

**ATTACHMENT TO WCR
FORTESCUE - 3
LOGGING WELL REPORT
(W 712)**

PE906835

PSLA 78/1277



EXPLORATION LOGGING OF AUSTRALIA, INC.

A SUBSIDIARY OF **BAKER**
INTERNATIONAL

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GEOLOGICAL - ENGINEERING WELL REPORT

ESSO AUSTRALIA LIMITED

FORTESCUE No. 3

DECEMBER 1978

CONFIDENTIAL

by

EXPLORATION LOGGING OF AUSTRALIA INC.

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 ROP, Dxc, Torque, Flowline Temp,
 Pore Pressure, ECD.
- E. Morning and Weekly Reports

I. INTRODUCTION

The Fortescue No 3 delineation well was drilled in the offshore Gippsland Basin, Bass Strait, Victoria at geographical coordinates $38^{\circ} 23' 22.876''$ S and $148^{\circ} 16' 02.533''$ E. The location is 3km S.E. of Fortescue No 1 and 2 km NW of West Halibut No 1.

The well was spudded on the 26th November 1978 in 68M of water and drilled to a T.D. of 2625M on the 18th December 1978. The primary objective was further evaluation of the stratigraphy and hydrocarbon potential of the Fortescue Reservoir Unit. The objective zone was cored and tested using the wireline RFT tool and then the well plugged and abandoned on the 23rd December 1978.

Drilling was contracted to the Odeco semi-submersible rig "Ocean Digger". Exploration Logging of Australia, Inc. provided a full data acquisition and formation evaluation service using the GEMDAS Level VI system. (Geological Engineering and Data Acquisition System).

II. WELL HISTORY

- a) 26" hole section, -: 99m (seabed) - 244m (20" casing point),
26th November, 1978.

N.B. # 1 HTC OSC3AJ 17½" W/26" hole opener 99-244m

The well was spudded with seawater and no returns to surface using a 17½" bit in tandem with a 26" hole opener. The 26" hole was drilled to 244m and a survey run indicating hole deviation of 1°. 700bbls of pre-hydrated gel mud were spotted in the open hole before pulling out to run the 20" casing. The 20" casing was then run and cemented with the shoe at 225m.

- b) 17½" hole section, 244 - 878m (13 3/8" casing point)
27-29th November 1978.

N.B. #2 HTC OSC3AJ 17½" 244-878m

After setting the 20" casing the shoe was drilled out and a 17½" hole drilled to 260m using sea-water. At 260m the sea-water was displaced by a sea-water-gel system and drilling of the 17½" hole continued with 8.9 ppg mud in the hole. Initially drill rates were as high as 300-400 m/hr but these rapidly decreased such that an average drill rate of 100m/hr was apparent over the first 300m of the section.

The samples over this section were initially calcarenites with abundant shell fragments and microfossils. With a change from 550m the samples showed a change to a more argillaceous marl/calciilutite with occasional calisiltite. With this lithology change the average drill rate also dropped to an average 60m/hr and then further decreased to about 20m/hr when approaching casing point below 800 metres. The gas readings whilst drilling this section remained around an average background of 5-10 units with occasional peaks up to 24 units. C₁ and C₂ only were recorded on the chromatographic analysis.

At 878m a wiper trip was made and the bit pulled to run wireline logs. FDC-GR (from TD - Sea bed), ISF - SONIC (from TD - 20" casing shoe). After running wireline logs the 13 3/8" casing was run and cemented with the shoe at 867m.

c) 12 $\frac{1}{4}$ " hole section, 878-1536m, 1-4 December 1978

NB #3	HTC	X1G	12 $\frac{1}{4}$ "	878 - 1271m
NB #4	HTC	X3A	12 $\frac{1}{4}$ "	1271 - 1508m
NB #5	HTC	X3A	12 $\frac{1}{4}$ "	1508 - 1536m

After cementing the 13 3/8" casing a 12 $\frac{1}{4}$ " BHA was picked up with Bit No.3, a HTC X1G with 18,18,18 jets and drilling of the 12 $\frac{1}{4}$ " hole continued with a lightly treated seawater-gel mud system with mud wt running about 9.1 ppg. After drilling out the 13 3/8" shoe, 15m of fresh formation was cut and drilling was halted at 893m to conduct a Formation Integrity Test (leak off test). The formation was pressured up to an equivalent mud weight of 13.7 ppg and no leak off was induced. Thus the fracture pressure at 893m is in excess of 13.7 ppg E.M.W. After the test, drilling continued in a sequence of calcisiltites, at rates varying from 8m - 100m/hr with an average rate of 37m/hr for the interval 878 - 1271m, the higher drill rates occurring from between 893m - 1271m.

No.4 bit, an HTC X3A 12 $\frac{1}{4}$ " bit with 18,18,18 jets was run in at 1271m and drilling proceeded to 1508m with the only problems arising from pump breakdowns. The average drill rate for this bit was 12 m/hr on a sequence of marls and calcareous mudstones.

On making a trip at 1508m, tight hole was encountered up to 1050m, and the hole did not take any mud during the trip out. Possibly the low circulation rates during the pump breakdown had reduced the "carrying capacity" of the circulatory system leading to a build up of cuttings around the drill string. After running the pipe back to bottom and circulating with high viscosity mud, the hole was circulated clean and the trip out was made without any further problems.

Drilling was resumed with Bit No.5, another HTC X3A 12 $\frac{1}{4}$ " bit with 18,18,18 jets when 2000 units of gas were yielded from a drill break at 1526m (Increase from 13m/hr to 21m/hr). Chromatographic analysis of the ditch gas indicated C₁ with traces of other hydrocarbons through to C₄. As a result of the high gas the mud weight was raised to 9.6 ppg and the hole conditioned prior to tripping out to run a core barrel.

d) 8 15/32" hole section, 1536 - 1548.6m, 4 December 1978.
 CB #1 CHRIS C20 8 15/32 1536 - 1548.6m

Core barrel No 1 was run in and core cut from 1536 - 1548.6m. Core recovery was 100% with no hydrocarbon shows in an overall lithology of marl.

e) 12 $\frac{1}{4}$ " hole section, 1548.6 -2409.5m, 4 - 12 December 1978

NB #6	HTC	X3A	12 $\frac{1}{4}$ "	1548.6 - 1600m
NB #7	HTC	X3A	12 $\frac{1}{4}$ "	1600 - 2052m
NB #8	HTC	X3A	12 $\frac{1}{4}$ "	2052 - 2409.5m

Bit No.6, a HTC X3A 12 $\frac{1}{4}$ " bit with 18,18,18 jets was then run and after reaming the core rat hole drilling continued normally with a background gas level of about 10 units at an average drill rate of 20 m/hr in a calcareous mudstone section. At 1600m problems with the BOP stack arose and drilling was temporarily suspended from the 6 - 8 December to make repairs.

Bit No.7, an HTC X3A 12 $\frac{1}{4}$ " bit with 18,18,20 jets was run after repairs to the stack. Trip gas at 1600m was 180 units (after being out of the hole 3 days) and drilling of the 12 $\frac{1}{4}$ " hole continued till 2052m at an average rate of 20 m/hr. Over this interval the lithology consisted of typical "Lakes Entrance Formation" calcareous mudstones with interbeds of calcisiltites. Between 1759 - 1762m and 1766 -1767m, salt water sensitive clays were encountered which produced high volumes of cavings and gave rise to viscosity problems with the mud. From 2000m the mud system was converted over to a polymer system to counter this problem.

Bit No 8, a HTC X3A 12 $\frac{1}{4}$ " bit with 20,20,20 jets resumed drilling in a predominantly calcareous mudstone lithology with an average drill rate of 19 m/hr until pulled at 2409.5m due to high torque readings. Returns were then circulated with the flowline temporarily blocking.

f) 8 15/32" hole section, 2409.5 - 2417m, coring 12 - 15 December 1978.

CB #2	CHRIS	RRC20	8 15/32	2409.5 - 2410.5m
CB #3	CHRIS	RRC20	8 15/32	2410.5 - 2416m
CB #4	CHRIS	RRC20	8 15/32	2416m
CB #5	CHRIS	RRC20	8 15/32	2416 - 2417m

From 2409.5 - 2417m, another four cores were attempted with varying success, the problems encountered being a jammed core barrel for CB #2 (cut 1m, 40% recovery), loss of 200 psi pump pressure coupled with severe sea conditions for CB #3, (cut 5.5m, 27% recovery), inability to drill for CB #4, no recovery and jammed barrel for CB #5, (10% recovery.) The nature of the encountered lithology, a calcareous mudstone, no doubt hindered successful coring to a large extent.

g) 12 $\frac{1}{4}$ " hole section, 2409.5 - 2440m, 15 - 16 December 1978.

NB #9	HTC	XDG	12 $\frac{1}{4}$ "	2409.5 - 2440m
-------	-----	-----	--------------------	----------------

At 2417m, Bit No 9, an HTC XDG 12 $\frac{1}{4}$ " bit with 15,15,14 jets was run in and the core rat hole reamed with drilling proceeding to 2440m at an average rate of 12 m/hr until a drilling break and gas peak of 30 units indicated the top of the "payzone".

h) 8 15/32" hole section, 2440 - 2480m; coring 16 - 18 December 1978.

CB	#6	CHRIS	C22	8 15/32	2440-2456m
CB	#7	CHRIS	RRC22	8 15/32	2456 - 2470m
CB	#8	CHRIS	RRC22	8 15/32	2470 - 2480m

Core Barrel No.6 was run in and bottom up circulated prior to coring.

Core No.6 was cut at an average penetration rate of 4.7 m/hr with 24000lbs and 84 RPM. Recovery was 71 % - 11.4 metres of hydrocarbon bearing sandstone core.

Core Barrel No. 7 was run and drilled at an average rate of 5.0 m/hr with 22,000 lbs and 102 RPM. 9.0m of hydrocarbon bearing sandstone were recovered down to 2465m, the lowest depth recovered, for a recovery of 64%.

Core Barrel No.8 was run in and drilled at an average rate of 3.3 m hr with 25000lbs and 85 RPM from 2470 to 2480m with zero core recovered.

i) 12 $\frac{1}{4}$ " hole section, 2440 - 2625m (TD), 18 - 19 December 1978.

RRNB	#9	HTC	XDG	12 $\frac{1}{4}$ "	2440-2625m
------	----	-----	-----	--------------------	------------

Following coring, Bit No.9 a HTC XDG 12 $\frac{1}{4}$ " bit was rerun and after reaming the core rathole, drilling continued normally to TD at 2625m. The section encountered consisted mainly of sandstone with frequent coal seams and shaly intervals. Average rate of penetration was initially 30 m/hr gradually dropping off to around 10 m/hr near TD. At 2625m. a full suite of wireline logs was run consisting of the following:-

ISF - BHC Sonic - MSFL; FDC - CNL - GR, HDT, Velocity Survey, RFT's and CST's.

Fortescue No. 3 was plugged and abandoned on the 23rd December 1978.

III. GEOPRESSURE ENGINEERING

A. PORE PRESSURE.

Fortescue No. 3 was found to have a normal hydrostatic pore pressure regime throughout the entire section drilled. No pressure related problems were encountered. Refer to Appendix C (iii) for a graphical presentation of the pore pressure regimes in Fortescue No 3.

The following parameters, drill rate, drilling exponent, flowline mud temperature, gas and hole behaviour were all continuously monitored and plotted in order to evaluate the formation pore pressure and detect any abnormal pressure during drilling. Refer to Appendix C (i) and (ii).

Pressure points plotted from the RFT runs give a water pressure gradient of about 8.55 ppg. Formation water RW values from wireline logs give water salinities of around 35,000 ppm which converts to a hydrostatic pressure gradient of 8.5 ppg. It is, therefore, safe to assume that the normal hydrostatic pressure gradient for Fortescue No. 3 to be 8.55 ppg.

LITHOLOGY -

Because of the absence of clean shales throughout the well, very little in the way of quantitative analysis could be performed. However, general compaction trends modified locally by lithological variations are readily observable in both the drill rate and drilling exponent plots.

DRILL RATE -

The top hole section of the well drilled at rates of up to 400 m/hr. These decreased with depth to 8 m hr. Apart from minor fluctuations the decrease was uniform. Eight cores were cut between 1536 - 1548m, 2409 - 2417 and 2440 - 2480 metres. Drill rates below 2400m during coring varied from 1 m/hr in siltstone to a maximum of 11.6 m hr in sandstone. The remainder of the well was drilled in a sequence of interbedded sandstones, siltstones and coal which were erratic in behaviour as regards drill rate and drilling exponents.

The use of bumper subs in the drill string was an obstacle to the accurate determination of drill rates and subsequent drilling exponent analysis. Wherever possible these inaccuracies have been removed.

DRILLING EXPONENTS -

As a result of the absence of clean shales it was not possible to establish a normal trend line for corrected 'd' exponent which was suitable for quantitative use. However, for the lithologies encountered normal compaction trends were readily apparent. A shift in trend does occur below 1750 metres, however, this was not considered to be an indication of abnormal pressure but a reflection of the change in the nature of the lithology in the interval below the base of xtalline limestone at 1750 metres. The 'd' exponent, being a compaction indicator might prove useful in the area for correlating and detecting seismic marker horizons as it has on the N.W. Shelf of W.A.

GAS -

Background gas ranged from a low of $\frac{1}{2}$ unit to 20 units. The maximum gas reading recorded was 2000 units at 1526 metres over a one metre interval. Below 1325 metres average background gas showed a steady decrease to 2 units to TD. Hydrocarbons were indicated in sands in cores #6, #7 and #8.

No connection gases were recorded and trip gas values were consistent with influencing factors such as length of time spent out of the hole, maximum trip gas of 180 units being recorded at 1600 metres after 3 days out of the hole to repair the stack and 100 units at 2052 metres. These were taken to be an indication that the pressure regime of the area was normal.

TEMPERATURE -

Continuous monitoring of the flowline temperature was carried out in an attempt to locate transition zones in the geothermal gradient due to changes in the thermal conductivity of the formations due to the presence of excess pore fluids. On all occasions when sudden decreases or increases in the flowline temperature occurred, either the addition of water or chemicals to the mud system was the apparent cause.

Calculations based on the flow line temperature data collected indicate that a normal regional trend of 1.12°C was in effect for Fortescue with the maximum temperature recorded in the flowline being 47.4°C at 2406 metres prior to the disruption of the mud system by coring at 2409.5 metres.

B. FRACTURE PRESSURE

The values of overburden pressure gradient (OBG) and estimated formation fracture gradient (FFG) are presented in Appendix C (iii). The overburden gradient curve was calculated by taking averaged formation density readings from the FDC log and summing the values for the whole well section. An averaged density from surface to any point is used to calculate the overburden pressure at that point. The kelly bushing was used as the zero datum level.

After establishing the OBG curve for the well the values were used to calculate theoretical fracture pressures using the "Mathews and Kelly" and "Eaton" methods which are derived from Gulf Coast data. These methods are explained more fully in Appendix A.

These theoretical values were compared with the one leak off test or formation integrity test (F.I.T.) of 13.7 ppg (without leak off) conducted on the 13 3/8" casing shoe at 867m. Assuming a true leak off of 14.0 ppg at the shoe then the methods give low theoretical results using coefficients derived from the Gulf Coast. Mathews and Kelly's method gave 12.78 ppg and Eatons method gave 11.47 ppg. In order to correct the coefficients a revised poissons ratio was back calculated from the FIT at the shoe and an acceptable fracture gradient curve produced for the whole well using Eatons method.

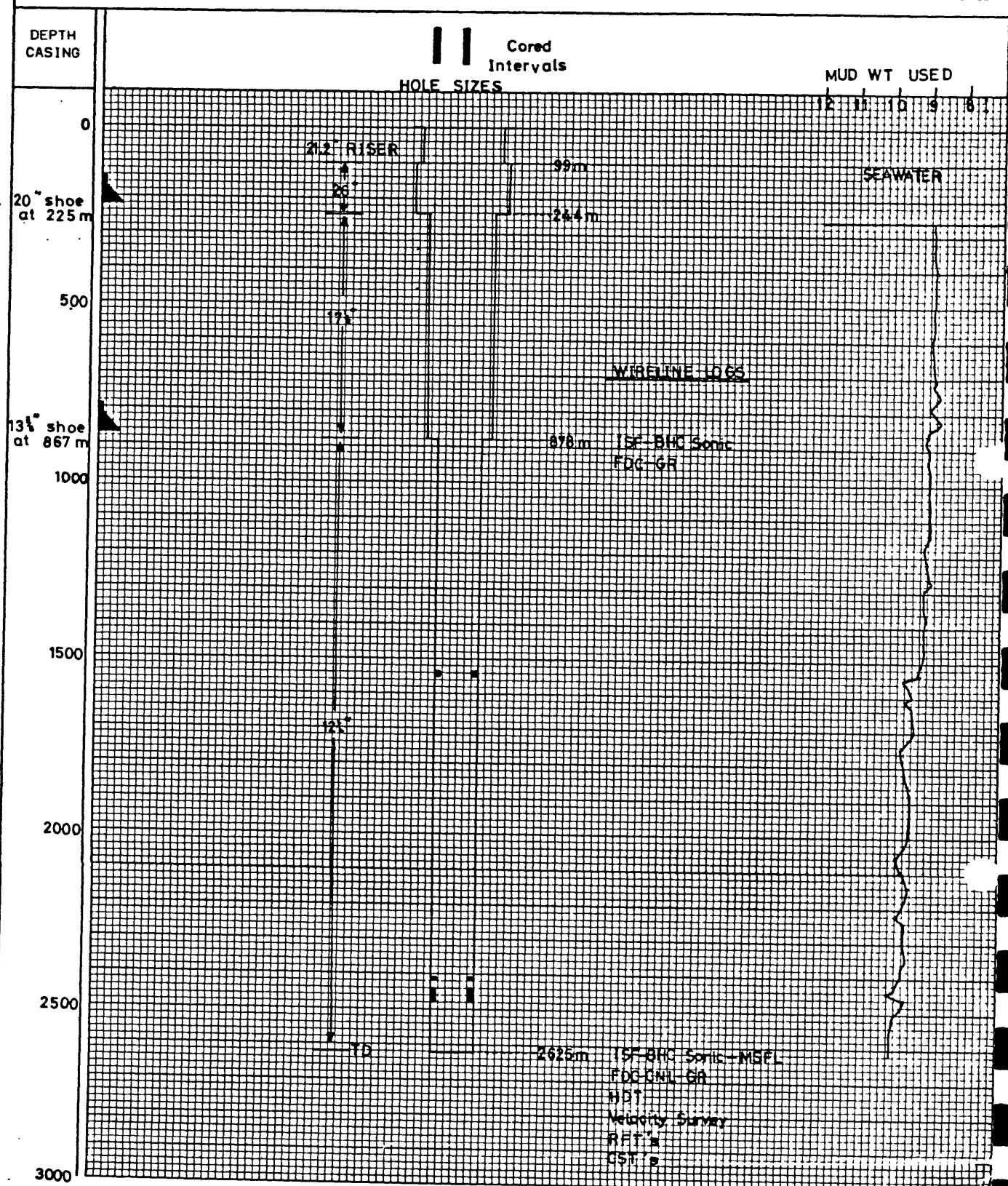
Due to the absence of abnormal pore pressure in the well, mud weights were low and no lost circulation problems encountered. Kick tolerance at 2625m, assuming 14.0ppg breakdown at the shoe and a 10ppg mud in the hole, is however only 1.3ppg EMW.

IV. DRILLING ENGINEERING

Monitoring and analysis of the Drilling Engineering at the wellsite was centred on the Bit Analysis, Hydraulics, Hole Condition and Hole Deviation.

The pertinent data for each engineering aspect covered is presented in a tabular format, in this section.

More detailed analysis of all the engineering parameters relevant to the drilling of the well, such as weight on bit, rate of penetration, torque, mud characteristics, detailed hydraulics and flow regime analysis, are presented in Appendix D as hard copy computer printouts and plots reduced to size for this Report or reference to the original listings in the Esso files.



A. WELL DATA

B.

BIT SUMMARY - COST ANALYSIS FORTESCUE No.3

BIT NO.	SIZE	MAKE	TYPE	IADC CODE	JET SIZES	DRILLED INTERVAL	DISTANCE DRILLED (m)	HOURS	AV ROP (m/hr)	FINAL COST/ METER	ACTUAL AVERAGE			TOTAL BIT REVOLUTIONS	IADC BIT CONDITION	REASON FOR PULLING BIT	
											WOB	RPM	TORQUE				
1	Spud in with 17 $\frac{1}{2}$ HTC OSC	3AJ	W/ 25" Hole opener and 20,20,20 jets.	Drill 1	to 244m and set 20" casing at 225m												
2	17 $\frac{1}{2}$	HTC	OSC 3AJ	1111	20,20,20	244-878	634	12.6	50	53	30	120	5000	93499	2 3 0	Run wireline logs set 13 3/8 csg at 867	
3	12 $\frac{1}{2}$	HTC	XIG	1341	18,18,18	878-1271	393	10.6	37	78	40	120	5000	82753	3 8 1/16		
4	12 $\frac{1}{2}$	HTC	X3A	1141	18,18,18	1271-1508	237	19.6	12	215	50	120	5000	134715	3 7 1/16	Slow drill rate, pump problems	
5	12 $\frac{1}{2}$	HTC	X3A	1141	18,18,18	1508-1536	28	1.6	17.5	538	50	120	5000	10964	3 1 0	pull to core	
Core No.1	8 15/32	CHRIS	C20	9999	-	1536-1548.6	12.6	0.6	21	1001	35	80	3000	9090		coring	
6	12 $\frac{1}{2}$	HTC	X3A	1141	18,18,18	1548 6-1600	51.4	2.5	20	323	51	120	5500	24412	1 1 0	defect in BOP	
7	12 $\frac{1}{2}$	HTC	X3A	1141	18,18,20	1600-2052	452	22.5	20	129	50	135	5500	180569	3 8 0		
8	12 $\frac{1}{2}$	HTC	X3A	1141	20,20,20	2052-2409.5	357.5	19.1	19	150	48	150	6000	146366	4 7 0	High torque - seized cone slow drill rate	
Core No.2	8 15/32	CHRIS	C20	9999	-	2409.5-2410.5	1.0	1.0	1.0	9032	20	85	3500	5837	-	barrel jammed	
Core No.3	8 15/32	CHRIS	C20	9999	-	2410.5-2416	5.5	5.2	1.0	5660	20	80	4000	28042	-	Severe sea conditions	
Core No.4	8 15/32	CHRIS	C20	9999	-	-	-	-	-	-	-	-	-	-	-	barrel jammed	
Core No.5	8 15/32	CHRIS	C20	9999	-	2416-2417	1.0	2.2	0.45	14400	28	50	3000	4965	-	barrel jammed.	
9	12 $\frac{1}{2}$	HTC	XDG	1351	15,15,14	2409.5-2440	23	1.9	12.1	1015	47	112	7000	18790	1 1 0	hit payzone pull to core	
Core No.6	8 15/32	CHRIS	C22	9999	-	2440-2456	16	3.4	4.7	2075	24	85	6000	16688	-	Coring Rec 11.4m	
Core No.7	8 15/32	CHRIS	C22	9999	-	2456-2470	14	2.8	5.0	1223	22	102	3800	34013	-	Coring Rec 9m	
Core No.8	8 15/32	CHRIS	C22	9999	-	2470-2480	10	3.0	3.3	1026	25	85	3000	48576	-	Coring Rec 0m	
RR 9	12 $\frac{1}{2}$	HTC	XDG	1351	15,15,14	2480-2625	145	11.6	12.5	310	35	110	5000	97208	-	T.D. at 2625m.	

C. HYDRAULICS ANALYSIS

FORTESCUE No.3

DEPTH INTERVAL (M)	Bit Hydraulic HP	Impact Force (lb)		%Pressure Drop at Bit		Jet Pressure Drop (PSI)		Jet Velocity ft/sec		Mud Wt in PPG		PV/YP					
		244-878	878-1600	1600-2052	2052-2410	2410-2417	2410-2440	2440-2480	2440-2625	Riser	Pipe	Collars	Critical (adj.Collars)				
244-878	17½	20,20,20	50	950	110	1800	95	83	56	-	8.9	4/9	331	883	49	1465	489
878-1600	12¼	18,18,18	21	900	105	2700	245	176	52	284	9.1	8/13	387	1221	45	1642	641
1600-2052	12¼	18,18,20	20	840	97	2905	219	164	48	309	9.5	10/16	335	956	33	1385	468
2052-2410	12¼	20,20,20	19	850	98	2800	222	166	49	330	9.5	12/18	296	746	27	1238	370
2410-2417	8 15/32	Coring	3	290	34	1550	76	59	Boost	-	9.6	14/20	-	-	-	-	-
2410-2440	12¼	15,15,14	12	660	76	3000	180	129	38	350	9.6	15/20	427	1577	53	1409	607
2440-2480	8 15/32	Coring	4	280	32	1550	76	54	Boost	-	9.6	16/20	-	-	-	-	-
2440-2625	12¼	15,15,14	12	640	74	2860	174	125	37	356	9.8	17/21	414	1521	53	1359	568

D. HOLE CONDITION

The borehole condition was monitored during the drilling of the well by observing the differential lag time, the type, percentage, size and shape of the cavings, the hole deviation, the estimated differential pressure, the percentage of swelling clays, and the differential annular velocity adjacent to the drill collars. During trips hole drag and fillup were monitored and recorded.

Hole problems were encountered in the section of the hole above 2409 metres and manifested themselves as either tight hole, blocked flowline or excessive cavings.

Tight hole was encountered during trips at 878, 1271 and 1508 metres. Tight hole caused most problems with the trip at 1508 metres, being present over the interval 1508 - 1050 metres. The same problem to a lesser extent was detected at 1111m. on the trip out at 1271 metres. Both problems were resolved without major changes to the mud system.

Blocked flowline and excessive cavings are attributed to a large extent to the reaction of the clays at 1759 metres with the salt water/gel mud. Change over of the mud system to a polymer one resolved this problem.

Excessive cavings were only encountered during 1759 - 1767 metre interval with estimates of percentage cavings rarely exceeding 5% during normal drilling. Comparison of calculated versus actual carbide log times also indicated a stable in-gauge hole condition.

V. HYDROCARBON EVALUATION

INTRODUCTION -

Hydrocarbon evaluation at the wellsite was performed while drilling by use of standard mud logging techniques. These included "hot wire" gas detection which indicated the relative amount of combustible gas in the drill returns. Both total gas and petroleum vapours (all combustible gases less methane) were monitored and recorded.

Gas held in cuttings was assessed by pulverising 100 cc's of cuttings in a blender with water and measuring the amount of gas liberated. A comparison of the cuttings' gas magnitude with that of the ditch gas was used to give a qualitative indication of formation permeability.

Ditch gas was analysed continuously and automatically by three chromatographs, standard catalytic, hydrogen flame ionization and thermo conductivity. The catalytic detector can become saturated at high gas levels and the flame ionization detector is used as a back-up in this event. The thermoconductivity chromatograph was used to detect inert gases, nitrogen and helium and also for carbon dioxide.

Samples of mud and pulverised cuttings gas were manually entered into the standard chromatograph directly from the blender.

Oil evaluation was undertaken by observing the mud and unwashed cuttings for oil. Cuttings samples were observed under the ultraviolet light for all fluorescence and solvent cut.

RESULTS -

Gas readings from Fortescue No. 3. were very low from 244m to 440m at less than 1 unit composed of C₁ methane only. From 440m to 2437m the background gas varies from 2 to 24 units with no prominent peaks and it is composed of C₁ and C₂ with occasional traces of C₃. There is one notable exception at 2526m where a 2000+ unit gas peak was detected composed of the gas C₁ through C₄. The peak was associated with a thin sandy interval which displayed a good trace of very light yellow fluorescence and white cut.

The main zone of interest was penetrated at 2437m to 2440m where 30 units of gas was produced from a sandstone. C₁ methane to C₅ pentane were detected and good fluorescence and cut was observed in the cuttings along with traces of oil in the mud. The section 2440m to 2480m was cored and few

readings were obtained due to slow circulation rates. The few results that were obtained were less than 2 units, but C₁ through to C₅ were present. The cores from 2440m showed good fluorescence, cut and oil staining.

In the interval 2480m to 2625m, the background gas was relatively low at 2 to 3 units with C₁ to C₄ present, the heavier gases decreasing in percentage with depth.

After drilling to TD at 2625m, wire line logs were run and the following RFT results obtained.

RFT No 1 - Depth 2440.0m

<u>Recovery</u>	<u>Chromatograph Analysis</u>	
C ₁	640,000	ppm
C ₂	109,350	"
C ₃	109,575	"
16,100 cc oil - 45 API at 60° F	I C ₄	35,325
1000 cc Filtrate - 3900 Cl ⁻	nC ₄	30,150
1750 cc oil/filtrate emulsion	C ₅	11,925
7.3 ft ³ gas	He?	1,000
	CO ₂	-
	H ₂ S	-

RFT No 2 - Depth 2448.5m

<u>Recovery</u>	<u>Chromatograph Analysis</u>
500 c.c oil - 41 api at 77° F.	Not enough gas to analyse
19900 c.c. Filtrate - 6000 Cl ⁻	
0.3 ft ³ gas	

RFT No 3 - Depth 2462m

<u>Recovery</u>	<u>Chromatograph Analysis</u>
19000 c.c formation water - 12,000 Cl ⁻	No gas

RFT No 4 - Depth 2457.5m

<u>Recovery</u>	<u>Chromatograph Analysis</u>
19000 c.c filtrate 6,000 Cl ⁻	Not enough gas to analyse
0.2 ft ³ gas	

RFT No 5 - Depth 2454.5m

<u>Recovery</u>	<u>Chromatograph Analysis.</u>		
	C ₁	103,360	ppm
	C ₂	59,230	"
3000 c.c oil 45 API at 68° F	C ₃	96,220	"
17000 c.c filtrate - 5800 Cl ⁻	IC ₄	28,910	"
0.4 ft ³ gas	NC ₄	26,360	"
	C ₅	7,950	"

Not enough gas for He, CO₂ and H₂S analysis.

GAS RATIOS

A gas ratio analysis of the chromatograph readings from 2110m to 2620m plus the RFT readings from runs 1 and 5 are presented in the table in figure 1.

Analysis of the plot of the C₁ / C₂ ratio from 2110m to 2620m (figure 2) shows a decrease in the C₁ / C₂ ratio at 2300m coinciding with the increase in formation shaliness at this depth. The hydrocarbon zone at 2437m is clearly evident on the plot with a further sharp drop in the C₁/C₂ ratio. Unfortunately the oil/water contact is not discernable due to the paucity of readings in the interval 2440 to 2480m.

Figure 3 is a gas ratio plot of the chromatograph readings at 2440m (mud stream) which attempts to determine the hydrocarbon phase and possible productivity by using the inverse methane ratios. In this case an oil zone is indicated which is probably non-productive due to the lower C₁/C₃ ratio compared to C₁/C₂.

Figure 4 is a triangular gas plot of the chromatograph readings from the RFT at 2440m. From experiment, a hydrocarbon coefficient (HC) of < 0.003 indicates an unproductive zone, 0.003<HC<0.175 indicates gas and HC>1.175 indicates oil. In this case the plot indicates a marginally productive oil zone.

In conclusion, the analysis suggests an oil bearing zone from 2437m to at least 2465m, and a probably productive zone at 2440m, the only interval with enough data to analyse. The oil/water contact could not be determined.

INTERACTION LOG.CFG

FORTESCUE NO 3

GAS RATIOS ANALYSIS

OFF-LINE PRINT-OUT

FILE#	DEPTH#	PPM					% OF TOTAL GAS					METHANE RATIOS					ETHANE RATIOS					PROPANE				IC4 DELTA										
		ft/ft	C1	C2	C3	IC4	nC4	CS	TOTAL	C1	C2	C3	IC4	nC4	CS	C2	C3	IC4	nC4	CS	C3	IC4	nC4	CS	IC4	nC4	CS	nC4	C's	IC4 DELTA						
21	21101	745	15	0	0	0	0	0	7601	98.03	1.97	0.00	0.00	0.00	0.00	.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	98.031				
31	21201	548	10	0	0	0	0	0	5581	98.21	1.79	0.00	0.00	0.00	0.00	.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	98.211				
41	21301	460	10	0	0	0	0	0	4701	97.87	2.13	0.00	0.00	0.00	0.00	.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	97.871				
51	21401	700	10	0	0	0	0	0	7101	98.59	1.41	0.00	0.00	0.00	0.00	.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	98.591				
61	21501	1360	20	0	0	0	0	0	13801	98.45	1.45	0.00	0.00	0.00	0.00	.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	98.551				
71	21601	591	28	0	0	0	0	0	6191	95.48	4.52	0.00	0.00	0.00	0.00	.05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	95.481				
81	21701	1752	28	0	0	0	0	0	17801	98.43	1.57	0.00	0.00	0.00	0.00	.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	98.431				
91	21801	191	25	0	0	0	0	0	19961	98.75	1.25	0.00	0.00	0.00	0.00	.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	98.751				
101	21901	1117	35	0	0	0	0	0	11521	96.96	3.04	0.00	0.00	0.00	0.00	.03	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	96.951				
111	22001	919	10	0	0	0	0	0	9291	98.92	1.08	0.00	0.00	0.00	0.00	.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	98.921				
121	22101	1270	20	0	0	0	0	0	12901	98.45	1.55	0.00	0.00	0.00	0.00	.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	98.451				
131	22201	1007	20	0	0	0	0	0	10271	98.05	1.95	0.00	0.00	0.00	0.00	.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	98.051				
141	22301	1095	15	0	0	0	0	0	11101	98.65	1.35	0.00	0.00	0.00	0.00	.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	98.651				
151	22401	1226	28	0	0	0	0	0	12541	97.77	2.23	0.00	0.00	0.00	0.00	.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	97.771				
161	22501	701	10	0	0	0	0	0	7111	98.59	1.41	0.00	0.00	0.00	0.00	.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	98.591				
171	22601	1007	15	0	0	0	0	0	10221	98.53	1.47	0.00	0.00	0.00	0.00	.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	98.531				
181	22701	1095	15	0	0	0	0	0	11101	98.65	1.35	0.00	0.00	0.00	0.00	.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	98.651				
191	22801	1358	10	0	0	0	0	0	13681	99.27	.73	0.00	0.00	0.00	0.00	.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	99.271				
201	22901	1226	10	0	0	0	0	0	12361	99.19	.81	0.00	0.00	0.00	0.00	.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	99.191				
211	23001	1139	36	0	0	0	0	0	11751	96.94	3.06	0.00	0.00	0.00	0.00	.03	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	96.941				
221	23101	438	21	0	0	0	0	0	4591	95.42	4.58	0.00	0.00	0.00	0.00	.05	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	95.421				
231	23201	964	35	0	0	0	0	0	9991	96.50	3.50	0.00	0.00	0.00	0.00	.04	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	95.501				
241	23301	1051	20	0	0	0	0	0	10711	98.13	1.87	0.00	0.00	0.00	0.00	.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	98.131				
251	23401	963	40	0	0	0	0	0	10031	96.01	3.99	0.00	0.00	0.00	0.00	.04	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	96.011				
261	23501	745	10	0	0	0	0	0	7551	96.68	1.32	0.00	0.00	0.00	0.00	.01	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	96.681				
271	23601	767	28	0	0	0	0	0	7951	96.48	3.52	0.00	0.00	0.00	0.00	.04	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	96.481				
281	23701	405	35	0	0	0	0	0	10861	96.78	3.22	0.00	0.00	0.00	0.00	.03	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	96.781				
291	23801	547	10	0	0	0	0	0	5571	98.20	1.80	0.00	0.00	0.00	0.00	.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	98.201				
301	23901	306	8	0	0	0	0	0	3141	97.45	2.55	0.00	0.07	0.00	0.00	.03	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	97.451				
311	24001	481	21	0	0	0	0	0	5021	95.82	4.18	0.00	0.00	0.00	0.00	.04	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	95.821				
321	24101	1200	25	0	0	0	0	0	12251	97.96	2.04	0.00	0.00	0.00	0.00	.02	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	97.961				
331	24201	420	12	0	0	0	0	0	4321	97.22	2.78	0.00	0.00	0.00	0.00	.03	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	97.221				
341	24301	440	26	15	0	0	0	0	4811	91.48	5.41	3.12	0.00	.07	0.00	.01	.08	0.00	.01	.06	.01	.07	.01	.08	.01	.09	.01	.08	.01	.09	.01	.08	.01	.09	88.361	
351	24401	471	24	40	0	0	0	0	6071	69.19	8.24	7.74	5.27	9.56	0.00	.12	.11	.08	.04	.01	.06	.01	.07	.01	.08	.01	.09	.01	.08	.01	.09	.01	.08	.01	.09	84.361
361	24501	380	4																																	

OFFLINE PLOT OF DEPTH AGAINST HYDROCARBON COEFFICIENT (HC) AND C1/C2

FORTESCUE NO 3 **FROM** **2110** **TO** **2620**

$\Delta C = (C_2 + C_3 + NC_4) = 0.01$ PLOT CHARACTERS := NC (-) C1/C2 (*)

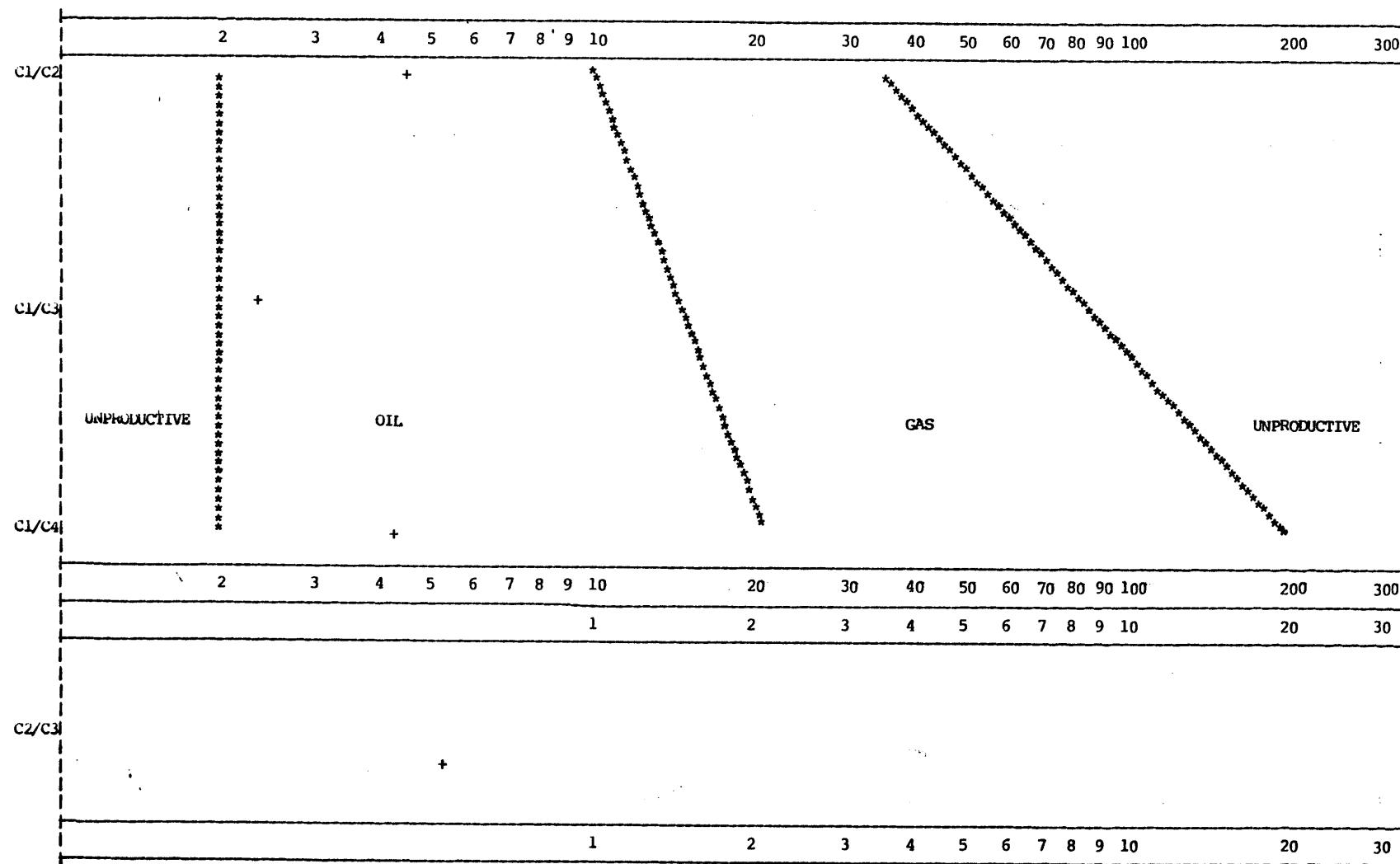
The figure consists of five vertically stacked plots, each representing a different time step from $t=2100$ to $t=2700$. The x-axis for all plots is labeled with values 0.001 , 0.01 , 0.1 , 1 , 10 , 100 , and 1000 at the top. The y-axis for all plots is labeled with values 0.001 , 0.01 , 0.1 , 1 , 10 , 100 , and 1000 on the left. Each plot contains a series of points forming a spiral pattern that moves downwards and to the right. The points are represented by small crosses (+). The spiral pattern is more pronounced in the earlier time steps (2100t, 2200t, 2300t) and becomes more horizontal and less distinct in the later time steps (2400t, 2500t, 2600t).

Figure 2

GAS RATIO PLOT TO DETERMINE POSSIBLE PRODUCTIVITY AND HYDROCARBON PHASE

FORTESCUE NO 3

INTERVAL FROM 2440 TO 2440



NOTES

Figure 3

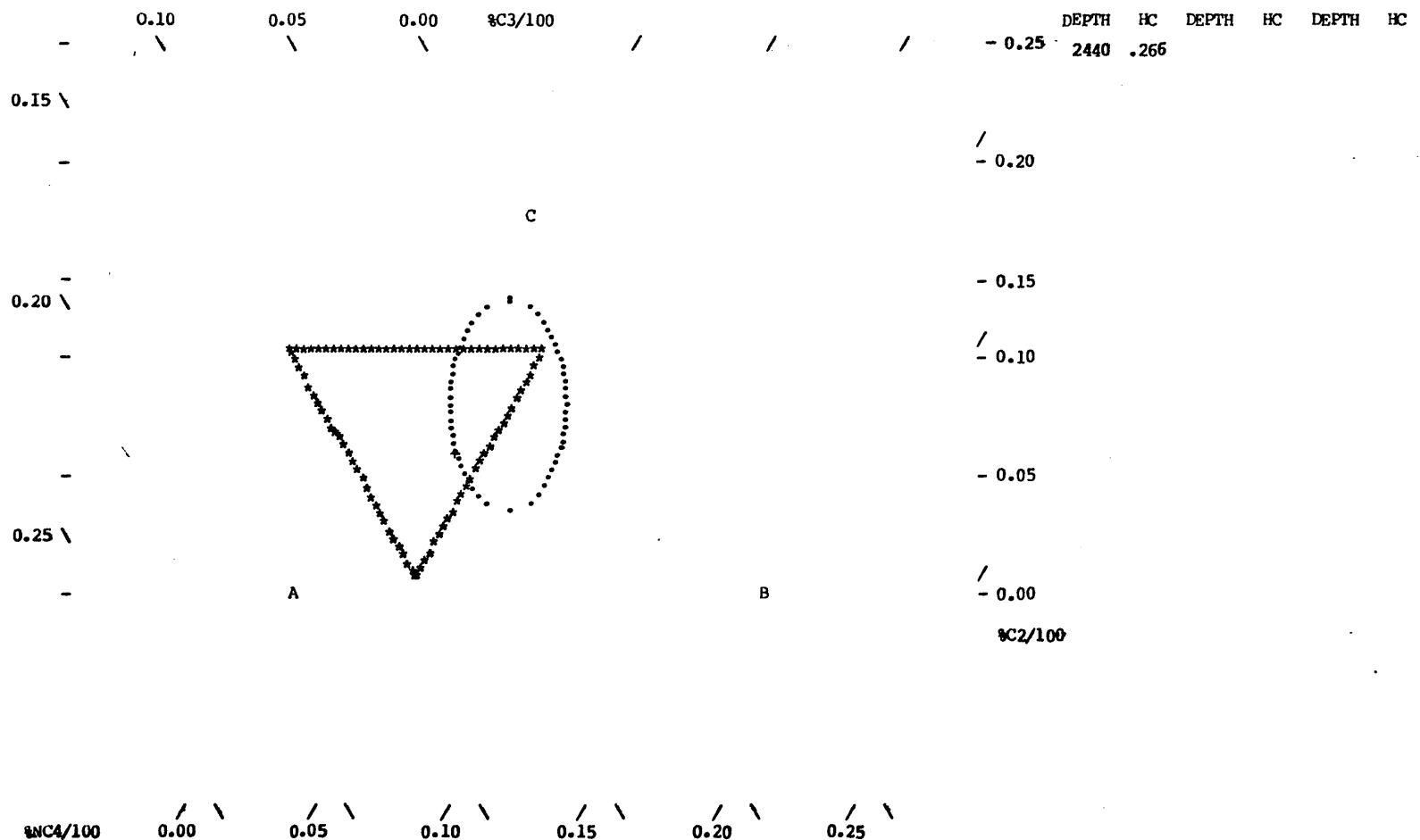
- 1) PRODUCTIVE DRY GAS ZONES MAY SHOW ONLY C1 BUT ABNORMALLY HIGH C1 ONLY SHOWS ARE INDICATIVE OF SALT WATER
- 2) IF THE C_1/C_2 RATIO FALLS LOW IN THE OIL SECTION & THE C_1/C_4 FALLS HIGH IN THE GAS SECTION THE ZONE IS PROBABLY UNPRODUCTIVE
- 3) IF ANY RATIO IS LOWER THAN THE PRECEDING RATIO THE ZONE IS PROBABLY NON-PRODUCTIVE
- 4) THE RATIOS MAY NOT BE DEFINITIVE FOR TIGHT LOW PERMEABILITY ZONES

Figure 4

GAS RATIO PLOT TO DETERMINE POSSIBLE PRODUCTIVITY AND HYDROCARBON PHASE

RFT #1 & 5, RATIOS INTERVAL FROM 2440 TO 2440

IF THE APEX OF THE TRIANGLE IS ABOVE THE BASE,GAS IS INDICATED.THE OPPOSITE INDICATES OIL.
IF THE DATA POINT PLOTS WITHIN THE ELLIPSE IT IS CONSIDERED PRODUCTIVE.THE SMALLER THE GAS TRIANGLE THEN THE
WETTER IT IS.THE LARGER THE OIL TRIANGLE THE HEAVIER THE OIL.
THE HYDROCARBON COEFFICIENT (HC) IS PROPORTINAL TO THE SIZE OF THE TRIANGLE.UNPRODUCTIVE - HC<.003,
GAS .003<HC<.175;OIL HC>.175.



VI CONCLUSIONS AND RECOMMENDATIONS

Fortescue No. 3 was drilled to 2625 metres in 24 days. The increase in drilling time compared to Fortescue No. 2 (2653 metres - 16 days), was mainly a result of increased coring requirements, weather and rig downtime.

For future wells in the Fortescue Field, it is recommended that correlation with the salt water sensitive clays found in Fortescue No. 3. at 1767 metres may prove useful as a marker for the changeover from a saltwater/gel mud to a polymer system to avoid problems in this section of the hole.

The anomalous "gas sand" encountered at 1526 metres bears further watching should it reoccur in other wells in the Fortescue Field area, for reasons of both safety, hydrocarbon potential and stratigraphic continuity.

Appendix A

Geopressure & Engineering Methods

A P P E N D I X A

GEOPRESSURE AND ENGINEERING METHODS

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Appendix A

Data Acquisition and Methods of Analysis

The methods used to obtain data, and the calculations employed to predict and quantify pore and fracture pressures are explained below.

A. Pore Pressure Prediction and Detection

I. Before Drilling

(1) Seismic Information

Field data from the reflection seismograph may be used to predict both the depth to abnormally pressured formations and the approximate pressure magnitude. The degree of accuracy depends upon the quality of the velocity spectrum. Where common depth point stacking is performed and scanned using RMS velocity increments of 50 feet/sec., areas of greatest semblance are enhanced. Therefore interval velocity calculations are more accurate and trends can be placed within closer limits.

From the velocity spectrum of RMS velocity versus two-way time, the interval transit time of the seismic energy (Eq. 2) (reciprocal of interval velocity $\times 10^6$) can be derived using Dix's formula (Eq. 1). A near exponential decrease of interval transit time with depth is usually seen in normally compacted sediments. Departures from this curve are usually caused by abnormal pressures, formation changes and poor resolution in the velocity analysis. With Interval Transit Time plotted on the semilogarithmic X axis (abscissa) and depth on the linear axis (ordinate), a "sonic log" type plot is produced. Therefore the compaction trend can be readily compared with that derived from shale interval transit time from the sonic wireline logging tool. Decreases in the rate of decrease of interval time (i.e. increase interval velocity) with depth within shale section is usually indicative of undercompaction and geopressures.

Screening of raw data during drilling of the well consists of selecting shale points and utilizing velocity survey data at casing points. This can help to reduce the log intervals over which data is averaged and so narrow down the range of possible normal trends. The greater the velocity data available in an area the more accurate the pore pressure predictions.

Assuming near horizontal beds

v_{n-1} ,

t_{n-1}

v_{int_n}

v_n ,

t_n

$$EQ. (1) v^2_{int_n} = (v_n^2 t_n - v_{n-1}^2 t_{n-1}) / (t_n t_{n-1})$$

where v_{int_n} = interval transit velocity for reflecting horizon n, ft/sec.

v_n = Rms velocity ft/sec for layer n

v_{n-1} = Rms velocity ft/sec for layer (n-1)

t_n = Two way time to layer n, secs

t_{n-1} = Two way time to layer (n-1), secs

$$EQ. (2) 1/v_{int_n} \times 10^6 = \text{interval transit time in micro secs}$$

(2) Well Histories

Data from other wells drilled in the vicinity are very useful prespud information. Information from seismic profiles, wireline logs (FDC, sonic and conductivity/resistivity), FIT and DST data, lithology and mud logs, and completion and pressure reports is of great asset in evaluating the pore pressure prospects in a new well.

II. Drilling Parameters

(1) Rate of Penetration

The rate of penetration is calculated from a kelly height versus time recorder.

With constant drilling conditions (i.e. bit size, weight on bit, rotary rpm, hydraulics and mud weight) in a uniform lithology, the rate of penetration will be determined by formation compaction characteristics. As the formations become more compacted with depth, the rate of penetration will decrease. The lithology used for determining the compaction rate is clean shale. On entering an overpressured shale there will be an increase in drill rate concomitant with the increase in porosity, and the decrease in differential pressure between mud weight and pore pressure.

It is not always possible to maintain constant parameters when drilling, and bit wear is usually an unknown factor.

To normalise the parameters and remove the effect of all non-lithological variations, the corrected drilling exponent was devised.

(2) D_{xc} (Drilling Exponent Corrected)

Various formulae have been proposed to allow control of the major drilling variables. The Jorden and Shirley formulation allows control of most of the drilling variables and has proved very successful in most areas.

$$D_x = \frac{\log \frac{R}{60N}}{\log \frac{12W}{10^6 D}}$$

where
 D = drilling exponent
 R = rate of penetration (ft/hour)
 N = rotary speed (rpm)
 W = weight on bit (lbs)
 D = bit diameter (in)

The drilling exponent will increase with depth, compaction and differential pressure in a homogenous shale. On entering an overpressured zone, the compaction and differential pressure will decrease, which is reflected by a decrease in the D exponent.

Rehm and McClendon proposed the following correction to allow for mud weight.

$$D_{xc} = D_x \times \frac{Weq}{ECD}$$

where
 D_{xc} = corrected D
 D_x = D exponent
 Weq = normal pore pressure gradient (Equivalent mud weight, ppg)
 ECD = effective circulating density

Any negative deviation of the D_{xc} from a normal trend (based on clean shale points) may be indicative of an increase in pore pressure.

(3) Mud Temperature

Heatflow is generated radially from the Earth's core and is usually constant in any given area across any given increment. This may be true for the average temperature gradient across normally pressured formations, but abnormally pressured formations have been shown to exhibit abnormally high geothermal gradients. The top of an overpressured zone will be marked by a sharp increase in geothermal gradient due to the higher than normal porosity of the formation which reduces thermal conductivity (insulates). The seal above zones of overpressure may exhibit a decrease in the geothermal gradient due to the insulating effect of the geopressured zone below and/or due to the greater thermal conductivity of the abnormally compacted seal rock.

The temperature of the drilling fluid at the flowline will be proportional to the geotemperature, but many variables must be taken into account. These variables include the mixing, treatment and addition of new, cooler mud into the circulatory system, pump rate, lag time, ambient temperature, lithology, casing size and length of riser.

Two other methods are also used to obtain geotemperature data whilst drilling. The first is the circulate returns temperature. Returns are usually circulated prior to pulling each bit, and after significant drilling breaks. A plot of these circulated returns temperatures usually provides a better approximation of the geothermal gradient than that obtained from the flowline temperature over the bit run. As with the standard method, recent mud additions can have a serious effect upon the circulated returns temperature.

A further method of obtaining geotemperature data is a survey Temp-Plate. This is a small, heat sensitised strip which is attached to the survey tool. A record of downhole survey temperature can therefore be kept. It has been found that this latter method more closely reflects the true geothermal gradient, although recorded temperature values are lower than true values:

Wireline log runs present an opportunity to calculate true bottom hole temperatures. By use of a Horner Plot, a method adapted from Horner's bottom hole pressure plots, reasonably accurate true bottom hole temperatures can be obtained. In most cases, the circulation time prior to running wireline logs is recorded. For each log run, time (in hours) since circulation stopped and the maximum bottom hole temperatures are recorded.

The recorded data may then be plotted on semilogarithmic paper, with temperature on the linear ordinate and the dimensionless time factor, $\frac{\Delta t}{t + \Delta t}$ on the semilog abscissa (where t = circulation hours and Δt = time since circulation stopped, hours). A straight line joining the plotted points is extrapolated to the temperature axis and true bottom hole static temperature is read off. (See Figure 1).

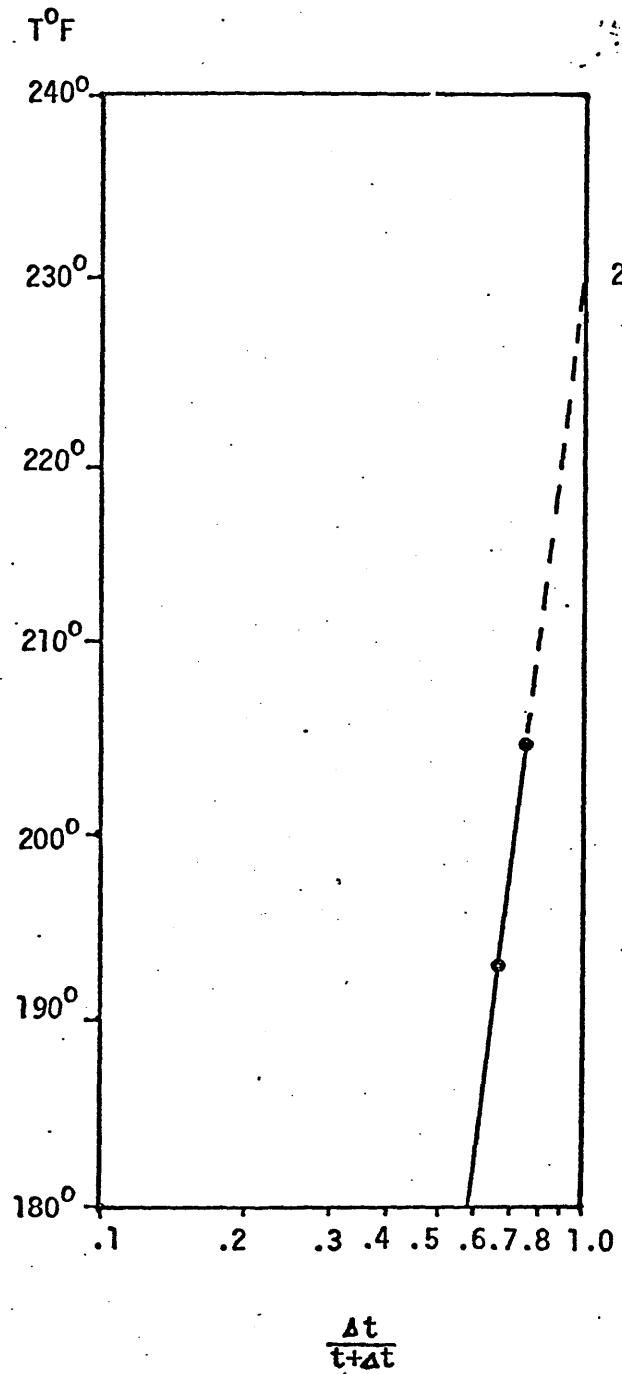
The method fails if circulation and the addition of new, cool mud into the system occurs between log runs.

(4) Gas

The amount of gas detected within the drilling mud at the flowline can be very useful indicator of differential pressure. Background gas values are very important. If the background gas increases with depth in a formation of constant lithology, permeability, and gas saturation with a fixed mud weight, then an increase in pore pressure may be indicated.

Gas magnitude is relative when gas is being used as a measure of differential pressure. Formation permeability and gas saturation must be considered in determining the amount of background gas to be expected while drilling. Low permeability formations are likely to yield only small amounts of background gas even with high gas saturation. This is also the case for a formation with high permeability and low gas saturation. Refer to Figure 2.

HORNER TEMPERATURE PLOT



230°F True BHT °F

 Δt = Hours since circulation began t = Circulation Time, Hours T = Max. Recorded BHT, °F

2nd Log run

 $t = 4.5$

1st Log run

Δt	T	$\frac{\Delta t}{t+\Delta t}$
9	193	.67
13	205	.74

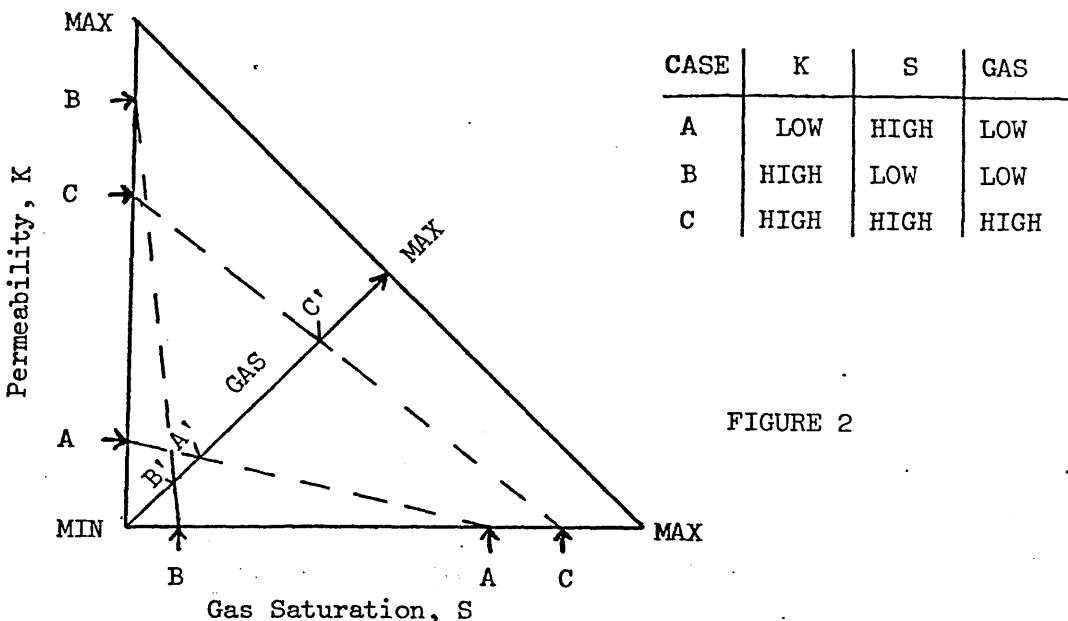


FIGURE 2

In a low gas saturated formation a slight increase in background gas may be significant while in a high gas saturated formation high background gas may not be significant. Thus, low background gas in low gas saturated or low permeability formations can be expected, even when drilling underbalanced. Disregard of this factor can lead to sloughing, bridging, stuck pipe, or a well kick if gas alone is used for determining an underbalanced hole condition.

The background gas after a gas peak should be compared with the background gas prior to the peak. A higher background gas after a peak than that before the peak may suggest an underbalanced hole condition.

Pore pressures cannot be quantified by gas readings alone, but they can be quantified (provided the above mentioned permeability and saturation factors are taken into account) by a comparison of changes in gas readings with changes in mud weight in hydrocarbon bearing formations.

Produced gas (e.g. connection gas, swab gas and trip gas) are also important factors to consider in pore pressure analysis. Their presence indicates a near balanced hole condition for permeable hydrocarbon bearing formations or even a slightly underbalanced

condition for low permeability hydrocarbon bearing formations.

Connection gas is due to the reduction in differential pressure caused in part by ceasing circulation and in part by swabbing, such that hydrocarbons (or other fluids) are produced (flow into the hole) from the formation.

Swab gas is that gas produced by a formation due to underbalance caused by the upward movement at the drill string. This may be accompanied by pump shutdown (e.g. during connections and trips) or not. There are two types of swabbing, one being the piston type (some part of the drill string acting as a plunger in the bore hole) and the other being the frictional type (friction between moving drill string and annular mud inducing a slight lifting force in annular mud column).

Trip gas is produced gas caused by pump shutdown, pulling the drill string, and lowering of the hydrostatic head (if the hole is not kept full) during a trip.

(5) Shale Density

Shale density in a homogeneous claystone/shale section which has a hydropressure gradient will increase with depth as compaction increases and porosity decreases. Values typically range from 1.7 to 2.7 gm/cc and show a steady rate of increase with depth. Anomalies from this normal compaction trend may be due to mineralogy, e.g., sideritic, dolomitic and calcareous shales exhibit higher than normal values. Sandy, silty shales and soft wet clay will produce further variations.

Geopressure is indicated by a constant or decrease in density with depth reflecting the increased porosity and fluid content. Cap rocks of higher than normal density may be present above this zone of abnormal pressure.

(6) Shale Factor (Refer Figure 3)

During normal deposition of clays, the principle component is montmorillonite. This is a flocculated sheet silicate which has a large capacity to absorb and retain water between the individual molecular sheets and between the flocculate particles. After deposition, montmorillonite undergoes compaction through gravity loading which flushes the intraparticle water into the pore spaces. Providing that the hydraulic conductivity is sufficiently high to remove this water, compaction will continue. The outer layers of water bonded to the clay particles may next be removed as montmorillonite alters diagenetically with depth to mixed-layer clays and finally to illite. This alteration involves compaction of pore spaces, orientation of particles and reduction in inter-layer and intraparticle area, thereby reducing the total area available for chemical absorption. Note that if the hydraulic conductivity is insufficient to remove the liberated water as it is flushed, then at depth the clays will be abnormally pressured and of a "younger" diagenetic age.

Illite or kaolinite may be deposited as the primary clays. As non-swelling clays they have very little intraparticle water. These clays dewater by loss of interparticle water through compaction. Again, if the hydraulic conductivity of the clays is lower than that required to efficiently flush the water, then these clays will be overpressured. Non-swelling clays, as stated above, are geometrically more compact than their swellable counterparts and therefore originally contain less sites for chemical absorption of free ions.

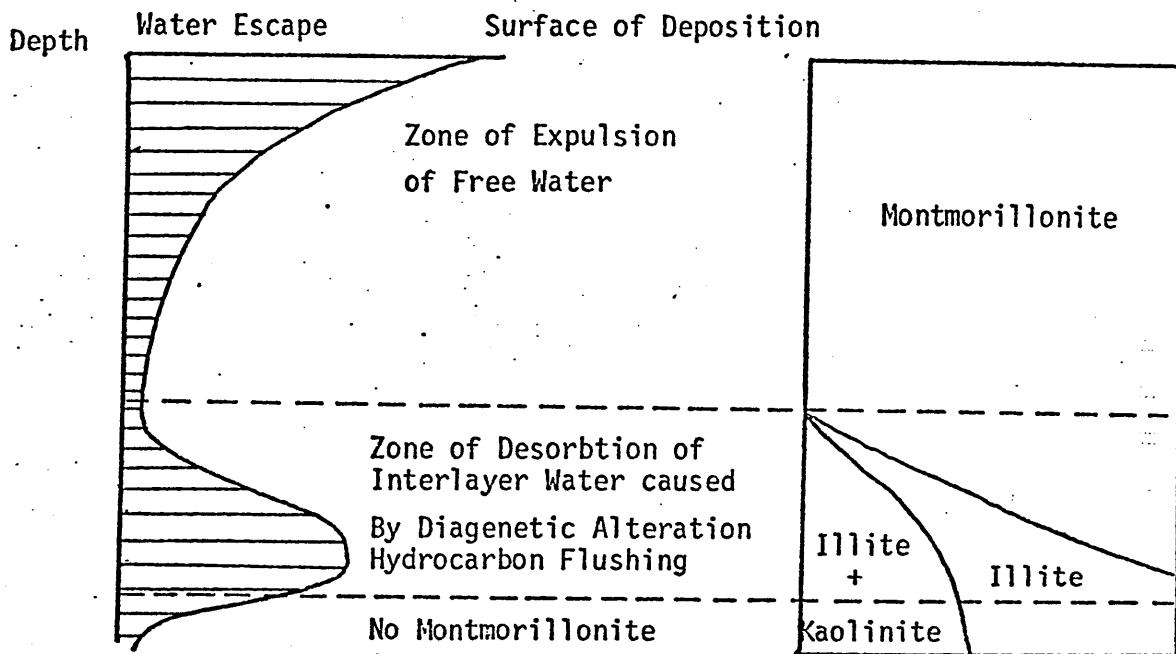
It is the diagenetic state (% montmorillonite) of the clays that shale factor reveals. If a crushed slurry of the shale is titrated with methylene blue solution, the dye will be absorbed onto the available sites by cation exchange mechanisms. The amount of dye required to saturate the cation exchange capacity of the shale will depend upon the latter's geologic maturity.

TYPICAL CLAY DIAGENESIS (AFTER MC POWERS (1967) FIGURE 3

1. MONTMORILLONITE

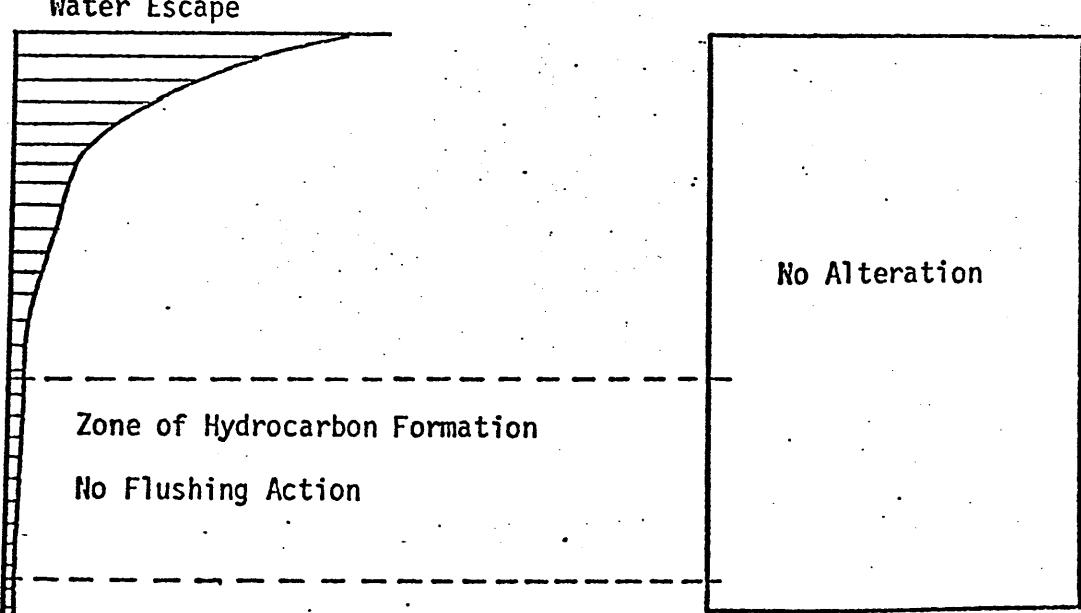
WATER LOSS vs DEPTH OF BURIAL

DIAGENETIC HISTORY



2. ILLITE/KAOLINITE

Water Escape



If the principle primary clay is montmorillonite, which undergoes compaction to "mixed-layer" clays and then illite, the shale factor values would initially be high, and would show a steady decline with diagenesis. Overpressured, undercompacted sections would theoretically show an increase of the shale factor due to the increased porosity and hence larger surface areas for cation exchange. Were illite and kaolinite the primary clays, the shale factor would be low initially. In the case of an overpressured section of such clays, the shale factor may show no increase whatsoever. Hence in sections of mature, reworked clays, shale factor may be of little use in the detection of geopressures.

If the geopressures is generated by tectonic forces rather than by abnormal compaction through gravity loading, shale factor ceases to be useful as a pressure indicator.

(7) Hole Condition (Carbide Results, Hole Behaviour, Cuttings Size)

Hole condition has to be used in conjunction with all other data. Tight hole on connections and trips, increased rotary torque, connection gases, swab gases, % and size of cuttings, texture of cuttings (i.e. gumbo or splintery), carbide lag time versus theoretical lag time are all indicators of hole condition and will tend to indicate the presence of abnormal pressure.

B. Pore Pressure Quantification

Pore pressure quantification can be made from either empirical data such as tight hole or kick information, or from pressure parameter data such as seismic data (ITT), drilling data including D_{xc} and cuttings Sh^S , and wireline log data including Δt , R_{SH} , Sh^S . The quantification of pore pressure from pressure parameter data requires knowledge of the normal pore pressure for the area, the establishment of a normal shale compaction trend line on a plot of the pressure parameter data, and a quantitative relationship between the pressure parameter deviation from normal and the abnormal pore pressure which causes such deviation.

The normal pore pressure for the area can either be assumed to be 8.3 - 9 ppg EMW on a rank wildcat well, estimated from area pressure data, or calculated from wireline log formation salinity data.

All the above mentioned pressure parameters usually increase (D_{xc} , Sh^S , R_{SH}) or decrease (ITT, Δt) exponentially with depth in clean normally pressured shales. Thus a best fit line drawn through the normally compacted clean shale points will generally be straight when the pressure parameter scale is log and the depth scale is linear. After a normal trend line has been established, and knowing the pore pressure that this trend line represents, quantification of the pore pressure for abnormally pressured shale points may be made.

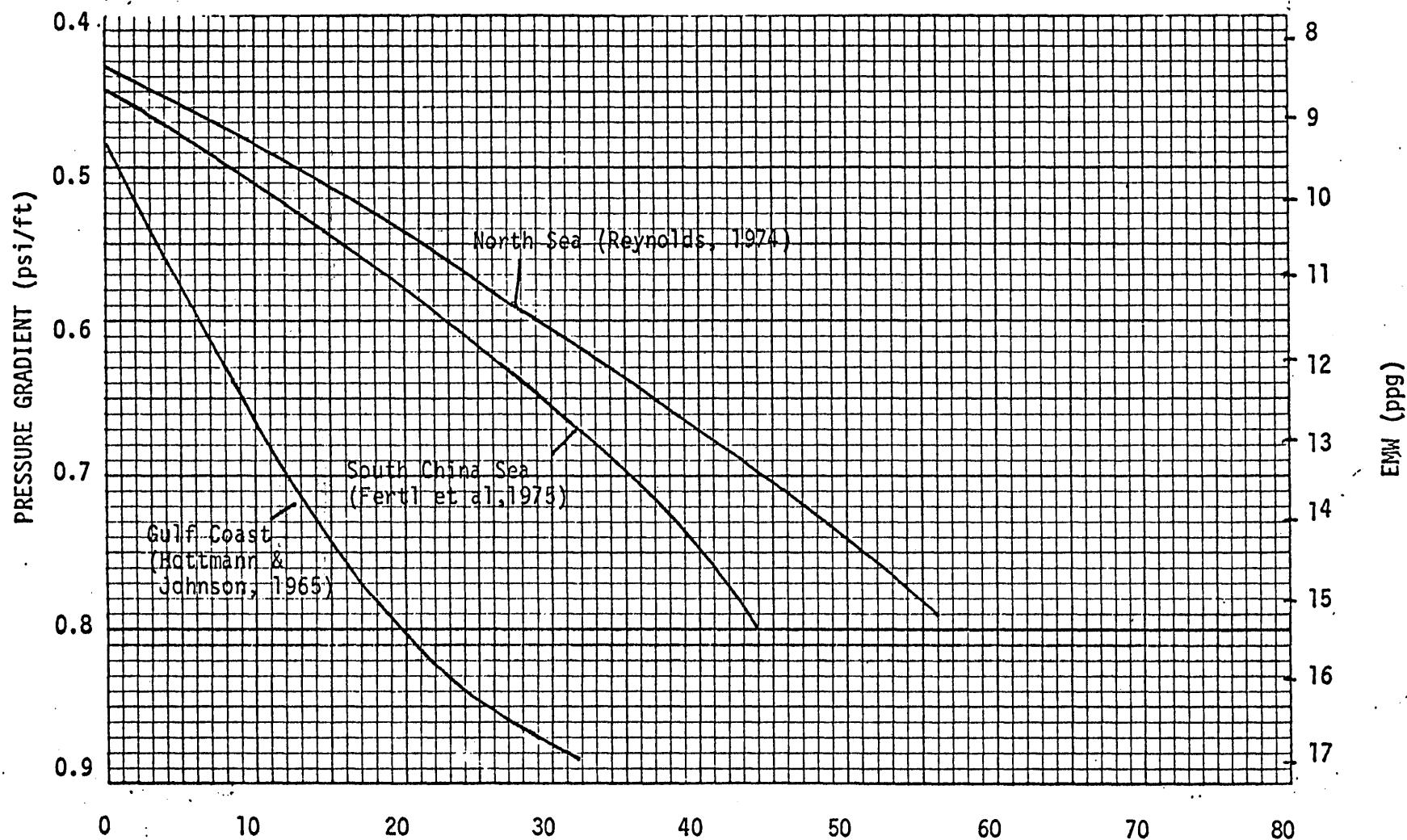
It should be emphasised that the above mentioned pressure parameters reflect changes in porosity, and hence compaction only, and do not reflect changes in pore pressure from other causes.

The degree of deviation of a pressure parameter value in shale from the normal trend is usually directly proportional to the amount of pore pressure increase. Several methods have been derived for relating the pressure parameter deviation from normal and the pore pressure change, with each method's reliability being questionable in a new geographical area until supported by empirical data.

These methods are:-

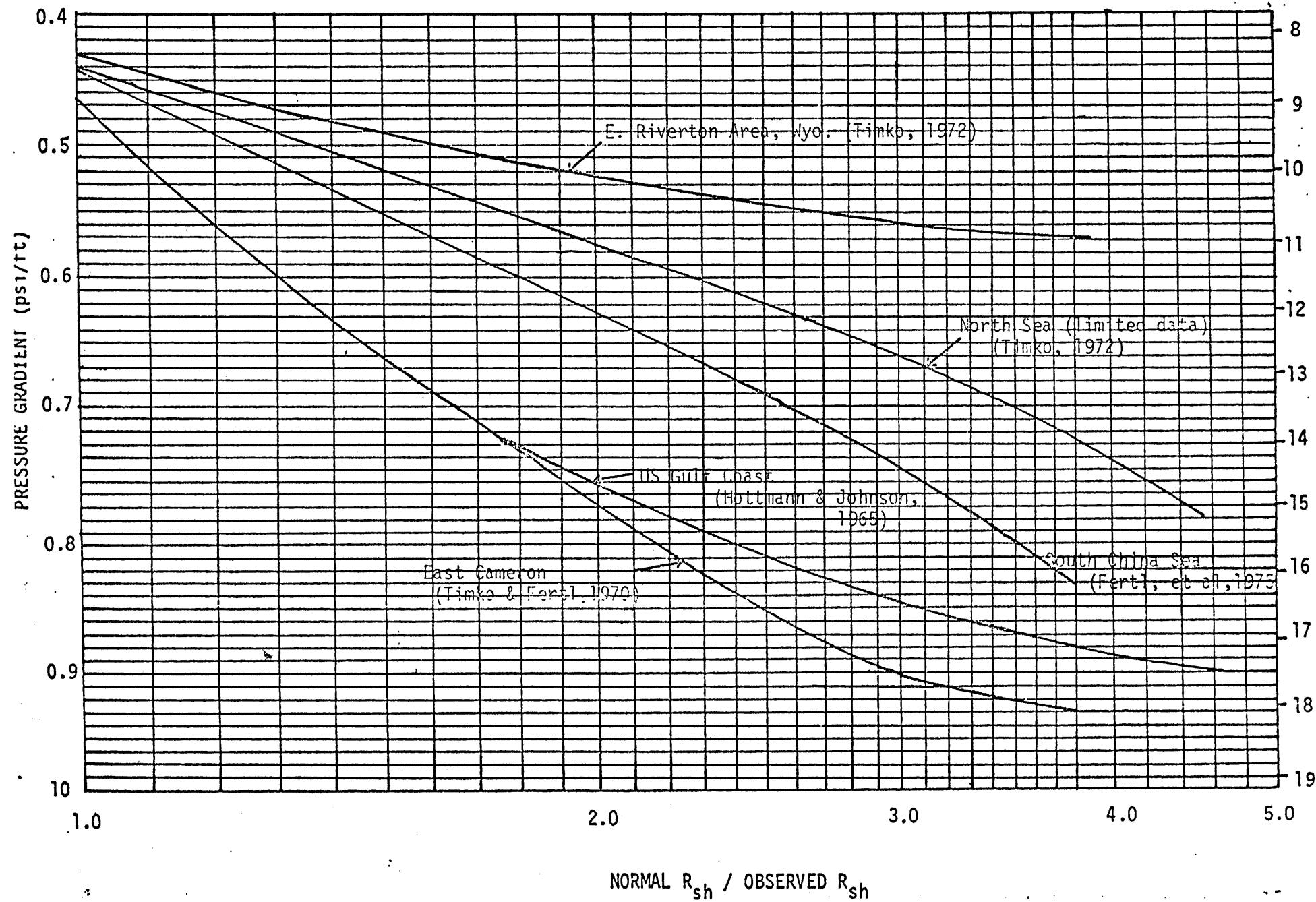
- (1) Empirical pore pressure/pressure parameter deviation composite reference curves from various geographical areas in the world. Refer to the Sonic Log Departure vs Pore Pressure and Shale Resistivity Ratio vs Pore Pressure Graphs on pages xv and xvi of this Appendix.
- (2) Theoretical equivalent depth or matrix stress method. Refer to page xvii of this Appendix for an explanation of this method.
- (3) Eaton's empirical variable overburden pressure method. Refer to page xviii of this Appendix for equations and graphs.

SONIC LOG DEPARTURE vs PORE PRESSURE



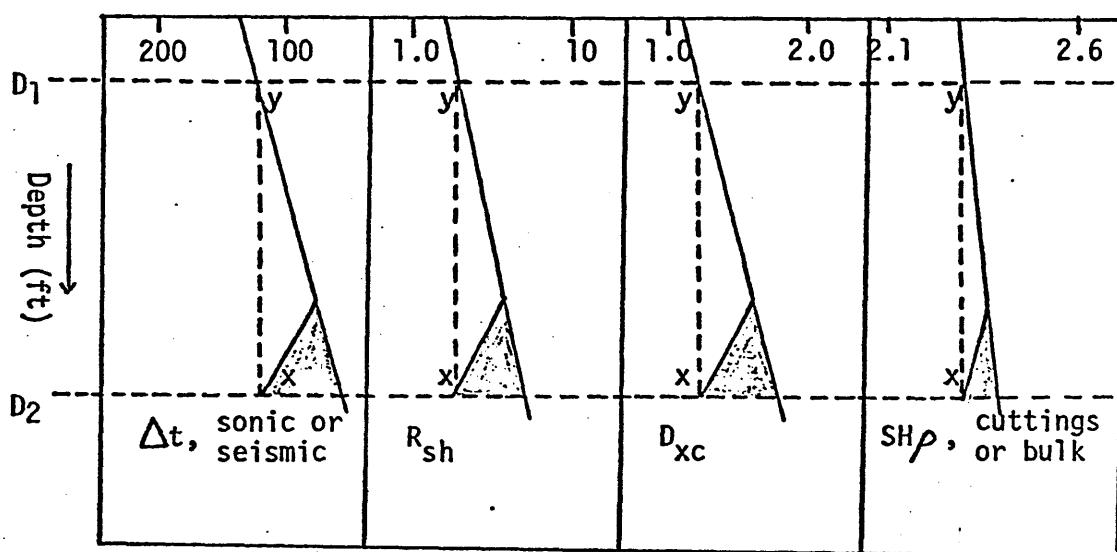
$$\Delta t_{\text{obs}} - \Delta t_{\text{norm}} \mu \text{ sec/ft}$$

SHALE RESISTIVITY RATIO vs PORE PRESSURE



Matrix Stress or Equivalent Depth Method

The matrix stress or equivalent depth method assumes that the part of the overburden supported by the clay matrix will be constant for clays with the same porosity. More precisely it assumes that the rock matrix stress at a particular depth in an overpressured zone is equal to the rock matrix stress at a shallower depth point where the pressure parameter value on the parameter normal trend is equal to the pressure parameter value at the depth of interest in the overpressured zone. In the diagram below point X at the point of interest has the same pressure parameter value as point Y on the normal pressure parameter trend line. With the overburden gradient and normal pore pressure known, the pore pressure at the depth of interest may be calculated as shown.



$$P_2 = D_2 P_{o2} - D_1 (P_{o1} - P_1)$$

P_2 = Pore pressure at D_2 , psi

D_2 = Depth of interest, feet

P_{o2} = Overburden gradient at D_2 , psi/ft

D_1 = Equivalent Depth

P_1 = Pore pressure at D_1 , a normal gradient, psi/ft

P_{o1} = Overburden gradient at D_1 , psi/ft

Eaton's Variable Overburden Method

Geopressure magnitude may be calculated from pressure parameter data using the following equations or charts.

$$1. \quad P/D = S/D - \sqrt{S/D - (P/D)n} \times \left(\frac{R_o}{R_n} \right)^{1.2}$$

$$2. \quad P/D = S/D - \sqrt{S/D - (P/D)n} \times \left(\frac{\Delta t_n}{\Delta t_o} \right)^{3.0}$$

$$3. \quad P/D = S/D - \sqrt{S/D - (P/D)n} \times \left(\frac{d_{c_o}}{d_{c_n}} \right)^{1.2}$$

P/D = Formation pressure gradient either normal or geopressured, psi per foot

(P/D)n = Normal water gradient in the area such as 0.465 in and along the Gulf of Mexico, or 0.433 in West Texas, psi per foot

Rn = Shale resistivity from normal line, ohm-meters

Ro = Shale resistivity from well log, ohm-meters

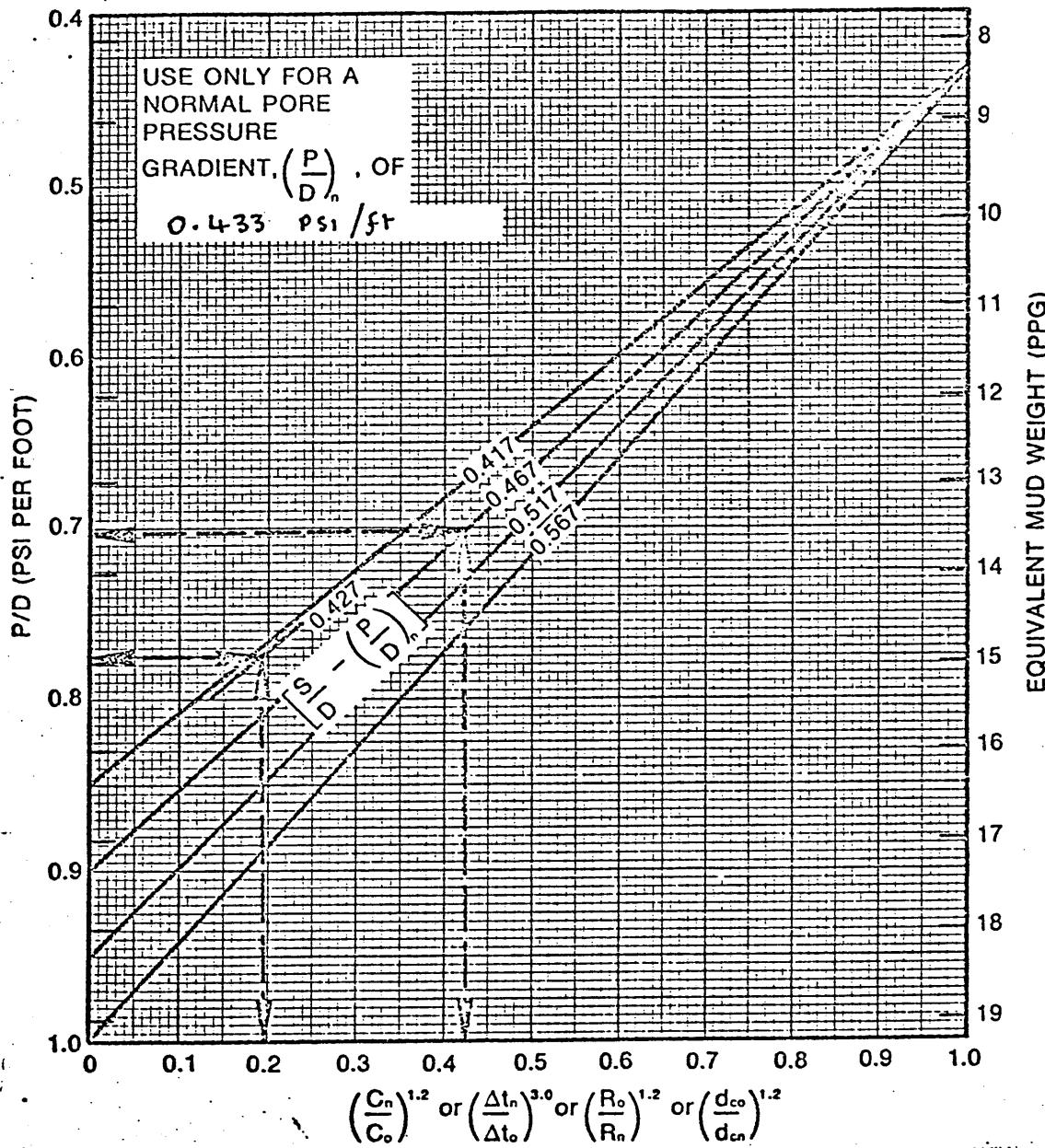
S/D = Overburden stress gradient, psi per foot

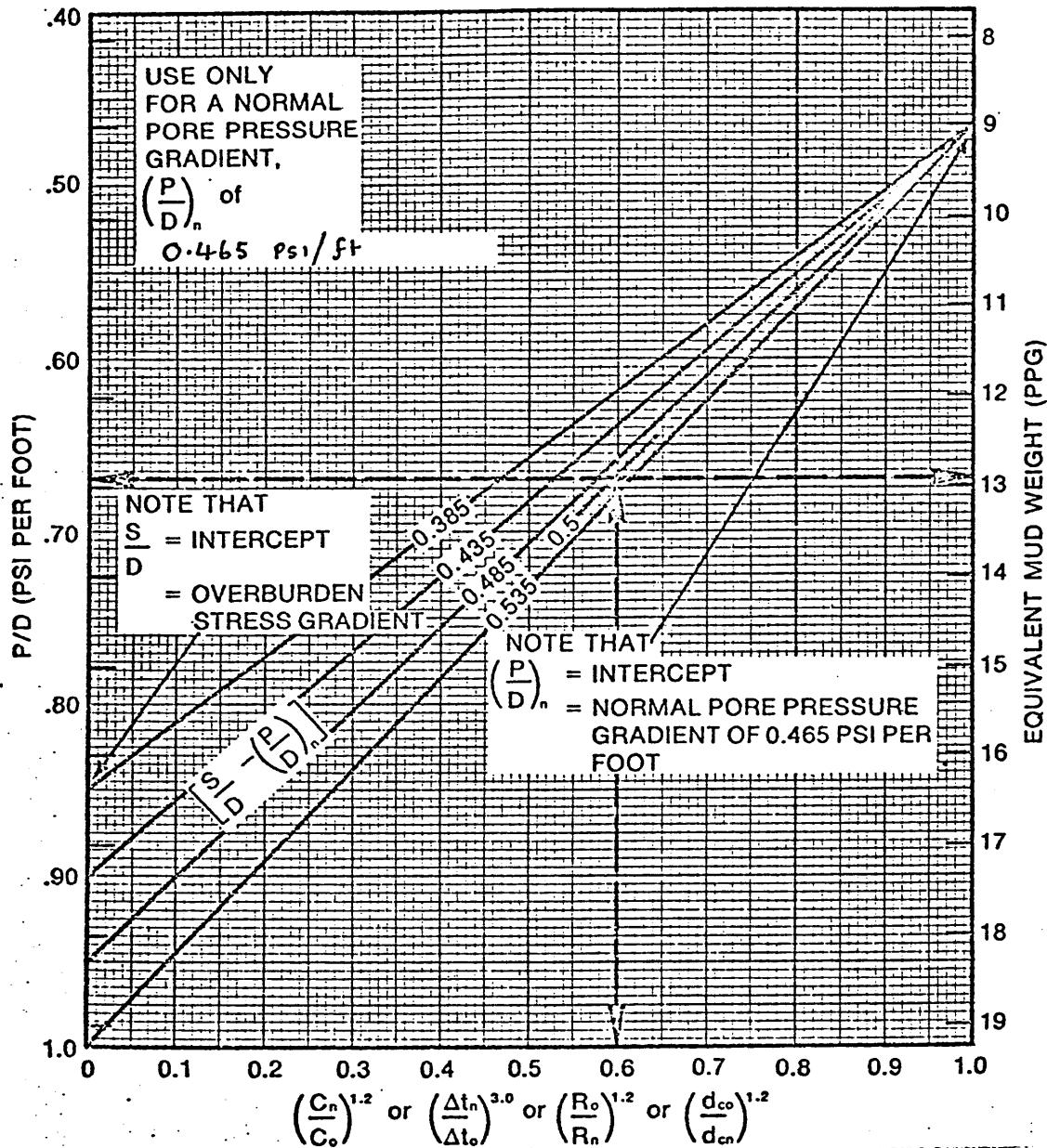
Δt_n = Normal shale travel time, micro-seconds per foot

Δt_o = Shale travel time value, micro-seconds per foot

d_c_n = Actual d_c from trend line

d_c_o = Actual d_c calculated





The D_{xc} compaction trend line is in general parallel to a line joining 1.4 and 1.7 (values of D_{xc}) 5,000 ft. apart. The quantification of pore pressure from D_{xc} is most usually effected by using the following equation.

$$P_o = P_n \times \frac{D_{xc}^n}{D_{xc}^o}$$

P_o = Pore pressure at depth of interest (ppg)
 P_n = Normal Pore Pressure (ppg)
 D_{xc}^o = Observed D_{xc} at depth of interest
 D_{xc}^n = The D_{xc} value on the trend line at the depth of interest

From this equation overlays can be constructed.

Shale density data is sometimes plotted on a linear-linear plot and sometimes on a linear (depth) log (Sh^f) plot. The matrix stress or equivalent depth technique is most usually utilised to quantify pore pressure from this pressure parameter.

C. Overburden Pressure Determination:

The average density for each successive 50 feet interval from surface to total depth is obtained from cuttings or, preferably, from the FDC log. The bulk density data are converted from gm/cc to psi/ft to give overburden pressure.

D. Fracture Pressure Determination

Both empirical and theoretical methods are utilised to determine the fracture pressure of the formation. Empirical data from loss circulation and formation integrity tests are the most reliable. Fracture data from well histories can be very beneficial. The following theoretical methods are currently accepted:

a) HUBBERT AND WILLIS

$$\begin{aligned}\frac{F_p}{D} &= \frac{P_p}{D} + \frac{1}{3} \left(\frac{P_o - P_p}{D} \right) \quad \dots \text{min} \\ &= \frac{P_p}{D} + \frac{1}{2} \left(\frac{P_o - P_p}{D} \right) \quad \dots \text{max}\end{aligned}$$

Where P_o is unknown an approximation of F_p can be derived making
 $P_o = 1.0$ thus:

$$\frac{F_p}{D} = \left(1 + \frac{2P_p}{D}\right) \frac{1}{3} \dots \text{min}$$

$$= \left(1 + \frac{P_p}{D}\right)^{\frac{1}{2}} \dots \text{max}$$

b) MATHEWS AND KELLY

$$\frac{F_p}{D} = \frac{P_p}{D} + \frac{K_i(P_o - P_p)}{D_i}$$

Where $D_i = D$ in normally pressured sections. If the formation pressure is greater than normal then:

$$D_i = \left(\frac{\frac{P_o}{D} - \frac{P_p}{D}}{\frac{P_o}{D} - \frac{P_n}{D}} \right) D$$

K_i is a variable matrix stress coefficient i.e. A variable horizontal to vertical stress ratio back calculated or using Gulf Coast and West Texas Data represented as a curve of D_i versus K_i .

c) EATON

$$\frac{F_p}{D} = \frac{P_p}{D} + \left(\frac{v}{1-v}\right) \left(\frac{P_o - P_p}{D}\right)$$

Where v is Poisson's ratio, either back calculated or using original Gulf Coast Data, a curve of $\frac{P_o}{D}$ versus v .

d) ANDERSON, INGRAM AND ZANIER

$$\frac{F_p}{D} = \frac{P_p}{D} \left(\frac{1-3v}{1-v}\right) + \frac{P_o}{D} \left(\frac{2v}{1-v}\right)$$

Where v is Poisson's ratio, either back calculated for a given area or using original Gulf Coast data of v versus a formation shaliness index.

Symbols used

Fp	=	Fracture Pressure, psi
Po	=	Overburden Pressure, psi
Pp	=	Formation Pressure, psi
Pn	=	Normal or Hydropressure Gradient, psi/ft
D	=	Depth, ft

Appendix B
Instrumentation & Data Collection Methods

A P P E N D I X B

INSTRUMENTATION AND DATA COLLECTION METHODS

INSTRUMENTATION AND DATA COLLECTION METHODS

INSTRUMENTATION -

The Gendas Level VI system consists of the following equipment packages:

- a) Two Hewlett Packard 21MX, 36K memory computer systems with associated link tape drives, operator consols, printer-plotter outputs and remote video display units. One system is online and the other is used for offline work and as a backup in the event of breakdown.
- b) Drill Monitor System (DMS Mk II) which monitors the drilling variables hook load, weight on bit, rotary RPM, total bit revolution, depth, kelly height, drill rate, torque, pump and casing pressures. The system monitors displays and records these variables and feeds them to the online computer system for analysis and final tape storage.
- c) Mud Monitoring System for recording total and individual pit volumes, mud weights in and out, mud temperatures in and out and pump flow in and out. These variables are also linked to the online computer.
- d) Gas detection system for the analysis of mud stream and blendor gases which includes the standard hot wire detectors for total gas and petrol vapours; standard chromatograph for hydrocarbons C₁ through C₅; FID-flame ionization detectors for total gas and C₁-C₅ for high percentage of these gases which would saturate a normal system; a thermoconductivity chromatograph for the detection of non combustible gases; and a H₂S detection system.

SOFTWARE CAPABILITIES -

The Gemdas System incorporates software capabilities that have been developed to monitor drilling operations, aid in drilling control and pressure detection and provide a permanent easy-recall record of all pertinent drilling data. The following basic units are involved:

- a) The drill monitor program which reads the various DMS equipment during drilling to provide a continuous readout of drilling variables. The program also computes such parameters as cost per foot, estimated tooth wear, D_{xc} and estimated pore pressure over a fixed depth or time interval.
- b) The trip monitor program which provides a critical monitoring of all necessary parameters during trips on a continuous real time basis. By monitoring the number of stands the program computes expected hook-load and pit level and compares these with the actual values. Pipe running speed, surge pressures and estimated completion time are also computed and displayed.
- c) The kick and kill monitor program provides a valuable method of analysing a kick situation. The program can be run prior to killing the well to compute the results of various kill mud weights and pump rates. The program also monitors and records the actual kill procedure.
- d) Data Collection:

The complete drilling data for Fortescue No 3 is stored on data tapes 1 to 3

Tape 1	244m	to	1600m
Tape 2	1600m	to	2410m
Tape 3	2410m	to	2625m

A complete printout of this data is presented in Appendix D (i) and selected parameters have been plotted on a 1:1000 scale and presented in Appendix D (ii) Handplots on a 1:2500 scale of drill rate, D_{xc}, background gas, shale density and mud temperature are presented in Appendix C.

Appendix C

Appendix C
Manual Plots & Charts

A P P E N D I X C

MANUAL PLOTS AND CHARTS -

(refer back pocket)

- (i) Drilling Data Pressure Log
- (ii) Temperature Data Log
- (iii) Pressure Analysis Log

PE604498

This is an enclosure indicator page.
The enclosure PE604698 is enclosed within the
container PE906835 at this location in this
document.

The enclosure PE604698 has the following characteristics:

ITEM_BARCODE = PE604498
CARRIER_BARCODE = PE906835
NAME = Pressure Log
BASIN = GIPPSLAND
PERMIT = VIC/L5
TYPE = WELL
SUBTYPE = WELL_LOG
DESCRIPTION = Pressure log (enclosure from Geological Engineering Well Report--attachment to WCR) for Fortescue-3
REMARKS =
DATE_CREATED = 23/12/78
DATE RECEIVED =
W_NO = W712
WELL_NAME = FORTESCUE-3
CONTRACTOR = EXPLORATION LOGGING
CLIENT_OP_CO = ESSO AUSTRALIA LTD

(Inserted by DNRE - Vic Govt Mines Dept)

PE604499

This is an enclosure indicator page.
The enclosure PE604499 is enclosed within the
container PE906835 at this location in this
document.

The enclosure PE604499 has the following characteristics:

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CONTAINER_BARCODE = PE906835
NAME = Temperature Data Log
BASIN = GIPPSLAND
PERMIT = VIC/L5
TYPE = WELL
SUBTYPE = WELL_LOG
DESCRIPTION = Temperature Data Log (enclosure from
Geological Engineering Well
Report--attachment to WCR) for
Fortescue-3
REMARKS =
DATE_CREATED = 31/07/77
DATE RECEIVED =
W_NO = W712
WELL_NAME = FORTESCUE-3
CONTRACTOR = EXPLORATION LOGGING
CLIENT_OP_CO = ESSO AUSTRALIA LTD

(Inserted by DNRE - Vic Govt Mines Dept)

PE604500

This is an enclosure indicator page.
The enclosure PE604500 is enclosed within the
container PE906835 at this location in this
document.

The enclosure PE604500 has the following characteristics:

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CARRIER_BARCODE =	PE906835
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BASIN =	GIPPSLAND
PERMIT =	VIC/L5
TYPE =	WELL
SUBTYPE =	WELL_LOG
DESCRIPTION =	Pressure Analysis Log (enclosure from Geological Engineering Well Report--attachment to WCR) for Fortescue-3
REMARKS =	
DATE_CREATED =	31/07/77
DATE RECEIVED =	
W_NO =	W712
WELL_NAME =	FORTESCUE-3
CONTRACTOR =	EXPLORATION LOGGING
CLIENT_OP_CO =	ESSO AUSTRALIA LTD

(Inserted by DNRE - Vic Govt Mines Dept)

Appendix D
Computer Prints & Plots

APPENDIX D

COMPUTER PRINTS (+) AND PLOTS (X) - + (i) Drilling Data Printout
X (ii)Drilling Data Plot 1:1000
ROP, Dxc, Torque, Flowline Temp,
Pore Pressure (FBG), ECD.

(i) DRILLING DATA PRINTOUT

ESSO AUSTRALIA FORTESCUE NO.3
JIT 1101 6:32 12/20/78

TIME	DEPTH	ROP	TURQUE	RPM	BIT	PUMP	WT	MINS	LB/GAL	GAL/MIN	TEMP(C)	PVT	REVS	MT	THIS BIT	ESTI	DXC	NWB	SP	ECD	NXMW									
									MIN	INST	MAX	WT	PSI	DEPTH	IN	OUT	IN	OUT	LAG	IN	OUT	CPMI	CPMB	TW						
WELL COORDINATES																														
WELL 26" HOLE TO 244 METRES																														
NO.2 HTC USC 3AJ 17 1/2" 20,20,20.																														
254	244	31.6	.8	.9	46	5.9	1156	244	8.9	1.3	839	717	14.1	18.9	18.8	452	2281	0	.0	61.91	69953	.001	.76	.95	14.1	8.5	8.41			
257	245	18.3	1.0	1.3	49	5.4	1158	244	8.9	9.0	839	810	14.1	18.6	18.8	440	2412	1	.1	108.3	8404	.001	.71	.95	15.3	8.5	8.41			
249	246	43.0	1.3	2.0	50	5.2	1155	244	8.9	9.0	831	674	14.1	18.1	18.8	429	2486	2	.1	49.96	2490	.001	.53	.95	20.3	8.5	8.41			
259	247	79.6	1.3	1.4	50	8.2	1126	244	8.9	9.0	844	681	14.1	18.0	18.8	424	2503	3	.1	29.54	1857	.001	.48	.95	24.3	8.5	8.41			
260	247	108	1.4	1.8	49	10.8	1135	244	8.9	9.0	828	680	14.1	17.8	18.8	429	2527	3	.1	18.55	1361	.001	.40	.95	27.1	8.5	8.41			
313	251	249	2.0	2.6	63	6.8	1150	244	8.9	9.0	857	695	14.1	17.3	18.8	445	2853	7	.1	7.84	679.1	.001	.26	.95	30.8	8.4	8.41			
313	252	184	1.4	1.9	63	9.6	1169	244	8.9	9.0	860	724	14.1	17.2	18.8	443	2878	8	.1	10.61	574.1	.001	.33	.96	29.3	8.4	8.41			
313	252	180	1.8	1.8	60	11.2	1139	244	8.9	9.0	868	722	14.2	17.2	18.8	440	2881	8	.1	11.46	557.4	.001	.35	.96	29.3	8.4	8.41			
313	252	153	1.4	1.5	63	10.0	1193	244	8.9	9.0	866	718	14.1	17.2	18.8	443	2890	8	.1	12.30	547.7	.001	.35	.95	29.3	8.4	8.41			
313	253	196	1.6	2.0	62	14.6	1159	244	8.9	9.0	860	713	14.1	17.2	18.8	445	2905	9	.1	10.87	499.8	.001	.34	.96	29.1	8.4	8.41			
314	255	285	2.4	2.4	.61	17.2	1142	244	8.9	9.0	850	719	14.2	17.1	18.8	438	2918	10	.1	5.93	439.8	.001	.27	.98	30.9	8.4	8.41			
314	255	229	1.8	2.3	63	8.8	1171	244	8.9	9.0	856	714	14.2	17.1	18.8	434	2934	11	.1	8.38	408.8	.001	.31	.96	29.8	8.3	8.41			
314	256	214	2.5	2.6	63	14.9	1152	244	8.9	9.0	858	707	14.1	17.0	18.8	438	2944	12	.1	9.67	389.5	.001	.35	.96	29.2	8.3	8.41			
314	256	220	2.5	2.6	60	22.2	1183	244	8.9	9.0	867	707	14.1	17.0	18.8	438	2950	12	.1	9.42	379.2	.001	.35	.96	29.2	8.3	8.41			
327	261	65.9	1.8	2.5	.63	14.9	1180	244	8.9	9.0	828	710	14.2	16.1	18.8	467	3258	17	.2	38.02	281.2	.011	.60	.95	20.1	8.4	8.41			
329	267	424	1.7	3.4	64	9.9	1126	244	8.9	9.0	844	718	14.2	16.2	18.8	419	3366	22	.2	8.85	219.3	.011	.35	.95	29.1	8.4	8.41			
330	272	173	1.3	3.7	.65	10.4	1155	244	8.9	9.0	817	724	14.2	15.6	18.8	393	3455	27	.3	11.57	190.7	.011	.44	.94	25.4	8.3	8.41			
340	277	403	2.3	3.0	.65	19.2	1171	248	8.9	9.0	834	974	14.2	16.9	12.6	205	3671	33	.3	4.75	158.9	.011	.20	.93	32.3	8.5	8.41			
341	282	295	1.8	3.0	.66	15.2	1131	248	8.9	9.0	836	1077	14.2	16.8	13.2	174	3737	38	.3	6.61	139.3	.011	.29	.93	30.5	8.4	8.41			
350	268	64.9	1.5	2.9	.65	11.1	1182	257	8.9	9.0	855	1130	15.1	17.3	14.0	207	4013	44	.4	24.31	123.1	.021	.53	.92	22.9	8.6	8.41			
351	292	151	2.0	3.1	.65	25.1	1123	260	8.9	9.0	842	1036	15.3	17.5	14.0	205	4110	48	.4	13.06	113.9	.021	.47	.91	25.3	8.6	8.41			
352	297	294	2.6	4.8	.68	20.8	1225	271	8.9	9.0	886	692	15.5	17.5	14.0	203	4227	53	.4	6.81	104.5	.021	.38	.89	28.4	8.6	8.41			
401	302	230	2.4	3.2	.76	19.4	1265	264	8.9	9.0	881	820	16.3	17.5	14.0	169	4478	58	.5	9.75	97.59	.021	.38	.89	28.9	8.6	8.41			
402	307	375	2.9	3.0	.65	23.3	1242	268	8.9	9.0	889	811	16.4	17.4	14.0	155	4567	63	.5	5.31	91.45	.021	.29	.88	30.8	8.6	8.41			
403	312	216	2.1	2.9	.65	14.8	1271	271	8.9	9.0	889	813	16.5	17.6	14.0	159	4655	68	.5	9.26	85.25	.031	.42	.88	27.3	8.6	8.41			
411	317	363	3.2	3.6	.60	29.2	1256	274	8.9	9.0	883	685	16.9	17.7	14.1	128	4894	73	.6	5.76	31.25	.031	.31	.87	30.4	8.6	8.41			
412	322	428	3.5	4.2	.60	30.3	1266	274	8.9	9.0	879	.35	17.0	17.7	14.1	130	4951	78	.6	4.67	75.49	.031	.29	.86	31.0	8.6	8.41			
421	327	41.0	3.0	4.5	.65	28.8	1087	287	8.9	9.0	800	776	17.3	17.8	14.1	110	5233	83	.7	47.83	73.44	.031	.71	.85	16.8	8.7	8.41			
422	332	295	4.2	4.7	.65	39.3	1065	287	8.9	9.0	791	712	17.3	17.8	14.1	111	5299	38	.7	6.56	70.20	.031	.37	.82	29.8	8.7	8.41			
423	337	266	3.8	4.5	.65	37.4	1403	291	8.9	9.0	929	619	17.3	17.7	14.1	104	5431	93	.7	7.36	67.37	.041	.42	.80	27.8	8.7	8.41			
434	342	202	3.8	4.0	.79	26.6	1227	300	8.9	9.0	880	917	17.4	18.2	14.1	71	5842	98	.8	10.78	65.86	.041	.45	.78	26.5	8.7	8.41			
435	347	193	2.6	4.1	.93	17.8	1262	302	8.9	9.0	888	889	17.5	18.1	14.1	681	5969	103	.8	10.39	63.04	.041	.50	.74	24.9	8.7	8.41			
439	352	136	3.5	3.6	.91	35.0	1206	312	8.9	9.0	893	911	17.6	13.5	14.2	681	6261	108	.8	14.72	61.54	.051	.54	.71	21.7	8.8	8.41			
437	357	461	3.4	5.0	.65	33.8	1304	324	8.9	9.0	910	929	17.2	19.1	14.7	1661	6590	113	.9	7.43	50.27	.051	.39	.86	28.3	8.8	8.41			
449	362	154	2.1	4.1	.66	18.4	1314	327	8.9	9.0	924	946	17.4	19.1	15.1	1691	5710	113	.9	13.28	58.31	.051	.52	.61	24.0	9.2	8.41			
500	367	114	1.9	3.3	.84	9.9	1244	335	8.9	9.0	900	953	17.4	19.6	15.9	184	7230	123	1.0	23.00	57.74	.051	.57	.61	21.7	8.8	8.41			
502	372	134	2.6	3.4	.84	21.3	1280	339	8.9	9.0	900	924	17.4	19.6	15.9	187	7421	128	1.1	15.24	56.32	.071	.53	.50	23.8	8.8	8.41			
505	377	127	2.4	3.2	.82	15.0	1229	340	8.9	9.0	900	872	17.4	19.5	16.2	1981	7617	133	1.1	16.14	55.01	.071	.53	.47	23.6	8.8	8.41			
515	382	142	2.6	3.3	.79	18.4	1322	350	8.9	9.0	900	892	17.4	19.8	16.9	197	8030	138	1.2	14.09	54.43	.0								

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 6:56 12/20/78

TIME	DEPTH	NOP	TURQUE	RPM	BIT	PUMP	RTNS	LB/GAL	GAL/MIN	TEMP(C)	PVT	THIS BIT	EST	DXC	NXB	SP	ECD	NYNW	REVS	MT	HRS	CPMI	CPMB	TWI			
002	427	135	3.5	4.2	94	32.7	1271	393	8.9	9.0	940	931	17.6	21.1	14.1	271	10535	183	1.6	14.77	47.54	.111	.58	.43	22.0	8.9	8.41
612	433	04.3	4.1	4.1	80	42.8	1343	406	8.9	9.0	940	89	17.6	20.8	16.7	284	10945	188	1.7	23.71	46.98	.121	.66	.47	19.4	8.9	8.41
614	437	161	3.8	4.8	93	20.9	13681	406	8.9	9.0	940	904	17.6	20.5	16.9	283	11128	193	1.7	12.39	46.29	.121	.56	.45	23.3	8.9	8.41
616	443	152	3.1	4.5	102	22.1	13481	406	8.9	9.0	940	942	17.6	21.4	17.1	292	11319	199	1.8	13.02	45.61	.131	.57	.46	22.9	8.9	8.41
625	448	182	3.3	4.6	86	38.7	14021	418	8.9	9.0	940	952	17.6	21.2	17.4	302	11663	204	1.8	10.93	45.07	.131	.51	.46	24.9	9.0	8.41
027	453	192	4.1	4.8	87	32.7	13981	419	8.9	9.0	940	939	17.6	21.1	17.4	298	11798	209	1.8	9.74	44.38	.131	.51	.41	25.1	9.0	8.41
629	458	142	4.8	5.1	88	44.9	14651	419	8.9	9.0	940	964	17.6	21.2	17.4	312	11952	214	1.9	14.50	43.77	.141	.63	.41	21.3	9.0	8.41
340	463	125	4.5	5.4	d1	40.1	14291	431	8.9	9.0	950	934	17.8	21.5	17.4	319	12351	219	1.9	15.98	43.54	.141	.61	.44	21.5	9.0	8.41
642	468	128	4.3	5.2	119	39.8	13531	432	8.9	9.0	950	912	17.8	20.9	17.5	319	12596	224	2.0	16.37	43.06	.151	.69	.47	18.9	9.0	8.41
653	472	127	4.4	5.3	113	33.6	14521	443	8.9	9.0	950	932	17.8	21.8	17.5	336	13178	229	2.0	16.58	42.89	.161	.68	.54	19.1	9.0	8.41
656	478	129	4.4	5.3	123	32.4	14801	445	8.9	9.0	950	943	17.8	21.4	17.5	338	13448	234	2.1	15.80	42.43	.161	.72	.53	18.1	9.0	8.41
059	483	02.0	3.3	5.1	123	19.5	14541	446	8.9	9.0	950	942	17.8	22.1	17.5	348	13829	239	2.1	32.04	42.11	.171	.88	.57	12.4	9.0	8.41
711	488	137	4.1	5.0	128	35.4	13531	459	8.9	9.0	950	978	17.8	22.3	17.5	360	14411	244	2.2	14.74	41.76	.181	.67	.58	19.8	9.0	8.41
713	493	135	4.5	4.9	126	39.8	13981	460	8.9	9.0	950	771	17.8	22.0	17.5	326	14696	249	2.2	14.85	41.34	.191	.69	.57	19.9	9.0	8.41
727	498	63.5	4.6	4.8	87	38.3	14071	473	8.9	9.0	950	908	17.8	22.4	17.6	288	15447	254	2.3	31.38	41.01	.191	.78	.60	15.4	9.0	8.41
730	503	131	3.8	4.9	88	31.5	13711	474	8.9	9.0	950	912	17.8	22.5	17.6	292	15628	259	2.3	15.02	40.64	.201	.61	.54	21.4	9.0	8.41
732	508	94.6	2.5	5.1	117	21.1	14271	479	8.9	9.0	950	918	17.9	22.4	17.7	290	15895	264	2.3	21.14	40.35	.201	.72	.54	17.7	9.0	8.41
748	513	129	4.0	5.2	118	28.8	13711	490	8.9	9.0	950	903	17.9	22.7	17.7	333	16008	269	2.4	15.67	40.09	.211	.66	.57	20.0	9.0	8.41
751	516	412	3.5	5.3	121	19.8	13591	495	8.9	9.0	950	899	17.9	22.5	17.7	335	16910	274	2.4	17.97	39.77	.221	.71	.57	19.2	9.0	8.41
754	523	111	3.0	4.8	123	19.6	13821	499	8.9	9.0	950	923	17.9	22.5	17.7	341	17297	279	2.5	18.16	39.54	.231	.71	.59	18.3	9.0	8.41
806	528	104	3.2	5.0	119	29.1	14011	503	8.9	9.0	950	563	17.9	22.8	17.7	360	17845	284	2.5	19.38	39.36	.231	.70	.58	18.7	9.0	8.41
809	533	144	4.8	4.8	120	41.5	13681	507	8.9	9.0	950	918	17.9	22.7	17.7	369	18143	289	2.6	14.07	39.08	.241	.62	.58	21.7	9.0	8.41
821	538	51.1	3.8	4.9	94	30.4	14261	512	8.9	9.0	950	843	18.0	22.4	17.7	371	18767	294	2.6	39.12	38.92	.251	.77	.59	15.8	9.0	8.41
822	543	199	4.0	5.4	121	42.2	13831	512	8.9	9.0	950	922	18.0	22.7	17.7	362	19932	299	2.7	10.70	38.59	.251	.58	.50	23.5	9.0	8.41
824	548	162	4.3	5.6	122	31.9	13591	513	8.9	9.0	950	678	18.0	22.8	17.7	346	19139	304	2.7	12.50	38.22	.261	.65	.48	20.9	9.0	8.41
838	553	135	4.1	5.7	88	30.2	14291	525	8.9	9.0	950	746	18.0	22.7	17.8	350	19899	309	2.8	14.86	38.19	.271	.63	.50	20.7	9.0	8.41
844	558	44.4	4.5	5.4	87	37.5	14161	529	8.9	9.0	950	881	18.0	23.2	17.8	358	20441	314	2.9	45.35	38.32	.281	.89	.52	12.2	9.0	8.41
848	563	97.9	4.0	5.1	118	36.1	14501	536	8.9	9.0	950	886	18.0	23.2	17.8	351	20876	319	2.9	20.43	38.24	.291	.75	.56	17.2	9.0	8.41
907	568	49.3	1.8	5.0	119	8.3	14681	552	8.9	9.0	950	830	18.0	23.3	17.8	348	22191	324	3.1	40.61	38.75	.311	.88	.57	12.3	9.0	8.41
911	573	14.7	3.3	4.9	123	11.0	14351	552	8.9	9.0	950	511	18.0	23.6	17.8	343	22749	329	3.2	25.77	38.73	.321	.80	.62	15.1	9.0	8.41
924	573	120	4.0	5.0	120	41.4	14391	561	8.9	9.0	950	930	18.0	23.7	17.9	355	23508	334	3.3	17.36	38.70	.331	.57	.65	20.3	9.0	8.41
929	563	04.0	3.2	5.3	117	30.7	14611	564	8.9	9.0	950	676	18.0	23.4	17.9	359	24009	339	3.3	25.07	38.65	.341	.79	.61	16.1	9.0	8.41
931	568	104	4.6	5.4	120	40.2	14421	565	8.9	9.0	950	835	18.0	23.6	17.9	362	24324	344	3.4	19.17	38.44	.351	.74	.60	17.6	9.0	8.41
945	593	57.1	4.3	5.5	120	40.2	13711	569	8.9	9.0	950	931	18.0	23.9	17.9	362	25142	349	3.5	21.10	38.48	.361	.75	.62	17.6	9.0	8.41
951	598	77.4	4.5	4.9	114	33.2	13541	574	8.9	9.0	950	901	18.0	23.8	17.9	348	25844	354	3.6	26.81	38.59	.371	.78	.66	16.5	9.0	8.41
1011	503	35.7	3.6	5.7	115	36.9	14171	584	8.9	9.0	950	930	18.1	24.2	17.9	362	27094	359	3.7	57.45	38.95	.401	.95	.69	10.2	9.0	8.41
1018	009	48.4	4.0	4.6	122	39.1	14011	591	8.9	9.0	950	535	18.1	24.0	17.9	377	29056	364	3.8	41.54	39.23	.421	.93	.71	11.5	9.0	8.41
1024	014	49.9	3.4	4.5	124	35.7	13651	593	8.9	9.0	950	912	18.1	24.2	17.9	395	29771	369	3.9	41.12	39.31	.431	.93	.74	11.5	9.0	8.41
1103	019	51.8	4.3	5.3	123	36.3	13931	603	8.9	9.0	950	911	18.1	24.4	17.9	394	29600	375	4.0	37.77	39.35	.441	.93	.73	11.6	9.0	8.41
1104	024	45.5	2.9	4.5	123	20.2	13971	604	8.9	9.0	950	869	18.1	24.2	17.9	401	30407	380	4.1	44.69	39.50	.461	.94	.77	11.2	9.0	8.41
1109	029	72.2	3.4	4.5	123	32.9																					

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 7:02 12/20/78

TIME	DEPTH	TOP M/H	TORQUE INST MAX	KRM	BIT	PUMP WT	RINS PSI	DEPTH	IN	OUT	LB/GAL	GAL/MIN	TEMP(C)	PVT	REVS	MT	THIS BIT		EST HRS	DXC	NXB	SP	ECD	NXMW			
																	IN	OUT	LAG	REV	MT	CPMI	CPMB	TWI			
11203	575	44.2	2.7	5.2	115	16.1	14621	656	8.9	9.0	950	878	18.2	25.0	18.0	516	37072	435	5.0	46.01	39.22	.571	.88	.70	13.3	9.1	8.41
11222	604	72.0	3.0	4.3	115	11.6	14661	659	8.9	9.0	950	966	18.2	25.1	18.0	520	37843	440	5.1	27.79	39.26	.581	.72	.71	18.2	9.1	8.41†
11226	689	80.8	4.2	4.5	117	34.1	14681	663	8.9	9.0	950	890	18.3	25.0	18.0	500	38292	445	5.1	25.50	39.18	.591	.76	.65	17.7	9.1	8.41
11230	694	57.9	4.0	4.7	118	32.4	14671	670	8.9	9.0	950	921	18.3	25.0	18.1	499	38794	450	5.2	36.37	39.13	.601	.87	.65	13.9	9.1	8.41
11244	699	55.7	4.0	6.4	122	32.0	14281	675	8.9	9.0	950	920	16.3	24.8	18.1	478	39686	455	5.3	37.16	39.15	.611	.91	.64	12.8	9.1	8.41
11245	704	51.7	4.4	6.1	122	34.6	14651	679	8.9	9.0	950	933	18.7	24.8	18.1	471	40220	460	5.4	39.84	39.14	.621	.91	.65	12.5	9.1	8.41
11300	709	47.3	3.7	4.8	119	34.3	14601	684	8.9	9.0	950	956	18.8	25.2	18.1	469	40998	465	5.5	42.27	39.13	.631	.89	.67	12.7	9.1	8.41†
11305	714	42.2	4.3	5.6	120	37.5	14781	686	8.9	9.0	950	952	18.8	25.1	18.1	453	41538	470	5.5	47.67	39.11	.641	.95	.63	11.4	9.1	8.41
11309	715	86.9	4.0	5.6	123	35.0	14851	691	8.9	9.0	950	968	18.9	25.3	18.1	460	42086	475	5.6	22.81	39.07	.651	.78	.67	16.9	9.1	8.41
11324	724	74.4	4.0	6.0	106	36.8	15661	697	8.8	9.1	950	969	19.0	25.6	18.1	486	43084	480	5.7	26.80	39.24	.671	.78	.67	16.8	9.1	8.41†
11334	729	44.0	3.7	6.4	117	36.8	15501	707	8.9	9.0	950	972	19.2	25.5	18.2	514	44153	485	5.9	49.37	39.57	.681	.94	.70	5.6	9.1	8.41
11335	731	43.3	4.0	4.6	113	37.3	15741	709	8.8	9.0	950	964	19.2	25.4	18.2	512	44381	487	5.9	46.21	39.61	.691	.93	.71	5.9	9.1	8.41
11336	732	51.1	4.0	4.7	118	28.2	15731	710	9.0	8.9	950	968	19.4	25.6	18.2	517	44649	488	6.0	40.54	39.64	.691	.88	.73	7.6	9.1	8.41
11350	735	48.9	4.5	4.9	117	36.1	14471	716	8.7	9.0	950	868	19.4	25.8	18.2	536	45226	491	6.0	43.58	39.68	.701	.86	.74	8.2	9.1	8.41†
11351	737	128	5.5	5.6	117	56.8	14741	717	8.7	9.0	950	924	19.4	25.5	18.2	517	45361	493	6.0	15.67	39.59	.701	.67	.69	15.8	9.1	8.41
11353	740	105	3.6	6.5	119	35.8	14621	720	8.7	9.0	950	960	19.4	25.4	18.2	483	45609	496	6.1	19.56	39.57	.711	.72	.68	13.3	9.1	8.41
11356	742	46.0	5.7	5.7	119	54.1	14291	722	8.9	9.0	950	938	19.4	25.6	18.3	488	45917	498	6.1	42.82	39.57	.711	.91	.67	6.3	9.1	8.41
11400	745	53.0	4.2	5.1	118	37.5	14731	723	6.7	9.0	950	966	19.4	25.7	18.5	483	46346	501	6.2	39.53	39.64	.721	.88	.69	7.4	9.1	8.41
11414	748	34.7	3.7	5.5	123	34.2	14631	729	8.8	9.0	950	950	19.4	26.0	18.7	471	47269	504	6.3	57.61	39.88	.731	.93	.72	5.2	9.0	8.41†
11415	750	140	4.3	4.6	122	39.2	14581	729	8.8	9.0	950	944	19.4	26.0	18.8	469	47353	506	6.3	14.62	39.82	.731	.64	.70	16.3	9.1	8.41
11419	752	50.7	4.5	5.3	121	32.3	14401	730	8.7	9.0	950	938	19.6	24.1	18.8	455	47829	508	6.4	40.75	39.90	.741	.90	.71	6.8	9.1	8.41
11423	755	31.0	4.6	5.3	123	47.9	14081	734	8.7	9.0	950	961	19.6	22.5	18.8	342	48380	511	6.4	64.65	40.04	.751	1.03	.72	3.6	9.0	8.41
11424	757	31.4	4.1	6.0	124	37.3	14661	736	8.8	9.0	950	955	19.6	25.9	18.8	239	48910	513	6.5	64.20	40.15	.761	1.01	.74	4.0	9.0	8.41
11432	760	54.7	3.5	5.1	121	33.7	14011	736	8.8	9.0	950	936	19.7	26.1	18.9	239	49397	516	6.6	36.55	40.25	.771	.85	.77	6.6	9.0	8.41
11443	762	97.2	4.6	5.1	118	49.8	14861	745	8.8	9.0	950	945	19.8	26.2	19.1	237	50045	518	6.6	21.44	40.36	.781	.73	.77	12.5	9.0	8.41†
11448	765	31.3	4.1	5.4	117	35.5	14881	748	9.0	9.0	950	952	19.9	26.1	19.1	232	50619	521	6.7	64.07	40.51	.791	1.00	.77	4.1	9.0	8.41
11452	768	53.1	3.1	5.3	116	36.0	15821	749	8.9	8.9	950	926	20.0	26.2	19.2	239	51122	523	6.8	46.35	40.62	.801	.92	.79	5.7	9.0	8.41
11456	770	42.3	3.7	5.1	120	34.7	16631	751	8.9	8.9	950	971	20.1	26.3	19.3	238	51505	526	6.8	48.29	40.66	.801	.93	.77	5.4	9.0	8.41
11458	772	50.2	3.9	4.5	121	32.0	16571	752	9.1	8.9	950	950	20.1	26.4	19.3	247	51840	528	6.9	39.59	40.68	.811	.88	.77	6.8	9.0	8.41
11509	775	72.6	3.3	4.6	30	34.3	16001	757	9.1	8.9	950	941	20.3	26.7	19.3	249	52224	531	6.9	29.85	40.66	.811	.74	.75	11.2	8.9	8.41†
11512	777	33.3	3.0	5.5	116	36.7	16901	758	9.0	9.0	950	907	20.5	26.6	19.3	258	52596	533	7.0	59.70	40.70	.821	.98	.72	4.3	9.0	8.41
11519	780	23.1	4.2	4.9	116	39.0	16371	763	9.2	9.0	950	919	20.9	26.3	19.3	259	53385	536	7.1	95.65	40.96	.831	1.04	.75	3.3	8.9	8.41
11520	782	81.1	5.6	5.7	118	47.7	16521	763	9.1	9.0	950	894	20.9	26.7	19.3	276	53592	538	7.1	24.65	40.91	.831	.78	.73	10.4	9.0	8.41
11526	785	26.0	4.0	5.7	117	39.6	16731	763	9.1	8.9	950	860	21.1	26.7	19.4	289	54256	541	7.2	82.65	41.10	.841	1.07	.73	2.8	9.0	8.41
11545	787	9.6	2.8	5.6	101	21.9	15291	774	8.8	9.3	950	1003	21.5	26.8	17.4	321	55678	543	7.4	208.3	41.70	.861	1.02	.80	3.0	9.1	8.41
11554	790	20.5	3.0	4.2	126	36.9	16131	777	8.9	9.2	950	1011	21.5	27.1	19.3	333	56675	546	7.6	97.63	42.06	.881	.96	.78	3.9	9.1	8.41
11601	792	19.9	3.6	4.2	120	36.0	15531	781	9.0	9.2	950	976	21.8	27.2	19.7	347	57553	548	7.7	104.3	42.33	.891	1.04	.80	2.9	9.2	8.41
11603	795	29.5	3.7	4.2	122	35.0	15771	784	8.9	9.2	950	917	21.8	27.2	19.6	356	58181	551	7.8	69.48	42.49	.901	.95	.80	4.5	9.2	8.41
11614	797	18.3	3.3	4.8	122	35.2	16091	788	8.9	9.2	950	901	22.1	27.1	20.1	379	59144	553	7.9	121.4	42.80	.921	1.07	.81	2.4	9.2	8.41
11621	800	22.0	3.7	4.3	123	36.9	15231	789	8.7	9.1	950	816	22.1	27.1	20.2	3											

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 7:07 12/20/78

TIME DEPTH	HHP	TORQUE	RPM	BIT	PUMP	RINS	LB/GAL	GAL/MIN	TEMP(C)	PVT	THIS BIT		EST	DXC	NKB	SP	ECD	NMM								
											WT	PSI	DEPTH	IN OUT	IN OUT	LAG	REVS	MT	HRS	CPMI	CPMB	TW				
1826	620 41.0	3.5	4.2	115	36.3	1536	.817	8.9	8.9	950	917	24.6	27.7	22.6	5261	72111	583	9.6	50.94	46.65	1.081	.88	.83	6.1	9.0	8.41
1834	630 10.1	1.5	5.0	117	22.3	1596	.820	8.9	8.8	950	884	24.6	27.6	22.8	5431	73071	586	9.7	123.9	46.94	1.091	.89	.74	5.0	9.0	8.41
1844	634 49.4	3.2	4.1	118	30.1	1540	.822	8.9	8.9	950	906	24.9	27.8	22.8	5521	74236	588	9.9	104.8	47.34	1.101	.95	.84	4.1	9.0	8.41
1850	835 44.3	3.1	4.1	120	32.6	1593	.824	8.9	9.0	950	847	24.9	27.8	23.0	5671	74981	591	10.0	83.00	47.52	1.111	.97	.83	3.7	9.0	8.41
1858	837 41.2	3.4	3.7	114	36.3	1524	.826	8.9	9.0	950	949	24.9	27.8	23.3	5861	75946	593	10.1	96.67	47.79	1.131	.95	.83	3.9	9.0	8.41
1857	640 14.9	3.5	3.9	113	34.2	1659	.831	8.9	9.1	950	937	25.2	27.8	23.8	5021	77095	596	10.3	134.8	48.11	1.141	.96	.82	3.6	9.0	8.41
1924	642 44.6	3.4	4.1	117	34.5	1649	.832	8.8	9.2	950	926	25.2	27.8	23.8	4641	77892	598	10.4	90.56	48.33	1.151	.98	.80	3.5	9.0	8.41
1933	645 14.5	2.4	3.9	116	24.8	1668	.835	8.9	9.3	950	993	25.5	28.1	24.2	4181	78993	601	10.5	141.1	48.66	1.161	.98	.89	3.2	9.1	8.41
1955	841 44.2	3.0	4.9	117	34.7	1654	.839	9.0	9.3	950	978	25.9	27.7	24.5	2531	80312	603	10.7	142.2	49.06	1.171	1.07	.81	2.0	9.1	8.41
2007	850 41.2	2.1	4.5	114	20.5	1369	.841	9.0	9.4	950	998	26.5	27.7	24.7	2701	81784	606	10.9	180.3	49.59	1.191	1.00	.76	2.8	9.0	8.41
2027	853 43.3	3.7	4.3	60	45.9	1671	.846	9.0	9.4	950	929	27.2	27.7	24.8	3241	83326	609	11.1	89.36	50.06	1.211	.92	.85	4.7	9.0	8.41
2037	855 14.3	4.6	4.9	118	34.7	1793	.848	9.0	9.4	950	895	27.3	27.7	25.0	3441	84444	611	11.3	158.1	50.44	1.221	1.28	.82	.7	9.0	8.41
2049	857 10.1	4.0	5.2	121	35.8	1827	.848	9.0	9.4	950	940	27.3	27.5	25.1	3431	84728	613	11.3	26.29	50.39	1.231	.85	.81	7.0	9.0	8.41
2050	860 19.7	3.3	4.9	120	34.1	1791	.851	9.0	9.4	950	839	27.5	27.8	25.1	3701	86051	616	11.5	104.5	50.82	1.251	1.16	.81	1.2	9.1	8.41
2057	862 40.9	4.1	4.8	120	35.9	1808	.852	9.0	9.4	950	850	27.4	27.5	25.3	3881	86777	618	11.6	96.42	50.96	1.261	1.15	.83	1.3	9.1	8.41
2107	865 11.9	3.2	5.0	118	32.1	1814	.854	9.0	9.4	950	846	27.5	27.7	25.7	4151	88055	621	11.8	178.1	51.37	1.271	1.26	.85	.6	9.1	8.41
2119	867 40.3	4.9	5.2	115	38.4	1819	.855	9.0	9.4	950	803	27.2	27.7	25.7	4481	88727	623	11.9	68.31	51.50	1.281	1.05	.86	2.4	9.1	8.41
2128	870 16.9	4.3	5.2	117	36.4	1846	.858	9.0	9.4	950	602	27.4	27.9	26.2	4701	89721	626	12.0	122.8	51.77	1.291	1.21	.87	.9	9.1	8.41
2136	872 11.5	4.7	5.0	117	36.4	1820	.861	9.1	9.3	950	612	27.5	27.8	26.7	4841	90673	628	12.2	115.7	52.03	1.311	1.20	.89	.9	9.1	8.41
2145	875 17.6	4.0	4.8	120	38.0	1833	.864	8.9	9.3	950	891	27.5	27.8	27.0	5071	91735	631	12.3	116.3	52.33	1.321	1.19	.91	1.0	9.1	8.41
2154	877 10.4	3.3	4.6	117	31.7	1835	.866	8.9	9.4	950	876	27.7	27.9	27.2	5291	92764	633	12.5	125.7	52.61	1.331	1.19	.93	.9	9.1	8.41
2200	879 10.7	1.6	3.9	116	18.5	1819	.867	8.9	9.3	950	811	27.7	27.9	27.2	5461	93449	634	12.6	185.6	52.85	1.341	1.16	.84	1.1	9.1	8.41
RUN E-LOC8 40 878m, ISB/SWIC, FDC/GR																			RUN AND CEMENT 13 3/8" CASING AT 867m.							
START DEPTH 878m																										
150	880 40.3	3.4	4.2	109	27.8	2495	.879	9.1	5.7	949	1011	18.9	14.4	27.3	6041	4950	1	.0	106.6	4889	.011	1.15	.90	1.5	9.1	5.61
204	882 30.0	2.6	4.6	117	5.9	2499	.880	9.1	5.4	964	976	18.8	13.3	27.3	3041	5635	4	.1	52.50	1863	.021	.04	.03	32.9	253.6	159.51
208	885 40.1	3.2	4.4	121	29.2	2521	.880	9.0	7.4	952	992	18.8	14.2	27.4	6041	6091	6	.2	55.40	1145	.031	.03	.03	32.9	276.6	176.21
210	887 40.8	3.0	5.0	123	32.7	2553	.880	9.1	8.1	953	1008	18.9	14.1	27.5	6041	6354	9	.2	30.33	837.7	.041	.02	.01	33.0	512.2	339.81
213	890 60.9	2.7	4.6	120	28.3	2497	.881	9.0	8.6	940	873	18.8	14.3	18.9	6041	6688	11	.3	41.42	667.4	.051	.13	.10	31.8	71.0	49.71
216	893 45.7	3.8	4.5	120	42.4	2533	.882	9.0	6.9	939	863	18.9	14.0	18.9	6041	7016	14	.3	35.52	540.6	.071	.13	.10	31.9	69.9	48.61
407	895 31.5	5.3	7.7	79	32.0	1919	.886	9.1	9.2	792	761	18.6	14.3	18.9	4361	7718	16	.4	67.76	473.6	.081	.18	.14	30.8	52.4	35.61
412	898 31.7	6.2	7.6	102	54.1	1789	.888	9.0	9.3	760	733	18.5	14.4	18.6	3781	8110	19	.4	53.05	412.6	.091	.72	.57	10.6	12.7	8.71
416	900 40.0	4.4	6.8	107	22.8	1760	.889	8.9	9.3	772	743	18.5	14.3	18.6	3371	8500	21	.5	55.82	377.1	.101	.76	.58	9.2	12.5	8.61
421	903 40.5	4.7	6.1	109	28.5	1704	.891	9.1	9.3	778	776	18.5	14.7	18.6	3021	6999	24	.6	66.30	345.4	.111	.78	.62	8.0	12.0	8.01
428	905 40.2	4.7	6.1	108	41.5	2292	.894	8.8	9.3	981	913	18.6	20.0	18.6	2511	9776	27	.7	71.43	317.7	.131	.84	.69	6.2	10.9	7.11
442	908 39.6	3.0	6.6	118	25.4	2445	.901	9.0	9.3	925	929	19.2	20.2	18.5	3011	10337	29	.7	49.41	295.7	.141	.97	.79	3.9	9.5	6.21
448	910 40.5	4.6	5.3	72	27.0	6621	.903	9.0	9.3	433	462	19.5	20.9	18.5	3111	10795	31	.8	41.24	276.4	.151	.91	.80	5.3	9.4	6.21
450	912 40.1	4.6	5.6	71	45.6	773	.903	9.0	9.3	472	495	19.4	20.6	18.5	3131	10954	34	.8	31.91	258.6	.151	.81	.75	8.5	9.4	6.51
500	915 40.4	2.8	5.1	118	20.3	2534	.906	9.0	9.3	956	912	19.8	22.0	18.5	3081	11695	36	.9	45.74	247.8	.171	.99	.77	3.7	9.3	6.31
502	917 47.8	4.8	5.1	115	49.1	2488	.906	9.0	9.3	938	924	19.9	22.1	18.5	3051	11881	39	1.0	11.21	233.6	.171	.67	.76	14.5	9.3	6.41
504	920 40.0	4.3	5.9	118	44.8	2508	.906	9.0	9.3	944	914	20.1	22.3	19.0	2981	12120	41	1.0	33.15	221.7	.181	1.05	.72	3.1	9.3	6.71
516	922 42.0	4.6	5.4	117	45.6	2505	.911	9.0	9.3	931	910	21.2	22.2	19.0	3031	12757</										

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 7:18 12/20/78

TIME	DEPTH	ROP	TURQUE	RPM	BIT	PUMP	WT	PSI	HTNS	LB/GAL	GAL/MIN	TEMP(C)	PVT	THIS BIT	EST	DXC	NKB	SP	ECD	NNW							
016	947	39.7	4.2	4.7	104	42.3	2368	936	9.0	9.1	897	881	21.0	23.4	14.8	116	17040	69	1.6	52.12	153.2	.321	1.05	.80	2.6	9.3	6.0†
019	950	67.8	4.2	4.6	120	48.8	2575	938	9.0	9.1	930	916	21.0	23.4	16.0	123	17344	71	1.6	30.79	149.5	.321	.94	.79	5.0	9.3	6.1†
021	952	63.1	3.9	4.5	120	40.1	2552	940	9.0	9.1	945	901	21.0	23.9	17.2	134	17638	74	1.7	31.87	145.6	.331	.96	.76	4.3	9.3	6.3†
024	955	57.0	3.6	4.5	120	28.1	2676	942	9.0	9.1	961	937	21.0	24.2	18.9	163	17931	76	1.7	34.97	142.2	.341	.99	.76	3.6	9.3	6.3†
027	957	44.8	2.3	4.4	120	18.2	2617	944	9.0	9.0	961	948	21.0	24.4	19.4	173	18299	79	1.8	44.97	139.1	.361	1.00	.76	3.3	9.3	6.3†
038	960	59.3	4.2	4.5	107	46.5	2577	946	9.0	9.0	936	903	21.0	24.3	20.5	275	19760	81	1.8	33.71	136.1	.351	.94	.76	4.2	9.3	6.2†
040	962	70.7	3.7	4.7	123	42.1	2567	948	9.0	9.0	962	871	21.0	24.0	20.6	297	19044	84	1.8	28.27	133.1	.371	.95	.75	4.3	9.3	6.3†
042	965	63.1	3.4	4.6	142	23.0	2661	950	9.0	9.0	961	856	21.0	24.5	20.7	304	19335	86	1.9	32.26	130.4	.381	.98	.75	3.8	9.3	6.3†
045	967	67.4	4.3	4.7	123	47.2	2618	953	9.0	9.0	955	851	21.0	24.3	20.8	335	19623	89	1.9	29.78	127.9	.391	.95	.75	4.4	9.3	6.3†
047	970	67.6	4.3	4.8	123	43.3	2618	955	9.0	9.0	961	861	21.1	24.9	20.8	342	19895	91	2.0	30.22	125.3	.401	.98	.74	3.9	9.3	6.3†
073	973	32.8	4.2	5.0	101	45.4	2585	960	9.0	9.0	940	1035	21.1	24.9	20.9	445	20514	94	2.0	60.63	123.2	.421	1.09	.78	1.8	9.3	6.0†
703	975	27.7	3.7	5.0	121	37.4	728	964	9.0	9.0	477	650	21.1	25.3	20.9	469	21042	96	2.1	73.97	121.9	.431	1.12	.79	1.4	9.3	5.9†
711	977	46.4	3.8	4.7	124	47.6	752	965	9.0	9.0	477	506	21.1	25.3	20.9	474	21412	99	2.1	43.36	119.9	.441	1.05	.81	2.4	9.3	5.8†
722	980	20.9	4.4	4.4	116	52.2	2651	972	9.0	9.0	948	804	21.1	25.2	20.9	455	22465	101	2.3	98.27	120.0	.481	1.35	.80	.3	9.3	5.8†
730	982	29.4	3.8	4.6	122	35.7	2650	973	9.0	9.1	952	898	21.1	25.7	21.0	472	23418	104	2.4	68.91	119.8	.511	1.24	.80	.7	9.3	5.8†
733	985	55.5	3.5	4.6	124	34.8	2640	974	9.0	9.1	938	932	21.1	26.1	21.0	476	23756	106	2.5	37.01	118.0	.521	1.02	.82	3.0	9.3	5.7†
746	987	59.8	4.2	4.7	117	47.7	2570	980	9.0	9.1	947	952	21.1	26.2	21.0	476	24247	109	2.5	34.49	116.3	.531	.98	.82	3.5	9.3	5.7†
748	990	48.8	4.3	4.7	118	53.9	2596	980	9.0	9.1	942	959	21.3	26.3	21.0	474	24552	111	2.6	40.95	114.6	.541	1.10	.80	1.9	9.3	5.8†
752	992	39.3	4.5	4.6	109	49.7	2534	981	9.0	9.1	923	934	21.3	26.8	21.0	484	24982	114	2.6	52.00	113.4	.561	1.13	.82	1.4	9.3	5.6†
755	995	52.5	4.1	4.6	117	43.1	2524	983	9.0	9.1	912	936	21.3	25.9	21.0	483	25312	116	2.7	38.48	112.0	.571	1.05	.82	2.4	9.3	5.6†
758	997	63.7	4.0	4.5	117	44.6	2518	985	9.0	9.1	899	938	21.5	27.0	21.0	493	25602	119	2.7	30.60	110.4	.571	1.00	.82	3.3	9.3	5.6†
808	1000	45.0	3.9	4.6	113	43.3	2521	986	9.0	9.1	465	904	21.5	26.8	21.0	488	26073	121	2.8	45.32	109.2	.591	1.11	.81	1.7	9.3	5.7†
811	1002	47.5	3.8	4.4	114	48.7	2568	986	9.0	9.1	461	916	21.5	26.6	21.0	488	26420	124	2.8	42.44	107.9	.601	1.12	.82	1.6	9.3	5.6†
816	1005	23.5	4.2	4.7	117	44.7	2552	989	9.0	9.1	460	946	21.5	27.2	21.0	490	27008	126	2.9	86.05	107.2	.621	1.30	.84	.4	9.3	5.5†
819	1007	57.2	4.1	4.5	116	44.9	2591	990	9.0	9.1	469	953	21.5	27.5	21.0	493	27375	129	3.0	37.99	106.1	.631	1.07	.85	2.5	9.3	5.4†
822	1010	59.3	4.0	4.5	112	52.1	2557	991	9.0	9.1	462	952	21.5	27.7	21.0	495	27668	131	3.0	33.75	104.9	.641	1.01	.83	2.8	9.3	5.5†
832	1013	50.4	4.3	4.6	96	47.2	2590	993	9.0	9.1	441	828	21.5	27.7	21.0	500	28166	134	3.1	39.70	103.6	.651	1.02	.82	2.7	9.3	5.5†
834	1015	68.1	4.4	4.6	115	52.2	2558	994	9.0	9.1	469	933	21.5	27.7	21.0	494	28387	136	3.1	31.17	102.6	.651	1.00	.80	3.2	9.3	5.7†
836	1017	61.4	3.9	4.6	117	46.0	2571	995	9.0	9.1	470	939	21.5	27.6	21.0	496	28671	139	3.1	32.29	101.4	.661	1.03	.79	2.6	9.4	5.8†
839	1020	72.5	4.1	4.6	118	48.4	2535	996	9.0	9.1	462	950	21.5	27.9	21.1	493	28955	141	3.2	27.86	100.3	.671	.99	.79	3.4	9.4	5.8†
843	1022	45.7	4.1	4.6	117	47.8	2528	998	9.0	9.1	461	953	21.7	28.2	21.1	493	29398	144	3.2	45.85	99.53	.691	1.13	.81	1.3	9.4	5.6†
845	1025	60.4	4.3	4.7	123	47.6	2580	999	9.0	9.1	950	955	21.7	28.3	21.2	498	29666	146	3.3	33.59	98.47	.691	1.05	.80	2.3	9.4	5.7†
857	1025	33.3	4.2	4.6	119	46.2	2667	1004	9.0	9.1	950	946	21.7	28.3	21.4	498	30141	146	3.3	59.05	99.06	.701	1.17	.81	.9	9.4	5.6†
857	1025	35.1	4.4	4.4	123	51.3	2684	1004	9.0	9.1	950	950	21.7	28.3	21.4	498	30154	146	3.3	57.12	99.00	.701	1.17	.81	1.0	9.4	5.6†
859	1028	59.0	4.1	4.6	120	49.9	2635	1008	9.0	9.1	950	943	21.7	28.0	21.4	496	30448	149	3.3	34.93	97.99	.711	1.05	.81	2.2	9.3	5.6†
902	1030	52.5	4.0	4.6	118	39.9	2649	1011	9.0	9.1	950	925	21.7	28.1	21.4	503	30750	151	3.4	38.12	97.01	.721	1.07	.80	2.0	9.3	5.6†
905	1032	48.9	2.7	4.4	120	36.5	2668	1015	9.0	9.1	950	941	21.7	28.6	21.4	505	31101	154	3.4	42.92	95.17	.731	1.04	.80	2.4	9.3	5.6†
907	1035	66.0	4.3	4.5	119	49.9	2621	1019	9.0	9.1	950	934	21.7	28.9	21.4	505	31334	156	3.5	23.70	95.16	.741	.94	.79	4.5	9.3	5.7†
908	1037	86.6	5.1	5.1	120	55.1	2636	1022	9.0	9.1	950	923	21.7	29.0	21.4	510	31526	159	3.5	22.79	94.10	.741	.94	.76	4.3	9.3	5.9†
916	1040	56.8	4.4	4.6	126	52.6	2627	1025	9.0	9.1	905	917	21.7	28.8	21.4	508	32040	161	3.6	35.24	93.76	.761	1.06	.77	1.9	9.3	5.8†
918	1042	78.1	4.3	4.6	126	51.5	2642	1025	9.0	9.1	933																

LSSU AUSTRALIA FORTESCUE NO.3
UNIT #101 7:22 12/20/78

TIME	DEPTH	ROP	TORQUE	RPM	BIT	PUMP1	WT	PSI	HTNS	LB/GAL	GAL/MIN	TEMP(C)	PVT	THIS BIT	EST	DXC	NXB	NP	ECD	NXW							
11003	1067	55.3	4.2	4.5	124	47.5	2492	1054	9.0	9.1	877	911	22.2	30.4	21.6	522	36004	189	4.1	30.80	86.54	.87	1.02	.81	2.5	9.3	5.41
11006	1070	62.2	4.1	4.8	123	43.5	2517	1056	9.0	9.1	906	913	22.2	29.9	21.6	522	36305	191	4.1	35.55	85.96	.88	1.08	.80	1.7	9.3	5.41
11008	1072	79.5	4.2	5.1	123	48.7	2647	1057	9.0	9.1	921	937	22.2	30.3	21.6	520	36554	194	4.2	24.96	85.22	.89	.98	.79	3.1	9.3	5.61
11011	1075	48.2	4.4	5.0	126	50.3	2656	1059	9.0	9.1	930	934	22.2	30.6	21.6	524	36948	196	4.2	41.98	84.75	.90	1.14	.79	1.1	9.3	5.51
11027	1077	20.2	4.0	4.8	123	45.2	2549	1065	9.0	9.1	913	916	22.2	30.9	21.9	510	37967	199	4.3	103.8	85.08	.93	1.36	.83	.1	9.3	5.31
11029	1080	36.4	4.0	4.6	126	45.4	2525	1066	9.0	9.1	916	924	22.2	30.9	21.9	510	38230	201	4.4	31.31	84.44	.93	1.04	.82	2.2	9.3	5.31
11032	1082	50.0	4.4	4.7	124	50.5	2622	1069	9.0	9.1	889	916	22.2	30.6	22.0	507	38579	204	4.4	40.67	83.93	.94	1.12	.81	1.2	9.3	5.31
11035	1085	43.3	4.3	5.4	126	49.0	2557	1073	9.0	9.2	891	942	22.2	31.1	22.1	508	38978	206	4.5	47.72	83.53	.96	1.18	.82	.8	9.3	5.31
11037	1088	82.2	4.3	4.7	125	49.0	2595	1075	9.0	9.2	912	946	22.2	31.3	22.1	510	39245	209	4.5	24.82	82.93	.97	.99	.82	3.1	9.3	5.31
11041	1090	40.0	4.1	5.3	125	51.0	2572	1077	9.0	9.2	914	925	22.3	31.4	22.1	510	39651	211	4.6	52.71	82.54	.98	1.22	.81	.5	9.3	5.31
11051	1092	74.8	4.1	5.0	123	52.1	2550	1078	9.0	9.2	884	926	22.3	31.9	22.1	519	40260	214	4.6	26.32	82.29	.99	1.00	.81	2.7	9.3	5.31
11056	1095	30.4	4.3	5.1	123	50.9	2588	1081	9.0	9.2	894	998	22.3	31.5	22.1	517	40262	216	4.7	56.00	82.13	1.01	1.30	.83	.3	9.3	5.21
11060	1097	31.8	4.2	4.7	124	51.7	2566	1085	9.0	9.2	908	914	22.3	31.9	22.1	515	41304	219	4.8	63.05	81.86	1.02	1.27	.85	.3	9.3	5.01
11104	1100	33.7	4.1	5.0	125	49.3	2541	1089	9.0	9.2	892	892	22.3	32.0	22.1	519	41825	221	4.8	59.09	81.52	1.04	1.26	.87	.4	9.3	4.91
11107	1102	40.1	4.0	5.1	123	49.8	2582	1091	9.0	9.2	909	902	22.3	32.2	22.1	524	42255	224	4.9	52.01	81.31	1.05	1.24	.89	.5	9.3	4.81
11120	1105	43.7	4.6	5.0	121	47.8	2449	1095	9.0	9.2	887	902	22.5	32.8	22.1	524	43079	226	5.0	50.00	81.39	1.07	1.19	.91	.6	9.3	4.71
11125	1107	32.4	4.2	5.4	123	49.0	2594	1098	9.0	9.2	907	923	22.5	32.2	22.2	529	43620	229	5.1	61.66	81.19	1.09	1.27	.91	.3	9.3	4.71
11128	1110	42.3	4.2	5.2	125	48.6	2603	1100	9.0	9.2	910	904	22.5	32.5	22.2	517	44025	231	5.1	47.56	80.85	1.10	1.19	.90	.6	9.3	4.71
11131	1112	45.6	4.1	4.9	125	50.5	2639	1102	9.0	9.2	906	901	22.5	32.7	22.2	529	44043	234	5.2	47.83	80.53	1.11	1.19	.91	.6	9.3	4.71
11135	1115	33.6	4.3	5.1	124	54.4	2575	1104	9.0	9.2	918	891	22.5	32.9	22.2	531	44918	236	5.3	59.15	80.30	1.12	1.25	.91	.3	9.3	4.71
11148	1117	25.1	3.9	4.7	92	47.8	2562	1106	9.0	9.2	905	884	22.5	33.3	22.2	538	45681	239	5.4	80.64	80.41	1.14	1.26	.92	.3	9.3	4.61
11152	1120	27.3	4.3	4.8	120	49.6	2599	1109	9.0	9.2	908	866	22.5	32.8	22.2	541	46144	241	5.4	73.66	80.22	1.15	1.30	.92	.2	9.3	4.61
11157	1122	25.1	4.3	5.3	121	52.4	2584	1113	9.0	9.2	899	876	22.5	33.1	22.3	546	46788	244	5.5	83.40	80.19	1.17	1.34	.94	.1	9.3	4.51
11202	1125	28.9	4.2	4.6	120	49.8	2602	1116	9.0	9.2	893	895	22.5	33.6	22.4	534	47394	246	5.6	69.29	80.12	1.19	1.25	.94	.2	9.3	4.51
11205	1127	53.2	4.3	4.7	120	47.9	2569	1117	9.0	9.2	901	901	22.5	33.6	22.4	539	47668	249	5.6	39.00	79.70	1.19	1.11	.92	1.2	9.3	4.51
11217	1130	24.2	4.5	5.3	116	47.0	2582	1120	9.0	9.2	896	880	22.5	33.9	22.4	546	49481	251	5.8	82.57	79.84	1.21	1.29	.92	.2	9.3	4.61
11220	1132	41.0	4.4	4.7	117	47.7	2643	1122	9.0	9.2	900	880	22.5	33.7	22.4	546	48912	254	5.8	50.95	79.63	1.23	1.17	.92	.6	9.3	4.51
11224	1135	35.5	3.8	4.7	117	43.7	2657	1124	9.0	9.2	913	890	22.8	33.9	22.4	543	49382	256	5.9	56.42	79.43	1.24	1.20	.92	.5	9.3	4.51
11227	1138	63.2	4.3	4.8	118	47.3	2641	1125	9.0	9.2	917	918	22.8	34.0	22.4	548	49663	259	5.9	31.82	79.05	1.25	1.04	.90	1.9	9.3	4.61
11230	1140	60.0	4.1	5.0	117	46.1	2643	1127	9.0	9.2	900	925	22.8	34.3	22.4	548	50041	261	6.0	32.77	78.74	1.25	1.05	.88	1.7	9.3	4.71
11233	1142	41.6	4.3	5.4	119	45.8	2635	1130	9.0	9.2	693	912	22.8	34.5	22.4	555	50384	264	6.0	47.30	78.43	1.26	1.16	.85	.7	9.3	4.91
11245	1145	39.4	4.2	4.9	125	48.7	2654	1133	9.0	9.2	909	907	22.3	34.3	22.4	546	51213	266	6.1	50.56	78.56	1.28	1.18	.87	10.7	9.3	9.11
11248	1147	47.3	4.3	4.9	126	46.6	2672	1134	9.0	9.2	907	919	23.2	34.6	22.4	551	51534	269	6.2	42.07	78.22	1.29	1.14	.86	12.0	9.3	9.21
11252	1150	30.7	4.4	4.8	126	50.8	2643	1137	9.2	9.3	917	917	23.5	34.5	22.4	558	52059	271	6.2	65.94	78.10	1.30	1.27	.87	8.8	9.3	9.11
11255	1152	42.1	4.2	4.8	126	48.7	2640	1140	9.2	9.3	917	913	23.5	35.1	22.4	557	52453	274	6.3	47.47	77.81	1.31	1.17	.88	11.3	9.3	9.01
11258	1155	53.1	4.2	4.7	127	50.6	2665	1142	9.1	9.4	919	920	23.8	34.8	22.4	562	52821	276	6.3	37.63	77.51	1.32	1.11	.87	13.2	9.3	9.21
11310	1157	33.7	4.3	4.8	116	49.6	2444	1145	9.1	9.1	868	909	24.1	35.3	22.5	567	53579	279	6.4	59.66	77.47	1.34	1.19	.89	10.6	9.3	9.01
11315	1160	24.7	4.2	4.6	116	46.2	2674	1148	9.1	9.3	922	910	24.5	35.1	22.7	572	54113	281	6.5	80.58	77.40	1.35	1.29	.87	8.4	9.3	9.11
11320	1163	61.9	4.3	4.6	116	46.3	2632	1152	9.1	9.3	913	917	24.8	35.3	22.7	569	54712	284	6.6	33.00	77.36	1.37	1.03	.88	15.3	9.4	9.01
11325	1165	27.2	4.2	5.1	118	46.9	2648	1155	9.1	9.4	915	880	24.8	35.7	22.9	574	55278	286	6.7	74.28	77.32	1.38	1.27	.88	8.9	9.4	9.11
1																											

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 7:27 12/20/78

TIME	DEPTH	ROP	TORQUE	RPM	BIT	PUMP	RTNS	LB/GAL	GAL/MIN	TEMP(C)	PVT	THIS BIT	ESTI	DXC	NXB	TP	ECD	NXNW		
1432	1192	46.9	4.7	5.4	120	46.5	2566	1180	9.1	9.3	892	907	27.7	37.1	25.5	495	62047	314	7.6 42.99 77.11 1.53	1.10 .89 14.2 9.4 9.2
1435	1195	33.7	4.2	5.3	120	43.5	2590	1162	9.1	9.2	900	910	28.1	37.1	25.7	498	52472	316	7.7 60.24 76.94 1.54	1.21 .87 11.2 9.4 9.4
1453	1197	41.7	4.4	5.7	118	43.8	2592	1187	9.0	9.2	884	888	29.0	36.6	26.1	496	63274	319	7.8 47.75 77.12 1.55	1.13 .91 13.3 9.4 9.1
1460	1200	20.6	4.4	5.6	117	49.2	2553	1191	9.1	9.2	889	906	29.0	37.0	26.1	500	64067	321	7.9 97.05 77.26 1.57	1.33 .91 8.4 9.3 9.0
1505	1202	25.6	4.2	5.5	117	43.4	2561	1195	9.1	9.2	891	910	29.4	37.1	26.3	508	64731	324	8.0 81.71 77.30 1.58	1.29 .93 9.3 9.3 8.9
1509	1205	33.7	4.0	5.4	118	41.1	2549	1197	9.0	9.1	888	894	29.4	37.4	26.4	510	65220	326	8.1 61.64 77.19 1.59	1.21 .93 11.6 9.3 9.0
1513	1207	36.3	4.7	5.3	118	52.5	2587	1197	9.1	9.2	883	904	29.4	37.5	26.8	515	65675	329	8.1 57.26 77.04 1.60	1.18 .92 12.5 9.4 9.1
1526	1210	20.5	4.9	5.8	120	51.3	968	1200	8.9	9.2	512	754	29.8	37.8	27.6	534	66590	331	8.3 99.31 77.25 1.62	1.31 .95 8.9 9.3 8.8
FLUSHING RISER WITH NO.2 PUMP																				
1534	1213	18.6	3.6	5.4	118	35.4	963	1203	9.1	9.2	948	932	30.4	34.1	28.2	522	67475	334	8.4 108.6 77.47 1.63	1.28 .93 9.3 9.4 9.0
1541	1215	22.0	4.4	5.2	117	50.5	968	1207	9.1	9.2	949	924	30.7	35.8	28.6	521	68280	336	8.5 95.45 77.64 1.65	1.26 .95 10.0 9.4 8.9
STOPPED FLUSHING RISER.																				
1549	1217	39.2	5.0	5.3	124	55.0	2686	1210	9.2	9.0	899	905	31.1	36.5	28.9	520	68987	339	8.6 51.25 77.51 1.66	1.19 .96 12.5 9.4 8.7
1555	1220	31.7	4.3	4.9	123	53.4	2665	1211	8.9	9.1	908	896	31.6	37.8	29.2	527	69614	341	8.7 63.04 77.59 1.67	1.25 .95 11.0 9.4 8.8
1612	1223	20.6	4.5	5.1	115	42.9	2602	1216	9.0	9.1	888	894	32.4	36.6	29.6	539	70605	344	8.8 95.50 77.80 1.69	1.19 .98 11.5 9.3 8.6
1614	1225	10.1	4.6	4.8	114	48.5	2573	1216	9.1	9.1	900	909	32.8	37.1	29.7	541	70849	346	8.8 20.07 77.55 1.70	.86 .95 22.2 9.4 8.9
1618	1227	35.1	4.5	5.5	118	48.8	2609	1217	9.2	9.2	895	901	33.1	37.0	29.9	527	71310	349	8.9 60.58 77.42 1.71	1.22 .92 11.7 9.4 9.2
1623	1230	34.3	4.5	5.6	118	45.4	2568	1220	9.0	9.2	893	897	33.1	37.3	30.2	532	71887	351	9.0 58.92 77.37 1.72	1.21 .94 12.0 9.4 9.0
1627	1232	30.3	4.6	5.7	117	46.1	2599	1222	9.1	9.3	891	905	33.5	37.4	30.2	539	72392	354	9.1 68.45 77.29 1.73	1.25 .93 11.0 9.4 9.1
1633	1235	21.1	4.4	5.8	116	48.3	2611	1223	9.2	8.9	904	890	33.8	37.2	30.5	551	73086	355	9.2 94.61 77.34 1.75	1.35 .93 8.8 9.4 9.1
1651	1237	25.9	4.3	5.8	109	45.7	2610	1229	8.9	9.3	884	899	34.1	38.0	31.3	556	73969	359	9.3 82.12 77.60 1.76	1.29 .95 10.5 9.4 9.0
1664	1240	39.6	4.2	5.6	111	45.0	2610	1232	9.0	9.4	896	879	34.5	37.4	31.5	566	74400	361	9.3 50.15 77.46 1.77	1.16 .94 13.7 9.4 9.1
1659	1242	43.9	4.5	5.1	117	51.2	2603	1234	8.9	9.4	896	893	34.9	37.1	32.1	570	74915	364	9.4 48.05 77.37 1.78	1.14 .93 14.6 9.4 9.2
1704	1245	32.8	4.5	5.9	120	44.6	2547	1236	9.0	9.0	898	897	34.9	37.7	32.6	580	75563	367	9.5 60.56 77.34 1.79	1.22 .93 12.2 9.4 9.2
1713	1247	39.7	4.5	5.0	116	43.2	2634	1236	9.0	8.7	905	783	34.9	37.2	32.9	571	76130	369	9.6 54.44 77.34 1.80	1.15 .92 13.9 9.3 9.3
1725	1250	19.7	4.1	6.1	115	46.1	2543	1240	9.0	9.2	899	769	35.3	37.8	33.4	569	76900	371	9.7 105.9 77.48 1.81	1.35 .90 9.1 9.3 9.5
1731	1252	19.4	4.3	5.6	114	45.0	2522	1244	8.9	9.2	883	800	36.1	37.6	33.7	569	77599	374	9.8 108.7 77.54 1.83	1.36 .92 9.0 9.3 9.4
1740	1255	13.6	4.3	5.4	116	41.5	2604	1247	8.9	9.2	898	801	36.1	38.0	34.0	589	78624	376	10.0 147.6 77.85 1.85	1.46 .95 7.0 9.3 9.1
1745	1257	28.6	4.3	5.2	116	47.4	2579	1250	9.0	9.2	891	779	36.1	37.7	34.2	562	79139	379	10.0 75.89 77.78 1.86	1.27 .95 11.1 9.3 9.1
1752	1260	17.2	4.4	4.9	116	45.1	2592	1252	8.8	9.2	894	811	36.1	38.0	34.7	555	79929	381	10.2 115.4 77.95 1.87	1.38 .94 8.6 9.3 9.3
1612	1263	12.0	3.5	5.5	114	23.0	2551	1256	9.0	9.2	902	811	36.1	38.9	35.1	567	81257	384	10.3 157.5 78.43 1.89	1.29 .97 10.0 9.2 9.0
1618	1265	37.9	5.6	5.7	120	44.2	2543	1259	8.9	9.2	916	812	36.1	38.1	35.4	578	81894	386	10.4 56.98 78.45 1.90	1.13 .99 15.3 9.2 8.8
1820	1267	49.2	5.1	6.1	124	47.8	2571	1260	8.9	9.2	895	805	36.1	37.9	35.6	584	82202	389	10.5 40.67 78.22 1.91	1.07 .93 16.8 9.2 9.4
1825	1269	20.0	5.6	5.9	79	48.2	2586	1262	8.9	9.2	915	794	36.4	38.1	35.8	589	82753	391	10.6 99.47 78.30 1.92	1.29 .88 10.9 9.2 10.0
TRIP OUT FOR BIT #4																				
44	1271	11.9	3.8	4.6	52	39.0	2745	1265	9.1	9.2	904	939	36.4	31.9	36.0	495	607	0	.0 167.9 62227 1.92	1.38 .96 .0 9.1 3.9
49	1272	11.7	3.8	4.5	76	45.8	2700	1270	9.2	9.2	902	889	19.4	32.5	36.0	507	1157	2	.1 173.9 6507 .02	1.27 1.05 .0 9.1 3.6
100	1275	15.6	3.7	4.3	75	41.9	2693	1270	9.2	9.2	897	757	19.5	32.3	36.0	501	1941	4	.3 131.0 2487 .07	1.28 1.04 1.5 9.1 5.8
120	1277	25.4	4.0	5.1	116	46.5	2584	1271	9.1	9.1	882	932	19.4	32.9	36.2	446	2867	7	.5 84.35 1605 .12	1.27 1.09 1.7 9.2 5.5
125	1280	23.1	4.2	4.6	114	49.4	2590	1273	9.1	9.1	890	894	19.4	33.2	36.3	453	3491	9	.6 86.85 1173 .18	1.35 1.07 1.1 9.2 5.6
130	1282	26.7	3.9	4.6	116	47.6	2587	1274	9.1	9.1	887	909	19.5	33.4	36.3	458	4085	12	.6 75.01 935.7 .24	1.30 1.08 1.5 9.3 5.6
136	1285	25.9	3.8	4.4	116	48.3	2522	1275	9.1	9.4	891	894	19.4	33.6	36.3	461	4794	14	.7 77.27 735.1 .30	1.29 1.09 1.4 9.3 5.5
145	1287	15.0	3.7	4.4	117	51.4	2602	1276	9.1	9.4	895	874	19.4	33.5	24.6	456	5752	17	.9 126.7 633.2 .39	1.44 1.11 .7 9.4 5.4
204	1290	21.0	4.0	4.5	114	45.4	2509	1283	9.1	9.4	879	917	19.5	33.3	19.6	474	7231	19	1.1 99.05 613.3 .47	1.35 1.14 1.1 9.3 5.2
210	1292	24.5	3.5	4.6	115	47.6	2571	1286	9.1	9.4	881	917	19.5	33.5	19.4	482	8008	22	1.2 81.54 553.7 .53	1.30 1.14 1.5 9.3 5.2
216	1295	24.9	3.8	4.5	123	52.9	2622	1287	9.1	9.4	906	878	19.5	33.6	19.4	444	8660	24	1.3 80.55 504.4 .58	1.33 1.15 1.4 9.3 5.2
225	1298	15.7	3.9</td																	

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 7:45 12/20/78

TIME M/H	DEPTH FT	ROP INST	TORQUE KHM MAX	BIT WT	PUMP PSI	HTNS DEPTH	LB/GAL IN OUT	GAL/MIN IN OUT	TEMP(C) IN OUT LAG	PVT	REVS	MT	THIS BIT			EST	DXC	NXB	SP	ECD	NXMW		
													HRS	CPMI	CPMB	TW							
250	1305	37.0	3.8	4.4	120	52.5	2576	1296	9.1 9.4	897 851	19.5 33.3	19.4	455	11996	34	1.7 53.98	384.8	.81	1.21	1.14	2.6	9.3	5.3
258	1307	23.0	3.8	4.5	123	49.2	2682	1298	9.1 9.4	916 886	19.4 33.5	19.4	465	12921	37	1.8 89.28	365.9	.89	1.36	1.15	1.2	9.3	5.2
307	1310	16.6	3.5	4.6	121	48.3	2686	1302	9.1 9.4	903 890	19.4 24.1	19.4	355	13997	39	2.0 127.1	350.4	.95	1.44	1.15	.8	9.3	5.2
315	1312	14.9	3.9	4.7	120	49.2	2688	1304	9.1 9.4	917 904	19.5 33.6	19.4	274	15003	42	2.1 133.9	336.2	1.01	1.48	1.19	.7	9.3	5.1
322	1315	22.5	3.5	4.0	123	49.9	2684	1306	9.1 9.4	918 896	19.4 33.5	19.4	269	15792	44	2.2 88.78	322.9	1.06	1.36	1.18	1.2	9.3	5.1
338	1317	36.0	3.9	4.3	120	49.2	2702	1310	9.1 9.2	918 905	19.4 33.4	19.4	281	16848	47	2.4 55.53	311.6	1.11	1.20	1.19	2.5	9.3	5.1
345	1320	17.0	4.0	4.6	123	49.3	2674	1311	9.1 9.2	919 914	19.4 33.6	19.4	283	17647	49	2.5 120.2	300.8	1.16	1.46	1.17	.8	9.3	5.2
350	1322	24.6	3.7	4.1	123	49.2	2710	1313	9.1 9.2	917 912	19.4 33.8	19.4	288	18246	52	2.6 81.96	289.4	1.19	1.34	1.16	1.5	9.3	5.2
354	1325	33.5	3.9	4.7	121	54.7	2700	1315	9.1 9.2	911 913	19.4 33.9	19.4	295	18741	54	2.6 59.41	278.5	1.23	1.28	1.13	2.1	9.3	5.3
401	1327	21.0	3.6	4.8	122	47.9	2693	1315	9.1 9.2	890 908	19.3 33.8	19.4	299	19617	57	2.8 96.38	270.9	1.28	1.41	1.14	1.1	9.3	5.3
418	1330	15.7	4.0	4.6	120	50.6	2712	1321	9.1 9.2	910 864	19.5 33.7	19.4	310	20818	59	2.9 132.4	265.4	1.33	1.44	1.17	.9	9.3	5.2
425	1332	19.2	4.3	4.6	120	51.8	2696	1324	9.1 9.2	887 969	19.4 33.8	19.4	309	21576	62	3.0 106.2	257.9	1.37	1.41	1.16	1.1	9.3	5.2
433	1335	20.2	3.6	4.7	122	49.9	2660	1327	9.1 9.2	694 939	19.4 34.1	19.4	297	22566	64	3.1 99.26	252.2	1.42	1.40	1.16	1.2	9.3	5.2
440	1337	40.7	3.9	4.7	123	48.7	2647	1328	9.1 9.2	921 889	19.4 34.2	19.4	292	23447	66	3.3 56.55	246.8	1.47	1.39	1.17	1.3	9.3	5.2
448	1340	20.0	3.8	4.7	121	44.3	2660	1331	9.1 9.2	913 906	19.3 34.1	19.4	287	24469	69	3.4 110.3	242.1	1.52	1.42	1.19	1.3	9.3	5.1
506	1343	15.4	3.6	4.1	113	45.0	2487	1335	9.1 9.2	853 877	19.5 34.2	19.4	287	25901	72	3.6 130.2	238.3	1.58	1.41	1.18	1.1	9.3	5.1
517	1345	13.3	3.2	4.1	92	31.9	1030	1338	9.1 9.2	496 553	19.5 34.1	19.4	314	26799	74	3.7 151.0	234.7	1.61	1.30	1.15	1.9	9.3	5.3
530	1347	16.5	3.0	4.0	104	35.3	897	1339	9.1 9.2	469 510	19.3 33.9	19.3	333	27779	77	3.9 131.9	231.5	1.63	1.29	1.13	1.9	9.3	5.4
542	1350	9.2	3.3	5.4	102	40.1	911	1341	9.1 9.2	480 505	19.4 33.6	19.3	344	29060	79	4.1 221.2	229.4	1.67	1.45	1.12	.8	9.3	5.4
552	1352	15.9	3.2	4.2	104	37.4	894	1342	9.1 9.2	473 504	19.4 33.3	19.3	322	30082	82	4.3 125.9	226.5	1.70	1.30	1.13	2.0	9.3	5.4
602	1355	15.1	3.7	4.8	104	45.1	906	1343	9.1 9.2	481 500	19.5 32.9	19.3	308	31106	84	4.4 135.3	224.0	1.74	1.41	1.15	1.2	9.3	5.3
629	1357	9.0	3.1	4.6	103	35.9	921	1348	9.1 9.1	495 514	23.8 32.3	19.3	260	33043	87	4.7 231.0	225.0	1.79	1.45	1.15	7.3	9.3	8.1
649	1360	7.3	3.4	4.0	102	35.9	961	1353	9.1 9.1	495 535	30.1 32.0	19.3	277	35126	89	5.1 276.1	226.4	1.85	1.49	1.18	6.4	9.3	7.9
701	1362	12.6	2.4	3.6	104	23.7	926	1355	9.1 9.1	486 489	27.8 31.7	19.3	286	36410	92	5.3 161.4	225.0	1.98	1.31	1.17	9.9	9.3	8.0
711	1365	16.2	3.7	4.0	120	43.9	2560	1356	9.1 9.1	873 633	16.5 31.7	19.3	243	37406	94	5.4 127.3	222.6	1.91	1.30	1.17	10.0	9.3	8.0
723	1367	19.6	3.2	4.4	97	31.1	915	1358	9.1 9.1	491 476	16.3 31.4	19.3	260	38334	97	5.6 101.8	219.7	1.94	1.22	1.12	11.9	9.3	8.3
752	1370	8.2	3.3	3.8	105	39.4	904	1362	9.1 9.2	492 460	15.5 31.0	19.5	231	40499	99	5.9 256.1	221.4	1.98	1.37	1.12	8.5	9.3	8.3
810	1373	8.3	2.9	3.7	106	31.7	933	1365	9.1 9.2	496 468	15.2 30.7	24.4	262	42403	102	6.2 241.6	222.0	2.03	1.42	1.15	7.7	9.3	8.2
822	1375	13.5	3.2	3.7	106	31.2	946	1368	9.1 9.2	489 444	15.4 30.6	28.0	212	43728	104	6.4 150.7	220.8	2.07	1.31	1.15	10.0	9.3	8.1
838	1377	11.0	3.3	3.7	106	34.3	950	1369	9.1 9.2	439 459	15.3 30.3	27.9	236	45385	107	6.7 188.0	220.7	2.11	1.37	1.16	8.9	9.3	8.1
849	1380	11.6	3.4	3.7	108	35.6	918	1371	9.1 9.2	498 454	15.4 30.1	22.3	250	46603	109	6.9 175.2	219.2	2.14	1.35	1.15	9.0	9.3	8.2
824	1382	b.6	3.3	4.5	106	38.5	907	1375	9.1 9.2	499 460	15.9 29.7	15.6	286	49414	112	7.3 233.1	221.6	2.20	1.42	1.13	7.8	9.3	8.3
939	1385	11.4	3.0	4.0	106	35.3	894	1377	9.1 9.2	500 490	16.2 29.6	15.3	222	50967	114	7.5 176.0	221.2	2.24	1.35	1.15	9.1	9.3	8.1
952	1387	9.9	3.3	3.7	109	37.0	894	1381	9.1 9.2	499 483	16.4 29.4	15.2	236	52423	117	7.7 202.1	220.5	2.28	1.39	1.16	8.2	9.3	8.1
1005	1390	11.7	2.9	3.8	109	36.0	924	1381	9.1 9.1	490 488	16.6 29.2	15.2	253	53759	119	8.0 175.3	219.4	2.31	1.36	1.15	9.3	9.3	8.1
1021	1392	9.2	3.1	4.0	108	37.3	936	1383	9.1 9.1	492 491	16.7 29.1	15.3	276	55516	122	8.2 218.1	219.5	2.35	1.41	1.15	8.0	9.3	8.2
1046	1395	9.6	2.9	3.8	107	33.4	905	1387	9.1 9.1	492 438	17.0 28.7	15.7	248	57589	124	8.5 210.1	220.2	2.40	1.40	1.14	8.5	9.3	8.1
1057	1398	11.4	3.1	3.5	106	36.2	928	1389	9.1 9.1	491 458	17.1 28.9	15.8	221	58809	127	8.7 181.0	219.0	2.43	1.34	1.16	9.2	9.3	8.1
1122	1400	4.7	3.0	3.6	109	36.8	949	1393	9.1 9.1	500 472	17.3 28.6	16.0	246	61456	129	9.1 450.5	221.2	2.49	1.61	1.17	5.0	9.3	8.0
1130	1402	12.4	3.1	4.0	109	37.0	878	1394	9.1 9.1	501 473	17.3 28.5	16.2	257	62378	132	9.3 162.2	219.2	2.52	1.35	1.16	9.5	9.3	8.1
1152	1405	9.2	3.2	3.9	118	36.5	947	1397	9.1 9.1	512 463	15.9 28.4	16.5	366	64406	134	9.6 219.1	219.7	2.56	1.46	1.18	7.6	9.3	8.0
1212	1407	13.8	3.5	4.2	99	39.7	946	1399	9.1 9.1	503 468	15.7 28.1	16.6	421	66123	137	9.8 155.9	219.4	2.61	1.38	1.17	9.4	9.3	8.0
1236	1410	24.4	3.2	4.4	118	47.5	901	1402	9.1 9.1	499 454	15.5 28.0	16.9	426	68184	139	10.1 81.97	219.7	2.65	1.22	1.19	12.5	9.3	7.9
1251																							

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 7:50 12/20/78

TIME	DEPTH	ROP	TORQUE	RPM	BIT	PUMP1	RINS	LB/GAL	GAL/MIN	TEMP(C)	PVT	THIS BIT	EST	DXC	Nxb	Mp	ECD	NXMW	TW								
1440	1430	8.9	3.1	5.7	117	35.5	892	1421	9.1	9.1	497	468	18.2	27.6	15.7	556	82202	159	12.1	233.8	218.0	2.99	1.49	1.20	7.4	9.3	7.81
1455	1432	10.5	3.4	4.3	118	35.5	908	1424	9.1	9.1	496	480	18.1	28.0	16.3	560	84029	162	12.3	195.3	217.9	3.04	1.47	1.24	7.8	9.3	7.61
1522	1435	10.1	3.7	4.2	109	40.5	950	1427	9.1	9.1	488	488	18.3	25.5	16.6	580	86388	164	12.7	201.7	218.8	3.09	1.39	1.21	9.2	9.3	7.81
1537	1437	10.2	3.3	4.9	109	34.1	951	1429	9.1	9.1	490	507	18.5	28.1	17.1	537	87938	167	12.9	198.8	218.4	3.12	1.43	1.21	8.5	9.3	7.71
1552	1440	9.2	3.0	4.6	107	44.8	960	1432	9.1	9.1	487	496	18.6	28.0	17.5	546	89547	169	13.2	231.2	218.3	3.16	1.44	1.21	8.3	9.3	7.81
1605	1442	11.1	3.3	4.2	109	33.0	956	1433	9.1	9.1	498	507	18.8	28.0	17.7	558	91014	172	13.4	182.6	217.7	3.19	1.40	1.18	9.0	9.3	8.01
1625	1445	8.7	2.9	4.0	110	31.1	908	1436	9.1	9.1	497	507	19.1	28.1	18.2	556	93109	174	13.7	299.9	218.4	3.23	1.49	1.19	7.3	9.3	7.91
1639	1447	9.4	3.0	4.1	118	33.8	927	1439	9.1	9.1	489	508	19.2	28.1	18.2	562	94781	177	14.0	221.0	218.3	3.26	1.44	1.20	8.2	9.3	7.91
1658	1450	11.1	3.6	5.2	95	49.9	958	1441	9.1	9.1	501	504	19.3	28.4	18.1	535	96176	179	14.2	180.9	217.7	3.29	1.38	1.22	9.5	9.3	7.71
1717	1452	9.0	3.2	4.7	97	38.4	966	1444	9.1	9.1	491	514	19.2	28.2	18.3	536	98029	182	14.5	232.5	218.3	3.32	1.44	1.20	8.3	9.3	7.91
1737	1455	9.4	3.1	4.2	98	37.9	932	1447	9.1	9.1	492	494	19.4	28.2	18.6	532	99948	184	14.8	220.6	219.1	3.35	1.40	1.18	9.3	9.3	8.01
1757	1458	10.0	3.3	4.5	97	32.2	978	1450	9.1	9.1	491	498	19.4	28.3	18.9	529	101902	187	15.2	202.3	219.8	3.39	1.38	1.17	9.5	9.3	8.11
1815	1460	6.3	3.5	4.3	97	45.5	949	1452	9.1	9.1	490	497	19.3	28.3	19.0	527	103618	189	15.5	245.0	220.1	3.41	1.45	1.20	8.2	9.3	7.91
1840	1462	12.7	3.2	4.4	126	33.7	926	1455	9.1	9.1	494	516	19.4	28.2	19.3	522	105491	192	15.8	157.2	220.4	3.45	1.36	1.18	9.7	9.3	8.01
DUMPING MUD																											
1852	1465	13.8	3.3	4.5	129	36.2	964	1456	9.1	9.1	486	515	19.2	27.9	19.3	417	107000	194	16.0	152.4	219.7	3.48	1.37	1.15	10.0	9.3	8.21
1906	1467	9.2	3.3	4.2	128	43.2	892	1458	9.1	9.1	495	513	19.3	27.8	19.3	392	108829	196	16.2	228.2	219.5	3.52	1.47	1.17	7.9	9.3	8.11
1921	1470	11.1	3.6	4.4	126	52.1	909	1460	9.1	9.1	492	494	19.4	27.7	19.3	383	1110725	199	16.4	183.7	219.3	3.56	1.46	1.21	8.4	9.3	7.81
1936	1472	9.9	3.0	4.4	127	34.3	888	1462	9.1	9.1	492	496	19.3	27.7	19.3	385	112611	202	16.7	201.8	219.1	3.60	1.46	1.16	8.0	9.3	8.11
2001	1475	9.6	3.6	4.3	128	42.7	946	1466	9.1	9.1	483	504	19.4	27.4	19.3	372	114958	204	17.0	224.7	219.5	3.65	1.46	1.24	8.1	9.3	7.61
2015	1477	11.2	3.6	4.6	129	41.8	934	1468	9.1	9.1	489	501	19.3	27.5	19.3	374	116775	207	17.2	179.3	219.2	3.69	1.43	1.20	9.0	9.3	7.91
BACK TO USING TWO PUMPS																											
2033	1480	14.1	3.8	5.0	126	47.1	1467	1471	9.1	9.2	617	600	19.4	27.6	19.3	369	118547	209	17.5	144.8	219.0	3.73	1.46	1.21	8.6	9.3	7.81
2046	1482	11.2	3.5	5.0	129	44.5	2687	1473	9.1	9.2	862	650	19.4	27.9	19.3	364	120099	212	17.7	180.2	218.4	3.77	1.54	1.18	7.4	9.3	8.01
2055	1485	17.9	4.1	5.5	127	60.1	2647	1475	9.1	9.2	877	658	19.4	28.6	19.3	355	121087	214	17.8	112.6	217.1	3.80	1.41	1.21	9.9	9.3	7.81
2114	1488	12.4	3.6	4.7	127	62.9	2808	1480	9.1	9.2	878	669	19.4	28.8	19.3	359	122951	217	18.1	161.5	216.5	3.85	1.40	1.19	9.6	9.3	8.01
2122	1490	19.0	4.1	5.5	128	50.9	2651	1482	9.1	9.2	867	875	19.4	29.4	19.3	369	124031	219	18.2	105.0	215.8	3.88	1.46	1.21	9.2	9.3	7.81
2136	1492	10.9	3.5	5.2	118	53.4	2646	1486	9.1	9.2	874	879	19.4	30.1	19.3	361	125530	222	18.4	192.8	215.5	3.91	1.54	1.19	7.5	9.3	7.91
2147	1495	14.2	3.4	5.4	136	40.5	2604	1487	9.1	9.2	876	878	19.3	30.3	19.3	367	1127020	224	18.6	148.4	214.9	3.95	1.49	1.21	8.6	9.3	7.81
2205	1497	5.7	3.4	4.3	134	42.3	2581	1491	9.1	9.2	872	869	19.3	30.8	19.3	364	129355	227	18.9	207.0	215.1	4.00	1.57	1.22	6.8	9.3	7.81
2213	1500	18.2	3.4	3.9	134	40.3	2597	1493	9.1	9.2	866	874	19.3	31.1	19.3	364	1130529	229	19.0	110.1	214.1	4.03	1.40	1.21	10.2	9.3	7.81
2232	1502	13.0	3.4	4.5	130	43.6	2673	1495	9.1	9.2	672	872	19.4	31.4	19.3	359	1132099	232	19.2	155.8	213.5	4.05	1.47	1.18	8.8	9.3	8.01
2243	1505	13.0	3.6	4.7	122	43.9	2699	1498	9.1	9.2	868	902	19.4	31.8	19.3	357	1133519	234	19.4	163.1	212.9	4.10	1.47	1.17	9.0	9.3	8.11
2253	1507	18.5	3.7	4.2	123	45.5	2739	1500	9.1	9.2	883	891	19.3	32.1	19.3	362	1134715	237	19.6	120.6	212.1	4.12	1.39	1.18	10.5	9.3	8.01
HOLE NOT TAKING MUD																											
2265	1510	15.0	4.0	5.5	106	42.4	2572	1507	9.1	9.2	847	704	28.3	29.0	19.3	290	794	2	.1	142.1	6956	.03	1.31	1.20	9.1	9.2	7.91
2252	1512	26.6	4.5	5.3	102	37.6	2570	1507	9.1	9.2	835	846	28.4	28.9	19.3	275	1269	4	.2	75.01	2813	.07	1.19	1.15	11.5	9.2	8.21
2310	1515	12.8	4.7	5.3	98	43.3	2731	1507	9.1	9.2	835	777	30.0	31.7	19.3	283	2446	7	.4	155.8	1728	.15	1.31	1.16	8.9	9.2	8.21
2319	1517	10.5	4.7	6.1	98	42.9	2815	1507	9.1	9.2	874	844	31.9	31.2	19.3	285	3511	9	.5	193.3	1336	.23	1.47	1.13	6.3	9.3	8.41
2327	1520	21.3	3.3	4.8	120	12.8	2801	1510	9.1	9.2	885	804	32.2	30.9	19.3	287	4373	12	.7	94.77	1068	.29	1.24	1.14	10.7	9.3	8.31
2333	1522	23.0	4.5	4.8	120	38.9	2749																				

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 6:48 12/20/78

TIME	DEPTH	ROP	TORQUE	RPM	BIT	PUMP WT	KINS PSI	LB/GAL	GAL/MIN	TEMP(C)	PVT	THIS BIT		ESTI	DXC	NXB	SP	ECD	NXMW							
												IN	OUT	LAG	REVS	MT	HRS	CPMI	CPMB	TWI						
1458	1540	1.7	2.0	3.2	82	38.8	1455	1537	9.5	9.9	285	281	29.6	29.5	31.5	290	11610	4	2.5	1241	5961 0.001	2.01	1.24	5.9	9.6	8.7
1517	1543	1.8	2.2	3.1	79	37.0	1412	1539	9.4	9.6	285	269	29.6	28.8	30.4	349	17897	6	3.8	1223	4047 0.001	1.99	1.13	6.1	9.6	8.0
1432	1545	1.6	1.9	3.1	80	34.3	1368	1542	9.4	9.6	276	265	29.5	28.3	29.5	402	23957	9	5.1	1389	3203 0.001	2.03	1.77	5.5	9.6	8.2
558	1547	1.3	2.3	5.4	79	34.5	1441	1545	9.4	9.5	283	250	29.4	28.6	29.5	462	30852	11	6.5	1692	2758 0.001	2.07	1.48	5.3	9.6	8.8
2200	1555	18.5	4.6	4.7	98	46.7	2520	1547	9.5	9.5	816	673	30.8	29.8	29.5	407	7446	7	.3	107.6	1612 .31	1.26	1.22	11.5	9.6	8.4
2201	1555	17.2	4.0	5.1	98	50.4	1577	1547	9.4	9.5	317	670	30.9	29.7	29.4	397	7522	8	.4	121.8	1609 .31	1.31	1.04	13.3	9.6	8.5
2202	1556	35.5	4.2	5.0	97	51.4	2523	1547	9.5	9.5	814	662	31.0	29.7	29.4	389	7603	9	.4	65.38	1412 .31	1.13	1.32	11.5	9.6	8.4
2205	1557	28.6	4.4	5.7	98	54.2	2554	1547	9.3	9.5	327	675	30.9	29.9	29.4	401	7853	10	.4	69.93	1278 .32	1.19	1.08	12.0	9.6	8.4
2208	1558	17.7	4.3	5.8	130	50.5	2724	1547	9.4	9.5	850	670	30.8	30.0	29.4	387	8177	11	.5	112.9	1165 .34	1.42	1.03	12.0	9.6	8.4
2211	1559	18.9	4.3	5.4	132	49.8	2697	1551	9.4	9.5	851	667	30.9	30.1	29.4	394	8603	12	.5	106.1	1074 .35	1.45	1.01	12.6	9.6	8.4
2215	1560	16.0	4.3	4.8	130	51.3	2709	1552	9.4	9.5	859	657	31.0	30.2	29.4	395	9090	13	.6	127.0	1000 .37	1.53	1.16	13.9	9.6	8.4
WTC A3A 12.25' WITH 18.18.18 JETS.																				START DEPTH 1547.5M.						
1217	1561	18.9	4.6	4.8	131	52.0	2723	1553	9.4	9.5	856	651	31.0	30.3	29.4	394	9476	14	.6	106.1	931.5 .39	1.48	1.19	12.1	9.6	8.4
1220	1562	25.4	4.5	4.9	131	55.4	2720	1554	9.4	9.5	845	654	31.1	30.4	29.3	387	9797	15	.7	80.71	873.1 .40	1.39	1.59	12.6	9.6	8.4
1222	1563	24.9	4.1	4.9	130	50.9	2687	1555	9.5	9.5	850	639	31.2	30.4	29.3	390	10093	16	.7	82.46	823.5 .41	1.40	1.04	12.9	9.6	8.4
1225	1564	22.7	4.4	5.0	131	51.6	2676	1556	9.4	9.5	835	652	31.2	30.5	29.5	392	10417	17	.7	88.49	777.4 .43	1.42	1.28	13.7	9.6	8.4
1226	1565	29.9	4.5	4.6	130	56.3	2738	1557	9.4	9.5	845	648	31.4	30.5	29.6	396	10608	18	.8	66.89	737.3 .43	1.34	1.82	15.4	9.6	8.4
1229	1566	26.7	4.3	5.6	130	49.7	2727	1558	9.5	9.5	852	657	31.5	30.6	29.7	396	10924	19	.8	75.51	702.3 .45	1.37	1.05	15.2	9.6	8.4
1248	1567	11.9	4.8	5.9	116	50.1	2688	1560	9.4	9.5	848	646	31.4	30.4	30.6	376	12539	20	1.0	170.7	683.3 .51	1.57	1.39	10.3	9.6	8.4
1251	1568	12.4	5.0	5.8	96	44.1	2689	1556	9.4	9.5	834	637	31.5	30.6	30.7	363	12816	21	1.1	166.3	658.3 .53	1.60	1.37	10.1	9.6	8.4
1253	1569	20.7	4.5	5.5	130	66.0	2641	1561	9.4	9.5	834	646	31.6	30.7	30.7	367	13132	22	1.1	192.2	634.5 .54	1.47	1.36	12.9	9.6	8.5
1257	1570	21.0	4.3	6.2	131	52.0	2666	1562	9.5	9.5	832	656	31.7	30.9	30.7	368	13555	23	1.2	98.21	609.6 .56	1.48	1.37	13.1	9.6	8.4
1259	1571	22.8	5.0	5.3	133	62.4	2673	1563	9.4	9.5	837	651	31.7	30.9	30.8	360	13797	23	1.2	97.73	588.7 .57	1.52	1.34	12.3	9.6	8.4
1303	1572	18.6	4.6	6.5	132	47.8	2654	1554	9.5	9.5	834	621	31.7	30.9	31.6	363	14307	25	1.3	116.7	559.3 .59	1.43	1.22	13.7	9.6	8.4
1305	1573	31.0	4.5	5.1	123	50.2	2508	1564	9.4	9.5	815	637	31.9	31.0	31.6	365	14575	26	1.3	66.64	550.6 .60	1.27	1.20	17.3	9.6	8.4
1309	1574	17.9	4.4	5.1	131	54.1	2623	1565	9.4	9.5	878	628	32.0	31.1	31.6	361	15030	27	1.4	112.3	533.9 .62	1.42	1.18	13.4	9.6	8.4
1311	1575	19.9	4.5	4.9	130	54.1	2767	1566	9.4	9.5	873	657	32.1	31.1	31.6	351	15268	28	1.4	110.4	520.3 .63	1.42	1.17	13.5	9.6	8.4
1313	1576	23.1	4.3	5.4	132	48.9	2782	1566	9.4	9.5	867	666	32.1	31.1	31.6	353	15596	29	1.4	87.03	502.5 .64	1.35	1.14	15.0	9.6	8.5
1316	1577	22.2	4.4	5.2	124	51.9	2793	1567	9.4	9.5	850	667	32.1	31.1	31.6	346	15922	30	1.5	93.56	488.4 .65	1.38	1.13	14.5	9.6	8.4
1233	1578	14.9	4.5	5.7	126	51.3	2668	1569	9.5	9.5	837	671	31.9	30.2	31.6	342	17024	30	1.6	137.6	479.8 .70	1.39	1.12	13.7	9.6	8.5
1332	1581	15.3	4.7	5.4	125	48.7	2669	1569	9.3	9.5	850	668	31.9	30.2	31.6	347	17172	34	1.6	134.1	474.6 .70	1.43	1.11	13.3	9.6	8.4
1335	1582	19.2	4.6	5.5	126	50.8	2678	1569	9.6	9.5	849	662	31.9	30.6	31.6	346	17496	35	1.5	115.4	428.3 .72	1.41	1.10	13.7	9.6	8.4
1337	1583	22.9	4.6	4.8	124	52.0	2678	1570	9.5	9.5	847	645	31.8	30.9	31.6	354	17790	36	1.7	91.36	419.3 .73	1.34	1.08	15.4	9.6	8.4
1343	1585	23.6	4.3	5.3	125	51.0	2672	1571	9.4	9.5	839	650	32.4	31.1	31.6	343	18450	38	1.8	85.85	400.9 .76	1.32	1.04	15.9	9.6	8.4
1343	1585	24.5	4.0	4.4	125	47.0	2686	1571	9.4	9.5	839	652	32.2	31.1	31.6	337	18465	38	1.8	82.35	400.7 .76	1.31	1.04	16.2	9.6	8.4
1347	1586	16.7	4.1	5.0	121	49.1	2712	1573	9.4	9.5	844	642	32.1	31.2	31.6	329	18992	39	1.9	120.0	394.8 .78	1.40	1.01	13.6	9.6	8.4
1350	1587	14.9	4.3	5.1	111	46.7	2568	1574	9.5	9.5	840	658	31.9	31.4	31.7	336	19343	39	1.9	140.0	387.7 .79	1.44	1.02	13.1	9.6	8.4
1356	1588	11.7	3.9	5.8	123	50.1	2723	1576	9.5	9.5	840	669	32.2	31.4	31.8	325	20023	41	2.0	174.3	393.5 .82	1.47	1.02	12.0	9.6	8.4
1360	1589	19.2	4.5	5.0	118	54.5	2724	1577	9.4	9.5	855	645	32.7	31.6	31.9	325	20430	42	2.1	105.1	376.7 .84	1.35	1.02	15.2	9.6	8.4
1590	1590	21.0	4.5	5.4	101	45.5	2730	1577	9.4	9.5	847	662	32.6	31.6	31.9	325	20670	43	2.1	96.23	369.7 .85	1.30	1.00	16.1	9.6	8.4
15	1591	20.3	4.2	5.4	122	52.1	2747	1578	9.5	9.5	841	649	32.5	31.5	32.1	330	21025	44	2.1	98.50	363.7 .86	1.31	.99	16.0	9.6	8.4
19	1592	16.4	3.6	6.0	122	45.6	2739	1579	9.4	9.5	85															

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 8:54 12/20/78

TIME	DEPTH	N/P	TORQUE	RPM	BIT	PUMP	RTNS	LB/GAL	GAL/MIN	TEMP(C)	PVT	THIS BIT	ESTI	DXC	NXB	SP	ECD	NXMW	REVS	MT	HRS	CPMI	CPMB	TWI																									
JUMP DIVERS, REPAIR STACK, TEST OK.																																																	
MD#7, HIC A3A 12.25" WITH 18,18,20 JETS.																																																	
7	52.4	2732	1593	9.6	9.3	839	868	24.9	31.2	35.8	396	1163	1	.1	123.8	12037	.02	1.30	.74	9.2	9.7	9.0	.1	.40	.73	7.6	9.7	8.71																					
510	1602	16.1	4.2	4.9	120	49.3	2668	1593	9.6	9.1	850	842	26.9	32.4	35.8	389	1566	2	.1	125.7	5810	.05	1.40	.73	7.6	9.7	8.71																						
513	1603	20.5	4.3	4.7	123	51.6	2728	1593	9.6	8.9	865	870	27.9	33.1	35.9	398	1896	3	.2	106.3	4005	.08	1.38	.74	8.0	9.7	8.31																						
516	1604	20.6	4.3	4.7	124	52.6	2717	1593	9.6	8.8	843	882	29.2	33.0	35.9	401	2256	4	.2	99.79	3022	.11	1.36	.74	8.4	9.7	8.91																						
519	1605	21.9	4.3	4.7	123	51.0	2739	1593	9.7	8.7	862	846	30.9	31.0	35.9	399	2637	5	.3	93.61	2421	.14	1.34	.73	8.7	9.7	9.11																						
523	1606	18.9	4.2	4.6	126	52.5	2720	1593	9.7	8.3	861	802	31.1	30.2	35.9	398	3076	6	.3	108.3	2028	.18	1.38	.73	8.1	9.8	8.31																						
526	1607	19.5	4.1	4.6	126	49.8	2717	1593	9.6	8.9	870	730	31.6	29.4	35.9	381	3461	7	.4	104.0	1755	.21	1.37	.74	8.2	9.8	8.31																						
548	1607	13.9	4.3	5.0	117	53.4	2708	1594	9.6	9.7	865	809	31.1	28.8	36.0	374	5030	7	.6	143.0	1855	.31	1.35	.75	8.5	9.8	8.51																						
548	1607	14.8	4.2	4.6	118	54.1	2754	1594	9.6	9.7	865	807	30.8	28.8	36.0	386	5057	7	.6	144.3	1848	.32	1.37	.76	8.1	9.8	8.61																						
550	1608	22.8	4.6	4.7	138	53.3	2901	1595	9.6	9.7	884	829	31.1	28.9	36.0	382	5277	8	.6	90.62	1597	.33	1.33	.74	9.3	9.8	8.51																						
553	1609	23.4	4.5	4.9	138	56.4	2883	1596	9.6	9.7	898	844	30.7	29.2	32.3	384	5683	9	.6	88.95	1441	.36	1.35	.73	8.7	9.8	9.01																						
555	1610	25.2	4.3	5.0	139	51.6	2849	1596	9.6	9.7	897	860	31.2	29.3	27.7	374	5971	10	.7	82.42	1300	.39	1.34	.73	9.1	9.8	8.91																						
557	1611	22.0	4.4	4.8	139	52.4	2879	1597	9.6	9.8	898	840	30.9	29.5	26.2	384	6343	11	.7	90.53	1194	.41	1.36	.73	8.7	9.8	8.81																						
559	1612	27.3	4.6	4.8	139	62.4	2870	1598	9.6	9.8	899	862	31.2	29.6	26.2	382	6549	12	.8	76.05	1101	.43	1.31	.74	9.6	9.8	9.11																						
602	1613	22.7	4.3	5.4	139	55.0	2840	1599	9.6	9.8	888	878	31.5	29.8	26.0	389	6969	13	.8	88.15	1022	.46	1.36	.74	8.8	9.9	8.51																						
604	1614	20.2	4.5	5.1	138	51.0	2801	1600	9.6	9.7	869	838	31.4	29.9	26.6	389	7316	14	.8	89.91	953.0	.50	1.38	.74	8.3	9.9	8.81																						
607	1615	21.2	4.3	4.6	139	50.9	2811	1600	9.6	9.6	887	858	31.6	30.1	27.4	379	7648	15	.9	96.93	897.0	.52	1.38	.75	8.3	9.8	8.31																						
610	1616	22.3	4.1	5.1	139	58.3	2761	1601	9.6	9.5	877	853	31.5	30.2	28.5	375	8055	16	.9	89.83	849.0	.55	1.37	.75	8.1	9.9	8.81																						
624	1619	11.7	4.2	5.3	129	48.6	2709	1601	9.6	9.4	871	851	31.9	29.9	31.0	379	9111	17	1.1	173.3	811.8	.62	1.51	.76	6.2	9.8	8.21																						
627	1619	19.3	4.1	4.8	132	47.5	2720	1602	9.6	9.4	862	849	31.9	29.9	31.0	384	9421	18	1.1	105.6	771.3	.64	1.37	.75	8.5	9.8	8.11																						
629	1619	22.9	4.1	4.7	134	47.2	2715	1603	9.6	9.4	859	857	32.2	30.1	31.1	375	9680	19	1.1	88.85	742.6	.65	1.33	.75	9.4	9.8	9.11																						
629	1620	25.0	4.3	4.7	136	50.9	2752	1603	9.6	9.4	889	835	31.8	30.2	31.1	386	9782	20	1.2	78.49	709.2	.66	1.29	.75	10.1	9.8	8.81																						
631	1621	26.1	4.1	4.7	135	53.4	2811	1604	9.6	9.4	886	820	32.1	30.2	31.1	379	9985	21	1.2	75.70	669.0	.67	1.29	.75	10.3	9.8	8.81																						
633	1622	23.9	4.2	4.7	132	47.4	2685	1605	9.6	9.4	857	872	31.8	30.3	31.0	382	10233	22	1.2	83.76	538.1	.69	1.31	.76	9.9	9.8	8.81																						
638	1623	32.1	4.7	4.7	136	67.4	2764	1607	9.6	9.4	886	826	32.1	30.6	31.0	381	10962	23	1.3	62.28	622.5	.73	1.03	.64	12.7	11.9	8.51																						
638	1623	32.6	4.7	5.1	136	55.7	2725	1607	9.6	9.4	875	823	32.0	30.6	31.0	378	10973	23	1.3	61.42	621.1	.73	1.24	.64	15.9	9.8	8.11																						
640	1624	43.3	4.5	4.8	135	51.4	2765	1607	9.6	9.4	877	839	32.1	30.6	30.9	382	11200	24	1.3	85.21	603.8	.75	1.32	.77	9.6	9.8	8.71																						
641	1625	21.3	4.1	4.6	136	49.4	2745	1608	9.6	9.4	883	833	32.6	30.7	30.9	391	11419	25	1.4	92.24	577.5	.76	1.34	.77	9.2	9.8	8.21																						
643	1626	16.4	4.2	4.5	136	49.5	2806	1609	9.6	9.4	880	832	32.4	30.7	30.9	375	11669	26	1.4	121.9	559.9	.77	1.42	.77	7.7	9.8	9.11																						
645	1627	18.1	4.3	4.6	136	52.6	2765	1609	9.6	9.4	888	837	32.2	30.7	30.9	379	11889	27	1.4	113.3	541.2	.79	1.41	.77	8.1	9.8	8.91																						
646	1628	24.5	4.5	4.6	135	55.0	2753	1610	9.6	9.4	874	824	32.4	30.8	30.9	382	12074	28	1.4	81.52	522.6	.80	1.31	.78	8.7	9.8	8.51																						
648	1629	27.3	4.3	4.6	136	52.4	2779	1610	9.6	9.4	884	853	32.5	30.8	31.0	391	12272	29	1.5	74.16	506.8	.81	1.29	.78	10.3	9.8	8.61																						
650	1630	22.9	4.1	4.6	136	49.0	2733	1610	9.6	9.4	857	821	32.6	30.9	31.0	379	12539	30	1.5	87.13	491.8	.83	1.33	.78	9.5	9.8	8.21																						
651	1631	26.5	4.3	4.7	136	50.5	2806	1610	9.6	9.4	869	821	32.8	30.9	31.1	382	12694	31	1.5	76.31	477.7	.83	1.30	.79	10.2	9.8	8.71																						
653	1632	27.5	4.7	5.3	138	61.1	2752	1610	9.5	9.4	874	813	32.9	31.0	31.1	393	13023	32	1.6	75.35	465.9	.85	1.31	.79	10.1	9.9	8.21																						
707	1633	10.5	4.2	5.6	133	60.4	2742	1614	9.5	9.4	872	585	32.9	30.6	31.6	389	14211	33	1.7	193.2	451.1	.92	1.56	.79	5.6	9.8	8.01																						

ALBANY 1237102

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 9:05 12/20/7

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 9:16 12/20/78

TIME	DEPTH	ROP	TORQUE	RPM	BIT	PUMP WT	RTNS PSI	LB/GAL	GAL/MIN	TEMP(C)	PVT	THIS BIT	ESTI	DXC	NKB	SP	ECD	NWRI				
1451	1737	15.0	4.9	5.6	169	49.8	2745	1726	9.7	9.4	859	877	36.2	33.6	34.5	304	57312	137	6.5	135.6	186.2	2.69
1457	1740	56.3	4.6	5.1	168	52.4	2722	1729	9.6	9.4	859	828	36.0	34.0	35.0	312	58603	140	6.6	35.59	184.7	2.72
1461	1744	16.8	4.4	6.2	168	51.2	2712	1732	9.5	9.5	859	827	36.5	34.1	35.3	307	60071	142	6.8	125.7	183.7	2.77
1463	1745	32.3	4.6	5.3	169	52.5	2704	1734	9.5	9.5	859	882	36.8	34.3	35.4	307	61282	145	6.9	64.98	182.3	2.81
1466	1747	20.1	3.9	5.2	169	43.5	2676	1735	9.4	9.4	844	857	36.6	34.5	35.7	316	62503	147	7.0	101.2	181.0	2.85
1469	1750	35.5	4.5	5.2	167	52.4	2666	1736	9.4	9.4	844	824	36.6	34.5	35.9	319	63308	149	7.1	59.47	179.2	2.88
1474	1752	16.2	4.8	5.5	167	51.3	2803	1739	9.5	9.4	8510	842	36.9	35.1	35.9	317	64533	152	7.2	123.6	178.0	2.91
1475	1755	27.3	5.0	5.1	170	55.1	2770	1739	9.5	9.4	8514	920	37.1	34.7	35.9	329	65389	155	7.3	74.79	176.3	2.94
1477	1757	19.1	4.3	5.1	168	33.2	2786	1739	9.5	9.4	8494	906	37.4	34.8	35.9	324	66303	157	7.4	104.7	174.8	2.97
1480	1759	42.1	5.0	5.1	167	54.5	2727	1740	9.5	9.4	8527	832	37.5	34.8	35.9	324	66881	160	7.5	55.67	172.9	2.99
1481	1762	40.0	4.9	5.2	168	54.7	2789	1740	9.5	9.4	8473	903	37.2	34.8	35.9	338	67352	162	7.5	50.33	170.8	3.00
1486	1764	16.0	4.7	5.3	104	54.2	2867	1747	9.5	9.4	8487	853	37.8	35.7	36.4	350	68857	164	7.7	125.9	170.7	3.04
1489	1767	41.1	4.9	5.8	104	65.3	2872	1749	9.5	9.4	8491	899	38.1	35.4	36.4	345	69159	167	7.8	48.72	168.8	3.04
CIRCULATE BOTTOMS DUE TO LARGE VOLUME OF CAVINGS.																						
MUD VISCOSITY 55.																						
1534	1769	31.4	4.5	6.0	152	51.7	2746	1766	9.5	9.8	8504	962	40.7	37.3	38.0	367	71569	169	8.0	80.53	169.9	3.10
1541	1772	25.1	3.9	5.2	151	44.8	2910	1766	9.6	9.8	8488	962	40.7	36.9	38.1	376	72526	172	8.1	87.24	168.8	3.12
1545	1775	24.3	5.3	5.3	153	54.0	2892	1766	9.6	9.7	8500	804	40.0	36.7	38.2	369	73246	174	8.2	82.31	167.3	3.15
1549	1777	59.5	5.3	5.4	154	51.8	2884	1766	9.5	9.7	8522	797	40.2	36.7	38.4	376	73867	177	8.3	35.49	165.8	3.16
1608	1780	27.0	4.6	5.3	142	53.8	2911	1766	9.6	9.8	8489	830	39.8	36.7	39.5	383	75230	179	8.5	79.25	165.5	3.19
1614	1782	17.9	4.6	5.3	145	41.8	2882	1768	9.6	10.0	8493	861	40.1	36.7	40.0	392	76063	182	8.6	112.1	164.4	3.22
1618	1784	44.0	4.8	5.2	145	57.1	2685	1770	9.6	10.3	8519	857	39.8	36.9	40.4	391	76713	185	8.6	50.93	163.1	3.24
1625	1787	17.2	5.1	5.3	142	51.8	2882	1773	9.6	10.2	8527	904	40.1	37.0	40.7	395	77629	187	8.7	117.5	162.1	3.26
1731	1790	22.9	4.6	5.5	152	53.5	2915	1775	9.6	10.1	8505	876	40.1	37.0	40.7	390	78614	189	8.9	87.32	161.2	3.29
1746	1792	44.3	4.7	5.3	145	52.4	2852	1778	9.5	9.6	8481	892	39.9	37.6	40.0	396	79570	192	9.0	45.18	160.5	3.31
1753	1793	22.9	5.0	5.4	152	56.1	2871	1780	9.5	9.6	8509	898	40.0	37.3	39.9	403	80413	195	9.1	68.38	159.5	3.33
1759	1797	21.9	4.3	5.3	151	44.5	2818	1784	9.5	9.6	8497	874	39.9	37.3	39.9	405	81335	197	9.2	94.34	158.5	3.36
1765	1800	21.8	5.0	5.6	151	53.6	2849	1786	9.5	9.6	8516	908	40.0	37.4	39.8	410	82212	199	9.3	91.69	157.5	3.38
TRANSFER MUD.																						
1771	1802	21.1	4.5	5.2	151	49.8	2853	1788	9.5	9.7	8501	856	40.3	37.3	39.8	369	83114	202	9.4	95.17	156.6	3.40
1774	1805	45.5	4.9	5.8	152	54.7	2797	1789	9.5	9.5	8491	410	39.9	37.3	39.8	360	83627	205	9.4	43.95	155.5	3.42
1779	1807	31.3	5.2	5.7	153	52.8	2865	1789	9.5	9.5	8482	868	39.9	37.1	39.8	376	84394	207	9.5	44.59	154.5	3.44
1783	1810	33.5	5.2	5.8	153	54.2	2848	1791	9.5	9.6	8488	891	40.1	37.2	39.8	369	84984	209	9.6	59.61	153.3	3.46
1785	1812	13.0	4.8	5.7	153	53.1	2890	1797	9.5	9.6	8490	853	40.5	37.8	39.8	376	86321	212	9.8	161.5	153.6	3.49
1788	1815	31.4	5.0	5.6	152	50.8	2830	1801	9.5	9.5	8485	897	40.4	37.9	39.9	364	87480	214	9.9	69.25	153.1	3.51
1817	1817	14.7	4.6	5.3	152	50.3	2870	1809	9.5	9.3	8474	981	40.5	38.4	40.2	364	88918	217	10.1	138.8	152.9	3.54
1821	1819	38.0	4.9	5.5	152	53.6	2859	1809	9.5	97.2	8496	981	40.9	37.9	40.1	362	89496	219	10.1	52.58	151.8	3.56
1828	1822	20.8	4.8	5.4	150	44.8	2871	1810	9.5	91.5	8497	981	40.7	38.0	40.1	360	90541	222	10.3	75.60	151.2	3.59
1834	1825	25.2	4.3	5.3	150	44.4	2885	1811	9.5	88.8	8512	981	41.3	38.1	40.1	362	91490	225	10.4	82.13	150.5	3.61
1840	1827	24.8	5.0	5.2	153	50.6	2862	1813	9.5	93.0	8522	981	40.9	38.2	40.2	371	92322	227	10.5	80.75	149.7	3.63
1848	1830	20.2	4.4	5.2	150	46.1	2866	1815	9.5	91.4	8506	981	41.3	38.2	40.3	372	93507	229	10.6	99.24	149.4	3.66
1903	1832	24.3	4.6	5.4	150	51.6	2871	1818	9.5	89.5	8515	981	41.3	38.2	40.6	367	94583	232	10.7	82.82	148.9	3.68
1909	1835	22.0	4.4	5.4	151	53.3	2654	1820	9.5	91.6	8483	981	41.2	38.3	40.7	367	95474	234	10.9	87.75	148.3	3.71
1915	1837	45.3	4.6	5.1	149	51.1	2794	1823	9.5	96.9	8507	981	41.1	38.6	40.8	378	96337	237	10.9	78.98	147.6	3.73
1922	1839	24.6	4.3	5.1	150	54.0	2868	1826	9.5	95.6	8484	981	41.5	38.7	40.9	381	97419	239	11.0	87.92	147.1	3.76
1929	1844	26.2	4.4	5.3	147	47.6	2828	1828	9.5	90.8	8481	981	41.3	38.6	40.9	383	98364	242	11.1	76.28	146.5	3.78
1904	1845	19.0	4.7	5.3	122	52.4	2879	1836	9.5	92.2	8474	981	42.3	39.3	41.1	325	100021	244	11.4	113.6	147.5	3.81
1914	1847	12.3	4.1	5.4	101	48.3	2899	1840	9.5	89.5	8480	981	42.3	39.8	41.3	334	101150	2				

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 9:21 12/20/78

TIME	DEPTH	ROP	TORQUE	RPM	BIT	PUMP WT	PSI	RINS DEPTH	LB/GAL IN OUT	GAL/MIN IN OUT	TEMP(C) IN OUT LAG	PVT	REVS	MT	THIS BIT			EST HRS	DXC	NXB	SP	ECD	NWW			
															IN	OUT	REV	CPMI	CPMB	TW						
1243	1854	16.1	4.5	5.4	104	52.2	2858	1843	9.6 89.5	8504	981	42.2	39.5	41.4	351	104089	254	12.1	148.9	147.3	3.87	1.27	1.00	7.6	9.8	8.2
1215	1854	14.0	4.7	5.3	100	52.4	2832	1850	9.5 92.9	8488	981	42.6	40.8	42.2	361	105254	254	12.3	142.4	148.9	3.89	1.20	1.00	8.5	9.8	8.6
1216	1854	13.6	4.6	4.6	101	53.7	2821	1850	9.5 92.1	8481	981	42.6	40.4	42.2	363	105353	254	12.3	148.6	148.9	3.89	1.24	1.03	7.8	9.8	8.1
2127	1857	14.2	4.1	5.4	102	37.3	2845	1853	9.5 89.2	8508	981	43.4	40.1	42.2	376	106498	257	12.5	140.4	149.0	3.91	1.25	1.01	7.3	9.8	8.6
1238	1859	13.5	3.5	5.3	101	42.9	2868	1854	9.5 91.4	8485	981	43.3	39.9	42.2	382	110763	259	12.7	156.2	149.1	3.92	1.18	.95	8.7	9.8	9.1
1247	1862	16.2	4.3	5.5	104	47.6	2795	1854	9.5 92.1	8523	981	43.3	39.9	42.2	386	1108493	262	12.8	125.2	148.8	3.94	1.23	.99	7.9	9.8	8.4
1256	1865	16.0	4.2	5.9	104	54.0	2861	1855	9.5 91.3	8487	981	43.2	40.0	42.5	397	1109417	264	13.0	143.9	148.6	3.95	1.25	.97	7.9	9.8	8.3
1206	1867	15.5	4.6	5.4	101	50.2	2831	1857	9.5 93.3	8500	981	43.6	40.1	42.5	387	1110422	267	13.1	131.3	148.5	3.97	1.21	.98	8.2	9.8	8.3
1223	1869	30.8	4.3	5.2	153	48.5	2845	1864	9.5 96.8	8492	981	44.1	40.0	43.3	389	1111735	269	13.3	68.41	148.6	3.99	1.20	1.00	9.0	9.8	8.0
1228	1872	26.3	4.8	5.4	154	54.1	2842	1865	9.5 90.4	8525	981	43.8	40.3	43.3	384	1112524	272	13.4	75.71	147.9	4.01	1.23	.98	8.3	9.8	8.4
1244	1875	29.5	4.3	5.4	152	47.7	2881	1866	9.5 95.8	8487	981	44.2	40.3	43.3	386	1113367	274	13.5	67.15	147.3	4.03	1.19	.97	9.1	9.8	9.0
1250	1877	24.0	4.3	5.3	152	38.3	2819	1867	9.5 96.0	8523	981	43.8	40.0	43.3	391	1114223	277	13.6	86.61	146.8	4.04	1.22	.97	8.3	9.8	8.3
1255	1880	25.9	4.5	5.4	152	45.6	2663	1868	9.6 95.4	8491	981	43.9	40.1	43.3	394	1115008	279	13.7	77.29	146.1	4.06	1.22	.95	8.2	9.8	8.2
1253	1882	22.9	4.2	5.3	150	51.4	2668	1869	9.5 91.5	8485	981	43.7	39.8	43.4	396	1116293	282	13.9	98.08	146.0	4.09	1.20	.95	8.4	9.8	8.1
1230	1885	20.4	4.4	5.3	151	49.6	2843	1872	9.5 95.1	8504	981	43.7	40.4	43.3	396	1117274	284	14.0	99.28	145.5	4.11	1.22	.94	7.9	9.8	9.0
1236	1887	21.9	4.2	5.2	152	48.3	2795	1875	9.5 91.6	8516	981	43.9	40.5	43.3	394	1118237	287	14.1	91.27	145.0	4.13	1.20	.94	8.2	9.8	8.9
CONTINUOUS LANCE VOLUME OF CALCAREOUS MUDSTONE CAVINGS, FROM 1750 METRES.																										
1235	1890	21.6	4.6	5.5	151	52.8	2857	1879	9.5 95.2	8503	981	43.8	40.6	43.9	401	1119517	289	14.2	95.83	144.8	4.15	1.24	.96	7.4	9.8	8.4
1241	1892	23.6	5.1	5.1	151	58.5	2844	1881	9.5 89.4	8508	981	43.8	40.7	43.9	392	1120451	292	14.3	87.16	144.3	4.17	1.23	.95	7.7	9.8	9.0
29	1895	26.3	4.8	5.8	136	59.6	2779	1888	9.5 9.2	860	883	45.3	42.6	43.9	406	1122082	295	14.6	76.16	144.7	4.19	1.17	.96	9.5	9.8	8.0
34	1897	25.5	4.7	5.3	151	56.7	2776	1889	9.5 9.2	861	863	45.4	41.8	43.8	401	1122794	297	14.7	97.48	144.5	4.21	1.33	.96	6.4	9.8	8.4
40	1899	22.3	5.1	5.7	134	65.3	2775	1891	9.5 9.2	837	919	45.1	41.8	43.6	401	1123550	299	14.8	91.18	144.0	4.23	1.31	.95	6.4	9.8	8.4
45	1902	33.5	5.7	5.9	134	56.0	2861	1893	9.5 9.1	844	907	44.9	41.7	43.6	408	1124233	302	14.9	70.38	143.3	4.24	1.24	.96	9.0	9.8	8.0
50	1905	25.0	4.6	5.9	132	51.6	2832	1894	9.5 9.1	861	827	45.2	41.6	43.9	411	1124944	304	14.9	79.97	142.8	4.26	1.27	.95	6.3	9.8	8.2
57	1907	32.3	5.0	5.3	130	46.8	2797	1894	9.5 9.2	857	833	45.3	41.6	43.8	404	1125919	307	15.1	61.83	142.5	4.27	1.20	.96	8.6	9.8	8.3
114	1910	20.4	3.2	5.9	141	17.4	2819	1896	9.5 9.2	847	842	44.7	41.2	43.8	404	1127341	309	15.2	100.4	142.5	4.30	1.24	.89	7.4	9.8	8.2
119	1912	20.2	4.6	5.4	143	46.0	2815	1898	9.5 9.4	839	841	44.7	41.8	43.8	406	1128030	312	15.3	77.78	142.0	4.31	1.27	.96	7.0	9.8	9.1
125	1914	25.4	5.2	5.6	142	53.0	2823	1901	9.5 9.5	854	826	45.2	42.2	43.8	404	1128823	314	15.4	92.52	141.6	4.32	1.29	.94	7.3	9.8	8.4
132	1917	21.8	4.6	5.7	134	49.9	2859	1904	9.5 9.4	857	839	45.3	42.2	44.0	415	1129672	317	15.5	98.65	141.2	4.34	1.27	.92	6.6	9.8	8.9
137	1920	21.8	5.6	6.1	107	43.6	2869	1905	9.5 9.4	858	810	45.2	42.3	44.8	409	1130362	319	15.6	91.74	140.6	4.35	1.29	.94	6.1	9.8	8.7
156	1922	10.4	5.3	5.7	154	54.0	2721	1909	9.5 9.0	822	774	45.2	42.8	45.2	423	1131364	322	15.8	192.7	140.7	4.36	1.15	1.06	8.3	9.8	8.1
203	1925	16.2	4.2	6.4	153	44.8	2793	1912	9.5 9.2	859	871	45.7	42.5	45.1	407	1132468	325	15.9	128.2	140.5	4.39	1.39	.94	10.7	9.8	8.3
207	1927	31.5	5.0	5.4	154	52.8	2845	1914	9.5 9.3	851	878	45.6	42.5	45.0	415	1133120	327	16.0	66.86	139.9	4.40	1.29	.96	13.5	9.8	8.5
214	1929	26.9	4.8	6.0	85	54.9	2893	1916	9.5 9.3	843	795	45.4	42.9	44.9	415	1133789	329	16.1	83.44	139.5	4.41	1.24	.96	14.4	9.8	8.7
228	1932	15.0	4.6	5.8	103	46.2	1190	1920	9.5 9.5	846	543	45.5	42.3	44.8	434	1134794	332	16.3	138.7	139.8	4.43	1.31	.95	12.5	9.8	8.8
USING ONLY ONE PUMP ON THE HOLE.																										
421	1935	7.9	4.8	5.7	104	45.2	1222	1921	9.5 9.2	845	499	44.9	42.4	44.9	439	1136665	334	16.6	257.7	140.5	4.45	1.38	.98	10.5	9.8	9.1
427	1937	16.7	3.8	6.0	104	41.6	1229	1923	9.6 9.2	847	490	45.3	42.2	45.0	447	1137336	337	16.7	120.0	140.1	4.46	1.28	.95	13.2	9.8	8.8
315	1939	12.3	4.8	5.5	106	48.3	1292	1927	9.5 9.2	500	516	44.7	42.2	45.1	430	1139122	339	17.0	171.0	140.9	4.48	1.32	.97	12.3	9.8	9.1
329	1942	12.7	3.9	5.2	104	29.7	1321	1930	9.5 9.3	503	507	44.3	42.0	45.3	440	1140615	342	17.2	156.9	141.3	4.49	1.25	.97	13.6	9.8	8.4
346	1945	11.8	4.0	5.0	10																					

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 9:31 12/20/78

TIME	DEPTH	ROP	TURQUE	RPM	BIT	PUMP WT	HIPS PSI	WINS DEPTH	LB/GAL IN	GAL/MIN IN	TEMP(C) OUT	PVT LAG	REVS	MT	THIS BIT HRS	EST CPMI	DXC	NXB	SP	ECD	NXMW							
									WT	PSI	IN	OUT	IN	OUT	IN	OUT	IN	CPMB	TWI									
514	1967	21.7	5.2	5.9	115	50.9	2835	1952	9.5	9.0	842	920	43.3	41.8	44.0	478	151033	367	18.7	94.17	140.1	4.65	1.26	.97	15.5	9.8	9.1	
522	1969	22.0	4.7	5.9	117	51.7	2780	1955	9.5	9.3	845	971	43.7	41.8	43.8	489	151864	369	18.8	90.78	139.9	4.67	1.26	.97	15.8	9.8	8.0	
530	1972	16.4	4.9	6.3	120	46.5	2777	1959	9.5	9.3	828	981	43.6	42.0	43.7	499	152674	372	19.0	123.7	139.7	4.68	1.32	.97	14.4	9.8	8.3	
546	1974	16.2	5.7	5.9	139	54.4	2730	1962	9.5	5.3	800	993	43.9	41.9	43.3	445	153683	374	19.1	125.1	139.6	4.69	1.20	.99	16.9	9.8	8.1	
549	1977	49.0	5.7	5.8	155	57.9	2820	1964	9.5	7.6	826	994	43.8	41.6	43.3	426	154216	377	19.2	43.06	139.1	4.70	1.19	.95	18.4	9.8	8.9	
553	1979	37.9	5.6	6.0	156	55.6	2844	1964	9.5	9.3	847	1008	43.9	41.5	43.4	430	154724	379	19.2	59.47	138.6	4.72	1.29	.91	16.2	9.8	8.7	
601	1982	25.9	5.9	6.3	111	58.0	2842	1967	9.5	10.0	825	1001	44.8	41.8	43.5	430	155878	382	19.4	92.72	138.3	4.74	1.32	.93	15.1	9.8	8.3	
607	1985	20.5	5.1	7.1	118	56.2	2825	1970	9.5	10.3	831	1033	44.5	40.6	43.5	420	156642	384	19.5	97.55	138.0	4.76	1.35	.95	14.6	9.8	8.4	
613	1987	30.8	4.8	6.0	161	56.2	2871	1972	9.6	10.2	840	1023	44.2	40.7	43.5	416	157477	387	19.6	73.56	137.7	4.77	1.34	.95	15.1	9.8	8.0	
628	1989	60.7	5.6	5.8	156	61.9	2807	1974	9.6	8.2	830	996	43.7	40.1	43.5	435	158208	389	19.7	38.21	137.3	4.79	1.14	.95	20.6	9.9	8.0	
633	1992	37.0	5.1	5.9	156	56.1	2785	1974	9.5	9.2	822	896	43.2	41.2	43.5	449	158889	392	19.7	54.72	136.8	4.80	1.26	.94	17.3	9.9	8.0	
639	1994	29.5	5.3	5.9	154	59.6	2775	1978	9.5	9.8	823	901	43.5	41.4	43.5	449	159889	394	19.8	72.16	136.6	4.83	1.25	.92	17.7	9.9	8.5	
644	1997	31.5	5.5	5.7	157	51.5	2722	1980	9.5	9.4	823	817	43.5	41.4	43.5	454	160575	397	19.9	63.49	136.1	4.84	1.29	.95	16.8	9.9	9.0	
649	1999	39.2	5.7	6.3	157	55.1	2763	1931	9.5	9.4	836	893	44.0	41.2	43.5	461	161303	399	20.0	53.61	135.8	4.86	1.25	.96	18.1	9.9	8.0	
709	2002	31.6	4.5	6.1	135	56.7	2809	1986	9.5	9.5	835	765	43.5	40.5	43.6	473	162564	402	20.2	62.64	135.7	4.88	1.21	.96	18.5	9.9	9.1	
714	2004	26.8	5.1	5.9	108	58.4	2797	1987	9.6	9.4	815	855	43.7	41.1	43.7	450	163325	404	20.2	76.15	135.4	4.90	1.27	.95	17.5	9.9	8.7	
719	2007	33.1	4.8	5.7	156	57.3	2789	1988	9.5	9.4	838	718	43.5	41.2	43.9	425	164016	407	20.3	61.74	134.9	4.91	1.28	.95	17.5	9.9	9.1	
722	2010	39.0	5.1	6.5	156	56.3	2763	1991	9.6	6.2	837	655	43.5	33.1	44.1	363	164507	409	20.4	51.24	134.4	4.92	1.18	.95	19.8	9.9	8.6	
LUMPING MW																												
727	2012	23.7	6.1	6.4	105	60.4	2816	1993	9.6	9.4	833	732	43.4	41.2	44.3	310	165190	412	20.5	87.13	134.1	4.94	1.35	.92	16.1	9.9	8.5	
744	2014	40.2	5.6	6.5	134	53.9	2739	1998	9.5	9.4	802	833	43.5	41.1	43.9	332	166309	414	20.6	101.0	134.0	4.96	1.36	.95	15.9	9.9	8.3	
751	2017	89.9	5.4	6.1	154	57.8	2843	2000	9.5	9.4	831	660	43.7	41.6	43.8	334	166837	417	20.7	21.59	133.6	4.97	.95	.93	25.2	9.9	8.5	
759	2019	18.0	5.1	6.8	158	54.1	2834	2003	9.6	9.4	825	636	44.0	41.7	43.5	344	167773	419	20.8	117.5	133.4	4.99	1.39	.95	15.4	9.9	8.5	
605	2022	46.2	5.0	6.2	102	54.0	2807	2006	9.6	9.4	836	594	44.5	41.7	43.5	346	168490	422	20.9	44.34	133.1	5.00	1.12	.93	21.9	9.9	8.9	
614	2024	13.1	4.7	6.6	106	47.7	2807	2011	9.6	9.5	824	611	44.3	41.6	43.7	358	169709	424	21.0	154.1	133.0	5.02	1.40	.94	15.1	9.8	8.7	
636	2027	16.7	4.6	6.0	156	43.1	2921	2015	9.6	9.4	845	789	43.9	41.6	43.6	365	171154	427	21.2	121.0	133.2	5.04	1.35	1.07	16.3	9.8	8.9	
641	2029	36.0	5.1	5.7	156	57.7	2891	2016	9.6	9.5	837	702	43.8	41.3	43.5	370	171915	429	21.3	58.11	132.8	5.05	1.22	.95	19.9	9.9	8.7	
647	2032	36.0	5.3	5.6	154	53.4	2839	2018	9.6	9.5	850	738	43.9	41.5	43.3	384	172756	432	21.4	60.35	132.5	5.07	1.24	.95	19.3	9.9	8.5	
654	2035	23.5	4.3	5.6	156	41.5	2889	2021	9.6	9.6	827	898	44.3	41.8	43.2	389	173773	434	21.5	92.84	132.3	5.09	1.31	.95	17.8	9.9	8.4	
659	2037	28.1	5.1	5.6	156	46.9	2850	2024	9.6	9.6	853	854	44.5	42.0	43.2	387	174576	437	21.6	75.82	132.0	5.10	1.30	.95	18.2	9.9	8.4	
CHECK																												
924	2040	0.7	4.0	5.8	117	40.2	2827	2027	9.6	9.5	718	845	44.6	42.0	43.7	413	173167	440	21.8	228.9	132.3	5.12	1.16	.96	20.2	9.9	9.0	
930	2042	42.1	5.8	6.1	94	46.1	2813	2028	9.6	9.5	828	900	44.6	42.0	44.0	401	176813	442	21.9	93.45	132.1	5.13	1.27	.95	18.9	9.9	8.9	
940	2044	18.0	4.1	6.3	94	47.1	2841	2032	9.6	9.3	838	944	44.7	42.3	44.0	427	177909	444	22.1	113.0	132.1	5.15	1.29	.96	18.3	9.9	8.5	
954	2047	17.8	4.7	6.5	106	41.9	2877	2037	9.6	8.3	836	936	44.5	42.5	44.0	428	179002	447	22.2	113.3	132.0	5.16	1.32	.97	17.9	9.9	8.6	
1101	2049	20.3	4.7	6.8	139	53.8	2917	2039	9.6	9.1	837	943	45.3	42.5	44.0	434	179779	449	22.4	101.0	131.9	5.17	1.29	.98	18.9	9.9	8.2	
1108	2052	20.2	5.5	6.2	145	51.9	2859	2039	9.6	9.3	845	917	45.0	42.7	43.9	432	180569	452	22.5	102.7	131.6	5.18	1.35	.98	17.8	9.9	8.2	
AT 2052 METRES WITH BIT #8, MAC X3A 12.25" WITH 20,20,20 JETS																												
134	2053	27.0	5.5	6.3	78	49.5	2763	2052	9.7	9.5	560	610	35.5	35.1	35.0	1881	1679	1	1	0	80.75	25144	.051	1.09	1.04	13.8	9.7	8.5
136	2054	33.0	6.1	6.4	93	45.1	2712	2052	9.6	9.5	560	610	35.4	35.4	35.0	2001	1799	2	1	1	60.							

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 9:39 12/20/78

TIME	DEPTH	RPM	TURQUE	BIT	PUMP	RINS	LB/GAL	GAL/MIN	TEMP(C)	PVT	REVS	MT	THIS BIT			EST	DXC	NKG	SP	ECD	NXMM						
													IN	OUT	LAG	HR	CPMI	CPMB	TWI								
111	2064	31.9	5.3	6.1	150	53.6	27631	2054	9.5	9.5	850	856	39.1	37.2	35.0	2031	5723	12	.6	57.26	1353	.16	1.33	1.11	8.6	9.7	8.51
113	2065	28.8	5.0	6.2	151	56.0	28081	2055	9.5	9.5	850	856	38.7	37.7	35.0	1971	6040	13	.7	69.16	1249	.171	1.40	1.09	7.5	9.7	8.51
135	2066	41.1	4.8	6.3	140	49.4	27491	2057	9.5	9.5	851	856	39.4	37.7	35.8	1891	7427	14	.8	183.1	1188	.201	1.54	1.09	4.8	9.7	8.51
139	2067	10.0	4.4	5.6	138	48.0	27271	2058	9.5	9.5	867	849	39.1	37.7	35.8	1891	7996	15	.9	201.7	1117	.221	1.55	1.09	4.6	9.7	8.51
140	2068	29.0	4.8	5.3	136	48.9	28471	2059	9.5	9.7	868	855	39.0	37.8	35.8	1981	8148	16	.9	71.12	1044	.221	1.29	1.10	9.5	9.7	8.51
141	2069	57.6	4.6	5.3	133	52.0	27891	2059	9.5	9.7	880	856	39.1	37.9	36.2	1711	8310	17	1.0	35.95	987.6	.231	1.08	1.06	14.9	9.9	8.51
144	2070	29.9	4.8	5.7	95	46.7	27201	2060	9.6	9.7	855	857	39.2	38.2	36.7	2071	8584	18	1.0	68.58	934.9	.231	1.21	1.04	7.0	9.9	8.51
149	2071	15.2	5.3	6.7	101	53.4	26771	2060	9.6	9.7	848	857	39.7	38.5	37.3	1831	9156	19	1.1	132.5	892.1	.251	1.41	1.04	7.0	9.9	8.41
153	2072	14.8	5.3	5.6	134	58.0	26101	2061	9.6	9.7	838	843	40.1	38.9	37.9	2001	9548	20	1.1	155.2	860.5	.261	1.42	1.01	7.0	9.9	8.51
155	2073	41.0	5.5	5.9	137	56.8	27071	2061	9.6	9.7	866	849	40.2	39.0	38.4	1831	9814	21	1.2	109.9	817.4	.271	1.44	1.09	6.6	9.9	8.51
157	2074	22.2	5.1	6.3	134	58.6	28551	2062	9.6	9.7	883	857	40.1	39.0	38.7	1711	10174	22	1.2	90.60	782.1	.281	1.36	1.07	8.1	9.8	8.51
201	2075	17.3	5.4	6.1	133	56.2	28661	2065	9.6	9.7	894	857	40.6	39.1	38.7	1781	10574	23	1.3	118.4	755.6	.291	1.41	1.08	7.1	9.8	8.51
406	2076	42.4	5.7	5.9	105	57.0	28941	2066	9.6	9.7	885	856	40.8	39.1	38.8	1691	11323	24	1.4	162.8	729.3	.311	1.49	1.08	5.7	9.8	8.51
408	2077	17.0	5.4	6.0	107	59.7	27871	2066	9.6	9.7	884	857	40.8	39.2	38.8	1751	11489	25	1.4	118.7	702.0	.311	1.41	1.09	7.2	9.8	8.61
410	2078	48.5	6.0	6.5	135	64.1	29051	2066	9.6	9.7	885	854	40.8	39.1	38.9	1731	11817	26	1.4	71.63	678.9	.321	1.36	1.11	8.5	9.9	8.51
427	2079	12.2	5.1	6.2	133	53.9	28581	2067	9.6	9.7	879	807	40.2	39.0	38.9	1951	12817	27	1.6	171.9	664.2	.351	1.45	1.02	6.4	9.9	8.51
428	2080	17.9	4.9	5.5	134	55.8	28641	2068	9.6	9.7	883	850	40.6	39.0	38.9	1881	13001	28	1.6	139.4	642.6	.361	1.44	1.09	6.6	9.9	8.51
430	2081	30.2	5.3	6.5	134	59.0	29041	2059	9.6	9.7	801	856	40.6	38.9	39.0	1971	13256	29	1.6	68.88	622.4	.351	1.28	1.09	10.3	9.9	8.51
434	2082	18.4	5.2	6.3	108	49.4	27881	2071	9.6	9.6	891	857	40.8	36.5	39.1	1521	13760	30	1.7	110.1	605.2	.381	1.39	1.08	7.7	9.9	8.51
437	2083	14.9	5.1	5.7	134	49.3	27961	2071	9.6	9.6	864	857	40.5	38.8	39.2	1971	14240	31	1.7	134.6	588.9	.391	1.44	1.09	6.5	9.9	8.51
441	2084	14.0	5.4	5.5	134	60.5	28031	2073	9.5	9.6	879	857	40.8	38.9	39.2	2051	14639	32	1.8	110.1	574.4	.401	1.39	1.10	7.6	9.9	8.51
444	2085	18.2	5.7	6.6	114	70.1	27711	2074	9.5	9.6	889	857	40.9	39.1	39.3	1991	15048	33	1.8	110.1	560.8	.411	1.36	1.07	8.2	9.9	8.51
449	2086	13.0	5.3	6.6	90	56.5	28721	2075	9.5	9.6	899	857	41.2	39.5	39.7	2001	15505	34	1.9	156.3	548.5	.421	1.44	1.10	6.7	9.9	8.61
256	2087	9.7	4.6	6.3	112	54.4	29051	2078	9.5	9.6	903	858	41.7	39.4	40.0	1781	16299	35	2.0	220.0	540.6	.451	1.53	1.07	5.1	9.9	8.61
258	2088	14.1	5.2	5.8	106	51.8	28881	2078	9.5	9.6	904	854	41.5	39.4	40.4	1841	16470	36	2.1	149.9	547.1	.451	1.43	1.12	6.9	9.9	8.41
301	2089	21.5	5.2	6.5	94	60.2	29271	2079	9.5	9.6	907	858	42.1	39.5	40.4	1831	16238	37	2.1	92.96	515.4	.461	1.31	1.10	9.4	9.9	8.51
303	2090	40.4	6.1	6.7	93	72.5	29471	2079	9.5	9.6	910	858	42.2	39.6	40.4	1901	17044	38	2.2	103.4	504.0	.471	1.40	1.13	8.0	9.9	8.51
309	2091	13.4	5.2	6.8	134	55.1	28991	2081	9.6	9.6	906	859	42.4	40.3	40.7	1911	17729	39	2.3	150.7	496.0	.481	1.48	1.10	6.0	9.8	8.61
348	2093	11.3	5.2	5.9	134	42.6	26581	2084	9.6	9.6	877	823	41.6	40.0	40.5	1901	19020	41	2.4	202.9	482.0	.521	1.37	1.11	8.2	9.8	8.51
328	2093	12.4	4.8	4.7	133	44.3	26841	2034	9.6	9.6	881	824	41.6	39.9	40.5	2001	19028	41	2.4	171.2	479.9	.521	1.34	1.09	8.1	9.8	8.51
330	2094	46.9	5.2	5.6	153	53.5	28631	2034	9.6	9.6	897	853	41.4	39.7	40.5	2051	19252	42	2.5	44.14	470.6	.531	1.10	1.10	14.5	9.8	8.51
333	2095	22.8	5.1	6.2	151	49.9	28601	2085	9.5	9.6	888	858	41.7	39.7	40.5	2031	19798	43	2.5	89.70	461.5	.541	1.35	1.09	8.3	9.8	8.51
336	2096	18.2	5.0	5.8	155	41.7	28231	2086	9.5	9.6	888	858	41.2	39.8	40.5	1931	20176	44	2.6	113.8	453.1	.551	1.41	1.10	7.5	9.8	8.51
338	2097	23.9	5.3	5.7	154	48.3	27921	2086	9.5	9.6	901	858	41.2	40.0	40.6	2021	20464	45	2.6	91.25	446.0	.561	1.37	1.09	8.3	9.8	8.51
341	2098	27.2	5.1	6.6	153	52.3	26551	2087	9.5	9.6	897	858	42.0	39.8	40.6	2121	20883	46	2.6	73.68	437.2	.571	1.33	1.07	9.3	9.8	8.51
343	2099	20.8	5.7	6.4	104	54.2	28721	2057	9.5	9.6	909	858	41.8	39.8	40.6	2021	21232	47	2.7	100.1	429.9	.581	1.37	1.07	8.3	9.8	8.51
346	2100	23.7	5.3	6.1	143	49.5	26781	2088	9.5	9.6	912	858	41.8	40.2	40.7	2071	21544	48	2.7	88.08	422.5	.591	1.27	1.07	10.7	9.8	8.51
348	2101	47.9	5.1	6.1	153	55.2	27831	2089	9.5	9.6	901	858	41.5	40.2	40.9	2051	21885	49	2.8	76.89	415.9	.601	1.32	1.07	9.4	9.8	8.51
350	2102	47.8	5.5	5.6	154	48.8	29211	2089	9.5	9.6	912	858	42.0	40.0	40.9	2051	22165	50	2.8	76.06	409.4	.611	1.32	1.05	9.5	9.9	8.51
352	2103	31.3	5.3	6.0	154	52.1	28411	2090	9.5	9.6	883	858	42.1	40.3	41.1	2031	22455	51	2.8	63.90	402.2	.611	1.28	1.05	10.0	9.9	8.51
354	2104	32.2																									

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 9:43 12/20/78

TIME	DEPTH	HOP	TORQUE	RPM	BIT	PUMP1	RTNS	LB/GAL	GAL/MIN	TEMP(C)	PVT	THIS BIT	EST	DXC	NXB	NP	ECD	NXMWI			
M/H	INST	MAX	WT	PSI	DEPTH	IN	OUT	IN	OUT	LAG	REVS	MT	HRS	CPMI	CPMB	TW					
421	2111	26.8	5.4	5.8	153	71.6	2887	2096	9.5	9.6	893	858	42.1	40.8	41.8	207	25624	59	3.2	87.89	360.8
422	2112	30.1	5.5	6.2	109	77.0	2880	2097	9.5	9.6	878	859	42.5	40.7	41.6	207	25860	60	3.2	68.12	356.1
426	2113	26.4	5.3	6.2	154	62.5	2910	2098	9.5	9.6	900	859	42.3	40.6	41.6	212	26336	61	3.3	79.34	351.2
428	2114	24.1	5.4	6.1	153	60.3	2908	2099	9.6	9.6	893	859	42.1	40.7	41.5	215	26753	62	3.3	91.65	347.7
430	2115	24.5	5.1	5.5	153	65.8	2900	2100	9.5	9.6	889	859	42.1	40.8	41.5	212	27018	63	3.3	83.33	343.1
432	2116	32.4	5.7	6.3	153	74.0	2865	2101	9.5	9.5	909	856	42.7	40.8	41.5	224	27360	64	3.4	68.63	338.6
435	2117	22.3	5.1	6.2	155	52.0	2863	2102	9.5	9.5	910	857	42.6	40.7	41.5	207	27763	65	3.4	91.52	334.5
502	2119	7.1	5.9	7.1	131	56.7	2551	2110	9.5	9.5	837	848	43.2	41.9	41.9	217	29648	66	3.7	279.1	338.2
504	2119	9.8	4.9	5.8	139	54.2	2439	2110	9.5	9.5	825	854	43.4	41.7	41.8	214	29870	67	3.8	225.3	335.2
505	2120	40.2	4.9	5.6	138	45.5	2452	2111	9.5	9.5	836	856	43.4	41.6	41.8	200	30047	68	3.8	49.76	330.7
507	2121	32.2	5.3	5.5	138	47.5	2526	2112	9.5	9.5	838	856	43.7	41.6	41.9	207	30343	69	3.8	61.95	327.0
511	2122	21.9	5.1	5.9	112	56.8	2576	2113	9.5	9.5	848	856	43.6	41.5	41.9	218	30776	70	3.9	93.28	324.1
514	2123	20.8	4.7	5.6	143	53.4	2530	2114	9.5	9.5	837	858	43.6	41.4	41.9	228	31227	71	3.9	96.29	321.2
518	2124	17.3	4.8	6.4	145	47.4	2528	2116	9.5	9.5	844	859	43.6	41.4	41.9	222	31766	72	4.0	116.4	318.4
522	2125	17.4	5.3	5.5	123	57.2	2582	2117	9.5	9.5	851	859	43.4	41.3	42.1	219	32304	73	4.1	117.1	315.9
532	2126	10.6	4.6	6.4	143	46.6	2511	2118	9.5	9.5	825	859	43.8	41.9	42.3	229	33646	74	4.2	189.1	316.5
534	2127	12.5	4.9	5.3	145	51.1	2521	2118	9.5	9.5	849	859	43.8	41.9	42.3	224	33873	75	4.3	165.5	313.3
536	2128	19.0	5.0	5.4	145	54.3	2828	2118	9.5	9.5	883	859	43.4	41.9	42.3	213	34153	76	4.3	105.4	310.0
539	2129	27.3	5.0	5.7	140	54.1	2805	2118	9.5	9.5	899	859	43.8	41.8	42.3	230	34546	77	4.3	73.26	307.0
541	2130	25.8	5.3	6.1	121	52.4	2917	2118	9.5	9.5	891	859	43.8	41.8	42.3	234	34816	78	4.4	79.76	304.4
544	2131	21.2	4.3	6.0	155	46.1	1400	2119	9.5	9.5	603	858	43.5	41.7	42.4	233	35267	79	4.4	96.77	302.1
614	2132	17.3	5.0	6.1	123	45.9	1152	2123	9.5	9.5	516	503	42.2	41.2	43.0	258	35661	80	4.5	115.7	301.0
617	2133	15.8	5.2	6.0	126	46.1	1149	2124	9.5	9.5	516	517	42.2	41.3	43.1	260	36131	81	4.6	126.6	298.8
620	2134	18.2	5.5	6.2	124	56.4	1137	2124	9.5	9.5	517	502	41.6	41.3	43.1	260	36484	82	4.7	114.3	296.5
624	2135	18.8	5.2	6.0	126	52.3	1131	2125	9.5	9.5	518	501	41.6	41.3	43.2	267	36905	83	4.7	106.4	294.1
628	2136	17.7	4.7	6.1	127	41.9	1128	2125	9.5	9.5	518	509	41.7	41.3	43.2	263	37409	84	4.8	113.1	292.3
633	2137	14.9	5.3	5.8	118	44.4	1138	2126	9.5	9.5	517	514	41.7	41.3	43.4	271	38038	85	4.9	134.2	290.7
637	2138	13.6	4.8	5.4	126	41.9	1132	2126	9.5	9.5	518	508	41.4	41.3	43.4	277	38565	86	4.9	147.2	289.2
640	2139	14.7	4.9	5.2	125	53.0	1189	2126	9.5	9.5	507	519	41.1	41.3	43.4	294	38916	87	5.0	136.4	287.0
644	2140	15.7	5.3	6.0	128	58.0	1163	2126	9.5	9.5	516	517	41.1	41.3	43.4	279	39399	88	5.0	128.0	285.3
ONLY ONE PUMP ON THE HOLE FROM 2130 METRES.																					
648	2141	15.9	5.4	6.4	125	45.9	1169	2127	9.5	9.5	516	502	41.5	41.3	43.4	282	39876	89	5.1	125.7	283.7
651	2142	17.1	5.5	5.7	127	57.5	1177	2128	9.5	9.5	514	505	41.5	41.3	43.4	289	40228	90	5.2	118.0	281.7
654	2143	16.4	5.3	6.2	127	60.6	1177	2129	9.5	9.5	507	511	41.1	41.3	43.5	294	40648	91	5.2	126.7	280.2
659	2144	16.6	4.5	6.1	125	44.7	1167	2130	9.5	9.5	517	515	41.1	41.3	43.5	298	41242	92	5.3	120.5	278.6
740	2145	12.9	4.8	5.6	108	47.7	1186	2136	9.6	9.5	515	591	42.1	41.5	43.2	305	42423	93	5.5	161.5	280.6
742	2146	14.6	6.1	6.0	108	62.8	1198	2137	9.6	9.5	505	590	42.0	41.5	42.7	313	42595	94	5.5	141.4	278.2
744	2147	24.2	5.4	6.9	98	58.2	1205	2137	9.6	9.5	514	577	41.9	36.8	42.7	306	42831	95	5.6	82.62	275.9
750	2148	17.8	4.8	7.1	134	49.5	1207	2139	9.6	9.5	514	581	41.6	39.7	42.2	268	43534	96	5.7	113.4	275.1
752	2149	17.9	5.1	6.7	134	44.2	1181	2139	9.6	9.5	516	577	41.3	39.6	42.2	270	43822	97	5.7	112.0	273.1
756	2150	16.1	4.5	5.3	134	47.9	1211	2140	9.5	9.5	506	569	41.0	39.5	41.9	261	44374	98	5.8	125.3	271.8
759	2151	16.9	4.9	5.7	133	49.9	1200	2141	9.5	9.5	516	568	41.2	39.4	41.9	267	44817	99	5.8	120.4	270.4
802	2152	19.8	5.2	5.6	134	49.3	1206	2142	9.5	9.4	514	563	40.9	39.4	41.7	273	45159	100	5.9	105.4	268.5
805	2154	17.9	4.7	6.0	133	47.8	1207	2143	9.6	9.4	507	566	40.8	39.4	41.7	280	45646	101	5.9	113.4	267.0
808	2155	20.0	5.6	5.8	135	56.1	1197	2144	9.6	9.4	515	568	41.2	39.4	41.6	280	46014	102	6.0	102.1	265.3
811	2156	20.8	5.2	6.8	135	59.3	1205	2144	9.5	9.4	505	563	40.9	39.1	41.6	282	46347	103	6.0	96.06	263.6
815	2157	20.1	4.6	6.0	134	46.3	1224	2145	9.6	9.4	506	567	40.6	39.0	41.4	287	46912	104	6.1	99.76	262.4
817	2158	19.3	5.5	6.2	134	51.1	1203	2145	9.6	9.4	507	562	40.9	38.9	41.3	289	47253	105	6.1	105.5	261.0
833	2159	12.9	5.1	5.9	135	50.7	1199	2145	9.6	9.4	492	524	40.3	38.9	41.2	299	48375	106	6.3	156.0	261.2
834	2160	14.7	5.0	5.5	134	47.3	1172	2145	9.6	9.4	498	523	40.3	38.9	41.2	302					

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 9:53 12/20/78

TIME	DEPTH	HOP	TORQUE	RPM	BIT	PUMP	RTNS	LB/GAL	GAL/MIN	TEMP(C)	PVT	REVS	MT	THIS BIT	EST	DXC	MGB	SP	EDC	NMMW							
																MIN	MAX	WT	PSI	DEPTH	IN	OUT	IN	OUT	LAG	REV	HR
1134	2160	14.7	5.0	5.5	134	47.3	1172	2145	9.6	9.4	498	523	40.3	38.9	41.2	302	48595	107	6.3	137.1	259.3	1.33	1.41	1.13	6.8	9.9	8.5
1136	2160	19.3	5.0	5.6	134	48.7	1152	2145	9.6	9.4	499	524	40.5	38.9	41.2	295	48844	108	6.3	116.0	257.8	1.33	1.39	1.15	7.4	9.9	8.6
1140	2162	23.2	5.4	6.3	135	55.7	1158	2145	9.6	9.4	498	523	40.4	38.9	41.2	311	49327	109	6.4	87.93	256.4	1.35	1.36	1.15	8.0	9.9	8.5
1143	2163	21.5	5.6	6.6	134	52.3	1179	2145	9.6	9.4	498	520	40.0	38.8	41.2	306	49722	110	6.5	93.15	255.1	1.36	1.35	1.14	8.1	9.9	8.5
1147	2164	18.1	5.3	5.9	122	53.9	1178	2145	9.6	9.4	501	519	39.8	38.8	41.0	318	50215	111	6.5	115.2	254.1	1.37	1.36	1.12	7.7	9.9	8.4
1148	2165	20.8	5.1	5.8	135	62.1	1201	2145	9.6	9.4	493	512	40.2	38.8	41.0	313	50425	112	6.5	97.21	252.2	1.38	1.33	1.14	8.4	9.9	8.4
1151	2166	21.1	5.8	6.3	135	62.8	1161	2145	9.6	9.4	498	518	40.0	38.8	41.2	318	50850	113	6.6	97.15	251.0	1.39	1.38	1.14	7.6	9.9	8.5
1155	2167	20.4	5.3	6.1	134	49.1	1192	2146	9.6	9.4	499	514	39.6	38.8	41.2	311	51274	114	6.7	103.1	248.7	1.41	1.36	1.12	7.9	9.9	8.6
1158	2168	18.7	4.8	5.7	135	43.9	1191	2147	9.6	9.4	498	514	39.5	38.8	41.1	309	51753	115	6.7	109.1	248.7	1.41	1.36	1.12	7.9	9.9	8.6
1161	2168	18.9	5.5	5.7	136	55.2	1171	2148	9.6	9.4	499	515	39.6	38.8	41.1	317	52150	116	6.8	107.0	247.4	1.43	1.36	1.12	7.8	9.9	8.5
1164	2170	19.9	5.2	5.9	134	46.7	1154	2149	9.6	9.4	498	510	39.6	38.8	41.4	318	52527	117	6.8	102.6	246.2	1.44	1.32	1.13	8.6	9.9	8.5
1168	2171	18.7	4.8	5.5	133	52.4	1199	2150	9.6	9.4	492	506	39.5	38.8	41.4	316	53002	118	6.9	107.1	245.2	1.45	1.35	1.12	7.9	9.9	8.6
1173	2173	13.2	5.1	5.5	126	48.3	1138	2158	9.6	9.4	498	507	39.1	37.3	41.0	330	56916	130	7.0	150.9	246.1	1.56	1.41	1.09	6.8	9.9	8.4
1175	2185	5.9	4.4	6.6	60	37.7	619	2160	9.6	9.4	285	352	39.0	37.1	40.9	328	57676	132	7.1	337.9	222.6	1.58	1.56	1.03	4.3	10.0	8.5
1177	2190	19.8	-5.0	6.3	145	51.7	2894	2167	9.6	9.4	872	645	39.8	38.0	40.6	294	59030	134	7.3	105.0	225.5	1.61	1.39	1.14	6.9	9.9	8.5
1184	2195	17.1	3.8	6.8	148	35.0	2666	2171	9.6	9.4	842	644	41.5	39.2	39.2	270	63176	146	7.8	131.2	229.7	1.73	1.30	1.07	8.0	9.9	8.5
1192	2206	30.8	5.4	7.0	153	50.6	2877	2171	9.6	9.4	867	646	41.4	39.6	38.8	263	65207	154	8.0	64.34	204.7	1.78	1.30	1.05	9.9	10.0	8.5
1193	2207	33.6	5.4	5.6	153	61.6	2832	2171	9.6	9.4	866	647	41.2	39.6	38.8	270	65291	155	8.0	60.02	204.2	1.78	1.27	1.05	10.7	10.0	8.5
1194	2208	36.0	5.9	6.6	107	50.3	2786	2171	9.6	9.4	861	644	41.2	39.5	38.8	282	65509	156	8.1	56.86	203.3	1.79	1.21	1.02	12.0	10.0	8.4
1196	2209	34.7	4.8	6.5	152	49.5	2801	2171	9.6	9.4	861	642	41.8	39.5	38.9	287	65822	157	8.1	59.18	202.5	1.80	1.23	1.03	11.4	10.0	8.4
1197	2210	21.1	4.8	6.0	152	55.4	2825	2171	9.6	9.4	865	646	41.8	39.5	39.2	290	66544	158	8.2	95.85	202.3	1.82	1.32	1.03	9.1	10.0	8.5
1198	2211	20.7	5.0	5.7	151	52.2	2806	2171	9.6	9.4	850	646	41.6	39.6	39.4	282	66802	159	8.2	97.63	201.4	1.83	1.36	1.04	8.6	10.1	8.5
1200	2212	18.3	5.6	5.9	151	58.9	2802	2171	9.7	9.4	828	566	41.5	39.4	39.8	296	67427	160	8.3	112.1	201.2	1.84	1.23	1.03	10.9	10.1	8.5
1201	2213	27.8	5.5	5.7	152	54.7	2809	2171	9.6	9.4	864	622	41.6	39.3	39.8	297	67559	161	8.3	72.52	200.2	1.85	1.23	1.03	11.4	10.1	8.5
1202	2214	32.0	5.5	5.9	153	53.4	2819	2171	9.6	9.4	859	636	41.3	39.3	39.8	302	67710	162	8.3	62.54	199.1	1.85	1.23	1.02	11.1	10.1	8.5
1203	2215	27.4	4.8	6.0	43	57.6	2808	2171	9.7	9.4	853	632	41.3	39.9	40.3	306	68023	163	8.4	72.73	198.9	1.86	.95	.71	18.3	10.1	8.4
REPAIR HISTORY TABLE.																											
1145	2216	22.3	5.4	6.9	145	49.7	2840	1041	9.6	9.7	858	641	42.4	42.3	42.3	395	68501	164	8.5	90.92	198.7	1.87	.85	.76	19.6	15.4	8.5
1148	2217	16.9	5.6	6.2	146	57.1	2830	1158	9.7	10.3	878	643	42.8	42.3	42.3	400	69007	165	8.5	118.8	198.2	1.89	.95	.67	16.9	14.9	8.4
1151	2218	19.1	4.7	5.6	146	50.1	2345	2215	9.7	8.9	764	643	42.2	42.3	42.4	412	69368	166	8.6	109.8	197.6	1.90	1.40	1.07	8.1	9.9	8.5
1152	2219	25.2	4.8	5.4	147	49.7	1771	2215	9.7	8.2	669	634	42.0	42.3	42.4	412	69536	167	8.6	79.35	196.6	1.90	1.30	1.07	9.6	9.9	8.5
1153	2220	34.1	5.1	6.4	145	55.0	2806	2215	9.7	8.3	838	626	42.1	42.3	42.4	419	69764	168	8.6	58.64	195.7	1.91	1.23	1.07	11.4	9.9	8.5
1155	2221	39.0	5.1	5.9	146	52.9	2887	2216	9.7	8.9	876	643	41.9	42.3	42.4	407	70056	169	8.6	51.28	195.0	1.91	1.21	1.05	12.3	9.9	8.5
1157	2222	32.5	5.2	5.7	146	49.9	2833	2216	9.7	9.1	871	640	42.3	42.3	42.4	412	70354	170	8.7	61.79	194.3	1.92	1.25	1.04	11.3	9.9	8.4
1159	2223	32.7	5.5	5.8	148	49.3	2841	2216	9.7	8.3	877	643	42.2	42.3	42.4	404	70574	171	8.7	61.96	193.5	1.93	1.26	1.03	11.1	10.0	8.5
1160	2224	32.5	5.4	6.2	147	66.8	2843	2216	9.8	8.5	861	645	42.2	42.3	42.4	426	70825	172	8.7	61.65	192.7	1.94	1.24	1.03	11.6	10.0	8.4
1161	2225	26.2	4.8	6.0	145	52.8	2803	2216	9.7	9.1	869	625	41.9	40.9	42.4	409	71555	173	8.8	76.98	192.9	1.96	1.28	1.02	10.6	10.0	8.4
1162	2226	26.0	4.7	5.6	145	52.9	2832	2216	9.6	8.9	861	643	41.9	39.1	42.4	425	71799	174	8.9	77.80	192.1	1.96	1.30	1.02	10.1	10.0	8.4
1167	2227	29.1	4.8	5.5	146	59.5	2845	2216	9.7	9.2	855	643	42.0	39.0	42.4	423	71933	175	8.9	78.46	191.5	1.97	1.31	1.02	10.3	10.0	8.5
1170	2228	31.4	5.3	6.5	147	55.6	2855	2217	9.7	9.0	879	642</															

MURKIN DRILLING

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 9:58 12/20/78

TIME	DEPTH	N/P	TORQUE	RPM	BIT	PUMP WT	RTNS PSI	LB/GAL IN OUT	GAL/MIN IN OUT	TEMP(C) IN OUT	LAG	PVT I	REVS	MT	THIS BIT HRS CPRI CPMB TWI	ESTI	DXC	NXB	SP	ECD	NXMW	
																	IN/H DIST MAX	WT DEPTH	IN OUT	IN OUT	LAG	REVS
1458	2239	27.9	5.5	5.8	149	55.4	2851	2224	9.5 10.1	877 616	42.3 39.4	42.2	373	76203	187	9.4 71.85	184.6 2.08	1.28	1.02	10.8	9.9	8.5
1459	2240	29.7	5.5	5.7	150	58.4	2812	2224	9.6 10.2	866 628	42.0 39.3	42.2	380	76330	188	9.4 70.61	184.0 2.09	1.28	1.01	10.8	9.9	8.5
1459	2241	58.8	5.8	6.2	150	61.3	2838	2224	9.4 10.2	879 636	42.1 39.4	42.1	375	76405	189	9.4 40.27	182.9 2.09	1.14	1.01	14.5	9.9	8.5
1501	2242	46.4	5.3	6.1	149	56.0	2824	2224	9.5 10.2	866 642	42.3 40.1	42.1	376	76757	190	9.4 45.06	182.5 2.10	1.16	.99	14.3	9.9	8.5
1503	2243	39.8	4.9	6.0	150	53.6	2833	2224	9.5 10.0	861 643	42.3 40.3	42.1	378	77006	191	9.5 49.85	181.8 2.10	1.19	.98	13.2	9.9	8.5
1506	2244	26.3	5.1	5.9	150	48.7	2840	2225	9.4 9.9	867 642	42.6 40.4	42.1	371	77393	192	9.5 76.10	181.4 2.12	1.29	.95	10.6	9.9	8.5
1508	2245	28.9	5.1	6.1	148	61.7	2854	2226	9.5 9.8	879 634	42.5 40.4	42.1	368	77678	193	9.5 70.95	180.8 2.12	1.32	1.00	10.2	9.9	8.5
1511	2246	24.1	5.4	5.7	148	59.8	2830	2228	9.5 10.0	867 642	42.6 40.5	42.2	361	78093	194	9.6 85.48	180.5 2.13	1.35	.99	9.5	9.9	8.5
1514	2247	21.4	4.5	6.2	150	49.7	2839	2229	9.4 9.8	876 644	42.7 40.5	42.0	368	78550	195	9.7 95.15	180.1 2.15	1.36	1.00	9.2	9.9	8.5
1517	2248	18.3	4.6	6.4	148	52.8	2817	2231	9.5 10.0	871 620	42.9 40.4	42.0	364	79020	196	9.7 109.9	179.7 2.16	1.42	1.01	8.0	9.8	8.5
1520	2249	24.0	5.3	6.1	149	56.7	2849	2232	9.5 9.8	872 637	43.1 40.4	41.9	366	79326	197	9.7 89.72	179.3 2.17	1.36	1.01	9.2	9.8	8.5
1525	2250	18.1	5.4	6.8	150	58.1	2846	2234	9.5 10.0	846 640	42.9 40.4	41.9	363	80007	198	9.8 110.2	179.3 2.19	1.39	1.03	8.4	9.8	8.5
1540	2251	14.4	5.4	5.7	147	53.0	2834	2237	9.5 10.0	834 609	43.2 41.1	41.9	366	80983	199	10.0 139.6	179.6 2.21	1.41	1.06	8.1	9.8	8.6
1542	2252	15.0	5.3	5.6	147	56.9	2806	2237	9.5 10.0	851 638	43.5 40.6	41.9	361	81234	200	10.0 139.1	179.1 2.22	1.47	1.05	7.2	9.8	8.4
1542	2253	20.8	5.4	5.6	148	57.9	2843	2238	9.6 10.0	853 640	43.4 40.6	41.9	361	81340	201	10.0 101.3	178.4 2.22	1.39	1.05	8.6	9.8	8.4
1544	2254	39.7	5.8	6.4	148	63.3	2833	2238	9.5 9.9	866 621	43.6 40.5	41.9	368	81561	202	10.0 56.66	177.7 2.23	1.27	1.07	11.8	9.8	8.6
1548	2255	30.4	5.0	6.4	149	55.8	2823	2241	9.6 9.7	868 641	43.5 41.1	41.9	361	82064	203	10.1 65.58	177.5 2.24	1.27	1.04	11.4	9.8	8.5
1551	2256	21.3	5.5	6.0	147	60.7	2827	2243	9.5 9.6	857 645	43.5 41.2	42.0	374	82525	204	10.1 94.93	177.2 2.26	1.37	1.04	9.2	9.8	8.5
1553	2257	22.0	4.8	5.8	148	55.0	2770	2243	9.6 9.6	855 614	43.6 41.2	42.0	380	82790	205	10.2 100.8	176.8 2.26	1.40	1.04	8.5	9.8	8.6
1555	2258	27.6	5.6	5.8	150	64.3	2829	2244	9.4 9.7	844 636	43.8 41.2	42.1	373	83084	206	10.2 80.87	176.2 2.27	1.35	1.05	9.9	9.8	8.5
1557	2259	31.7	5.5	6.3	150	59.8	2833	2245	9.6 9.8	860 644	43.5 41.3	42.1	365	83375	207	10.2 63.02	175.6 2.28	1.29	1.05	11.1	9.8	8.6
1600	2260	26.7	4.9	6.1	148	55.3	2805	2246	9.5 9.8	871 635	43.9 41.5	42.1	361	83827	208	10.3 77.76	175.3 2.29	1.33	1.03	10.1	9.8	8.6
1603	2261	20.7	5.0	6.0	124	57.6	2787	2247	9.5 9.7	855 641	43.8 41.6	42.2	378	84333	209	10.3 96.98	175.0 2.30	1.35	1.02	9.6	9.8	8.5
1605	2262	25.0	5.7	5.9	150	68.3	2797	2247	9.5 9.6	855 641	44.2 41.8	42.3	366	84507	210	10.4 84.12	174.4 2.31	1.34	1.04	10.0	9.8	8.5
1606	2263	26.4	4.7	6.4	136	48.7	2804	2248	9.5 9.8	846 641	44.2 41.5	42.3	363	84781	211	10.4 76.71	173.9 2.32	1.35	1.04	9.9	9.8	8.5
1621	2264	17.2	5.2	6.1	148	52.6	2811	2251	9.5 10.0	856 592	44.2 42.2	42.8	366	85907	212	10.5 116.7	174.3 2.35	1.38	.99	8.9	9.8	8.5
1622	2265	17.4	5.5	5.6	149	59.3	2826	2251	9.6 10.4	857 635	44.2 41.8	42.9	356	86118	213	10.6 117.8	174.1 2.35	1.37	1.03	9.0	9.8	8.5
1623	2266	20.2	5.1	5.6	147	53.6	2872	2251	9.4 10.4	840 638	44.6 41.6	42.9	354	86254	214	10.6 104.3	173.3 2.36	1.38	1.04	9.2	9.8	8.5
1624	2267	44.7	5.9	5.9	148	78.5	2860	2251	9.5 10.6	862 639	44.5 41.6	42.9	352	86402	215	10.6 57.54	172.8 2.36	1.23	1.04	13.3	9.8	8.5
1631	2268	21.0	4.4	7.1	148	56.3	2857	2253	9.5 9.8	860 640	44.5 41.9	43.0	352	87417	216	10.7 96.79	173.0 2.39	1.34	1.03	9.9	9.8	8.4
1633	2269	19.0	5.5	5.5	149	59.5	2829	2254	9.5 9.9	844 639	44.4 42.0	43.1	353	87672	217	10.7 107.3	172.5 2.40	1.40	1.04	8.7	9.8	8.5
1635	2270	19.6	4.7	5.6	149	54.4	2834	2255	9.4 9.8	860 640	44.2 42.1	43.1	352	87974	218	10.8 103.7	171.9 2.40	1.40	1.05	8.7	9.8	8.4
1637	2271	32.7	5.4	5.7	151	55.0	2808	2255	9.4 9.8	849 640	44.1 42.0	43.1	347	88227	219	10.8 61.19	171.5 2.41	1.26	1.04	11.7	9.8	8.5
1638	2272	33.3	5.0	5.5	151	49.8	2834	2256	9.5 9.9	869 640	44.4 42.0	43.1	356	88484	220	10.8 60.76	170.9 2.42	1.25	1.03	12.2	9.8	8.5
1639	2273	42.8	4.7	5.5	148	50.6	2809	2256	9.4 10.0	869 640	44.5 41.9	43.2	356	88634	221	10.8 51.60	170.4 2.42	1.21	1.02	13.3	9.8	8.5
1641	2274	44.9	5.4	6.2	153	58.1	2838	2257	9.5 10.2	870 638	44.0 41.9	43.2	356	88857	222	10.9 44.95	169.8 2.43	1.19	1.02	13.9	9.8	8.5
1643	2275	34.3	5.3	6.5	151	57.1	2839	2258	9.5 10.3	868 636	44.1 42.1	43.2	352	89256	223	10.9 58.23	169.5 2.44	1.25	.98	12.3	9.8	8.6
1645	2276	28.9	5.2	5.8	149	53.4	2820	2259	9.5 10.1	858 640	44.4 42.3	43.2	349	89555	224	11.0 69.11	169.1 2.45	1.29	.98	11.4	9.8	8.5
1651	2277	17.3	4.9	6.2	146	53.3	2813	2261	9.5 9.8	870 632	44.3 42.4	43.4	361	90379	225	11.0 115.9	169.2 2.47	1.38	1.00	9.1	9.8	8.5
1701	2278	17.7	5.3	5.8	150	49.2	2802	2264	9.4 9.9	861 632	44.4 42.5	43.6	352	90816	226	11.1 112.7	169.0 2.48	1.33	1.00	9.8	9.8	8.5
1701	2279	30.5	5.2	5.6	150	59.8	2805	2264	9.5 9.9	851 633	44.5 42.4	43.6	352	90856	227	11.1 90.96	168.3 2.48	1.28	1.00	13.5	9.8	8.4
1704	2280	35.6	5.5	6.7	142	51.0	2793	2264	9.6 10.1	849 633	44.6 42.0	43.8	361	91232	228	11.1 56.23	167.9 2.49	1.17	1.00	13.7	9.8	8.5
1707	2281	30.7	5.2	6.1	150	51.3	2757	2264														

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 10:03 12/20/78

TIME	DEPTH	ROP M/H	TORQUE INST MAX	RPM WT	BIT PUMP PSI	RTNS DEPTH	LB/GAL IN OUT	GAL/MIN IN OUT	TEMP(C) IN OUT LAG	PVT	REVS	MT	THIS BIT HRS CPMI CPMB	EST TWI	DNC	NDB	NP	ECD	NMM								
1725	2289	23.2	5.5	5.9	150	48.1	2767	2271	9.5	9.5	859	628	45.0	43.1	44.3	347	94118	237	11.5	86.24	164.7	2.57	1.28	.95	11.4	9.8	8.5
1727	2290	33.9	5.4	6.1	150	43.9	2798	2272	9.5	9.6	832	625	45.0	43.0	44.3	345	94373	238	11.5	60.81	164.3	2.58	1.17	.94	14.1	9.8	8.5
1739	2291	27.4	5.1	5.9	150	44.8	2799	2276	9.5	9.2	831	625	44.7	42.7	44.3	347	95157	239	11.6	74.10	164.3	2.60	1.20	.95	13.3	9.8	8.5
1740	2292	32.1	5.4	6.0	153	50.5	2827	2276	9.5	9.6	854	623	44.5	42.4	44.2	354	95342	240	11.6	67.55	163.9	2.61	1.19	.94	13.5	9.8	8.5
1741	2293	53.9	6.0	6.7	153	51.0	2792	2276	9.6	9.6	843	618	44.6	42.5	44.2	347	95427	241	11.6	45.55	163.2	2.61	1.10	.94	16.3	9.8	8.6
1743	2294	47.1	5.0	7.0	102	46.1	2794	2277	9.5	9.6	843	616	44.7	42.8	44.2	352	95673	242	11.7	43.25	162.9	2.61	1.11	.92	16.2	9.8	8.6
1746	2295	32.2	5.2	6.8	152	46.7	2776	2277	9.5	9.6	460	619	44.4	43.1	44.2	371	96078	243	11.7	62.29	162.7	2.63	1.17	.89	14.2	9.8	8.4
1747	2296	30.6	6.0	6.5	154	53.2	2763	2277	9.5	9.7	403	620	44.6	43.2	44.2	359	96226	244	11.7	65.40	162.1	2.63	1.24	.91	12.7	9.8	8.5
1750	2297	25.9	5.3	6.9	131	45.6	2797	2277	9.6	9.7	393	621	44.7	43.0	44.2	366	96614	245	11.8	77.86	161.9	2.64	1.24	.86	12.7	9.8	8.5
1751	2298	34.6	5.3	6.2	153	43.4	2801	2277	9.6	9.8	401	622	44.7	43.0	44.2	359	96773	246	11.8	61.85	161.5	2.64	1.21	.91	13.5	9.8	8.5
USING ONE PUMP ON THE HOLE FROM 2295 METRES.																											
1753	2299	28.9	5.1	6.7	153	40.3	2804	2278	9.5	9.6	402	620	44.8	42.9	44.2	356	97099	247	11.8	69.96	161.1	2.65	1.20	.93	13.5	9.8	8.6
1756	2300	28.6	4.9	6.3	123	45.2	2781	2279	9.5	9.6	393	615	45.0	43.0	44.2	367	97400	248	11.9	71.67	160.8	2.66	1.16	.92	14.4	9.8	8.5
1758	2301	27.2	6.1	6.2	152	41.5	2781	2279	9.6	9.7	402	613	44.9	43.2	44.2	352	97606	249	11.9	73.61	160.5	2.67	1.19	.91	13.6	9.8	8.5
1759	2302	30.5	5.3	6.5	153	33.9	2782	2280	9.5	9.6	394	615	44.8	43.3	44.2	347	97831	250	11.9	68.84	160.0	2.67	1.24	.91	12.7	9.9	8.5
1803	2303	27.7	5.5	6.4	104	44.1	2767	2280	9.6	10.0	402	616	44.7	43.0	44.2	363	98266	251	12.0	73.61	159.9	2.69	1.14	.79	15.0	9.9	8.5
1816	2304	20.5	5.2	6.0	152	36.0	2797	2283	9.5	9.4	403	627	45.4	43.4	44.3	364	99143	252	12.1	99.78	160.0	2.71	1.24	.91	12.2	9.8	8.5
1817	2305	22.3	5.5	5.9	153	39.7	2769	2283	9.5	9.5	392	637	45.2	43.1	44.4	364	99228	253	12.1	90.34	159.5	2.71	1.24	.91	12.3	9.9	8.5
1818	2306	38.2	5.4	6.0	153	42.6	2763	2283	9.6	9.7	394	631	45.2	43.0	44.4	361	99420	254	12.1	59.32	159.0	2.72	1.14	.90	15.1	9.9	8.5
1820	2307	45.0	5.3	5.9	152	42.4	2785	2284	9.5	9.6	403	621	45.4	43.4	44.4	361	99750	255	12.2	44.68	158.7	2.73	1.07	.89	17.0	9.9	8.6
1826	2308	20.5	4.3	6.5	158	35.7	2810	2285	9.5	9.6	415	622	45.4	43.6	44.5	359	100500	256	12.3	98.55	158.9	2.75	1.19	.89	13.2	9.9	8.4
1829	2309	17.0	5.2	5.7	154	33.6	2782	2286	9.5	9.4	753	627	45.2	43.5	44.5	361	100964	257	12.3	117.3	158.6	2.76	1.31	.89	10.7	9.9	8.5
1830	2310	18.6	5.4	5.8	155	39.7	2805	2286	9.5	9.4	627	627	45.3	43.7	44.5	354	101164	258	12.3	107.6	158.2	2.76	1.31	.91	10.8	9.9	8.5
1831	2311	35.8	5.1	5.7	156	41.3	2777	2286	9.5	9.3	419	628	45.4	43.6	44.5	361	101317	259	12.3	67.19	157.8	2.77	1.19	.91	14.2	9.9	8.5
1832	2312	52.0	5.2	5.7	155	44.9	2804	2286	9.6	9.4	403	630	45.4	43.4	44.5	354	101454	260	12.4	42.16	157.4	2.77	1.07	.90	17.5	9.9	8.4
1834	2313	40.2	5.1	6.3	156	41.3	2783	2286	9.5	9.5	404	621	45.5	43.6	44.5	352	101843	261	12.4	50.41	157.1	2.78	1.11	.88	16.0	9.9	8.5
1837	2314	28.0	4.9	5.7	155	36.4	2746	2287	9.5	9.4	787	620	45.8	43.2	44.5	352	102297	262	12.5	71.38	156.8	2.80	1.20	.88	13.6	9.9	8.6
1840	2315	22.9	5.1	5.7	154	44.6	2807	2288	9.6	9.2	626	617	45.6	43.7	44.4	373	102723	263	12.5	87.33	156.6	2.81	1.25	.89	12.3	9.9	8.5
1843	2316	20.6	4.8	5.8	155	33.3	2730	2289	9.4	9.6	852	624	45.6	43.5	44.4	361	103210	264	12.6	98.93	156.4	2.82	1.29	.90	11.4	9.9	8.6
USING TWO PUMPS.																											
1900	2317	17.3	4.9	5.8	153	35.1	2764	2292	9.5	9.4	842	625	45.5	42.9	44.7	361	104342	265	12.7	117.1	156.6	2.85	1.32	.92	10.8	9.9	8.5
1901	2318	20.7	5.8	5.8	153	41.8	2759	2293	9.5	9.5	862	625	45.6	43.1	44.7	356	104487	266	12.7	100.3	156.2	2.86	1.27	.91	11.7	9.9	8.4
1901	2319	28.4	5.5	5.7	152	44.2	2764	2294	9.5	9.4	862	625	45.6	43.3	44.7	366	104585	267	12.7	72.02	155.7	2.86	1.20	.92	13.7	9.9	8.5
1904	2320	38.5	5.2	6.5	154	37.4	2767	2295	9.5	9.4	863	617	45.3	43.4	44.8	356	104985	268	12.7	52.67	155.5	2.87	1.13	.89	15.7	9.9	8.5
1906	2321	37.6	5.8	6.3	153	54.4	2778	2295	9.5	9.4	849	616	45.3	43.3	44.8	361	105216	269	12.7	55.35	155.2	2.88	1.16	.90	15.2	9.9	8.5
1907	2322	30.5	6.5	6.9	155	55.1	2754	2297	9.5	9.3	852	612	45.3	43.2	44.8	361	105485	270	12.8	65.87	154.8	2.88	1.23	.90	13.3	9.9	8.5
1911	2323	25.1	5.6	6.5	154	43.2	2771	2301	9.6	9.1	863	603	45.5	43.6	44.6	371	106049	271	12.8	79.80	154.6	2.90	1.24	.90	12.6	9.8	8.5
1913	2324	24.9	5.6	6.3	155	45.8	2772	2303	9.4	9.2	865	609	45.1	43.4	44.6	371	106357	272	12.9	80.34	154.3	2.91	1.27	.91	12.2	9.8	8.4
1916	2326	22.2	5.3	6.5	125	39.1	2751	2303	9.5	9.3	864	602	45.0	43.5	44.5	364	106778	273	12.9	91.53	154.2	2.92	1.29	.91	11.8	9.8	8.5
1918	2327	26.5	6.5	7.0	157	64.5	2780	2304	9.5	9.4	853	615	45.3	43.6	44.5	378	107035	274	12.9	77.05	153.8	2.93	1.29				

2025 RELEASE UNDER E.O. 14176

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 10:08 12/20/78

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 10:12 12/20/7

TIME	DEPTH	ROP M/H	TORQUE INST MAX	RPM	BIT WT	PUMP PSI	RTNS DEPTH	LB/GAL IN OUT	GAL/MIN IN OUT	TEMP(C) IN OUT LAG	PVT REVS MT	THIS BIT HRS CPMI CPMB	EST TW	DNC	NXB	NP	ECD	NXMN									
7	2386	6.2	6.2	7.7	101	41.5	2839	2376	9.5	9.7	853	602	48.5	46.0	49.2	387	133294	334	16.8	322.2	150.8	3.64	1.47	.98	8.0	9.8	8.51
26	2387	6.6	6.3	7.4	99	20.6	2879	2380	9.6	8.9	871	624	49.7	45.8	49.6	370	135097	335	17.1	314.9	152.1	3.69	1.37	1.00	9.6	9.8	8.51
29	2388	9.3	6.5	7.0	170	32.7	2842	2381	9.5	9.3	862	639	49.5	45.8	49.5	356	135502	336	17.1	215.2	151.9	3.70	1.30	.99	11.3	9.8	8.51
33	2389	11.5	6.9	7.4	110	26.5	2865	2382	9.5	9.2	870	642	49.6	46.2	49.5	370	135968	337	17.2	178.8	151.9	3.72	1.25	.98	12.7	9.8	8.51
38	2390	13.6	5.7	7.3	138	27.9	2866	2382.	9.5	9.4	857	638	49.7	46.2	49.5	363	136565	338	17.3	153.4	152.0	3.73	1.22	.96	13.6	9.8	8.51
RUNNING TWO PUMPS																											
44	2391	12.4	6.2	7.1	98	37.8	2856	2384	9.6	9.0	840	633	49.9	46.2	49.5	370	137204	339	17.4	163.5	152.1	3.75	1.24	.98	13.1	9.8	8.51
48	2392	11.7	6.1	7.2	93	38.9	2866	2385	9.5	9.1	866	633	50.0	46.6	49.7	366	137577	340	17.5	171.9	152.0	3.76	1.26	.98	12.6	9.8	8.51
52	2393	13.5	7.1	7.6	90	35.3	2874	2385	9.5	9.1	852	663	49.5	46.6	49.5	363	137960	341	17.5	147.7	152.0	3.77	1.22	.99	13.4	9.8	8.51
55	2394	16.1	6.5	7.4	90	35.3	2838	2386	9.5	9.1	863	680	49.3	47.0	49.3	368	138300	342	17.6	123.9	151.9	3.78	1.19	.96	14.5	9.8	8.51
59	2395	16.5	5.4	7.4	105	33.4	2872	2386	9.5	8.7	853	677	50.0	46.8	49.1	370	138664	343	17.6	122.9	151.8	3.79	1.18	.96	14.8	9.8	8.61
113	2396	10.7	5.8	7.5	102	28.7	2809	2387	9.5	9.4	850	698	49.9	47.0	48.9	373	139631	344	17.8	187.4	152.2	3.82	1.20	.95	13.8	9.8	8.51
116	2397	11.8	6.0	7.4	101	31.7	2773	2387	9.5	8.6	859	884	49.6	46.1	48.7	370	139936	345	17.8	173.1	152.1	3.82	1.24	.95	13.2	9.8	8.61
121	2398	11.7	5.4	7.7	44	37.4	2793	2388	9.6	9.2	860	904	49.4	46.8	48.7	369	140350	346	17.9	173.6	152.1	3.84	1.24	.95	13.3	9.8	8.41
126	2399	13.2	7.1	7.8	83	25.8	2822	2389	9.5	9.5	874	863	49.6	47.4	48.8	382	140803	347	18.0	152.5	152.3	3.85	1.21	.95	14.0	9.8	8.51
131	2400	11.9	6.0	7.7	86	45.6	2833	2390	9.5	9.2	854	867	49.7	47.3	49.0	378	141227	348	18.1	172.6	152.3	3.86	1.27	.95	12.7	9.8	8.51
136	2401	12.2	6.4	7.4	90	49.2	2853	2391	9.5	9.4	881	861	49.5	46.9	49.2	383	141599	349	18.2	167.1	152.3	3.87	1.26	.95	13.0	9.8	8.51
141	2402	12.1	5.7	7.5	92	31.1	2842	2392	9.4	9.5	872	871	49.6	47.1	49.4	380	142085	350	18.3	166.4	152.4	3.88	1.24	.94	13.2	9.8	8.51
147	2403	11.9	7.1	7.6	85	33.6	2835	2394	9.5	9.7	880	871	49.7	46.8	49.5	378	142524	351	18.3	167.5	152.5	3.89	1.24	.93	13.4	9.8	8.41
153	2404	11.2	7.4	7.6	86	33.8	2780	2395	9.5	9.7	881	870	50.1	46.5	49.7	390	143077	352	18.4	184.3	152.7	3.91	1.26	.94	12.7	9.8	8.51
157	2405	11.6	5.9	7.5	84	39.1	2782	2395	9.5	9.6	877	872	50.3	46.9	49.7	396	143455	353	18.5	173.9	152.6	3.92	1.27	.95	12.7	9.8	8.51
202	2406	11.7	6.1	7.5	66	31.1	2794	2396	9.7	9.5	865	871	49.9	47.4	49.5	397	143839	354	18.6	174.4	152.7	3.93	1.24	.93	13.4	9.8	8.51
209	2407	10.4	6.9	7.6	57	40.0	2838	2398	9.7	9.4	868	864	49.9	47.4	49.6	409	144329	355	18.7	192.3	153.0	3.94	1.29	.96	11.9	9.8	8.51
217	2408	8.2	6.9	7.3	91	34.1	2865	2399	9.6	10.0	874	861	49.9	47.4	49.9	418	145002	356	18.8	260.2	153.3	3.96	1.35	.96	10.7	9.8	8.61
235	2409	6.3	10.7	10.7	119	49.4	2913	2402	9.5	10.1	755	798	49.8	47.1	49.5	416	146366	357	19.1	315.3	154.1	4.00	1.58	1.01	6.7	9.8	8.61
CORE #2, CHRIS C20, SIZE: 8 15/32"																											
213	2410	3.7	3.0	3.8	41	10.2	15661	2406	9.6	9.5	296	66	40.8	38.2	49.7	394	2341	1	0	542.3	37906	.001	1.45	.53	13.7	9.8	8.51
232	2410	2.8	2.7	4.1	43	16.8	16721	2407	9.6	9.4	546	540	39.1	34.5	49.9	390	3138	1	3	745.2	14353	.001	1.28	.54	15.6	9.9	8.61
PUMP NO 2 ON RISEN ONLY																											
306	2411	2.9	2.6	3.9	88	16.0	15301	2408	9.6	9.4	293	538	36.2	33.5	50.0	399	5837	2	9	713.6	9032	.001	1.53	.54	12.1	9.9	8.51

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 10:19 12/20/78

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 10:24 12/20/78

TIME	DEPTH	NOP	TORQUE	RPM	BIT	PUMP ¹	RTNS	LB/GAL	GAL/MIN	TEMP(C)	PWT	THIS BIT	EST	DXC	NXB	SP	ECD	NXMW									
M/H	DIST	MAX	WT	PSI	DEPTH	IN	OUT	IN	OUT	IN	LAG	REVS	MT	HRS	CPMI	CPMB	TW										
717	2448	4.1	3.2	5.5	85	24.7	1473	2440	9.4	9.9	284	319	42.4	41.3	42.7	410	5170	8	1.0	499.2	3319	.00	1.48	.87	14.4	9.8	8.7
728	2449	5.3	3.5	5.1	82	18.1	1594	2440	9.4	10.0	284	135	42.1	40.8	43.0	403	6109	9	1.2	389.0	2986	.00	1.44	.86	15.5	9.8	8.7
741	2450	4.2	3.5	5.0	84	25.0	1555	2440	9.4	9.6	283	261	41.8	40.9	43.2	410	7187	10	1.4	517.8	2727	.00	1.54	.86	13.3	9.8	8.6
803	2451	2.4	4.8	6.0	66	25.9	1474	2440	9.6	9.8	295	228	41.1	40.5	43.8	396	9057	11	1.8	962.6	2554	.00	1.57	.81	11.9	9.8	8.4
816	2452	5.6	4.1	6.9	85	25.6	1528	2440	9.5	10.0	291	331	41.0	40.6	44.1	389	10025	12	2.0	354.4	2373	.00	1.38	.88	16.1	9.8	8.6
850	2453	1.1	3.9	7.1	85	29.2	1490	2441	9.5	9.9	295	184	40.6	40.6	44.6	382	12752	13	2.6	1853	2266	.00	1.80	.88	7.5	9.9	8.5
913	2454	2.8	3.7	5.5	87	28.2	1511	2445	9.5	10.5	284	237	40.1	40.3	45.3	377	14701	14	3.0	771.7	2168	.00	1.57	.86	12.0	9.8	8.4
937	2455	2.6	3.0	5.0	86	27.6	1505	2448	9.4	10.7	292	265	40.0	40.5	44.4	387	16688	15	3.4	835.4	2075	.01	1.57	.86	11.8	9.8	8.5
POOH AT 2456 METERS, CORED 16 METERS, RECOVERED 11.4 METERS 718.																											
C887 CHRIS C22, START DEPTH 2456 METERS CIRCULATE BOTTOMS UP PRIOR TO CORING.																											
1948	2457	3.4	3.4	5.3	101	21.8	1596	2450	9.6	9.5	279	753	44.6	39.7	42.7	434	19450	17	3.9	640.1	1888	.01	1.58	.90	12.4	9.8	8.6
1957	2458	11.6	3.4	5.1	99	21.7	1648	2450	9.7	9.5	283	731	42.4	40.4	42.3	436	20406	18	4.0	345.5	1809	.01	1.37	.78	21.8	9.8	8.7
2004	2459	5.3	3.6	7.0	100	20.5	1723	2451	9.7	9.5	282	753	41.4	40.7	42.3	434	21128	19	4.1	373.4	1717	.01	1.42	.82	16.2	9.8	8.7
2016	2460	4.0	3.6	5.6	98	24.2	1653	2452	9.7	9.4	283	469	40.9	40.2	41.9	458	22261	20	4.3	513.2	1655	.01	1.46	.86	14.8	9.8	8.4
2026	2461	6.1	3.8	5.3	104	19.1	1510	2452	9.6	9.5	284	497	40.1	39.1	41.6	458	23365	21	4.5	395.7	1595	.01	1.43	.83	16.2	9.8	8.5
2035	2462	8.1	4.1	5.8	102	24.0	1667	2453	9.7	9.7	283	471	39.8	40.9	41.3	458	24225	22	4.6	256.2	1533	.01	1.33	.89	18.7	9.8	8.6
2050	2463	4.9	3.4	6.9	101	16.1	1617	2453	9.5	9.6	283	459	39.6	40.6	41.1	461	25693	23	4.9	421.4	1486	.01	1.49	.85	14.8	9.9	8.7
2101	2464	5.9	3.4	4.9	103	25.0	1514	2453	9.7	9.9	284	490	39.4	40.2	40.9	472	26910	24	5.1	339.5	1440	.01	1.40	.86	16.5	9.9	8.7
2116	2465	4.1	3.4	4.5	101	19.8	1486	2454	9.7	9.7	264	421	39.3	39.7	40.9	477	28445	25	5.3	493.2	1402	.01	1.46	.86	14.6	9.9	8.6
2129	2466	5.6	3.6	4.7	103	20.9	1529	2454	9.6	9.5	255	753	38.9	37.4	40.7	436	29809	26	5.6	356.7	1365	.01	1.41	.89	16.2	9.9	8.5
2141	2467	7.7	4.0	5.9	103	22.2	1605	2455	9.7	9.4	276	775	37.8	37.2	40.4	439	31015	27	5.7	302.9	1329	.01	1.32	.86	19.3	9.9	8.5
2150	2468	7.6	3.4	4.7	102	13.1	1512	2455	9.5	9.3	280	457	37.4	37.0	40.1	451	31883	28	5.9	296.7	1293	.01	1.31	.86	18.6	9.9	8.4
2204	2470	10.6	4.8	6.0	89	21.0	1152	2455	9.7	9.8	241	405	36.8	38.3	40.0	438	33395	30	6.1	189.1	1223	.01	1.17	.83	21.6	9.9	8.4
POOH AT 2470 METERS, CORED 14 METERS, RECOVERED 9 METERS 64t.																											
C888 CHRIS C22, START DEPTH 2470 METERS, CIRCULATE BOTTOMS UP PRIOR TO CORING.																											
748	2470	3.7	6.3	6.4	38	19.0	1456	2470	9.7	9.5	147	181	45.4	44.7	45.4	446	33555	30	6.1	6610	1213	.15	1.30	1.07	2.5	9.9	8.9
805	2471	4.1	4.1	8.6	68	15.3	994	2470	9.7	9.5	147	156	44.7	43.2	45.4	441	34625	33	6.4	4365	1228	.15	1.29	.96	5.4	9.9	9.9
806	2473	3.4	4.8	4.8	71	17.3	1020	2470	9.7	9.5	147	53	44.8	43.2	45.4	441	34652	33	6.4	2440	1128	.15	1.31	.96	6.8	9.8	9.9
815	2474	6.4	4.3	7.1	63	23.2	1243	2470	9.7	9.5	210	171	43.9	42.7	45.4	448	35264	34	6.6	314.4	1104	.15	1.26	1.13	18.5	10.0	8.4
820	2474	4.0	3.7	5.2	63	21.7	1197	2470	9.7	9.6	208	92	43.6	42.4	45.4	450	35603	34	6.6	498.9	1112	.15	1.37	1.10	16.3	10.0	8.6
822	2475	3.7	3.4	3.8	62	17.7	1356	2470	9.7	9.7	208	455	43.7	42.3	45.4	455	35721	34	6.7	535.3	1112	.15	1.40	1.12	15.2	10.0	8.5
837	2475	4.1	3.3	5.0	61	23.4	1712	2470	9.7	9.8	285	322	42.9	41.9	45.4	458	36620	35	6.9	510.3	1094	.15	1.36	1.09	16.2	10.0	8.7
854	2476	3.5	2.9	4.8	60	16.4	1537	2470	9.8	9.8	285	515	42.2	41.9	45.4	460	37633	36	7.2	569.7	1079	.16	1.40	1.07	14.9	10.0	8.8
913	2477	2.9	2.7	3.7	60	21.5	1701	2470	9.7	9.8	285	814	41.8	41.8	45.4	441	38824	37	7.5	722.2	1067	.16	1.47	1.08	13.7	10.0	8.8
932	2478	2.6	3.0	3.8	104	25.3	1845	2470	9.7	9.4	272	595	40.2	38.6	45.4	450	40629	38	7.8	820.7	1056	.16	1.63	1.08	11.7	10.0	8.8
940	2479	8.6	3.5	4.7	103	20.1	1603	2470	9.8	9.4	-1	659	39.5	38.1	45.4	460	41396	39	8.0	247.2	1036	.16	1.34	1.07	18.8	10.0	8.9
959	2480	2.0	3.0	4.6	104	19.1	1601	2470	9.7	9.4	281	482	38.7	37.3	45.4	460	43344	40	8.3	1078	1026	.16	1.71	1.06	9.6	10.0	9.0
POOH AT 2480 METERS WITH CORE NO 8, CORED 10 METERS RECOVERED 0 METER.																											
240	2480	5.1	6.5	7.1	109	40.5	2819	2473	9.8	9.4	624	448	41.2	42.2	44.7	467	17640	2	0	386.6	12453	.01	1.47	1.16	6.8	10.1	8.6
240	2481	5.3	6.7	6.6	109	38.5	2838	2473	9.8	9.4	633	451	41.2	42.2	44.7	471	17646	2	0	377.2	12455	.01	1.47	1.17	6.8	10.1	8.6
240	2482	6.6	5.7	7.1	109	45.0	2796	2473	9.8	9.4	627	444	41.2	42.2	44.7	467	17678	2	0	301.7	11057	.01	1.44	1.18	6.7	10.1	8.5
449	2483	9.0	6.0	7.6	124	23.4	2782	2474	9.8	9.4	620	437	41.1	42.0	43.1	474	18468	3	0.2	221.9	7240	.09	1.24	1.11	11.1	10.1	8.6
DRILL TO 2480 METERS, CIRCULATE BOTTOMS UP.																											
418	2484	8.9	6.4	6.8	114	35.7	2781	2481	9.8	9.2	630	425	44.1	44.4</td													

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 10:29 12/20/78

TIME	DEPTH	ROP	TORQUE	RPM	BIT	PUMP WT	RTNS PSI	IN DEPTH	LB/GAL IN	GAL/MIN OUT	TEMP(C) IN	PVT OUT	LAG	THIS BIT	EST HRS	DXC	NXB	NP	ECD	NXW		
430	2488	22.9	6.4	7.2	104	37.7	2792	2481	9.7	9.2	641	443	43.7	43.2	42.3	455	21974	8	.4	87.21	2747	.24
433	2489	23.2	6.8	7.3	112	33.6	2793	2481	9.7	9.2	645	505	43.7	43.4	42.3	452	22221	9	.5	87.47	2465	.26
434	2490	37.7	6.7	7.4	112	32.9	2794	2481	9.8	9.2	632	520	43.8	43.4	42.8	454	22392	10	.5	56.72	2206	.28
437	2491	27.1	6.4	7.5	112	34.4	2811	2481	9.7	9.4	631	536	43.7	43.2	42.8	448	22687	11	.5	73.72	2018	.31
439	2492	21.8	6.2	7.4	109	39.2	2828	2481	9.7	9.5	647	517	43.5	42.9	43.2	462	22935	12	.6	93.27	1874	.33
443	2493	19.1	5.6	7.3	110	27.5	2807	2481	9.7	9.6	642	529	43.2	42.8	43.2	462	23290	13	.6	104.8	1720	.37
455	2494	17.7	6.0	7.4	110	31.9	2769	2481	9.8	9.7	636	534	43.0	42.2	43.8	450	23822	14	.7	122.5	1615	.39
457	2495	22.9	6.2	7.2	113	23.9	2760	2481	9.8	9.7	635	528	42.7	42.0	43.8	455	24090	15	.7	88.24	1505	.42
460	2496	27.1	6.2	7.3	111	28.9	2805	2481	9.8	9.7	631	534	42.7	41.9	44.0	441	24331	16	.8	78.58	1412	.44
501	2497	31.9	6.4	7.4	111	39.6	2828	2481	9.8	9.7	642	516	42.6	42.2	44.0	443	24531	17	.8	67.65	1340	.46
504	2498	35.7	6.6	7.5	115	44.1	2815	2481	9.8	9.7	637	508	42.4	42.4	44.1	469	24786	18	.8	55.61	1250	.48
505	2499	29.9	6.9	7.4	112	34.6	2792	2481	9.8	9.7	644	589	42.7	42.4	44.1	465	24958	19	.9	67.97	1201	.50
507	2500	38.9	6.7	7.4	124	36.3	2831	2481	9.8	9.7	639	576	42.3	42.4	44.1	455	25127	20	.9	51.44	1143	.51
508	2501	33.4	6.7	7.5	115	37.9	2808	2481	9.8	9.7	636	613	42.2	42.3	44.3	451	25333	21	.9	59.84	1096	.53
510	2502	47.7	6.6	7.4	115	36.1	2778	2481	9.8	9.7	633	568	42.4	42.2	44.3	450	25491	22	.9	41.97	1045	.54
511	2503	42.1	6.7	7.3	116	33.2	2762	2481	9.8	9.7	640	564	42.3	42.1	44.3	448	25663	23	1.0	48.54	1003	.56
513	2504	33.8	6.8	7.5	117	29.2	2814	2481	9.8	9.7	635	569	42.1	42.1	44.3	448	25890	24	1.0	60.89	962.8	.58
515	2505	28.8	6.7	7.4	115	37.9	2829	2481	9.8	9.7	641	577	42.2	42.2	44.4	452	26136	25	1.0	69.47	927.3	.60
517	2506	30.9	7.2	7.5	116	41.5	2809	2481	9.7	9.8	643	568	42.4	42.2	44.4	441	26341	26	1.1	67.85	893.9	.62
528	2507	30.1	6.9	7.5	112	36.8	2847	2481	9.8	9.8	633	561	42.1	42.0	44.4	441	26767	27	1.1	66.75	862.6	.64
529	2508	40.4	6.4	7.6	114	32.1	2838	2481	9.8	9.8	648	560	41.8	41.6	44.4	448	26946	28	1.1	55.39	838.2	.65
531	2509	30.0	7.0	7.2	116	36.0	2844	2482	9.8	9.8	642	581	41.8	41.9	44.4	446	27209	29	1.2	61.91	807.7	.68
532	2510	68.6	6.5	7.3	116	33.7	2788	2482	9.8	9.8	633	558	41.9	41.8	44.4	443	27289	30	1.2	36.00	784.7	.68
534	2511	35.6	6.6	7.4	115	34.8	2849	2482	9.8	9.8	644	592	41.9	41.8	44.4	455	27540	31	1.2	55.73	759.5	.70
539	2512	15.7	6.5	7.3	112	35.5	2842	2484	9.8	9.8	637	559	41.6	41.8	44.3	448	28100	32	1.3	130.2	741.1	.75
541	2513	16.4	6.6	7.2	113	37.4	2850	2485	9.8	9.8	629	576	41.7	41.7	44.3	441	28327	33	1.3	129.8	721.4	.77
543	2514	30.9	6.5	7.3	115	39.7	2777	2485	9.8	9.8	637	621	41.7	41.7	44.2	448	28520	34	1.3	64.81	702.7	.78
546	2515	26.4	6.6	7.4	110	41.2	2775	2487	9.8	9.8	645	581	41.7	41.8	44.2	455	28813	35	1.4	77.59	684.6	.81
548	2516	21.4	6.3	7.4	114	32.6	2777	2488	9.8	9.8	645	565	41.7	41.7	44.2	465	29114	36	1.4	93.29	668.2	.83
550	2517	29.8	6.7	7.3	114	36.7	2828	2488	9.8	9.8	653	568	41.4	42.0	44.2	443	29311	37	1.5	69.97	652.2	.84
553	2518	26.5	6.9	7.5	113	42.3	2849	2489	9.8	9.8	652	568	41.8	42.0	44.2	443	29606	38	1.5	75.45	637.6	.87
556	2519	20.0	6.1	7.0	112	28.9	2859	2490	9.8	9.8	649	584	41.6	41.6	44.0	452	29993	39	1.6	99.86	623.8	.89
608	2520	27.7	6.1	7.3	112	42.4	2874	2492	9.8	9.8	644	647	41.4	41.9	43.7	441	30393	40	1.6	71.55	607.2	.91
609	2521	47.3	6.6	7.2	112	40.4	2831	2492	9.8	9.8	634	603	41.5	41.7	43.7	441	30575	41	1.6	42.29	596.5	.92
612	2522	27.0	6.6	7.1	111	41.4	2866	2493	9.8	9.8	648	618	41.6	41.8	43.5	438	30842	42	1.7	77.78	585.1	.94
613	2523	27.3	6.8	7.1	112	41.4	2879	2494	9.8	9.8	641	592	41.5	41.6	43.5	436	31048	43	1.7	73.23	572.6	.96
616	2524	28.3	6.0	7.2	110	30.4	2831	2495	9.8	9.8	629	604	41.3	41.2	43.5	423	31302	44	1.7	76.17	561.8	.97
618	2525	31.3	6.6	7.1	112	37.2	2815	2496	9.8	9.8	639	591	41.6	41.9	43.2	420	31518	45	1.8	67.16	550.5	.99
620	2526	27.6	6.9	7.2	112	40.5	2846	2498	9.8	9.8	652	608	41.3	41.9	43.2	429	31750	46	1.8	72.35	540.1	1.00
622	2527	28.0	7.0	7.4	112	37.1	2803	2499	9.8	9.8	635	603	41.4	41.9	43.0	434	31998	47	1.8	73.57	530.6	1.02
624	2528	30.9	6.6	7.2	113	33.3	2859	2500	9.8	9.8	641	611	41.5	41.8	43.0	428	32206	48	1.9	67.62	521.0	1.04
625	2529	36.5	6.8	7.3	112	35.5	2861	2501	9.8	9.8	642	608	41.8	41.9	43.0	431	32377	49	1.9	56.38	511.5	1.05
627	2530	32.0	6.6	7.2	113	36.2	2831	2502	9.8	9.8	645	636	41.9	42.0	42.7	438	32583	50	1.9	63.23	502.3	1.06
629	2531	35.7	6.5	7.2	113	34.3	2821	2503	9.8	9.8	643	591	41.7	41.9	42.7	422	32778	51	2.0	56.00	494.0	1.08
631	2532	27.3	6.7	7.2	114	38.5	2839	2503	9.8	9.8	640	638	41.9	41.8	42.7	434	33038	52	2.0	77.53	487.2	1.09
655	2533	19.6	5.0	7.2	90	31.3	2803	2509	9.8	9.8	632	627	41.7	42.0	42.3	434	33785	53	2.1	102.3	476.1	1.12
655	2534	33.0	4.6	5.7	107	38.7	2858	2509	9.8	9.8	639	625	42.0	41.4	42.3	441	33837	54	2.1	77.44	472.1	1.12
701	2535	16.5	4.9	8.3	107	37.2	2841	2511	9.8	9.8	632	631	41.9	41.7	42.1	438	34386	55	2.1	122.8	466.0	1.16
706	2536	9.5	4.9	6.3	109	34.9	2864	2513	9.9	9.8	652	594	41.9	42.3	42.0	426	34938					

ESSO AUSTRALIA FORTESCUE NO.3
UNIT #101 10:33 12/20/78

TIME	DEPTH	ROP	TORQUE	RPM	BIT	PUMP	RTNS	LB/GAL	GAL/MIN	TEMP(C)	PVT	REVS	MT	THIS BIT	EST	DXC	NDB	NP	ECD	NXW		
717	2538	10.8	4.8	5.9	111	37.3	2863	2517	10.0	9.8	627	601	42.2	42.3	41.6	426	36180	58	2.4	193.0	451.6	1.27
726	2539	8.7	7.0	8.2	110	41.3	2827	2519	9.9	9.8	635	619	42.6	42.2	41.6	435	37160	59	2.6	230.4	448.9	1.33
733	2540	9.2	4.7	8.4	110	37.9	2817	2523	9.9	9.8	644	573	42.7	42.4	41.5	438	37921	60	2.7	232.2	445.4	1.38
737	2541	8.9	5.7	8.0	110	37.9	2806	2524	9.9	9.8	628	589	42.6	42.5	41.5	427	38366	61	2.8	225.6	440.6	1.41
744	2542	10.3	5.5	8.3	115	42.0	2844	2528	9.9	9.8	643	559	42.5	42.7	41.4	436	39136	62	2.9	196.4	437.1	1.45
747	2543	10.5	5.5	8.3	109	41.9	2831	2529	9.9	9.8	627	530	42.4	42.6	41.4	450	39501	63	2.9	194.0	432.3	1.48
753	2544	12.8	7.3	8.4	112	40.3	2820	2530	9.9	9.8	643	565	42.5	42.6	41.4	441	40088	64	3.0	155.7	428.2	1.51
755	2545	17.9	5.5	8.3	110	40.6	2826	2530	9.9	9.8	634	603	42.8	42.7	41.5	433	40403	65	3.1	115.7	423.2	1.53
820	2546	7.0	6.1	8.4	111	37.9	2945	2534	9.9	9.7	655	573	43.6	44.5	41.8	418	41972	66	3.3	284.8	422.0	1.62
823	2547	8.5	5.5	6.9	111	34.4	2930	2534	9.9	9.8	656	588	43.5	44.5	41.8	428	42297	67	3.3	243.2	418.6	1.63
824	2548	26.4	6.1	7.4	112	40.7	2932	2534	9.9	9.8	645	559	43.4	44.4	41.8	421	42405	68	3.3	82.77	413.9	1.64
830	2549	13.0	6.1	8.5	112	41.9	2882	2536	9.9	9.8	650	553	43.5	44.5	41.8	419	41343	69	3.4	154.6	410.2	1.68
833	2550	13.3	5.6	7.1	112	38.1	2853	2536	9.9	9.8	649	579	43.5	44.3	41.8	419	43473	70	3.5	163.1	406.4	1.70
835	2551	28.9	6.0	6.3	114	38.2	2864	2536	9.9	9.8	642	545	43.7	44.1	41.9	424	43634	71	3.5	69.26	400.9	1.71
839	2552	17.2	5.7	6.6	112	41.6	2833	2537	9.9	9.8	642	565	43.9	44.6	42.1	402	44147	72	3.6	116.5	397.6	1.74
841	2553	21.7	8.2	8.1	114	40.9	2841	2537	9.9	9.8	639	548	43.9	44.3	42.1	407	44362	73	3.6	92.19	393.1	1.75
843	2554	30.9	5.6	8.2	112	42.8	2907	2537	9.9	9.8	648	531	44.0	44.5	42.1	421	44551	74	3.7	66.46	388.8	1.77
844	2555	37.8	7.8	7.8	112	41.4	2901	2538	9.9	9.8	648	551	43.8	44.6	42.3	420	44709	75	3.7	52.92	384.3	1.77
847	2556	25.8	7.0	8.3	113	40.6	2835	2538	9.9	9.8	653	568	44.1	44.5	42.3	421	45025	76	3.7	78.58	380.7	1.79
851	2557	15.4	5.6	6.2	110	33.9	2818	2539	9.9	9.8	643	560	43.9	44.4	42.4	412	45465	77	3.8	129.5	377.4	1.82
853	2558	21.2	5.9	6.6	112	41.7	2866	2540	9.9	9.8	652	555	43.9	44.3	42.4	412	45687	78	3.8	94.50	373.4	1.83
909	2559	13.0	5.8	6.7	111	34.4	2822	2542	9.9	9.8	634	536	44.1	44.7	42.5	397	46587	79	3.9	157.5	371.8	1.87
913	2560	9.7	6.1	8.1	112	38.5	2837	2543	9.9	9.8	630	544	44.2	45.2	42.5	424	47086	80	4.0	206.2	369.2	1.89
916	2561	15.8	7.4	7.9	112	40.6	2824	2543	9.9	9.8	630	542	44.2	44.9	42.5	419	47376	81	4.1	126.4	365.7	1.91
918	2562	28.7	5.6	8.4	110	46.2	2848	2543	9.9	9.8	636	537	44.0	44.9	42.5	421	47547	82	4.1	77.77	362.0	1.92
926	2563	9.4	4.2	8.2	108	41.8	2885	2543	9.9	9.8	636	542	44.5	44.7	42.6	412	48508	83	4.2	211.5	361.1	1.97
939	2564	5.0	5.0	8.2	106	41.7	2854	2546	9.9	9.8	639	552	44.4	45.1	42.9	424	49872	84	4.4	409.1	361.9	2.04
942	2565	9.0	7.3	8.0	109	45.5	2883	2541	9.9	9.8	645	532	44.7	45.1	43.2	426	50217	85	4.5	229.8	358.9	2.06
948	2566	13.9	6.4	8.1	112	46.2	2867	2549	9.9	9.8	637	547	44.3	44.9	43.3	417	50859	86	4.6	149.6	357.3	2.10
957	2567	8.0	4.8	8.1	109	42.4	2875	2553	9.9	9.9	649	528	44.5	45.1	43.6	431	51857	87	4.7	260.0	356.5	2.15
1001	2568	11.9	4.6	8.1	109	47.7	2895	2554	9.9	9.9	646	533	44.4	45.5	43.6	420	52280	88	4.8	183.0	354.5	2.17
1005	2569	16.2	5.0	7.8	110	42.3	2851	2556	9.9	9.9	643	535	44.3	44.8	43.7	423	52746	89	4.9	124.5	351.7	2.20
1009	2570	19.0	4.9	6.1	112	41.4	2825	2556	9.9	9.9	638	538	44.2	45.3	43.7	426	53159	90	4.9	105.6	349.2	2.22
1014	2571	11.9	5.1	6.2	109	48.3	2846	2557	9.9	9.9	638	510	44.2	45.2	43.8	424	53786	91	5.0	170.2	347.7	2.25
1021	2572	9.7	4.6	7.6	109	46.2	2814	2558	9.9	9.9	639	533	44.3	45.2	43.9	426	54499	92	5.1	209.9	346.3	2.29
1042	2573	10.8	5.6	7.9	109	40.1	2953	2561	9.9	9.8	644	548	44.2	45.2	43.9	409	55616	93	5.3	184.4	346.0	2.33
1053	2574	6.9	6.7	8.0	112	38.9	2893	2562	9.9	9.9	644	539	44.2	45.2	44.1	424	56818	94	5.5	290.3	346.3	2.39
1056	2575	14.4	7.0	7.9	112	42.1	2841	2563	9.9	9.9	648	538	44.2	45.1	44.2	419	57209	95	5.5	162.4	343.9	2.41
1105	2576	8.3	4.9	7.7	112	39.1	2883	2564	9.9	9.9	640	561	44.4	45.0	44.3	410	58198	96	5.7	241.4	343.7	2.45
1111	2577	8.7	4.5	7.2	109	44.0	2863	2565	9.9	10.0	630	566	44.3	45.5	44.4	407	58853	97	5.8	239.3	342.1	2.49
1118	2578	8.6	5.2	6.9	110	45.2	2893	2566	9.9	9.9	644	524	44.5	45.3	44.4	426	59563	98	5.9	245.5	341.1	2.52
1121	2579	12.7	5.8	6.4	112	44.7	2871	2567	9.9	10.0	643	466	44.8	45.4	44.4	407	59941	99	5.9	172.7	339.0	2.54
1127	2580	11.3	4.7	7.6	109	46.8	2873	2568	9.9	10.0	639	487	44.7	45.6	44.3	412	60584	100	6.0	183.7	337.5	2.57
1133	2581	9.4	4.2	7.8	109	39.0	2873	2569	9.9	10.0	624	476	44.8	45.5	44.3	417	61264	101	6.2	218.7	336.3	2.61
1154	2582	2.8	4.2	7.9	110	36.4	2907	2571	9.9	9.8	651	464	45.1	45.3	44.2	421	63536	102	6.5	770.5	339.7	2.70
1159	2583	5.7	5.4	5.6	110	37.8	2853	2571	9.9	9.8	630	368	44.9	45.5	44.2	414	64089	103	6.6	367.8	338.2	2.73
1203	2584	13.6	5.4	5.6	112	43.9	2811	2572	9.9	9.8	637	385	45.0	45.5	44.2	426	64515	104	6.6	147.3	336.2	2.74
1205	2585	18.2	4.6	6.6	109	35.7	2843	2573	9.9	9.8	643	364	45.0	45.6	44.2	412	64785	105	6.7	111.2	333.9	2.75
1218	2586	17.0	5.5	7.0	106	35.9	2737	2574	9.9	9.7	620											

ESSU AUSTRALIA FORTESCUE NO.3
UNIT #101 10:38 12/20/78

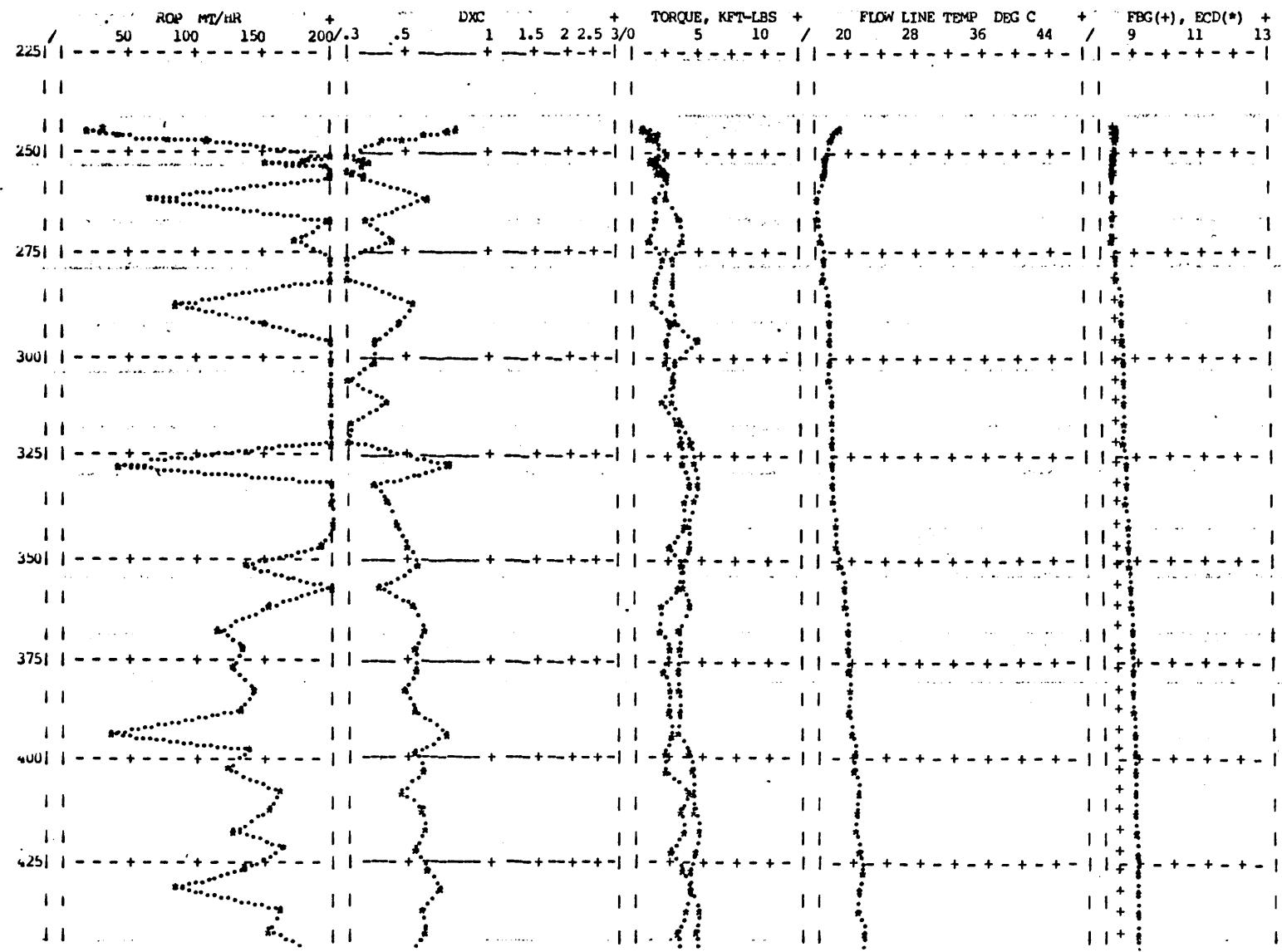
TIME	DEPTH	HOP	TORQUE	RPM	BT	PUMP	RTNS	LB/GAL	GAL/MIN	TEMP(C)	PVT	THIS BIT			EST	DXC	NMB	NP	ECD	NMMI							
												N/H	INST	MAX	WT	PSI	DEPTH	IN	OUT	LAG	REVS	MT	HRS	CPMI	CPMB	TW	
1220	2588	49.0	5.6	6.3	108	36.7	27461	2574	9.9	9.7	625	465	44.9	45.9	44.3	423	65625	108	6.8	41.58	326.8	2.78	.92	.96	22.6	10.2	8.51
1222	2589	25.5	5.3	5.9	109	33.4	28001	2574	9.9	9.8	624	406	44.7	45.4	44.2	412	65878	109	6.8	79.42	324.6	2.79	1.06	.94	18.6	10.2	8.61
1225	2590	23.0	4.3	5.9	107	36.7	28081	2575	9.9	9.8	629	310	44.7	45.5	44.2	421	66250	110	6.9	88.11	322.7	2.80	1.12	.94	17.1	10.3	8.51
1238	2591	6.8	5.8	7.6	111	37.0	28951	2577	9.9	9.8	640	394	44.8	45.6	44.3	417	67645	111	7.1	298.0	323.6	2.86	1.43	.93	9.9	10.3	8.51
1243	2592	12.6	4.3	6.8	109	34.8	28601	2578	9.9	9.8	635	571	44.9	45.6	44.4	408	68130	112	7.2	163.8	322.2	2.88	1.27	.95	13.7	10.3	8.61
1253	2593	7.3	5.6	7.8	109	38.9	28721	2579	9.8	9.8	644	523	44.8	45.5	44.5	405	69232	113	7.3	276.9	322.3	2.92	1.40	.95	10.5	10.3	8.51
1259	2594	9.1	4.7	6.3	108	39.1	28791	2579	9.8	9.8	623	485	45.1	45.9	44.7	420	69943	114	7.4	254.7	321.4	2.95	1.37	.96	12.0	10.3	8.61
1302	2595	17.8	4.6	5.2	109	37.1	28241	2579	9.8	9.8	633	526	45.1	45.8	44.7	407	70229	115	7.5	112.1	319.5	2.96	1.15	.95	15.9	10.3	8.61
1307	2596	13.3	5.1	7.9	109	38.5	28641	2580	9.8	9.8	631	503	45.2	45.6	44.8	409	70820	116	7.6	150.2	318.4	2.98	1.24	.94	14.1	10.3	8.51
1311	2597	11.7	4.9	5.7	109	34.1	28661	2580	9.9	9.8	634	470	44.8	45.6	44.8	395	71238	117	7.6	171.6	316.8	3.00	1.26	.95	13.6	10.3	8.61
1317	2598	12.2	5.3	5.8	107	39.1	29041	2582	9.9	9.9	633	376	45.2	46.1	44.9	402	71839	118	7.7	163.4	315.8	3.02	1.24	.95	13.9	10.3	8.51
1335	2599	14.2	5.3	5.8	106	38.7	28671	2586	9.9	9.9	631	493	45.4	45.8	45.1	405	72502	119	7.8	160.5	314.4	3.04	1.19	.95	15.3	10.2	8.51
1335	2600	48.2	5.0	5.7	110	35.6	28571	2586	9.9	9.9	613	490	45.2	45.8	45.1	402	72567	120	7.8	73.92	312.5	3.04	1.02	.94	20.0	10.2	8.61
1339	2601	24.7	5.5	5.9	110	36.2	28101	2587	9.9	9.8	632	469	45.1	45.1	45.0	405	72946	121	7.9	81.38	310.3	3.05	1.08	.93	18.3	10.2	8.51
1344	2602	13.9	4.5	5.8	109	41.4	28651	2587	9.9	9.9	634	463	45.2	46.1	45.0	412	73473	122	8.0	145.5	309.2	3.07	1.24	.92	14.4	10.2	8.51
1348	2603	12.4	4.8	5.9	109	34.0	28391	2588	9.9	9.9	626	466	45.2	46.2	45.0	393	73888	123	8.0	161.8	307.8	3.09	1.26	.92	13.7	10.2	8.51
1354	2604	10.8	5.8	7.0	111	40.8	28211	2589	9.9	9.8	624	331	45.2	46.3	44.9	402	74569	124	8.1	189.8	307.1	3.11	1.29	.93	13.1	10.2	8.51
1359	2605	10.1	6.0	6.4	111	39.4	28321	2590	9.9	9.8	622	508	45.2	46.4	44.8	409	75159	125	8.2	197.6	306.1	3.14	1.31	.94	12.1	10.2	8.51
1406	2606	10.3	4.8	6.3	110	36.1	28691	2590	9.9	9.8	618	484	45.2	45.8	44.8	404	75878	126	8.3	195.7	305.4	3.16	1.29	.94	13.1	10.2	8.61
1409	2607	15.2	4.9	5.4	110	35.3	28441	2591	9.9	9.8	627	561	45.2	45.8	44.8	396	76288	127	8.4	134.3	304.0	3.18	1.20	.94	15.3	10.2	8.61
1413	2608	16.9	4.6	5.2	109	32.9	28011	2591	9.9	9.8	635	574	45.0	43.1	44.8	389	76659	128	8.4	124.5	302.7	3.19	1.17	.94	16.5	10.2	8.61
1419	2609	11.5	4.9	5.3	109	39.0	27981	2593	9.9	9.9	618	446	44.6	45.8	44.9	408	77309	129	8.5	176.5	301.8	3.21	1.28	.94	13.5	10.2	8.61
1431	2610	5.8	4.6	5.9	107	37.6	27891	2595	9.9	9.9	637	274	44.8	46.2	44.9	398	78599	130	8.7	358.4	302.6	3.26	1.46	.93	9.6	10.2	8.51
1438	2611	6.7	4.5	6.0	107	39.4	27751	2596	9.9	9.9	623	370	45.0	45.8	44.9	401	79421	131	8.9	306.1	302.3	3.29	1.41	.94	10.5	10.2	8.61
1508	2612	5.6	3.9	5.4	104	37.9	28311	2601	9.8	9.8	635	353	45.0	45.8	45.1	382	80998	132	9.1	354.8	303.6	3.34	1.46	1.01	9.3	10.2	8.61
1530	2613	2.7	4.2	6.3	110	37.9	28491	2606	9.9	9.9	646	534	44.8	45.9	45.2	388	83417	133	9.5	807.4	307.0	3.43	1.60	.96	6.9	10.2	8.61
1534	2614	6.1	4.3	5.0	110	35.3	28181	2607	9.9	9.9	635	493	44.9	45.9	45.3	375	84258	134	9.6	330.1	306.7	3.46	1.41	.96	10.5	10.2	8.51
1541	2615	14.4	3.8	4.8	109	36.5	28501	2607	9.9	9.8	626	515	44.9	46.4	45.3	383	84641	135	9.6	152.1	305.4	3.47	1.22	.97	15.1	10.2	8.51
1546	2616	16.8	3.9	4.4	109	40.6	28921	2607	9.9	9.8	633	472	44.7	45.8	45.2	372	85098	136	9.7	122.2	304.2	3.49	1.21	.97	15.6	10.2	8.61
1557	2617	6.2	5.1	5.7	110	45.2	28421	2609	9.9	9.7	637	473	44.8	45.8	44.6	368	86397	137	9.9	337.7	305.0	3.53	1.43	.97	10.3	10.2	8.51
1605	2618	9.4	4.2	5.4	109	38.7	28441	2609	9.8	9.7	646	279	45.0	45.6	44.7	381	87208	138	10.0	227.3	304.6	3.56	1.32	.97	13.0	10.2	8.51
1619	2619	4.0	4.0	4.4	109	41.1	28531	2610	9.8	9.7	642	516	44.5	45.7	44.9	391	88772	139	10.3	511.1	305.8	3.51	1.53	.98	8.5	10.2	8.61
1631	2620	4.8	4.1	4.5	110	40.9	28671	2610	9.8	9.6	636	370	44.9	45.9	44.9	389	90033	140	10.5	434.8	306.5	3.66	1.52	.99	8.7	10.2	8.61
1646	2621	3.9	3.8	5.2	108	41.6	28111	2612	9.9	9.7	641	396	44.6	45.5	44.9	408	91739	141	10.7	628.9	308.2	3.72	1.60	.97	7.2	10.2	8.61
1701	2622	3.9	3.8	4.9	101	36.4	28451	2614	9.9	9.7	640	421	44.6	45.4	44.9	401	93332	142	11.0	523.6	309.4	3.77	1.56	.98	8.1	10.2	8.61
1709	2623	6.0	3.7	7.0	101	37.4	28721	2615	9.9	9.7	640	432	44.5	45.6	44.9	398	94167	143	11.1	359.6	309.3	3.80	1.41	1.00	10.9	10.2	8.61
1721	2624	5.8	4.1	4.5	102	42.2	28271	2616	9.9	9.7	627	354	44.6	45.7	44.9	415	95393	144	11.3	342.0	310.0	3.83	1.43	1.01	10.3	10.2	8.61

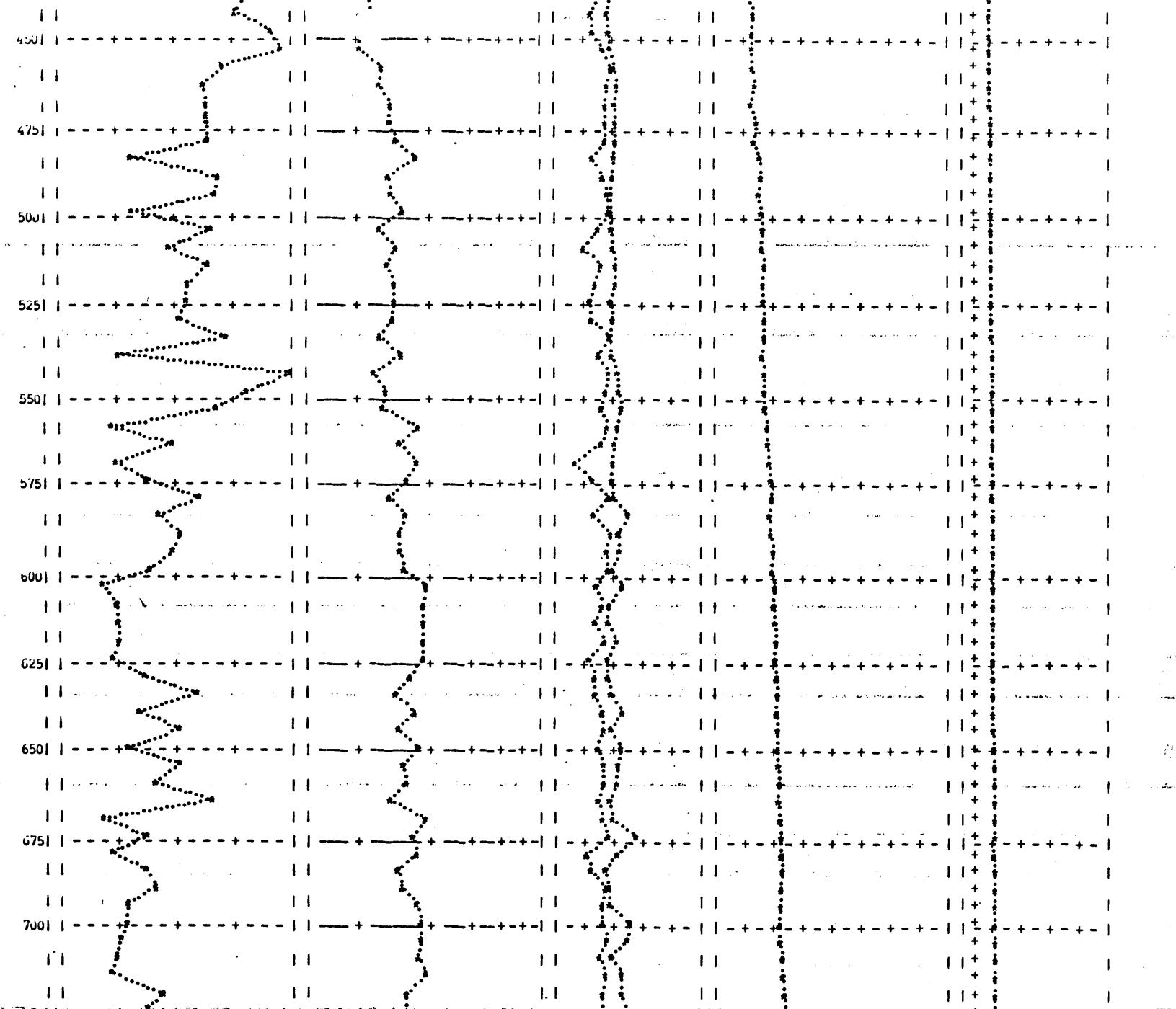
DEPTL DEPTH : 2625 METERS, MAKE WIPER TRIP AND POOH TO RUN WIRELINE LOGS.

(ii) DRILLING DATA PLOT 1:1000

(b) ROP, D_{xc}, Torque, Flowline Temp,
Pore Pressure, ECD

OFFLINE PLOT: SCALE OF 1 TO 1000

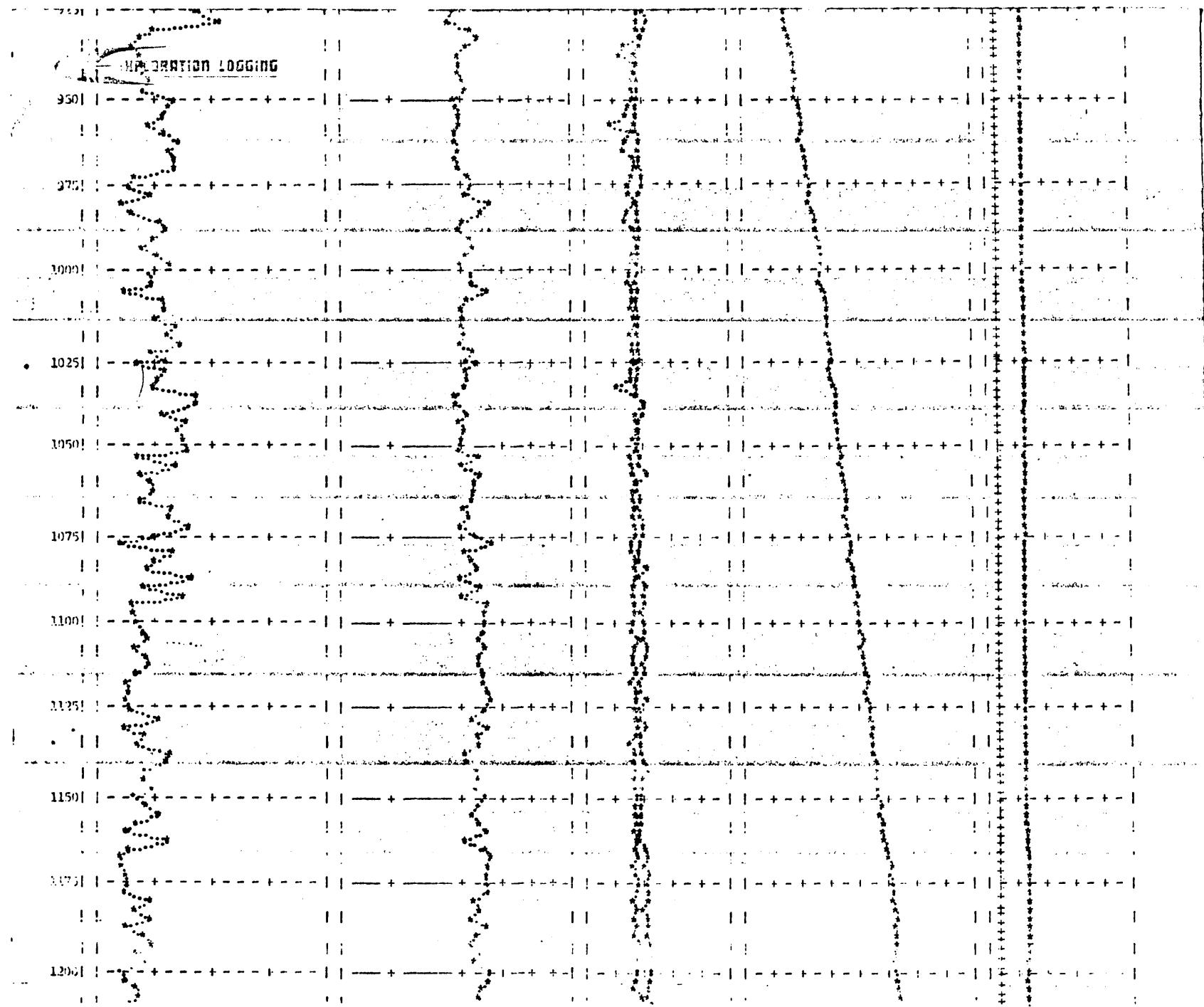




EXPLORATION LOGGING

y6

OFFLINE PLOT: SCALE OF 1 TO 1000



EDUCATION LOGGING

15001 PLEASANT RIVER -

15251

15501

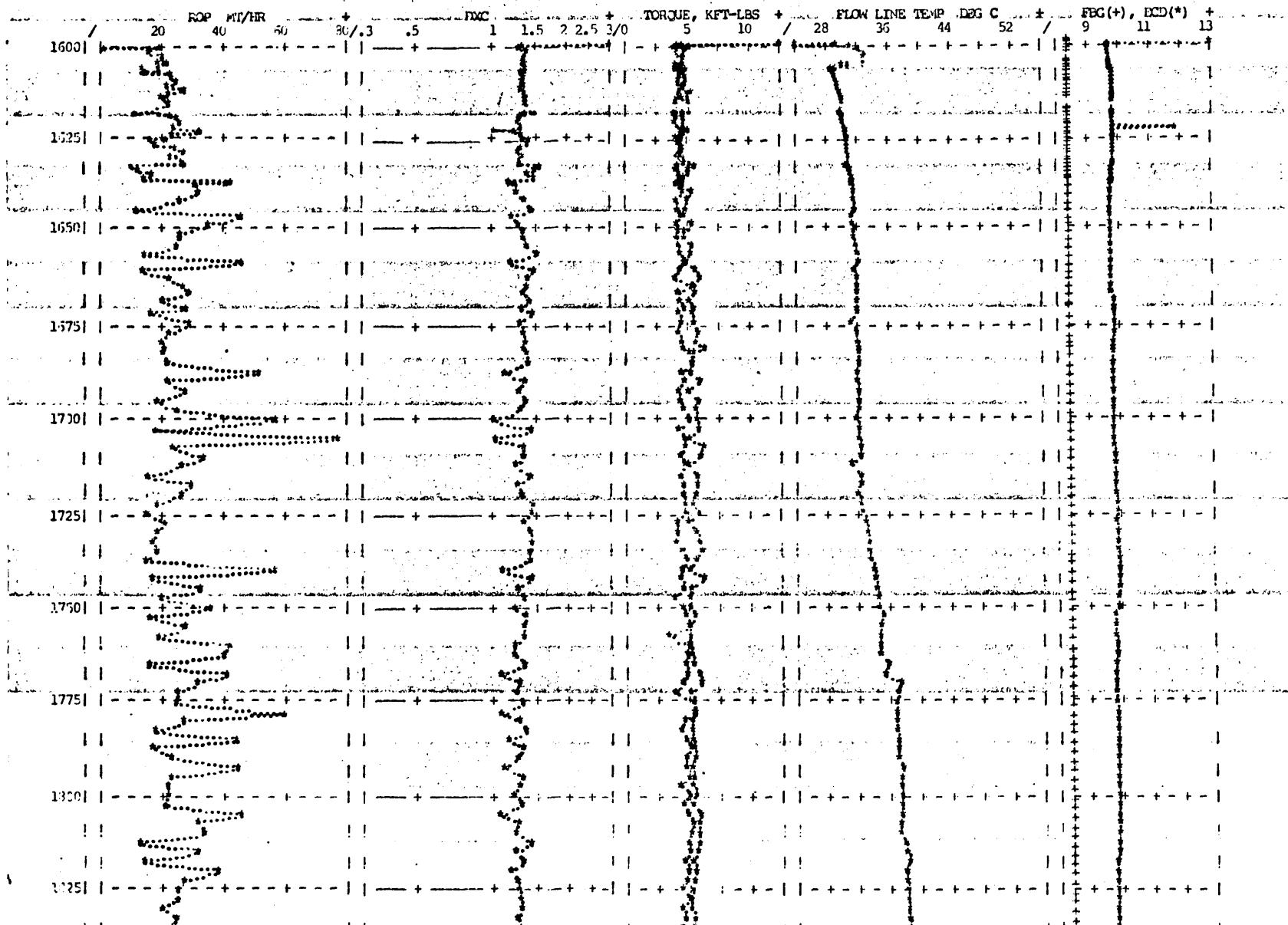
15751

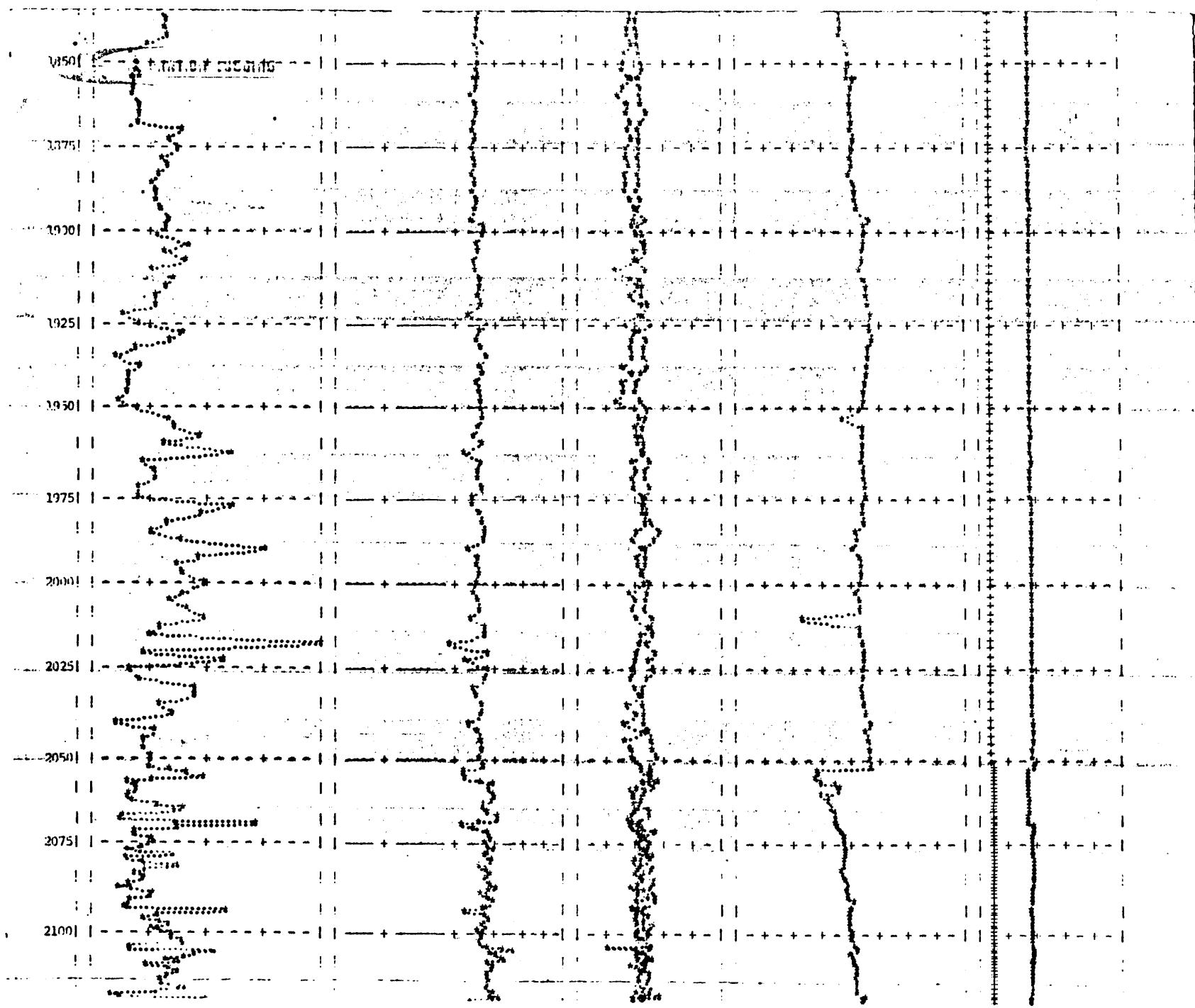
16001

16251

EXPLORATION LOGGING

Offline Plot: Scale of 1 to 1000





~~EXPLORATION LOGGING~~

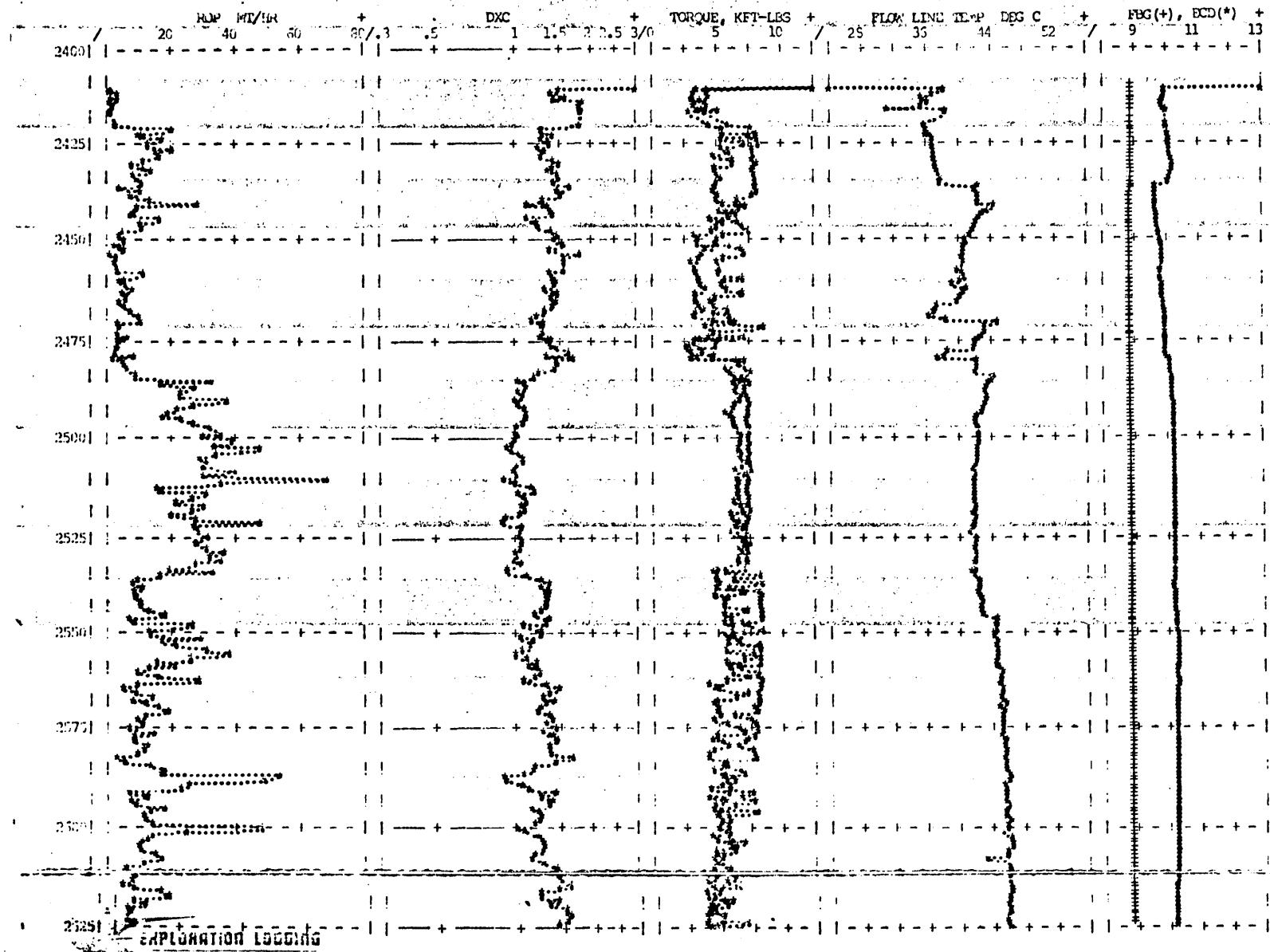
2125| - + - - + - - | - - + - + - | - + - + - | - + - + - + - | - + - + - | + - + - + - |
2150| - - - + - - + - | - - + - + - | - + - + - | - + - + - + - | - + - + - | + - + - + - |
2175| - - - + - - + - | - - + - + - | - + - + - | - + - + - + - | - + - + - | + - + - + - |
2200| - - - + - - + - | - - + - + - | - + - + - | - + - + - + - | - + - + - | + - + - + - |

2225| - - - + - - + - | - - + - + - | - + - + - | - + - + - + - | - + - + - | + - - + - + - |
2250| - - - + - - + - | - - + - + - | - + - + - | - + - + - + - | - + - + - | + - - + - + - |
2275| - - - + - - + - | - - + - + - | - + - + - | - + - + - + - | - + - + - | + - - + - + - |
2300| - - - + - - + - | - - + - + - | - + - + - | - + - + - + - | - + - + - | + - - + - + - |
2325| - - - + - - + - | - - + - + - | - + - + - | - + - + - + - | - + - + - | + - - + - + - |
2350| - - - + - - + - | - - + - + - | - + - + - | - + - + - + - | - + - + - | + - - + - + - |
2375| - - - + - - + - | - - + - + - | - + - + - | - + - + - + - | - + - + - | + - - + - + - |
2400| - - - + - - + - | - - + - + - | - + - + - | - + - + - + - | - + - + - | + - - + - + - |

~~EXPLORATION LOGGING~~

F X

OFFLINE PLOT: SCALE OF 1 TO 1000



~~EXPLORATION LOGGING~~

A P P E N D I X E

MORNING AND WEEKLY REPORTS

PETROLEUM ENGINEERING SUMMARY REPORT

COMPANY ESSO AUSTRALIA

WELL NAME FORTESCUE NO. 3.

DATE 28 Nov. 78. TIME 0530 HRS.

DEPTH 392M LAST REPORT DEPTH -

DRILL RATE 60-400 M/HR
 CORRECTED D EXPONENT .4
 FLOWLINE TEMPERATURE 20°C
 SHALE DENSITY -
 SHALE FACTOR -
 MAX. FORMATION GAS 0
 BACKGROUND GAS 0
 CONNECTION GAS 0
 TRIP GAS 0
 LITHOLOGY: Calcareous

SPM	100	
GPM	890	
DP AN VEL	64.0	FT/M
DC AN VEL	88.6	"
CRITICAL VEL		
PRESS(TOTAL)	1250	
PRESS(BIT)	766	
PRESS(SYSTEM)	484	
BIT NOZ VEL	310	FT/SEC
HOLE VOL	452	BBLS
AN. VOL	401	BBLS
PIPE VOL	17.8	BBLS
PIPE DISPL.	33.5	BBLS
BIT TYPE	HTC	OSC 3A
	22	72
	72	22

MUD WT. IN	<u>8.9</u>	PV/YP	<u>-</u>
MUD WT. OUT	<u>9.0</u>	CL.	<u>-</u>
ECD	<u>8.9 -</u>	% SOLIDS	<u>-</u>
ESTIMATED PORE PRESS	<u>8.4</u>		
MAX. ESTIMATED PORE PRESS IN OPEN HOLE	<u>8.4</u>		
ESTIMATED FRACTURE PRESS	<u>9.0</u>		
MIN. EST. FRAC. PRESS. IN OPEN HOLE	<u>9.0</u>		

Av. WOB	25
Av. RPM	80
Av. TORQUE	3.5 Kft
TIGHT HOLE	-
FILL	-
△ LAG	-
EST. % SAVINGS	-

COMMENTS:

PETROLEUM ENGINEERING SUMMARY REPORT

COMPANY ESSO AUSTRALIA LTD
 WELL NAME FORTESCUE No. 3
 DATE 29 NOV. 78 TIME 0530 HRS.
 DEPTH 878 M LAST REPORT DEPTH 392 M

DRILL RATE	10 - 200 M/HR	SPM	110
CORRECTED D EXponent	.7 - 1.25	GPM	950
FLOWLINE TEMPERATURE	26.0°	DP AN VEL	83 FT/MIN
SHALE DENSITY	2.25	DC AN VEL	95 FT/MIN
SHALE FACTOR	-	CRITICAL VEL	83 FT/MIN
MAX. FORMATION GAS	24 units	PRESS(TOTAL)	1800
BACKGROUND GAS	10 units	PRESS(BIT)	883
CONNECTION GAS	-	PRESS(SYSTEM)	917
TRIP GAS	-	BIT NOZ VEL	331 FT/SEC
LITHOLOGY:	Calcsiltite	HOLE VOL	927 BBLs
		AN. VCL	838 BBLs
		PIPE VCL	45.7 BBLs
		PIPE DISPL.	44.9 BBLs
		BIT TYPE	NTC OSC 3A1
MUD WT. IN	8.9	JETS	20 20 20
MUD WT. OUT	9.3	AV. WOB	30
ECD	9.1	AV. RPM	120
ESTIMATED PORE PRESS	8.4	AV. TORQUE	5.0 K ft lb
MAX. ESTIMATED PORE PRESS IN OPEN HOLE	8.4	TIGHT HOLE	-
ESTIMATED FRACTURE PRESS	14.0	FILL	-
MIN. EST. FRAC. PRESS. IN OPEN HOLE	10.0	Δ LAG	-
		EST. % CAVINGS	5%

COMMENTS: POOH TO LOG AND RUN 13 3/8" CASING.

PETROLEUM ENGINEERING SUMMARY REPORT

COMPANY ESSO AUSTRALIA LTD

WELL NAME FORTESCUE No.3

DATE 30TH NOV 78. TIME 0530 HRS

DEPTH 878 M LAST REPORT DEPTH 878 M

DRILL RATE _____

SPM _____

CORRECTED D EXPONENT _____

GPM _____

FLOWLINE TEMPERATURE _____

DP AN VEL _____

SHALE DENSITY _____

DC AN VEL _____

SHALE FACTOR _____

CRITICAL VEL _____

MAX. FORMATION GAS _____

PRESS(TOTAL) _____

BACKGROUND GAS _____

PRESS(BIT) _____

CONNECTION GAS _____

PRESS(SYSTEM) _____

TRIP GAS 7 units.

BIT NOZ VEL _____

LITHOLOGY: _____

HOLE VOL _____

AN. VOL _____

PIPE VOL _____

PIPE DISPL. _____

BIT TYPE	
----------	--

JETS	
------	--

MUD WT. IN	PV/YP
------------	-------

MUD WT. OUT	CL-
-------------	-----

ECD	% SOLIDS
-----	----------

ESTIMATED PORE PRESS	<u>8.4</u>	TIGHT HOLE	DRAG ON TRIP
----------------------	------------	------------	--------------

MAX. ESTIMATED PORE PRESS IN OPEN HOLE 8.4

FILL

ESTIMATED FRACTURE PRESS 14.0

△ LAG

MIN. EST. FRAC. PRESS. IN OPEN HOLE 10.0

EST. % CAVINGS

COMMENTS: RUN E-LOGS AND 13 $\frac{3}{8}$ " CASING
SHOE AT 867 M

PETROLEUM ENGINEERING SUMMARY REPORT

COMPANY ESSO AUSTRALIA LTD

WELL NAME FORTESCUE NO.3

DATE 1ST DEC 1978.

TIME 0530 HRS

DEPTH 932

LAST REPORT DEPTH

878 M

DRILL RATE 20-30 M/HR

CORRECTED D EXPONENT 1.15

FLOWLINE TEMPERATURE 30°C

SHALE DENSITY —

SHALE FACTOR —

MAX. FORMATION GAS 10

BACKGROUND GAS 5

CONNECTION GAS 0

TRIP GAS D units

LITHOLOGY: CALCISILTITE

SPM 110

GPM 950

DP AN VEL 180 FT/MIN

DC AN VEL 247 FT/MIN

CRITICAL VEL

PRESS(TOTAL) 2500

PRESS(BIT) 1361

PRESS(SYSTEM) 1139

BIT NOZ VEL 409 FT/SEC

HOLE VOL 533 BBLS

AN. VOL 441 BBLS

PIPE VOL 46.5 BBLS

PIPE DISPL. 49 BBLS

BIT TYPE	HTC XIG
JETS	18, 18, 18.
AV. WOB	30
AV. RPM	120
AV. TORQUE	S. KFT lbs
TIGHT HOLE	—
FILL	—
Δ LAG	—
EST. % CAVINGS	10%

COMMENTS:

DRILL OUT 13³/₈" CASING AND RUN
PRESSURE INTEGRITY TEST AT 813 M. TD

EXPLORATION DRILLING

DAVIER

PETROLEUM ENGINEERING SUMMARY REPORT

COMPANY ESSO AUSTRALIA LTDWELL NAME FORTESCUE NO.3DATE 2 ND DEC 1978 TIME 0530 HRSDEPTH 1347M LAST REPORT DEPTH 932M

DRILL RATE	<u>25 m hr</u>
CORRECTED D EXPONENT	<u>1.25</u>
FLOWLINE TEMPERATURE	<u>33.8</u>
SHALE DENSITY	<u>-</u>
SHALE FACTOR	<u>-</u>
MAX. FORMATION GAS	<u>19 units</u>
BACKGROUND GAS	<u>10 units</u>
CONNECTION GAS	<u>-</u>
TRIP GAS	<u>100 units</u>
LITHOLOGY:	<u>CALCISILTITE AND MARL</u>
MUD WT. IN	<u>9.1</u>
MUD WT. OUT	<u>9.2+</u>
ECD	<u>9.3</u>
ESTIMATED PORE PRESS	<u>8.4</u>
MAX. ESTIMATED PORE PRESS IN OPEN HOLE	<u>8.4</u>
ESTIMATED FRACTURE PRESS	<u>14.0</u>
MIN. EST. FRAC. PRESS. IN OPEN HOLE	<u>14.0</u>

SPM	<u>105</u>
GPM	<u>900</u>
DP AN VEL	<u>176 FT/MIN</u>
DC AN VEL	<u>245 FT/MIN</u>
CRITICAL VEL	
PRESS(TOTAL)	<u>2700</u>
PRESS(BIT)	<u>1221</u>
FEELS(SYSTEM)	<u>1479</u>
BIT NOZ VEL	<u>387 FT/SEC</u>
HOLE VOL	<u>761 BBLs</u>
AN. VOL	<u>630 BBLs</u>
PIPE VOL	<u>73 BBLs</u>
PIPE DISPL.	<u>60 BBLs</u>
BIT TYPE	<u>HTC X3A</u>
JETS	<u>18 18 18.</u>
AV. WOB	<u>50</u>
AV. RPM	<u>120</u>
AV. TORQUE	<u>5. KFT 16c</u>
TIGHT HOLE	<u>1111 M</u>
FILL	<u>-</u>
△ LAG	<u>-</u>
EST. % CAVINGS	<u>5%</u>

COMMENTS: PODFF TO CHANGE B.T. TIGHT HOLE AT
1111 M APPROX

PETROLEUM ENGINEERING SUMMARY REPORT

COMPANY ESCO AUSTRALIA LTD.

WELL NAME FORTESCUE NO.3

DATE 3RD DEC 1978.

TIME 0530 HRS.

DEPTH 1508M. LAST REPORT DEPTH 1347M.

DRILL RATE	<u>10 m hr</u>
CORRECTED D EXPONENT	<u>1.45</u>
FLOWLINE TEMPERATURE	<u>23.3</u>
SHALE DENSITY	<u>-</u>
SHALE FACTOR	<u>-</u>
MAX. FORMATION GAS	<u>8 units</u>
BACKGROUND GAS	<u>5 units</u>
CONNECTION GAS	
TRIP GAS	<u>42 units AT 1508M</u>
LITHOLOGY:	<u>CALCAREOUS MUDSTONE</u>
MUD WT. IN	<u>9.1</u>
MUD WT. OUT	<u>9.2</u>
ECD	<u>9.3</u>
ESTIMATED PORE PRESS	<u>8.4</u>
MAX. ESTIMATED PORE PRESS IN OPEN HOLE	<u>8.4</u>
ESTIMATED FRACTURE PRESS	<u>14.5</u>
MIN. EST. FRAC. PRESS. IN OPEN HOLE	<u>14.0</u>

SPM	<u>900</u>
GPM	<u>105 L</u>
DP AN VEL	<u>176 FT/MIN</u>
DC AN VEL	<u>245 FT/MIN</u>
CRITICAL VEL	
PRESS(TOTAL)	<u>2700</u>
PRESS(BIT)	<u>1221</u>
PRESS(SYSTEM)	<u>1479</u>
BIT NOZ VEL	<u>387 FT/SEC</u>
HOLE VOL	<u>826 BBLs</u>
AN. VOL	<u>685 BBLs</u>
PIPE VOL	<u>81.5 BBLs</u>
PIPE DISPLAY	<u>63.4 BBLs</u>
BIT TYPE	<u>HTC X3A</u>
JETS	<u>18, 18, 18.</u>
AV. WOB	<u>45</u>
AV. RPM	<u>120</u>
AV. TORQUE	<u>5.0 K FT lbs</u>
TIGHT HOLE	<u>1508 - 1050</u>
FILL	<u>-</u>
△ LAG	<u>-</u>
EST. % CAVINGS	<u>-</u>

COMMENTS: P.O.H AT 1508M. TIGHT HOLE TO 1050 M
HOLE NOT TAKING MUD. RUN BACK TO BOTTOM
AND CIRCULATE HIGH VISCOS MUD. THROUGH
SYSTEM. P.O.D.H.

PETROLEUM ENGINEERING SUMMARY REPORT

COMPANY ESSO AUSTRALIA LTD

WELL NAME FORTESCUE NO.3.

DATE 4TH DEC. 1978. TIME 0530 HRS

DEPTH 1547 M LAST REPORT DEPTH 1508 M.

DRILL RATE 1-2 M/HR
 CORRECTED D EXPONENT 1.95
 FLOWLINE TEMPERATURE 29°C
 SHALE DENSITY -
 SHALE FACTOR -
 MAX. FORMATION GAS 2000+ units
 BACKGROUND GAS 8 units
 CONNECTION GAS -
 TRIP GAS 2 units
 LITHOLOGY: CALCAREOUS MUDDSTONE

SPM 35
 GPM 285
 DP AN VEL 56 FT/MIN
 DC AN VEL 77 FT/MIN
 CRITICAL VEL
 PRESS(TOTAL) 1400
 PRESS(BIT) 13
 PRESS(SYSTEM) 1387
 BIT NOZ VEL 39 FT/SEC
 HOLE VOL 848 BBLs
 AN. VOL 710 BBLs
 PIPE VOL 85 BBLs.
 PIPE DISPL. 57 BBLs

BIT TYPE CHRIS C20
 JETS -

MUD WT. IN <u>9.6</u>	PV/YP <u>16/13</u>	AV. WOB <u>35</u>
MUD WT. OUT <u>9.7</u>	CL- <u>3800</u>	AV. RPM <u>80</u>
ECD <u>9.7</u>	% SOLIDS <u>93%</u>	AV. TORQUE <u>3 K-Ft lbs</u>
ESTIMATED PORE PRESS <u>8.4</u>		TIGHT HOLE <u>-</u>
MAX. ESTIMATED PORE PRESS IN OPEN HOLE <u>8.4</u>		FILL <u>-</u>
ESTIMATED FRACTURE PRESS <u>14.5</u>		Δ LAG <u>-</u>
MIN. EST. FRAC. PRESS. IN OPEN HOLE <u>14.0</u>		EST. % CAVINGS <u>-</u>

COMMENTS: DRILL FROM 1508 - 1536M. ENCOUNTER HIGH GAS SHOW FROM 1526 M. RUN CORE BARREL 8

PETROLEUM ENGINEERING
FORMATION LOGGING

PETROLEUM ENGINEERING
SUMMARY REPORT

COMPANY ESSO AUSTRALIA

WELL NAME Fortescue No. 3

DATE Dec. 5th 1978. TIME 0600

DEPTH 1600m LAST REPORT DEPTH 1547m

Drill Rate ..	<u>15m/hr ave</u>
Corrected "D" Exponent ..	<u>1.47</u>
Flowline Temperature ..	<u>31.8°C</u>
Shale Density
Shale Factor
Maximum Formation Gas ..	<u>8 units</u>
Background Gas ..	<u>5 to 6 units</u>
Connection Gas ..	<u>nil</u>
Trip Gas ..	<u>18 units from 1547.5m</u>
Lithology ..	<u>Calcareous Mudsone</u>			

S.P.M.....	<u>98</u>
G.P.M.....	<u>850</u>
D.P. An.Vel.....	<u>166.6</u>
D.C. An.Vel.....	<u>222.1</u>
Critical Vel.....	<u>273.1</u>
Press.(total).....	<u>2706</u>
Press.(bit).....	<u>2620</u>
Press.(system).....	<u>2680</u>
Bit...Noz.Vel.....	<u>366</u>
Hole...Vol.....	<u>870</u>
An...Vol.....	<u>724</u>
Tub...Vol.....	<u>85</u>
Displ...Vol.....	<u>61</u>
Bit Type	<u>HTC X3A</u>
Jets	<u>3x18...</u>

Mud Weight IN ..	<u>PV/YP 12/12</u>	..
Mud Weight OUT ..	<u>CF 38.00</u>	..
Effective Circulating Density (ECD)	<u>% Solids 12</u>	..
Estimated Pore Pressure ..	<u>8.4 70.8.5 lb/gal</u>	..
Maximum Estimated Pore Pressure in Open Hole ..	<u>8.5 lb/gal</u>	..
Estimated Fracture Pressure at T.D. ..	<u>14.5 lb/gal</u>	..
Minimum Estimated Fracture Pressure in Open Hole	<u>14.0 lb/gal</u>	..

Avg...WOB.....	<u>51000</u>
Avg...RPM.....	<u>120</u>
Avg...Torque.....	<u>5500</u>
Light Hole.....	-
Fill.....	-
Δ...Lag.....	<u>+100 STKS</u>
Est...%Cavings.....	-

Comments: Stopped drilling at 1600m. Waiting for repair to BOP's

PETROLEUM LOGGINGPETROLEUM ENGINEERING
SUMMARY REPORTCOMPANY Esso AustraliaWELL NAME Fortescue #3DATE 9 Dec 1978TIME 0600DEPTH 1610 m LAST REPORT DEPTH 1600 m

Drill Rate	22	SPM	104
Corrected "D" Exponent	1.34	G.P.M.	900
Flowline Temperature	30.2	D.P. An. Vel.	176.4 ft/min
Shale Density	-	D.G. An. Vel.	235.2 ft/min
Shale Factor	-	Critical Vel.	307.9 ft/min
Maximum Formation Gas	3 units	Press. (total)	2850 psi
Background Gas	2-3 units	Press. (bit)	2677 psi
Connection Gas	nil	Press. (system)	2854 psi
Trip Gas	180 units	Bit. Noz. Vel.	3.59 ft/sec
Lithology	Calcareous Mudstone	Hole. Vol.	874 bbls
		An. Vol.	728 bbls
		Tub. Vol.	86 bbls
		Displ. Vol.	61 bbls
		Bit Type	HTC x3A
		Jets	18, 18, 20
Mud Weight IN	1.6	Ay. WOB	451,000
Mud Weight OUT	1.4	Ay. RPM	120
Effective Circulating Density (ECD)	1.7	Ay. Torque	5000
Estimated Pore Pressure	8.4	Tight Hole	-
Maximum Estimated Pore Pressure in Open Hole	8.5	Fill	-
Estimated Fracture Pressure at T.D.	14.5	Δ Lag	-
Minimum Estimated Fracture Pressure in Open Hole	14.0	Est. % Cavings	-

Comments:

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PETROLEUM ENGINEERING SUMMARY REPORT

COMPANY ESSO AUSTRALIA

WELL NAME FORTESCUE No 3.

DATE 10th Dec. 1978 TIME 0600

DEPTH 1975m LAST REPORT DEPTH 1610m

DRILL RATE	<u>15 to 22 m/Hr.</u>
CORRECTED D EXPONENT	<u>1.40</u>
FLOWLINE TEMPERATURE	<u>41.6°C</u>
SHALE DENSITY	<u>-</u>
SHALE FACTOR	<u>-</u>
MAX. FORMATION GAS	<u>0 units</u>
BACKGROUND GAS	<u>4 to 5 units</u>
CONNECTION GAS	<u>nil</u>
TRIP GAS	<u>nil no trips</u>
LITHOLOGY:	<u>Marl</u>
MUD WT. IN	<u>9.5 lb/gal</u>
MUD WT. OUT	<u>9.3 lb/gal</u>
ECD	<u>9.8 lb/gal</u>
ESTIMATED PORE PRESS	<u>8.4 lb/gal</u>
MAX. ESTIMATED PORE PRESS IN OPEN HOLE	<u>8.5</u>
ESTIMATED FRACTURE PRESS	<u>14.5 lb gal</u>
MIN. EST. FRAC. PRESS. IN OPEN HOLE	<u>14.0</u>

SPM	<u>97</u>
GPM	<u>840</u>
DP AN VEL	<u>2645 ft/min</u>
DC AN VEL	<u>219.5 ft/min</u>
CRITICAL VEL	<u>309.5 ft/min</u>
PRESS(TOTAL)	<u>2905 psi</u>
PRESS(BIT)	<u>3252 psi</u>
PRESS(SYSTEM)	<u>2790 psi</u>
BIT NOZ VEL	<u>335 ft/sec</u>
HOLE VOL	<u>1049 bbl</u>
AN. VOL	<u>874 bbl</u>
PIPE VOL	<u>104 bbl</u>
PIPE DISPL.	<u>71 bbl</u>
BIT TYPE	<u>HFC X3A</u>
JETS	<u>18, 18, 20</u>
AV. WOB	<u>49,000 lb</u>
AV. RPM	<u>150</u>
AV. TORQUE	<u>5800 ft lbs</u>
TIGHT HOLE	<u>-</u>
FILL	<u>-</u>
△ LAG	<u>+ 100 stroke</u>
EST. % CAVINGS	<u>-</u>

COMMENTS:

PETROLEUM ENGINEERING SUMMARY REPORT

COMPANY ESSO AUSTRALIA

WELL NAME FORTESCUE NO.3.

DATE 11 Dec. 1978

TIME 0600

DEPTH 2131

LAST REPORT DEPTH

1975

API GRADE	<u>20</u>	SPM	<u>104</u>
CORRECTED TO EXponent	<u>1.42 @ 2125m</u>	SPM	<u>900</u>
TOOL LIFE TEMPERATURE	<u>411.8°C</u>	DP IN VEL	<u>176.4 ft/min</u>
SLUDGE VENTILITY	<u>-</u>	DC IN VEL	<u>235.2 ft/min</u>
BURST FACTOR	<u>-</u>	CRITICAL VEL	<u>268.6 ft/min</u>
HOLE DILUTION AS	<u>9 and 0.2050m</u>	PRESS (TOTAL)	<u>2875 PSI</u>
EXCAVATION LAG	<u>3 to 4</u>	PRESS (BIT)	<u>3529 PSI</u>
CONNEXION GAS	<u>nil</u>	FAULTS (VOL/HR)	<u>2805 PSI</u>
BLDG GAS	<u>100 units</u>	BIT NO. VOL	<u>314 ft/sec</u>
LITHOLOGY	<u>Mud & Calcareous - Mudat.</u>	HOLE VOL	<u>1134 bbls.</u>
		DRILL VOL	<u>936 bbls.</u>
		DRILL VES	<u>118 bbls.</u>
		FILE DIA.	<u>79 bbls.</u>
		BIT TYPE	<u>HTC X3A</u>
		JETS	<u>3x20</u>
MUD WT. IN	<u>9.5 lb/gal</u>	AV. WOB	<u>48</u>
MUD WT. OUT	<u>9.5 lb/gal</u>	AV. RPM	<u>152</u>
ECD	<u>9.8 lb/gal</u>	AV. TORQUE	<u>5900</u>
ESTIMATED TOTAL PRESS	<u>8.4 lb/gal</u>	TIGHT HOLE	<u>-</u>
MAX. ESTIMATED FORC. PRESS IN OPEN HOLE	<u>8.5</u>	FILL	<u>-</u>
ESTIMATED FRI. TIME (sec.)	<u>14.5</u>	Δ LAG	<u>-</u>
MIN. EST. FRAC. PRESS. IN OPEN HOLE	<u>14.0</u>	EST. % SAVINGS	<u>-</u>

COMMENTS:

PETROLEUM ENGINEERING SUMMARY REPORT

COMPANY ESSO AUSTRALIA
 WELL NAME FORTESCUE No 3
 DATE 12 DEC 78 TIME 06⁰⁰
 DEPTH 2409 m LAST REPORT DEPTH 2131 m

DRILL RATE 18 m/hr average
 CORRECTED D EXponent 1.30 at 2380m
 FLOWLINE TEMPERATURE 47.0 °C
 SHALE DENSITY -
 SHALE FACTOR -
 MAX. FORMATION GAS 9 units at 2260 m
 BACKGROUND GAS 2 - 4 units
 CONNECTION GAS -
 TRIP GAS -
 LITHOLOGY: MARL & CALCAREOUS MUDSTONE

SPM	<u>98</u>
GPM	<u>850</u>
DR. IN VOL	<u>166</u>
DC IN VOL	<u>222</u>
CIRCULAT. VOL	<u>330</u>
PRESS (TOTAL)	<u>2800</u>
FRESC (BLIT)	<u>746</u>
FRESC (SYSTEM)	<u>2054</u>
BUT NOT VOL	<u>296</u>
HOLE VOL	<u>1255</u>
AN. VOL	<u>1037</u>
PIPE VOL	<u>133</u>
FIRE VOL.	<u>85</u>
BIT TYPE	<u>NB 8 HTC X3A</u>
JIT	<u>3 x 20</u>

MIN. ST. IN	<u>9.5</u>	MAX. ST. IN	<u>12/18</u>
MIN. ST. OUT	<u>9.5</u>	ST. OUT	<u>3700</u>
ECO	<u>9.8</u>	ST. OUT	<u>10</u>
ESTIMATED DRILL PRESS	<u>8.4</u>		
MAX. ESTIMATED FORC. PRESS. IN OPEN HOLE	<u>8.5</u>		
ESTIMATED FRC. PRESS. IN HOLE	<u>16.5</u>		
MIN. EST. FRC. PRESS. IN OPEN HOLE	<u>14.0</u>		

AV. WOB	<u>40</u>
AV. RPM	<u>125</u>
AV. TURBL.	<u>5-6,000</u>
TURBL. VOL	<u>-</u>
STL	<u>-</u>
Δ LAS	<u>- 200 stree</u>
F. RELAVING	<u>-</u>

COMMENTS:

Drill from 2131 m to 2409 m.
High torque at 2409 m.
Circulate Returns - blocked flowline

PETROLEUM ENGINEERING SUMMARY REPORT

COMPANY ESSO. AUSTRALIA.
 WELL NAME FORTESCUE No 3
 DATE 13 DEC 78 TIME 06⁰⁰ hrs
 DEPTH 2412 m LAST REPORT DEPTH 2409 m

DRILL RATE	CORING AV. 2.5 m hr	SPM	35
WIDENED D EXPONENT	AV 1.45	GPM	300
FLUID LINE TEMPERATURE	38 °C	DP AN VEL	64 ft/min
SALT DENSITY	-	DC AN VEL	77 ft/min
SHALE FACTOR	-	CRITICAL VEL	-
MAX. FORMATION GAS	1 unit	PRESS(TOTAL)	1560
BACKGROUND GAS	1 unit	PRESS(BIT)	-
CONNECTION GAS	-	PRESS(SYSTEM)	-
TRIP GAS	13 units at 2409	BIT NOZ VEL	-
LITHOLOGY	MARL + MUDSTONE	HOLE VOL	1256
		AN. VOL	1038
		PIPE VOL	133
		PIPE DISPL.	85
		BIT TYPE	CORING
		JETS	CHRIS C20 8 ^{15%}
MUD WT. IN	9.6	AV. WOB	20,000 lbs
MUD WT. OUT	9.5	AV. RPM	85
ECD	9.8	AV. TORQUE	3500 ft lbs
ESTIMATED PORE PRESS	8.4	TIGHT HOLE	-
MAX. ESTIMATED PORE PRESS IN OPEN HOLE	8.5	FILL	-
ESTIMATED FRACTURE PRESS	16.5	Δ LAG	-
MIN. EST. FRACT. PRESS. IN OPEN HOLE	14.0	EST. SCAVINGS	-

COMMENTS: CORING FROM 2409.5 m
CORE BARREL JAMMED.
POOF TO RETRIEVE CORE. NO 2.

NOTES ON UNIT SAFETY FEATURES:-

- (1) AGITATOR MOTOR IS EXPLOSION PROOF FOR GASES WITH FLASH POINT > 280 °C.
- (2) OUTSIDE LINES CONNECTED TO POWER SUPPLY VIA SHUNT DIODE SAFETY BARRIERS

PETROLEUM ENGINEERING SUMMARY REPORT

COMPANY ESSO AUSTRALIA

WELL NAME FORTESCUE No 3

DATE 14 DEC 78

TIME 0600 HRS

DEPTH

2416 m

LAST REPORT DEPTH

2410.5 m

DRILL RATE	average	1.2 m hr
CORRECTED D EXPONENT	average	1.60
PIPELINE TEMPERATURE		36.0 °C
SHALE DENSITY		—
SHALE FACTOR		—
MAX. FORMATION GAS	6 units.	
BACKGROUND GAS	3 units	
CONNECTION GAS	—	
TRIP GAS	4 units at 2410.5m	
LITHOLOGY	<u>CALCAREOUS MUDSTONE</u>	
MUD WT. IN	9.6	PV/YP 19/22
MUD WT. OUT	9.6	CL - 2200
ECD	9.9	% SOLIDS 14
ESTIMATED PORE PRESS	8.4	
MAX. ESTIMATED PORE PRESS IN OPEN HOLE	8.5	
ESTIMATED FRACTURE PRESS	16.5	
MIN. EST. FRACT. PRESS. IN OPEN HOLE	14.0	

SPM	33 - 34
GPM	290
DP AN VEL	59 ft/min
DC AN VEL	76 ft/min
CRITICAL VEL	—
PRESS(TOTAL)	1600
PRESS(BIT)	—
PRESS(SYSTEM)	—
BIT NOZ VEL	—
HOLE VOL	1257 bbl
AN. VOL	10.39 bbl
PIPE CAP:	135 bbl.
PIPE DISPL.	83 bbl
BIT TYPE	C#3 CHRIS C20
JETS	coring
AV. WOB	20,000 lbs
AV. RPM	80
AV. TORQUE	4,000 ft/lbs
TIGHT HOLE	—
FILL	—
Δ LAG	—
EST. %CAVINGS	—

COMMENTS

RIH, CORE FROM 2410.5 TO 2416m (5.5m)
 Lost 200 psi PUMP PRESSURE AT 2413m.
 POOH at 2416m DUE TO WEATHER CONDITIONS.
 RETRIEVE CORE No 3 (1.5m, 28%)

TRIP AT 2410.5m : TRIP out, calc displacement 83 bbl, Actual 87 bbl
 TRIP in, calc displacement 83 bbl, Actual 109 bbl

TRIP AT 2416.0m : TRIP out, calc displacement 83 bbl, Actual 90 bbl.

PETROLEUM ENGINEERING SUMMARY REPORT

COMPANY ESSO AUSTRALIA

WELL NAME FORTESQUE No 3

DATE 15 DEC 78

TIME 06⁰⁰ HRS

DEPTH 2417 m

LAST REPORT DEPTH

2416 m

DRILL RATE	Average	1.0 m hr
CORRECTED D EXPONENT	Average	1.80
FLOWLINE TEMPERATURE		39.0 °C
SHALE DENSITY		-
SHALE FACTOR		-
MAX. FORMATION GAS	2 units	
BACKGROUND GAS	2 units	
CONNECTION GAS		
TRIP GAS	4 units on core 4, 2 units on core 5	
LITHOLOGY		<u>CALCAREOUS MUDSTONE</u>
MUD WT. IN	9.6	PV/YP 14/20
MUD WT. OUT	9.6	GL - 2600
ECD	9.9	SOLIDS 13
ESTIMATED PORE PRESS		8.4
MAX. ESTIMATED PORE PRESS IN OPEN HOLE	8.5	
ESTIMATED FRACTURE PRESS		16.5
MIN. EST. FRAC. PRESS. IN OPEN HOLE		14.0

SPM	34
GPM	290
DP AN VEL	59
DC AN VEL	76
CRITICAL VEL	-
PRESS(TOTAL)	1550
PRESS(BIT)	-
PRESS(SYSTEM)	-
BIT NOZ VEL	-
HOLE VOL	125T bbl
AN. VOL	1039 ₁₁
PIPE VOL	135 Capacity
PIPE DISPL.	83.
BIT TYPE	CHRIS C20
JETS	coning
AV. WOB	25 - 30,000 lbs
AV. RPM	50
AV. TORQUE	3,000 ft lbs
TIGHT HOLE	-
FILL	-
▲ LAG	-
EST. SCRIVINGS	-

COMMENTS: RIH with core No 4, would not drill, POTH, change BHA
 RIH with core no 5, Core 2416 - 2417m (core 1m, rec 0.1m 2C)
 RIH with Bit no 9 HTC XOG with 15/15/14 jets

TRIP AT 2416 m Trip IN with core 4 Calc disp 83 bbl Actual 70 bbl

TRIP AT 2416 m Trip OUT with core 4 Calc disp 83 Actual 73 } Overall

TRIP AT 2417 m Trip IN with core 5 Calc disp 83 Actual 68 } 5 bbl loss

TRIP AT 2417 m Trip OUT with cores 5 Calc disp 83 Actual 120

Trip IN with Bit 9 Calc disp 83 IN PROGRESS.

PETROLEUM ENGINEERING SUMMARY REPORT

COMPANY ESSO AUSTRALIA

WELL NAME FORTESCUE NO 3

DATE 16 DEC 78 TIME 05⁰⁰

DEPTH 2440 m LAST REPORT DEPTH 2417 m

DRILL RATE	<u>12 m/hr</u>
CORRECTED D EXPONENT	<u>1.12 - 1.66</u>
FLOWLINE TEMPERATURE	<u>42.3 °C</u>
SHALE DENSITY	<u>-</u>
SHALE FACTOR	<u>-</u>
MAX. FORMATION GAS	<u>30 units at 2440</u>
BACKGROUND GAS	<u>2 units</u>
CONNECTION GAS	<u>-</u>
TRIP GAS	<u>16 units</u>
LITHOLOGY	<u>calcareous mudstone + siltstone</u>

MUD WT. IN	<u>9.6</u>	PV/YP	<u>15/20</u>
MUD WT. OUT	<u>9.6</u>	CL.	<u>3600</u>
ECD		% SOLIDS	<u>13</u>
ESTIMATED PORE PRESS		AV. WOB	<u>47,000 ft-lb</u>
MAX. ESTIMATED PORE PRESS IN OPEN HOLE	<u>8.5</u>	AV. RPM	<u>112</u>
ESTIMATED FRACTURE PRESS	<u>16.5</u>	AV. TORQUE	<u>7,000 ft-lb</u>
MIN. EST. FRAC. PRESS. IN OPEN HOLE	<u>14.0</u>	TIGHT HOLE	<u>-</u>

SPM	<u>76</u>
GPM	<u>660</u>
DP AN VEL	<u>180 ft/min</u>
DC AN VEL	<u>129 ft/min</u>
CRITICAL VEL	<u>350 ft/min</u>
PRESS(TOTAL)	<u>3000</u>
PRESS(BIT)	<u>1577</u>
PRESS(SYSTEM)	<u>1423</u>
BIT NOZ VEL	<u>427 ft/sec</u>
HOLE VOL	<u>1267 bbl</u>
AN. VOL	<u>1045 bbl</u>
PIPE VOL	<u>136 bbl cu</u>
PIPE DISPL.	<u>86 bbl</u>
BIT TYPE	<u>BN 9 HTC XDG</u>
JETS	<u>15 15 14</u>
AV. WOB	<u>47,000 ft-lb</u>
AV. RPM	<u>112</u>
AV. TORQUE	<u>7,000 ft-lb</u>
FILL	<u>-</u>
Δ LAG	<u>-</u>
EST. % SAVINGS	<u>-</u>

COMMENTS: Bit No 9, Drill 2417 to 2440 m, POUH to core
RIH w/ core # 6, Circ B.U. prior to coring.

TRIP AT 2440m Trip out w/ Bit 9 Calc 86 bbl Actual 100 bbl
Trip in w/ core 6 Calc 83 bbl Actual 85 bbl

PETROLEUM ENGINEERING SUMMARY REPORT

COMPANY

ESSO AUSTRALIA

WELL NAME

FORTESCUE No 3

DATE

17 DEC 78

TIME

06⁰⁰ HRS

DEPTH

2470 m LAST REPORT DEPTH

2440 m

DRILL RATE

5.0 m/hr average

CORRECTED D EXPONENT

1.17 - 1.68

FLOWLINE TEMPERATURE

44.8°C

SHALE DENSITY

-

SHALE FACTOR

-

MAX. FORMATION GAS

1 mi.t

BACKGROUND GAS

1 mi.t

CONNECTION GAS

-

TRIP GAS

12 units at 2440

LITHOLOGY:

2 units at 2456

SANDSTONE w/ SHALE

SPM

32

GPM

280

DP AN VEL

54

DC AN VEL

76

CRITICAL VEL

-

PRESS(TOTAL)

1550

PRESS(BIT)

-

PRESS(SYSTEM)

-

BIT NOZ VEL

-

HOLE VOL

1277 bbl

AN. VOL

1059 bbl

PIPE VOL

138 bbl

PIPE DISPL.

80 bbl

BIT TYPE

CHRIS C22

— coring

JETS

22 - 24

MUD WT. IN

9.6

PV/YP

16/20

MUD WT. OUT

9.6

CL

3900

ECD

9.8 - 9.9

% SOLIDS

13

TIGHT HOLE

—

FILL

—

LAG

—

EST. % CAVINGS

—

COMMENTS:

CORE No 6 2440 - 2456 Rec 11.4 m 71%

CORE No 7 2456 - 2470 Rec 9.0 m 64%

RIH w/ CB # 8

TRIP AT 2456m { POOH w/ core No 6 Calc 80 bbl Actual 81 bbl

{ RIH w/ core No 7 Calc 80 bbl Actual 75 bbl

TRIP AT 2470m { POOH w/ core No 7 Calc 80 bbl Actual 80 bbl

{ RIH w/ core No 8 Calc 80 bbl Actual 84 bbl

PETROLEUM ENGINEERING SUMMARY REPORT

COMPANY ESSO AUSTRALIA

WELL NAME FORTESCUE No 3

DATE 18 DEC 78

TIME 06⁰⁰

DEPTH 2519

LAST REPORT DEPTH

2470 m

DRILL RATE 10 - 15 m/hr (25) m/h
 CORRECTED D EXPONENT 1.0
 FLOWLINE TEMPERATURE 42 °C
 SHALE DENSITY -
 SHALE FACTOR -
 MAX. FORMATION GAS 3 mits 2483
 BACKGROUND GAS 2 mits.
 CONNECTION GAS 5 units at 2470m (coning)
 TRIP GAS 15 units at 2470m (reaming)
 LITHOLOGY: SANDSTONE w/ SHALE

SPM 74
 GPM 640
 DP AN VEL 125
 DC AN VEL 174
 CRITICAL VEL 351
 PRESS(TOTAL) 2800
 PRESS(BIT) 1475
 PRESS(SYSTEM) 1325
 BIT NOZ VEL 414 ft/sec
 HOLE VOL 1304 bbl
 AN. VOL 1077 bbl
 PIPE VOL 141 cu bbl
 PIPE DISPL. 86 bbl
 BIT TYPE HTC XDG

JETS	<u>15 15 14</u>
AV. WOB	<u>35,000 lbs</u>
AV. RPM	<u>100</u>
AV. TORQUE	<u>7,000 ft lbs</u>
TIGHT HOLE	<u>-</u>
FILL	<u>-</u>
Δ LAG	<u>-</u>
EST. SAVINGS	<u>-</u>

MUD WT. IN	<u>9.7</u>	PV/YP <u>15/20</u>
MUD WT. OUT	<u>9.8</u>	GL <u>4200</u>
ECD	<u>10.0</u>	% SOLIDS <u>13</u>
ESTIMATED PORE PRESS	<u>8.5</u>	
MAX. ESTIMATED PORE PRESS IN OPEN HOLE	<u>8.5</u>	
ESTIMATED FRACTURE PRESS	<u>16.5</u>	
MIN. EST. FRACT. PRESS. IN OPEN HOLE	<u>14.0</u>	

COMMENTS: CORE No 8 2470 - 2480 m Rec: 0 m

RIH w/ RR#9 HTC XDG Reram out rat hole.

Drill 2480m - 2483m Circ B.U. max gas 3 units

Drilling 2483 to 2519m

TRIP AT 2480m TRIP out w/ core 8 Calc: 81 bbl Actual 85 bbl

TRIP IN w/ BIT RR9 Calc: 86 bbl Actual 66 bbl

PETROLEUM ENGINEERING SUMMARY REPORT

COMPANY

ESSO AUSTRALIA

WELL NAME

FORTESCUE No 3

DATE

19 DEC 78

TIME

06⁰⁰ HRS

DEPTH

2625 m

LAST REPORT DEPTH

2519 m.

DRILL RATE	<u>Av 12.5 m hr</u>
CORRECTED D EXPONENT	<u>0.93 - 1.53</u>
FLOWLINE TEMPERATURE	<u>46 °C</u>
SHALE DENSITY	<u>-</u>
SHALE FACTOR	<u>-</u>
MAX. FORMATION GAS	<u>3 units</u>
BACKGROUND GAS	<u>2 units</u>
CONNECTION GAS	<u>-</u>
TRIP GAS	<u>10 units on wiper trip</u>
LITHOLOGY	<u>SANDSTONE /COAL/ SH.</u>
MUD WT. IN	<u>9.9</u>
MUD WT. OUT	<u>9.8</u>
ECD	<u>10.1</u>
ESTIMATED FROE PRESS.	<u>8.5</u>
MAX. ESTIMATED FROE PRESS. IN OPEN HOLE	<u>8.5</u>
ESTIMATED FRACTURE PRESS.	<u>17.0</u>
MIN. EST. FROE PRESS. IN OPEN HOLE	<u>14.0</u>

SPM	<u>74</u>
BPM	<u>640</u>
BP AN VEL	<u>125 ft/min</u>
DC AN VEL	<u>174 ft/min</u>
CRITICAL VEL	<u>356 ft/min</u>
PRESS(TOTAL)	<u>2860</u>
PRESS(BIT)	<u>1521</u>
PRESS(SYSTEM)	<u>1339</u>
BIT NOZ VEL	<u>414 ft/sec</u>
HOLE VOL	<u>1355 bbl</u>
AN. VOL	<u>1119 bbl</u>
PIPE VOL	<u>147 bbl</u>
PIPE DISPL.	<u>89 bbl</u>
BIT TYPE	<u>RR9 HTC XD</u>
DETS	<u>15, 15, 14</u>
AV. MDP	<u>35,000 lbs</u>
AV. RPM	<u>110</u>
AV. TORQUE	<u>5,000 lbs</u>
TIGHT HOLE	<u>-</u>
FILL	<u>-</u>
A LAT	<u>+ 500 ft</u>
EXT. REVENGE	<u>-</u>

Comments:

Drill 2519 m - 2625 m
wiper trip then POTH directional survey
Running pipeline logs.

TRIP AT 2625m Trip out w/ Bit 9 Calc: 89 bbl
Actual 115 bbl



EXPLORATION LOGGING INTERNATIONAL INC.

A Geological-Engineering Service

APARTADO 650, PANAMA, REPUBLIC OF PANAMA

2006, ORCHARD TOWERS, 400, ORCHARD ROAD, SINGAPORE 9.
TELEPHONE: 2354544 (4 LINES) TELEX RS 21084

ESSO AUSTRALIA LTD., FORTESCUE NO.3
EXPLORATION LOGGING, UNIT 101, OCEAN DIGGER.
WEEKLY REPORT NO.1 : 0 - 893 METRES

DRILLING SUMMARY

THE RIG MOVED ON LOCATION ON THE 26/11/78 AND RAN ANCHORS. THE WELL SPUNDED THE SAME DAY, DRILLING WITH NO RETURNS WITH A $17\frac{1}{2}$ " BIT AND 26" HOLE OPENER. AT 244 METRES THE BIT WAS PULLED AND 20" CASING RUN AND CEMENTED WITH THE SHOE AT 225 METRES. A SURVEY AT T.D. SHOWED HOLE ANGLE TO BE 10° .

THE 20" SHOE WAS DRILLED OUT WITH A $17\frac{1}{2}$ " OSC 3AJ BIT USING SEAWATER TO 260 METRES WHERE THE CHANGEOVER TO 8.9PPG MUD WAS MADE. T.D FOR THE $17\frac{1}{2}$ " HOLE WAS AT 878 METRES AND THE BIT WAS PULLED TO RUN LOGS AND CASING.

A WIPER TRIP WAS MADE AND SCHLUMBERGER ISF/SONIC AND FDC/GR LOGS WERE RUN TO T.D. FOLLOWING CONDITIONING OF THE MUD TO REDUCE WATER LOSS, $13\frac{3}{8}$ " CASING WAS RUN TO 867 M WHERE THE SHOE WAS CEMENTED.

DRILLING CONTINUED WITH A $12\frac{1}{4}$ " X1G BIT AND AT 893M A PRESSURE INTEGRITY TEST WAS CARRIED OUT TO 13.7PPG EMW DRILLING CONTINUES.

DRILLING PARAMETERS

LITHOLOGY: FIRST SAMPLES TO SURFACE WERE CALCARENITE WITH ABUNDANT SHELL FRAGMENTS AND MICROFOSSILS. AROUND 550 METRES A MORE ARGILLACEOUS MATERIAL APPEARED, MARL OR CALCILUTITE. THE CALCARENITE BECAME A FINER CALCISILTITE AND THIS WAS QUITE UNIFORM DOWN TO CASING POINT.

DRILL RATES: DRILL RATES OF 300-400 M/HR WERE RECORDED IN THE TOPMOST SECTION OF THE HOLE DROPPING TO AN AVERAGE OF 100 M/HR FOR THE FIRST 300 METRES. THE RATE SLOWED THEN TO 60 M/HR IN THE CLAYEY SECTION AROUND 550 METRES AND PICKED UP SLIGHTLY IN THE CALCISILTITE. DRILL RATES DROPPED OFF TOWARDS THE CASING POINT WITH AVERAGES AROUND 20 M/HR. THIS WAS SLOWER THAN IN THE FORTESCUE NO.2 WELL.



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DRILLING EXPONENT : A GOOD TREND WAS ESTABLISHED AS DRILL RATES BEHAVED IN ACCORDANCE WITH THE COMPACTION TREND OF THE LITHOLOGIES .NORMAL GRADIENT OF 8.4 PPG E&M.W. IS TAKEN FOR THIS AREA.

GAS : GAS READINGS WERE NEGLIGIBLE DOWN TO 400 METRES WHERE A BACKGROUND OF 5-6 UNITS APPEARED.HIGHEST READINGS WERE 24 UNITS AGAINST A GENERAL BACKGROUND OF 10 UNITS.METHANE AND SLIGHT TRACES OF ETHANE WERE DETECTED.

TEMPERATURE : A VERY STEADY AND SLOW INCREASE IN FLOWLINE TEMPERATURE WAS RECORDED WITH NO APPARENT ANOMALIES.

HIGHEST TEMPERATURE RECORDED WAS 28°C AT 878 METRES.

HOLE CONDITIONS: ON THE FINAL TRIP FOR THE LOGGING SOME OVERPULL WAS EXPERIENCED.THE CALIPER LOG SHOWED VERY LITTLE WASHOUT OF THE HOLE AND NO PROBLEMS WERE EXPERIENCED WITH RUNNING OF THE LOGGING TOOLS TO BOTTOM.CARBIDES RUN IN THIS SECTION INDICATED GOOD HOLE CONDITION.



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2006, ORCHARD TOWERS, 400, ORCHARD ROAD, SINGAPORE 9.
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WEEKLY REPORT #2: DEC. 1ST TO DEC. 8TH 1978
ESSO AUSTRALIA LIMITED. FORTESCUE NO.3
EXPLORATION LOGGING UNIT 101, THE OCEAN DIGGER.
DEPTH INTERVAL: 893 TO 1600 METRES.

DRILLING SUMMARY

NB#3 A HTC X3A WAS USED TO DRILL OUT THE 13 3/8" CASING SHOE AND 12 1/4" HOLE TO 1271 METRES. THE BIT WAS THEN REPLACED WITH NB#4 ALSO A HTC X3A AND THIS BIT DRILLED TO 1343 METRES. DURING THIS BIT RUN PUMP NUMBER 2 BROKE DOWN SO DOWN TO 1481 METRES ONLY ONE PUMP WAS USED ON THE HOLE. AT 1481 METRES THE PUMP WAS REPAIRED AND BOTH PUMPS WERE USED ON THE HOLE. AT 1508 METRES IT WAS DECIDED TO PULL THE BIT. ON THE TRIP OUT TIGHT HOLE WAS EXPERIENCED UP TO 1050 METRES AND IT WAS FOUND THAT THE HOLE WAS NOT TAKING ANY MUD OR FILL UP. RAN BACK TO BOTTOM AND CIRCULATED WITH HIGH VISCOSITY MUD. PULLED OUT OF THE HOLE WITH NO FURTHER PROBLEMS AND RAN BACK WITH NB#5 ANOTHER HTC X3A. A GAS SHOW OF 2000 UNITS OCCURED AT 1526 METRES. DRILLING WAS STOPPED AND RETURNS CIRCULATED AT 1536 METRES. CHROMATAGRAPH ANALYSIS INDICATED THAT THE GAS WAS MAINLY METHANE WITH MINOR TRACES OF HEAVIER HYDROCARBONS THROUH TO C4. THE MUD WEIGHT WAS RAISED TO 9.6 LB/GAL AND THE MUD CONDITIONED PRIOR TO COMING OUT OF THE HOLE FOR THE CORE BARREL. CORE #1 WAS THEN CUT, FROM 1536 TO 1548.6 METRES, USING A CHRIS C20 CORE BIT. RECOVERY WAS 100% AND NO HYDROCARBON SHOWS WERE DISCOVERED IN THE CORE WHICH CONSISTED OF MARL. NB#6 ANOTHER HTC X3A WAS RUN BACK IN THE HOLE AND THIS DRILLED TO 1600 METRES BEFORE PROBLEMS WITH THE STACK CAUSED DRILLING OPERATIONS TO BE STOPPED. AT PRESENT WE ARE OUT OF THE HOLE AND WAITING ON THE DIVERS TO COMPLETE REPAIRS TO THE STACK.

DRILLING PARAMETERS

LITHOLOGY: THIS HAS CONSISTED OF A SEQUENCE OF CALCISILTITES, CALCAREOUS MUDSTONES AND MARL. OVER THE INTERVAL DRILL RATES VARIED FROM 100 TO 8 METRES PER HOUR. THE FASTER RATES OCCURRING BETWEEN 893 AND 1350 METRES. BELOW 1350 METRES DRILL RATE DROPPED OFF TO AN AVERAGE OF 12 METRES PER HOUR.

GAS: BACK GROUND GAS VARIED FROM 4 TO 20 UNITS WITH A SHOW OF 2000 UNITS AT 1526 METRES. A DRILLING BREAK FROM 13 METRES PER HOUR TO 21 METRES PER HOUR COINCIDES WITH THE GAS SHOW. UNFORTUNATELY EXAMINATION OF CUTTINGS FROM THE INTERVAL DID NOT SHOW ANY REASON FOR THE HIGH



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GAS READINGS, NOR WERE ANY OTHER ANOMOLOUS READINGS RECORDED WHILST CUTTING CORE #1. THE POSSIBILITY THAT THE SHOW WAS CAUSED BY HERETO UNKNOWN SURFACE ACTIVITIES CANNOT BE DISCOUNTED ON PRESENT EVIDENCE.

PRESSURE INDICATORS:

DRILLING EXPONENT: THE PLOT OF THE D_{xc} DOES NOT SHOW ANY ANOMOLOUS TRENDS. HOWEVER A NORMAL COMPACTION TREND IS READILY APPARENT. UNFORTUNATELY THE ABSENCE OF CLEAN SHALES PRECLUDES ANY QUANTITATIVE ANALYSIS.

GAS: NO CONNECTION GASES OR ABNORMALY HIGH TRIP GASES HAVE OCCURRED. A READING OF 2000 UNITS WAS OBTAINED FROM 1526 METRES BUT IT IS SUSPECTED THAT THIS MAY HAVE BEEN CAUSED BY SURFACE ACTIVITY.

TEMPERATURE: THIS SHOWS A NORMAL TREND TO 1270 METRES. FROM 1270 TO 1475 METRES THERE IS AN APPARENT REVERSAL IN TREND. THIS IS BELIEVED TO HAVE BEEN CAUSED BY THE ADDITION OF WATER AND CHEMICALS TO THE MUD SYSTEM. BELOW 1475 METRES A NORMAL TREND AGAIN BECOMES ESTABLISHED.

HOLE CONDITION: TIGHT HOLE WAS EXPERIENCED ON THE TRIP OUT AT 1508 METRES. APART FROM THIS THE HOLE IS BELIEVED TO BE IN GOOD CONDITION AND CARBIDES HAVE GIVEN A LAG NOT EXCEEDING THE THEORETICAL LAG BY MORE THAN 100 STROKE UNFORTUNATELY WE HAVE NOW BEEN OUT OF THE HOLE FOR 3 DAYS AND IT REMAINS TO BE SEEN WHETHER OR NOT THE HOLE CONDITION WILL HAVE DETERIORATED DURING THIS TIME.

PORE PRESSURE: IT IS BELIEVED THAT PORE PRESSURE IS 8.4 TO 8.5 LB/GAL

HOWEVER THE AS YET UNEXPLAINED GAS SHOW AT 1526 METRES INDICATES THAT CAUTION BE EXERCISED.

БОЛАРГУЛ СЕНАЛ ГАСЫЛТЫК ТО ОТВЕЧАДЫ, КИТАС ОК НОГДАН МОРЫ

ДЕРІГІЛІСІЛДІРДІ ОЛ 2016 ІЧІНІ БЕЛАРГАЛ НЕМІЗЕМДЕСІМДІК ЗЕРТІЛІК

А НІҢІЛІТ МОНГІРДІ ТА, БЕТАНІМЕСІДІН ҚАЗАНАН БУДЫРАЛ

ЭНІ, САЛМАРАСЫН, ҮЗДІЛІСІРІН, БАСЫРЫН, АЗЫРЫНДЫРЫЛЫП БАУ БІЛЕТЕЛ

ОЛ, НӨДЕГІ, АУЫЛ, ӘМА, ҚАСАДАСЫН МЕСЕДІР, МОДАС, 1999 ИНДІСІНДА АТЫС

А ҚАДЫМДАРЫНЫҢ, ОДАЛЫҚ, БАСЫРЫН, АЗЫРЫНДЫРЫЛЫП ТОЛЫК

МОДАС, ЖАҢЫНА ОЛ СМЕДДОРЫ, ҮЛДІССІРДІМ СУМ, ОНА САЙЫС



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WEEKLY REPORT # 3 DEC 8 TO DEC 15 1978
ESSO AUSTRALIA LTD, FORTESCUE #3
EXPLORATION LOGGING, UNIT 101 OCEAN DIGGER
DEPTH INTERVAL: 1600M TO 2417M

DRILLING SUMMARY

DRILLING RESUMED ON 9 DEC AFTER REPAIRS TO THE BOP'S WERE SUCCESSFUL. BIT #7, AN HTC X3A 12 $\frac{1}{2}$ " WITH 18,18,20 JETS DRILLED FROM 1600M TO 2052M AT AN AVERAGE PENETRATION RATE OF 17M/HR, USING AN AVERAGE BIT WEIGHT OF 50,000 LBS AND AN RPM OF 120. ANOTHER X3A DRILLED TO 2409.5M AND WAS PULLED DUE TO A SIEZED CONE. THIS BIT AVERAGED 19M/HR. TRIP GAS AT 1600M WAS 180 UNITS, AND 100UNITS AT 2052M. MUD WEIGHTS USED THROUGHOUT THE WHOLE INTERVAL AVERAGED 9.3 TO 9.6 PPG. CORE #2 WAS CUT WITH AN 8 15/32" CHRIS C20 BIT FROM 2409.5M TO 2410.5M. THE CORE WAS PULLED AFTER ONE METRE DUE TO THE JAMMING OF THE BIT. 40CM WAS RECOVERED. AVERAGE RATE OF PENETRATION WAS 2.5 M/HR, USING 20,000 LBS WEIGHT AND 85 RPM. TRIP GAS AT 2409.5 M WAS 4 UNITS. CORE #3 WAS CUT FROM 2410.5M TO 2416M. 200 PSI PUMP PRESSURE WAS LOST AT 2413M. THE CORE WAS PULLED AT 2416M DUE TO DETERIORATING WEATHER CONDITIONS. 1.5 M WAS RECOVERED, 27%. CORE #4 WAS RUN IN TO BOTTOM, BUT THE BIT JAMMED BEFORE ANY CORE WAS CUT, TRIP GAS WAS 4 UNITS. THE CORE BARREL WAS PULLED OUT AND RUN BACK AFTER CHANGING THE BHA, TRIP GAS WAS 2 UNITS. CORE #5 WAS CUT FROM 2416M TO 2417M AND WAS PULLED DUE TO THE BIT BEING IN A JAMMING. 10 CM OF CALCAREOUS MUDSTONE WAS RECOVERED. THE CURRENT OPERATION IS DRILLING WITH BIT #9, AN HTC XDG 12 $\frac{1}{2}$ " BIT WITH 15,15,14 JETS.

LITHOLOGY

THE SECTION FROM 1600M TO 2417M CONSISTS OF TYPICAL LAKES ENTRANCE FORMATION: CALCAREOUS MUDSTONES WITH SPORADIC INTERBEDS OF CALCISILTITE BELOW 2300M CALCAREOUS SHALES PREDOMINATED. AT 1730M TO 1750M A CRYSTALLINE LIMESTONE WAS DRILLED: THIS PROBABLY REPRESENTED THE "HIGH VELOCITY CHANNEL". FROM 1759M TO 1762M AND FROM 1766M TO 1767 M A VERY SOFT HYGROTURCID CLAY WAS DRILLED, WHICH PRODUCED A VOLUME OF CAVINGS AND MUD VISCOSITY PROBLEMS TO APPROX 2100M.



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DRILLING EXPONENT

THE DXC PLOT IS REPRESENTATIVE OF A NORMAL COMPACTION TREND IN THIS INTERVAL. IF MINOR VARIATIONS DUE TO SLIGHT LITHOLOGICAL CHANGES ARE CORRECTLY INTERPRETED, THEN IT CAN BE SEEN THAT THE TREND IS REFLECTIVE OF A NORMAL PORE PRESSURE GRADIENT OF APPROX 8.5 PPG.

GAS

AVERAGE BACKGROUND GAS THROUGHOUT THE INTERVAL AVERAGED 4 UNITS AND NEVER ROSE ABOVE 10 UNITS. NO CONNECTION GASSES WERE DETECTED. THE LARGE TRIP GAS AT 1600M WAS DUE TO THE LENGTH OF TIME SPENT OUT OF THE HOLE WHILE REPAIRING THE STACK AND WAITING ON WEATHER.

TEMPERATURE

AFTER INTERPRETATION DUE TO SURFACE ACTIVITIES IT APPEARS THAT THE ESTABLISHED REGIONAL TREND OF 1.12°C IS CONTINUING, THE MAXIMUM TEMPERATURE RECORDED WAS 47.5°C AT 2400M.

HOLE CONDITION

CARBIDE LAG TIMES INDICATE THAT THE AVERAGE OPEN HOLE GUAGE IS VERY CLOSE TO $12\frac{1}{4}^{\text{in}}$. ALL TRIPS RAN SMOOTHLY WITH AN ABSENCE OF ANY INDICATION OF SIGNIFICANT DRAG.

PORE PRESSURE

ESTIMATED TO CONTINUE AT A NORMAL 8.5 PPG EQUIVALENT MUD WEIGHT.

DAINES/NOLAN

Plans