.5 Kg / cm2 (4516 ps

water cushion (1600 m) : 176.0 Kg / cm2 (2504 ps

P on formation : 141.5 Kg / cm2 (2012 ps

RECORDER DEPTH:

: 2 ameradas + 1 RT7 at 2900 m (log)

BT at 2902 m (")

BT at 2888.5 m (log)

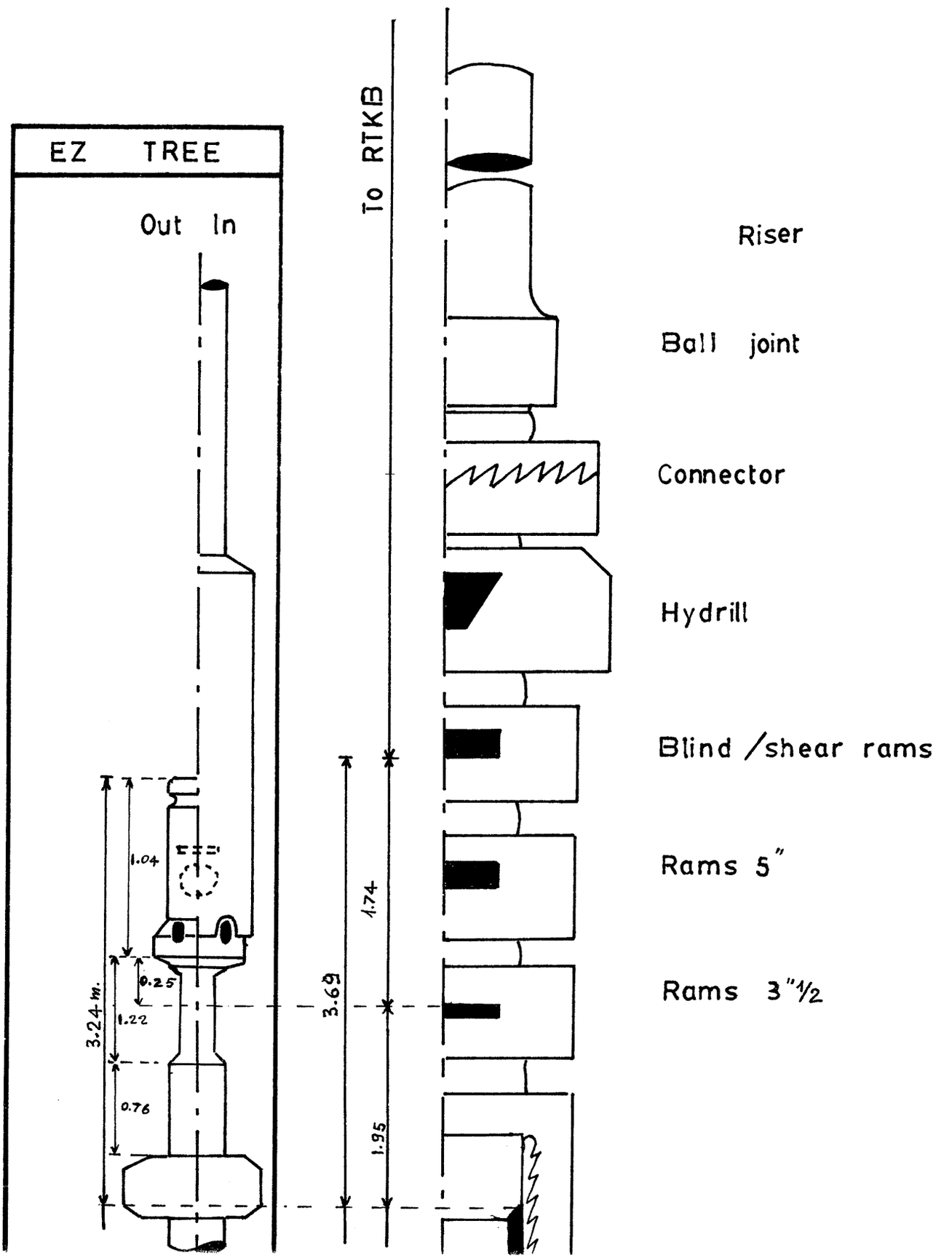
BT at 2879.8 m (")

OCEAN DIGGER

WELL OMEO 1

Fig

BOP EZ TREE SHEMATIC

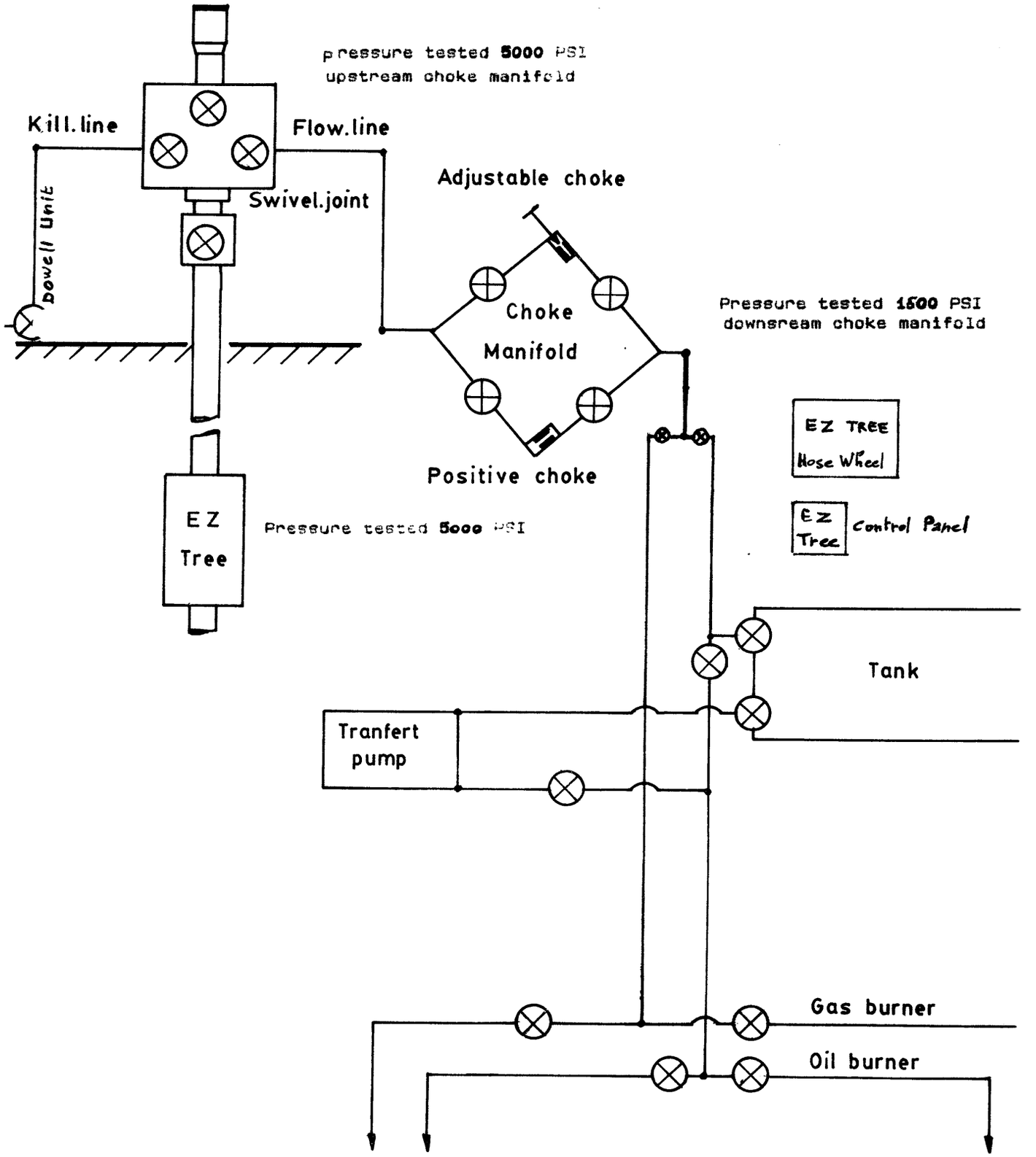


Fig

OCEAN DIGGER

OMEO # 1

SURFACE EQUIPMENT LAY OUT



OMEO 1

Perforations : 2918.0 - 2925.0 m
2932.o - 2939.0 m

Test No.1

PERTINENT VOLUMES DATA:

Liner 7" - 26 # - N80	Capacity :	19.95 l / m
Casing 9-5/8" - 47 # - N80	Capacity :	38.19 l / m
Riser 21" ID	Capacity :	223.50 l / m
Drill pipe 5" - 19.5 #	Capacity :	9.16 l / m
Drill pipe 3½" - 13.3 #	Capacity :	3.87 l / m
Drill collar 4¾"	Capacity :	2.56 l / m

ANNULUS VOLUME - (to APR - M valve) → 85.54 r

Riser - 5" drill pipe	:	210.8 x 91 = 19183 l
Casing 3-5/8 x 5" drill pipe	:	25.5 x 2367 = 60358 l
Casing 9-5/8 x 3½ drill pipe	:	32.0 x 45 = 1440 l
Liner 7" - 3½" drill pipe	:	13.7 x 239 = 3274 l
Liner 7" - 4¾" drill pipe	:	8.4 x 140 = 1190 l

TUBING VOLUME - (to APR - M valve) → 23.97

Drill pipe 5"	:	9.16 x 2458 = 22515 l
Drill pipe 3½"	:	3.87 x 284 = 1099 l
Drill pipe 4¾"	:	2.56 x 140 = 358 l

WATER CUSHION - (to APR - N valve) → 12.41
(1620

Drill pipe 5"	:	9.16 x 1196 = 10955 l
Drill pipe 3½"	:	3.87 x 284 = 1099 l
Drill pipe 4¾"	:	2.56 x 140 = 358 l

AIR CUSHION - (to surface) → 11.60
(1266

Drill pipe 5"	:	9.16 x 1266 = 11597 l

VOLUME BELOW PACKER → 0.88

LINER 7"	:	19.95 x 44 = 878 l