

ESSO AUSTRALIA LTD. BARRACOUTA # 4 EXTENDED SERVICE WELL REPOR

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ENCLOSURE 6

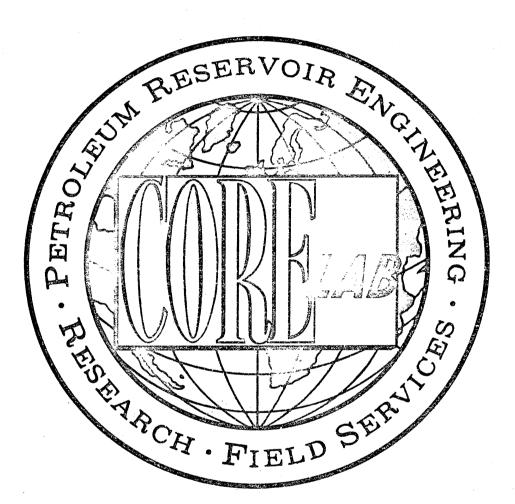
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EXTENDED SERVICE

ESSO AUSTRALIA, LTD., BARRACOUTA # 4 EXTENDED SERVICE WELL REPORT





CORE LABORATORIES INTERNATIONAL LTD.

24A, LIM TECK BOO ROAD. SINGAPORE 19. TELEPHONE:2821222; CABLE: CORELAB; TELEX: RS21423.

CORE LABORATORIES INTERNATIONAL LTD.

Petroleum Reservoir Engineering SINGAPORE

REPLY TO: 24-A. LIM TECK BOO ROAD. SINGAPORE. 19. CABLE: CORELAB TELEPHONE: 2821222. 2821587 TELEX: CORELAB RS 21423

20th MAY 1977

ESSO AUSTRALIA, LTD., P.O. BOX 372, SALE, 3850 VICTORIA. AUSTRALIA.

ATTENTION MR. L.D. ATTAWAY.

Dear Sir,

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Accompanying this well summary report, for your inspection and referance, are all logs and relavent data (computer recorded) pertaining to the drilling and activities of BARRACOUTA # 4. If you have any queries or suggestions on the presentation of this well report and data found within, do not hesitate to contact us.

CORE LABORATORIES appreciates being of special assistance to ESSO AUSTRALIA during the entire drilling operations of BARRACOUTA # 4 and look forward to our continuing association on future exploratory work in Australia.

Yours Sincerely

S. La Groma.

S.R. LA ROSA (UNIT SUPERVISOR)

UNITED STATES . CANADA . SOUTH AMERICA . EUROPE . AFRICA . ASIA . AUSTRALIA

BARRACOUTA # 4 was drilled by ESSO AUSTRALIA in the Gippsland Basin of the Bass Strait. The development well was drilled by ODECO's semi-submersible drilling rig, Ocean Endeavour. The well was spudded in a water depth of 153' on the 30th. of March 1977 and total depth of 4783' was reached at 1305 hours on the 22nd. of April 1977. '

Well location co-ordinates being :-

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•				20, 789"	
Latitude	:	38	17'	21.667" S 03, 194" 4.015" E	
Longitude	:	147 ⁰	42'	4.015" E	

A Core Laboratories Extended Services fully integrated computer unit (with back-up facilities) was located on board the Ocean Endeavour to monitor all drilling parameters below 20" casing depth. All computer data found within this report is stored on magnetic tape and can be retrieved at any time, at the request of the client.

The Core Laboratories well site crew consisted of the following :-

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Unit: Supervisor	-	Sal La Rosa
E.S. Engineer	·	Mike Warner
E.S. Engineer	. –	Ingolf Hansen
Mud Loggers	-	Joseph Greener
	•	David Gilbert
		Ron Wigham



CORE LABORATORIES EXTENDED SERVICE EQUIPMENT

A. MUDLOGGING

- 1 Hot Wire Gas Detector.
- 1 Total FID Gas Chromatograph.
- 1 FID Chromatograph.
- 1 Carbon Dioxide Detector.
- · 1 Hydrogen Sulphide Detector.
 - 1 Cutting Gas Analyser.
 - 1 Shale Density Apparatus.
 - 1 Thermal Extractor (Steam Still).
- 1 U-V Light, Microscope & Other Geological Testing Equipment.
- 6 Chart Recorders For All Drilling Parameters.

B. CORE ANALYSING

- 1 Complete On-Site Core Analysis Equipment For Porosity, Permeability & Fluid Saturation Measurements.
- 1 Core Slabbing Saw.
- C. COMPUTER SYSTEM & PERIPHERALS
 - 2 Hewlett Packard 2100A Computers.
 - 2 Texas Instruments Keyboard-Send Receive Units.
 - 3 Computer Digital Displays.
 - 2 Hewlett Packard 7210A Plotters.
 - 4 Linc Tape Magnetic Recorders.
 - 1 Hewlett Packard HP65 Programmable Calculator.

D.

- EXTERNAL SENSING APPARATUS INCLUDED
- 2 Mud Density Sensors.
- 2 Mud Temperature Sensors.
- 2 Mud Resistivity Sensors.
- 1 Rotary Speed Sensor.
- 1 Hookload Sensor.
- 1 Rotary Torque Sensor.
- 1 Pump Pressure Sensor.
- 1 Casing Pressure Sensor.
- 1 Mud Flow Out Sensor.
- 1 Gas Trap.
- 1 Depth & Rate Of Penetration Sensor.
- 2 Pump Stroke Counters.
- 3 Pit Level Sensors.
- 1 Trip Tank Level Sensor.
- 1 Six-Extension Intercom System.

E. PRESSURE TESTING EQUIPMENT

1 Hewlett Packard 2811B Quartz Pressure Gauge System.

BORATORIES

RIG DESCRIPTION

The Ocean Endeavour is a self-propelled octagonal shaped semi-submersible drilling rig, constructed for Ocean Drilling & Exploration Company by Transfield (WA) Pty. Ltd., Perth, Western Australia.

The unit is 320' long, 266' wide with 7,000 HP twin screw diesel electric propulsion. The hull consists of four parallel pontoons, each measuring 28' in diameter. Four 12" diameter and eight 24" diameter stabilising columns are connected to the four pontoons. The tops of the columns which support the main deck of the rig are 120' from the base of the pontoons. The unit has capabilities of drilling at 70' draft in water depths up to 1,000'. The Ocean Endeavour is designed to withstand waves up to 110' with 15 seconds periods, simultaneously with 3 knot current and 100 knot winds and still remain within the American Bureau of Shipping allowable stress levels.

RIG EQUIPMENT

- 1 Lee C. Moore 40' x 40' x 162' Cantilever Mast rated 1,400,000 API GNC.
- 1 Continental-Emsco C-3 Type 2 Drawworks grooved for 1.375" line, V-200 Parmac Hydromatic Brake, Emsco Catheads, Sandreel Assembly mounted on Drawworks, driven by three 1,000 HP DC Motors.
- 1 Continental-Emsco 37.5" Rotary Driven by 1,000 HP . DC Motor with 2 speed transmission.
- 1 Continental-Emsco RA-60-6-1.375" Traveling Block, rated 650 ton.



- 1 Continental-Emsco 650 ton Swivel, L650.
- 1 Bryon-Jackson Hydrahook, rated 500 ton.
- 1 Lee C. Moore 6-60" Sheave Crown, 1-60" Fast Line Sheave.
- 1 Koomey Accumulator, 320 gallon, 3,000 PSI W.P., with electric Master and Remote Panels.
- 1 18.75" 5,000 PSI Cameron BOP System with 600' 22"
- Vetco Marine Riser.
- 4 Riser Tensioners, 80,000 lbs. units.
- 1 Motion Compensator, Rucker 400,000 lbs.
- 2 Continental-Emsco FA-1300 Triplex Pumps, 6.5" x 12", driven by 1,300 HP DC Motor, each supercharged with a 5" x 6" Mission Centrifugal Pump.
- 1 Sub-Sea Television System.
- 2 Mission 6x 8R, H30 Centrifugal Mud Mix Pumps with 10.5" Impellers and 100 HP AC Motors.
- 3 Milchem Triple RVS-96 Shale Shakers.

10,000' 5" O.D. 19.5 lbs./ft., Grade E Drill Pipe.

5,000' 5" 0.D. 19.5 lbs./ft., G-105 Drill Pipe.

30 8" O.D. Drill Collars.

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24 6.5" O.D. Spiral Drill Collars.

- 2 Favco Cranes with 120' Booms, rated 40 tons at 30' radius and 23 tons at 90' radius.
- 1 Halliburton HT 400 Cement Unit, Pioneer T-16-4 Desilter, Pioneer T-10-6 Desander, Pit-0-Graph and Swaco Degasser.
- 8 Clarke Chapman 1 Drum Electric Anchor Windlasses, each with one 1,000 HP DC Motors, rated 440,000 lbs. pull.
- 8 30,000 lbs. LWT Anchors with 3,600' of 3" Steel Link Anchor Chain.



1 International Electric Corporation Offshore Technology Corporation, Adaptive Oceanography Data Reporting System for monitoring and recording, with Hole Position Indicator Recorder and Riser Angle Indicator Recorder.

CORE LABORATORIES

INC

STORAGE CAPACITY

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Fuel	-	6,972 bbls.
Drill Water	-	14,320 bbls.
Potable Water	-	385 bbls.
Dry Mud		140 s. tons.
Bulk Mud & Cement		9,600 cu.ft.
Liquid Mud	600	1,344 bbls.
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DESCRIPTION OF LOGS

Core Laboratories Extended Service Package includes sensors, recorders and computer facilities useful in the prediction and measurement of abnormal formation pressures and in obtaining rapid, effective and safe drilling. In addition to plots of variables important for pressure detection and drilling optimisation there are available wireline log interpretation programs for the wellsite geologist, well bore hydraulics (synthesis and analysis), well kill, bit nozzle selection, swab and surge created by drill pipe movement, drill bit performance programmes for the wellsite drilling supervisors. As there are two computer systems on board, these programmes can be run while the main computer system is in the real-time drilling mode.

The E.S. Logs include the following: E.S. Drill Log - Scale 1:6000

Information plotted on this log includes rate of penetration, 'd' exponent corrected for mud weights, total mud gas as measured by the hot wire detector, shale density of drilled cuttings, casing depth, bit runs, dates and other relevant drilling information. Both rate of penetration and total gas are plotted on a semi log scale and shale density on a linear scale. The 'd' exponent is the primary overpressure detection plot. Corrected 'd' exponent, 'dcs' is rate of penetration normalised for rotary speed, weight on bit per inch of diameter and mud weight. The modification of 'dcs' was first implemented by Rhem & McClendon, to compensate for increases in mud weight. This particular procedure involves multiplying the standard 'd' exponent value by the

inverse ratio of the mud weight increase. A multiplier of nine (9) was originally used for convenience to return the magnitude of the 'dcs' to a comparable value of its uncorrected state. In Core Lab's real-time drilling programmes a multiplier of ten (10) is used. An overlay is used on the 'dcs' to give a quantitative measurement of formation pore pressure. This method of pore pressure prediction is very accurate for homogenous shales but where the sandstone/siltstone ratio varies a great deal, inaccuracies may occur, consequently all other variables are considered in assigning a value to pore pressure.

E.S. Temperature Log

The three variables on the Core Laboratories E.S. temperature log are:-

- 1. Temperature differential between suction and flowline drilling fluids, is on the left of the E.S. log.
- 2. Flowline temperature is the middle plot.
- 3. The end to end normalised flowline temperature is on the right of the log.

The temperature differential plot or delta T plot emphasizes changes in flowline temperature caused by surface effects such as mud addition or cooling during trips. Accompanying the plot are notations identifying the causes for temperature irregularities. The flowline temperature plot illustrates the change in flowline temperature during a bit run. Each bit run is labelled and the temperatures are logged to correspond to mud circulated from the bottom as the foot was cut. There are also notations to explain accountable



variations. The end to end normalised flowline temperature plot is the principle interpretive plot. The information from the other two plots are taken into account, normalised and plotted as one continuous bit run. The flowline temperature is normalised for an annular velocity of 100 ft./ minute and a hole of constant diameter. There is also a compensation for specific changes in temperature of the drilling fluid. This factor is obtained by the implications of changes in surface dissipation of heat. For example, if the flowline mud temperature at the surface is reduced by a stabilised 30°F. then chemicals are added to the mud system, the temperature of the same quantity of mud is reduced only 15°F. for the same initial flowline temperature and the same pit volume then the specific heat has changed by a In this manner the correction for chemicals factor of two. added can be accounted for from bit run to bit run as long as initial conditions are kept constant, including the same initial suction pit temperature at the start of the bit run. Along with this plot are temperatures from Schlumberger electric log runs, the time after circulation and depth. When two or more points are available, there is projected bottomhole temperature obtained using inverse time versus log temperature plots, when bottomhole temperature is the temperature corresponding to the logrithmic value at 1/Time = 0.

E.S. Pressure Log

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Information plotted on this log includes formation pore pressure, E.C.D. (equivalent circulating density) and formation fracture pressure. The formation pore pressure

plotted on this log is estimated from all formation pressure indicators. This is a conclusion log, therefore plotted data may well be modified on results from formation breakdown tests (PIT Tests), FIT's or DST's. The E.S. pressure log is the best estimation of downhole formation pressure conditions by the Core Lab well-site E.S. Engineer, based upon all relevant well data processed throughout the well drilling operations. This log is plotted on linear graph paper at a vertical scale of 1:6,000 to coincide with all other E.S. logs.

E.S. Geoplot 1

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This log includes rate of penetration, corrected 'd' exponent, drilling correlative porosity, formation fracture pressure, pore pressure and equivalent circulating density. It is plotted by the computer, either during the actual drilling of the hole or after TD, from the drilling data stored on magnetic tape. Once again this log is plotted on a 1:6,000 vertical scale. The horizontal dashed lines indicate the initation of a new bit run.

E.S. Geoplot 2

This log is similar to the Geoplot 1 in that it is computer plotted. However the following variables are plotted:weight on bit, rotary speed, pump pressure and mud density in.

HP Quartz Pressure Gauge

This highly accurate bottomhole pressure gauge is used in conjunction with the Schlumberger F.I.T. tool. The Hewlett

Packard Quartz Pressure Guage measures well bore pressure with a resolution of 0.01 psi over a dynamic range in excess of 10,000 psi. This capability makes it possible to accurately measure pressure changes that cannot be detected with conventional gauges using bourdon tube transducers.

WELL LOG PARAMETERS

1. Grapholog

Scale 1:400, containing drilling rate, hot wire total gas, chromatographic analysis, percentage strip lithology, lithology descriptions and remarks column, casing points, individual bit runs, dates, mud data, deviation surveys and core descriptions.

2. E.S. Drill Log

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Scale 1:6,000, containing rate of penetration, hot wire total gas, corrected 'd' exponent, shale density, bit runs, dates and casing points.

3. E.S. Temperature Log

Scale 1:6,000, containing flowline temperature, \triangle T:flowline temperature minus suction temperature, end to end plot (dimensionless).

4. E.S. Pressure Log

Scale 1:6,000, containing formation pore pressure, equivalent circulating density, formation fracture gradient.

5. E. S. Geoplot 1

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Scale 1:6,000, containing rate of penetration corrected 'd' exponent, drilling porosity, formation pore pressure, equivalent circulating density and formation fracture gradient.

6. E.S. Geoplot 2

Scale 1:6,000, containing weight on bit, rotary RPM, mud density in and pump pressure.

BARRACOUTA # 4 WELL SUMMARY

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Barracouta # 4 was spudded on the 30th. March 1977, water depth being 153 feet. A 26" hole was drilled from the sea floor to 718' using sea water, with returns to the sea floor. 20" casing was set at 657', followed by B.O.P. and 20" marine riser emplacement.

A 17.5" hole was drilled from 718' to 3200'. The lithology over the section 718' to 2640' consisted mainly of soft to firm calcarenite grading to calcareous siltstones. The low background gas, absence of connection gas, low torque and few cavings indicated that this section was normally pressured and drilling took place in an overbalanced con-The uncompacted nature of the sediments and the dition. variability of the drilling rate tends to indicate that much of this section was drilled by jet extrusive action as well as bit cutting action. This is reflected in the erratic nature of the corrected 'd' exponent and the computer-calculated drilling porosity, as neither mathematical model is designed to correct for hydraulic or jet extrusive drilling. The nature of surface hole sediments and the effect of jet extrusive drilling hampers pressure predictions over this interval.

The interval 2645' to 2800' was predominately loose to poorly consolidated sandstone of medium to coarse grain. Rates of penetration between 2645 - 2951 feet ranged from 146 to 1560 feet/hour. Lost circulation was encountered at 2951' and after regaining partial returns, ISF - SONIC -GR logs were run to 2942' for correlation purposes over the interval of lost returns. Proceeded to drill to 3200' without returns. 13.375" casing was set at 3147' and a tempe-

rature log run from surface to 3053'. Drilled out of shoe with 12.25" bit and 11.2 ppg fresh water/gel mud followed by a formation pressure test at 3225' equal to a 13.5 ppg mud weight equivalent. Lithology from 3200' to 3425' was mainly marl and minor siltstone and from 3425' to 4783' (T.D.) comprised of sandstone interbedded with coal and siltstone. The section 4065' - 4105' was coal and resulted in a 60 bbl drilling fluid loss, however after a flow check and drilling ahead, no significant loss of returns resulted. Controlled drilling the sand section between 3446' - 4232' and attempted to run an ISF - SONIC to 4232' but were unable to go deeper than 3124'. Proceeded to ream and mill junk and drilled to 4232' but were unable to go deeper than 3124'. Proceeded to ream and mill junk and drilled to 4240'. Run ISF -SONIC from 3940' - 3147'; FDC -GR - CNL from 3936' - 3147'; velocity survey; ISF - SONIC from 4237' - 3800'; HDT from 4015'-3147'; sidewall cores over interval 4000' - 3150', and opened hole to 16" over interval 3200' - 4240'. Run FDC caliper - gamma ray logs prior to running 10.75" liner. Liner shoe set at 4244' and hung at 2670'. Run temperature survey and cement bond log. Drilled out shoe with a 9.625" bit to 4274' and pressure tested formation to 13.5 ppg mud weight equivalent, then proceeded to 4566'. The lithology over this section being in the main loose quartz sands of fine to very coarse grain and poorly sorted, interbedded with thin coal seams.

Cores were cut over the following intervals:

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Core	1	-	45661	-	45941
Core	2	-	4594 '	-	46351
Core	3	-	46351	-	4668 '
Core	4	-	46681	`	47021

and full descriptions of the above cores can be found at the tail of the grapholog enclosed within this report. The section 4702' - 4783' (T.D.) was essentially loose quartz sands with minor claystone/siltstone stringers. Final electric logs were run which included the following :

FDC - CNL - CALIPER	4783' - 4241'
GR	4783' - 3600'
ISF - SCT	4783' - 4241'
VELOCITY SURVEY	4783' - 4241'
HDC	4783' - 4241'
SIDE WALL CORES	4780' - 4250' (30)
FIT'S	4635' - 4649', 4646'
RFT'S	4745', 4695', 4678', 4649',
	4648', 4647', 4646', 4635',
	4648', 4722', 4693', 4655',
•	4648.5', 4634'

CONCLUSION

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Considering all the data, processed and analyzed, it can be assumed that Barracouta # 4 was normally pressured throughout. Such findings can be confirmed in that part of the well which was subjected to direct formation pressure readings made by the HP quartz probe run with the 14 RFT's and 3 FIT's listed above, which revealed normally pressured formation. Most hole problems were of a mechanical nature and partially due to the fast drilling rates and formation characteristics in those sections of lost circulation. Possible coal fracturing, high equivalent circulating densities and partial "packing off" of the annulus by large coal cavings could account for the lost returns during the interval 4065'- 4105'.



Total loss of returns over the interval 2951'- 3200' could be attributed to a number of factors; excessively high, uncontrolled drilling rates leading to high loading of the annulus, and consequent increase in the equivalent circulating density and subsequent induced fracturing of the poorly consolidated sandstones could be one explanation, while high porosity/permeability of the sands with possible fractures coupled with the above could be another. Leak off tests to determine formation pressure/fracturing pressures were made in marl and calcaremite, while no tests were made in the sand sections encountered. Thus, no estimation of the upper value limits for equivalent circulating density were ascertained for that portion of the hole which was sands/sandstone.

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VARIABLE		UNITS
BIT INTERVAL	•• ••	FEET
SIZE	•• ••	INCHES
JETS	•••	32'S OF AN INCH
BIT RUN	•• ••	FEET
CONDITION	•• ••	TEETH/BEARING/GAUGE
OD'S, ID'S	•• ••	INCHES
LENGTH	•• ••	FEET
DEPTH	••	FEET
WOB	• • • • * • •	THOUSANDS OF POUNDS
PUMP RATE	•• ••	STROKES PER MINUTE
FLOW RATE	•• ••	GALLONS PER MINUTE
PUMP PRESSURE	••••••	POUNDS PER SQUARE INCH
MUD WEIGHT		POUNDS PER GALLON
PV .	<u>^</u> ● ● ●	CENTIPOISE
YP	•• ••	POUNDS PER 100 SQ.FT.
TEMPERATURE	•• ••	FARANHEIT
PRESSURE DROPS (P)	•• ••	POUNDS PER SECOND ²
JET VELOCITY	•• ••	FEET PER SECOND
ANN. VELOCITIES	•• ••	FEET PER MINUTE
ECD	•• ••	POUNDS PER GALLON

BIT DATA



INC

ANDIC:	BIT RUN DATA SHEET.											
NWK KA	ESI	P	UNIT NO.	1010		RUN NO. 2		BIT NO. 1				
COMPANY ESSO AUSTR	ALIA	WELL BARRAC	OUTA # 4		ATION ASS STR		INT 23	erval 6 '-71 8				
BIT	MAKE HUGI	HES	TYPE OSC-3A	' <u>1</u>	BITRUN	4821	тот. З	AL REVS 5700				
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	SIZE 17•5'	1		JETS 2(0/20/	20	HOURS RI 9	иц • 8		DITION 1-5-1
DRILL						OD		ID		· ·
STRING &	DRILL PIPE						5"	4.276	11	LENGTH
BOTTOM HOLE	HW DRILL P									
ASSEMBLY	DRILL COLL	ARS		-			811	<i>₿</i> 3"		101.93'
	HW DRILL C	OLLAR	IS							
CASING &	OD		ID			GRADE		SET AT		
LINER	20"			19.12	24"			657 •		HUNG AT.
DEPTH										
WOB	1					-				
RPM ·										
PUMP RATE			• • • •						· · · · · · · · · · · · · · · · · · ·	
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PV										
YP										
SAND %										
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Psurface										
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JET VEL										
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DP/OH	1						<u></u>			
DP/CSG	1								<u> </u>	
ECD									<u></u>	
REMARKS;			·					······································		
	DRILLING CONTROLLI LOW WOB I SPOT HOLI	ED DR DUE T	ILI	LING, DNLY	WITH 101.9	SEA W 3' OF	ATER. DRILL	COLLARS. ECTRIC LO	GS.	
	•									
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MAIDIE	7			BI	TRL	JN	DA		HEE	T.		****
WIKI JA	ESI	P		UN	IIT NO.		101	0	RUN N	10. ^I	4	BIT NO. 4
COMPANY ESSO AUSTI	RALIA	WELI					CATION PPSLAND BASIN			INTERVAL 3201'-3573'		
BIT	MAKE HUGH	L		TYPE	X3A			BIT RUN				AL REVS 41000
	SIZE 12.2			JETS	6/16/	/16		HOURS R			CON	DITION 5-206"
DRILL STRING &						0)		ID		L	
BOTTOM HOLE ASSEMBLY	DRILL PIPE HW DRILL P DRILL COLL HW DRILL C	ARS	RS					5" 8"		4•276 3"		LENGTH 474.361
CASING &	OD		ID			GF	ADE		SET	AT		
LINER	13.375	11		12.41	5"					3147	}	HUNG AT.
DEPTH	3350					I						
WOB	19											
RPM	91									<u> </u>		
PUMP RATE	129											
FLOWRATE	680											
PUMP PRESS	2410									·		
MW ·	11.2											
PV	18											
YP SAND %	12									 		
TEMP.	85											
Psurface							{		· · · · · · · · · · · · · · · · · · ·			
Pstring	17							•				
Pbit	733									 		
Pannulus	<u>1655</u> 14							2				
Ptotal	2419									 		
HHP	· · · · · · · · · · · · · · · · · · ·											
IMPACTFORCE	720 1852	÷	·		. <u>.</u>			· · · · · · · · · · · · · · · · · · ·	· · · ·	 		
JET VEL	428					•						
DC/OH	193					······	{					
DP/OH	133									f		
DP/CSG	129									¦		
ECD	11.3	1								İ		
REMARKS; D	RILL OUT	CEM	ENT	, STA	RT DR	IL		G FORM	ATIOI	AT C	540	hours.
	ORMATION							ppg.				
	IRCULATE IRCULATE				-			•				· ·
	ULL OUT (•					
		•	-				1 1		•			
			•					•		-		e a secondaria de la companya de la
•	•		÷ .		•							

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MAIDIT			B	BITRL	JN D	ATA	SHE	ET.			
	B ESI	Ρ		JNIT NO.	1 0 [.]	10	DI M	NO.	5		5
COMPANY								INU.		BIT NO.	
	RALIA	WELL BA	RRACOU	TA # 4		GIPP	N SLAND	BASI	N 35	rerval 5 73'- 423	321
BIT	MAKE		TYPE			BITF			тот	AL REVS	
	HUGHI	ES		X3A			659	t.		165000	
•	SIZE	511	JETS	16/16/	' 16	HOU	RS RUN 23•	3		NDITION	511
DRILL					OD	-	ID			1	
STRING &	DRILL PIPE		•			511		4.2	76"	LENGTH	
BOTTOM	HW DRILL P	IPE			1						
HOLE ASSEMBLY	DRILL COLL	ARS				811		311		561	+•95
	HW DRILL C	OLLARS	\$								
CASING &	OD		D		GRAD	E	SE	TAT			
LINER	13.37	7511	12.	415"				314	71	HUNG AT	
·. ·		~		1.1	1						•
DEPTH	3700		3800	39	00	1	4000			1	
WOB	45		20	39			45		·····		
RPM	122		114	12			118				
PUMP RATE	149		143	12	3	1	127	1			
FLOWRATE	716		704	60			620				
PUMP PRESS	2720		619	200	0		2140				
MW	11.2	1	1.2	11.	3		11.3				·
PV	21	2	1	21			21				
YP	13	1	3	13			13			•	· ·
SAND %											
TEMP.	93.7	9	8.1	101	•4		101				***************
Psurface	20	2	0	20			20	1			
Pstring	939	9	13	73	4		785				· · · · · · · · · · · · · · · · · · ·
Pbit	1745	1	686	125		1	334				
Pannulus	19		19	1	8		18				
Ptotal	2723	2	638	2031		2	157				
ННР	765		735	46			523				
IMPACTFORCE	1953		887	140		. L	493				
JET VEL	431		+28	36			382	·]			
DC/OH	204		200	17			176		··		
DP/OH	140		138	11			121				
DP/CSG	136		133	11			118				
ECD REMARKS;	11.5	1	1.5	11	•6	l	11.4				

GAS KICK, 400units HOT WIRE CUT MUD TO 10.6ppg AT 3610'. PUMP # 1 DOWN, BACK WORKING 0605hours AT 3631'. AT 4232' CIRCULATE BOTTOMS UP, RUN SHORT TRIP, CIRCULATE BOTTOMS UP, PULL OUT OF HOLE FOR ELECTRIC LOGS AND TO RUN 10.75" LINER.

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			BITR	ЛГ	DA	ATA SH	IEET.			
	s Es	\mathbf{P} .								
			UNIT NO.	1		-	RUN NO.	5	BIT NO. 6	
COMPANY		WELL	governa // h			ATION	D DAGTN	INT	ERVAL 321 -42401	
BIT	MAKE HUGH	ES	TYPE XD7			BIT RUN	81	Тот	AL REVS 2000	
	SIZE 12.2	5"	JETS 18/18	/18		HOURS R	JN 3		IDITION	
DRILL				0			ID			
STRING &	DRILL PIPE		· · · · · · · · · · · · · · · · · · ·		5	11	4.27	6"	LENGTH	
BOTTOM HOLE	HW DRILL P									
ASSEMBLY	DRILL COLL				8	11	311		474.361	
	HW DRILL C	OLLARS								
CASING &	OD	ID		GF	ADE		SET AT			
LINER	13.37	5"	12.415"				3147¥		HUNG AT.	
DEPTH			<u> </u>	- I		r'	L		1	
WOB										
RPM ·									-	
PUMP RATE										
FLOWRATE										
PUMP PRESS										
MW										
PV			•							
YP										
SAND %										
ТЕМР.					·					
Psurface								1.1		
Pstring										
Pbit				•			· ·			
Pannulus		-								
Ptotal	•									
ННР						•				
IMPACTFORCE										
JET VEL	· · · · · · · · · · · · · · · · · · ·						•			
DC/OH	ļ									
DP/OH										
DP/CSG	· .									
ECD	l				<u> </u>	·				
REMARKS;				•	•					

RUN IN HOLE, TIGHT SPOT AT 4059', REAM TO 4223', CIRCULATE TO CLEAN HOLE, PULL OUT OF HOLE, TIGHT SPOT AT 4030', RUN BACK IN, CIRCULATE BOTTOMS UP TWICE. TIGHT SPOT AGAIN AT 3850'. RUN IN HOLE AND CIRCULATE, PULL OUT, RUN ELECTRIC LOGS, TIGHT HOLE AT 3830'.

CLE-12

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			BI	TRU	IN DA	TA SH	IEE	Т.		والمتكافية فيتلبه توالمانين والمناوين والمتكفي المتشاهلات والمراجع والمتا		
I IIIRKA	ES	P										
			UN	IT NO.	1010) I	RUN N	o. 7		BIT NO. 6RR		
COMPANY ESSO AUSTR	ΑΤ.ΤΑ	WELL	RACOUTA	# 4		ATION				ERVAL 2011- 36321		
BIT	MAKE		TYPE	XD7	BIT RUN					TOTAL REVS		
	HUGHI	ES	w/15'		RREAM 431					m		
	SIZE 12.	25"	JETS 18	3/18/	18 HOURS RUN							
DRILL					OD ID							
STRING &	DRILL PIPE				. 5	511		4.276	11	LENGTH		
BOTTOM HOLE	HW DRILL P											
ASSEMBLY	DRILL COLL				8	311		3"		474.361		
· · · ·	HW DRILL C											
CASING &	OD	[1	D		GRADE		SET A	· · · · · · · · · · · · · · · · · · ·	·			
LINER	13.37	75"	12.41	15"				3147!		HUNG AT.		
DEDTU				1		· 	L					
DEPTH WOB												
RPM				<u> </u>								
PUMP RATE				<u> </u>								
FLOWRATE												
PUMP PRESS							.					
MW	{											
PV												
YP												
SAND %												
TEMP.												
Psurface						•	· · · · ·					
Pstring												
Pbit												
Pannulus		-										
Ptotal												
ННР												
IMPACTFORCE												
JET VEL												
DC/OH												
DP/OH												
DP/CSG		<u> </u>										
ECD	<u> </u>			L								
REMARKS;	•				. •		1.1					

RE-REN BIT # 6 WITH 15" UNDERREAMER TO ALLOW SETTING OF 10.75" LINER.

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CLE-12

			B	ITRL	JN DA	ATA SH	IEET.			
	B ESI	P								
WWIND	<u></u>	•	U	JNIT NO.	1010) I	RUN NO. 8		bit no. 6RR	
COMPANY		WELL			1	ATION			ERVAL	
ESSO AUSTR		BARF	RACOUT		1 1 1		D BASIN	36321- 42401		
віт	MAKE		TYPE	XD7	w/15"	BITRUN	-0.	TOTAL REVS		
	HUGHI	<u> 35</u>		DERREA	MER		081	-		
	SIZE 12.25	5"	JETS	18/18/	18	HOURS R				
DRILL			•		OD		ID			
STRING &	DRILL PIPE					5"	4.27	611	LENGTH	
BOTTOM HOLE	HW DRILL P				1					
ASSEMBLY	DRILL COLLARS					811	3"		47346	
	HW DRILL C				<u> </u>					
CASING &	OD		D		GRADE	· · · · · · · · · · · · · · · · · · ·	SET AT			
LINER	13.37	25"	12.	415"			31471		HUNG AT.	
DEPTH					ł	I				
WOB										
RPM		ŀ								
PUMP RATE										
FLOWRATE										
PUMP PRESS										
MW					•					
PV										
YP						·				
SAND %										
TEMP.										
Psurface					•••					
Pstring										
Pbit	·			·						
Pannulus		· · ·				·				
Ptotal	· · ·									
ННР	· · · ·	· ·								
IMPACTFORCE				•						
JET VEL										
DC/OH						 				
DP/OH										
DP/CSG			· · · · · · · · · · · · · · · · · · ·							
ECD		<u> </u>	·			l				
REMARKS	· · ·						• .			

PULL OUT OF HOLE TO RUN 10.75" LINER.

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	7		BI	TRL	IN DA	ATA SH	HEET.			
	B ES	P		IT NO.	1010		RUN NO. 9)	bit no. 6rr	
				TI NO.						
COMPANY ESSO AUSTI	RALIA	WELL BARR	ACOUTA	# 4	1	ATION PSLAND	BASIN	INTERVAL 4240 '- 4254 '		
BIT	MAKE HUGH	ES	TYPE	XD7		BIT RUN	141	TOTAL REVS		
	SIZE		JETS			HOURS R	UN		NDITION	
	12.2	5"		/18/	·····		•••		••	
DRILL					OD		ID			
STRING & BOTTOM	DRILL PIPE		•		5	11	4.27	6"	LENGTH	
HOLE	HW DRILL P									
ASSEMBLY	DRILL COLL				8	in	3"		474.36	
	HW DRILL COLLARS									
CASING &	OD		D		GRADE		SET AT		<u> </u>	
LINER	13.375	375" 12.415"					3147		HUNG AT.	
DEPTH	1			1	. <u></u>	1				
WOB										
RPM					<u></u>	1				
PUMP RATE						1				
FLOWRATE	·					1				
PUMP PRESS			•			1				
MW										
PV				1		1				
YP										
SAND %						1				
TEMP.						1				
Psurface										
Pstring	1			1	•	1				
Pbit						1				
Pannulus		-		1						
Ptotal										
ННР										
IMPACTFORCE										
JET VEL										
DC/OH	·									
DP/OH										
DP/CSG										
ECD	1		•	<u> </u>						
REMARKS;	•		.°		•					
ATTEMPTED TO RUN LINER, STUCK, PULL LINER OUT OF HOLE TO FIND HAVE LOST 24 CENTRALIZERS DOWN HOLE. PICK UP BIT AND JUNK SUB TO RUN IN AND MILL JUNK.										
DRILL AN EXTRA 141.										

			BI	TRL	JN D	A	TA SH	IEE	Т.			***
A LIKKA	ESI	P .										
			U	NIT NO.	1010	C		RUN N	10. 10)	Bľ	t no. 7
COMPANY ESSO AUSTE	RALIA	WELL BARF	ACOUTA	. # 4		LOCATION GIPPSLAND BAS						VAL .'-4570'
BIT	MAKE		TYPE		,I	٦	BIT RUN					REVS
	HUGHI	<u>es</u>	Х	:1G	3161							1000
	SIZE		JETS				HOURS RUI			CONDITION		
	9.62	25"	1	2/12/	Y		5	5.1			4-	6 - I
DRILL STRING &					OD			ID				
BOTTOM	DRILL PIPE		ļ		511		4.276	,11		ENGTH		
HOLE	DRILL COLL											
ASSEMBLY	HW DRILL CO				 	6	•5"		2:812	5"		566.401
CASING &	OD	1[)		GRAD	E		SET	AT	·····		
LINER	13.37	'5''					3147'			HUNG AT.		
	10.75	511	12•415" 9•95"						4244 .			2670'
DEPTH	4370		561								Τ	
WOB	18		23									•
RPM	101		108									
PUMP RATE	90		93									
FLOWRATE	444		60									
PUMP PRESS	2810	the second s	80	ļ				· · · · ·				
MW	11.2	10		ļ		_						
PV	18		18			_						
YP	12		12			_			ļ		_	
SAND % TEMP.		_		<u> </u>		-					-	
Psurface	<u>98</u> 20		0 <u>3</u> 19			4			<u> </u>		_	
Pstring	454		<u>54</u>			+	·		 		-	·····
Pbit	2328	23				+				~ ~		
Pannulus	31		36			+			 			
Ptotal	2833	28				+					-	
ННР	610		35	1		╈	<u></u>				-	
IMPACTFORCE	1315	13				╉						
JET VEL	507		21			\dagger		 、				
DC/OH	216		24			Ť						
DP/OH	-					T						·
DP/CSG	147		52			T			· ·			
ECD	11.4	10	•8			T						
REMARKS;					,							

PRESSURE INTEGRETY TEST TO 13.5 ppg MUD WEIGHT EQUIVALENT AT 4274'

MAINTO				BIT	RU	IN	DA	TA SH	HEE	Т.			
	B ES	P								•			
WWINU.		a.		UNIT	NO.	10	10		RUN N	0. 11		BIT NO. CB 1	
COMPANY		WELL		,		Ī	LOC	ATION			INT	ERVAL	
ESSO AUST		BAR	RAC	OUTA #	<u> 4 </u>	GIPPSLAND PASIN					45661-45941		
ВІТ	MAKE			ТҮРЕ				BIT RUN			TOTAL REVS		
	CHRIS	Τ.		<u> </u>	22	27*			71	10900			
	SIZE 8.47	11	JETS 🕳				HOURS RUN			^{JN} 3•5		DITION GOOD	
DRILL						OD			ID				
STRING &	DRILL PIPE			5" 4.270					11	LENGTH			
BOTTOM HOLE	HW DRILL P		•										
ASSEMBLY	DRILL COLLARS						6.5	,n 		2.812	5"	623.75	
	HW DRILL C								<u> </u>			·	
CASING &	OD		ID			GR	ADE		SET A				
LINER		13.375" 12.415"				3147 * 4244 *						HUNG AT.	
	10,75	5"		9.95"				r	4	244		2670	
DEPTH	4580												
WOB	15 50								<u></u>				
RPM						_					<u>-</u>		
PUMP RATE	1-16									·			
FLOW RATE PUMP PRESS	265		· · · · · · · · · · · · · · · · · · ·										
MW	637												
PV	10.6										·		
YP	18												
SAND %	14		·										
TEMP.	07												
Psurface	97								····				
Pstring													
Pbit			·····			•			·				
Pannulus													
Ptotal	·												
ННР													
IMPACTFORCE								<u></u>					
JET VEL	1												
DC/OH	1				•								
DP/OH													
DP/CSG		1											
ECD	10.8	_										· · · · · · · · · · · · · · · · · · ·	
REMARKS;							A						

DRILLERS DEPTH CORRECTION AT 4570' BACK TO 4566' CORED 27'. CORE BARREL JAMMED P.O.O.H

CLE-12

	BIT RUN DATA SHEET.										
	ESP				• •						
I WVIDLE"			UNIT NO.	1010	1	RUN NO. 12		BIT NOCB.1RR			
COMPANY	l w	ELL			ATION	12	INT	ERVAL			
ESSO AUSTR			OUTA # 4		PPSLAND	BASIN		45941-46351			
BIT	MAKE CHRIS		TYPE C-22		BIT RUN		TOTAL REVS 14400				
	CHRIS)T.	U= 22		1	14400					
	SIZE 8.47"		JETS		HOURS RUN 4.0			DITION			
DRILL			·	OD	OD ID						
STRING &	DRILL PIPE		5.0	D11	4.276"		LENGTH				
BOTTOM HOLE	HW DRILL PIPE	•									
ASSEMBLY	DRILL COLLAR			6.	511	2.8125	t	623.75			
	HW DRILL COLL	ARS.									
CASING &	OD	ID	_	GRADE		SET AT					
LINER	13.375" 12.415"					31471	HUNG AT.				
<u>.</u>	10.75"		9•95"		·····	4244		2670			
DEPTH	4620						<u></u>				
WOB	20			·	_	·					
RPM	60				ļ						
PUMP RATE	54										
FLOW RATE	265			-			·····				
PUMP PRESS	1000						_,				
PV	10.6			·							
	19 14										
YP SAND · %	14	· · · · · · · · · · · · · · · · · · ·									
TEMP.	92										
Psurface	/						··				
Pstring											
Pbit											
Pannulus				·							
Ptotal			······								
ННР											
IMPACTFORCE											
JET VEL	1										
DC/OH					····.						
DP/OH							har da i an a <u>s</u> a				
DP/CSG	1										
ECD	10.8										
REMARKS;											

CORED TO 4635'. 4' FAST BREAK. P.O.O.H RECOVERED 27'.HYDROCARBONS IN BOTTOM SECTION OF RECOVERED CORE. STRAPPED PIPE 42 STANDS.

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MAIND			BI.	r RU	INE	λ(TA SH	IEE	Т.			
KIRKA	ESI	2										
			UN	T NO.	10	10	1	RUN N	0. 13		BIT N	O.CB.1RR.
COMPANY ESSO AUSTI	RALIA	WELL BARRAC	OUTA	# 4			ATION PPSLANI) BA	SIN	INTI 463	ERVA	L +668¶
BIT	MAKE CHRIS	ST.	TYPE C	-22	BIT RUN 33"				тот	TOTAL REVS		
	SIZE 8.4	711	JETS		HOURS RUN 2					CONDITION FAIR		
DRILL			l		OD ID							
STRING &	DRILL PIPE			.0	.11	4	276"		LEN	GTH		
BOTTOM	HW DRILL PI	PE				, ,						
HOLE ASSEMBLY	DRILL COLLA	ARS			6.	•5	11	2	8125	1	62	3.751
ASSEIVIDET	HW DRILL CO	LLARS						1	·····			
CASING &	OD	ID			GRA	DE		SET	٩T			
LINER	13.375" 12.415"					3				•	HUN	G AT.
	10.75"	9	•95"					42	441		267	701.
DEPTH	4660								· ·			
WOB	20											
RPM ·	30											
PUMP RATE	35											
FLOWRATE	35 172											
PUMP PRESS	800											
MW	10.6											
PV	19											
YP	14											
SAND %												
TEMP.	92											
Psurface												
Pstring												
Pbit												
Pannulus		-							· ·			
Ptotal												
ННР												
IMPACTFORCE	·	_										
JET VEL						\square		<u>`</u>	ļ			
DC/OH	l							.				
DP/OH												
DP/CSG												
ECD	10.8		·						l			
REMARKS;	•				•							

CUT CORE NUMBER 3 CORE JAMMED.PUMPED SLUG .P.O.OH.

MADE	BIT RUN DATA SHEET.							
	B ES		UNIT NO.)	RUN NO.		BIT NO. CB 3RR
COMPANY		WELL		1	ATION	D1 0755	INT	ERVAL
ESSO AUSTR		BARRA	COUTA # 4	GI	PSLAND	BASIN		681 - 47021
ВІТ	MAKE		TYPE		BIT RUN	71	Тот	AL REVS
	CHRIS	51.	C -22		341			6000
	SIZE		JETS	HOURS				DITION
	8.47		-		L	1.5	J	FAIR
DRILL STRING &	DRILL PIPE			OD	5"	diama di seconda di se	<u></u>	LENGTH
BOTTOM	HW DRILL P				2''	4.27	0	LENGTH
HOLE	DRILL COLL				5.5"	2.81	251	627 751
ASSEMBLY	HW DRILL C			0.9		2.81	<u> </u>	623.75'
CASING &	OD			GRADE		SET AT		
LINER			12.415"	ICHADE				HUNG AT.
Litter	13.375 10.75		9.95"			3147 4244	.1	26701
DEPTH	10.75			I	<u> </u>			
WOB				<u></u>	<u> </u>			
RPM					1			
PUMP RATE	1							
FLOWRATE								
PUMP PRESS								
MW			· · · ·			· ·		
PV					· .			
YP			•					
SAND %								
TEMP.	l	· ·						
Psurface								
Pstring								
Pbit				• • •				
Pannulus Ptotal					· ·			
	·							
HHP IMPACTFORCE								
JET VEL	·							
DC/OH								·····
DP/OH								
DP/CSG								
ECD								
• •			L out of h	ole.				
	100% reco	very.						2.4
	· · · · ·	. <u>.</u>		•	•			
	•				۰.			
•			• • •	\backslash				•
•	•	•	•	· /				
				•	·			
		•						
•	•		•	;	• ;	•		•
		•						
CLE-12				•				
•					•	•		
								•
				•		· · · ·		
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	7			BI	TRL	JN DA	ATA S	HEE.	г.					
	ESI	Р		UN	IT NO.	10	10		D. 1	15	BIT N	0. 8		
COMPANY		WEL					ATION				ERVAL			
	RALIA			ACOUT	A # 4		GIPPSLAND BASIN				4702' - 4783'			
BIT	MAKE			TYPE						AL RE				
	HUGH	ES			X1 G		BITRUN	811	}			9000		
	SIZE			JETS			HOURS				NDITION			
	9.62	5"		1	0/12/	12		1.1		1	1-1-I			
DRILL	· · · · · · · · · · · · · · · · · · ·					OD	8	ID						
STRING &	DRILL PIPE	·······				•	511		4.276	511	LENC	атн		
BOTTOM	HW DRILL P	IPE												
HOLE		ILL COLLARS					6.5"		2.812	25"		565.21		
TOOLINDET	HW DRILL C	OLLA	RS			4								
CASING &	OD			GRADE		SET A	SET AT .							
LINER	13.3	75"		12.41		<u> </u>			3147	1	HUN	GAT.		
	10.7	5"	L	9.95	**	L	······		4244	.1	L	26701		
DEPTH					[ļ					<u></u>		
WOB							 							
RPM							 							
PUMP RATE														
FLOWRATE	· · · · · · · · · · · · · · · · · · ·								•			·		
PUMP PRESS														
MW PV					·									
YP					 									
SAND %								·····		<u>.</u>				
TEMP.														
Psurface							- <u></u>							
Pstring	 					•						<u></u>		
Pbit														
Pannulus						· · ·								
Ptotal	<u> </u>													
ННР														
IMPACTFORCE														
JET VEL														
DC/OH														
DP/OH	ļ													
DP/CSG														
ECD	<u> </u>		. <u></u>		L		L							
REMARKS;				•										
•	RUN IN HO				•			PIGHT	HOLE	, 4	+07 •	-4570'.		
1	REAM RAT	HOLI	S FI	ROM 45	570'	TO 470	21.							
· · ·]	DRILL FRO	OM 47	702	TO L	+7831	, TOI	TAL DEI	PTH.				• •		
CIRCULATE OUT AND CONDITION MUD. RUN SHORT 6 STAND WIPER TRIP.														
CIRCULATE OUT AND CONDITION MUD PRIOR TO PULLING OUT OF HOLE														
. !	ro run ei	LECTI	RIC	LOGS	•	•	•							
,														

MUD DATA

VARIABLE	•		UNITS
DEPTH	••	• •	FEET
MUD WEIGHT	• •	هز ه	POUNDS PER GALLON
FUNNEL VISCOSI	TY	••	A.P.I. SECONDS
PLASTIC VISCOS	ITY	••	CENTIPOISE
YIELD POINT	••	• •	LBS./100 SQ.FT.
GEL: INITIAL/1	O MIN.	••	LBS./100 SQ.FT.
FILTRATE	• •	• •	cc./30 MINUTES
CAKE THICKNESS		••	THIRTY SECONDS OF AN INCH
SALINITY	••	••	РРМ
SOLIDS/SAND/01	L.	••	PERCENTAGE



MUD INFORMATION DATA SHEET

	MUD IN	IFORM	ATION E	DATA SH	IEET		
SP			UNIT NO.	1010	SHEET	NO. 1	
	WELL BARI	RACOUTA	# 4	LOCATION GIPPSLAND BASIN			
719	719	2225	2415	2700	3052	3201	
31/3/77	1/4	1/4	1/4	2/4	2/4	3/4	
2200	0300	1200	1800	0300	1500	1200	
8.6	8.5	8.9	8.9	9.0	Seawater	8.6	
30	32	33	34	35	-	41	
	-	4	5	5		9	
		7.	10	11		13	
			6/12	5/12		10/20	
			9	9.5		9•5	
		NC	NC	NC .		24	
			13000	11000		10000	
			-/.75/0	4.4.75/-			
		· ·					
	719 31/3/77 2200 8.6	ESP WELL BARI 719 719 31/3/77 1/4 2200 0300 8.6 8.5	ESP WELL BARRACOUTA 719 719 2225 31/3/77 1/4 1/4 2200 0300 1200 8.6 8.5 8.9 30 32 33 4 7. 7.	ESP UNIT NO. WELL BARRACOUTA # 4 719 719 2225 2415 31/3/77 1/4 1/4 1/4 2200 0300 1200 1800 8.6 8.5 8.9 8.9 30 32 33 34 4 5 7.10 6/12 9 NC NC NC	WELL LOCATION 719 719 2225 2415 2700 31/3/77 1/4 1/4 1/4 2/4 2200 0300 1200 1800 0300 8.6 8.5 8.9 8.9 9.0 30 32 33 34 35 4 5 5 5 7.10 11 11 11 6/12 5/12 9 9.5 NC NC NC NC 13000 11000 11000	WELL LOCATION BARRACOUTA # 4 GIPPSLAND BAS 719 719 2225 2415 2700 3052 31/3/77 1/4 1/4 1/4 2/4 2/4 2200 0300 1200 1800 0300 1500 8.6 8.5 8.9 8.9 9.0 Seawater 30 32 33 34 35 - 4 5 5 - - - 30 32 33 34 35 - 30 32 33 34 35 - 9 9.5 5 - - - 10 11 - - - - - 9 9.5 - - - - - 10 NC NC NC - - -	

REMARKS:

DEPTH	3201	3201	3201	3225	3429	3430	3612
DATE	4/4	5/4	6/4	7/4	8/4	8/4	8/4
TIME	0300	1200	0300	0300	0300	0330	1800
WEIGHT	8.6	8.6	11.2	11.2	11.2	11.1+	11.1+
FUNNEL VISCOSITY	43	42	41	43	43	44	45
PLASTIC VISCOSITY	9	(Pits)	21	19	18	22	21
YIELD POINT	14		15	11	13	12	13
GEL INITIAL/10 MIN	9.0/22		6/14	3/10	4/10	3/10	3/9
PH	9.5		11	10	10	10	10
FILTRATE	26		8.2	7	6.8	7.0	6.7
САКЕ			2	2	2	2	2
SALINITY	11500		2200	2000	2000	2000	2300
SOLIDS/SAND/OIL			11/.5/-	11/.3/-	11/.25/	- 12/.75/	13/.3/-
REMARKS:	· .		· ·	······································		.	L

CLE-2

MUD INFORMATION DATA SHEET

MUD INFORMATION DATA SHEET												
WINISAD				UNIT NO.	1010	SHEET	NO. 2					
COMPANY ESSO AUSTRAI	LIA	WELL BAR	RACOUTA	<i>#</i> 4	LOCATION GIPPS	LAND BA	SIN					
DEPTH	3800	4190	4240	4254	4432	4595	4783					
DATE	9/4	9/4	11/4	16/4	19/4	20/4	24/4					
ТІМЕ	0300	1800	0400	0300	0600	0300	0100					
WEIGHT	11.2	11.2	11.2	11.2	10.6	10.6	10.6					
FUNNEL VISCOSITY	. 45	46	45	47	51	43	46					
PLASTIC VISCOSITY	22	20	21	23	20	18	23					
YIELD POINT	13	16	14.	14	13	14	9					
GEL INITIAL/10 MIN	3/9	3/10	2/7	3/9	4/16	4/16	2/5					
PH	10	10.5	10	11.5	12	11	11					
FILTRATE	6.2	4.4	4.6	6	5.6	6	4.6					
САКЕ	2	2	2	2	2	2	2					
SALINITY	2300	2300	3500	3500	4000	4000	4000					
SOLIDS/SAND/OIL	14/1/2-	14/.75/-	12/1/-	14/11/4/-	12/1/-	13/1/-	13/1/-					
REMARKS.												

REMARKS:

DEPTH DATE • TIME . WEIGHT FUNNEL VISCOSITY PLASTIC VISCOSITY YIELD POINT GEL INITIAL/10 MIN PH FILTRATE CAKE SALINITY SOLIDS/SAND/OIL **REMARKS:**

CLE-2

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COST PER FOOT CHARTS

1.1

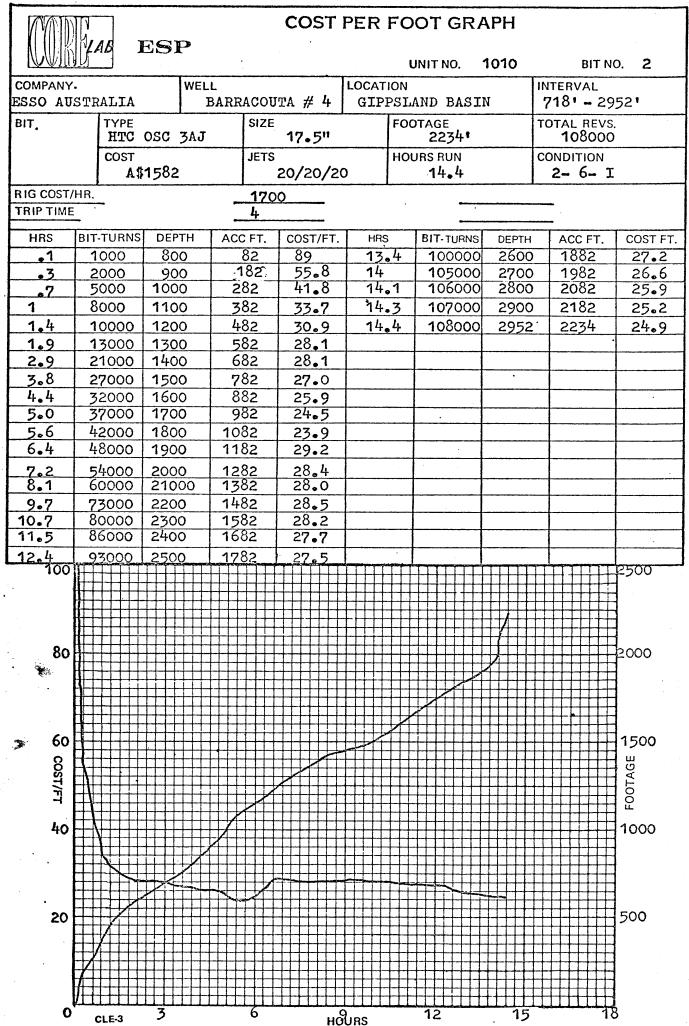
 $\left(\right)$

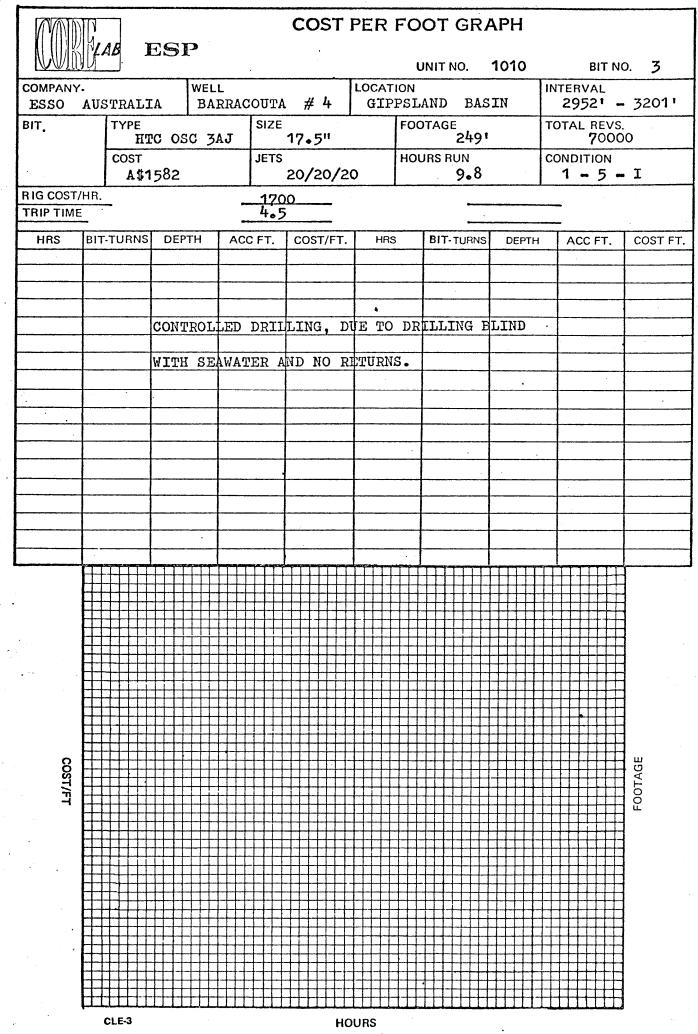
INTERVAL	••	. • •	FEET
FOOTAGE	••	••	FEET
BIT SIZE	••	••	INCHES
JET SIZE	••	• •	THIRTY SECONDS OF AN INCH
CONDITION	••	••	TEETH/BEARING/GAUGE
COST	••	••	DOLLARS

HOURS AND BIT TURNS ARE THE ACTUAL HOURS AND TURNS ON BOTTOM.

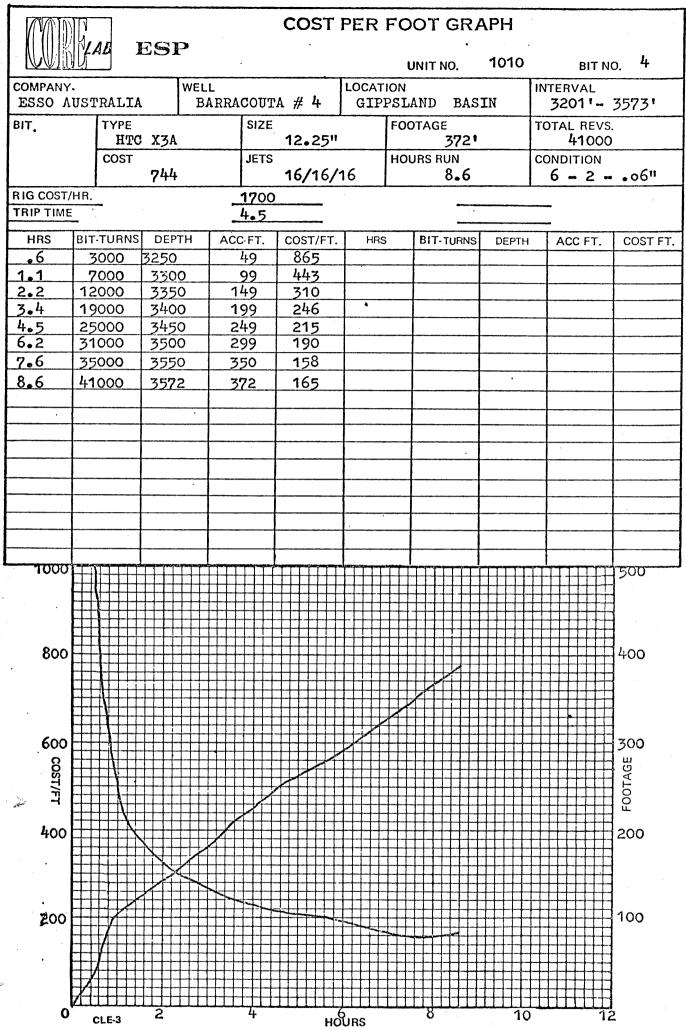
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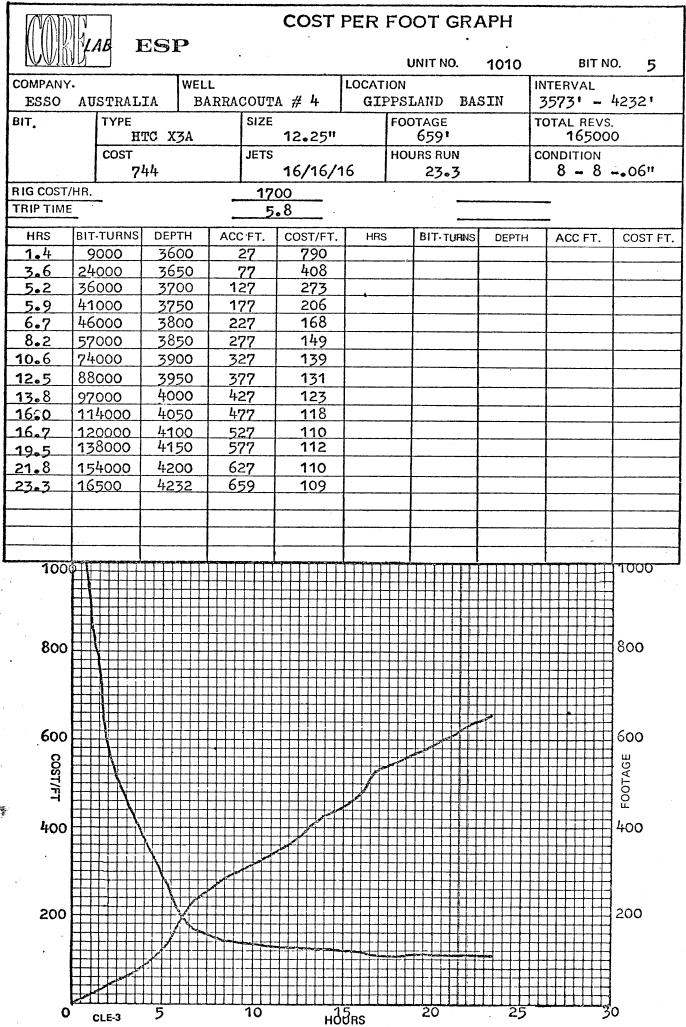


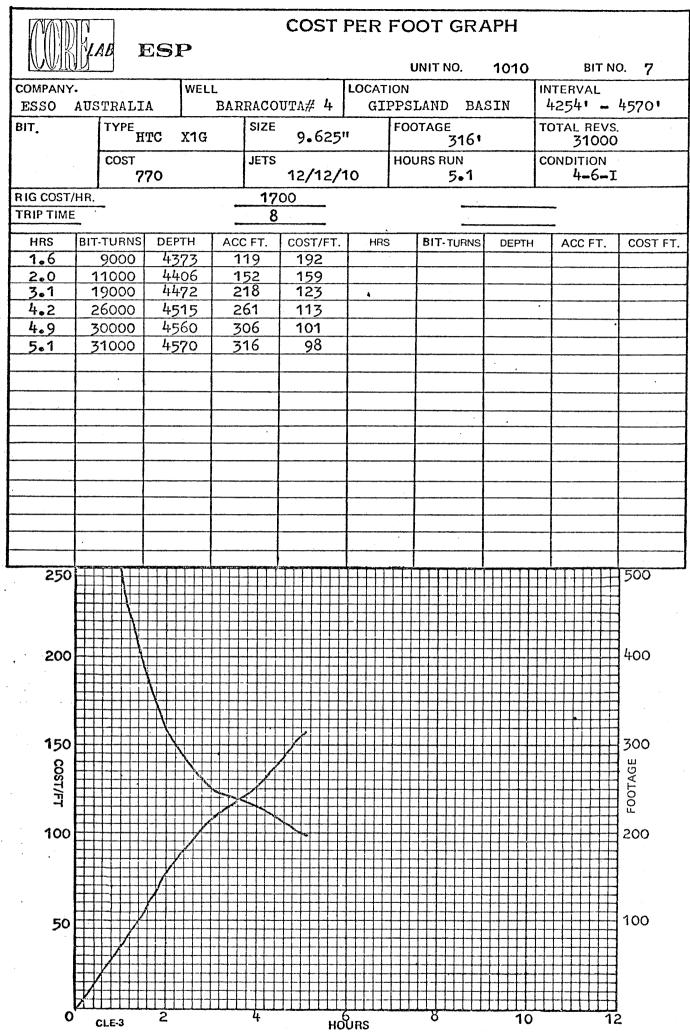


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DUMP A

DEPTH	-	Well depth in feet
TIME	-	Time of day in hours and minutes
ROP	-	Rate of penetration in feet per hour
WOB		Weight on bit in thousands of pounds
RPM	-	Rotary speed in revolution per minute
MID	-	Mud density in, in pounds per gallon
MDO	-	Mud density out, in pounds per gallon
ECD	-	Equivalent circulating density of the drilling fluid at the bottom of the hole. The sum of the hydrostatic pressure and the annular pressure drop, measured in pounds per gallon
рр	-	Pore pressure gradient, in pounds per gallon, is the pressure exerted by the fluids in the pore space of the formation. It is determined by analysing deviations from the trend line of the drilling porosity.
FG	-	Fracture gradient is the pressure required to fracture the formation, expressed in pounds per

POR

DEXP

11

fracture gradient is the pressure required to fracture the formation, expressed in pounds per gallon. It is derived from the pore pressure, calculated by the program using the Matthews and Kelly equation and an appropriate matric stress curve

Drilling porosity. This is the calculated porosity of the formation being drilled, derived from the general drilling equation. It is a function of the drilling variables: WOB, ROP, RPM, Toothwear, differential pressure and rock strength

Calculated 'd' exponent. The 'd' exponent is a function of WOB, ROP, RPM and hole size. A correction is made to the 'd' exponent for variations in mud density to give the corrected 'd' exponent

CORE LABORATORIES

ESSO BARRACOUTA # 4

DEPTH	TIME	RDP	ЫDВ	RPM	MIII	MDD	ECD	PP	FG	PDR	DEXP
				NEW 3	BIT II): 2					
720 750 760 770 780 790 800 810 815 820	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	543.2 1090.9 445.0 743.9 821.9 459.5 796.4 268.6	11 21 16 14 19 21 19 17	140 138 148 111 106 127 142 140	8.5 8.5 8.5 8.5 8.5 8.5 8.5	8.6 8.6 8.6 8.6 8.6 8.6 8.6 8.6		8.60	10.9 10.9 10.9 11.0 11.0 11.0 11.0 11.0	68.7 55.6 51.6 47.8 57.1 51.9 42.5 52.2 27.8 43.2	.63 .53 .73 .52 .52 .73 .60 .90
830 840 850 860 870 880 885 895 895 900	0.0 7:16 0.0 7:25 0.0 7:26 0.0 7:28 0.0 7:36 0.0 7:37 5.0 7:38 0.0 7:38 0.0 7:38 0.0 7:38	613.2 685.7 385.6 413.4 646.4 439.0 419.5 416.6	14 21 22 16 16 18 15	101 119 127 113 129 123 125 124	8.6 8.6 8.7	8.6 8.6 8.6 8.6 8.6 8.6	9.0	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	11.1 11.1 11.1 11.1 11.2 11.2 11.2 11.2		.91 .69 .61 .71 .69 .72
905 910 915 920 940 951 955 960 965	5.0 7:48 0.0 7:49 5.0 7:51 0.0 7:52 0.0 8: 3 0.0 8: 5 5.0 8: 5 0.0 8: 6 5.0 8: 7 0.0 8:37	251.2 219.0 227.7 476.6 294.2 493.1 356.4 318.5	13 12 15 16 13 13	118 115 115 114 110 127 118 118	8.7 8.7 8.7 8.7 8.6 8.7 8.7	8.7 8.7 8.7 8.7 8.7 8.7 8.7 8.7	9.1	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	11.2 11.2 11.2 11.3 11.3 11.3 11.3 11.3	54.8 52.1 48.0	.81 .83 .65 .77 .62 .69 .73
975 980 985 990 995 1000 1005 1010 1020 1030).0 8:40 5.0 8:41).0 8:42).0 8:43).0 8:55 1.0 8:55 1.0 8:55 1.0 8:55 1.0 8:57 1.0 8:57 1.0 9:58 1.0 9:13	275.1 235.5 312.0 263.8 445.6 208.6 341.0 314.8	15 16 16 17 17 15 22 24	114 113 114 111 102 105 103 104	8.6 8.7 8.7 8.6 8.6 8.5 8.6	8.7 8.7 8.7 8.7 8.7 8.7 8.7 8.7 8.7 8.7	8.8 8.9 9.0 8.8 9.7 8.8 8.8 8.8 8.8 8.8 8.8 8.8 8.8 8.8 8	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	11.3 11.3 11.3 11.4 11.4 11.4 11.4 11.4	31.8	.77 .79 .84 .77 .83 .68 .86 .79 1.00 .82
1035 1040 1045 1050 1055 1060 1070).0 9:14 5.0 9:15).0 9:17 5.0 9:19).0 9:31	530.9 387.0 264.2 191.2 362.9	27 25 26 27 26	107 110 111 113 103	8.6 8.6 8.7 8.8	8.7 8.7 8.7 8.7 8.7 8.7 8.7	8.8 8.8 8.9 8.9 8.6 8.7	8.60 8.60 8.60 8.60 8.60 8.60 8.60	11.4 11.4 11.4 11.4 11.4 11.5 11.5	33.0 31.3 25.7 20.8	.75 .71 .79 .93 1.05 1.00 .78

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ESSD BARRACOUTA # 4

			•						e		
INEPTH	TIME 33	FOP	MDB	RPM	MDI	MDO	ECD	PP	FG	POR	DEXP
1080.0	9:33	389.4	26 93	108	8.5	8.7 8.7	8.8 8.8	$8.60 \\ 8.60$	11.5 11.5	29.1 22.3	.80 .97
1085.0	9:35 9:43	250.4 666.6	27 21	110	8.6 8.6	°.7 8.7	0.0 8.8	8.60	11.5	41.7	.61
1090.0	9:44	446.5	17	106	8.7	8.7	8.8	8.60	11.5	42.2	.68
1100.0	9:45	266.6	30	105	8.7	8.7	8.8	8.60	11.5	22.4	.94
1105.0	9:46	228.1	24	109	8.7	8.7	8.8	8.60	$11.5 \\ 11.5$	26.0 27.3	.93 .91
1110.0	9:48 0:50	243.5	25	109 112	8.7 8.7	8.7 8.7	8.9 8.9	$8.60 \\ 8.60$	11.5		1.08
1115.0 1120.0	9:50 9:51	139.0	26 23	111	8.7	8.7	9.0	8.60	11.5		.85
1120.0	10: 3	269.8	21	99	8.7	8.7	8.8	8.60	11.6	30.9	.86
	49										
1135.0	10:4	290.4	55	116	8.8	8.7	8.9	$8.60 \\ 8.60$	$11.6 \\ 11.6$	31.1 21.4	.86 1.09
1140.0	10: 6	145.0	23	126 126	8.7 8.7	8.7 8.7	8.9 9.0	8.60 8.60	11.6	35.4	.81
1145.0 1150.0		365.9 308.7	53 55	120	.8.7	8.7	9.0	8.60	11.6	33.2	.87
1155.0		186.2	24	124	8.7	8.8	8.9	8.60	11.6	23.3	1.05
1160.0	10:19	355.0	23	117	8.8	8.9	8.8	8.60	11.6	32.1	.82
1165.0		266.6	23	124	8.7	9.0 9.0	8.8 8.9	$8.60 \\ 8.60$	11.6 11.6	28.4 27.8	.91 .95
1170.0		286.9 256.7		130 130		9.0 9.0	o.> 8.9	8.60	11.6		.93
1175.0 1180.0		212.5		132	8.8	9.0	9.0	8.60	11.6		1.03
	69										
	10:37	296.0	25	119	8.8	8.9	8.9	8.60	11.6	28.3 24.5	.89 1.00
1195.0		195.2	25 19	119 124	8.8 8.8	8.8 8.8	8.9 9.0	$8.60 \\ 8.60$	11.6 11.7	24.J 39.0	.78
1200.0		367.1		124	0.0 8.8	0.0 8.8	9.0	8.60	11.7	28.3	.95
1210.0		193.6		126	8.7	8.9	9.0	8.60	11.7	23.0	1.08
1215.0	10:44	300.5	24	117	8.7	8.9	9.0	8.60	11.7	33.7	.85
1220.0		164.6	24	120		9.1 9.1	8.8 8.9	8.60 8.60	11.7		1.06 .97
1225.0 1230.0		229.7 158.5		125 127		8.9	8.8	8.60	11.7		1.10
1235.0		228.5				8.9	8.9	8.60	11.7	27.9	.95
	93				_						
1240.0		169.4	55			8.9	8.9 8.9	8.60 8.60	11.7	25.0 28.3	1.03 .93
1245.0		260.1	25 24	126 113		8.8 9.0	0.7 8.7	8.60	11.7		.94
1250.0 1255.0		251.2		124		8.9		8.60	11.7		
1260.0		139.5		128		8.8	8.7	8.60	11.7		
1265.0	11:15	175.7		127		8.8	8.7	8.60	11.7		1.10
1270.0		275.6				9.0	8.8 8.8	$8.60 \\ 8.60$	11.7 11.8		.92 1.03
1275.0 1280.0		187.9				8.9 8.9	0.0 8.8		11.8		.78
1290.0		624.9				8.9	8.9	8.60	11.8		
	210										
1295.0		165.5				8.9	·8.8	8.60	11.8		1.04 .92
1300.0		294.9				8.9 8.9	8.9 8.9	$8.60 \\ 8.60$	11.8		
1305.0		217.9				8.9	8.9	8.60	11.8		.91
1315.0		79.4				9.0	8.6	8.60	11.8	13.5	1.23
1320.0		133.5	20	116	8.7	9.0	8.7	8.60	11.8		
1325.0		66.8				8.8	8.8	8.60 0 40	11.8		•
1330.0		128.0			8.7 8.7	8.8 8.8	8.9 8.9	$8.60 \\ 8.60$	11.8 11.8	29.4	
1335.0	· 12: 6 12:12	107.0				8.8	8.8	8.60	11.8		1.30
	44	an a € an'									

244

ESSD BARRACOUTA # 4

PAGE 3 - A

- 	DEPTH		FDP	WDB	FPM	MD I	мро	ECD	PP	FG	PDR	DEXP
and a second sec	1345.0 1350.0 1355.0 1360.0 1365.0 1370.0 1380.0 1385.0 1390.0 1395.0	12:29 12:33 12:36 12:40 12:44 12:46 12:59 13:2 13:5 13:7	119.6 95.1 141.5 101.9 111.8 218.7 129.7 128.0 95.8 145.3	19 26 26 26 23 19 19 21 22	125 126 128 129 129 129 120 122 124 124	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		8.8 8.9 8.9 8.8 8.8 8.8 8.8 8.8 8.8 8.8	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	11.8 11.9 11.9 11.9 11.9 11.9 11.9 11.9	18.4 13.8 12.6 26.9 21.7 20.3	1.28 1.15 1.27 1.28 .97 1.14 1.15 1.18
A second se	$1410.0 \\ 1415.0 \\ 1420.0 \\ 1425.0 \\ 1430.0 \\ 1435.0 \\ 1440.0 \\ 1445.0 \\ 1$	13: 9 13:11 13:18 13:20 13:21 13:22 13:25 13:27 13:36 13:38	172.7 166.5 163.9 176.4 204.1 269.6 126.1 145.1 95.4 152.6	20 21 24 25 25 25 25 25	125 124 118 121 127 128 128 127 123 128	8.6 8.6 8.7 8.7 8.8 8.6 8.6 8.6 8.6 8.6	8.8 8.8 8.8 8.8 8.8 8.8 8.8 8.8 8.9 8.7 8.6	8.9 8.8 8.8 8.8 8.8 8.8 8.8 8.8 8.8 8.7	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	11.9 11.9 11.9 11.9 11.9 11.9 11.9 12.0 12.0 12.0	26.7 26.3 22.6 24.1 28.6 16.5 21.1	1.04 1.05 1.02 .93 1.20 1.11 1.26
to a construction of the second secon	$\begin{array}{c} 30\\ 1450.0\\ 1455.0\\ 1460.0\\ 1465.0\\ 1465.0\\ 1470.0\\ 1475.0\\ 1480.0\\ 1485.0\\ 1490.0\\ 1495.0\\ 1495.0\\ \end{array}$	13:41 13:44 13:47 13:51 13:57 13:59 14:3 14:5 14:5 14:7 14:12	117.1 104.1 101.0 76.4 166.2 195.5 97.7 128.1 131.1 91.6	25 25 27 27 27 28 28 28 28	130 128 117 117 100 123 128 128 128	8.5 8.6 8.5 8.6 8.6 8.6 8.6 8.6 8.6 8.6 8.6 8.6 8.6	8.7 8.7 8.8 8.5 8.4 8.7 8.8 8.7	8.7 8.8 8.8 8.7 8.7 8.8 8.8 8.8 8.8	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	12.0 12.0 12.0 12.0 12.0 12.0 12.0 12.0	14.8 14.6 10.9 20.5 20.1 9.2 16.4	1.23 1.22 1.30 1.04 1.07 1.34 1.18
fi e e e e e e e e e e e e e e e e e e e	1505.0 1510.0 1515.0 1520.0 1525.0 1530.0 1535.0	14:19 14:21 14:26 14:30 14:32 14:33 14:35 14:43 14:44 14:45	150.3 120.8 96.0 87.4 211.6 177.1 135.8 122.1 246.1 289.6	27 28 27 27 27 27 27 27 27 27 27 27 27 29	114 121 123 125 123 123 126 115 121	8.5 8.5 8.5 8.5 8.5 8.5 8.5 8.5 8.5	8.6 8.6 8.8 8.7 8.9 8.9 8.9 8.9 8.9	8.7 8.7 8.7 8.7 8.7 8.7 8.7 8.7 8.8	8.60 8.60 8.60 8.60 8.60 8.60 8.60	12.0 12.0 12.0 12.1 12.1 12.1 12.1 12.1	14.9 7.9 9.6 22.1 20.1 22.7 18.6	1.20 1.37 1.36 1.03 1.09 1.10 1.15 .99
	1550.0 1555.0 1560.0 1565.0 1570.0	14:46 14:49 15:0 15:2 15:4 15:12 15:14 15:16 15:20	207.5 222.0 202.2 228.8 169.3 151.7 159.8 179.8 153.9 159.4	29 27 25 23 24 24 24 24 24 26	123 125 125 128 131 134 132 128 130 127	8.5 8.5 8.6 8.6 8.6 8.6 8.6 8.7 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	8.9 8.9 8.9 8.9 8.9 8 8 8 8 8 9 9 8 8 8 9 9 8 8 9 9 9 8 9	8.7 8.7 8.7 8.7 8.7 8.8 8.8 8.8 8.8	8.60 8.60 8.60 8.60 8.60 8.60 8.60	12.1 12.1 12.1 12.1 12.1 12.1 12.1 12.1	22.4 22.6 24.4 23.3 24.5 21.2 23.8	$1.02 \\ 1.04 \\ 1.00 \\ 1.06 \\ 1.07 \\ 1.10 \\ 1.05 \\ 1.10 \\ 1.05 \\ 1.10 \\ 1.10 \\ 1.10 \\ 1.10 \\ 1.10 \\ 1.10 \\ 1.10 \\ 1.10 \\ 1.05 \\ 1.10 \\ 1.00 \\ $

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ESSO BARRACOUTA # 4

PAGE 4 - A

and a second second	DEPTH	TIME 05	POP	WDB	RPM	MDI	MDO	ECD	PP	FG ·	PDR	DEXP
	1610.0 1615.0 1620.0 1635.0 1650.0 1655.0 1660.0 1665.0 1670.0 1675.0	15:26 15:27 15:29 15:34 15:42 15:44 15:46 15:48 15:50 15:56	169.9 268.7 155.2 179.5 182.4 168.2 185.2 137.2 157.5 184.6	21 25 26 26 26 25 25 25 26 24 22	115 125 127 130 126 127 128 130 131 132	8.5 8.5 8.6 8.7 7 7 8 8 8 8 8 8 8 8 8 8 8 8 8	8.9 8.9 8.6 8.6 8.6 8.6 8.6 8.6 8.6	9.0 9.0 9.0 8.9 8.9 8.9 8.9 8.9 8.9	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	12.2 12.2 12.2 12.2 12.2 12.2 12.2 12.2	30.6 30.9 23.5 24.6 24.5 23.9 25.2 19.9 23.4 27.1	.97 .92 1.09 1.05 1.05 1.06 1.04 1.15 1.09 1.03
no service of the ser	45 1680.0 1685.0 1690.0 1695.0 1700.0 1710.0 1720.0 1725.0 1730.0 1735.0 49	15:58 16: 0 16: 2 16: 4 16: 6 16:16 16:18 16:20 16:22 16:24	139.3 197.5 144.5 155.7 140.7 186.9 223.2 166.5 123.3 152.7	21 25 26 26 26 27 27 28 27 28 28	130 133 134 133 121 132 134 136 136	8.6 8.5 8.6 8.6 8.6 8.6 8.6 8.7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	8:7 8.6 8.6 8.7 8.6 8.6 8.6 8.7 8.5	8.8 8.8 8.8 8.8 8 8 8 8 8 8 8 8 8 8 8 8	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	12.2 12.2 12.3 12.3 12.3 12.3 12.3 12.3	24.1 24.6 19.8 20.3 19.6 24.0 24.1 21.4 17.0 20.4	$1.10 \\ 1.04 \\ 1.14 \\ 1.13 \\ 1.16 \\ 1.05 \\ 1.04 \\ 1.11 \\ 1.21 \\ 1.14$
	1740.0 1745.0 1750.0 1755.0 1760.0 1765.0 1770.0 1775.0 1780.0 1785.0	16:25 16:26 16:35 16:36 16:38 16:40 16:42 16:42 16:45 16:54 16:56	175.0 141.6 191.0 201.2 149.8 152.0 158.9 156.1 114.4 141.4	25 26 26 26 27 26 27 26 25 25 27	137 123 121 123 126 128 129 125 118	8.6 8.6 8.8 8.8 8.8 8 8 8 8 8 8 8 8 8 8	8.5 8.9 8.8 8.8 8.8 8.6 8.6 8.6 8.6 8.8	9.1 9.2 8.8 8.8 8.8 8.9 8.9 8.9 8.9 8.9	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	12.3 12.3 12.3 12.3 12.3 12.3 12.3 12.3	27.1 25.0 26.1 25.2 21.3 21.6 22.3 23.4 19.3 20.6	$1.05 \\ 1.10 \\ 1.02 \\ 1.02 \\ 1.11 \\ 1.11 \\ 1.10 \\ 1.09 \\ 1.19 \\ 1.12 $
	1790.0 1795.0 1800.0 1805.0 1810.0 1815.0 1820.0 1825.0 1830.0 1835.0	17: 0 17: 3 17: 6 17:14 17:17 17:19 17:22 17:25 17:25 17:27 17:34	145.5 172.0 97.5 139.3 126.1 121.3 140.3 98.9 129.6 122.4	27 27 26 24 24 25 23 25 23 27	126 129 134 115 113 117 114 117 117 126	8.6 8.6 8.6 8.6 8.6 8.6 8.6 8.6 8.6 8.6	8.7 8.6 8.8 8.8 8.8 8.6 8.6 8.6 8.7	8.7 8.7 8.7 8.7 8.8 8.8 8.8 8.8 8.8	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	12.4 12.4 12.4 12.4 12.4 12.4 12.4 12.4	18.6 21.1 15.6 22.8 22.0 24.7 22.4 20.1 24.2 18.7	1.16 1.10 1.26 1.09 1.11 1.09 1.10 1.18 1.09 1.18 1.09 1.18
	1855.0 1860.0	17:36 17:37 17:38 17:39 17:39 17:40 17:42 17:42 17:43 17:45 22:14	125.9 103.1 99.6 140.9 159.0 192.2 157.9 138.0 130.6 202.3	27 27 26 26 28 28 27 26 27	138 140 143 139 139 139 141 140 141 131	8.7 8.6 8.6 8.5 8.6 8.6 8.6 8.6 8.6 8.6 8.6 8.7	8.7 8.9 8.8 8.7 8.7 8.7 8.8 8.8 8.8 8.8 8.8 8.8	8.8 8.8 8.9 8.9 8.9 9.0 9.0 9.1	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	$12.4 \\ 12.4 \\ 12.4 \\ 12.4 \\ 12.4 \\ 12.4 \\ 12.5 \\ $	17.5 16.2 15.7 20.0 22.5 25.1 22.2 22.5 28.6	$1.22 \\ 1.26 \\ 1.27 \\ 1.17 \\ 1.12 \\ 1.06 \\ 1.13 \\ 1.15 \\ 1.16 \\ 1.01 $

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ESSO BARRACOUTA # 4

PAGE 5 - A

	DEPTH 60		PDP	MDB	RPM	MDI	MDO	ECD	PP	FG	PDR	DEXP
	1905.0 1910.0 1915.0	22:16 22:18 22:20 22:23	150.4 178.5 102.7 117.7	25 26 26 23	120 136 135 133	9.7 8.8 8.7 8.6	8.8 8.8 8.8 8.9	8.8 8.8 8.9 8.9	8.60 8.60 8.60 8.60	12.5 12.5 12.5 12.5	24.3 24.6 16.6 22.8	1.08 1.08 1.71 1.15
-	1920.0 1925.0 1930.0	22:25 22:34	130.7 74.2	22 25 26	135 135 135 127	9.0 9.0 9.0	9.0 9.1 8.8	8.9 9.0 9.1	8.60 8.60 8.60	12.5 12.5 12.5	25.1 15.2 26.1	1.11 1.34 1.08
	1935.0 1940.0 1945.0	22:36 22:40 22:43	148.7 78.2 137.0	29	125 122 122	8.9 8.9 8.9 8.9	9.0 8.9 8.9	9.1 9.1 9.1	8.60 8.60 8.60	12.5 12.5 12.5	15.9 23.5 20.0	1.30 1.12 1.21
	1950.0	22:46 45	105.8		160	0.0	0.2	~ * * *	0.00	1210		
-[]	1955.0		131.1	29	126	9.0	819	9.1	8.60	12.5	21.8	1.17
	1960.0	22:52	108.6	27	126	9.0	8.8	9.1	8.60	12.5	21.6	1.18
1997 - 1997 -	1965.0	23: 2	122.7	27	117	9.0	8.8	9.1	8.60	12.5	23.8	1.12
	1970.0	23: 4	132.4	30	108	9.0	8.9	9.1	8.60	12.5		1.11
[]	1975.0	23: 6	171.5	58	120	9.0	8.9	9.1	8.60	12.5	27.2	1.04
	1980.0	23: 8 -	154.1	29	121	9.0	8.9	9.1	8.60	12.5	25.1	1.08
: F].	1985.0	23:10	159.7	31	120	9.0	8.9	9.2	8.60	12.6	24.8	1.08
	1990.0	23:12	140.8	29	122	9.0	9.0	9.2	8.60	12.6	25.1	1.10
	1995.0	23:19	112.9	26	124		9.0	9.2	8.60 8.60	12.6 12.6	23.8 28.9	1.15 1.06
n - , , , , , , , , , , , , , , , , , ,	2000.0	23:22	137.2	- 23	126	9.0	9.0	9.2	0.00	16.0	CO. 7	1.00
•	69 2005.0	23:24	146.3	24	127	9.2	9.0	9.2	8.60	12.6	29.1	1.05
ų,	2003.0	23:26	149.1	30	128	9.2	9.0	9.2	8.60	12.6	25.1	1.10
[]	2015.0	23:27	179.9	30	129	9.2	9.0	9.2	8.60	12.6	27.2	1.05
	2020.0	23:31	102.0	28	135	9.0	9.0	9.3	8.60	12.6	22.0	1.21
	2025.0	23:34	139.1	31	119	9.0	9.0	9.4	8.60	12.6	24.0	1.14
T.	2030.0	23:45	154.8	27	121	9.0	9.1	9.2	8.60	12.6		1.05
·	2035.0	23:47	143.4		124	9.0	9.1	9.1	8.60	12.6	25.8	1.09
	2040.0	23:50	145.0		125		9.1	9.1	8.60	12.6	21.7	1.16
[⁻]	2045.0	23:52	160.3		126		9.1	9.2	8.60	12.6	23.5	1.11
	2050.0	23:55	116.6	33	126	9.1	9.1	9.1	8.60	12.6	18.4	1.23
د	74 2055.0	2 0:7	101.6	32	120	9.1	9.1	9.2	8.60	12.6	20.0	1.21
-	2055.0	0:7	83.6	0e 1 31			9.1	9.2	8.60	12.6	18.0	
	2065.0	0:13 0:14	95.5	32	124		9.1	9.2	8.60	12.6	19.0	
	2070.0	0:16	137.4	32	124		9.1	9.3	8.60	12.6	23.5	
ŕ1	2075.0	0:18	151.8	33.			9.1	9.3	8.60	12.6	24.5	1.11
	2080.0	0:20	154.9	31	125	9.2	9.0	9.3	8.60	12.6	26.1	1.09
· • •	2080.0	0:21	94.6	32	129		8.9	9.3	8.60	12.6	19.8	1.24
` ,	2095.0	0:35	107.1	32	127		9.0	9.4	8.60	12.7	20.8	1.23
	2100.0	0:39	101.1	31	133		9.0	9.4	8.60	12.7	20.6	1.25
	2105.0	0:41	169.8	30	133	9.2	9.0	9.4	8.60	12.7	27.4	1.09
	78				100	·	0.0	o .	8.60	12.7	22.8	1.19
l,		0:44	116.2	31	133 131	9.2 9.3	9.0 9.0	.9.4 9.3	e.60 8.60	12.7	18.0	
1. J.	2115.0	0:48 1: 3	95.1 63.8	32 32	131	7.3 9.3	9.0	9.4	8.60	12.7	15.1	1.37
- { }	2120.0 2125.0		61.8	эс 31	129		9.0	9.3	8.60	12.7	14.9	
	2130.0	1:15	51.6	33	130		9.0	9.3	8.60	12.7	12.1	1.43
•	2135.0	1:17	116.6		126		9.0	9.3	8.60	12.7	21.3	
••	2140.0	1:22	84.4	35	131	9.1	9.0	9.3	8.60	12.7	14.6	
	2145.0	1:27	71.6	36	129		9.0	9.3	8.60	12.7	13.2	
	2150.0	1:39	73.6	36	125		9.0		8.60	12.7	13.3	
с. 9. Т. с. с.	2155.0	1:43	83.0	35	125	9.2	9.0	9.3	8.60	12.7	15.8	1.32
	83	4.					•		*			

PAGE 6

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				1.15370	F1 F1 64	MDI	MDO	ÉCD	PP	FG	PDF	DEXP
	DEPTH T 834	IME	PDP .	MDB	FFM	1101	ribu		1 6	1.0	1 01.	
	2160.0 2165.0 2170.0	1:47 1:58 2:4	65.4 60.1 55.4	34 29 31	127 126 133	9.2 9.2 9.2	9.0 9.0 9.0 9.0	9.3 9.3 9.3 9.3	8.60 8.60 8.60 8.60	12.7 12.7 12.7 12.7	13.9 16.1 14.5 15.1	1.38 1.36 1.39 1.37
	2180.0 2185.0	2: 9 2:13 2:27 2:32	58.8 71.9 56.4 60.7	31 29 28 30	132 132 122 122	9.1 9.1 9.1 9.1	9.0 9.0 9.0	9.3 9.2 9.2	8.60 8.60 8.60	12.7 12.7 12.7	18.5 16.7 15.2	1.30 1.34 1.36
	2195.0 2200.0 2205.0	2:38 2:45 2:49	52.5 55.2 78.5	30 31 31	124 124 123	9.1 9.1 9.1	9.0 9.0 9.0	9.2 9.2 9.2	8.60 8.60 8.60	12.7 12.8 12.8	13.3 13.2 17.2	1.41 1.41 1.31
	2215.0 2220.0	2:54 3:5 3:9	62.7 81.3 80.9	31 32 38	123 112 126	9.1 9.1 9.1	9.0 9.0 9.0	9.2 9.2 9.2 9.2	8.60 8.60 8.60 8.60	12.8 12.8 12.8 12.8	15.8 18.4 13.3 15.4	1.35 1.27 1.38 1.33
	2235.0 2240.0	3:13 3:16 3:18 3:21	83.2 90.2 143.5 106.1	37	128 127 126 128	9.1 9.1 9.1 9.1	9.0 9.0 9.0 9.0 9.0	9.2 9.2 9.3 9.3	8.60		15.7 20.9 18.0 19.3	1.32 1.18 1.27 1.26
	2245.0 2250.0 2255.0 930	3:33 3:36 3:39	102.5 97.5 117.1	33 38 37	126 131 136	9.1 9.1 9.1	9.0 9.0	9.2 9.2	8.60 8.60	12.8 12.8	16.2 18.0	1.31 1.27
ſ	2260.0 2265.0 2270.0 2275.0	3:41 3:44 3:46 3:56	133.2 126.1 134.2 128.2	38 37 38 35	137 134 134 130	9.1 9.1	9.0 9.0 9.0 9.0	9.2 9.2 9.2 9.3 9.3	8.60 8.60 8.60 8.60 8.60 8.60	12.8 12.8 12.8 12.8 12.8	19.3 18.7 19.9 21.0 18.0	1.23 1.25 1.22 1.21 1.21
	2280.0 2285.0 2290.0 2295.0 2300.0		127.8 117.7 164.6 119.7 140.5	41 39 38 40 41	132	9.1 9.1 9.1 9.1	9.0 9.0 9.0 9.0 9.0 9.0	7.3 9.3 9.3 9.3 9.3	8.60 8.60 8.60 8.60 8.60 8.60	12.8 12.8 12.8 12.8 12.8 12.8	18.4 21.8 18.1 18.8 20.4	1.25 1.17 1.26 1.23 1.21
	2305.0 978 2310.0 2315.0			40 36 40 40	124 130	9.1	9.0 9.0 9.0	9.3 9.3 9.3	8.60 8.60	12.9 12.9 12.9	24.0 20.9 20.5	1.13 1.19
	2320.0 2325.0 2330.0 2335.0	4:22 4:25 4:27 4:29 4:29	144.9 124.4 150.8 178.9 112.3	40 42 41 42 34	132 132 132	9.1 9.1 9.1	9.0 9.0 9.0 9.0	9.3 9.3	8.60 8.60 8.60	12.9 12.9 12.9 12.9	17.9 20.2 22.5 21.0	
	2340.0 2345.0 2350.0 2355.0 1023	4:40 4:42 4:45	165.3 154.5 97.2	40 39 41	129		9.0 9.0 9.0	9.3 9.3 9.3	8.60 8.60	12.9 12.9 12.9	22.3 21.7 15.7	1.15
	2360.0 2365.0 2370.0	4:48 4:50 4:58	114.6 119.1 145.6	41 42 39 39	120	9.1 9.1	9.0 9.0 9.0 9.0	9.3 9.3 9.3 9.3		12.9 12.9 12.9 12.9	17.7 17.8 21.8 22.4	1.27 1.17
	2380.0	5: 0 5: 3 5: 5 5: 8 5:11 5:20	159.0 112.9 120.7 130.2 111.8 139.2	37 41 40 40 41 40	124 125 126 127	9.1 9.1 9.1 9.1	9.0 9.0 9.0 9.0 9.0	93 93 93 93	8.60 8.60 8.60	12.9 12.9 12.9 12.9 12.9 12.9	18.0 18.4 19.6 17.6 19.5	1.27 1.25 1.23 1.28
	2400.0 2405.0 1068	5:22	109.9	39			9.0	9.2		12.9	17.6	

ESSD BARRACOUTA # 4

PAGE 7 -

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	IFPTH	TIME	PDP	MDB	RPM	MDI	MDD	ECD	PP	FG	PDR	DEXP
:	10											
	2410.0	5:25	96.2	39	122	9.1	9.0	9.2	8.60	12.9	16.5	1.31
ł	2415.0	5:28	100.4	38	123	9.1	9.0	9.2	8.60	12.9	17.5	1.29
. I.	2420.0	5:31	102.5	38	124	9.1	9.0	9.2	8.60	13.0	18.1	1.28
-	2425.0	5:34	110.8	40	124	9.1	9.0	9.2	8.60	13.0	17.8	1.28
1.	2430.0	5:37	111.3	38	125	9.1	9.0	9.3	8.60	13.0	19.1	1.25
1	2435.0	5:57	80.5	39	126	9.1	9.0	9.2	8.60	13.0	14.7	1.37
\$	2433.0	6: 1	94.5	36	121	9.1	9.0	9.2	8.60	13.0	17.4	
	2445.0	6: 3	118.6	40	126	9.1	9.0	9.2	8.60	13.0	17.6	1.27
1		6: 6	102.8	42	129	9.1	9.0	9.2	8.60	13.0		
	2450.0		87.5	40 40	131	9.1	9.0	9.2	8.60	13.0	14.5	1.37
	2455.0	6:10	or.J	40	101	2 • 1	2.0		0.00	1010	14.0	1.1.1
1.	11		122.2	41	131	9.1	9% 0	9.2	8.60	13.0	17.7	1.28
14	2460.0	6:12			122	9.1	9.0	9.2	8.60	13.0	17.0	1.30
ţ.	2465.0	6:22	100.3	40			9.0	9.2	8.60	13.0	19.3	1.23
	2470.0	6:25	132.0	41	125	9.1				13.0	17.9	
	2475.0	6:27	117.8	42	126	9.1	9.0	9.3	8.60			
. '	2480.0	6:30	132.9	41	127	9.1	9.0	9.3	8.60	13.0		1.23
	2485.0	6:32		41		9.1	9.0	9.3	8.60	13.0	18.2	1.27
1	2490.0	6:34	145.4	42	127	9.1	9.0	9.3	8.60	13.0	20.6	1.20
	2495.0	6:45	105.4	38-	108	9.1	9.0	9.3	8.60	13.0	19.9	
	2500.0	6:48	117.4	42	109	9.1	9.0	9.3	8.60	13.0		1.24
	2505.0	6:50	124.5	42	110	9.1	9.0	9.3	8.60	13.0	19.5	1.22
1	116	7				•						
	2510.0	6:53	111.5	41	112	9.1	9.0	9.3	8.60	13.0	18.6	1.25
s	2515.0	6:56	136.9	43	130	9.1	9.0	9.3	8.60	13.0	19.2	1.24
i i	2520.0	6:58	116.0	44	130	9.1	9.0	9.3	8.60	13.0	17.0	1.30
	2530.0	7:10	113.4	42	125	9.1	9.0	9.3	8.60	13.0	18.3	1.28
	2535.0	7:12	120.0	40	122	9.1	9.0	9.3	8.60	13.0	20.1	1.24
7	2540.0	7:15	126.1	44	123	9.1	9.0	9.3	8.60	13.1	18.4	1.26
i.	2545.0	7:17	117.1	43	130	9.1	9.0	9.3	8.60	13.1	17.8	1.29
ند •	2550.0	7:20	134.8	- 44	129	9.1	9.0	9.3	8.60	13.1	19.0	1.25
	2555.0	7:22	147.8	45	128	9.1	9.0	9.3	8.60	13.1		1.23
ł		7:31	141.1	44	124	9.1	9.0	9.3	8.60	13.1	20.0	1.22
4.	2560.0 12		141.1	मन.	164	. • I			0.00			
· ·	2565.0	7:34	97.5	43	124	9.1	9.0	9.3	8.60	13.1	16.7	1.33
	2570.0	7:38	87.7	45 45	125	9.1	9.0	9.3	8.60	13.1	14.2	1.39
	2575.0	7:42	77.6	45 45	126	9.1	9.0	9.3	8.60	13.1	12.9	1.43
-	2580.0	7:45	104.3	44	126	9.1		9.3	8.60	13.1	16.3	1.33
T	2585.0	7:48	104.3	45	125	9.1	9.0	9.3	8.60	13.1	15.7	1.35
4	2590.0	7:58	107.1	43	120	9.1	9.0	9.3	8.60	13.1	17.4	1.30
	2595.0	8:1	115.0	44	118	9.1	9.0	9.2	8.60	13.1	18,1	1.28
4 		8:4	106.4	45	130	9.1	9.0	9.3	8.60	13.1	15.9	
	2600.0								8.60	13.1	14.4	1.39
ŝ.	2605.0	8: 7	93.0	45	135	9.1	9.0					
:	2610.0	8:10	107.7	44	135	9.1	9.0	9.3	8.60	13.1	16.1	1.35
-	12					· ~ •	~ ~		0.20	10.1	10.1	1 00
· .	2615.0	8:13	123.5	41	136	9.1	9.0	.9.3	8.60	13.1	19.1	1.28
•	2620.0	8:55	147.8		126	9.1	9.0	9.3		13.1		
	2625.0	8:26	86.3	42	123	9.1	9:0	9.3	8.60	13.1		
•	2630.0	8:29	105.6	43	125	9.1	9.0	9.3	8.60	13.1	17.2	
	2635.0.	8:31	125.9	42	127	9.1	9.0	9.3	8.60	13.1	19.9	1.25
•	2640.0	.8: 33	157.5	41	126	9.1	9.0	9.3	8,60	13.1		
		8:35	169.5	43	125	9.1	9.0	9.3	8.60	13.1	22.9	
•	2650.0	8:43	188.8	40	126	9.1	9.0	9.3	8.60	13.1	25.1	
	2655.0	8:45	174.3	32	133	9.1	9.0	9.3	8.60	13.1	29.0	1.08
•	2660.0	8:46	369.6	35	116	9.1	9.0	9.3	8.60	13.2	36.6	.85
	13	09					• .					
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ESSO BARRACOUTA # 4

с. Н.,											
	DEPTH TIME 1309	PDP	MDB	RPM	MDI	MDD	ECD.	PP	FG	PDR	DEXP
	2665.0 8:46	497.1	42	126	9.1	.9.0	9.3	8.60	13.2	35.3	.83
	2670.0 8:47		41	127	9.1	9.0	9.3	8.60	13.2	33.2	.90
•	2680.0 8:48	608.0	44	126	9.1	9.0	9.4	8.60	13.2	36.9	.77
	2690.0 8:59	595.7	41	123	9.1	9.0	9.3	8.60	13.2	37.3	.77
	2700.0 9:0		41	126	9.1	9.0	9.3	8.60	13.2	40.6	.69
	2710.0 9: 1		44	127	9.1	9.0	9.4	8.60	13.2	36.7	.79
	2720.0 9:12	368.1	28	113	9.1	9.0	9.3	8.60	13.2	41.1	.80
	2730.0 9:14	471.2	34	126	9.1	9.Ò	9.3	8.60	13.2	39.4	.79
	2740.0 9:15		46	122	9.1	9.0	9.3	8.60	13.2	34.4	.83
	2750.0 9:23	670.2	41	113	9.1	9.0	9.4	8.60	13.2	40.5	.69
	1320	0/0 E	45	a	~ •		~ .				•
	2760.0 9:24	368.5	45	124	9.1	9.0	9.4	8.60	13.2	30.4	.96
	2765.0 9:25 2770.0 9:26	311.4 482.5	46 45	125 127	9.1	9.0	9.4	8.60	13.2	28.9	1.00
	2775.0 9:35	40c.J 246.9	41	127 125	9.1 9.1	9.0 9.0	9.4 9.3	8.60	13.2	34.2	.85
	2780.0 9:35		39	113	9.1 9.1	9.0 9.0	7.3 9.4	8.60 8.60	13.2	29.0 44.5	1.03
	2790.0 9:36	514.2	43	116	9.1	9.0	9.4 9.4	8.60	13.2	44.J 37.0	.61 .79
۰.	2800.0 9:40	297.2	45	128	9.1	9.0	9.4	8.60	13.3	27.5	1.06
	2805.0 9:42	146.0	45	119	9.1	9.0	9.4	8.60	13.3	21.7	1.21
	2810.0 9:50	403.3	38	100	9.1	9.0	9.3	8.60	13.3	35.6	.86
	2820.0 9:52	388.2	44	119	9.1	9.0	9.3		13.3	32.2	.91
	1340										
	2830.0 9:53	630.6	34	137	9.1	9.0	9.3	8.60	13.3	36.5	.89
•		1369.0	45	110	9.1	9.0	9.4	8.60	13.3	46.8	.48
•		1237.0	33	105	9.1	9.0	9.4	8.60	13.3	52.3	.46
		1579.1	45	111	9.1	9.0	9.4	8.60	13.3	48.2	.44
÷	2870.0 10: 2	893.2	40	113	9.1	9.0	9.4	8.60	13.3	44.7	.60
	2880.0 10:13 2890.0 10:13	474.5 906.6	33	131		9.0	9.4	8.60	13.3	40.9	.82
	2895.0 10:13	302.2	44	122 123	9.1 9.1	9.0 9.0	9.4	8.60	13.3	42.3	.64
		1512.7	45	125	9.1	9.0 9.0	9.4 9.4	8.60 8.60	13.3 13.3	28.9 47.5	1.01
	2910.0 10:23	740.7	37	119	9.1	9.0	9.3	8.60	13.3 13.3	43.7	.49 .66
	1353						2.0	0.00		т Э т (.00
	2920.0 10:24	674.1	33	117	9.1	9.0	9.4	8.60	13.4	45.6	.66
	2925.0 10:25	190.7	46	119	9.1	9.0	9.4	8.60	13.4	25.1	1.13
	2930.0 10:26	229.2	46	124	9.1	9.0	9.4	8.60	13.4	27.2	1.07
	2935.0 10:36	162.3	45	119	9.1	9.0	9.4	8.60	13.4	24.3	1:16
	2940.0 10:37	226.1	47	130	9.1	9.0	9.4	8.60	13.4	25.8	1.11
	2950.0 10:38	1303.9	21	130	9.1	9.0	9.4	8.60	13.4	61.2	.45
	2960.0 36:24	542.7	5	79	8.6	8.6	8.6	8.60	13.4	82.8	.45
	2965.0 36:24 2970.0 36:24	123.1 126.6	4	85 os	8.6	8.6	8.6	8.60	13.4	76.8	.74
	2975.0 36:24	117.0	55	85 93	8.6 8.6	8.6	8.6	8.60	13.4	71.6	.75
	1374	111.00		20	0.0	8.6	8.6	8.60	13.4	69.0	.78
	2980.0 36:24	129.0	7	93	8.6	8.6	8.6	8.60	13.4	58.9	.81
	2985.0 36:24	105.3	5	95	8.6	8.6	8.6	8.60	13.4	63.4	.83
	2990.0 36:24	88.1	5	95	8.6	8.6	8.6	8.60	13.4	63.1	.86
	2995.0 36:24	79.9	5	82	8.6	8.6	8.6	8.60	13.4	64.9	.83
	3000.0 36:24	91.5	4	91	8.6	8.6	8.6	8.60	13.4	74.8	.81
	3005.0 36:24	84.0	4	90	8.6	8.6	8.6	8.60	13.4	74.0	.82
	3010.0 36:24	71.0	4	90	8.6	8.6	8.6	8.60	13.4	80.0	.84
	3015.0 36:24	81.0	3	90	8.6	8.6	8.6	8.60	13.4	95.7	.79
	3020.0 0: 0	45.2		90	8.6	8.6	.8.6	8.60		102.9	.89
	3025.0 0:2	80.5	4	91	8.6	8.6	8.6	8.60	13.4	75.7	.83
	1076										

ESSD BARRACOUTA # 4

	DEPTH 13	TIME	PDP	WOB	RPM	MDI	MDD	ECD	PP	FG	POR	DEXP
	3030.0 3035.0 3040.0 3045.0	0:10 0:49 0:53 0:57	47.3 32.7 55.7 53.3	4433	92 93 94 96	8.6 8.6 8.6 8.6	8.6 8.6 8.6 8.6	8.7 8.7 8.6 8.7	8.60 8.60 8.60 8.60	13.4 13.4 13.4 13.4	68.6 66.7 79.3 88.7	.96 1.08 .89 .89
	3050.0 3055.0 3060.0	1:13 1:31 2: 2	22.2 19.1 10.5	4 5 5	96 97 98	8.6 8.6 8.6	8.6 8.6 8.6	8.7 8.7 8.6	8.60 8.60 8.60	13.4 13.4 13.5	49.6 42.6	
	3065.0 3070.0 3075.0 143	2:20 2:23 2:34	43.2 42.4 33.7	500	94 102 87	8.6 8.6 8.6	8.6 8.6 8.6	8.6 8.6 8.7	8.60 8.60 8.60	13.5 13.5 13.5		1.00 .92 .98
	3080.0 3085.0 3090.0	2:51 3:18 3:38	18.9 12.6 27.2 22.2	4 4 4	87 88 105 125	8.6 8.6 8.6 8.6	8.6 8.6 8.6 8.6	8.7 8.7 8.6 8.6	8.60 8.60 8.60 8.60	13.5 13.5 13.5 13.5	64.8 57.5 53.2 51.2	1.08 1.19 1.15 1.19
	3095.0 3100.0 3105.0 3110.0	3:56 4:23 4:51 5:13	19.3 11.3 13.9	4 5 5	112 121 124	8.6 8.6 8.6	8.6 8.6 8.6	8.6 8.6 8.6	8.60 8.60 8.60	13.5 13.5 13.5	63.8 42.2 42.9	1.18 1.32 1.29
	3115.0 3120.0 3125.0 148	5:28 5:46 6: 7	23.7 17.5 15.3	5	124 130 154	8.6 8.6 8.6	8.6 8.6 8.6	8.6 8.6 8.6	8.60 8.60 8.60	13.5 13.5 13.5		1.21 1.26 1.30
	3130.0	6:36 6:55 7:11 7:30	14.6 16.0 19.7 16.1	សភ័ត្	153 156 155 156	8.6 8.6 8.6 8.6	8.6 8.6 8.6 8.6	8.6 8.6 8.6 8.6	8.60 8.60 8.60 8.60	13.5 13.5 13.5 13.5	42.2 41.7	1.32
	3150.0 3155.0 3160.0 3165.0	7:48 8: 7 8:29 8:42	16.5 16.2 23.2 22.9	5 6 7	154	8.6 8.6 8.6 8.6	8.6 8.6 8.6 8.6	8.6 8.6 8.6 8.6	8.60 8.60 8.60 8.60	13.5 13.5 13.5 13.5	41.9 38.7	1.31 1.28 1.25 1.31
	3170.0 3175.0 153	8:54 9:5 3	26.6 28.9	8	150 151	8.6 8.6	8.6 8.6	8.6 8.6	8.60 8.60	13.5 13.5	34.3 35.3	1.30 1.28
· · · ·	3190.0 3195.0	9:17 9:27 9:40 9:55	25.6 37.4	8 11	151 119	8.6	8.6	8.7 8.7	8.60 8.60 8.60 8.60	$13.5 \\ 13.5$	36.6 35.0 32.6	1.26 1.30 1.24
na na seu	3200.0 3201.0	10: 4 10: 7	28.2	7	141	8.6	8.6	8.7	8.60 8.60	13.6	38.8	1.24
1 A	3210.0 3215.0 3220.0	2:16 2:20 5:46	116.0 105.2 83.6 53.0	21 20	100 102	11.1	11.2 11.2 11.2	11.2	8.60	13.6	42.0	.98
T 2	15 3225.0 3230.0 3235.0 3240.0	5:47 5:49 5:54 5:58	68.0 67.0 64.9 73.0	19 23 22	86 87 90	11.1 11.1 11.1 11.1	11.2 11.2 11.2	11.2 11.2 11.2	8.60 8.60 8.60 8.60	13.6 13.6 13.6	41.7 37.8 39.8	.98 1.04 1.01
		6:2 6:6 6:10	88.6 76.9 77.2	20	106	11.1 11.1 11.1	11.2 11.2 11.2		8.60 8.60 8.60	13.6 13.6 13.6	40.7	

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ESSD BARRACOUTA # 4

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		ROP	MDB	RPM	MDI	MDD	ECD	ዮዮ	FG	PDR	DEXP
3260.0 3265.0 3270.0 3275.0 3280.0 3285.0 3290.0 3295.0 3300.0 3305.0	6:29 6:31 6:34 6:41 6:44 6:46 6:55 6:56 6:58 7: 0	91.0 111.3 130.0 118.0 120.8 127.1 131.8 154.1 165.4 145.8	21 23 24 24 24 23 25 25 26 28	126 125 107 122 125 129 125 129	11.1 11.1 11.1 11.1 11.1 11.1 11.1 11.	11.2 11.2 11.2 11.2 11.2 11.2 11.2 11.2	11.2 11.2 11.2 11.2 11.3 11.3 11.3 11.3	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	13.6 13.6 13.6 13.6 13.6 13.6 13.6 13.6	41.1 42.2 43.1 41.8 42.6 43.4 43.3	1.00 1.00 .96 .95 .98 .97 .96 .94 .94 .99
		< > >	17	07	4 4 4	44. 0	11 0	0 60	10 6	<i>A A E</i>	1 00
3315.0 3320.0 3325.0 3330.0 3335.0 3340.0 3345.0 3350.0 3355.0	7:13 7:29 7:40 7:48 7:56 8:4 8:13 8:22 8:27	63.9 46.1 62.2 28.3 36.0 36.4 39.3 37.7 79.1 62.3	17 12 10 12 13 14 14 15 18 16	92 89 86 99 92 91 95 95	11.1 11.1 11.1 11.1 11.1 11.2 11.2 11.2	11.2 11.2 11.2 11.2 11.2 11.2 11.2 11.2	11.3 11.2 11.2 11.2 11.2 11.2 11.3 11.3	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	13.6 13.6 13.6 13.6	48.9 52.7 43.4 43.5 42.7 43.6	$1.00 \\ .96 \\ .92 \\ 1.06 \\ 1.05 \\ 1.06 \\ 1.04 \\ 1.06 \\ .95 \\ .97 \\ .97 \\$
		62.0	16	1.03	11.2	11.2	11.3	8.60	13.7	45.3	. 99
3365.0 3370.0 3375.0 3380.0 3385.0 3390.0 3395.0 3400.0 3405.0	8:37 8:42 8:47 8:59 9:5 9:13 9:19 9:28 10:16	62.0 58.9 55.9 61.7 46.1 61.0 41.5 47.6 41.2 41.3	16 15 16 17 15 16 17 17 18 19	104 95 93 95 94 95 94 100	11.2 11.2 11.2 11.2 11.2 11.2 11.2 11.2	11.2 11.2 11.2 11.2	11.3 11.4 11.4 11.4	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	13.7 13.7 13.7 13.7 13.7 13.7 13.7	46.0 45.7 45.7 45.5 45.7 40.8 41.8	.99 .98 .97 1.00 .98 1.07 1.05 1.12 1.08
3410.0	10:38	30.0	19	99	11.2	11.2	11.3	8.60	13.7	33.2	1.23
		56.1 65.0 31.4 55.8 56.4 65.2 61.9 34.7 40.8	17 15 17 21 20 22 21 16 15	108 99 90 96 96 97 60	11.2 11.2 11.2 11.2 11.2 11.2 11.2 11.2	11.2 11.2 11.2 11.2 11.2 11.2 11.2 11.2	$11.3 \\ $	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	13.7 13.7 13.7 13.7 13.7 13.7 13.7 13.7	$43.1 \\ 46.8 \\ 37.8 \\ 40.1 \\ 40.4 \\ 40.7 \\ 40.6 \\ 44.4 \\ 47.2 \\ $	1.02 .97 1.15 1.05 1.05 1.04 1.04 1.00 .96
		42.8	12	63	11 2	11 2	11 3	8 60	13.7	52 K	.90
3465.0 3470.0 3475.0 3480.0 3485.0 3495.0 3495.0 3500.0	13:19 13:25 13:31 13:48 13:52 14:6 14:17 14:43 15:4	42.0 28.2 80.1 67.9 90.2 101.3 32.4 34.6 12.2 15.2	12 9 8 7 6 6 8 12 14	68 68 70 58 63 53 56	11.2 11.2 11.2 11.2 11.2 11.2 11.2 11.2	11.2 11.2 11.2 11.2 11.2 11.2 11.2 11.2	$ 11.3 \\ 11.4 \\ 11.3 \\ 11.3 $	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	13.7 13.7 13.7 13.7 13.7 13.7 13.7 13.7	54.2 66.4 67.6 65.5 76.4 59.9 41.5 39.5	.90 .93 .75 .77 .81 .65 .81 .85 1.12 1.13
	$\begin{array}{c} 16\\ 3260.0\\ 3265.0\\ 3270.0\\ 3270.0\\ 3275.0\\ 3280.0\\ 3290.0\\ 3290.0\\ 3295.0\\ 3300.0\\ 3305.0\\ 3315.0\\ 3315.0\\ 3320.0\\ 3325.0\\ 3325.0\\ 3335.0\\ 3340.0\\ 3345.0\\ 3355.0\\ 3345.0\\ 3355.0\\ 3360.0\\ 3365.0\\ 3375.0\\ 3365.0\\ 3375.0\\ 3365.0\\ 3375.0\\ 3385.0\\ 3375.0\\ 3385.0\\ 3390.0\\ 3385.0\\ 3395.0\\ 3395.0\\ 3395.0\\ 3395.0\\ 3395.0\\ 3395.0\\ 3395.0\\ 3395.0\\ 3400.0\\ 3405.0\\ 3405.0\\ 3405.0\\ 3405.0\\ 3405.0\\ 3405.0\\ 3445.0\\ 3455.0\\ 3455.0\\ 3485.0\\ 3490.0\\ 3495.0\\ 3495.0\\ 3495.0\\ 3495.0\\ 350$	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	1605 3260.0 $6:29$ 91.0 3265.0 $6:31$ 111.3 3270.0 $6:34$ 130.0 3275.0 $6:41$ 118.0 3280.0 $6:44$ 120.8 3285.0 $6:46$ 127.1 3290.0 $6:55$ 131.8 3295.0 $6:56$ 154.1 3300.0 $6:58$ 165.4 3305.0 $7:0$ 145.8 1653 3310.0 $7:6$ 63.9 3315.0 $7:13$ 46.1 3320.0 $7:49$ 28.3 3330.0 $7:48$ 36.0 3335.0 $7:56$ 36.4 3345.0 $8:13$ 37.7 3350.0 $8:27$ 62.3 1702 3360.0 $8:32$ 3365.0 $8:37$ 58.9 3375.0 $8:47$ 61.7 3380.0 $8:59$ 46.1 3395.0 $9:5$ 61.0 3390.0 $9:13$ 41.5 3395.0 $9:19$ 47.6 3400.0 $9:28$ 41.2 3405.0 $10:38$ 30.0 3415.0 $10:38$ 30.0 3415.0 $10:38$ 30.0 3415.0 $10:38$ 30.0 3410.0 $10:38$ 30.0 3415.0 $10:38$ 30.0 3410.0 $10:38$ 30.0 3415.0 $10:38$ 30.0 3415.0 $10:38$ 30.0 3445.0 $11:30$ 55.8 3435.0 <	1605 3260.0 $6:29$ 91.0 21 3265.0 $6:31$ 111.3 23 3270.0 $6:34$ 130.0 22 3275.0 $6:41$ 118.0 24 3280.0 $6:44$ 120.8 24 3285.0 $6:46$ 127.1 24 3295.0 $6:56$ 154.1 25 3300.0 $6:58$ 165.4 26 3305.0 $7:0$ 145.8 28 1653 3310.0 $7:6$ 63.9 17 3315.0 $7:13$ 46.1 12 3320.0 $7:48$ 36.0 13 3335.0 $7:56$ 36.4 14 3340.0 $8:4$ 39.3 14 3345.0 $8:13$ 37.7 15 3350.0 $8:22$ 79.1 18 3355.0 $8:32$ 62.0 16 3360.0 $8:32$ 62.0 16 3365.0 $8:37$ 58.9 15 3370.0 $8:42$ 55.9 16 3395.0 $9:5$ 61.0 16 3390.0 $9:13$ 41.5 17 3400.0 $9:28$ 41.2 18 3405.0 $10:43$ 30.0 19 3415.0 $10:41$ 56.1 17 3400.0 $9:13$ 41.5 17 3400.0 $11:30$ 55.8 21 3405.0 $10:53$ 31.4 17 3400.0 $11:45$ 61.9 2	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 1605\\ 2260,0 & 6:29\\ 3275,0 & 6:34\\ 111,3 & 23\\ 126\\ 111,1 & 11,2 & 11,2 & 8,60\\ 3275,0 & 6:44\\ 118,0 & 29\\ 125\\ 111,1 & 11,2 & 11,2 & 8,60\\ 3280,0 & 6:44\\ 120,8 & 24\\ 122\\ 111,1 & 11,2 & 11,2 & 8,60\\ 3280,0 & 6:44\\ 120,8 & 24\\ 122\\ 111,1 & 11,2 & 11,3 & 8,60\\ 3295,0 & 6:46\\ 127,1 & 24\\ 125\\ 111,1 & 11,2 & 11,3 & 8,60\\ 3295,0 & 6:56\\ 154,1 & 25\\ 125\\ 111,1 & 11,2 & 11,3 & 8,60\\ 3305,0 & 7: & 0 & 145,8 & 28\\ 126\\ 111,1 & 11,2 & 11,3 & 8,60\\ 3305,0 & 7: & 0 & 145,8 & 28\\ 126\\ 111,1 & 11,2 & 11,3 & 8,60\\ 3305,0 & 7: & 0 & 145,8 & 28\\ 126\\ 111,1 & 11,2 & 11,3 & 8,60\\ 3305,0 & 7: & 0 & 145,8 & 28\\ 126\\ 111,1 & 11,2 & 11,3 & 8,60\\ 3305,0 & 7: & 0 & 63,9 & 17\\ 97\\ 111,1 & 11,2 & 11,3 & 8,60\\ 3306,0 & 7: & 9 & 62,2 & 10 & 89\\ 111,1 & 11,2 & 11,2 & 8,60\\ 3326,0 & 7: & 86,4 & 13 & 99\\ 111,1 & 11,2 & 11,2 & 8,60\\ 3335,0 & 7: & 66,4,1 & 12 & 92\\ 111,1 & 11,2 & 11,2 & 8,60\\ 3335,0 & 7: & 66,4 & 13 & 99\\ 111,1 & 11,2 & 11,2 & 8,60\\ 3345,0 & 8: & 39,3 & 14 & 91\\ 111,2 & 11,2 & 11,2 & 8,60\\ 3345,0 & 8: & 13 & 37,7 & 15 & 95\\ 112,2 & 11,2 & 11,3 & 8,60\\ 3355,0 & 8: & 27 & 79,1 & 18 & 98\\ 112,2 & 11,2 & 11,3 & 8,60\\ 3365,0 & 8: & 27 & 79,1 & 18 & 98\\ 112,2 & 11,2 & 11,3 & 8,60\\ 3365,0 & 8: & 27 & 78,9 & 15 & 104\\ 112,2 & 11,2 & 11,3 & 8,60\\ 3360,0 & 8: & 32 & 62,0 & 16 & 103\\ 112,2 & 11,2 & 11,3 & 8,60\\ 3370,0 & 8: & 42 & 55,9 & 16 & 95\\ 112,2 & 11,2 & 11,3 & 8,60\\ 3390,0 & 8: & 59 & 46,1 & 15 & 95\\ 112,2 & 11,2 & 11,3 & 8,60\\ 3390,0 & 9: & 5 & 61,0 & 16 & 94\\ 112,2 & 11,2 & 11,3 & 8,60\\ 3390,0 & 9: & 19 & 47,6 & 17 & 94\\ 112,2 & 11,2 & 11,3 & 8,60\\ 3400,0 & 9: & 28 & 41,2 & 18 & 100\\ 112,2 & 11,2 & 11,3 & 8,60\\ 3400,0 & 9: & 114,4 & 65,1 & 17 & 103\\ 112,2 & 11,2 & 11,3 & 8,60\\ 3405,0 & 10: & 14 & 45,1 & 17 & 103\\ 112,2 & 11,2 & 11,3 & 8,60\\ 3405,0 & 10: & 14 & 45,1 & 17 & 103\\ 112,2 & 11,2 & 11,3 & 8,60\\ 3405,0 & 13: & 42,8 & 12 & 63\\ 112,2 & 112,2 & 11,3 & 8,60\\ 3405,0 & 13: & 42,8 & 12 & 63\\ 112,2 & 112,2 & 11,3 & 8,60\\ 3405,0 & 13: & 42,8 & 12 & 63\\ 112,2 & 112,2 & 113,3 & 8,60\\ 3405,0 & 13: & 42,8 & 12 & 96\\ 112,2 & $	$\begin{array}{c} 1605\\ 3260.0 & 6:29 & 91.0 & 21 & 106 & 11.1 & 11.2 & 11.2 & 8.60 & 13.6 \\ 3270.0 & 6:34 & 130.0 & 22 & 125 & 11.1 & 11.2 & 11.2 & 8.60 & 13.6 \\ 3270.0 & 6:41 & 120.8 & 24 & 107 & 11.1 & 11.2 & 11.2 & 8.60 & 13.6 \\ 3275.0 & 6:44 & 120.8 & 24 & 107 & 11.1 & 11.2 & 11.2 & 8.60 & 13.6 \\ 3285.0 & 6:44 & 120.8 & 24 & 102 & 11.1 & 11.2 & 11.3 & 8.60 & 13.6 \\ 3285.0 & 6:44 & 120.8 & 24 & 122 & 11.1 & 11.2 & 11.3 & 8.60 & 13.6 \\ 3295.0 & 6:55 & 131.8 & 23 & 129 & 11.1 & 11.2 & 11.3 & 8.60 & 13.6 \\ 3300.0 & 6:58 & 154.1 & 25 & 125 & 11.1 & 11.2 & 11.3 & 8.60 & 13.6 \\ 3300.0 & 6:58 & 154.1 & 25 & 125 & 11.1 & 11.2 & 11.3 & 8.60 & 13.6 \\ 3300.0 & 6:58 & 154.4 & 129 & 11.1 & 11.2 & 11.3 & 8.60 & 13.6 \\ 1653 & & & & & & & & & & & & & & & & & & &$	$\begin{array}{c} 1605 \\ 2260.0 \\ 6129 \\ 91.0 \\ 211 \\ 100 \\ 111.3 \\ 2275.0 \\ 6131 \\ 111.3 \\ 2275.0 \\ 6131 \\ 111.3 \\ 2275.0 \\ 6131 \\ 111.3 \\ 2275.0 \\ 6131 \\ 111.3 \\ 2275.0 \\ 6131 \\ 111.3 \\ 2275.0 \\ 6134 \\ 112.0 \\ 2275.0 \\ 6134 \\ 112.0 \\ 2275.0 \\ 6144 \\ 112.0 \\ 2275.0 \\ 6144 \\ 112.0 \\ 2275.0 \\ 6144 \\ 112.0 \\ 2275.0 \\ 6144 \\ 112.0 \\ 2275.0 \\ 6144 \\ 120.8 \\ 241 \\ 2211.1 \\ 111.2 \\ 11.2 \\ 11.3 \\ 8.60 \\ 13.6 \\ 43.6 \\ 43.6 \\ 3300.0 \\ 6155 \\ 131.8 \\ 23 \\ 120 \\ 111.1 \\ 11.2 \\ 11.3 \\ 8.60 \\ 13.6 \\ 43.6 \\ 43.3 \\ 3300.0 \\ 6158 \\ 155 \\ 125 \\ 125 \\ 111.1 \\ 11.2 \\ 11.3 \\ 8.60 \\ 13.6 \\ 43.6 \\ 43.3 \\ 3300.0 \\ 6158 \\ 155 \\ 125 \\ 125 \\ 111.1 \\ 11.2 \\ 11.3 \\ 8.60 \\ 13.6 \\ 43.6 \\ 3310.0 \\ 6158 \\ 1658 \\ 1658 \\ 1658 \\ 1658 \\ 1658 \\ 1658 \\ 1658 \\ 1658 \\ 1658 \\ 1658 \\ 125 \\ 127 \\ 128 \\ 111.1 \\ 11.2 \\ 11.3 \\ 8.60 \\ 13.6 \\ 43.6 \\ 13.6 \\ 44.5 \\ 3300.0 \\ 7140 \\ 23.1 \\ 2385.0 \\ 8113 \\ 37.7 \\ 159 \\ 911.1 \\ 11.2 \\ 11.2 \\ 11.2 \\ 11.2 \\ 11.2 \\ 8.60 \\ 13.6 \\ 42.7 \\ 3345.0 \\ 812 \\ 37.7 \\ 159 \\ 911.1 \\ 11.2 \\ 11.2 \\ 11.2 \\ 11.3 \\ 8.60 \\ 13.6 \\ 43.6 \\ 42.7 \\ 3345.0 \\ 812 \\ 75.8 \\ 128 \\ 128 \\ 112 \\ 11.2 \\ 11.2 \\ 11.3 \\ 8.60 \\ 13.7 \\ 45.8 \\ 3365.0 \\ 8127 \\ 58.9 \\ 15 \\ 91 \\ 12. \\ 11.2 \\ 11.2 \\ 11.2 \\ 11.3 \\ 8.60 \\ 13.7 \\ 45.7 \\ 3360.0 \\ 8142 \\ 55.9 \\ 16 \\ 91 \\ 11.2 \\ 11.2 \\ 11.2 \\ 11.3 \\ 8.60 \\ 13.7 \\ 45.7 \\ 3365.0 \\ 8127 \\ 58.9 \\ 15 \\ 91 \\ 12. \\ 11.2 \\ 11.2 \\ 11.3 \\ 8.60 \\ 13.7 \\ 45.7 \\ 3365.0 \\ 8127 \\ 58.9 \\ 15 \\ 91 \\ 12. \\ 11.2 \\ 11.2 \\ 11.3 \\ 8.60 \\ 13.7 \\ 45.7 \\ 3365.0 \\ 8137 \\ 58.9 \\ 15 \\ 11.2 \\ 11.2 \\ 11.3 \\ 8.60 \\ 13.7 \\ 45.7 \\ 3365.0 \\ 8137 \\ 58.9 \\ 15 \\ 100 \\ 11.2 \\ 11.2 \\ 11.3 \\ 8.60 \\ 13.7 \\ 45.7 \\ 3365.0 \\ 8137 \\ 58.9 \\ 15 \\ 100 \\ 11.2 \\ 11.2 \\ 11.3 \\ 8.60 \\ 13.7 \\ 45.7 \\ 3365.0 \\ 813 \\ 37.7 \\ 15 \\ 3365.0 \\ 813 \\ 37.7 \\ 15 \\ 3365.0 \\ 813 \\ 37.7 \\ 12 \\ 12. \\ 11.2 \\ 11.3 \\ 8.60 \\ 13.7 \\ 45.7 \\ 3365.0 \\ 113.7 \\ 45.8 \\ 11.2 \\ 11.2 \\ 11.3 \\ 8.60 \\ 13.7 \\ 45.7 \\ 3360 \\ 13.7 \\ 45.8 \\ 3365.0 \\ 13.7 \\ 45.8 \\ 12. \\ 11.2 \\ 11.3 \\ 8.60 \\ 13.7 \\ 45.8 \\ 3365.0 \\ 13.7 \\ 45.8 \\ 3365.0 \\ 13.7 \\ 45.8 \\ 3365.0 \\ 13.7 \\ 45.8 \\ 3365.0 \\ 13.7 \\ 45.8 \\ 14.8 \\ 11.2 \\ 11.2 \\$

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ESSD BARRACOUTA # 4

	ЛЕРТН 18		RDP	MDB	RPM	MDI	MDD	ECD	PP	FG	PDR	DEXP
ř,		15:14	145.6	10			11.2					
	3515.0	15:18	151.7	5								
1	3520.0	15:19	301.0	7								
t	3525.0	15:20	118.7	3								
	3530.0	15:21	153.0	5								
		15:40		2								
	3540.0		110.4									
		0 15:47 70.2 1 66 11.2 11.2 11.3 8.60 13.8 128.052										
5	3555.0		52.9	10	58	11.2	11.2	11.3	8.60	13.8	59.1	.82
÷	18				~ A		*		~ ~ ~			
d'	3560.0											
1												
1												
				$ \begin{array}{cccccccccccccccccccccccccccccccccccc$								
			4 		NEW 1	BIT ID	: 5					
:	3575.0	2:23	11.4	16	104	11.2	1111	11.3	8.60	13.8	26. 8	1 35
i	3580.0	10 10 66 11.2 11.3 8.60 13.8 38.4 1.20 10 17:30 27.6 10 65 11.2 11.3 8.60 13.8 49.0 1.00 10 17:40 17.9 12 64 11.2 11.3 8.60 13.8 42.5 1.08 NEW BIT ID: 5 NEW BIT ID: 5 0 2:23 11.4 16 104 11.2 11.1 11.3 8.60 13.8 26.8 1.35 .0 2:23 11.4 16 104 11.2 11.1 11.3 8.60 13.8 26.8 1.35 .0 3:3 9.5 18 103 11.2 11.1 11.3 8.60 13.8 23.2 1.43 .0 3:19 27.7 28 109 11.1 11.3 8.60 13.8 22.7 1.41										
1	3585.0											
. •	3590.0	3:29	103.3									
•	3595.0	3:31	192.2									
١, .	3600.0	3:39	486.4									
1	190						•	•				
1	3605.0	3:41	173.4									
	3610.0	3:43	167.9									
ł	3615.0	4:12	12.8									
ar C	3620.0	4:40	13.6									
-	3625.0	5:14	19.8									
•	3630.0	5:51	18.6									
	3635.0	6:20	27.3									
•	3640.0 3645.0	6:26 6:31	73.9 74.1									
	3650.0	6:38	74.1 38.5	-								
j_	1958		30.0	47	104	11.0	1111	11.4	0.00	10.0	10.0	
	3655.0	6:49	34.1	47	122	11.2	11.1	11.4	8.60	13.8	16.6	
1	3660.0	6:59	30.5									
	3665.0	7:18	29.7		-							
·	3670.0	7 : 28	29.0	47			11.1					
1	3675.0	7:41	25.0	47	117	11.2	11.1	11.4	8.60	13.9	15.2	1.62
÷	3680.0	7:51	28.1	46	118	11.2	11.1	11.4	8.60	13.9	16.6	1.58
	3685.0	8: 5	27.5	46	118	11.3	11.2	11.4	8.60	13.9	16.2	1.59
ì	3690.0	8:11	34.8	45		11.3	11.2	11.4	8.60	13.9	19.1	1.52
	3695.0	8:58	61.4	45		11.3	11.2	11.4	8.60	13.9	25.0	1.35
	3700.0	8:32	85.8	46	117	11.3	11.2	11.4	8.60	13.9	28.2	1.26
	200		~~ -	2 			Ì.		~ ~ *			
	3705.0	8:37 0:46	62.5 po o	45 44		11.3	11.2	11.4	8.60	13.9	24.6	1.37
•	3710.0 3715.0	8:46 8:50	38.9 79 0	44		11.3	11.2			13.9	20.3	1.50
. •	3713.0 3720.0	8:59	79.0 120.1	43 40		11.3 11.3	11.2	11.4	8.60 0 20	13.9	28.5	1.27
•	3725.0	8.J3 9: 1	115.6	31		11.3	11.2	$11.5 \\ 11.5$	8.60 8.60	13.9 13.9	33.5	1.14
	3730.0	9:6	58.0	31		11.3	11.2	11.5	8.60 8.60	13.9	36.7	1.10
	3735.0	9:10	32.9 82.9	30		11.3	11.2	11.5	8.60	13.9	32.1 35.4	1.22
	nart fadhart∎ Na	2 - 2 U		0.0	at has fail				0.00	1415		1.1.1

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	DEPTH 20		RDP	MOB	RPM	MDI	MDD	ECD	PP	F15	POR	DEXP
	3740.0 3745.0 3750.0 3755.0 3760.0 3765.0 3770.0 3775.0 3780.0 3785.0	9:15 9:16 9:19 9:21 9:29 9:32 9:33 9:38 9:47 9:57	77.6 169.7 135.3 128.1 186.5 113.7 291.7 77.7 43.7 67.5	31 31 29 24 22 16 13 13 13 18 17	124 120 120 120 114 102 106 103	$ \begin{array}{c} 11.3\\ 11.3\\ 11.3\\ 11.3\\ 11.3\\ 11.3\\ 11.3\\ 11.3\\ 11.3\\ 11.3\\ 11.3\\ 11.3\\ 11.3\\ \end{array} $	11.2 11.2 11.2 11.2 11.2 11.2 11.2 11.2	$ \begin{array}{r} 11.5\\ 11.5$	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.9	33.8 40.7 41.2 44.4 50.9 50.9 67.2 51.0 41.0 46.2	1.18 1.00 1.01 .97 .83 .90 .61 .93 1.09 .98
	20								~ ~ ~			
	3790.0 3795.0 3800.0 3805.0 3810.0 3815.0 3820.0 3825.0 3830.0 3835.0 21	10: 0 10: 4 10:13 10:22 10:25 10:28 10:28 10:38 10:42 10:49 11: 8	119.3 75.5 33.7 40.4 95.8 94.0 101.9 86.6 93.1 70.1	14 12 20 19 19 20 18 16	113 113 112 125 127 104 122 122	$ \begin{array}{c} 11.3\\ 11.3\\ 11.3\\ 11.3\\ 11.3\\ 11.3\\ 11.3\\ 11.3\\ 11.3\\ 11.3\\ 11.3\\ \end{array} $	11.2 11.2 11.2 11.2 11.2 11.2 11.2 11.2	$ \begin{array}{r} 11.5 \\ $	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	13.9 13.9 13.9 13.9 13.9 13.9 13.9 13.9	54.7 54.4 45.3 37.9 45.7 46.5 48.2 48.2 44.7 42.3 40.9	.85 .89 1.06 1.15 .98 .97 .92 1.00 1.07 1.13
			14 6	00		11.3	11.2	11.4	8.60	14 0	18.7	1.57
	3840.0 3845.0 3850.0 3855.0 3860.0 3865.0 3875.0 3875.0 3880.0 3885.0	11:42 11:50 12:1 12:22 12:39 12:47 13:2 13:13 13:29 13:36	14.6 38.8 79.0 15.3 19.1 39.6 23.3 27.4 28.8 71.3	29 33 37 38 40 39 40 -39 31	110 103 114 111 108 116 115 111	11.3 11.3 11.3 11.3 11.3 11.3 11.3 11.3	11.2 11.2 11.2	$11.4 \\ $	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	$14.0 \\ $	18.7 27.6 33.6 15.8 17.3 25.1 19.3 20.7 22.1 32.0	1.37 1.33 1.16 1.65 1.60 1.39 1.55 1.51 1.47 1.23
	2164		•									
	3890.0 3895.0 3900.0 3905.0 3910.0 3915.0 3920.0 3925.0 3930.0 3935.0	13:47 14:1 14:23 14:35 14:49 15:19 15:38 15:49 15:58 16:8	29.4 29.4 16.5 23.7 23.1 20.7 29.6 33.5 31.5	37 39 39 38 40 46 45 44 44	115 120 136 119 124 117 121 122	11.3 11.3		11.4 11.4 11.4	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	$14.0 \\ $	22.4 21.7 14.8 19.2 19.6 16.0 14.1 19.0 20.4 19.9	1.47 1.48 1.56 1.55 1.65 1.70 1.56 1.52 1.54
	2214		.		4.55.4				~ ~ ~	4.4 0		
•	3940.0 3945.0 3950.0 3955.0 3960.0 3965.0 3970.0 3975.0 3980.0 3985.0 2261	17:11 17:22 17:41 17:48 17:57	24.2 58.6 33.7 59.8 50.4 22.3 28.0 32.2 63.4 34.4	444544444555 44444555 44555	110 128 124 124 132 132 128 112	11.3 11.3 11.3 11.3 11.3 11.3 11.3 11.3	11.2 11.2 11.2 11.2 11.2 11.2 11.2 11.2	$11.4 \\ $	8.60 8.60 8.60 8.60 8.60 8.60 8.60 8.60	$14.0 \\ $	17.2 25.7 19.3 26.0 23.8 16.3 18.5 19.7 26.1 21.2	$1.62 \\ 1.36 \\ 1.56 \\ 1.37 \\ 1.43 \\ 1.65 \\ 1.59 \\ 1.55 \\ 1.36 \\ 1.51 $

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ESSD BARRACOUTA # 4

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$\begin{array}{cccccccccccccccccccccccccccccccccccc$. No						•						
$\begin{array}{c} 3990.0 \ 18:4 \ 34.4 \ 45 \ 119 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.0 \ 21.0 \ 1.51 \ 32.3 \ 1.8 \ 3995.0 \ 18:16 \ 61.7 \ 46 \ 115 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 22.5 \ 1.5 \ 4005.0 \ 18:12 \ 01.8 \ 0.2 \ 45 \ 124 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 22.5 \ 1.5 \ 1.5 \ 10.0 \ 18:59 \ 14.5 \ 45 \ 124 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 12.9 \ 1.4 \ 405.0 \ 19:12 \ 32.3 \ 49 \ 135 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 12.9 \ 1.4 \ 405.0 \ 19:12 \ 32.3 \ 49 \ 135 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 12.9 \ 1.7 \ 4025.0 \ 19:14 \ 17.3 \ 49 \ 135 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 15.1 \ 1.7 \ 4025.0 \ 19:14 \ 17.3 \ 49 \ 135 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 15.1 \ 1.7 \ 4035.0 \ 20:0 \ 9 \ 32.5 \ 48 \ 140 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 15.1 \ 1.7 \ 4035.0 \ 20:0 \ 9 \ 32.5 \ 48 \ 140 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 15.7 \ 1.5 \ 8.60 \ 14.1 \ 15.7 \ 1.5 \ 8.60 \ 14.1 \ 15.7 \ 1.5 \ 8.60 \ 14.1 \ 15.7 \ 1.5 \ 8.60 \ 14.1 \ 15.7 \ 1.5 \ 8.60 \ 14.1 \ 15.7 \ 1.5 \ 8.60 \ 14.1 \ 15.7 \ 1.5 \ 8.60 \ 14.1 \ 15.7 \ 1.5 \ 8.60 \ 14.1 \ 15.7 \ 1.5 \ 8.60 \ 14.1 \ 15.7 \ 1.5 \ 8.60 \ 14.2 \ 15.7 \ 1.5 \ 8.60 \ 14.2 \ 15.7 \ 1.5 \ 8.60 \ 14.2 \ 15.7 \ 1.5 \ 8.60 \ 14.2 \ 15.7 \ 1.5 \ 8.60 \ 14.2 \ 15.7 \ 1.5 \ 8.60 \ 14.2 \ 15.7 \ 1.5 \ 8.60 \ 14.2 \ 15.7 \ 1.5 \ 8.60 \ 14.2 \ 15.7 \ 1.5 \ 8.60 \ 14.2 \ 15.7 \ 1.5 \ $				RDP	WDB	PPM	MDI	MID	ECD	PP	FG	POP	DEXP
$\begin{array}{c} 4000.0 \ 18:20 \ 122.0 \ 44 \ 114 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 22.3 \ 1.18 \ 4005.0 \ 18:59 \ 14.5 \ 45 \ 124 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 12.9 \ 1.74 \ 4015.0 \ 19:17 \ 25.3 \ 47 \ 125 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 12.9 \ 1.74 \ 4015.0 \ 19:17 \ 25.3 \ 47 \ 125 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 11.7 \ 8 \ 1.61 \ 4025.0 \ 19:46 \ 17.3 \ 48 \ 143 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 11.7 \ 8 \ 1.61 \ 4025.0 \ 19:46 \ 17.3 \ 48 \ 143 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 11.7 \ 8 \ 1.61 \ 4025.0 \ 19:46 \ 17.3 \ 48 \ 143 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 11.7 \ 8 \ 1.61 \ 4025.0 \ 20:9 \ 32.2 \ 47 \ 133 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 18.7 \ 1.59 \ 2307 \ 20.9 \ 32.5 \ 48 \ 140 \ 11.2 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 18.7 \ 1.59 \ 2307 \ 20.9 \ 32.2 \ 47 \ 133 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 18.7 \ 1.59 \ 2405.0 \ 20:9 \ 32.2 \ 47 \ 133 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 18.7 \ 1.59 \ 4050.0 \ 20:9 \ 32.2 \ 47 \ 133 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 18.7 \ 1.59 \ 4055.0 \ 20:9 \ 32.6 \ 48 \ 128 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 18.7 \ 1.59 \ 4055.0 \ 20:5 \ 23.0 \ 48 \ 128 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 18.7 \ 1.59 \ 4055.0 \ 20:5 \ 23.0 \ 48 \ 128 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 17. \ 159 \ 4055.0 \ 20:5 \ 22.1 \ 09 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 14.7 \ 157 \ 156 \ 4075.0 \ 21:3 \ 72.2 \ 40 \ 40.1 \ 40.2 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 40.4 \ 4$	÷.	3990.0	18: 4										
$\begin{array}{c} 4015.0 & 19:17 & 25.3 & 47 & 136 & 11.3 & 11.2 & 11.4 & 8.60 & 14.1 & 14.5 & 1.71 \\ 4020.0 & 19:28 & 34.3 & 49 & 135 & 11.3 & 11.2 & 11.4 & 8.60 & 14.1 & 11. & 11.61 \\ 4025.0 & 19:46 & 17.3 & 48 & 143 & 11.2 & 11.4 & 8.60 & 14.1 & 15.1 & 1.70 \\ 4030.0 & 20:0 & 25.7 & 48 & 140 & 11.3 & 11.2 & 11.4 & 8.60 & 14.1 & 18.7 & 1.59 \\ 4040.0 & 20:27 & 2207 & 210.2 & 11.2 & 11.4 & 8.60 & 14.2 & 19.1 & 1.5 & 207 & 2007 & 2$		3995.0											
$\begin{array}{c} 4015.0 & 19:17 & 25.3 & 47 & 136 & 11.3 & 11.2 & 11.4 & 8.60 & 14.1 & 14.5 & 1.71 \\ 4020.0 & 19:28 & 34.3 & 49 & 135 & 11.3 & 11.2 & 11.4 & 8.60 & 14.1 & 17.8 & 1.61 \\ 4025.0 & 19:46 & 17.3 & 48 & 143 & 11.2 & 11.4 & 8.60 & 14.1 & 15.1 & 1.70 \\ 4030.0 & 20:0 & 25.7 & 48 & 140 & 11.3 & 11.2 & 11.4 & 8.60 & 14.1 & 18.7 & 1.59 \\ 4040.0 & 20:75 & 32.2 & 47 & 133 & 11.3 & 11.2 & 11.4 & 8.60 & 14.1 & 18.7 & 1.59 \\ 4045.0 & 20:33 & 40.1 & 47 & 117 & 11.3 & 11.2 & 11.4 & 8.60 & 14.1 & 18.7 & 1.59 \\ 4045.0 & 20:45 & 32.2 & 47 & 133 & 11.3 & 11.2 & 11.4 & 8.60 & 14.1 & 12.7 & 1.48 \\ 4055.0 & 20:52 & 33.0 & 48 & 132 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 19.7 & 1.58 \\ 4055.0 & 20:52 & 33.0 & 48 & 132 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 19.1 & 1.58 \\ 4065.0 & 21:19 & 16.1 & 48 & 140 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 19.1 & 1.58 \\ 4065.0 & 21:19 & 16.1 & 48 & 140 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 41.5 & 91 \\ 4070.0 & 21:37 & 223.0 & 44 & 96 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 41.5 & 91 \\ 4090.0 & 21:37 & 223.0 & 34 & 102 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 47.0 & 79 \\ 4085.0 & 21:38 & 227.0 & 38 & 102 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 52.2 & .68 \\ 4095.0 & 21:40 & 409.1 & 32 & 84 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 54.0 & .64 \\ 4100.0 & 21:53 & 23.6 & 29 & 91 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 54.0 & .79 \\ 4105.0 & 21:53 & 23.6 & 29 & 91 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 54.0 & .74 \\ 4115.0 & 23:0 & 135.3 & 29 & 78 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & .70 \\ 4125.0 & 01:41 & 7.9 & 44 & 125 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & .138 \\ 4135.0 & 11:1 & 142.1 & 42 & 124 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & .138 \\ 4145.0 & 11:1 & 39.6 & 43 & 122 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & .138 \\ 4145.0 & 11:1 & 39.6 & 43 & 121 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & .148 \\ 4155.0 & 11:3 & 91.5 & 42.0 & 91 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & .148 \\ 4156.0 & 1:43 & 44.5 & 42 & 109 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & .148 \\ 4156.0 & 1:43 & 44.5 & 42 & 109 & 11.3 & 11.2 &$	ŗ	4000.0											
$\begin{array}{c} 4015.0 & 19:17 & 25.3 & 47 & 136 & 11.3 & 11.2 & 11.4 & 8.60 & 14.1 & 14.5 & 1.71 \\ 4020.0 & 19:28 & 34.3 & 49 & 135 & 11.3 & 11.2 & 11.4 & 8.60 & 14.1 & 17.8 & 1.61 \\ 4025.0 & 19:46 & 17.3 & 48 & 143 & 11.2 & 11.4 & 8.60 & 14.1 & 15.1 & 1.70 \\ 4030.0 & 20:0 & 25.7 & 48 & 140 & 11.3 & 11.2 & 11.4 & 8.60 & 14.1 & 18.7 & 1.59 \\ 4040.0 & 20:75 & 32.2 & 47 & 133 & 11.3 & 11.2 & 11.4 & 8.60 & 14.1 & 18.7 & 1.59 \\ 4045.0 & 20:33 & 40.1 & 47 & 117 & 11.3 & 11.2 & 11.4 & 8.60 & 14.1 & 18.7 & 1.59 \\ 4045.0 & 20:45 & 32.2 & 47 & 133 & 11.3 & 11.2 & 11.4 & 8.60 & 14.1 & 12.7 & 1.48 \\ 4055.0 & 20:52 & 33.0 & 48 & 132 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 19.7 & 1.58 \\ 4055.0 & 20:52 & 33.0 & 48 & 132 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 19.1 & 1.58 \\ 4065.0 & 21:19 & 16.1 & 48 & 140 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 19.1 & 1.58 \\ 4065.0 & 21:19 & 16.1 & 48 & 140 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 41.5 & 91 \\ 4070.0 & 21:37 & 223.0 & 44 & 96 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 41.5 & 91 \\ 4090.0 & 21:37 & 223.0 & 34 & 102 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 47.0 & 79 \\ 4085.0 & 21:38 & 227.0 & 38 & 102 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 52.2 & .68 \\ 4095.0 & 21:40 & 409.1 & 32 & 84 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 54.0 & .64 \\ 4100.0 & 21:53 & 23.6 & 29 & 91 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 54.0 & .79 \\ 4105.0 & 21:53 & 23.6 & 29 & 91 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 54.0 & .74 \\ 4115.0 & 23:0 & 135.3 & 29 & 78 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & .70 \\ 4125.0 & 01:41 & 7.9 & 44 & 125 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & .138 \\ 4135.0 & 11:1 & 142.1 & 42 & 124 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & .138 \\ 4145.0 & 11:1 & 39.6 & 43 & 122 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & .138 \\ 4145.0 & 11:1 & 39.6 & 43 & 121 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & .148 \\ 4155.0 & 11:3 & 91.5 & 42.0 & 91 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & .148 \\ 4156.0 & 1:43 & 44.5 & 42 & 109 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & .148 \\ 4156.0 & 1:43 & 44.5 & 42 & 109 & 11.3 & 11.2 &$	ļ,	4005.0											
$\begin{array}{c} 4020.0 \ 19:28 \ 34.3 \ 48 \ 135 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 17.8 \ 1.61 \ 4025.0 \ 19:46 \ 17.3 \ 48 \ 143 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 15.1 \ 1.70 \ 4035.0 \ 20:9 \ 33.5 \ 48 \ 140 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 15.1 \ 1.70 \ 4035.0 \ 20:9 \ 33.5 \ 48 \ 140 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 18.7 \ 1.59 \ 2007 \ 4045.0 \ 20:25 \ 32.2 \ 47 \ 133 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 18.7 \ 1.59 \ 4045.0 \ 20:25 \ 32.2 \ 47 \ 133 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 18.7 \ 1.59 \ 4045.0 \ 20:26 \ 32.2 \ 47 \ 133 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 18.7 \ 1.59 \ 4045.0 \ 20:26 \ 33.0 \ 48 \ 132 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 18.7 \ 1.59 \ 4055.0 \ 20:42 \ 31.2 \ 48 \ 128 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 18.7 \ 1.59 \ 4055.0 \ 20:42 \ 33.0 \ 48 \ 132 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 19.1 \ 1.58 \ 4050.0 \ 21:39 \ 90.5 \ 22 \ 109 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 19.1 \ 1.58 \ 4050.0 \ 21:37 \ 223.0 \ 44 \ 96 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 49.4 \ .95 \ 4075.0 \ 21:37 \ 223.0 \ 38 \ 102 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 49.4 \ .95 \ 4075.0 \ 21:37 \ 223.0 \ 38 \ 102 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 49.4 \ .95 \ 4055.0 \ 21:39 \ 40.5 \ 22:52 \ 90 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 49.4 \ .95 \ 4055.0 \ 21:39 \ 40.5 \ 22:52 \ 90 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 45.0 \ .97 \ 4065.0 \ 21:39 \ 40.5 \ 22:52 \ 60 \ 91 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 45.0 \ .97 \ 4065.0 \ 21:40 \ 40.5 \ 11.9 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 45.0 \ .97 \ 4065.0 \ 21:40 \ 40.5 \ 11.40 \ 40.1 \ 40.5 $													
$\begin{array}{c} 4025.0 & 19:46 & 17.3 & 48 & 143 & 11.8 & 11.2 & 11.4 & 8.60 & 14.1 & 11.9 & 1.80 \\ 4030.0 & 20:0 & 25.7 & 48 & 140 & 11.3 & 11.2 & 11.4 & 8.60 & 14.1 & 15.1 & 1.70 \\ 4035.0 & 20:0 & 33.5 & 48 & 140 & 11.3 & 11.2 & 11.4 & 8.60 & 14.1 & 18.7 & 1.59 \\ 2307 \\ \hline \\ 4040.0 & 20:25 & 32.2 & 47 & 133 & 11.3 & 11.2 & 11.4 & 8.60 & 14.1 & 22.1 & 1.48 \\ 4050.0 & 20:42 & 31.2 & 48 & 128 & 11.3 & 11.2 & 11.4 & 8.60 & 14.1 & 22.1 & 1.48 \\ 4055.0 & 20:52 & 33.0 & 48 & 132 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 19.9 & 1.58 \\ 4065.0 & 21:0 & 36.0 & 48 & 134 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 19.9 & 1.58 \\ 4065.0 & 21:19 & 16.1 & 48 & 140 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 19.9 & 1.58 \\ 4070.0 & 21:35 & 90.5 & 22 & 109 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 41.5 & .91 \\ 4070.0 & 21:35 & 90.5 & 22 & 109 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 47.0 & .99 \\ 4080.0 & 21:39 & 419.7 & 33 & 101 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 47.6 & .81 \\ 2344 \\ 4090.0 & 21:39 & 419.7 & 33 & 101 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 52.2 & .68 \\ 4095.0 & 21:40 & 409.1 & 32 & 84 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 54.0 & .64 \\ 4100.0 & 21:59 & 419.7 & 33 & 101 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 54.0 & .79 \\ 4105.0 & 22:50 & 73.4 & 29 & 78 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 54.0 & .74 \\ 4120.0 & 0:3 & 6.3 & 35 & 102 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 9.1 & 1.34 \\ 4140.0 & 0:58 & 46.5 & 43 & 122 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.2 & 1.43 \\ 4140.0 & 0:58 & 46.5 & 43 & 132 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & 1.34 \\ 4140.0 & 11.9 & 36.4 & 42 & 126 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & 1.34 \\ 4140.0 & 11.9 & 36.4 & 42 & 126 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & 1.43 \\ 4140.0 & 11.9 & 36.4 & 42 & 126 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & 1.43 \\ 41450.0 & 1133 & 19.5 & 42 & 120 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & 1.43 \\ 41450.0 & 1133 & 19.5 & 42 & 120 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & 1.43 \\ 4150.0 & 1133 & 19.5 & 42 & 120 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & 1.43 \\ 4150.0 & 1133 & 19.5 & $	(
$\begin{array}{c} 4030.0 \ 201 \ 0 \ 25.7 \ 48 \ 140 \ 11.2 \ 11.4 \ 11.4 \ 8.60 \ 14.1 \ 15.1 \ 1.70 \ 2017 \ 2017 \ 33.5 \ 48 \ 140 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 18.7 \ 1.59 \ 2017 \ 4045.0 \ 20132 \ 40.1 \ 47 \ 117 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 18.7 \ 1.59 \ 4045.0 \ 20132 \ 40.1 \ 47 \ 117 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.1 \ 18.7 \ 1.59 \ 4055.0 \ 20132 \ 33.0 \ 48 \ 132 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 18.7 \ 1.59 \ 4055.0 \ 20132 \ 33.0 \ 48 \ 132 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 18.7 \ 1.59 \ 4055.0 \ 21139 \ 16.1 \ 48 \ 140 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 19.1 \ 1.58 \ 4055.0 \ 21139 \ 16.1 \ 48 \ 140 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 19.9 \ 1.56 \ 4055.0 \ 21139 \ 16.1 \ 48 \ 140 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 49.4 \ .55 \ 4055.0 \ 21139 \ 16.1 \ 48 \ 140 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 47.0 \ .79 \ 4065.0 \ 21139 \ 225.0 \ 44 \ 96 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 47.0 \ .79 \ 4065.0 \ 21139 \ 225.0 \ 44 \ 96 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 47.0 \ .79 \ 4065.0 \ 21139 \ 419.7 \ 33 \ 101 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 47.0 \ .79 \ 4065.0 \ 21139 \ 419.7 \ 33 \ 101 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 42.6 \ .81 \ 25344 \ 4090.0 \ 21138 \ 225.4 \ 29 \ 79 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 42.6 \ .81 \ 25344 \ 4090.0 \ 21138 \ 22.4 \ 409.1 \ 32.7 \ 77 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 24.8 \ .81 \ .79 \ 4105.0 \ 21139 \ 22.4 \ 409.1 \ 32.7 \ 77 \ 11.3 \ 11.2 \ 11.4 \ 8.60 \ 14.2 \ 24.8 \ .81 \ .79 \ 4105.0 \ 21139 \ 22.4 \ 41.6 \ .81 \ .27 \ 4105.0 \ 22.5 \ 21.4 \ 4100.0 \ 21138 \ 22.4 \ 41.4 \ .41.5 \ .41 \$	(
$\begin{array}{c} 4035.\ 0\ \ 2012\ 9\ \ 33.5\ \ 48\ \ 140\ \ 11.3\ \ 11.2\ \ 11.4\ \ 8.60\ \ 14.1\ \ 18.8\ \ 1.59\\ \hline 4040.\ 0\ \ 2012\ \ 32.2\ \ 47\ \ 133\ \ 11.3\ \ 11.2\ \ 11.4\ \ 8.60\ \ 14.1\ \ 18.7\ \ 1.59\\ \hline 4045.\ 0\ \ 2012\ \ 32.2\ \ 47\ \ 133\ \ 11.3\ \ 11.2\ \ 11.4\ \ 8.60\ \ 14.1\ \ 18.7\ \ 1.59\\ \hline 4055.\ \ 2012\ \ 32.2\ \ 32.2\ \ 47\ \ 133\ \ 11.3\ \ 11.2\ \ 11.4\ \ 8.60\ \ 14.1\ \ 18.7\ \ 1.59\\ \hline 4055.\ \ 2015\ \ 32.0\ \ \ 48\ \ 128\ \ 11.3\ \ 11.2\ \ 11.4\ \ 8.60\ \ 14.2\ \ 19.7\ \ 1.59\\ \hline 4065.\ \ 2015\ \ 32.0\ \ \ 48\ \ 132\ \ 11.3\ \ 11.2\ \ 11.4\ \ 8.60\ \ 14.2\ \ 19.7\ \ 1.59\\ \hline 4065.\ \ 2015\ \ 32.0\ \ \ 48\ \ 132\ \ 11.3\ \ 11.2\ \ 11.4\ \ 8.60\ \ 14.2\ \ 19.7\ \ 1.59\\ \hline 4065.\ \ 2110\ \ 0\ \ 2110\ \ 36.0\ \ \ 48\ \ 134\ \ 11.3\ \ 11.2\ \ 11.4\ \ 8.60\ \ 14.2\ \ 19.7\ \ 1.59\\ \hline 4075.\ \ 21137\ \ 223.0\ \ \ 44\ \ 96\ \ 11.3\ \ 11.2\ \ 11.4\ \ 8.60\ \ 14.2\ \ 49.4\ \ .95\\ \hline 4075.\ \ 21138\ \ 327.\ \ 38\ \ 102\ \ 11.3\ \ 11.2\ \ 11.4\ \ 8.60\ \ 14.2\ \ 47.\ \ 0\ \ .79\\ \hline 4085.\ \ 21138\ \ 327.\ \ 38\ \ 102\ \ 11.3\ \ 11.2\ \ 11.4\ \ 8.60\ \ 14.2\ \ 47.\ \ 0\ \ .79\\ \hline 4085.\ \ 21138\ \ 327.\ \ 38\ \ 102\ \ 11.3\ \ 11.2\ \ 11.4\ \ 8.60\ \ 14.2\ \ 47.\ \ 0\ \ .79\\ \ 4085.\ \ 21138\ \ 327.\ \ 38\ \ 102\ \ 11.3\ \ 11.2\ \ 11.4\ \ 8.60\ \ 14.2\ \ 47.\ \ 0\ \ .79\\ \ 4085.\ \ 21138\ \ 327.\ \ 38\ \ 11.3\ \ 11.2\ \ 11.4\ \ 8.60\ \ 14.2\ \ 47.\ \ 1.79\ \ 1.46\ \ 41.2\ \ 41.5\ \ .79\ \ 4085.\ \ 1.42\ \ 41.3\ \ 11.2\ \ 11.4\ \ 11.4\ \ 11.4\ \ 14.6\ \ 14.2\ \ 54.\ \ 0\ \ 14.2\ \ 41.5\ \ .79\ \ 1.41\ \ 11.4$													
$\begin{array}{c} 2307 \\ 4040.0 & 20125 & 38.2 \\ 4045.0 & 20133 & 40.1 \\ 4050.0 & 20142 & 31.2 \\ 4050.0 & 20142 & 31.2 \\ 41250.0 & 20142 & 31.2 \\ 41250.0 & 20142 & 31.2 \\ 41250.0 & 20142 & 31.2 \\ 41250.0 & 20142 & 31.2 \\ 41250.0 & 20142 & 31.2 \\ 41250.0 & 20142 & 31.2 \\ 41250.0 & 20142 & 31.2 \\ 41250.0 & 20142 & 31.2 \\ 41250.0 & 21133 & 223.0 \\ 41250.0 & 21135 & 90.5 \\ 41250.0 & 21137 & 223.0 \\ 41250.0 & 21137 & 223.0 \\ 41250.0 & 21137 & 223.0 \\ 41250.0 & 21138 & 327.0 \\ 41250.0 & 21138 & 327.0 \\ 41250.0 & 21138 & 327.0 \\ 41250.0 & 21138 & 327.0 \\ 41250.0 & 21138 & 223.0 \\ 414 & 96 & 11.3 & 11.2 \\ 11.4 & 8.60 & 14.2 & 47.0 \\ 41250.0 & 21138 & 223.0 \\ 41250.0 & 21138 & 223.0 \\ 41250.0 & 21138 & 228.2 \\ 41250.0 & 21138 & 228.2 \\ 41250.0 & 21138 & 228.2 \\ 41250.0 & 21138 & 419.7 \\ 4105.0 & 22138 & 419.7 \\ 4105.0 & 22138 & 419.7 \\ 4105.0 & 22138 & 236.6 & 29 \\ 4110.0 & 22153 & 236.6 & 29 \\ 4110.0 & 22153 & 236.6 & 29 \\ 4110.0 & 22153 & 236.6 & 29 \\ 4110.0 & 22153 & 236.6 & 29 \\ 4111.3 & 11.2 & 11.4 & 8.60 & 14.2 & 54.0 \\ 41250.0 & 0141 & 7.9 & 44 \\ 41251.0 & 0141 & 7.9 & 44 \\ 41251.0 & 0141 & 7.9 & 44 \\ 41251.0 & 0141 & 7.9 & 44 \\ 41251.0 & 0141 & 7.9 & 44 \\ 41251.0 & 0141 & 7.9 & 44 \\ 41261.0 & 117 & 39.6 & 43 \\ 4130.0 & 0158 & 46.5 & 43 \\ 4131 & 11.2 & 11.4 & 8.60 & 14.2 & 24.2 \\ 41435.0 & 11.1 & 1142.1 & 42 \\ 124 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 25.1 \\ 1.48 \\ 41450.0 & 1143 & 44.5 & 42 \\ 109 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 \\ 1.44 \\ 4165.0 & 2132 & 32.0 & 38 \\ 114 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 \\ 1.44 \\ 4165.0 & 2132 & 32.0 & 38 \\ 114 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 \\ 1.47 \\ 4165.0 & 2132 & 32.0 & 38 \\ 114 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 \\ 1.47 \\ 4165.0 & 2132 & 32.0 & 38 \\ 114 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 \\ 1.44 \\ 4250.0 & 3135 & 16.9 & 43 \\ 119 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 \\ 1.44 \\ 4260.0 & 3135 & 16.9 & 43 \\ 119 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 \\ 1.44 \\ 4260.0 & 3135 & 16.9 & 41 \\ 119 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 \\ 1.44 \\ 4260.0 $													
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$\begin{array}{c} 4070.0 \\ 21135 \\ 90.5 \\ 22137 \\ 2034 \\ 20344 \\ 2034$													
$\begin{array}{c} 4075, 0 & 21:37 & 223.0 & 44 & 96 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 41.5 & .91 \\ 4080, 0 & 21:38 & 327.0 & 38 & 102 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 47.0 & .79 \\ 4085, 0 & 21:38 & 282.2 & 36 & 102 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 46.6 & .81 \\ 2344 & 4090, 0 & 21:39 & 419.7 & 33 & 101 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 52.2 & .68 \\ 4095, 0 & 21:39 & 419.7 & 33 & 101 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 52.2 & .68 \\ 4095, 0 & 21:40 & 409.1 & 32 & 84 & 11.3 & 11.2 & 11.5 & 8.60 & 14.2 & 54.0 & .64 \\ 4100, 0 & 21:51 & 119.2 & 17 & 77 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 54.0 & .79 \\ 4105, 0 & 22:53 & 23.6 & 29 & 91 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 26.8 & 1.35 \\ 4110, 0 & 22:58 & 73.4 & 29 & 78 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 28.7 & 1.04 \\ 4115, 0 & 23: 0 & 135.3 & 29 & 78 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 9.1 & 1.84 \\ 4125, 0 & 0:41 & 7.9 & 44 & 125 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 9.1 & 1.84 \\ 4125, 0 & 0:58 & 46.5 & 43 & 122 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.2 & 1.43 \\ 4130, 0 & 0:58 & 46.5 & 43 & 122 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.2 & 1.43 \\ 4145, 0 & 1:1 & 142.1 & 42 & 124 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.5 & 1.48 \\ 4145, 0 & 1:1 & 39.6 & 4 & 42 & 126 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.5 & 1.48 \\ 4145, 0 & 1:33 & 19.5 & 42 & 120 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.4 & 1.42 \\ 4160, 0 & 2:12 & 15.2 & 38 & 115 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 21.4 & 1.52 \\ 4170, 0 & 2:51 & 15.9 & 39 & 127 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 21.4 & 1.52 \\ 4170, 0 & 2:51 & 15.9 & 39 & 127 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 21.4 & 1.52 \\ 4190, 0 & 3:35 & 16.9 & 43 & 119 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & 1.44 \\ 2423 \\ 4190, 0 & 3:52 & 48.0 & 41 & 119 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & 1.44 \\ 2423 \\ 4190, 0 & 3:55 & 16.9 & 43 & 119 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 26.4 & 1.37 \\ 4200, 0 & 4:13 & 52.0 & 34 & 121 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 26.4 & 1.37 \\ 4200, 0 & 4:13 & 52.0 & 34 & 121 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 26.4 & 1.37$													
$\begin{array}{c} 4080.0 & 21:38 & 327.0 & 38 & 102 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 47.0 & .79 \\ 4085.0 & 21:38 & 282.2 & 36 & 102 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 46.6 & .81 \\ 2344 \\ 4090.0 & 21:39 & 419.7 & 33 & 101 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 54.0 & .64 \\ 4095.0 & 21:40 & 409.1 & 32 & 84 & 11.3 & 11.2 & 11.5 & 8.60 & 14.2 & 54.0 & .79 \\ 4105.0 & 21:51 & 119.2 & 17 & 77 & 11.3 & 11.2 & 11.5 & 8.60 & 14.2 & 54.0 & .79 \\ 4105.0 & 22:53 & 23.6 & 29 & 91 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 26.8 & 1.35 \\ 4110.0 & 22:58 & 73.4 & 29 & 78 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 26.8 & 1.35 \\ 4110.0 & 22:58 & 73.4 & 29 & 78 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 44.8 & .89 \\ 4120.0 & 0: 3 & 6.3 & 35 & 102 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 9.1 & 1.84 \\ 4125.0 & 0:41 & 7.9 & 44 & 125 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 7.0 & 1.93 \\ 4130.0 & 0:58 & 46.5 & 43 & 122 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.2 & 1.43 \\ 4135.0 & 1: 1 & 142.1 & 42 & 126 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 23.1 & 1.47 \\ 4140.0 & 1: 9 & 36.4 & 42 & 126 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 23.1 & 1.47 \\ 4140.0 & 1: 17 & 39.6 & 43 & 131 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 23.1 & 1.47 \\ 4150.0 & 1:33 & 19.5 & 42 & 120 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.4 & 1.42 \\ 4160.0 & 2:12 & 15.2 & 38 & 115 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.4 & 1.42 \\ 4160.0 & 2:32 & 32.0 & 38 & 114 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.4 & 1.42 \\ 4160.0 & 3:35 & 16.9 & 43 & 119 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 16.3 & 1.66 \\ 4175.0 & 3:46 & 37.1 & 40 & 115 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & 1.44 \\ 2423 \\ 4190.0 & 3:52 & 48.0 & 41 & 119 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 26.3 & 1.38 \\ 4195.0 & 3:46 & 37.1 & 40 & 115 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 26.3 & 1.38 \\ 4195.0 & 3:58 & 48.5 & 41 & 118 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 26.4 & 1.37 \\ 4205.0 & 4:13 & 52.0 & 34 & 121 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.8 & 1.44 \\ 4215.0 & 4:14 & 66.7 & 35 & 120 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.8 & 1.44 \\ 4215.0 & 4:14 & 66.7 & 35 & 120 &$	• •												
$\begin{array}{c} 4085.0 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	• • •												
$\begin{array}{c} 2344\\ 4090.0&21:39&419.7&33&101&11.3&11.2&11.4&8.60&14.2&52.2&68\\ 4095.0&21:40&409.1&32&84&11.3&11.2&11.5&8.60&14.2&54.0&.64\\ 4100.0&21:51&119.2&17&77&11.3&11.2&11.5&8.60&14.2&26.8&1.35\\ 4110.0&22:53&23.6&29&91&11.3&11.2&11.4&8.60&14.2&26.8&1.35\\ 4110.0&22:58&73.4&29&78&11.3&11.2&11.4&8.60&14.2&38.7&1.04\\ 4115.0&23:&0&135.3&29&78&11.3&11.2&11.4&8.60&14.2&38.7&1.04\\ 4125.0&0:&3&6.3&35&102&11.3&11.2&11.4&8.60&14.2&24.2&8.9\\ 4120.0&0:&3&6.3&35&102&11.3&11.2&11.4&8.60&14.2&24.2&1.43\\ 4125.0&0:41&7.9&44&125&11.3&11.2&11.4&8.60&14.2&24.2&1.43\\ 4135.0&0:58&46.5&43&122&11.3&11.2&11.4&8.60&14.2&24.2&1.43\\ 4135.0&0:58&46.5&43&122&11.3&11.2&11.4&8.60&14.2&23.5&9&1.10\\ 2374\\ 4140.0&1:&9&36.4&42&126&11.3&11.2&11.4&8.60&14.2&22.5&1.48\\ 4145.0&0&1:17&39.6&43&131&11.3&11.2&11.4&8.60&14.2&23.1&1.47\\ 4150.0&1:33&19.5&42&120&11.3&11.2&11.4&8.60&14.2&24.4&1.42\\ 4160.0&2:12&15.2&38&115&11.3&11.2&11.4&8.60&14.2&24.4&1.42\\ 4160.0&2:51&15.9&39&127&11.3&11.2&11.4&8.60&14.2&24.4&1.42\\ 4160.0&2:51&15.9&39&127&11.3&11.2&11.4&8.60&14.2&24.4&1.42\\ 4160.0&3:35&16.9&43&119&11.3&11.2&11.4&8.60&14.2&24.1&1.52\\ 4175.0&3:16&14.6&41&120&11.3&11.2&11.4&8.60&14.2&24.1&1.52\\ 4170.0&2:51&15.9&39&127&11.3&11.2&11.4&8.60&14.2&24.1&1.52\\ 4190.0&3:52&48.0&41&119&11.3&11.2&11.4&8.60&14.2&24.1&1.52\\ 4190.0&3:55&48.5&41&118&11.3&11.2&11.4&8.60&14.2&24.1&1.44\\ 2423\\ 4190.0&3:52&48.0&41&119&11.3&11.2&11.4&8.60&14.2&26.3&1.38\\ 4195.0&3:56&48.5&41&118&11.3&11.2&11.4&8.60&14.2&24.1&1.44\\ 2423\\ 4190.0&3:52&48.0&41&119&11.3&11.2&11.4&8.60&14.2&24.1&1.44\\ 2425.0&3:16&14.4&117&11.3&11.2&11.4&8.60&14.2&24.1&1.44\\ 425.0&3:46&37.1&40&115&11.3&11.2&11.4&8.60&14.2&24.8&1.41\\ 2423\\ 4190.0&3:52&48.0&41&119&11.3&11.2&11.4&8.60&14.2&24.8&1.44\\ 425.0&3:46&37.1&40&115&11.3&11.2&11.4&8.60&14.2&24.8&1.41\\ 425.0&3:46&37.1&40&115&11.3&11.2&11.4&8.60&14.2&24.8&1.41\\ 425.0&3:56&48.5&4&1&116&11.3&11.2&11.4&8.60&14.2&24.8&1.41\\ 425.0&5:5&15&27.0&40&117&11.3&11.2&11.5&8.60&14.2&24.8&1.42\\ 4220.0&5:2&14.4&38&117&11.3&11.2&11.5&8.60&14.2&25.4&1.42\\ 4222.0&5:5&15&6&40&9&11.3&11.2&11$. •												
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Ξ,									8.60	14.2	9.1	
$\begin{array}{c} 4135.0 & 1: 1 & 142.1 & 42 & 124 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 35.9 & 1.10 \\ \hline 2374 \\ 4140.0 & 1: 9 & 36.4 & 42 & 126 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 22.5 & 1.48 \\ 4145.0 & 1:17 & 39.6 & 43 & 131 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 23.1 & 1.47 \\ 4150.0 & 1:33 & 19.5 & 42 & 120 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.4 & 1.42 \\ 4155.0 & 1:43 & 44.5 & 42 & 109 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.4 & 1.42 \\ 4160.0 & 2:12 & 15.2 & 38 & 115 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 21.4 & 1.52 \\ 4170.0 & 2:32 & 32.0 & 38 & 114 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 21.4 & 1.52 \\ 4170.0 & 2:51 & 15.9 & 39 & 127 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 14.1 & 1.72 \\ 4180.0 & 3:35 & 16.9 & 43 & 119 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 14.1 & 1.72 \\ 4180.0 & 3:35 & 16.9 & 43 & 119 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & 1.44 \\ 2423 \\ 4190.0 & 3:52 & 48.0 & 41 & 119 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 26.6 & 1.37 \\ 4200.0 & 4:13 & 52.0 & 34 & 121 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 26.6 & 1.37 \\ 4200.0 & 4:13 & 52.0 & 34 & 121 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 26.6 & 1.37 \\ 4210.0 & 4:30 & 26.5 & 32 & 119 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.8 & 1.17 \\ 4210.0 & 4:30 & 26.5 & 32 & 119 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.8 & 1.17 \\ 4220.0 & 5: & 2 & 14.4 & 38 & 117 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.8 & 1.44 \\ 4215.0 & 4:41 & 36.7 & 35 & 120 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 25.4 & 1.42 \\ 4220.0 & 5: & 2 & 14.4 & 38 & 117 & 11.3 & 11.2 & 11.5 & 8.60 & 14.2 & 25.4 & 1.42 \\ 4220.0 & 5: & 2 & 14.4 & 38 & 117 & 11.3 & 11.2 & 11.5 & 8.60 & 14.2 & 21.1 & 1.54 \\ 4230.0 & 5:43 & 14.8 & 40 & 122 & 11.3 & 11.2 & 11.5 & 8.60 & 14.2 & 21.1 & 1.54 \\ 4232.0 & 5:55 & 15.6 & 40 & 98 & 11.3 & 11.2 & 11.5 & 8.60 & 14.2 & 17.8 & 1.62 \\ \hline \\ $;												1.93
$\begin{array}{c} 2374 \\ 4140.0 & 1i & 9 & 36.4 & 42 & 126 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 22.5 & 1.48 \\ 4145.0 & 1:17 & 39.6 & 43 & 131 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 23.1 & 1.47 \\ 4150.0 & 1:33 & 19.5 & 42 & 120 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.4 & 1.42 \\ 4160.0 & 2:12 & 15.2 & 38 & 115 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.4 & 1.42 \\ 4160.0 & 2:12 & 15.2 & 38 & 115 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 21.4 & 1.52 \\ 4170.0 & 2:51 & 15.9 & 39 & 127 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 16.3 & 1.66 \\ 4175.0 & 3:16 & 14.6 & 41 & 120 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 16.3 & 1.66 \\ 4175.0 & 3:16 & 14.6 & 41 & 120 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 14.1 & 1.72 \\ 4180.0 & 3:35 & 16.9 & 43 & 119 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 14.1 & 1.72 \\ 4180.0 & 3:35 & 16.9 & 43 & 119 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.1 & 1.44 \\ 2423 \\ 4190.0 & 3:52 & 48.0 & 41 & 119 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 26.3 & 1.38 \\ 4195.0 & 3:58 & 48.5 & 41 & 118 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 26.6 & 1.37 \\ 4200.0 & 4:13 & 52.0 & 34 & 121 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 26.6 & 1.37 \\ 4201.0 & 4:30 & 26.5 & 32 & 119 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.8 & 1.44 \\ 4215.0 & 4:41 & 36.7 & 35 & 120 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 24.8 & 1.44 \\ 4225.0 & 5:15 & 27.0 & 40 & 117 & 11.3 & 11.2 & 11.4 & 8.60 & 14.2 & 25.4 & 1.42 \\ 4220.0 & 5:43 & 14.8 & 40 & 122 & 11.3 & 11.2 & 11.5 & 8.60 & 14.2 & 25.4 & 1.42 \\ 4220.0 & 5:43 & 14.8 & 40 & 122 & 11.3 & 11.2 & 11.5 & 8.60 & 14.2 & 21.1 & 1.54 \\ 4230.0 & 5:43 & 14.8 & 40 & 122 & 11.3 & 11.2 & 11.5 & 8.60 & 14.2 & 17.8 & 1.67 \\ 4232.0 & 5:55 & 15.6 & 40 & 98 & 11.3 & 11.2 & 11.5 & 8.60 & 14.2 & 17.8 & 1.62 \\ \hline \begin{array}{c}$	• •												
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$: J	4170.0	2:51	15.9	39	127	11.3						
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$		4180.0							11.4	8.60	14.2	15.1	
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4225.0 5:15 27.0 40 117 11.3 11.2 11.5 8.60 14.2 21.1 1.54 4230.0 5:43 14.8 40 122 11.3 11.2 11.5 8.60 14.2 15.6 1.70 4232.0 5:55 15.6 40 98 11.3 11.2 11.5 8.60 14.2 17.8 1.62													
4230.0 5:43 14.8 40 122 11.3 11.2 11.5 8.60 14.2 15.6 1.70 4232.0 5:55 15.6 40 98 11.3 11.2. 11.5 8.60 14.2 17.8 1.62	•	4225.0											
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		4232.0	5:55	15.6									
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ESSO BARRACOUTA # 4

PAGE 14 - A

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DEPTH 24	TIME 74	ROP	WDB	RPM	MDI	MDO	ECD	PP	FG	POR	NEXP	
4235.0 4240.0 4245.0	2:20 2:48 21:44	31.1 24.2 43.0		116 45	11.3 11.3 11.2		11.4 11.4 11.3	$8.60 \\ 8.60$	14.3 14.3 14.3	27.4 53.9	1.37	
4250.0 4255.0 4260.0	21:44 21:48 21:49	34.0 16.1 44.0	11 18 21	76 93	11.2 11.2 11.2	11.1 11.1 11.1	11.3 11.3 11.3	8.60 8.60 8.60	14.3 14.3 14.3	27.2 32.3	1.32 1.19	
4265.0 4270.0 4275.0	21:52 22: 0 23:53	38.6 40.8 58.5	19	95	11.2 11.2 11.2	11.1 11.1 11.1	11.3 11.4 11.4		14.3 14.3 14.3	33.0		
4280.0 250		64.7			11.0	11.0	11.4		14.3		1.36	
4285.0 4290.0	0:14 0:18	92.9 80.4	32 33	101	10.8 10.8	10.9 10.9	11.4	8.60	14.3 14.3	29.9	1.20	
4295.0	0:22	84.6 169.3	33 33	85	10.8 10.8 10.8	10.9	11.3 11.1 11.0	8.60	14.3	30.5 36.6 22.6	1.21 1.01 1.43	
4305.0 4310.0 4315.0	1: 6 1:13 1:14	68.7 93.2 191.3	35 36 36	101	10.8 10.8 10.8	10.9 10.9 10.9	10.9 11.0	8.60	14.3 14.3 14.3	24.3 35.0	1.37	
4320.0 4325.0	1:14 1:15	310.2	35 36	99	10.8	10.9	11.0	8.60	14.3 14.3	40.5	.87	
4330.0 25-		327.0	34	•	10.7	10.8	11.0	8.60	14.3	43.0	.79	
4335.0 4340.0 4345.0	1:27 1:28 1:29	278.1 271.4 292.2	36 36 36	105	10.7 10.7 10.7		11.0 11.0 11.0		14.3 14.3 14.3	38.4 38.4 39.1		
4350.0	1:30	467.5	33 35	109	10.7	10.8	11.0	8.60 8.60	14.3			
4360.0 4365.0	1:42 1:45	293.6 116.2		78 101	$10.7 \\ 10.7$	10.8 10.8	11.0	$8.60 \\ 8.60$	14.3 14.3	$47.7 \\ 44.0$.74 .99	
4370.0 4375.0	1:50 1:58	75.4 48.5		105	10.7	10.8	11.0	8.60 8.60	14.3	38.2	$1.08 \\ 1.09 \\ 0.1$	
4380.0 256	2:1 58	139.2	18	103	10.7	10.8	10.9	8.60	14.3	44.7	.94	
4385.0	2: 3	146.2	17	103	10.7	10.8	10.9	8.60	14.3	44.7	. 94	
4390.0 4395.0	2:18 2:19	57.5 180.6	27 26	114	10.7 10.7	$10.8 \\ 10.8$	10.9 10.9	8.60 8.60	14.3 14.3	28.0 39.5	1.31 .99	
4400.0 4405.0	2:22	118.7		121	10.7	10.8		8.60 8.60	14.3 14.3	36.7 50.1	1.09	
4410.0 4415.0 4420.0	2:33 2:37 2:50	36.8 70.4 78.8	11 12 8	122	10.7 10.7 10.7	10.8 10.8 10.8	10.9 10.9 10.9	8.60 8.60 8.60	14.3 14.3 14.3	39.6 44.2 51.7	1.15 1.04 .94	
4425.0	2:54 3:0	73.3		107	10.7	10.8	10.9	8.60 8.60	14.4 14.4	52.4 45.3	.92	•
261	10	•		•								
4435.0 4440.0 4445.0	3:7 3:11 3:14	64.7 65.7 112.4	21 21 21	105	10.7 10.7 10.7	10.8 10.8 10.8	10.9 10.9 10.9	8.60 8.60 8.60	14.4 14.4 14.4	34.6 34.3 39.6	1.18	
44450.0 4455.0	3:15	191.0	15 9	102	10.9	10.8 10.8 10.8	10.9	8.60 8.60	14.4 14.4	51.3 52.7	1.04 .81 .89	
4460.0	3:36	42.2	15	110	10.8	10.8	11.0	8.60	14.4	36.7	1.21	
4465.0 4470.0	3:42 3:46	62.6 79.6	22 22		10.8 10.8	10.8 10.8	11.0 11.0	8.60 8.60	14.4 14.4	33.4 35.9,	1.20 1.13	
4475.0 4480.0	3:51 3:54	64.3 85.9	22	106	10.8	10.8	11.0	8.60 8.60	14.4 14.4	33.8	1.19	
4480.0		00.7	. 63	101	10.0	10.0	1 1 e V	0.00	1-1	-0-0-1 1	1.10	

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	DEPTH	TIME	FOF	WEIB	RPM	MDI	MDO	ECD	PP	FG	PDR	DEXP	
	265								0 20	• • • •	39.6	1.05	•
	4485.0	4: 6	101.4	21		10.8	10.8 10.8	$11.0 \\ 11.0$	8.60 8.60	14.4 14.4	27.1	1.38	
•	4490.0		38.0 48.0	24 31		$10.7 \\ 10.7$	10.8	11.0	8.60	14.4	24.2	1.43	
	4495.0	4:22	40.0 39.5			10.7	10.8	11.0	8.60	14.4	22.4	1.49	
	4500.0 4505.0	4:31 4:40	53.1	32 32		10.8	10.8	11.0	8.60	14.4	23.3	1.46	
	4510.0		39.5			10.8	10.8	11.0	8.60	14.4	20.6	1.54	
	4515.0	5:12	23.1	33		10.8	10.8	11.0	8.60	14.4	17.7	1.63	
	4520.0		21.6			10.9	10.8	11.0	8.60	14.4	17.2	1.64	
	4525.0		108.6			10.8	10.8	11.0	8.60	14.4	31.9	1.20	
•.	4530.0	5:32	209.2			10.8	10.8	11.0	8.60	14.4	40.1	.96	
	269						•						
	4535.0	5:33	242.6	30	103	10.7	10.8	11.0	8.60	14.4		.90	
	4540.0	5:34	170.9			10.8	10.8	11.0	8.60	14.4	39.4	1.00	
	4545.0		169.5			10.8	10.8	11.0	8.60	14.4		.99	
	4550.0		186.7			10.7	10.8	11.0	8.60	14.4		.90	
	4555.0		40.6	17		10.7	10.8	11.0	8.60	14.4	33.8	1.24	
	4560.0	6: 2	40.0			10.7	10.8	11.0	8.60	14.4		1.33	
	4565.0		73.9			10.7	10.8	11.0	8.60	14.4	35.3	1.16	
	4570.0	6:10	89.4		111		10.8	11.0	8.60	14.4		1.06	
	4575.0		111.0			10.7	10.8	11.0	$8.60 \\ 8.60$	14.4 14.4	45.4	.98	
	4580.0	0:19	25.8	8	46	10.6	10.7	10.7	0.00	1.4.4.4	40.4	•	
	27: 4585.0		80.8	13	59	10.6	10.7	10.8	8.60	14.4	45.3	.88	
• •	4590.0		34.8			10.6	10.7	10.7	8.60	14.4	30.8	1.22	
	4595.0	1:35	66.0			10.6	10.7	10.8	8.60	14.4	41.0	.98	
•	4600.0	1:53	20.0			10.6	10.6	10.7	8.60	14.4	29.3	1.27	
	4605.0	4:24	78.9			10.6	10.7	10.8	8.60	14.4	40.6	. 99	
	4610.0	4:46	30.3			10.6	10.8	10.8	8.60	14.4	26.1	1.34	
	4615.0	5: 8	45.5		61	10.6	10.7	10.8	8.60	14.4	26.4	1.33	
	4620.0	5:41	10.7	~	61	10.7	10.7	10.8	8.60	14.5	14.9	1.64	• •
	4625.0	6:12	11.6	24	63	10.7	10.7	10.8	8.60	14.5		1.62	
	4630.0	7: 9	6.2	55	65	10.7	10.7	10.8	8.60	14.5	11.1	1.75	
		786			(1 m							
	4635.0	7:52	6.9	55		10.7	10.6	10.8	8.60	14.5	12.7	1.71	
	4640.0		59.0			10.7		10.8		14.5			
	4645.0		32.2				10.6			14.5			
	4650.0		39.0				10.6		$8.60 \\ 8.60$	14.5 14.5		.92	
	4655.0		82.9				$10.6 \\ 10.6$			14.5			
	4660.0		74.0				10.6			14.5			
• .		16:48 1:18	6.8				10.6			14.5			
	4670.0		13.9				10.6			14.5			
		1:55	30.1				10.6			14.5			
	4000.0				•	,							
	4685.0		32.4	8	65	10.7	10.6	10.8	8.60			1.00	
		2:11	58.6	8	62	10.7	10.6	10.9	8.60			.87	
	4695 0	2:14	107.1	7	62	10.7	10, 6	11.0	8.60	14.5	59.5		
	4700.0	2:19 2:22	78.0	6	67				8.60			.76	
	4703.0	5:55	53.4	6	67	10.7	10.6	10.9	8.60	14.5	54.6	.83	
			······································		NEW J	BIT ID	: 9						
	3705 0	11:51	170 2	10	140	104	107	10 7	8.60	14.5	49 A		
	4710 0	11:51	85.5	14	144	10.6	10.7	10.7	8.60	14.5	40.1	1.07	
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	ES	1010		ESSI	D BAR	PACOUT	A # 4			F	AGE	16 - A
I	EPTH 28	TIME 65	RDP	MDB	PPM	MDI	MDO	ECD	PP	FG	PDR	DEXP
	4715.0 4720.0 4725.0	11:52 11:52 12: 3	134.0 114.0 147.7	16 14 13	144	10.6 10.6 10.6	10.7 10.7 10.7	10.7 10.7 10.7	8.60 8.60 8.60	14.5 14.5 14.5	41.4 42.8 46.1	1.00
r •	4730.0 4735.0	12: 4 12:10	208.9 73.7	15 13	.137 127	$10.6 \\ 10.6$	$10.7 \\ 10.7$	$\begin{array}{c} 10.7 \\ 10.7 \end{array}$	8.60 8.60	$14.5 \\ 14.5$	47.5 39.9	1.08
	4740.0 4745.0 4750.0	12:18 12:21 12:24	51.1 105.0 110.0	15 15 15	133	10.6 10.6 10.6	10.7 10.7 10.7	10.7 10.7 10.8	8.60 8.60 8.60	14.5 14.5 14.5	33.1 42.0 42.2	1.24 1.02 1.01
	4755.0 4760.0	12:48 12:55	25.6 80.7	14 15	138	10.6 10.6	10.7	10.9 10.7	8.60 8.60	14.5 14.5	29.1 33.6	1.37
	29 4765.0 4770.0	12:57 13: 0	113.7 96.8	16 16		10.6 10.6	$10.7 \\ 10.7$	10.8 10.7	8.60 8.60	14.5 14.5	41.4 39.8	1.03 1.07
	4775.0 4780.0		145.7 129.2	16 16	141 141	$10.6 \\ 10.6$	$10.7 \\ 10.7$	10.8 10.8	8.60 8.60	$14.5 \\ 14.5$	43.6 42.3	.97 1.01
	4783.0	13: 7	64.8	16	144	10.6	10.7	10.8	8.60	14.5	36.2	1.17
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DUMP B

RS	-	Calculated rock matrix strength. A dimension-
		less number derived from previous field data
		which relates to the strength of the rock.
MTI	-	The mud temperature in, in degrees farenheit
мто	-	Mud temperature out, in degrees farenheit
MRO	• • • • •	The mud resistivity out, in ohm-metres
үрм	-	The yield point of the mud in lbs/100 sq. ft.
PVM		The Plastic viscosity of the mud in centipoise
MVI	-	The mud flow rate in gallons per minute, com- puted from the pump rate and pump output
	1	

The mud density override setting

MDOV

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	DEPTH	TIME 64	RS	ITM	мто	MRI	МРО	YPM	PVM	MVI	MDOV RECDS
					NEW E	IT ID:	2				
Structure in the second se	720.0 750.0 760.0 770.0 780.0 790.0 800.0 810.0 815.0 820.0	6:56 6:57 6:58 7:3 7:4 7:5 7:5 7:14 7:15	1.07 1.52 1.66 1.80 1.48 1.66 1.99 1.65 2.50 1.97	64 64 64 64 65 65 65	70 73 73 72 72 72 71 72 72 72 72	.00 .00 .00 .00 .00 .00 .00 .00 .00	.00 .00 .00 .00 .00 .00 .00 .00 .00	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	555555555555555555555555555555555555555	1164 1171 1171 1171 1181 1202 1202 1202 1202 1202 1202	$egin{array}{cccc} .0&1\\ .0&1\\ .0&1\\ .0&1\\ .0&1\\ .0&1\\ .0&1\\ .0&1 \end{array}$
and the second of the measured of the second of the second s	830.0 840.0 850.0 860.0 870.0 880.0 885.0 890.0 895.0 900.0	7:25 7:26 7:28 7:36 7:37 7:38 7:38 7:39	1.91 1.88 2.14 2.54 1.91 1.99 1.81 1.94 1.68		71 71 73 75 75 75 76	.00 .00 .00 .00 .00 .00 .00 .00	.00 .00 .00 .00 .00 .00 .00 .00		ទទទទទទទ	1090 1110 1150 1137 1124 1121 1121 1121 1121 1117 1135	$egin{array}{cccc} .0 & 1 \ .0 & 2 \ .0 & 1 \ .0 & 1 \ .0 & 1 \ .0 & 1 \ .0 & 1 \ .0 & 1 \ .0 & 1 \ .0 & 1 \ .0 & 1 \ .0 & 1 \end{array}$
terration of the second of the second se	905.0 910.0 915.0 920.0 940.0 950.0 955.0 960.0 965.0 970.0	7:48 7:49 7:51 7:52 8: 3 8: 5 8: 5 8: 5 8: 6 8: 7 8: 7 8:37	1.69 1.96 2.08 1.82 1.88 1.58 1.68 1.82 2.03	66 66 66	77 78 79 79 79 80 81 82 75	.00 .00 .00 .00 .00 .00 .00 .00	.00 .00 .00 .00 .00 .00 .00 .00	<u>พพพพพพ</u> พพพพ	មភភភភភភភភភភភភ	1159 1159 1159 1162 1162 1162 1165 1165 1159 1163	.02 .04 .01 .02 .02
المراجع والمراجع والم	975.0 980.0 985.0 990.0 995.0 1000.0 1005.0 1010.0 1020.0 1030.0	8:41 8:42 8:43 8:55 8:57 8:58 9:2 9:13	1.96 2.12 2.23 2.09 2.20 2.12 2.33 2.40 2.72 2.47	64 64 64 64 64 64 65 64	70 71 75 75 74 74 75 76	.00 .00 .00 .00 .00 .00 .00 .00	.00 .00 .00 .00 .00 .00 .00 .00	<u></u>	ទទទទទទទទទទ	1168 1172 1172 1172 1172 1168 1128 1128 1130 1126 1129	$egin{array}{cccc} .0 & 1 \\ .0 & 2 \\ .0 & 1 \\ .0 & 2 \\ .0 & 2 \\ .0 & 1 \\ .0 & 2 \\ .0 & 1 \\ .0 & 3 \\ .0 & 1 \end{array}$
	1035.0 1040.0 1045.0 1050.0 1055.0 1060.0 1070.0	122 9:14 9:14 9:15 9:17 9:19 9:31 9:32	2.42 2.37 2.43 2.63 2.80 2.89 2.52	63 63 62 63 64 64	75 75 76 76 75 76	.00 .00 .00 .00 .00 .00	.00 .00 .00 .00 .00 .00	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	មទទទទទ	1139 1134 1140 1135 1123 1158 1164	$egin{array}{cccc} .0 & 1 \ .0 & 1 \ .0 & 1 \ .0 & 2 \ .0 & 2 \ .0 & 3 \ .0 & 2 \ .0 & 1 \ .0 & 1 \end{array}$

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ESSO BARRACOUTA # 4

PAGE 2 - B

	DEPTH	TIME	RS	MTI	мто	MRI	MRO	YPM	PVM	MVI	MDOV	
•		133						•				CDS
	1080.0			64	76	.00	.00	2	5	1166	.0	2
	1085.0			64	76	.00	.00	2	5	1165	.0	3
	1090.0			64	76	.00	.00	2	5	1165	.0	1
:	1095.0		2.05	66	75	.00	.00	2	5	1123	.0	1
	1100.0			66	74	.00	.00	2	5	1124	.0	2
	1105.0	-	2.63 2.58	66 66	. 75	.00	.00	2	5	1126	.0	1
	1115.0			66 67	75 76	.00	.00	2	5	1126	.Ŭ	1
	1120.0		2.41	67	· 76 76	.00 .00	.00	2	5	1126	.0	2
t s	1130.0		2.46	67	75	.00	.00	2	5 5	1126	.0	1
		49	L. 40	01	rυ	.00	.00	c	5	1131	.0	2
	1135.0		2.45	68	76	.00	•.00	2	5	1137	.0	9
а. А	1140.0		2.80	68	77	.00	.00	5	5	1156	.0	2
	1145.0		2.30	68	77	.00	.00	2	5	1256	.0	Э 1
	1150.0		2.38	68	77	.00	.00	5	5	1200	.0 .0	1
•	1155.0		2.73	68	 78	.00	.00	2.	5	1314	.0	23
	1160.0			67	77	.00	.00	2	5	1247	.0	1
	1165.0	10:20	2.56	68	78	.00	.00	2	5	1247	.0	1
r. L	1170.0	10:21	2.58	68	79	.00	.00	ē	5	1247	.0	ż ż
	1175.0	10:23	2.53	68	79	.00	.00	2	5	1250	.0	2
· ·	1180.0	10:24	2.68	68	79	.00	.00	2	5	1250	.0	3
; · .		59				,		_	-		• •	
1	1190.0	10:37	2.57	69	78	.00	.00	2	5	1247	.0	2
÷.,	1195.0	10:38	2.70	69	78	.00	.00	2	5	1244	.0	ē.
	1200.0	10:39	2.18	69	80	.00	.00	2	5	1242	.0	ž
•	1205.0	10:40	2.57	69	80	.00	.00	2	5	1242	.0	3
	1210.0	10:43	2.76	68	80	.00	.00	2	5	1245	.0	च
	1215.0	10:44	2.38	68	80	.00	.00	8	5	1240	.0	1
	1220.0	10:53	2.82	68	78	.00	.00	2	5	1256	. 0	
	1225.0	10:54	2.68	68	- 78	.00	.00	2	5	1259	. 0	2
	1230.0	10:57	2.89	68	- 78	.00	.00	2	5	1262	.0	र्य
	1235.0	10:58	2.59	66	79	.00	.00 .	. 2	. 5	1262	.0	2
• •	19							•				
	1240.0	11: 0	2.69	66	79	.00	.00	2	5	1260	9	2
	1240.0	11: 1 11: 9		66 64	79	.00	.00	2	. 5	1260	.0	1
	1255.0	11: 9 11:11	2.70 2.72	64	78 70	.00	.00	5	5	1247	. 0	2
	1260.0	11:13	3.07	64 65	78 70	.00	.00	2	5	1238	.0	2
	1265.0	11:15	3.07 2.95	66 66	79 79	.00	.00	22	5	1238	.0	.3
•••	1270.0	11:16	2.63	66 66	79 79	.00	.00	С О -	5	1247	.0	2
	1275.0	11:25	2.76	67	78 78	.00	.00 .00	С Э	- 5	1256	.0	1
	1280.0	11:26	2.45	67	76	.00	.00	2 2	55	1261	.0	2
	1290.0	11:27	2.26	67	77	.00	.00	2	5	1261 1268	.0	1
		10	b • b	<u>.</u>	••		.00	Ľ.	J	1600	.0	1
•	1295.0	11:29	2.67	67	77	.00	.00	2	5	1264	.0	З
	1300.0	11:30	2.63	67	77	.00	.00	2	5	1262	.0	2
	1305.0	11:31	2.64	66	77	.00	.00	ž	5	1262	.0	1
• .	1310.0	11:32	2.58	66	77	.00	.00	2	5	1262	.0	1
	1315.0	11:52	3.13	68	78		.00	2		1271	.0	3
	1320.0	.11:55	2.88	69	79	.00	.00	2		1264	.0	4
	1,325.0	12: 1	3.10	70	79	.00	.00	5		1256	.0	
	1330.0	12: 3	2.56	69	78	.00	.0.0	2		1249	.0	5 5 5
	1335.0	12: 6	2.67	69	78	.00	.00	2		1269	.0	
	1340.0	12:12	3.13	69	78	.00	.00	ē		1281	.0	5
	24	44							_	·		-

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ESSO BARRACOUTA # 4

11.14				· ·								
	DEPTH	TIME 44	RS	MTI	МТО	MRI	MRO	YPM	PVM	MVI	MDOV PECDS	
	1345.0 1350.0 1355.0 1360.0 1365.0	12:29 12:33 12:36 12:40 12:44	2.78 3.20 2.96 3.15 3.18	69 68 68 67 67	78 79 79 79 79	.00 .00 .00 .00 .00	.00 .00 .00 .00 .00	2222	5 5 5 5 5 5 5 5	1286 1269 1262 1274 1280	.0 .0 .0 .0 .0	4 4 3 4 4 4
	1370.0 1380.0 1385.0	12:46 12:59 13: 2	2.66 2.85 2.90	67 68 69	79 78 79 80	.00 .00 .00 .00	.00 .00 .00 .00	2 2 2 2 2	5 5 5 5 5	1283 1277 1266 1266	.0 .0 .0 .0	2639
,	1390.0 1395.0 27	13: 7	2.95 2.75	70 69	80	.00	.00	5	5	1267	.0	2
	1400.0 1405.0 1410.0 1415.0 1420.0 1425.0 1430.0 1435.0 1440.0 1445.0 30	13: 9 13:11 13:18 13:20 13:21 13:22 13:25 13:25 13:27 13:36 13:38	2.60 2.67 2.69 2.82 2.77 2.61 3.05 2.88 3.15 2.91	69 68 68 68 68 67 67 68 68	80 80 79 80 80 80 80 79 79	.00 .00 .00 .00 .00 .00 .00 .00 .00	• 00 • 00 • 00 • 00 • 00 • 00 • 00 • 00	<u>ສ</u> ສສສສສສສສສສ	55555555555	1279 1281 1299 1293 1295 1298 1286 1283 1293 1294	.0 .0 .0 .0 .0 .0 .0 .0 .0	3343224441
	1450.0 1455.0 1460.0 1465.0 1470.0 1475.0 1480.0 1485.0 1490.0 1495.0	13:41 13:44 13:47 13:51 13:57 13:59 14: 3 14: 5 14: 7 14:12	3.12 3.12 3.27 2.91 2.93 3.33 3.07 3.09 3.28	68 67 67 68 68 67 67 68	79 79 79 75 78 79 80 80	.00 .00 .00 .00 .00 .00 .00 .00	.00 .00 .00 .00 .00 .00 .00 .00	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	ទទទទទទទទទទ	1302 1302 1300 1296 1281 1275 1275 1285 1282	.0 .0 .0 .0 .0 .0 .0 .0 .0	4544153425
	34 1500.0 1505.0 1510.0 1515.0 1520.0 1525.0 1530.0 1535.0 1540.0 1545.0 37	14:19 14:21 14:26 14:30 14:32 14:33 14:35 14:43 14:44 14:45	2.98 3.13 3.40 3.38 2.87 2.95 2.85 3.00 2.85 2.78	67 66 67 67 67 67 68 68 68	79 79 79 79 79 79 79 78 78 78	.00 .00 .00 .00 .00 .00 .00 .00 .00	.00 .00 .00 .00 .00 .00 .00 .00	<u>ย พ พ พ พ พ พ พ พ</u>	555555555555	1285 1289 1287 1281 1282 1282 1282 1283 1263 1270	.0 .0 .0 .0 .0 .0 .0 .0 .0	3343223312
	57 1550.0 1555.0 1565.0 1570.0 1575.0 1580.0 1585.0 1590.0 1600.0 40	14:46 14:49 14:49 15:0 15:2 15:4 15:12 15:14 15:16 15:20	2.90 2.87 2.86 2.79 2.83 2.79 2.92 2.92 2.92 2.90 2.92	68 68 68 69 69 69 69 69 69 69	79 79 79 80 80 80 80 80	.00 .00 .00 .00 .00 .00 .00 .00 .00	.00 .00 .00 .00 .00 .00 .00 .00		ទទទទទទទទទ	1264 1264 1274 1273 1277 1285 1288 1284 1284	.0 .0 .0 .0 .0 .0 .0 .0 .0	1122433557

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ESSO BARRACOUTA # 4

PAGE 4

В

1	DEPTH	TIME 405	RS	MTI	мто	MRI	MRD	YPM	PVM	MVI	MDOV RECDS	
amonto corpora	1610.0 1615.0 1620.0 1635.0 1650.0 1655.0 1660.0 1665.0 1670.0 1675.0	15:26 15:27 15:29 15:34 15:42 15:44 15:46 15:48 15:50 15:56	2.58 2.57 2.84 2.80 2.81 2.83 2.79 2.99 2.86 2.72	69 68 68 68 68 67 68 68	80 77 78 79 79 80 81 81	.00 .00 .00 .00 .00 .00 .00 .00	.00 .00 .00 .00 .00 .00 .00 .00	<u>ของของของ</u> ของของ	55555555555	1276 1282 1283 1282 1277 1267 1270 1275 1281 1267	$ \begin{array}{cccc} & .0 & 2 \\ .0 & 10 \\ .0 & 2 \\ .0 & 2 \\ .0 & 2 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ .0 & 5 \\ $	3 - 0
	1680.0 1685.0 1690.0 1695.0 1700.0 1710.0 1720.0 1725.0 1730.0 1735.0	16: 0 16: 2 16: 4 16: 6 16:16 16:18 16:20 16:22 16:24	2.84 2.82 3.00 2.98 3.00 2.84 2.84 2.95 3.11 2.98	68 68 69 69 69 69 69 69	80 81 81 81 76 80 81 81	.00 .00 .00 .00 .00 .00 .00 .00	\$00 .00 .00 .00 .00 .00 .00 .00	<u>ุล ล ล ล ล ล ล ล</u> ล	5555555555	1256 1279 1281 1278 1280 1249 1271 1273 1270 1262	$ \begin{array}{cccc} & .0 & .0 \\ $	4334545534
a second a s	1740.0 1745.0 1750.0 1755.0 1760.0 1765.0 1775.0 1775.0 1780.0 1785.0	492 16:25 16:26 16:35 16:38 16:38 16:40 16:42 16:45 16:54 16:56	2.74 2.82 2.77 2.81 2.96 2.95 2.92 2.88 3.04 2.99	69 69 68 67 67 68 68 68 68	82 82 81 81 81 82 81 79 80	.00 .00 .00 .00 .00 .00 .00 .00	.00 .00 .00 .00 .00 .00 .00 .00		5555555555	1269 1273 1278 1270 1251 1251 1259 1268 1268 1274	.0 1 .0 3	1
and the second of the second o	1790.0 1795.0 1800.0 1805.0 1810.0 1815.0 1820.0 1825.0 1830.0 1835.0	17: 3 17: 6 17:14 17:17 17:19 17:22 17:25 17:27 17:34	3.07 2.97 3.18 2.91 2.95 2.84 2.93 3.02 2.87 3.08	68 69 70 70 70 70 71 71 71	81 81 82 82 82 82 82 82 82	.00 .00 .00 .00 .00 .00 .00 .00	.00 .00 .00 .00 .00 .00 .00	<u></u>	5555555555	1278 1277 1277 1273 1264 1261 1263 1264 1264 1257	.0 9 .0 9 .0 5 .0 5 .0 5 .0 5	
	5, 1840.0 1850.0 1855.0 1860.0 1860.0 1880.0 1880.0 1885.0 1890.0 1900.0 60	17:40 17:42 17:43 17:45 22:14	3.12 3.17 3.19 3.03 2.94 2.94 2.95 2.96 2.94 2.72	71 71 71 71 71 71 70 70 71	81 82 82 82 82 82 82 82 82 82 81	00 00 00 00 00 00 00 00	.00 .00 .00 .00 .00 .00 .00 .00	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	សសសសសស ភេទសសសស ភេទស	1255 1255 1255 1255 1257 1263 1256 1256 1256 1254	0.0 0 0 0 0 0 0 0 0 0 0 0 0 0	

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В

			F	64 77 T	6.4 mm mm -	MED T	MRO	YPM	PVM	MVI	MDOV	
	DEPTH	TIME 01	RS	MTI	MTO	MRI	PURCE	1511	E 913	114.1	RECDS	
	1905.0	22:16	2.88	73	81	.00	.00	5	5	1254	. Ü	4
	1910.0	22:18	2.87	73	84	.00	.00	2	5	1258	.0	4
	1915.0	22:20	3.72	71	85	.00	.00	5	5	1077	.0	4
	1920.0	55:53	2.94	- 69	85	.00	.00	2	5	1259	.0	5
	1925.0	22:25	2.85	70	85	.00	.00	2	5	1239	.0	5
	1930.0	22:34	3.23	72	85	.00	.00	2	5	1232	.0	2
	1935.0	22: 36	2.82	74	85	.00	.00	5	5	1239	. Ü	5 5
	1940.0	22:40	3.21	75	85	.00	.00	2	5 5	1234	.0	5
	1945.0	22:43	2.92	74	85	.00	.00	5	о 5	1234	.0	5
	1950.0	22:46	3.06	73	85	.00	.00	c	0	1230	• •	
	64 1055 0		2.99	75	85	.00	•. 00	2	5	1227	.0	5
e.	1955.0	22:49 22:52	3.00	76	85 85	.00	.00	2	5	1226	.0	5
	1960.0 1965.0	23: 2	2.91	77	86	.00	.00	2	5	1226	.0	3
	1960.0	23: 4	2.93	78	86	.00	.00	Ē	5	1234	.0	5
	1975.0	23: 6	2.78	78	87	.00	.00	2	5	1229	.0	5
	1980.0	23: 8	2.87	78	88	.00	.00	2	5	1230	.0	
	1985.0	23:10	2.88	77	88	.00	.00	2	5	1225	.0	4
	1990.0	23:12	2.87	77	88	.00	.00	2	5	1225	.0	5
	1995.0	23:19	2.92	77	87	.00	.00	2	- 5	1197	.0	5
	2000.0	23:22	2.73	78	87	.00	.00	5	5	1172	.0	-5
÷	6	92				•						_
	2005.0	23:24	2.72	. 77	88.	.00	.00	2	5	1161	.0	5
•	2010.0		2.88	77	88	.00	.00	2	5	1160	.0	2
	2015.0	23:27	2.80	77	88	.00	.00	2	cu cu	1174 1227	.0 .0	5
	2020.0	23:31	3.00	77	88	.00	.00 .00	2	5	1227	.0	5
	2025.0	23:34	2.92	78 79	89 89	.00	.00	2	5	1235	.0	5
	2030.0 2035.0	23:45 23:47	2.75	79	90	.00	.00	2	-5	1237	.0	š
	2030.0	23:50	3.01	79	90	.00	.00	2	5	1234	. 0	លែហលលាលល
	2045.0	23:52	2.94	79	90	.00	.00	Ē	5	1224	.0	5
	2050.0	23:55	3.14	79	89	.00	.00	2	. 5	1209	.0	5
	74										· · · ·	
	2055.0	0:7	3.08	79	88	.00	.00	5	5	1213	. 0	5
	2060.0	0:11	3.16	81	90	.00		2			.0	5
	2065.0	0:14	3.12	81	91	.00	.00	2	5	1816	.0	3
	2070.0	0:16	2.95	82	92	.00	.00	2	5	1222	.0	ខេត្ត
	2075.0	0:18	2.91	83	92	.00	.00	2	5	1221	.0	э 4
÷	2080.0	0:20	2.85	83	92	.00	.00	2	5 5	1219	.0	1
	2080.0	0:21	3.10	183	92	.00	.00	2	5	1220 1219	.0	7
	2095.0	0:35	3.06	82	91 00	.00 .00	.00	2	5	1217	.0	5
	2100.0	0:39	3.07 2.81	82 82	92 92	.00	.00	2	5	1214	.0	4
	2105.0 78	0:41 <	c.01	06	76	.00	.00			1 - 1 -	•••	•
-	2110.0	0:44	2.99	. 82	92	.00	.00	· 2	5	1213	.0	5
	2115.0	0:48	3.17	83	93	.00	.00	2	5	1213	0	
	2120.0	1: 3	3.29	84	94	.00	200	2	5	1213	.0	5
	2125.0	1: 9	3.30	85	94	.00	.00	2	5	1210	.0	លលលលល
	2130.0	1:15	3.41	85	94	.00	.00	2	5	1221	.0	5
	2135.0	1:17	3.05	85	94	.00	.00	5	5	1227	.0	5
	2140.0	1:22	3.31	85	94	.00	.00	2	5	1226	.0	5
	2145.0	1:27	3.37	85	94	.00	.00	5	5	1217	.0	
	2150.0	1:39	3.37	86	95	.00	.00	2	5	1222	.0	4
	2155.0	1:43	3.27	86 -	96	.00	.00	5	5	1245	.0	4
	8	34										

ESSO BARRACOUTA # 4

PAGE 6 – B

· · · · · ·				1. A.								
	DEPTH 83	TIME	RS	MTI	МТО	MRI	MRD	YPM	PVM	MVI	MDDV RECDS	
	2160.0	1:47	3.35	87	96	.00	.00	2	5	1245	.0	5
I		1:58	3.26	88	97	.00	.00	2	5	1185	.0	4
	2165.0		3.33	00 89	97	.00	.00	5	5	1201	.0	5
1 + 1 = 1	2170.0	2:4			77 98	.00	.00	2	5	1208	.0	-
•	2175.0	2: 9	3.30	89				5		1206	.0	55
1.1	2180.0	2:13	3.17	90	98	.00	.00	ے م				_4
	2185.0	2:27	3.24	90	98	.00	.00	2	. 5	1232	.0	- 4
	2190.0	2:32	3.30	90	96	.00	.00	2	5	1235	.0	55
E	2195.0	5:38	3.38	89	97	.00	.00	2	5	1233	.0	5 5
	2200.0	2:45	3.38	89	99	.00	.00	2	5	1231	.0	0 5
t	2205.0	2:49	3.23	89	98	.00	.00	2	5	1231	.0	
	89							-	-			-
	2210.0	2:54	3.29	89	99	.00	•.00	5	5	1231	.0	55
	2215.0	3: 5	3.18	89	97 1		.00	5	5	1236	. 0	
	2220.0	3: 9	3.38	88	99	.00	.00	. 2	5	1238	. 0	4
- M -	2225.0	3:13	3.31	88	99	.00	.00	5	5	1233	. 0	5
	2230.0	3:16	3.30	88	100	.00	.00	- 2	5	1219	.0	4
1. 1. 1.	2235.0	3:18	3.09	88	100	.00	.00	2	5	1219	.0	55
F 1	2240.0	3:21	3.21	88	100	.00	.00	5	5	1216	. 0	5
	2245.0	3:33	3.16	89	100	.00	.00	5	5	1214	.0	55
	2250.0	3:36	3.28	88	100	.00	.00	5	- 5	1199	. 0	5
	2255.0	3:39	3.21	89	100	.00	.00	2	5	1208	.0	5
	930			. –	. ·		х х			·		÷.,
	2260.0	3:41	3.16	89	100	. 00	.00	2	5	1218	.0	5
	2265.0	3:44	3.19	89	100	.00	.00	2	5	1218	. 0	4
- r	2270.0	3:46	3.14	90	100	.00	.00	2	5	1218	.0	5
	2275.0	3:56	3.10	90	100	.00	.00	2	5	1220	. 0	4
1.3	2280.0	3:59	3.22	50 89	99	.00	.00	2	5	1225	.0	5
	2280.0	4: 1	3.20	88	100	.00	.00	5	5	1225	.0	5
			3.07	00 88	100	.00	.00	2	5	1225	.0	5
	2290.0		3.07		100	.00	.00	2	5	1223	.0	5
	2295.0	4:6			100	.00	.00	2	5	1228	.0	5
	2300.0	4:8	3.19	90 90		.00	.00	2	5	1228	.0	5
	2305.0	4:16	3.13	90	100	.00	.00	<u>ح</u>	. J	1000	.0	О ₍ .)
	97			0.0	100	00	0.0	2	5	1214	.0	5
	2310.0	4:18	2.99	90		.00	.00					5 5
	2315.0			89 00	100	.00	.00	2	· 5		.0	
	2320.0	4:22	3.13	88	100	.00	.00	2	5	1214	.0	4
4	2325.0	4:25	3.23	88	99	.00	.00	. 5	5	1214	.0 '	5
	2330.0	4:27	3.15	88	100	.00	.00	2	5	1214	.0	5
	2335.0	4:29	3.05	87	101	.00	.00	2	5	1214	.0	4
	2340.0	4:38	3.12	. 85	101	.00	.00	5	5	1229	. 0	5
	2345.0	4:40	3.06	85	101	.00	.00	2	5	1230	.0	4
	2350.0	4:42	3.09	85	101	.00	.00	2	5	1230	.0	3
•	2355.0	4:45	3.33	85	101	.00	.00	5	5	1230	.0	5.
	102				J.,		- -		· ·		· · · · · · ·	
	2360.0	4:48	3.25	85	101	.00	.00		5	1228	.0	4
	2365.0	4:50	3.25	85	101	.00	.00	2	5 -	1226	.0	5 3
	2370.0	4:58	3.09	86	99	.00	.00	2	5	1241	. 0	3
	2375.0	5: 0	3.07	86	98	.00	.00	5	5	1244	• .0	4
•	2380.0	5: 3	3.24	85	99	. 00	.00	2 2	5	1244	. Ū	5
	2385.0	5: 5	3.23	85	101	.00	.00	2	5	1241	.0	5
••	2390.0	5: 8	3.18	85	100	.00	.00	2	5	1242	. 0	5
	2395.0	5:11	3.26	86	100	.00	.00	ē,	5	1243	. 0	5
· · · ·	2400.0	5:20	3.19	86	100	.00	.00	2	5	1249	. 0	5
	2405.0	5:22	3.27	85	100	.00	.00	ž	5	1263	.0	4
e general de	1068		That II has I	"and "app" /	÷ • •		•	-	-			•

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ESSD BARRACDUTA # 4

PAGE 7

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ЛЕРТН	TIME	RS	MTI	МТО	MRI	MRO	YPM	PVM	MVI	MDOV	
$100 \\ 2410.0 \\ 2415.0 \\ 2420.0 \\ 2425.0 \\ 2435.0 \\ 2435.0 \\ 2445.0 \\ 2445.0 \\ 2455.0 \\ 2455.0 \\ 11 \\ 11$	5:25 5:28 5:31 5:34 5:37 5:57 6: 1 6: 3 6: 6 6: 10	3.31 3.27 3.25 3.27 3.21 3.39 3.28 3.28 3.28 3.28 3.36 3.40	86 86 87 88 87 86 86 87 88	$99 \\ 100 \\ 100 \\ 100 \\ 100 \\ 100 \\ 99 \\ 100 \\ $.00 .00 .00 .00 .00 .00 .00 .00	.00 .00 .00 .00 .00 .00 .00 .00	<u></u>	ទីស្ទីស្ទីស្ទីស្ទីស្ទីស្ទីស្ទីស្ទីស្ទីស្	1261 1262 1262 1262 1262 1262 1262 1262	RECDS .0 .0 .0 .0 .0 .0 .0 .0 .0 .0	ខេត្តមានមាន
2460.0 2465.0 2470.0 2475.0 2480.0 2485.0 2490.0 2495.0	6:12 6:22 6:25 6:27 6:30 6:32 6:34 6:45 6:48 6:48	3.28 3.31 3.21 3.27 3.21 3.26 3.17 3.20 3.24 3.22	88 90 90 91 91 91 91 91	$100 \\ 100 \\ 100 \\ 101 \\ 101 \\ 101 \\ 101 \\ 101 \\ 101 \\ 101 \\ 102 \\ 102 \\ 102 \\ 100 $.00 .00 .00 .00 .00 .00 .00 .00	.00 .00 .00 .00 .00 .00 .00 .00	<u></u>	ទទទទទទទទទទ	1212 1229 1241 1241 1228 1222 1222 1214 1196 1196	.0 .0 .0 .0 .0 .0 .0 .0	5555554555
2510.0 2515.0 2520.0 2530.0 2535.0 2540.0 2545.0 2550.0 2555.0 2560.0	6:53 6:56 6:58 7:10 7:12 7:15 7:17 7:20 7:22 7:31	3.25 3.23 3.22 3.27 3.20 3.27 3.29 3.25 3.22 3.21	91 91 91 91 91 91 91 91 91	102 102 103 100 100 101 102 102 103	.00 .00 .00 .00 .00 .00 .00 .00	.00 .00 .00 .00 .00 .00 .00 .00	22222222222	ទទទទទទទទ	1193 1204 1217 1226 1236 1238 1238 1238 1238 1238	.0 .0 .0 .0 .0 .0 .0 .0	លលក្លក្លក្លក្លប
1220 2565.0 2570.0 2575.0 2580.0 2585.0 2590.0 2595.0 2600.0 2605.0 2610.0 126	7:34 7:38 7:42 7:45 7:48 7:58 8: 1 8: 4 8: 7 8:10	3.35 3.44 3.50 3.37 3.39 3.32 3.30 3.39 3.45 3.38	91 92 92 92 92 92 92 92 93	$102 \\ 103 \\ 103 \\ 103 \\ 103 \\ 104 $.00 .00 .00 .00 .00 .00 .00 .00	.00 .00 .00 .00 .00 .00 .00 .00	10 10 10 10 10 10 10 10 10		1340 1341 1344 1342 1331 1325 1325 1325 1325	.0 .0 .0 .0 .0 .0 .0 .0	5555554555
2615.0 2620.0 2625.0 2635.0 2640.0 2645.0 2655.0 2655.0 2655.0 2660.0	8:13 8:22 8:26 8:29 8:31 8:33 8:35 8:43 8:45 8:45	3.26 3.25 3.40 3.34 3.23 3.13 3.11 3.03 2.87 2.57	93 93 93 94 94 94 94 94	104 104 103 104 105 105 105 105 105 105	.00 .00 .00 .00 .00 .00 .00 .00	.00 .00 .00 .00 .00 .00 .00 .00 .00	$10\\10\\10\\10\\10\\10\\10\\10\\10\\10\\10\\10\\10$	សត្តសត្តសត្ត	1325 1338 1352 1336 1335 1337 1337 1335 1337 1335	.0 .0 .0 .0 .0 .0 .0	4455555331

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1	DEPTH	TIME	RS	MTI	MTD	MRI	MRD	YPM	PVM	MVI	MDOV
C		1309	• -								RECDS
	2665.		2.62	94	105	.00	.00	10	5	1340	.0 1
1.			2.70	94	104	.00	.00	10	5	1335	.0 1
la di	2670.		2.56	94	104	.00	.00	10	5		.0 1
	2680.						.00	10	5	1347	.0 2
f	5690.		2.54	94	101	.00					.0 1
	2700.		2.41	95	99	.00		10	5	1349	
ίω τη Γ	2710.		2.57	95	100	.00	.00	10	5	1349	.0 1
•	2720.	0 9:12	2.40	94	102	.00	.00	10	5	1335	.0 1
[2730.	0 9:14	2.47	94	102	.00	.00	10	5	1331	.0 1
n in the second s	2740.	0 9:15	2.67	94	102	.00	.00	10	5	1331	.0 1
	2750.	0 9:23	2.42	93	102	.00	.00	10	5	1313	.0 1
r) i		1320					•				
	2760.		2.84	93	102	.00	.00	10	5	1301	.0 3 .0 2
	2765.		2.90	93	103	.00	. 00	10	5	1300	.0 2
۰.				93	103	.00	.00	10	5	1300	.0 1
	2770.		2.69						5		
	2775.		5:90	92	103	.00	.00	10		1327	
ы. н	2780.		2.27	92	103	.00	.00	10		1324	.0 1
	2790.	0 9:36	2.57	98	103	.00	.00	1.0	5	1324	.0 1
	2800.	0 9:40	2.96	93	104	.00	.00	10		1319	.0 3
	2805.	0 9:42	3.20	93	1.05	.00	.00	10	5	1319	.0 3
•	2810.		2.64	94	105	.00	.00	10	5	1342	$ \begin{array}{ccc} .0 & 1 \\ .0 & 3 \\ .0 & 3 \\ .0 & 3 \end{array} $
in a l	2820.		2.78	94	105	.00	.00	1.0	5	1363	.0 2
		1340		- ·		• • •			-		
	2830.		2.60	94	106	.00	.00	10	. 5	1366	.0 2
· .						.00	.00	10	5	1368	.0 1
	2840.		2.18	94	106						
	2850.		1.96	93	106	.00	.00	10	5	1331	.0 1
د <u>ب</u> ا	2860.	0 10: 1	2.13	93	106	.00	.00	10	5	1326	.0 1
	2870.	0 10: 2	2.28	93	1 07	.00	.00	10	5	1326	.0 1 .0 2
	2880.		2.43	93	106	.00	.00	10	5	1344	.0 2
i	2890.		2.37	93	105	.00	.00	10	5	1344	.0 1
	2895.		2.93	93	1.05	.00	.00	10	5	1347	.0 2
- 1	2900.		2.16	94	105	.00	.00	10	5	1351	.0 1
			2.32	92	105	.00	.00	10	5	1342	.0 1
	2910.		c. 0c	PC	100	.00	.00	10		1040	.0 1
		353	0.05		1.60	~ ~	00	1.0	· E	1040	5 I
	2920.		2.25	92	106	.00	.00	10	• 5	1342	.0 1
	2925.		3.09	92	1.06	.00	.00	10	. 5	1342	.0 3
اسم م	2930.	0 10:26	3.01	92	1.05	.00	.00	10	5	1342	.0 1
,	2935.	0 10:36	3.13	92	105	.00	.001	10	5	1350	.0 3
	2940.		3.07	91	105	.00	.00	10	5	1374	.0 2
	2950.		1.60	91	105	.00	.00	10	5	1359	.0 1
	2960.		.71	57	61	.00	.00	1	- 5	1261	.0 1
···1							.00	1	5	1261	.0 2
	2965.		.96	57	61	.00		. –			.U C
<u>د</u>	2970.		1.18		61	.00	.00	1	5	1253	.0 2 .0 1
1.4	2975.		1.28	57	61	.00	.00	1	5	1245	.0 1
· · · ·		1374				· · · ·	•	•			
	2980.	0 36:24	1.70	57	61	.00	.00	1	5	1245	.0 1
·· • •	2985.	0 36:24	1.52	57	61	.00	.00	1	5	1245	.0 2
	2990.		1.53	57	61	.00	.00	1	5	1245	.0 2
•	2995.		1.46	57	61	.00	.00	1	5	1179	.0 4
				57	61	.00	.00	1	5	1286	.0 2
•	3008.		1.04					-			
	3005.		1.08	57	61	.00	.00	1	5	1286	
	3010.		.83	57	61	.00	.00	1	5	1286	.0 1
	3015.	0 36:24	.18	57	61	.001	.00	1	5	1286	.0 1
	3020.	0 0: 0	12	57	61	.00	.00	1	5	1286	.0 1
÷	3025.		1.01	57	61	.00	.00	1	5	1286	.0 3
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	NEPTH 13	TIME 92	RS	MTI	МТО	MRI	MRÓ	YPM	PVM	MVI	MDDV PECDS	
	3030.0	0:10	1.31	57	61	.00	.00	1	5	1283	.0	4
(]	3035.0	0:49	1.38	57	61	.00	.00	1	5	1233	.0	4
	3040.0	0:53	.86	57	61	.00	.00	1	5	1231	.0	3
2	3045.0	0:57	.47	57	61	.00	.00	• 1	5	1233	.0	3
1.1	3050.0	1:13	1.36	57	60	.00	.00	. 1	5	1235	.0	5
	3055.0	1:31	2.10	56	59	.00	.00	1	· 5	1235	.0	<u>.</u> 2
	3060.0	5: 5	2.39	56	59	.00	.00	1	5	1235	.0	5
1	3065.0	5:50	1.74	55	58	.00	.00	. 1	5	1228	.0	5
	3070.0	2:23	.39	55	58	.00	.00	1	5	1223	. Ū	2
ь .,	3075.0	2:34	.89	55	58	.00	.00	1	5.	1223	• Ū .	5
•	143				•						•	8 - Î
. .	3080.0	2:51	1.47	55	58	. 00	. 00	1	5	1223	.0	5
tg.	3085.0	3:18	1.78	56	59	.00	.00	. 1	5	1223	.0	55
	3090.0	3:38	1.96	55	58	.00	.00	1	5	1223		5.
17	3095.0	3:56	2.04	56	- 59	.00	.00	1	5	1223	.0	5
	3100.0	4:23	1.41	56	59	.00	.00	1	5	1222	.0	5
	3105.0	4:51	2.42	57	60	.00	.00	1	5	1224	.0	5
en e	3110.0	5:13	2.39	57	61	.00	.00	1 -	5	1228	.0	5
		5:28	2.25	57	61	.00	.00	1.	5	1228	.0	5
L	3115.0		2.37	57	61	.00	.00	1	5	1228	.0	വനന
	3120.0	5:46			62	.00	.00	1.	5	1228	.0	5
	3125.0	6: 7	2.33	07	00	.00	.00	. 1		1200	• • •	
	148		~ ~ ~	=0	20	.00	.00	1	5	1236	.0	5
1.2	3130.0	6:36	2.26	58	62 70		.00	1	5	1246	.0	5
· · · ·	3135.0	6:55	2.42	58	62	.00			5	1244	.0	5
ţ, t	3140.0	7:11	2.45		62	.00	.00	1 1	5	1240	.0	5
Lj.	3145.0	7:30	2.49	58	63 70	.00	.00	1	5	1238	.0	5
•	3150.0	7:48	2.45	58	63	.00	.00	-	5	1235	.0	5
<u>[]</u> .	3155.0	8: 7	2.44	58	62	.00	.00	1				5
	3160.0	8:29	2.58	58	63	.00	.00	1	5	1226	.0	5
	3165.0	8:42	. 2.72	- 58	63	.00	.00	1	5	1198	.0	ੁ ਵ
r 1	3170.0	8:54	2.77	58	64	.00	.00	1	5	1199	.0	55
	3175.0	9: S	2.72	58	64	.00	.00	1	. 5	1202	.0	0
()	153	3	•		•				-		•	
	3180.0	9:17	2.80	58	64	.00	.00	1	, 5	1203	.0	5
	3185.0	9:27	2.67	58	65	.00	.00	1	5	1178	• 0 • • •	5
L	3190.0	9:40	2.74	58	65	.00	.00	1	<u>j</u> 5	1142	• 0	5 5
3.0	3195.0	9:55	2.84		65	.00	.00	1	5	1137	.0	
r i	3200.0	10: 4	2.74	58	65	.00	.00	1	5	1164	.0	5
	3201.0	10: 7	2.58	58	65	.00	.00	1	5	1166	.0	1
[~]`		· ·			NEW B	IT ID:	4					
	3205.0	2:13	2.41	 74	81	.00	.00	12	18	781	.0	3
-	3210.0	2:16	2.41	74	81	.00	.00	12	18	792	.0	4
	3215.0	5:50	2.45		81	.00	.00		18	794	.0	5
			2,55	75	85	.00	.00	12	18	793	.0	1
	3220.0	5:46 74	ليدايد والتنا	1.0	6 . 6.		\sim	<u>له</u> م.	÷		• ***	-
, s. i			0 45	75	83	.00	. 00	12	18	728	. 0	1
: •	3225.0	5:47	2.45	75 75	00 83	.00	.00	12	18	712	.0	
	3230.0	5:49 5:53	2.46	73 75	00 84	.00	.00	12	18	712	.0	3 5 5
	3235.0	5:54	2.63			.00	.00	12	18	710	.0	5
	3240.0	5:58	2.54	75 74	- 85 os		.00 .00	12	18	711	.0	5
	3245.0	6: 2	2.47	76	85 05	.00	•		18	710	.0	5
	3250.0	6: 6	2.51	76	85	.00	.00	12		674	.0	5
	3255.0	6:10	2.55	76.	84	.00	.00	. 12	18	0/4	• •	
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in a state of the	IVEPTH	TIME 605	RS	MTI	MTO	MRI	MRO	YPM	PVM	MVI	MDOV RECDS	
	3260.0		2.49	76	85	.00	.00	12	18	755	.0	5
	3265.0		2.50	76	85	.00	.00	12	18	774	. 0	4
I - J	3270.0		2.45	76	85	.00	.00	12	18	747	. 0	5
	3275.0		2.41	75	86	.00	.00	12	18	784	. 0	55
	3280.0		2.47	75	85	.00	.00	12	18	792	. 0	5
	3285.0		2.44	75	86	.00	.00	12	18	792	.0	5
	3290.0		2.40	76	86	.00	.00	12.	18	800	.0	55
Γ	3295.0		2.41	76	86	.00	.00	12	18	810	.0	5
	3300.0	6:58	2.42	76	85	.00	.00	12	18	809	.0	4
	3305.0		2.53	76	86	.00	.00	12	18	805	.0	5
- F1.	16						4					·
	3310.0		2.36	76	86	.00	.00	12	18	805	.0	5
	3315.0		2.17	77	87	.00	.00	12	18	763	.0	5
T	3320.0		2.01	77	87	.00	.00	12	18	722	.0	4
	3325.0		2.41	76	87	.00	.00	12	18	733	.0	5
	3330.0		2.41	77	87	.00	.00	12	18	741	.0	5
	3335.0		2.44	77	85	.00		12	18	743	.0	5
	3340.0		2.40	78 70	86 87	.00	.00	12	18	739	.0	55
	3345.0		2.45	78 70	86 07	.00	.00	12	18 18	736 739	.0	.) E
_	3350.0		2.30 2.30	78 78	86 86	.00 .00	.00	12 12	18 18	739	.0	5
	3355.0	8:27 702	c.30	78	00	. 00	.00	10	10	T E T	• •	~
	3360.0		2.33	78	86	.00	.00	12	18	747	. 0	5
	3365.0		2.30	78	86	.00	.00	12	18	749	.0	5
	3370.0		2.32	79	85	.00	.00		18	749	.0	5
	3375.0		2.32	79	85	.00	.00	12	18	747	.0	5
	3380.0		2.33	79	85	.00	.00	12	18	740	.0	5
ſ,	3385.0		2.32	79	86	.00	.00	12	18	740	. 0	4
	3390.0		2.53	79	86	.00	.00	12	18	747	.0	5
	3395.0			79	86	.00	.00	12	18	747	. 0	55
Ţ	3400.0		2.64	79	87	.00	.00	12	18	745	. 0	5
, i a c	3405.0		2.58	81	88	.00	.00	12	18	744	.0	5
1	17	51	•							_		_
	3410.0	10:38	2.86	82	88	.00	.00	12	18	747	.0	5
	3415.0	10:41	2.44	81	85	.00	.00	12	18	733	.0	3
	3420.0		2.28	81	85	.00	.00	12	18	733	• 0 .	1
	3425.0		2.67	81	83	.00	.00	12	18	747	.0	4
	3430.0	11:30	2.57	83	85	.00	.00	12	18	749 740	.0	5 5
	3435.0	11:36	2.56	84 04	85 05	.00	.00	12	18 19	748 746	.0	5 -
	3440.0		2.54	84 04	85	.00	.00	12	18 10	746 747	.0	5 5
	3445.0		2.55	84 04	85 00	.00	.00	12 12	18 18	747 754	.0	5
•	3450.0		2.39	84 04	88 89	.00	.00 .00	12	18 18	704 756	.0	5
	3455.0	13: 1 794	2.27	84	07	. 00	.00	15	10	1.00	• •	• •• •
	3460.0	794 13: 8	2.04	84	89	.00	.00 ·	12	18	758	.0	5
	3465.0	13:19	1.97	85	89 89	.00	.00	12	18	758	.0	5
· . •	3470.0	13:25	1.45	85	90	.00	.00	12	18	753	.0	5
	3475.0	13:31	1.39	85	90	.00	.00	12	18	751	.0	5
	3480.0		1.49	85	90	.00	.00	12	18	775	.0	3
•	3485.0	13:52	1.02	85	91	.00	.00	12	18	743	.0	5
	3490.0	14: 6	1.40	84	91	.00	.00	12	18	745	. 0	55
	3495.0	14:17	1.73	85	92	.00	.00	12	18	749	. 0	5
1. F. 4	3500.0	14:43	2.52	87	94	.00	.00	12	18	751	. 0	5
	3505.0	15: 4	2.61	85	94	.00	.00	• 12	18	749	. 0	5
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	DEPTH 18	TIME 342	RS	MTI	MTD	MRI	MRD	YPM	PVM	MVI	MDDV RECDS	
. [3510.0	15:14	1.42	87	95	.00	.00	12	18	769	.0	З
	3515.0	15:18	.51	87	95	.00	.00	12	18	780	.0	4
	3520.0	15:19	.74	87	95	.00	.00	12	18	762	.0	1
r i	3525.0	15:20	.10	87	95	.00	.00	12	18	726	.0	ē
	3530.0	15:21	.56	87	95	.00	.00		. 18	725	.0	-1
Ĺ	3535.0		-1.52	87	96	.00	.00	12	18	778	.0	ŝ
	3540.0		-1.36	87	97	.00	.00	12	18	781	.0	1
1	3545.0	15:44		87	97	.00	.00	12	18	781	.0	ò
			-3.23	88	97	.00	.00	12	18	781	.0	2 3
•				00 87	97 97	.00	.00	12	18	751	.0	4
12	3555.0	•	1.77	07	21	.00	.00	10	10	1.014	• •	т .
		366	0 40	87	96	.00	.00	12	18	738	. 0	5
е. <u>і</u>	3560.0	16:20					.00	12	18	•	.0	
	3565.0	17: 8		87	96	.00				733 700		5 4
	3570.0	17:30		88	98 1 0 0	.00	.00	12 12	18 18	722	.0	4
	3573.0	17:40	2.49	87	100	.00	.00			668 	.0	с
					NEW B	IT ID:	5					_
. [] . [.]	3575.0	2:23	3.17	79	89	.00	.00	12	18	739	. 0	0
	3580.0	3: 3	3.33	82	92	.00	.00	12.		740	.0	ឧភស
ć i	3585.0	3:19	3.35	83	92	.00	.00	12	18	787	.0	
	3590.0	3:29	2.96	03 83	92 92	.00	.00	12	18	785		4
- -	3595.0	3:31	2.33	03 83	92 92	.00	.00	12	18	786		
5	3600.0	3:39	1.68	03 83	76 93	.00	.00	12	18	803	.0	3 1
	3000.0 19		1.00	60	20	.00	.00	10	10	003	.0	1
	3605.0	3:41	2.34	83	93	.00	.00	12	18	806	.0	3
	3610.0	3:43	2.13	00 83	93	.00	.00	12	18	810		
5	3615.0	3:43 4:12	3.25	03 83	20 93	.00	.00	12	18	773	.0	·4
21	3620.0	4:40	3.78	84	94	.00	.00	12	18	728	.0	
	3625.0	5:14	3.61	83	92	.00	.00	12	18	617	.0	- H. E.
ŕ	3630.0	5:51	3.72	83	91	.00	.00	12		587		Е
				82	92				18		.0	មហមាលបាល
£.	3635.0	6:20	3.69			.00	.00	12	18	542		0 E
	3640.0	6:26	3.30	82	91	.00	.00	12	18	612	.0	
1.	3645.0	6:31	3.29	82	92	.00	.00	12	18	609 500	.0	
	3650.0 195	- 6: 38	3.56	82	92	.00	.00	12	18	593	.0	5
r	3655.0	c 6:49	3.64	82	92	.00	.00	12	18	588	.0	
	3660.0	6:59	3.64 3.68	82	92 92	.00	.00	12	18	Joo 585	.0	5
	3665.0	7:18	3.65	83	92 92	.00	.00	12	19	568	.0	5 5
•••••	3670.0	7:28	3.63 3.63	03 83	91	.00	.00	12	21	588	.0	5
	3675.0	7:41	3.00 3.70	83	92	.00	.00	13	21	586		
	3680.0	7:51	3.64	83 84	93						.0	5 5
						.00	.00	13	21	583 570	.0	2
7	3685.0	8: 2	3.66	84 04	93	.00	.00	13	21	579 460	.0	5
	3690.0	8:11	3.54	. 84.	93	.00	.00	· 13	21	699	.0	5
	3695.0	8:28	3.28	85	93	.00	.00	13	21	758	.0	5
÷.,	3700.0 200;	8:32	3.14	85	94	.00	.`00	13	21	762	.0	5
ŀ	3705.0	8:37	3.30	86	0.4	.00	.00	13	94	760		
•				86 86	94 04	.00	.00		21	762 740	.0	4
	3710.0	8:46	3.49		94 05			13	21	763 744	.0	5
	3715.0	8:50	3.13	87 07	95 05	.00	.00	13	21	761 740	.0	5
	3720.0	8:59	2.92	87 07	95	.00	.00	13	21	760 765	.0	3
	3725.0	9:1	2.78	87	95	.00	.00	13	21	755	.0	3
	3730.0	9: 6 9: 10	2.98	87	95 oc	·.00	.00	· 13	21	759 750	.0	5
	3735.0	9:10	2.84	87	96	.00	.00	13	21	758	.0	4
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ESSO BARPACOUTA # 4

PAGE 12 - B

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DEPTH 20	TIME	RS	MTI	МТО	MRI	MRD	YPM	PVM	MVI	MDDV RECIS
3740.0	9:15	2.91	87	96	.00	.00	13	21	758	.0 5
8			87	96	.00	.00	13	21	758	·.0 S
3745.0	9:16	2.60			.00	.00	13	21	758	.0 4
3750.0	9:19	2.58	87	96			13	21	758	.0 4
3755.0	9:21	2.44	88	96	.00	.00			756	.0 3
3760.0	9:59	2.16	88	97	.00	.00	13	21		.0 4
3765.0	9:32	2.16	88	96	.00	.00	13	21	764 744	
3770.0	9:33	1.44	88	96	.00	.00	13	21	764	.0 1
3775.0	9:38	2.16	88	97	.00	.00	13	21	764	.0 5
3780.0	9:47	2.59	88	97	.00	.00	13	.21	764	.0 5
3785.0	9:57	2.37	. 88	97	.00	.00	13	21	762	.0 5
)69									· · ·
3790.0	10: 0	2.00	88	97	.00	.00	13	21	775	.0 5
3795.0	10: 4	2.01	88	97	.00	.00	13	21	749	.0 5 .0 5
3800.0	10:13	2.41	89	98	.00	. 00	13	21	748	.0 5
3805.0	10:22	2.74	89	98	.00	.00	13	21	750	.0 5
3810.0	10:25	2.39	89	98	.00	.00	13	21	750	.0 4
3815.0	10:28	2.36	90	98	.00	.00	13	21	747	.0 5
	10:28	2.29	90	99	.00	.00	13	21	759	.0 5
3820.0	•		90 90	97	.00	.00	13	21	763	.0 5 .0 5 .0 5 .0 5 .0 5
3825.0	10:42	2.44		27 95	.00	.00	13	21	762	.0 5
3830.0	10:49	2.55	90		.00	.00	13	21	758	.0 5
3835.0	11: 8	2.61	90	96	.00	.00	10	L- 1	1.00	•••
211		~ ~ ~		100	.00	.00	13	21	711	.0 5
3840.0	11:42	3.60		100			13	21	693	.0 5
3845.0	11:50	3.20		100	.00	.00				.0 2
3850.0	12: 1	2.94	91	100	.00	.00	13	21	699 74 E	
3855.0	15:55	3.73	91	100	.00	.00	13	21	715	.0 5
3860.0	12:39	3.66	92	101	.00	.00	13	21	709	.0 5
3865.0	12:47	3.32	92	101	.00	.00	13	21	712	.0 5
3870.0	13: 2	3.57	92	99	.00	.00	13	21	706	.0 5
3875.0	13:13	3.51	92	101	$.00^{\circ}$.00	13	21	704	.0 5
3880.0	13:29	3.45	92	102	.00	.00	13	21	652	.0 5
3885.0	13:36	3.02		102	.00	.00	13	21	658	.0 - 4
	64				•					$\gamma = 1$
	13:47	3.44	92	102	.00	.00	13	· 21	655	.0 .5
3895.0	14: 1	3.48	92	101	.00	.00	13	21	652	.0 5
3900.0	14:23	3.78		101	.00	.00	13	21	645	.0 5
3905.0	14:35	3.59		101	.00	.00	13	. 21	644	.0 5
3910.0	14:49	3.57		101	.00	.00	13	21	646	.0 5
3915.0	15:19	3.73		101	.00	. 00	13	21	670	.0 5
3920.0	15:38	3.82		101	.00	.00	13	21	640	.0 5
3925.0	15:49	3.60		101	.00	.00	13	21	647	.0 5
3930.0	15:58	3.54		101	.00	.00	13	21	647	.0 5.
3935.0	16: 8	3.56		101	.00	.00	13	21	647	.0 5
	214	0.00	. 1	101						
3940.0	16:20	3.68	91	101	.00	.00	13	21	646	.0 5
		3.31	92	101	.00	.00	13	21	650	.0 5
3945.0	16:33 16:44	3.59		100	.00	.00	13	21	652	.0 5
3950.0				100	.00	.00	13	21	655	.0 5
3955.0	16:50	3.30			.00	.00	13	21	660	.0 5
3960.0	16:57	3.40		101		.00	13	21	648	.0 5
3965.0	17:11	3.73		101	.00		13	21	645	.0 5
3970.0	17:22	3.64		99	.00	.00				
3975.0	17:41	3.58		100	.00	.00	13	21	646 757	
3980.0	17:48	3.30		100	.00	.00	13	21	656	
3985.0	17:57	3.52	91	101	.00	.00	13	21	662	.0 5
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ESSD BARRACOUTA # 4

PAGE 13 - B

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	DEPTH		RS	MTI	мто	MRI	MRO	YPM	PVM	MVI	MDDV PECDS
	22	18:4	3.53	91	101	.00	.00	13	21	661	.0 4
	3990.0		3.34	92	101	.00	.00	13	21	665	.0 3
	3995.0	18:16	3.03	92	101	.00	.00	13	21	662	.0 5
	4000.0	18:20		91	101	.00	.00.	13	21	662	.0 4
11	4005.0	18:30	3.51	91	101	.00	.00	13	21	628	.0 5
	4010.0	18:59	3.90	92	101	.00	.00	13	21	669	.0 5
	4015.0	19:17	3.83	92 92	100	.00	.00	13	21	660	.015.
	4020.0	19:28	3.68		100	.00	.00	13	. 21	653	.0 5 .0 5 .0 5 .0 5 .0 5
	4025.0	19:46	3.94	92			.00	13	21	654	.0 5
-	4030.0	50: 0	3.80	92	102	.00		13	21	654	.0 5
7 7	4035.0	20: 9	3.64	92	102	.00	.00	10	F 1		••
	23			•		<i></i>	~ ~	10	21	660	.0 5
1.1	4040.0	20:25	3.65	92	101	.00	.00	13	21	685	.0 5
:	4045.0	20:33	3.49	91	100	.00	.00	13		684	
	4050.0	20:42	3.65	92	100	.00	.400	13	21	683	.0 5 .0 5 .0 5 .0 5 .0 3
	4055.0	20:52	3.63	92	101	.00	.00	13	21	684	.0 5
1 -	4060.0	21: 0	3.60	92	102	.00	.00	13	21		.0 5
[]	4065.0	21:19	3.97	92	102	.00	.00	13	21	682	.0 0
	4070.0	21:35	2.27	92	102	.00	.00	13	21	681 675	
1. 	4075.0	21:37	2.63	92	101	.00	.00	13	21	675	
	4080.0	21:38	2.38	92	100	.00	.00	13	21	675	.0 2
	4085.0	21:38	2.40		100	.00	.00	1,3	21	675	.0 1
	23							•			
	4090.0	21:39	2.15	92	100	.00	.00	13	21	675	.0 1
10	4095.0	21:40	2.07		101	.00	.00	13	21	679	.0 1
	4100.0	21:51	2.07		102	.00	.00	13	21	702	.0 1
	4100.0	22:53	3.30		101	.00	.00	13	21	461	.0 3 .0 5
т. Г.Т.		22:58	2.76	81	98	.00	.00	13	21	478	.0 5
	4110.0	23: 0	2.49		100	.00	.00	13	21	564	.0 4
1.1	4115.0	0:3	4.10		100	.00	.00	13	21	595	$ \begin{array}{ccc} .0 & 5 \\ .0 & 5 \\ .0 & 4 \end{array} $
	4120.0	0:41	4.19		100	.00	.00	13	21	670	.0 - 5
	4125.0	0:58	3.42		101	.00	.00	13	21	691	
	4130.0		2.90		101	.00	.00	13	21	700	.0 1
	4135.0	1: 1	c.90	.~1	101	• • •	•••				
F		174 ¹	0 E 0	91	101	.00	.00	13	. 21	710	.0 5
1.5	4140.0					.00	.00	13	21	705	.0 5
с. 21-	4145.0	1:17	3.48		101	.00	.00	13	21	7.06	.0 5
	4150.0	1:33	3.75		102		.00	13	21	707	.0 5
	4155.0	1:43	3.42		102	.00	.00	13	.51	702	.0 5
L		2:12	3.86		102	.00		13	21	699	.0 5 .0 5 .0 4
	4165.0	2:32	3.56		101	.00	.00 .00	13	21	706	.0 5
· · · · · · · · ·	4170.0	2:51	3.79		103	.00	.00	13	21	706	.0 5 .0 5 .0 5 .0 5
U	4175.0	3:16	3.89		104	.00		13	21	709	.0 5
	4180.0	3:35	3.84		104	.00	.00	13		708	.0 5
		3:46	3.44	94	105	.00	.00			.100	
•	248		_					10	21	708	.05 .05 .05
	4190.0	3:52	3.34		105	.00	.00	13		708 710	.0 5
d a	4195.0	3:58	3.33		105	.00	.00	13	21		.0 5
	4200.0	4:13	3.17		105	.00	.00	13	21	728 725	.0 5
ŧ. i	4205.0	4:18	2.96		104	.00	.00	13	21	725	.0 5
	4210.0	4:30	3.41		102	.00	.00	13	21	703	.0 5 .0 5 .0 5 .0 5 .0 5
	4215.0	4:41	3.39		103	.00	.00	16	21	715	.0 5
	4220.0	5: 2	3.80	93	105	.00	.00	20	20	722	.0 5
	4225.0	5:15	3.58	: 93	105	.00	.00		03	722	.0 5
	4230.0	5:43	3.84		105	.00	.00	50	20	727	
	4232.0	5:55	3.74	95	106	.00	.00	20	20	725	.0 2
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ESSD BARRACOUTA # 4

			TOPPA	COUTA	# 4			PBB	<u> </u>	- 1	. • ¹ .
ES 1010		ESSU	Place			,					
пЕРТН ТІМЕ	RS	MTI	MTD	MRI	MRD	YPM	PVM.	MAI		ECDS	~
DEPTH TIME 2474 4235.0 2:2 4240.0 2:4 4245.0 21:4 4255.0 21:4 4255.0 21:4 4260.0 21:4 4265.0 21:5 4270.0 22: 4275.0 23:5	0 3.00 8 3.30 4 2.10 4 2.49 48 3.31 49 3.08 52 3.10 0 3.05	83 85 79 79 80 80 5 80 7 80	97 96 93 97 96 95 90 90	.00 .00 .00 .00 .00 .00 .00 .00		20 20 20 20 20 20 20 20 20 20	20 20 20 20 20 20 20 20 20 20	682 712 314 369 371 372 370 371 373 421	.0 .0 .0 .0 .0 .0 .0 .0))))	3 5 1 1 1 2 5 4 5
$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	9 3.39 14 3.14	4 78 0 78 7 79 9 81 3 82 6 84 7 84 2 84 0 84	88 90 91 91 92 92 92 92 92 92		00. 00 00 00 00 00 00 00 00 00 00 00	20 20 20 20 20 20 20 20 20	20 20 20 20 20 20 20 20 20	459 459 461 462 458 458 458 458 458		0 0 0 0 0 0 0	5 5 5 5 5 5 5 5 5 1 1
$\begin{array}{r} 2542 \\ 4335.0 & 13 \\ 4340.0 & 13 \\ 4345.0 & 13 \\ 4350.0 & 13 \\ 4355.0 & 13 \\ 4360.0 & 13 \\ 4365.0 & 13 \\ 4365.0 & 13 \\ 4370.0 & 13 \end{array}$	27 2.8 28 2.8 29 2.7 30 2.5 31 2.9 42 2.9 45 2.9 50 2.5 58 2.9	32 84 32 84 59 84 54 84 97 84 40 84 57 84 63 84 73 85	; 9 9 9	3.0 3.0 3.0 3.0 3.0 4.0 5.0 5.0	0 .01 0 .01 0 .0 0 .0 0 .0 0 .0	0 21 0 21 0 21 0 21 0 21 0 21 0 21 0 21) 2 0 2 0 2 0 2 0 2 0 2 0 2 0 2	$\begin{array}{ccc} 0 & 470 \\ 0 & 470 \\ 0 & 470 \\ 0 & 470 \end{array}$) •) • 5 • 9 7 7	0 0 0 0 0 0 0 0 0	2 1 1 2 1 3 5 5 5 5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2:18 3. 2:19 2. 2:22 2. 2:24 2. 2:33 2. 2:37 2. 2:50 2. 2:54 2.	54 86 31 87 78 87 91 8 30 8 78 8 57 8 22 8 .19 8	57 9 77 9 78 8 9 9	96 .(96 .) 97 .) 97 .) 98 . 98 . 98 . 99 .	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	0 2 00 2 00 2 00 2 00 2 00 2 00 1	20 8 20 8 20 8 20 8 20 8 20 8 20 8 20 8	20 45	18 17 19 18 18	.0 .0 .0 .0 .0 .0 .0 .0	4 5 4 4 5 4 4 5 5
$4430.0 \\ 2610 \\ 4435.0 \\ 4440.0 \\ 4445.0 \\ 4445.0 \\ 4450.0 \\ 4455.0 \\ 4455.0 \\ 4460.0 \\ 1000000000000000000000000000000000$	3: 0 2 3: 7 3 3:11 3 3:14 2 3:15 2 3:26 2 3:26 2 3:36 2 3:46 2 3:46 2 3:51 3 3:54 6	.03 8 .79 9 .25 9 .18 9 .92 9 .92 9 .92 9 .96 9	9 9 90 90 90 1 90 1 90 1 90	99 98 98 98 00 00 00 01 01 01	00 00 00 00 00 00 00 00 00 00	00 00 00 00 00 00	20	20 4 20 4 20 4 20 4 20 4 20 4 20 4 20 4	55 56 56 49 50 52 51 49 50	.0 .0 .0 .0 .0 .0 .0 .0	54400105554

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ESSD BARRACOUTA # 4

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	DEPTH	TIME	RS	MTI	MTD	MRI	MPD	YPM	PVM	MVI	MDOV	1997. 1997 1997 1997 1997 1997 1997 1997 1997 1997 1997 1997 1997 1997 1997
		-52									RECI	IS .
	4485.0	4: 6	2.80	91	101	.00	.00	20	50	450	.0	2
	4490.0	4:14	3.38	90	101	.00	.00	20	20	450	.0	5
	4495.0	4:22	3.51	90	101	.00	.00	20	20	448	.0	5
	4500.0	4:31	3.59	90	101	.00	.00	20	20	449	.0	5
	4505.0	4:40	3.55		101	.00	.00	20	20	447	.0	5
	4510.0	4:50	3.68		101	.00	.00	20	· 20	446	.0	5
ę ł	4515.0	5:12	3.81	87	99	.00	.00	20	20	449	.0	5
	4520.0	5:26	3.84		98	.00	.00	20	20	454	.0	5
	4525.0	5:30	3.16	88	99	.00	.00	20	20	456	.0	มมมนม
	4530.0	5:32	2.78		100	.00	.00	20	20	457	. 0	З
÷.,					• • •		•••				• • • • • • •	
-	4535.0	5:33	2.68	89	100	. 00	.00	20	20	457	.0	1
-	4540.0	5:34	2.81	89	100	.00	.00	20	20	457	. 0	З
-	4545.0	5:36	2.79	89	100	.00	.00	20	20	458	. 0	3
	4550.0	5:45	2.54		100	.00	.00	20	20	462	.0	3
-	4555.0	5:55	3.08	88	100	.00	.00	20	20	463	.0	00000
1	4560.0	6:2	3.31	88	100	.00	.00	50	50	462	.0	5
	4565.0	6: 7	3.01	89	100	.00	.00	20	20	461	.0	5
	4570.0	6:10	2.74	89	100	.00	.00	20	20	460	. 0	4
		6:10	2.19	89	100	.00	.00	20	20	461	.0	1
	4575.0	0:19	2.54	84	97	.00	.00	14	18	265	.0	5
1	4580.0 273		C. 94	04	21	. 00	.00	14	10	L '0' 0'	• •	
	4585.0	0:23	2.55	85	94	.00	.00	14	18	337	.0	5
	4353.0	1:30	3.22	84	93	.00	.00	14	18	284	.0	$\widetilde{5}^{\circ}$
. 1	4595.0	1:30	2.75	82	90	.00	.00	14	18	322	.0	5
a di tang a	4600.0	1:53	3.29	82	93	.00	.00	14	18	307	.0	5
. 3	4605.0	4:24	2.77	78	90	.00	.00	14	18	333	.0	5
.,	4610.0	4:46	3.45	76	88	.00	.00	14		345	.0	5
	4615.0	5:8	3.44	77	92	.00	.00	14	18	339	.0	5
j,	4620.0	5:41	3.97	80	92	.00	.00	14	18	333	.0	5 5
	4625.0	6:12	3.95	82	91	.00	.00	14	18	335	.0	5
	4630.0	7:9	4.15	82	92	.00	.00	14	18	349	.0	5
	4030.0		7.10		• •				•••	- • •	• •	. –
. •	4635.0	7:52	4.08	83	92	. 00	.00	14	. 18	363	.0	5
-	4640.0	15:21	3.17	83	89	.00	.00	14	18	355	. 0	5
	4645.0	15:35	3.35	79	76		.00	14	18	209	. 0	5
	4650.0		3.05	78	82	.00	.00		18	180	.0	5
7	4655.0	15:53	2.72	78	83	.00	.00	14	18	257	.0	5
	4660.0		2.89	77	85	.00	.00	14	18	261	. 0	5
1	4665.0	16:48	4.01	76	87.			14	18	281	.0	5
, ,		1:18	3.91	77	88	.00	.00	14	18		.0	5
	4675.0	1:44	3.06	76	89		.00	14	18	266	. 0	5
÷	4680.0	1:55	2.84		91	.00	.00	14	18	273	. 0	5
,	4660.0			1 8	• ±	a <u>1</u> .						-
	4685.0		2.63	77	91	.00	.00	. 14	18	263	. 0	5
		2:11	2.38	77	91	.00		14		198	.0	5
÷	4695.0	2:14	1.90	77	91	.00	.00	14	18	196	.0	5
	4700.0		1.97	77		.00	.00	14	18	191	.0	5
1	4703.0	2:22	2.13	77	90	.00	.00		18	191	.0	3 -
ł						-						 *
		-			NEW B	IT ID:	9					
	میں میں سے میں میں سے ہیں۔ ربی اعمال ہی جب اور								••••••••••••••••••••••••••••••••••••••			-
	4705.0		2.36	82	91	.00	.00	12	19	369 247	.0	1
	4710.0	11:52	2.81	82	91	.00	.00	12	19	367	.0	1
¢		•		÷ 1		· .		•				
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DEPTH	TIME	RS	MTI	мто	MRI	MRO	YPM	PVM	MVI	MDOV		
	2865				•					RECDS	X	
4715.		2.75	82	91	.00	.00	12	19	367	.0	1.	
4720.		2.69	82	91	.00	.00	12	19	367	.0	1	
4725.		2.53	82	92	.00	.00	12	19	387	. 0	3	
4730.		2.47	82	92	.00	.00	12	. 19	391	. 0	З	
4735.		2.83	82	92	.00	.00	12	19	392	.0	5	
4740.		3.15	82	- 92	.00	.00	12	19	397	. 0	5	
4745.		2.73	82	. 95	.00	.00	12	19	397	.0	4	
4750.		2.72	82	92	.00	.00	12	19	397	.0	5	
4755.	0 12:48	3.34	82	91	.00	.00	12	19	406	.0.	5	
4760.	0 12:55	3.13	82	91	.00	4. 00	12	19	394	.0	З	
	2900											
4765.	0 12:57	2.76	82	91	.00	.00	12	19	396	.0	4	
4770.	0 13: 0	2.84	82	92	.00	.00	12	19	395	.0.0	3	
4775.	0 13: 1	2.66	85	92	.00	.00	12	19	394	. 0	4	
4780.	0 13: 4	2.72	82	92	.00	.00	12	19	393	. 0	4	
4783.	0 13: 7	3.01	82	93	.00	.00	12	19	394	.0	3	

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	•	• · · ·	DUMP C
	DEPTH	-	Well depth in feet
	STEP		Depth increment in feet
	CHRS	-	Cumulative bit hours. The number of hours that the bit has actually been 'on bottom' ás opposed to in the hole, recorded in
			decimal hours
	WOB	-	Weight on bit in thousands of pounds
	HKLDX	-	Maximum hookload. This is the total weight of
	•		the string. The value for maximum hookload picked up by the computer is the average value of the total weight of the string over a 5
•	·	• •	second interval beginning after the rotary table has made five revolutions after the
	•	· · ·	slips have been pulled. This value is then
÷	•		fixed in the computer memory until the next time the slips are set, when a new value is taken.
	HKLD	· _ ·.	Current hookload. This is the weight of the
	IIKLD	-	string when 'on bottom' i.e. whilst actually drilling. The difference between the maximum hookload is the computer calculated weight on bit.
•	BWOV	-	The weight on the bit override setting. This is used in the event of a hookload sensor
		· .	malfunction to enable the operator to inform the computer of the WOB in use.
•	SPM1	-	Stroke rate/minute for pump number 1
	SPM2	-	Stroke rate/minute for pump number 2
۰.	PMPR		The pump pressure, psi
	PCSG	-	Casing pressure. This is the pressure exerted on the casing after the well has been shut in following a 'kick'.
•	HSP	-	Hydrostatic pressure. This is the pressure exerted by the column of mud in the hole, measured in psi.
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CORE LABORATORIES



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ESSD BARRACOUTA # 4

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)EPTH	STEP 64	CHRS	NDB	нкерх	HKL D	BMDA	SPM1	SPM2	PMPP	PCSG	HSP
				NEW	BIT I	D:	2				
720.	00	.0	6	150	144	· 0	1111.0	99.0	1901	0	32
750.			11	151	140	0					34
760.	0 10.0				130	0					35
770.					135	0					36
780.			14		137		. 109.3				36 37
790.			19		132		109.2 108.9				
800.			21 19		130		108.5				38
810. 815.					133		109.6				36
820.					135	0 0					36
830.	$78 \\ 0 10.0$.2	19	151	132	0	82.5	99.0	1668	0	37
840.					137	Ŭ.					37
850.					130	Ō	101.5		•		38
860.				151	129	0	101.2	99.0	1866		39
870.			16	151	135			99.0			41
880.	0 - 10.0				135		97.5				4
885.					133			99.0			4
890.					136		98.0				4: 48
895. 900.	$ \begin{array}{ccc} 0 & 5.0 \\ 0 & 5.0 \end{array} $				133 139	0 0	98.0 101.4				4
	90					_					
905.				151	138	0		99.0			48 48
910.						0	105.3	101.0			40 48
915.					$\frac{140}{137}$	0		101.0			
920. 940.					136		107.0				43
950.					139	Õ		101.0			44
955.					139	Ō		101.0			4.
960.					140	. 0	107.8	101.0	1972	0	45
965.		.5		153	139	0		101.0	1973	0	4
970.		.5	15	152	138	0	107.9	101.0	1975	0	40
975.	$106 \\ 0 5.0$.5	12	152	140	0	106.8	101.0	1975	0	4.
980.			15	152	137	0		101.0	1989	Û	44
985.	0 5.0	.6	16	152	136	Û		101.0	1990	0	45
990.			16		136	0		101.0	1996	0	45
995.			17	154	136	0		101.0	1996	0	48
1000.			17	155	138	0		101.0	1978 1848	0 0	45 45
1005.			15	155 155	140 133	0 0		101.0		0	45
1010.			22 · 24	155	133	0		102.5		0	46
1020.0	0 10.0		22	155	133	Ŏ		103.3	1847	ů	46
	122	•		4 10 10	4.55.4	o '	107 0	100 0	1884	0	47
1035.			25 27	156 156	131 129	0	107.9			0 0	47 47
1040.0			27 25	155	130	0		103.3		0.	47
1040.0		· .8	26 26	155	129	0		103.3		0	48
1055.		.8	27	155	128	Ō		103.3		Û	4:
1060.0		. 9	26	155	128	0		103.3		0	47
1070.1		.9	27	155	128	0	107.2	103.3	1953	0	48

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ESSD BARRACOUTA # 4

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	DEPTH S		CHRS	WDB	HKLDX	HKLD	BWDV.	SPM1	SPM2	PMPR	PCSG	HSP
الدرية "	1080.0	10.0	.9	26	155	129	0		103.3	1964	0	489
	1085.0	5.0	1.0	27	155	128	0		103.3	1977	· 0	495
	1090.0	5.0 5.0	1.0	21 17	156 156	134 139	0 0		103.3	1977 1862	0 0	497 501
• • •	1095.0	5.0 5.0	1.0	30	156	126	0		103.3	1868	0	502
	1105.0	5.0	1.0	24	155	130	Ō		103.3	1870	0	507
الم	1110.0	.5.0	1.0	25	155	130	0		103.3	1874	0 -	511
- 1	1115.0	5.0	1.1	56	155	129	0		101.5	1870	0	516
	1120.0	5.0	1.1	23 21	155 155	132 134	0 0	106.5		1875	0 0	521 516
₽	1130.0	10.0	1.1	C1	100	1.24	Ū.	101.1	22.0	1900	U.	
	1135.0	5.0	1.2	22	156	134	.0	109.7	99.8	1929	0	521
9 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1140.0	5.0	1.2	53	156	133	0	110.0	99.8	1986	0	526
	1145.0	5.0	1.2	88	156	134	0	117.8	99.8	2316	0	531
$\langle \Box \rangle$	1150.0	5.0	1.2 1.2	23	156 156	133 131	0 0	122.2	99.8 99.8	2625 2535	0 - 0	536 535
	1155.0	$5.0 \\ 5.0$		24 23	155	132	0	117.0	99.8		0	530
	1165.0	5.0	1.3	23	155	132	Ū	117.0	99.8	2303	Ũ	533
	1170.0		1.3	55	155	133	0	117.0	99.8	2306	0	537
1_1	1175.0	5.0	1.3	23	155	132	Û	117.1		2313	0	542
·	1180.0 16	5.0	1.4	23	155	132	0	117.2	99.8	2318	0	547
	1190.0	10.0	1.4	25	155	135	0	117.9	104.4	2314	0	545
њя :	1195.0	5.0	1.4	25	155	130	0		109.0	2314	0	551
	1200.0	5.0	1.4	19	155	136	0	117.2		2307		557
	1205.0	5.0	1.4	24	155	131	0	116.8		2303	0	560
	1210.0	5.0	1.5	24	155 155	131	0	116.8 116.4		2294 2288	· 0 0	564 570
	1215.0	5.0	1.5 1.5	24 24	100	131 137	0 0	118.4		2342	. 0	558
	1225.0	5.0	1.6	25	156	131	0	119.3		2356	0	562
	1230.0	5.0	1.6	25	156	131	-0	119.3	109.0	2352	0	563
	1235.0	5.0	1.6	23	156	133	0	118.5	111.1	2333	0	567
٤j -	19		• <i>z</i> `	22	157	135	ň	118.8	444 4	2331	0	571
1	1240.0 1245.0	$5.0 \\ 5.0$	$1.6 \\ 1.7$	25	157	130	0	118.3		2328	0 0	576
	1250.0	5.0	1.7	24	157	133	Ŭ	116.3		2275	0	564
دين	1255.0	5.0	1.7	25	157	132	0	115.3	111.1	2258	Û	567
·	1260.0	5.0	1.7	27	157	130	0	115.3		2255	0	568
	1265.0	5.0	1.8	26	157	131	0	116.1		2281	0	573 570
	1270.0 1275.0	5.0 5.0	1.8 1.8	24 23	157 157	133 134	-0 0	119.4 119.4		2331 2339	0 0	579 581
	1280.0	5.0	1.8	27	157	134 130	0 0	119.5		2360	0 -	585
	1290.0	10.0	1.8	26	157	131	Ū	119.9		2365	Û	592
	5		•									
	1295.0	5.0	1.9	20	157	137	Û	119.4		2356	0	593
	1300.0 1305.0	$5.0 \\ 5.0$	$1.9 \\ 1.9$	27 23	157 157	130 134	0 0	119.3 119.5		2356 2354	0 0	597 602
[]	1310.0	5.0	1.9	26	157	131	0	119.3		2347	0	602 607
	1315.0	5.0	2.0	22	157	141	. 0	120.6	111.1	5399	0	588
(.) 	1320.0	5.0	2.0	20	157	148		117.7		2385	0	595
[]	1325.0	5.0	2.1	20	161	146	0	114.4		2360	0	602
	1330.0 1335.0	5.0 5.0	2.2 2.2	16 17	164 164	148 147	0 0	110.7 115.9		2328 2396	0 0	609 612
•	1350.0 1340.0	5.0	с.с 2.3	20	164	147	. 0	120.0		2376 2436	0	612
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	DEPTH	STEP 244	CHPS	HDB	HKLDX	HKLD	BMDA	SPM1	SPM2	PMPR	PCS6	HSP
and the second s	1345. 1350. 1355.	0 5.0 0 5.0 0 5.0	2.4 2.5	19 26 26	166 168 168	146 142 142 142	0 0 0	119.7 120.0	115.5 115.5 115.5 115.5	2474 2428 2423	0 0 0 0	611 615 622 625
	1360. 1365. 1370. 1380.	$ \begin{array}{ccc} 0 & 5.0 \\ 0 & 5.0 \end{array} $	2.6	26 26 23 19	168 168 168 161	142 142 145 143	0 0 0	120.1 120.5	115.5 115.5 115.9	2415 2415 2417 2427	0 0 0	623 623 625 623
And a second second	1385. 1390. 1395.	0 5.0	2.8	19 21 22	160 160 160	141 139 138	0 0 0	123.2	118.1 118.1 118.1	2428 2433 2432	0 0 0	628 636 643
	1400. 1405. 1410.	$\begin{array}{ccc} 0 & 5.0 \\ 0 & 5.0 \\ 0 & 5.0 \end{array}$	2.9	20 21 21	160 161 162	140 140 142	• • • • • • • • • • • • • • • • • • •	120.8	118.1 118.1	2430 2430 2505	0 0 0	648 650 643
	1415. 1420. 1425. 1430.	$\begin{array}{ccc} 0 & 5.0 \\ 0 & 5.0 \\ 0 & 5.0 \end{array}$	3.0 3.0 3.0 3.1	24 25 24 25	164 164 164 164	140 139 140 139	0 0 0 0	121.3 121.1 121.2 121.3	118.1 118.8 119.5	2511 2514 2506 2502	0 0 0 0	644 647 649 653
	1435. 1440. 1445.	0 5.0	3.1 3.2 3.2	' 25 25 24	164 165 165	139 140 141	0 0 0	121.3	119.5 119.5 119.5	2444 2488 2505	0 0 0	660 653 653
and a second	1450. 1455. 1460. 1465.	0 5.0 0 5.0 0 5.0	3.2 3.3 3.3 3.4	25 25 26 27	165 167 167 167	140 142 141 140	0 0 0 0	121.7 121.6 122.1 122.3	119.5 119.9	2512 2510 2513 2515	0 0 0	654 657 661 664
	1470. 1475. 1480. 1485.	0 5.0 0 5.0	3.5 3.5 3.5 3.6	27 27 28 27	167 167 167 167	140 140 139 140	0 0 0 0	121.8 119.7 120.2 120.4	120.0 120.0	2501 2453 2452 2446	0 0 0	662 665 668 673
	1490. 1495. 1500.	0 5.0 346	3.6 3.7 3.7	28 28 27	167 167 167	139 139 140	0 0 0	120.6 120.8 120.0	120.0	2453 2454 2465	0 0	677 681 677
	1505.0 1510.0 1515.0	0 5.0 0 5.0 0 5.0	3.8 3.8 3.9	27 28 27	167 167 167	140 139 140	0 0 0	118.7 123.8 124.4	117.7 117.7 117.7	2465 2451 2450	0 0 0	677 677 678
	1520.) 1525.) 1530.) 1535.) 1540.)	0 5.0 0 5.0 0 5.0	$\begin{array}{c} 4.0 \\ 4.0 \\ 4.0 \\ 4.0 \\ 4.0 \\ 4.1 \end{array}$	27 27 22 24 30	167 167 167 165 167	140 140 145 145 137	0 0 0 0 0	124.0 123.9 124.0 117.6 116.2	117.7 117.7 117.7	2453 2454 2455 2404 2389	0 0 -0 -0	685 689 691 693
	1545.(3 1550.() 5.0 372) 5.0	4.1 4.1	29 29	167 167	138 138	ů , 0	116.3 116.2	118.0 118.0	2392 2395	0	698 701 703
	1555.0 1560.0 1565.0 1570.0) 5.0) 5.0	4.1 4.2 4.2 4.2	29 127 25 23	167 167 167 167	138 140 142 144	0 0 0 0	116.3 116.2 116.9 117.5	118.0 118.0	2394 2396 2444 2465	0 0 0 0	705 707 707 709
	1575.0 1580.0 1585.0 1590.0) 5.0) 5.0) 5.0) 5.0	4.2 4.3 4.3 4.3	21 24 24 24	167 167 167 167	146 143 143 143	0 0 0	117.7 118.0 120.4 120.6	118.0 118.0 118.0 118.0	2465 2473 2511 2514	0 0 0	711 714 718 721
	1600.0 4) 10.0 105	4.4	26	167	141	0	120.7	120.6	2518	0	726

ESSO BARPACOUTA # 4

had a			•									
	DEPTH	STEP 405	CHRS	MDB	HKLDX	HKLD	BMDA	SPM1	SPM2	PMPR	PCSG	HSP
	1610.0	0 10.0	4.5 4.5	21	163	156	0		121.0	2513	0	747
r j	1615.(1620.(4.5	25 26	· 167 167	$141 \\ 141$	· 0		121.0	2501 2474	0	751 754
	1620.0		4.6	20	167	141 140	0		121.0	2474	0.	758
	1650.0		4.6	26	167	141	0		121.5	2486	0	758
11	1655.0		4.7	25	167	142	ŏ		122.0	2480	0	760
	1660.0		4.7	25	167	142	Ő		122.0	2480	0	764
المستر الم	1665.0	5.0	4.8	26	167	141	0	122.9	122.0	2478	0	767
f i.	1670.0		4.8	24	167	143	Û,		122.0	2478	0	767
	1675.0		4.8	23	166	144	0	119.8	118.0	2431	. 0	769
. Annist in the	4	151) 5.0	4.9	21	100	140	0	113 8	110 0	2000		
Γ	1685.0		4.9	25	164 167	142 141	0 10		118.0 118.0	2399 2485	0	767 767
	1690.0		4.9	26	167	141	0		118.0	2489	0	767
х.,	1695.0		4.9	26	167	141	Õ		118.0	2491	.0	768
, [].	1700.0		5.0	26	167	141	0		119.0	2497	 0	773
	1710.0	10.0	5.0	24	168	143	0	116.3	123.0	2385	0	775
	1720.0		5.1	27	168	141	0		123.0	2468	0	781
	1725.0		5.1	27	168	141	0		123.0	2477	0	786
	1730.0		5.2	28	168	140	0		123.0	2473	0	788
	1735.0	92	5.2	28	168	140	0	118.8	123.0	2475	0	799
T÷.	1740.0		5.2	25	168	143	0	119.0	123.0	2477	0	819
	1745.0		5.3	26	168	142	0		123.0	2475	0	828
÷ +;	1750.0		5.3	24	169	144	0		123.0	2491	0	799
	1755.0	5.0	5.3	26	169	143	Ó		122.3	2487	. 0	801
	1760.0		5.4	27	169	142	· 0	121.4	121.0	2452	0	805
	1765.0		5.4	27	169	142	0		121.0	2445	0	809
	1770.0		5.4	26	169	143	0		121.0	2449	0	811
	1775.0		5.5	26	169	143	0		121.0	2456	0	818
1	1780.0		- 5.5 5.5	25 27	168 169	143 142	0	120.8	121.0	2471 2499	0	820
		28	0.0	L (105	176.	0	110.0	161.0	6422	Ū.	810
	1790.0		5.6	27	169	142	0	119.1	119.1	2501	0	808
	1795.0	5.0	5.6	27	169	142	0	119.5		2511	0	811
	1800.0	5.0	5.7	26	169	143	0	119.6	118.6	2512	0	815
	1805.0	5.0	5.7	24	169	145	0	118.8		2501	Û	Ş17
e 1.3	1810.0	5.0	5.7	24	169	145	0	116.2		2462	0	820
	1815.0 1820.0	5.0 5.0	5.8 5.8	21 25	169 169	148 144	0	116.1		2456	0	822
e la construction de la construcción de la construc	1825.0	5.0	J.O 5.9	23 23	169	144	0 0	115.6 116.3		2460 2469	0 0	824 827
:	1830.0	5.0	5.9	22	169	147	0	116.4		2469 2470	0	.ocr 831
	1835.0	5.0	6.0	27	169	142	· 0	116.7		2445	0	833
		76		•								
r Ť	1840.0	5.0	6.0	27	169	142	0	117.2		2442	0	836
	1845.0	5.0	6.1	. 27	169	142	0	117.1		2444	0	842
1	1850.0	5.0	6.1	27	169 170	142	0 N	116.8		2441	0	846
· .	1855.0 1860.0	$5.0 \\ 5.0$	6.1 6.2	27 26	169 169	142 143	0 0	117.1		2443 2442	0	849
	1870.0		6.2	26 26	169 169	143	0	117.3 117.5		2446 2450	0 0	853 861
<u>،</u>	1880.0	10.0	6.3	-28	169	143	0	117.3		2400 2451	0	869
1 4	1885.0	5.0	6.3	27	169	142	Ŭ	116.9		2452	0	876
	1890.0	5.0	6.4	26	169	143	0	117.3		2457	Ű	885
i.	1900.0	10.0	6.4	27	169	142	0	117.2		2464	Ü	895
	60	01						•				

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ESSD BARRACOUTA # 4

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	DEPTH 6	STEP 01	CHRS	MDB	HKLDX	HKLD	BMDA	SPM1	SPM2	PMPR	PCSG	HSP
	1905.0 1910.0 1915.0 1920.0	5.0 5.0 5.0 5.0		25 26 26 23	171 171 171 171	146 145 145 148	0 0	117.4 116.1 117.9	118.2 118.2	2498 2487 2477	0 0 0	871 875 878 883
	1925.0 1930.0 1935.0	5.0 5.0		22 25 26	171 169 171	149 146 144	0 0 0	118.0 120.2	120.6 121.2 121.2	2473 2501	0 0	888 899 907
e an e a an eag	1940.0 1945.0 1950.0	5.0	6.8	29 29 28	172 172 172	143 143 144	0, U 0	118.2	121.2 120.9 119.7	2455		912 917 920
	1955.0 1960.0 1965.0	5.0 5.0 5.0	6.9 7.0 7.0	29 27 27	172 172 172	143 145 145	•0 0 0	117.1 117.9	119.7 119.7 119.7	2444 2453	0 . 0	924 925 929
	1970.0 1975.0 1980.0 1985.0	5.0 5.0	7.0 7.1 7.1 7.1	30 28 29 31	172 172 172 172	142 144 143 141	0 0 0 0	118.8 119.0	119.7 119.7 117.4 116.9	2478 2471		929 935 937 941
	1990.0 1995.0 2000.0	5.0 5.0 5.0	7.2 7.2 7.3		172 169 167	143 143 143	0 0 0	118.8 113.4	116.9 113.9 109.5	2460 2359	8	949 953 953
	6' 2005.0 2010.0 2015.0	5.0 5.0	7.3 7.3 7.4	24 30 30	167 172 172	142 142 142	0 0 0	106.8	109.5 109.5 113.5	2259 2259 2331		958 961 965
	2020.0 2025.0 2030.0	5.0 5.0 5.0	7.4 7.5 7.5	28 31 27	172 172 167	144 141 141	0 0 0	120.1 119.9 121.9	119.5 119.5	2487 2489 2506	0	972 984 968 964
	2035.0 2040.0 2045.0 2050.0	5.0 5.0 5.0	7.5 7.6 7.6 7.7	27 32 32 33	169 172 172 172	141 140 140 139	0 0 0 0	120.9	119.5 120.9 121.9 121.9			965 969 971
	74 2055.0	5.0	7.7	35	172		-	119.5 128.6		2444 2522	0	984 982
	2060.0	5.0 5.0 5.0	7.8 7.8 7.9	31 32 32	172 172 172	$ 141 \\ 140 \\ 140 \\ 140 \\ 190 \\ $	0 0 0	128.8 128.5	121.9 122.2	2515 2514	0	987 992
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2075.0 2080.0 2080.0	5.0 5.0 .0	7.9 7.9 7.9	33 31 32		139 141 140 140	0 0 0 0	128.2 128.5 125.4 126.7	123.6 123.6	2516 2513 2515 2513	0 0 0 0	997 1003 1007 1020
	2095.0 2100.0 2105.0 78	$5.0 \\ 5.0$	8.0 8.1 8.2	32 31 30	172 172 172	140 141 142	0	123.7 122.7	123.6	2496 2489	0 0	1024 1026
	2110.0 2115.0 2120.0	5.0 5.0 5.0	8.2 8.3 8.4	31 32 32	173 173 172	142 141 140	0 0 0	123.0 123.8 124.2	123.9	2493 2491 2493	0 0 0	1029 1024 1030
	2125.0 2130.0 2135.0	5.0 5.0 5.0	8.5 8.5 8.6	31 33 33	171 173 175	$140\\140\\141$	0' 0 0	124.9 125.7 126.3	123.9 123.9	2495 2497 2502	0 0	1027 1028 1027
	2140.0 2145.0 2150.0	5.0 5.0 5.0	8.7 8.8 8.8	35 36 36		141 140 140	0	125.1 125.9 125.8	125.5 125.5		0 0 0	1028 1029 1031
	2155.0 83	5.0 34	8.9	35	176	141	0	127.7	160.0	2623	Ų	1036

ESSO BARPACOUTA # 4

PAGE

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	HSP 0 1040 0 1043 0 1047
2160.0 5.0 9.0 34 176 142 0 128.0 125.5 2622	0 1043
	0 1047 -
	0 1047
	$0 1047 \\ 0 1048$
	0 1041
	0 1043
	0 1045 0 1049
	0 1049 0 0 1052 0
882	
	0 1055
2215.0 5.0 9.9 32 177 144 [•] 0 124.6 123.6 2576 • 2220.0 5.0 10.0 38 177 139 0 125.8 120.4 2584 ••	0 1056 0 1058 -
	0 1061
	0 1064
	0 1069
	0 1074
	0 1077
	1079
930	
) 1084) 1087
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	1101 1103
$\begin{array}{cccccccccccccccccccccccccccccccccccc$) 1113) 1116
2325.0 5.0 10.9 42 178 136 0 120.3 116.4 2509 0	
2330.0 5.0 10.9 41 178 137 0 120.6 115.6 2513 0	
2335.0 5.0 11.0 42 178 136 0 120.5 115.6 2515 0 2340.0 5.0 11.0 34 171 137 0 118.2 115.6 2572 0	
$^{\circ}$ 2340.0 5.0 11.0 34 171 137 0 118.2 115.6 2572 0 2345.0 5.0 11.0 40 178 137 0 118.7 115.6 2574 0	
2350.0 5.0 11.1 39 178 139 0 119.0 115.6 2577 0	
2355.0 5.0 11.1 41 178 137 0 118.4 114.6 2575 0	
1023 2360.0 5.0 11.2 41 178 137 0 118.7 113.9 2573 0	1139
2370.0 5.0 11.3 39 177 150 0 117.5 113.9 2631 0	
2375.0 5.0 11.3 39 177 138 0 117.8 113.9 2645 0	
2385.0 5.0 11.4 41 177 136 0 117.6 116.7 2635 0 2390.0 5.0 11.4 40 177 137 0 117.7 116.7 2637 0	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
2405.0 5.0 11.5 39 177 138 0 119.1 116.7 2724 0	
1068	

ESSD BARPACOUTA # 4

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		STEP 068	CHRS	MOB	HKLDX	HKLD	BMDA	SPM1	SPM2	PMPR	PCSG	HSP	
			0 11.6	5 - 39	177	138	0	118.0	118.0	2718	0	1145	
	2410.	0 5.				139	0		118.8			1150	
						139	Ő		118.8			1155	
	2420.					137	0	•	118.8			1160	
r -	2425.								116.8	2721		1165	
(i	2430.					139	0						
λ, ¹ .	2435.					138	0		115.5			1164	•
	2440.					141	0		115.5			1159	
1	2445.	0 5.	0 11.9	9 40		138		112.8				1161	
[2450.	0 5.	0 12.0) 42	178	136	0		115.5			1166	
	2455.	0 5.	0 12.0) 40	178	138	0	113.0	115.5	2529	0	1171	
r . 1	1	118						•					
{	2460.	0 5.	0 12.1	41	178	137	Ó	113.8	116.5	2532	0	1176	
k	2465.					142	0	116.7	116.8	2606	Ũ	1180	
	2470.					137	0	119.3	116.8	2660	Ũ	1183	
	2475.					136	0		116.8	2660	0	1186	
	2480.					137	0		116.8	,2603	· 0 ·	1189	
Ý	2485.					137			118.6	2579		1192	
Γ.						136	Ů		119.8	2578	Û	1195	
						140		114.6		2549		1197	
ί.		0 5.								2478		1199	
	2500.								•				
	2505.		0 12.5	5 42	178	136	Û	114.8	119.8	2472	0	1202	
	1						. :				· _		
7 •	2510.			5 41		137	0		119.5	2471	Û	1204	
, L	2515.	0 - 5.		5 43	178	135	Û		119.1	2516		1206	
	2520.	0 5.	0 12.6	5 44	178	134	0	114.8	119.1	2575	Ū	1515	
	2530.	0 10.		42	177	135	0	115.2	119.1	26.05	0	1218	
2. 2. 1	2535.					138	0	116.9	119.1	2645	0	1219	
	2540.					134	. 0	116.8	117.7	2650	0	1220	
	2545.		0 12.8			135	0		115.6	2655	0	1224	
•	2550.		0 12.9			134			115.6	2659		1225	
·· ·	2555.		0 12.9	•		133	Õ		115.6		0	1228	
						134	ů		115.6	2656	0	1229	
e de la	2560.		0 13.0	. 44	111	104	· ·	110.0	11010		· ·		
2	1				4.77	104	0	114 0	118.9	9660	0	1232	
			0 13.0										
	2570.				177		0		119.7	2663	0	1233	
	2575.					132	0		119.7	2665	0	1234	•
·	2580.				177	133	0		119.7	5669	0	1235	٠.
	2585.				177	132	0	115.7		2623	0	1237	
ţ, j	2590.				177	134	0	115.6		2588	0	1239	÷
	2595.		0 - 13.3		177	-133	0	114.5		2598	0.	1241	
	2600.	0 5.	0 13.4	45	177	132	0	115.0		2599	0	1244	
	2605.	0 5.	0 13.4	45	177	132	0	114.8	113.8	2599	0	1247	
d.	2610.	0 5.	0 13.5	; 44	177	133	0	114.7	113.8	2600	0	1249	
		269				• •							4
	2615.		0 13.5	i 41	177	136	0	114.7	113.7	2603	0	1252	
3	2620.				177	134	0	115.7		2652	0	1255	
	2625.				177	135	0	116.0		2707	0	1256	
•					177	133	0	115.8		2640	ů 0	1259	
	2630.					134	0	115.9		2648	0	1261	
	2635.				177						0	1261	
• • •	2640.				177	136		115.8		2659			
•	2645.				177	134	0	115.7		2655	0	1268	
	2650.				177	140	0	115.5		2647	0	1270	
	2655.				177	154	0	115.8		2658	0	1274	
1	2660.		0 13.8	35	177	142	Ū	115.8	114.5	2652	0	1280	
		1309				•					•		

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ESSD BARRACOUTA # 4

PAGE 8 - C

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		STEP 1309	CHRS	WDB	HKL.DX	HKLD	выпл	SPM1	SPM2	PMPR	PCSG	HSP
i:	2665.		13.9	42	177	135	0	117.7	115.4	2668	0	1285
	2670.		13.9		177	136	0		114.2	2652	0	1289
	2680.		13.9	44	177	133	0	115.9	114.0	2661	0	1298
	2690.		13.9	41	177	138	0	117.1	115.2	2697	0	1292
	2700.	•	13.9	41	177	136	0	117.1	116.1	2711	0	1304
	2710.		13.9	44	177	133	0	117.0	116.0	2714	0	1313
	2720.	0 10.0	14.0	28	177	147	0	115.0	109.1	2658	0	1307
•	2730.	0 10.0	14.0	34	177	143	0		108.0			1316
[]	2740.	0 10.0	14.0	46	177	131	0 ·	114.9				1326
	.2750.		14.0	41	177	136	0	111.8	109.3	2580	0	1334
		1320					_				-	
	2760.		14.0	45	177	132	. 0		107.8	2542	0	1340
	2765.		14.0	46	177	131	•0		107.6			1338
ы а ,	2770.		14.1	45	177	132	Û		107.1	2530	0	1342.
r. 7	2775.		14.1	41	177	157	0.		110.3		· 0	1342
	2780.		14.1	39	177	138	0		112.7	2627	Ŭ	1347
	2790.		14.1	43	177	134	0		110.2		0	1356
	2800.		14.1	45	177	146	0		108.9	2617	0	1357
	2805.		14.2	45	177		0		108.1		0	1359
	2810.0		14.2	38	177	139	0		110.6		0	1356
	2820.		14.2	44	177	133	. O	114.6	112.0	2782	Ŭ	1358
	2830.	1340 0 10.0	14.2	34	177	158	0	11C C	113.7	2797	0	1365
	2840.1		14.2	34 45	177	132	0		113.7	2800	0	1360
	2850.1		14.2	40 33	177	13C 144	0		114.1	2664	0	1378
	2860.1		14.2	30 45	177	132	0		114.1	26649	0	1389
	2870.0		14.2	40	177	137	0		113.1	2650	0	1396
	2880.0		14.2	33	178	163	0	-110.6		2724	0	1393
	2890.0		14.3	44	178	134	0	113.3		2731	0	1405
	2895.0		14.3	48	178	130	0	110.8		2739	0	$1400 \\ 1410$
	2900.0		14.3	45	177	132	ů Ŭ		113.2	2750	0	1414
1	2910.0	and the second	14.3	37	177	161	ů Ú		112.5		ů ů	1407
		353	178.5		111	¥ '-' 1	•				•	* "I W I
	2920.0		14.3	33	177	144	0	111.0	113.2	2721	0	1417
	2925.(14.3	46	177	131	0	109.8		2722	0	1419
1	2930.0) 5.0	14.4	46	177	131	0	110.4	112.3	2728	0	1425
	2935.0) 5.0	14.4	45	177	133	0	111.4	113.7	2760	0	1423
	2940.0	5.0	14.4	47	177	130	0	113.4	116.2	2844	0	1423
]	2950.(10.0	14.4	21	177	156	0	116.5	116.6	2789	0	1431
ŀ.	2960.0	10.0	.0	5	146	140	0	128.1	125.2	2345	0	1324
	2965.(5.0	.0	4	146	142	0	126.3		2356	0	1326
1	2970.0		.1	5	144	142	Ū.	123.8		2321	0	1328
	2975.0		.1	5	145	140	0	121.9	125.1	5595	0	1331
÷.,		374									· •	
	2980.0		.2	2.	145	138	0	123.4		2293	. 0	1333
•	2985.0		. 2	· 5	145	140	0	122.2		2293	0	1335
	2990.0	•	.3	5	145	140	.0.	121.6		2298	0	1337
1.	2995.0		.3	5	138	138	0	105.3		2078	0	1339
•	3000.0		.4	4	144	140	0	126.4		2449	0	1342
•	3005.0		.4	4	144	140	0	128.0		2451	Ŭ	1344
· .	3010.0		.5	4	144	140	0	127.6		2450	0	1346
÷	2015.0		.6	3	144	141	0	128.2		2448	0.	1349
	(3020.0 2025 0		.7	3	144	141		128.5		2443	0	1351
, i 1	3025.0		.7	- 4	. 144	142	Û	127.4	131.4	2444	0	1354
	1.3	92									•	

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ES 1010

ESSO BAFRACOUTA : 4

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			•		•	•								
	DEPTH STE	P	CHRS	ЫПВ	HKLDX	HKLD	BMD	W	SPM1	SPM2	PMPR	PCSG	HSP	• •
	1392	•												
		5.0	.8	4	145	143		0	125.3	131.4	2433	0	1359	
		5.0	1.1	4	145	140		Ũ	123.7	123.6	2262	0	1361	
t i		5.0	1.2	3	145	142		0	124.2	121.2	2248	0	1360	
		5.0	1.3	З	145	142		0	124.8	120.9	2267	0	1366	
		5.0	1.4	4	145	141		0	124.6	121.1	2271	0	1370	
		5.0	1.8	5	145	140		Û	124.8	121.0	2269	0	1371	
		5.0	2.1	5	145	140		Ũ	124.4	120.4	5568	Û	1369	
		5.0	2.5	5	144	139		0	121.8	121.8	2251	0	1371	
*		5.0	2.6	3	144	141		0	119.4	124.2	2237	· 0	1376	
. [] ·		5.0	2.8	3	144	141		٥·	119.1	124.5	2242	0	1381	
	1433								•					
		5.0	3.0	4	144	140		0	119.7	124.4	2246	Ū	1386	
[]]		5.0	3.3	4	145	141		0	119.7	124.2	2238	0	1385	
		5.0	3.8	4	145	141	4	0	119.7	124.3	2239	Ū	1382	
L		5.0	4.0	4	145	141		0	119.0	123.1	2236	0	1386	
r		5.0	4.4	4	145	141		Ũ	120.2	120.2	2237	$\cdot 0$	1386	
		5.0	4.7	5	145	140		0	122.1	121.0	2243	0	1389	
		5.0	5.2	5	145	140		0	124.6	121.4	2266	. Ū.	1291	
		5.0	5.5	5	145	140		0	124.4	122.0	2270	0	1393	
; [].		5.0	5.7	5	145	140		0		121.7		0	1397	
		5.0	6.1	5	145	140		0	125.5		2269	0	1400	
	1483			-				_	· · ·	•				
		5.0	6.4	5	145	140		0	125.7	123.8	2295	0	1402	
		5.0	6.8	5	146	141		Û	125.7		2330	0	1404	
£ _		5.0	7.0	6	146	140		0	125.2		2358	0	1406	
r.		5.0	7.3	5	146	141		Ū	125.4		2313	0	1409	
antipe and		5.0	7.6	5	146	141		0	125.5		2310	Ō	1411	
		5.0	8.0	6	146	140		Ū	125.7		2317	. 0	1413	
•		5.0	8.2	7	147	139			124.0		2264	0	1415	
		5.0	8.4	7	148	140		0	120.1		2168	0	1418	
		5.0	8.6	8	148	139		Ō		118.2	2175	0	1420	
•		5.0	8.8	- 18	148	139		õ	120.8		2184	Ō	1422	
	1533		141 B (141		A 10-		•	•				-		
		5.0	9.0	8	148	·139		0	122.8	119.7	2192	Û	1425	
		5.0		8	148	140		Õ	120.3		2103	Ő	1430	·
	3190.0 5	5.0	9.4	8	•	140		Õ	116.1		1976	Ū.	1435	
	3195.0 5	5.0^	9.6	11	148	138		0	115.0		1965	0	1435	
LI		5.0	9.7	ġ	148	139		Ŭ.	121.3		2057		1437	
		1.0		7	148	141		0	122.0		2064	Õ	1438	•
\square		·		·										
··[]			•		NEW	BIT II	0:	4	4					
1. A.														
	3205.0	. 0	. 0	22	175	153		0	66.1	80.8	2599	0	1847	
•		5.0	. 1		175	153		0	69.1	80.5	2671	0	1853	
• •		5.0	.1	20	175	155		0	69.5	80.0	2690	0	1857	
f 1		5.0	.2	20	176	156		0	77.6	74.5	2678	0	1856	
	1576							-	• • • •			-	· · · · · ·	
		5.0	.3	19	176	157	. 1	Û	74.2	65.6	8279	Û	1862	
		5.0	.4	19	176	157	•	Ō	70.9		2184	0	1866	
		5.0	.4	23	180	157		õ	70.6	62.8	2190	0	1871	
		5.0	.5	55	177	155		Õ.		62.0	2179	0	1876	
•		5.0	.6	21	177	156		Ŭ	70.9	61.8	2178	Ũ	1882	
1		5.0	.6	20	177	157		Õ			2176	Õ	1887	
•		5.0	.7	22	177	155		Ŭ	69.4		1994	Ű	1892	
. ,	ngartanurnan Tanit Erfahi ina		• •		• • 1						1	·•·		-
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ESSD BARRACOUTA # 4

PAGE 10

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ł	DEPTH		CHRS	MOB	HKLDX	HKLD	BMDA	SPM1	SPM2	PMPR	PCS6	HSP	
'		605 0 5.0	.8	21	176	155	· 0	71.1	71.5	2456	Ũ	1889	
1	3260.			23	175	152	Ö	73.4	74.8	2567	0	1890	
	3265.			23	175	152	0	72.6	68.3	2395	0	1893	
	3270.				175	151	Õ	74.9	72.4	2631	0	1895	
	3275.				175	151	Ŭ	75.0	74.6	2686	0	1901	
1	3280.				175	151	0	75.1	74.0	2676	0	1906	
1	3285.					152	0	77.5	73.6	2730	0	1910	
	3290.						0	80.2	74.0	2802	0.		
•	3295.				-		0	80.1	73.4	2791	Ũ	1915	
1	3300.					146	-0	80.0	73.4	2775		1919	
	3305.		1.1	58	174	140	, v	0010					
1		1653		47	174	157	0.	79.2	72.8	2764	0	1923	
1	3310.						Ŭ	75.3	69.0	2512		1922	
•	3315.						0	72.3	62.9	2260			
	3320.						0	70.1	65.6	2322		1922	
	3325.	and the second			•		0	69.4		2375		1924	-
	3330.							69.5	68.8			1927	
	3335.						0	69.8		2384		1935	
ł	3340.						0				-	1945	
	3345.						0	69.3				1953	
.,	3350.						0	69.1			-	1960	
1	3355.		2.3	16	177		0	66.3	67.5	2010	Ų	1200	
		702					0	72.1	66.8	2424	0	1963	
i							0	72.6				1968	
	3365.						0	73.5	•			1973	
ł	.3370.							73.3				1977	
ļ	3375.						0	73.0		2389		1981	
	3380.						• 0					1980	
•	3385.						0	71.5				1980	
	3390.						0	74.6				1980	
, i	3395.						0	75.4				1983	
1	3400.	0 5.0					. 0	74.6				1984	
	3405.		3.3	19	178	159	0	74.5	67.4	2420	Ū	1204	
1		751		•				74 5	27 O	2436	0	1987	
	3410.						0	74.5				1991	
	. 3415.						Ũ	74.2				1997	
J							0	74.7				1999	·
	3425.						0	73.5				1998	
	3430.						0	71.6				2003	
1	3435.						0	71.5				2008	
	3440.					•	0	71.6				2013	
7	3445.	0 5.0					0	71.6				2008	
1	3450.	0 5.8	4.4				0	75.1				2008	
÷	3455.	0 5.0	4.6	15	181	166	0	75.2	68.6	2504	Ų	2010	
	· · · ·					•			25 0	0510	0	2015	
ł	0400.							71.2					
	3465.						0	71.2				2023	
•	3470.						Û,	71.3				2030	
•	3475.						0)	71.2					
	3480.						0	75.5				2031 2032	
	3485.						0	67.0					
	3490.	0 5.0) 5.4				0	69.7				2034	
	3495.	0 5.0) 5.6				0	69.3				2036	
	3500.) 5.9				0	70.1				2037	
	3505.) 6.4	14	180	167	0	70.7	65.9	2473	0	2040	
		842							•				
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ESSD BARRACOUTA # 4

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		STEP 1842	CHRS	MDB	HKLDX	HKLD	EMOA	SPM1	SPM2	PMPP	PCS6	HSP	÷
	2510. 2515. 2520. 2525.	$\begin{array}{cccc} 0 & 5.0 \\ 0 & 5.0 \\ 0 & 5.0 \\ 0 & 5.0 \\ 0 & 5.0 \end{array}$	6.6 6.6 6.6	5 7 3	$\frac{180}{180}$	170 175 173 177	0 0 0 0	69.9 70.9 73.7	72.1 68.4 58.3	2660 2550 2328	0	2043 2048 2054 2057	
	3530. 3535. 3540. 3545. 3550.	$\begin{array}{ccc} 0 & 5.0 \\ 0 & 5.0 \\ 0 & 5.0 \end{array}$	6.7 6.8 6.9	2 2 2	182 182	175 179 180 180 181	0 0 0 0 0	72.5 73.5 73.6 74.4 74.0	68.1 70.1 69.6	2644 2670 2669	0 0 0	2064 2067 2071 2075 2073	
	3555. 1	0 5.0 866	7.0	10	181	171	. 0	72.5	64.7	2484	0	2076	
	3560.) 3565.) 3570.) 3573.)	0 5.0 0 5.0	8.0 8.4		180 179 179 181	169 169 169 169	0 0 0 0	71.4 70.9 72.7 68.4	$64.2 \\ 60.1$	2312	.0	2082 2084	
- [-]-					NEW	BIT I	D: 5	5					
	3575.0 3580.0 3585.0 3590.0 3595.0 3600.0	$\begin{array}{cccc} 0 & 5.0 \\ 0 & 5.0 \\ 0 & 5.0 \\ 0 & 5.0 \\ 0 & 5.0 \\ 0 & 5.0 \end{array}$	1.2 1.4	16 18 28 29 26 20	190 190 192 192 192 189	174 173 164 162 166 169	0 0 0 0 0 0	66.8 68.0 77.6 77.9 77.8 76.6	72.6 73.9 76.8 76.1 76.1 80.1	2750	0 0	2082 2085 2093	
	3605.0 3610.0 3615.0 3620.0 3625.0 3630.0 3635.0 3640.0 3645.0 3650.0	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.3 3.4	25 17 18 32 32 37 46 45 45 47	189 189 189 189 189 192 196 196 196	164 172 171 156 157 154 150 151 151	0 0 0 0 0 0 0 0 0	.0 20.2 33.1 60.3	76.2 76.1 114.2 114.1 90.7 91.3	2927 2681 2402 1758 1606 1384 1741	0 0 0 0 0	2113 2115 2115 2118 2121 2124 2127 2132 2132	
	3655.0 3660.0 3665.0 3670.0 3675.0 3680.0 3685.0 3690.0 3695.0 3700.0	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3.8 3.9 4.1 4.3 4.5 4.5 5.0 5.1 5.2	46 45	196 196 198 198 198 198 198 198 199	149 149 150 151 152 152 153 153	0 0 0 0 0 0 0 0	69.9 50.7 26.2 .0 .0	72.3 79.6 113.2 112.8 113.1 113.2 81.2	1606 1537. 1653 1640 1623 1605 2308	0 0 0 0 0 0 0 0	2147 2149 2152 2155 2158	•
	2705.0 3710.0 3715.0 3720.0 3725.0 3730.0 3735.0	5.0 5.0 5.0 5.0 5.0 5.0	5.3 5.4 5.5 5.6 5.7 5.7	45 44 43 31 31 30	199 199 199 197 193 193 193	154 155 156 162 163 163	0 0	74.3 74.2 74.1 74.1 71.0 70.8 71.2	72.6 72.8 72.4 72.6 74.1 75.6 74.5	2700 2690 2685 2650	0 0 0 0 0	2179 2184 2189 2194 2196 2200 2204	

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ESSÓ BARRACOUTA # 4

PAGE 12 - 0

			ç.						1. A.		
	DEPTH STE	P CHR	S WDB	HKLIX	HKLD	BWOM	SPM1	SPM2	PMPR	PCS6	HSP
	3740.0 3745.0	5.0 5	.8 31 .9 31 .9 29	193	162 162 164	0 0 0	71.4 71.0 71.3	74.5 74.7 74.4	2682 2682 2679		2207 2213 2216
	3755.0	5.0 5	.9 24	193	170	0		74.6	2684		5550
			.0 22		171 177	0 0	68.9 69.6	75.9 77.2	2662 2717		2223 2225
1.1			$.0 16 \\ .0 13$		177 180	0	17.2	77.2	2714		2231
			.1 13		179	Õ	65.6	77.5	2713		
	3780.0 5	5.0 6	.2 18		175	0 `	69.2	76.9			5535
	3785.0 5 2069	5.0 6	.3 17	192	176	Û	68.8	77.1	2706	0	5535
-[]		5.0 6	.4 14	191	176	٩Ŭ	72.4	77.0	2801	0	2235
	3795.0 5	5.0 6	.4 12	191	179	0	70.6	72.3	2616	0	2237
			.6 12		179	0	70.8	72.0	2618	0	2240
			.7 20 .8 20		179 179	0 0	71.1 70.8	71.7 71.8	2628 2622	Ö O	2243 2247
- :		5.0 - 6			180	0	70.4	71.5			2251
			.9 19		179	Ũ	73.2	71.1		0	2251
			.0 20		179	Ū	73.6	72.1			2255
			.1 18		181	0 0	73.6	71.0	2707	0 0	2259
	3835.0 5 2118	5.0 7.	.2 16	199	183	U .	(3.0	. 11.4	2687	U	2261
		5.0 4.	.7 29		170	0	69.0	68.0	2383	0	2257
			.1 33		166	0	65.8	64.6	2273	0	2260
<u>_</u>			.2 37 .4 38		163 162	0 0	68.8 67.7	62.9 67.3	2316 2409	0	2264 2266
: المطر			.4 38 .7 40		160	0	68.5	65.6	2378	0	2269
- [7]			9 39		161		68.8	66.2	2395	Ö	2272
		5.0 9.		200	161	0	68.4	65.5	2358	0	2275
		5.0 9.	-		160	- 0	66.1	67.7		0	2278
[]		5.0 9. 5.0 9.	,5 39 ,6 31	198 190	161 159	0 0	58.3 59.8	64.2 64.1	2031 2068	0	2281 2285
	2164			120	102	Ū.	07.0	07.1	LUCO	U	
	3890.0 5		8 37		159	0 1			2055	0	5595
		5.0 10.		198	159	0	61.9	62.9 61.6	2037	0	2295
		5.0 10. 5.0 10.		198 198	159 159	0 0 -	61.1	61.6	1996 1991	0 0	2293
()		5.0 10.		198	160	Ũ	61.2	61.6	2001	0	2296
		5.0 11.		198	158	0	62.4	63.4	2141	0	2299
		5.0 11.		198	152	0	60.2 Fo F	61.7	1971	0	2302
		5.0 11. 5.0 11.		198 198	153 154	$0\\0$	59.5 59.3	63.3 63.7	2014 2010	0 0	2305 2308
		5.0 11.		198	154	0	59.4	63.4	2010	0	2311
s.•••	2214	,									
		6.0 12.		198	154	· 0	59.2	62.9	2002	0	2313
		5.0 12. 5.0 12.		197 198	153 153	0 0	59.7	63.2 63.4	2029 2040	0	2317 2322
		i.0 12.		198	154 154	0,	59.5	63.9	2060	0	2328
	3960.0 5	.0 12.	6 44	198	154	0	59.6	64.6	2086	Û	2333
••		.0 12.		198	154		60.8	62.1	2023	0	2338
		.0 13.		198 198	154 153	0	$61.4 \\ 61.3$	$61.0\\60.9$	2004 2010	0	2341 2343
		1.0 13.		198	$153 \\ 153$	0	58.7	66.5	2010	0	2343
· . ·		.0 13.		198	153	Ō	62.5	64.0	2103	Ũ	2349
	2261		. 1	-			-				

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ESSO BARRACOUTA # 4

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		STEP	CHRS	WDB	HKLDX	HKLD	выом	SPM1	SPM2	PMPR	PCSG	HSP
	3990.					153 152	0 0	62.2 60.3				2351 2352
.]	3995.					154	Ő	61.0				2355
	4000.					153	0	61.0				2360
	4005.					154	ò	40.1				2361
- 3	4010.					152	0	59.8		2150		
	4020.					151	0	61.1	63.3			2365
ن ہ۔ اب	4025.					151	0	62.6				2367
•	4030.					151	· 0	62.5				2370
	4035.				199	151	Q	63.0	60.7	2064	0	2373
المريحة		2307			1. J.	÷	•					0076
i.	4040.	0 5.0	15.6				0	63.0		2097		2376 2379
1	4045.	0 5.0					0	62.9	66.4			2382
	4050.					151	0	62.8	66.5		0	2385
с 	4055.						· 0 0	63.0 63.0	$66.1 \\ 66.1$			5388
1	4060.					151 151	0 0	62.7				2391
ç,	4065.						0	62.9		2234		2394
	4070.						0	64.3				2399
	4075.) 16.7) 16.7				Õ	64.6				2404
	4080.		16.7				Ō	64.2				2409
		2344	, TOTİ	·••·••								
	4090.) 16.7	33	199	166	0	65.0	62.3			2413
	4095.						0	65.4				
	4100.						0	67.6				2421
	4105.					171	0	60.9				2418
	4110.			29	200	171	0	.0				2418
•	4115.				200		0	26.4				
5 P	4120.) 17.7				0	55.5				2422
	4125.						0	61.1				2423 2426
	4130.						0	64.2 66.6				2433
1	4135.) 18.9	42	200	158	· Q	00.0	00.0		•	ha "T'a''a'
art gen	Ê			40	200	158	0	65.3	65.6	2417	0	2435
	4140.						0		66.3			
	4145.						0	65.0				
1	4150.						0	65.1				2445
	4155.						Û	65.2	65.0		•	2447
f.	4160.						0	64.9	65.3	2359	0	2449
							0	65.3		2400	0	2452
÷.							0	65.4	66.5			
-	4180.					159	0,	65.3				
	4185.				202	162	0	65.4	65.9	2411	0	2461
	2	2423		· ·			•. •					المناجر وروحو
	4190.						0	65.5		•		2464
				•			0	65.7				2467 2470
	4200.							< 66.3				
	4205.						0	67.2				2473
	4210.						0;					2481
	4215.						0	67.9				2482
1. 	- 1 L. L. V	•					0	68.5				
	4225.						0	69.3				
	4230.						Ő					
	400C.		مە ئە اسە بىلى - ئى سەر بىلە سەر سەر سەر سەر سەر									
					NEW	BIT I	D:	6				

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61:		•									•	
	DEPTH	STEP	CHRS	WOB	HKLDX	HKLD	BWOV	SPM1	SPM2	PMPR	PCS6	HSP
		474									· .	
E.T.	4235.		. 1	20	188	171	0	66.8	65.8	1645	Û	2485
	4240.		.3	25	195	164	0	65.6	66.3	1776	0	2488
ы	4245.	0 . 5.0	.1	8	179	171	0		76.9	1420	0	2471
r i	4250.		.3	11	179	168	0	.0	114.0	1941	0	2475
		0 5.0	.6		179	161	0	.0	112.9	1959	0	2480
ί. Ι	4260.		.7		179	158	0		112.7		Û	2484
	4265.	0 5.0	.8	50	179	159	0	. 0	113.5	1949	· 0	2488
	4270.	0 5.0	.9	. 19	179	160	0		113.0		Ū	2491
L.	4275.	0 5.0	1.0	18	177	159	0	. 0	109.9			
	4280.	0 5.0	1.2	30	182	152	0	.0	98.3	2512	0	2499
		2506					•					•
	4285.	0 5.0	1.3		183	151	` 0			2860	0	2499
	4290.		1.4		183	150	0	.0		2860		2493
5.1	4295.	0 5.0	1.5	33	183	150	. 0	.0				
	4300.	0 5.0	1.5	33	184	151	0	.0		2876		
L 3	4305.	0 5.0	1.6	35.	184	149	0	.0	95.5	2879		2419
1.1	4310.1	0 5.0	1.7	36	184	148	0	.0	91.5			
	4315.	0 5.0	1.8	36	184	148	0	.0	91.2	2832	0	
i.i	4320.0	0 5.0	1.8	35.	184	149	0	.0				
	4325.1	0 5.0	1.8	36	184		Û	.0				
	4330.0	0 5.0	1.8	34	184	150	0	. 0	90.5	2807	0	2433
L		2542		• . •								
	4335.0		1.9		184	148	0	.0	93.6			2436
F)	4340.1		1.9	36	184	148	0	.0	93.3		0	2441
	4345.0		1.9	36	· 184	148	0	.0	94.1	2977	0	2445
**	4350.0		1.9	33	184	151	0	. 0	93.4		· 0	2449
ri	4355.0		1.9	35	184	149	0	.0			0	2457
	4360.0		2.0	25	184	159	0	. 0				2452
E.,]	4365.0			14	184	170	0	.0			0	2454
	4370.0		2.1	18	184	166	0	.0			0	2453
	4375.0		2.2	12		172	0	.0			0	2458
	4380.0		5.3	18 _	184	166	Û	.0	91.0	2836	0	2456
		2568						•			·	
1	4385.0		2.3	17	184		0		91.0		0	
	4390.0		2.4	.27	183	157	0	.0	90.9	2815	0	2456
• j.	4395.(2.5	26	184	158	0	. 0	90.9	2820	0	2456
eher.	4400.0		2.5	24	184	160	Û	.0	90.9	2827	0	2460
	4405.0		2.5	14	184	170	0	.0	90.9	2817	0	2466
	4410.(2.6	11	184	173	0	.0	90.6	2817	0	2468
~	4415.0		2.7	12	184		0	.0	90.5	2807	0	2471
	4420.(2.8	8	184	176	0	. 0	91.0	2822	0	2473
	4425.(2.9	. 9	184	175	0	.0	90.5	2805	0	2473
	4430.0		3.0	13	184	170	0	.0	90.5	2797	Ū	2476
1 · ·		510	~ .		404	1 × 1	•	• •	<u>.</u>	0700	0	-
•	4435.0		3.1	21	184	164	. 0	.0	90.8	2793 ° 9795	Û	2480
	4440.0		3.2	21	185	164	6	.0	90.5	2785 2727	0	2482
	4445.(3.2	21	185	164	0	.0	90.7	2797 9900	0	2484
	4450.0		3.2	15	185 185	170	0 0	.0	91.0 90.4	2800 2785	0 0	2488 2500
•	4455.0		3.3	9		176		.0		2785	U 0	
	4460.0		3.4	15 22	185 185	170	0 0	.0 .0	90.1 90.7	2765 2765	U 0	2507
	4465.0		3.5			163	0	.0	90.7 90.3	2758	0	2511
	4470.0		3.6	22 22	185	163 142	0	.0	90.3 90.5	2760		2515
	4475.0		3.7	53 55	185 185	163 162	0	.0 .0	90.5 90.5	2760 2769	0 0	2520 2525
	4480.0) 5.0 52	3.8	63	TOG	100	. 0	• 0	20.0	6102	U	にしてい
	<u>c</u> 0	- JE						•				

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* ESSD BARRACOUTA # 4

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		1			•							
		STEP 2652	CHRS	MDB	HKLDX	HKLD	в₩ОА	SPM1	SPM2	PMPR	PCSG	HSP
	4485.		3.8	21	185	164	0	.0	<i>`</i> 89.8	2760	0	
1	4490.			24	185	161	. 0	.0	89.9	2751	0	2527
	4495.			31	185	154	0	.0	89.4	2724	0	2523
K	4490.			32	185	153	Ú.	. 0	89.5	2722	0	2526
F 1		0 5.0		32	185	153	0	.0		2724	0	2527
	4510.			33	185	152	0	. 0	91.1	2722	0	2531
L.	4510.			33	178	151	0	.0	90.4	2764	0	2539
				34	185	151	0		91.7	2834	0	2549
	4520.			32	185	153	- Õ	`.0	92.0	2851	0	2555
	4525.			31	185	154	Ŭ Ö	.0		2850	- 0	2559
	4530.		ل دا لي: ر	1	100	401	1990 -					
r i	4535.	2697 0 5.0	5.1	30	185	155	•0	. 0	91.9	2847	0	2564
				28	185	157		.0	91.9	2846	0	2567
	4540. 4545.				185	157	Ő	.0	92.0	2852	0	
r i	4540.			20	185	165	Ũ	.0	92.6		0	
- in	4555.			17	185	168	Ő	. 0		2887	0	
L	4560.			23	185	162	0	.0	93.1	2884	0	2563
	4565.			22	185	163	0	.0		2879	0	2564
	4570.				185	168	Ō	.0		2885	Û.	2567
	4575.				185	175	0	.0	93.5		0	2575
	4580.				184	172	0	. 0		637	0	2530
F 1	- ·	2736	• •	. .	101							
	4585.		.4	13	184	172	0	.0	51.0	986	0	2547
1	4590.			14	184	172	0	22.4			. 0	2537
ri	4595.			13	184	172	0	56.8		910	0	2549
	4600.			13	184		0	55.2		835	0	2538
ي. آ	4605.			14	184	171	0	22.0			0	2554
r-i	4610.			18	184	166	0	.0	51.6	1037	0	2557
ţ,	4615.			19	184	165	· 0	.0	51.8	1002	0	2563
L.	4620.			24	188	164	0	.0	52.7	976	0	2563
ł	4625.		•		189	165	0	.0	51.5	984	0	2567
	4630.			22	189	167	0	.0	57.1	1064	0	2568
	2		9 2					•				
1	4635.			25	189	167	0	. 0		1145	0	2578
	4640.			19	189	170	0	. 0	56.5	947	0	2591
	4645.			18	189	171	0	.0	31.3		0	
	4650.			17	189	172	Û	31.1				2611
Π	4655.	0 5.0	6.2	17	189	172	0	35.3			0	
	4660.		6.3	16	189	173	0	35.9			0	2617
	4665.		6.8	18	189	171	Û	40.6				2594
c,	4670.	0 5.0	7.8	17	186	169	0	46.1				
1.15	4675.	0 5.0	8.3	. 9		173	. 0	41.2				2603
L	4680.		8.7	- 10	182	172	• 0	42.4	.0	681	0	2611
		2836	·				·	• • •	-	س ہو ہو		
	4685.	•				174	0	42.4			0	
ļ	4690.					174	0	25.9				
3	4695.					175	0	23.1				
ŀ		0 5.0		6			0	24.0			0	
	4703.	0 3.0	9.2	6	182	176	0	23.9	.0	000 		
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												· · · · · · · · · · · · · · · · · · ·
	4705.							76.2				
	4710.	0 5.0	. 1	14	186	172	0	74.7	.Ů	1854	0	2596
		•			•					•		· · ·
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14	1917 - 1917 - 1917 - 1917 - 1917 - 1917 - 1917 - 1917 - 1917 - 1917 - 1917 - 1917 - 1917 - 1917 - 1917 - 1917 -												
	DEPTH	STEP	CHRS	MDB	HKLDX	HKLD	BMOA	SPM1	SPM2	PMPR	PCS6	HSP	
1		2865											
	4715.		. 1	16	186	170	0	75.7	.0	1856	0	2600	
	4720.	· · · · ·	.1	14	186	172	0	75.7	.0	1847	0	2604	
and the second second	4725.		.2	13	186	172	Ū	79.7	.0	2055	0	2606	
			.2	15	186	171	Ŏ	81.0	.0	2086	0	2611	
	4730.				186	173	0	80.9	.0	2103	0	2615	
	4735.		.3	13						2146	, n	2619	
	4740.	0 5.0	.4	15	186	171	0	82.3	.0				
	4745.	0 - 5.0	.5	15	186	171	• 0	82.8	.0	2160	0	2624	
	4750.	0 5.0	.5	15	186	171	0	82.4	.0	2154	0	2641	
	4755.		.7	. 14	186	172	0	81.5	.0	2254	0	2677	
1	4760.		.9	15	186	171	0	81.5	.0	2128	0	2632	
		2900						•					
-	4765.		.9	16	186	170	•0	82.0	.0	2139	0	2640	
1	4770.		1.0	16	186	17.0	0	82.0	. Ū	2130	0	2638	÷
1	4775.	-	1.0	16	186	170	Û	81.5	.0	2119	0	2647	
				16		170	Ū	81.2	.0	2120	0	2651	
2	4780.	· · · ·	1.1				0		.0	2128	0	2649	
: ور	4783.	0 3.0	1.1	16	186	170	, U	81.4	. 0	. 6160	v		

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This is an enclosure indicator page. The enclosure PE602714 is enclosed within the container PE903923 at this location in this document.

The enclosure PE602714 has the following characteristics: $ITEM_BARCODE = PE602714$ CONTAINER_BARCODE = PE903923 NAME = Barracouta 4 Geo-Plot log BASIN = GIPPSLAND PERMIT = VIC/L2 TYPE = WELLSUBTYPE = WELL_LOG DESCRIPTION = Barracouta 4 Geo-Plot log (from enclosure 6, WCR) REMARKS = $DATE_CREATED = 22/04/77$ DATE_RECEIVED = $W_NO = W688$ WELL_NAME = Barracouta-4 CONTRACTOR = Core Laboratories International Ltd CLIENT_OP_CO = Esso Exploration Australia Inc (Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE602715 is enclosed within the container PE903923 at this location in this document. Ì.

The enclosure PE602715 has the following characteristics: $ITEM_BARCODE = PE602715$ CONTAINER_BARCODE = PE903923 NAME = Barracouta 4 Drill Log .1 BASIN = GIPPSLAND PERMIT = VIC/L2TYPE = WELL SUBTYPE = WELL_LOG DESCRIPTION = Barracouta 4 Drill log (from enclosure 6, WCR) REMARKS = DATE_CREATED = 22/04/77DATE_RECEIVED = $W_NO = W688$ WELL_NAME = Barracouta-4CONTRACTOR = Core Laboratories International Ltd CLIENT_OP_CO = Esso Exploration Australia Inc (Inserted by DNRE - Vic Govt Mines Dept)

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This is an enclosure indicator page. The enclosure PE602716 is enclosed within the container PE903923 at this location in this document.

	2716 has the following characteristics:
$ITEM_BARCODE =$	
CONTAINER_BARCODE =	
NAME =	Barracouta 4 Pressure Log
BASIN =	GIPPSLAND
PERMIT =	VIC/L2
TYPE =	WELL
SUBTYPE =	WELL_LOG
DESCRIPTION =	Barracouta 4 Pressure Log (from
	enclosure 6, WCR)
REMARKS =	
$DATE_CREATED =$	22/04/77
$DATE_RECEIVED =$	
W_NO =	W688
WELL_NAME =	Barracouta-4
CONTRACTOR =	Core Laboratories International Ltd
CLIENT_OP_CO =	Esso Exploration Australia Inc
(Inserted by DNRE -	Vic Govt Mines Dept)
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This is an enclosure indicator page. The enclosure PE602717 is enclosed within the container PE903923 at this location in this document.

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The enclosure PE602717 has the following characteristics: ITEM_BARCODE = PE602717 CONTAINER_BARCODE = PE903923 NAME = Barracouta 4 Geo Plot 2 BASIN = GIPPSLAND PERMIT = VIC/L2 TYPE = WELLSUBTYPE = WELL_LOG DESCRIPTION = Barracouta 4 Geo Plot 2 (from enclosure 6, WCR) REMARKS = $DATE_CREATED = 22/04/77$ DATE_RECEIVED = $W_NO = W688$ WELL_NAME = Barracouta-4 CONTRACTOR = Core Laboratories International Ltd CLIENT_OP_CO = Esso Exploration Australia Inc

(Inserted by DNRE - Vic Govt Mines Dept)

This is an enclosure indicator page. The enclosure PE602718 is enclosed within the container PE903923 at this location in this document.

The enclosure PE602718 has the following characteristics: ITEM_BARCODE = PE602718 CONTAINER_BARCODE = PE903923 NAME = Barracouta 4 Temperature 1 BASIN = GIPPSLAND PERMIT = VIC/L2TYPE = WELL SUBTYPE = WELL_LOG DESCRIPTION = Barracouta 4 Temperature log (from enclosure 6, WCR) REMARKS = DATE_CREATED = 22/04/77DATE_RECEIVED = $W_NO = W688$ $WELL_NAME = Barracouta-4$ CONTRACTOR = Core Laboratories International Ltd CLIENT_OP_CO = Esso Exploration Australia Inc (Inserted by DNRE - Vic Govt Mines Dept) \mathbf{G}

This is an enclosure indicator page. The enclosure PE602719 is enclosed within the container PE903923 at this location in this document.

The enclosure PE602719 has the following characteristics: ITEM_BARCODE = PE602719 CONTAINER_BARCODE = PE903923 NAME = Barracouta 4 Grapholog (Mud Log) BASIN = GIPPSLAND PERMIT = VIC/L2 TYPE = WELL SUBTYPE = MUD_LOG DESCRIPTION = Barracouta 4 Grapholog (from enclosure 6, WCR) REMARKS = DATE_CREATED = 22/04/77DATE_RECEIVED = $W_NO = W688$ WELL_NAME = Barracouta-4 CONTRACTOR = Core Laboratories International Ltd CLIENT_OP_CO = Esso Exploration Australia Inc (Inserted by DNRE - Vic Govt Mines Dept)