Geoservices Pioneering Technology Worldwide	**FINAL WELL REPORT** BASKER-7	ROC

Flair

Fluid Logging & Analysis In Real time

ROC OIL AUSTRALIA LTD

BASKER-7

BASKER / VIC/L26
Offshore Melbourne, Australia
JULY-AUGUST 2009

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ABSTRACT

General Information:

- Well Spudded on: 22nd July 2009
- FLAIR Logging Interval: 3190 to 3921 m
- FLAIR Logging dates: 2nd August 2009 – 6th August 2009

The FLAIR logging of the well Basker 7 permitted gas observations to be made in quasi real time. The principle aim of this study is to present the available FLEX/FLAIR gas data and to analyze various fluids encountered throughout the well, in order to delineate fluid characteristics in various formations encountered while drilling through the reservoir.

The interpretation of the gas data has led to the identification of THREE (3) main fluids.

The data used is corrected from recycling effect and Extraction Efficiency calibration for C1-C5 components:

Fluids are labeled as per Basker-6ST1 well. Comparable formation fluids with similar signature recorded in Basker-7 are labeled same as per fluids encountered in Basker-6ST1 well.

Fluids 1A, 1B, 8, 9B & 9C of Basker-7 are comparable to the fluids 1A, 1B, 8, 9B & 9C encountered in Basker-6ST1 well. Fluids 9A in Basker 6ST1 and 9E in Basker-7 are compositionally different and thus labeled differently.

FLUID 1A: is composed of 61% of C1 in the C1-C5 range. It comprises all the components in the analysed range with relatively very high presence of C6+ especially C7H14, even though the general gas level is very low. The lithology consists of argillaceous sand. *There are no indications of HC bearing zone based on LWD data, however, FLAIR indicates presence of heavy HC composition.*

FLUID 1B: is composed of 73-75% of C1 in the C1-C5 range. It comprises all the components in the C1-C5 range. The gas level is very low. The lithology consists of argillaceous siltstone in the interval 2-4 and clean sand in the interval 9.

Fluid 1A & 1B were recorded in Basker 6ST1 well

FLUID 8: is composed of 80-83% of C1 in the C1-C5 range. It comprises all the components in the C1-C4 range with minor presence of C5s. C6+ components are not present. The gas level is relatively higher compared to the upper intervals. It was recorded in argillaceous siltstone.

Fluid 8 was recorded in Basker 6ST1 well

FLUID#	PEAK#	Measured Depth From (m)	To (m)
1A'	1	3324	3328.2
1B	2	3328.6	3334.6
	3	3355.5	3361.9
	4	3383.8	3386.5
8	5	3465	3469.7
	6	3471.8	3490
	7	3501	3509
	8	3514	3518
1B	9	3545.5	3549

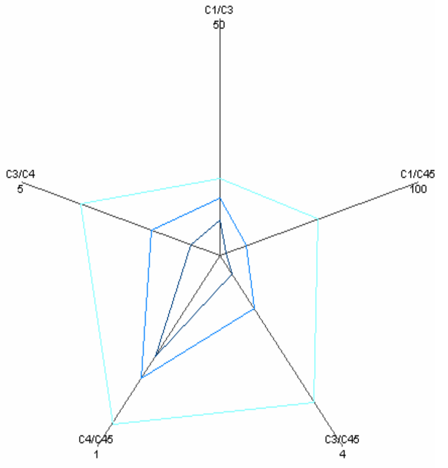


Fig.1: Star diagram for Fluids 1A, 1B and 8.

FLUID 9B: is composed of 80-82% of C1 in the C1-C5 range. It comprises all the components in the C1-C5 range with relatively high presence of C6+. The gas level is moderate to high.

FLUID 9C: is composed of 84-85% of C1 in the C1-C5 range. It comprises all the components in the analysed range (C1-C8, Benzene, Toluene and Methylcyclohexane). The gas level is relatively high. It was found in clean sands, intervals 10-12 and 15. Possible HWC can be placed around 3586m MD.

FLUID 9E: is composed of 87-90% of C1 in the C1-C5 range. It comprises all the components in the C1-C5 range with traces or minor amounts of C6+. The gas level is relatively high. It was recorded in clean sands.

Fluid 9B & 9C were recorded in Basker 6ST1 well

FLUID#	PEAK#	Measured Depth From (m)	To (m)
9C	10	3556.9	3567.5
	11	3574.1	3580
	12	3581.3	3588.2
9E	13	3616.2	3622.4
9B	14	3626.2	3630.3
9C	15	3638.1	3650.8
9B	16	3652.7	3658.6
9C	17	3663.6	3675.5
	18	3677.7	3679.9
	19	3684	3687.8
9E	20	3691.3	3694.8
9C	21	3700.2	3707.5
9B	22	3712.6	3724.6
	23	3731	3737
	24	3754.5	3762
9C	25	3774.1	3780
	26	3787.6	3789.7
	27	3796.8	3810.7
9B	28	3816.5	3826.5
9C	29	3834.5	3839.9
9B	30	3850.5	3854.7
	31	3858	3862
	32	3865.5	3869.5
9E	33	3891.5	3895.5

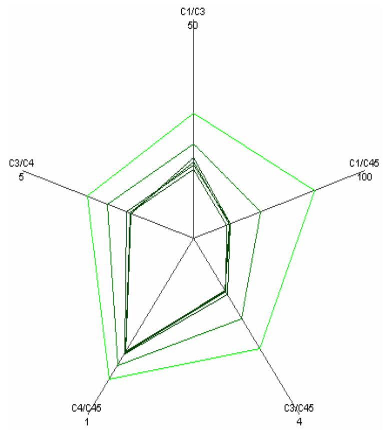


Fig.2: Star diagram for Fluid 9.

COMPARISON OF BASKER-7 FLAIR COMPOSITION WITH BASKER-2 PVT

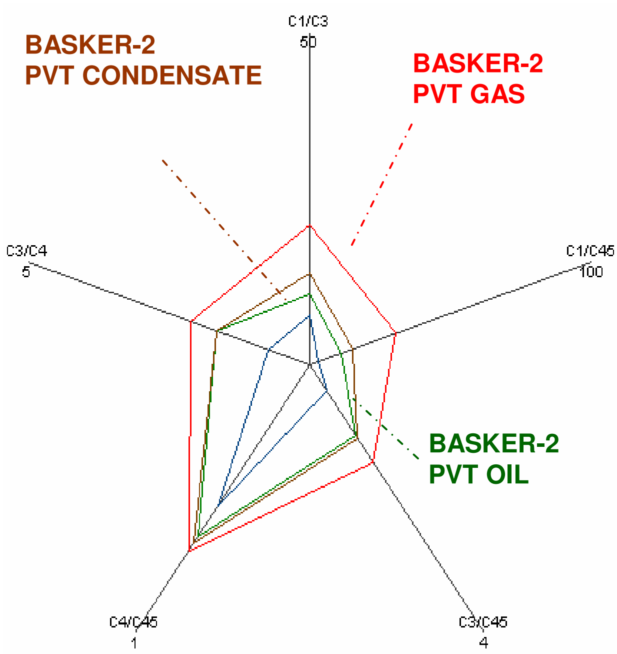


Fig.3: Star diagram for Fluids 1A, & Basker-2 PVT samples.
FLUID 1A' in Basker 7 exhibits anomalously heavy signature as compared to Basker 2 PVT OIL

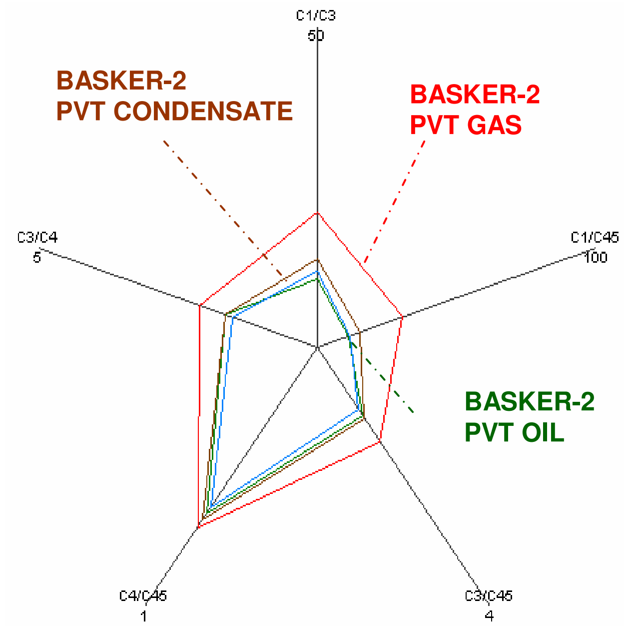


Fig.4: Star diagram for Fluids 1B, & Basker-2 PVT samples.

FLUID 1B in Basker 7 exhibits same signature as Basker 2 PVT OIL

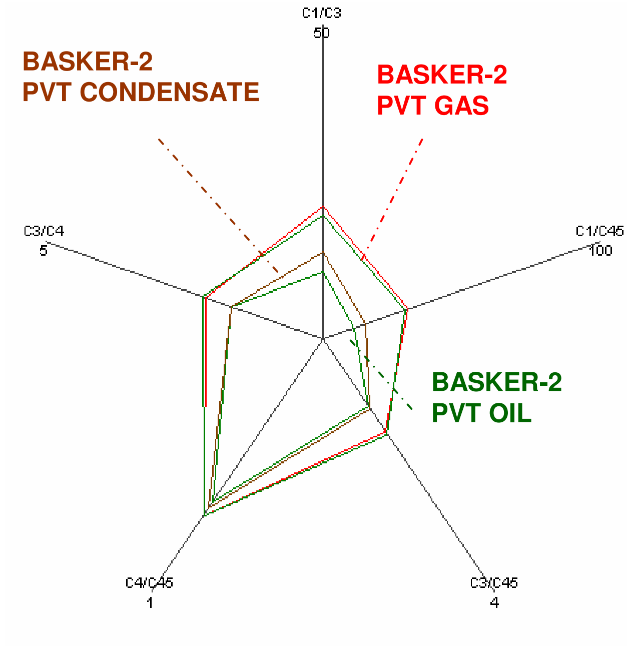


Fig.5: Star diagram for Fluids 9C, & Basker-2 PVT samples.

FLUID 9C in Basker 7 exhibits same signature as Basker 2 PVT GAS

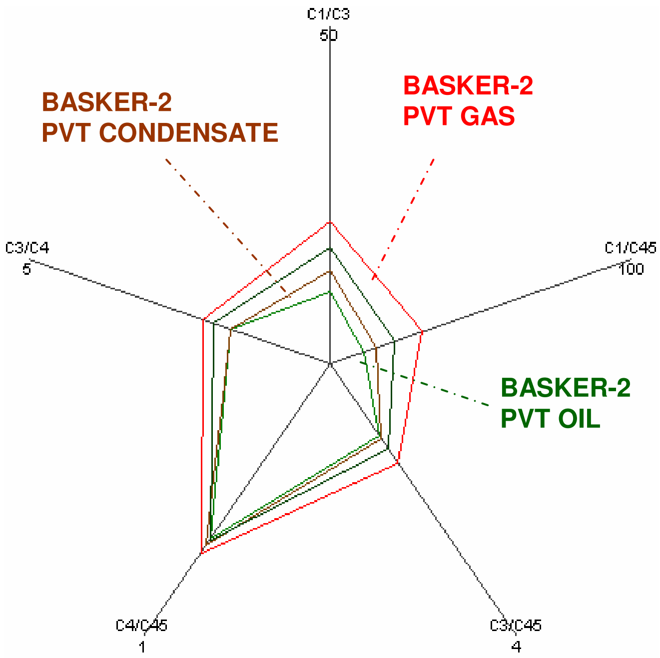


Fig.6: Star diagram for Fluids 9B, & Basker-2 PVT samples.

FLUID 9B in Basker 7 exhibits signature intermediate to Basker-2 PVT GAS and PVT OIL

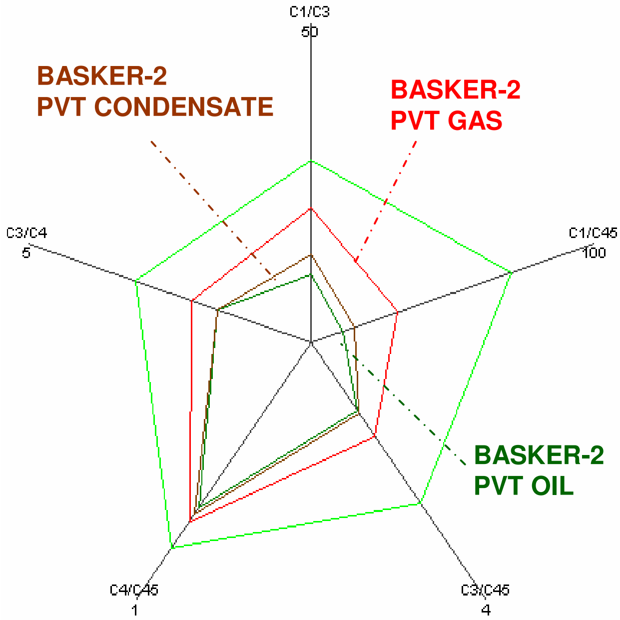


Fig.7: Star diagram for Fluids 9E, & Basker-2 PVT samples.

FLUID 9E in Basker 7 exhibits significantly light signature as compared to Basker 2 PVT GAS

OBJECTIVES

The principle aim of this study is to present the available information from FLAIR gas data to evaluate the potential for hydrocarbons in encountered reservoirs, determine fluid compositional changes and any barriers present.

The Flair service was employed to provide information on the following issues:

- Fluids recognition and characterization of hydrocarbons in the primary objective Zone 2 in the south-eastern area of Basker Oil Field.
- Fluids recognition and characterization of hydrocarbons in the secondary objectives. The secondary objective of Basker-7 is to further appraise all major reservoirs (zones 0, and 6) in the south-eastern area of the Basker oil field.
- Recognition of eventual fluid variation and/or fluid contacts to better locate eventual pay zones within the investigated intervals (Zones 0-7).
- Fluids recognition and characterization of hydrocarbons in the additional reservoirs if intersected, above, within and possibly below the known reservoir interval.

This report contains the relevant logs and observations gathered over the time of the FLAIR job. The second part is dedicated to the maintenance and calibration of the equipment ensuring FLAIR data validity.

INTRODUCTION

The present study is an analysis of the gas data acquired using the new FLAIR system from the BASKER-7 well. The following components have been monitored:

FAMILY	HYDROCARBON		MASS	CHANNEL MS
n-Alkanes	Methane	C1	Mass 15	Ion 1
	Ethane	C2	Mass 26	Ion 2
	Propane	C3	Mass 43	Ion 3
	i-Butane	iC4	Mass 43	
	n-Butane	nC4	Mass 43	
	i-Pentane	iC5	Mass 43	
	n-Pentane	nC5	Mass 43	
	n-Hexane	nC6	Mass 43	
	n-Heptane	nC7	Mass 43	
	n-Octane	nC8	Mass 43	
Aromatics	Benzene	C_6H_6	Mass 78	Ion 4
	Toluene	C_7H_8	Mass 91	Ion 6
Cyclo-Alkanes	Methylcyclohexane	C_7H_{14}	Mass 83	Ion 5

Table.1: Ions detected by the GCMS

The identification and measurement of the hydrocarbon species listed above is achieved using a Gas Chromatograph Mass Spectrometer (GCMS). The GCMS was configured for *6* ions (as outlined in the table), with a cycle analysis time of 90 seconds.

The gas was extracted using a FLEX (fluid extractor), placed in the possum belly of the shale shaker to monitor gas coming out (Gas OUT) from the well. A second extractor was located in the suction pit to monitor gas going back in the well (Gas IN) in order to determine the level of gas recycling.

The FLEX extractor heats the mud to a constant temperature in order to extract the heavier components from C6 to C8, as well as some other particular species (C_6H_6, C_7H_8 and C_7H_{14}) and helps improving the extraction efficiency of all the monitored components. This is further improved with constant volume of extraction and constant pressure maintained in the gas line.

The principle aim of this study is to present the available information from FLAIR gas data for reservoir and formation evaluation purposes.

FLEX Location

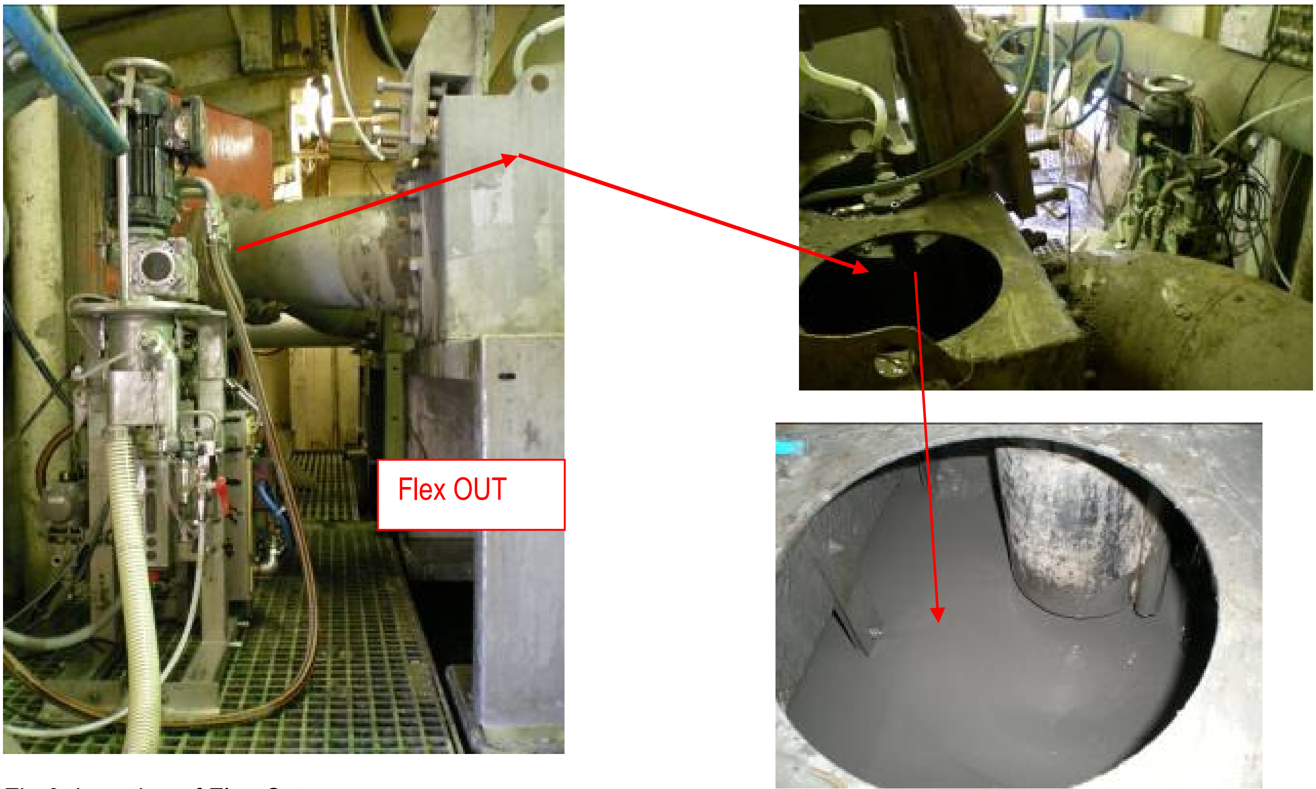


Fig.8: Location of Flex Out.

Fig.9: Location of Flex In.

Flex Out Probe was installed in the Header box of the shaker. The red arrow indicates the position of probe.

Flex In Probe was installed in the Active pit in the pit room. The arrow indicates the position for the probe.

REVIEW OF FLAIR CALIBRATION PROCEDURES AND DATA

The calibration of the FLAIR system is achieved by performing six procedures: 1. Calibration Check; 2. Gas Integrity Test; 3. Leak Detection Test; 4. Mud Background Check and 5. Extraction Efficiency Calibration. Descriptions of these procedures are given below.

1. Calibration Checks

Full calibration checks are performed prior to 8 ½" section logged using FLAIR, to ascertain the stability of the GCMS (reference: calibration reports in annex).

2. Gas Integrity Test

This test is performed prior to drilling each phase, with an aim to check the integration process between the FLEX extractor and FLAIR analyzer over a wide range of concentrations. A jerry can is connected before the flow restrictor in the filtration assembly of the FLEX. This jerry can has a dilution port to displace the gas with air and to maintain a constant pressure during the test. It is ensured that the jerry can is uncontaminated by checking that the MS records almost 0 ppm of gas. A bottle of 10 % C1 mixture is connected to the jerry can entry and fully opened for five seconds. The response on the MS is recorded for linearity and good integration for each component until very low values are reached.

In this well gas Integrity test was performed prior to drilling the 8 ½" phase and is reported in the annex.

3. Leak Detection Test

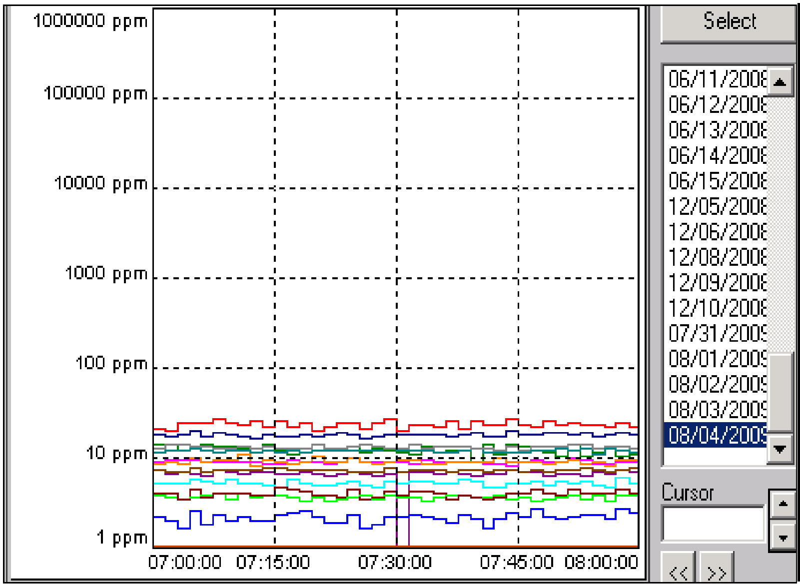
Prior each section an LDT is performed to ascertain the integrity of the Flex filtration assembly, gas line and GC used on the FLAIR system. The test is performed to ensure that the system is «leak proof» and the gas data acquired are not affected by a possible leak due to a damaged or faulty part for each FLEX used on FLAIR system LDT performed in this well are reported in the annex.

4. Contribution of WBM in Gas Readings

The mud background test was performed during a trip at 3537m to change Anadrill tools to ascertain the contribution from WBM and to define an average signature.

The mud (a Water based mud KCl/KlaStop/Polymer type with MW= 1.14 sg) was taken from the suction pit during the bit trip.

The test was carried out using FLEX IN, heating the mud as per standard drilling conditions (70° C) until stable readings were achieved.



Gas IN	Average Value
C1	24.13
C2	12.64
C3	18.32
iC4	6.74
nC4	12.12
iC5	9.24
nC5	7.56
nC6	5.32
nC7	4.15
nC8	2.13
C6H6	3.86
C7H8	13.46
C7H14	9.32

Fig. 10: Real time display of FLEX IN analysis of Water based mud.

The table above shows average values of contamination in the mud.

The maximum contribution of around 24.13 ppm & 18.32 ppm was of C1 & C3 gas components respectively, the contribution level of C2, nC4, & C7H8 were in the range of 12-13 ppm. iC4, nC5 & nC6 were around 6-7 ppm while iC5 & C7H14 were around 10 ppm. The contribution from nC7, nC8 and C6H6 was around 3-4 ppm.

5. Extraction Efficiency Calibration

When drilling with an Oil Based Mud or Synthetic Based Mud, the efficiency of the extraction process is not equal to 1. This means that the sampled mud is not fully degassed. Moreover, all the components are not extracted in the same manner. Many factors influence the extraction process, among them: hydrocarbon and mud chemistry, mud temperature, viscosity and shale content.

The aim of this procedure is to establish the extraction efficiency of the equipment and to correct the gas readings. This allows the operator to finally obtain the real composition of the gas in the mud.

When the same mud is introduced several times into the extractor, it has been observed that the gas readings decrease exponentially in first approximation. The decreasing concentration is not the same for the different components.

Extraction efficiency is reduced with increasing molecular weight of the gas components, for example methane will be extracted more efficiently (closer to 1) than butane. It has also been observed that for one molecule, the characteristics of the exponential decrease do not depend on the initial quantity or composition of the gas in the mud.

The sum of the gas quantities after an infinite number of passes represent all the gas that can be extracted from the mud in the present thermo dynamical conditions at specific P&T conditions. Hence, for a given mud, knowing the characteristics of the exponentials for each molecule, it is possible to compute the gas value corresponding to an infinite number of passes from the result of the first pass.

When degassing the mud at 70°C, the thermo dynamical conditions are favorable enough to extract the C1-C5 range hydrocarbons after an infinite number of passes in the degasser. That's why, after establishing the exponentials characteristics, it is possible to give the real composition (C1-C5) of the gas in mud, from the gas values corresponding to the first pass of the mud in the extractor.

The results presented below were obtained on 05/09/2009 from gas peak at 3824mMD while 8½" hole drilling.

Mud Type: WBM. MW: 1.14 SG FV:51 PV:16 YP:28 Gel:08/10

Gas Component	C1	C2	C3	iC4	nC4	iC5	nC5
Correcting coefficients	1.1500	1.2962	1.4498	1.5911	1.6536	1.8452	1.9091

GAS FROM FORMATION

Synchronization of Gas IN and OUT data

The data of GAS IN recorded versus time are synchronized with the GAS OUT in order to evaluate the effect of gas recycling. The synchronization is performed using the gas interpretation software InFact.

The plots in the next pages, display the comparison of Gas OUT vs. Gas IN for the light range as well as the heavy range. The scale of each plot has been adapted according to levels recorded in different drilled phases, to emphasize the gas content and recycling effect.

The comparison log clearly shows the presence of formation gas (represented by colour filling between gas out and gas in curves) and total recycling (when the 2 curves are overlapped) which helps to highlight the presence of intervals of interest.

On the next pages Gas In has been synchronized and plotted with Gas Out in order to evaluate the amount of gas from formation above the recycled levels.

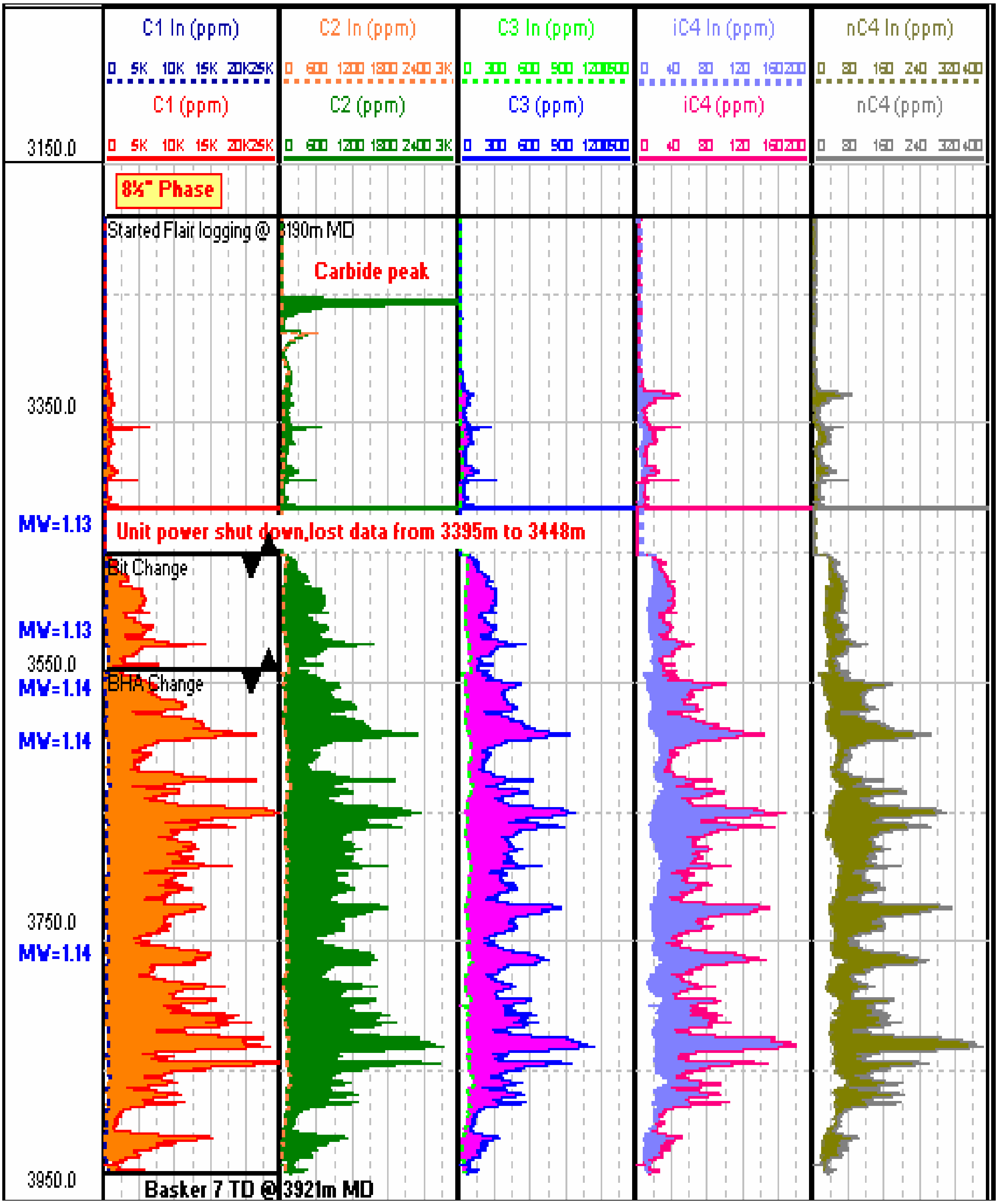


Fig.11: Light Gas Out and Gas In Comparison, 3190m MD-3921m MD.

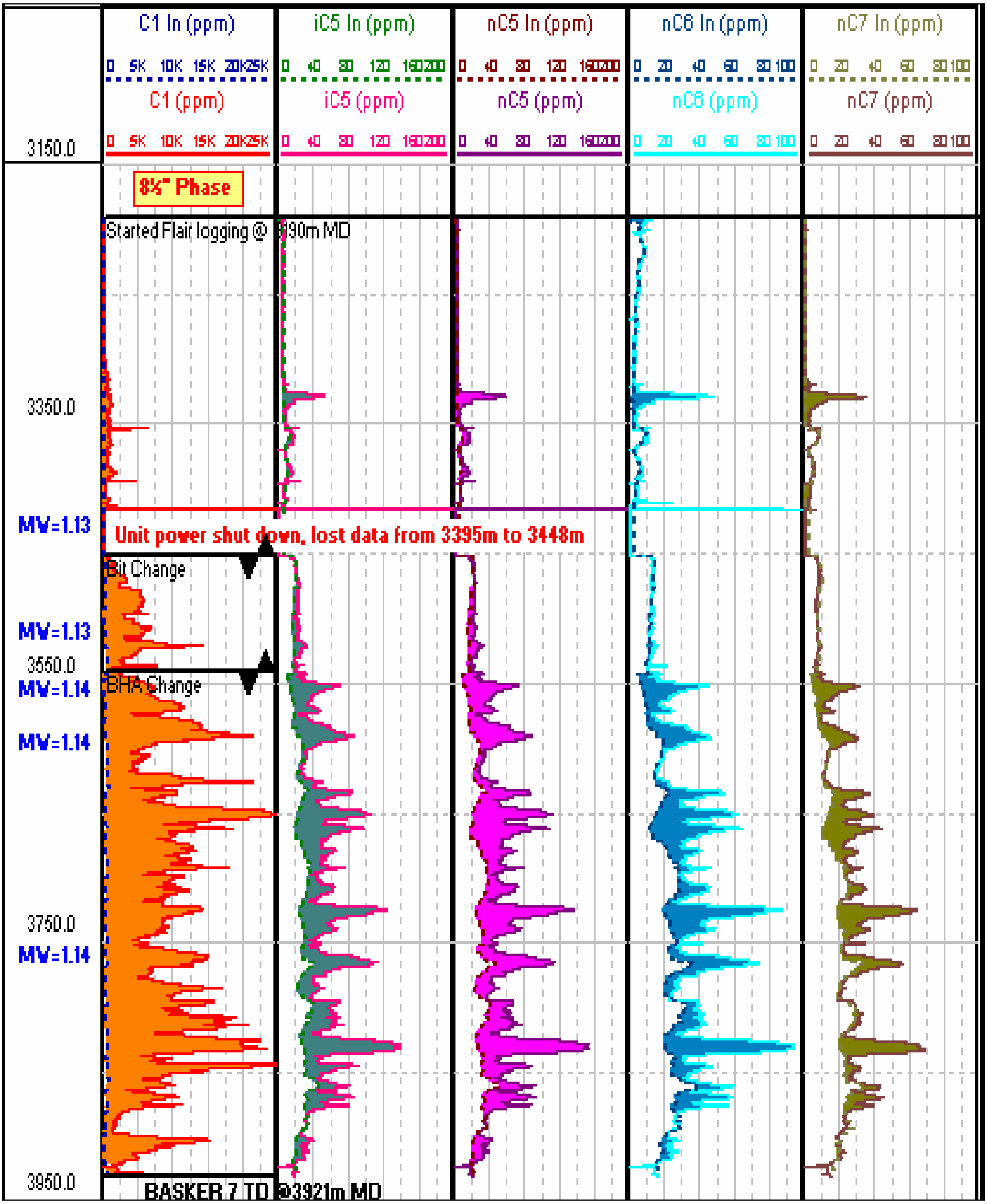


Fig.12: Medium Gas Out and Gas In Comparison, 3190m MD- 3921m MD.

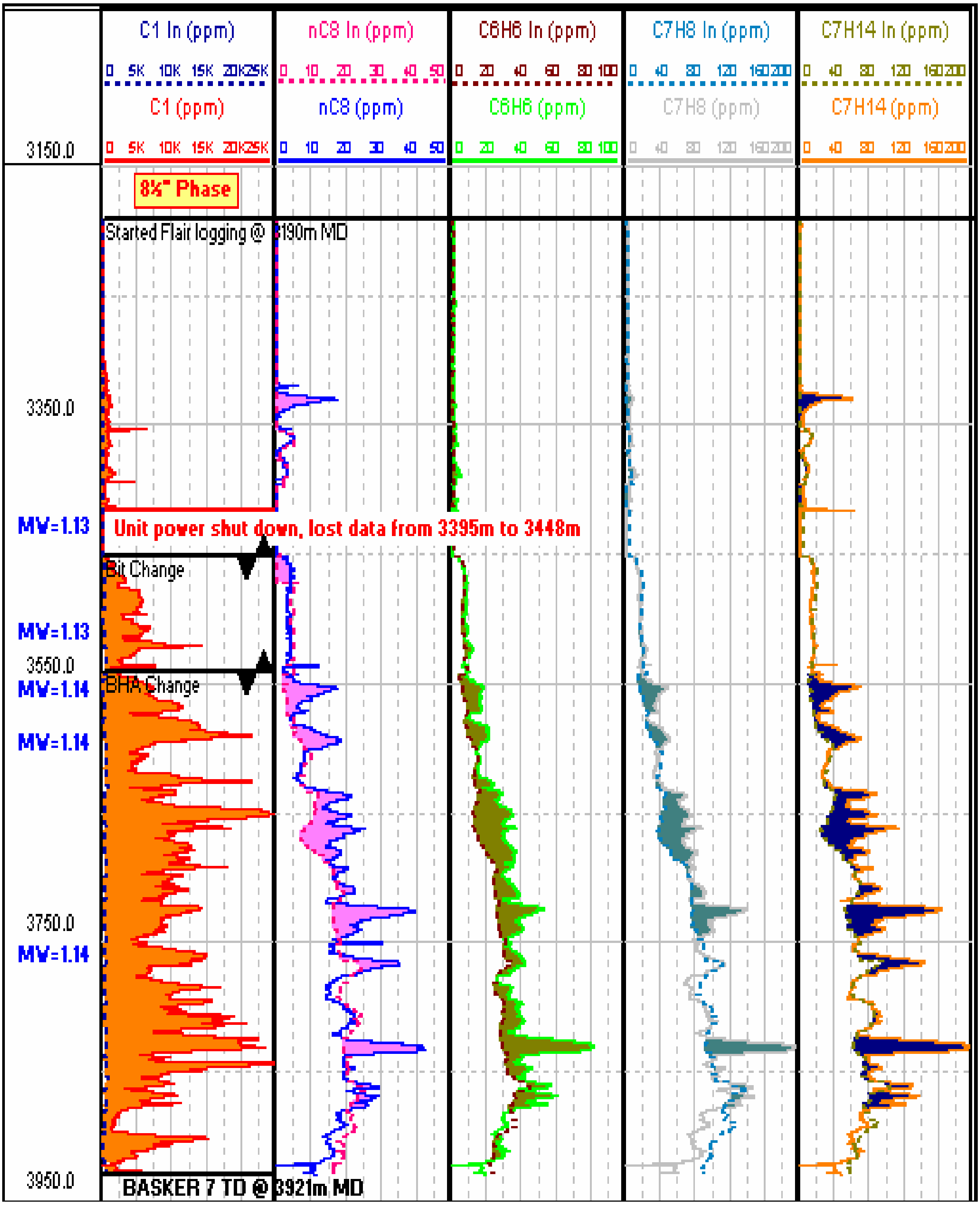


Fig.13: Heavy Gas Out and Gas In Comparison, 3190m MD- 3921m MD.

Corrected FLAIR Data

The gas data presented in the logs has been corrected for recycling effect (GAS OUT-GAS IN), to demonstrate the actual gas contribution from formation.

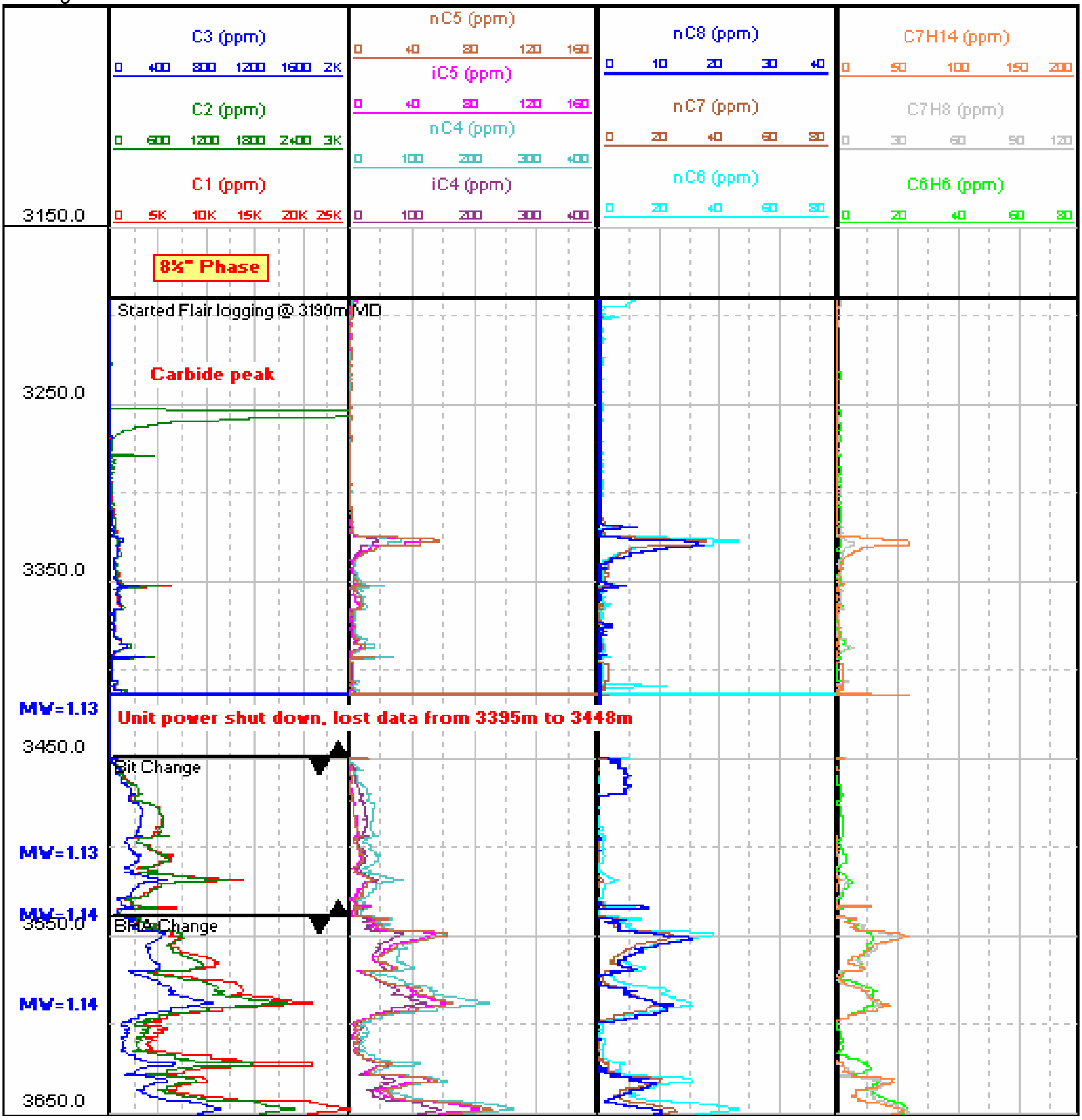


Fig. 14: Chromatolog for actual Gas from formation 3190m-3650m MD.

The above log demonstrates the actual gas contribution from formation (Gas Out corrected for Recycling effect) for the 8 ½" Phase. The above log clearly shows an increase in gas components (C1 to nC8, C6H6, C7H8 & C7H14) at 3448m. There was another increase of gas values at 3545m.

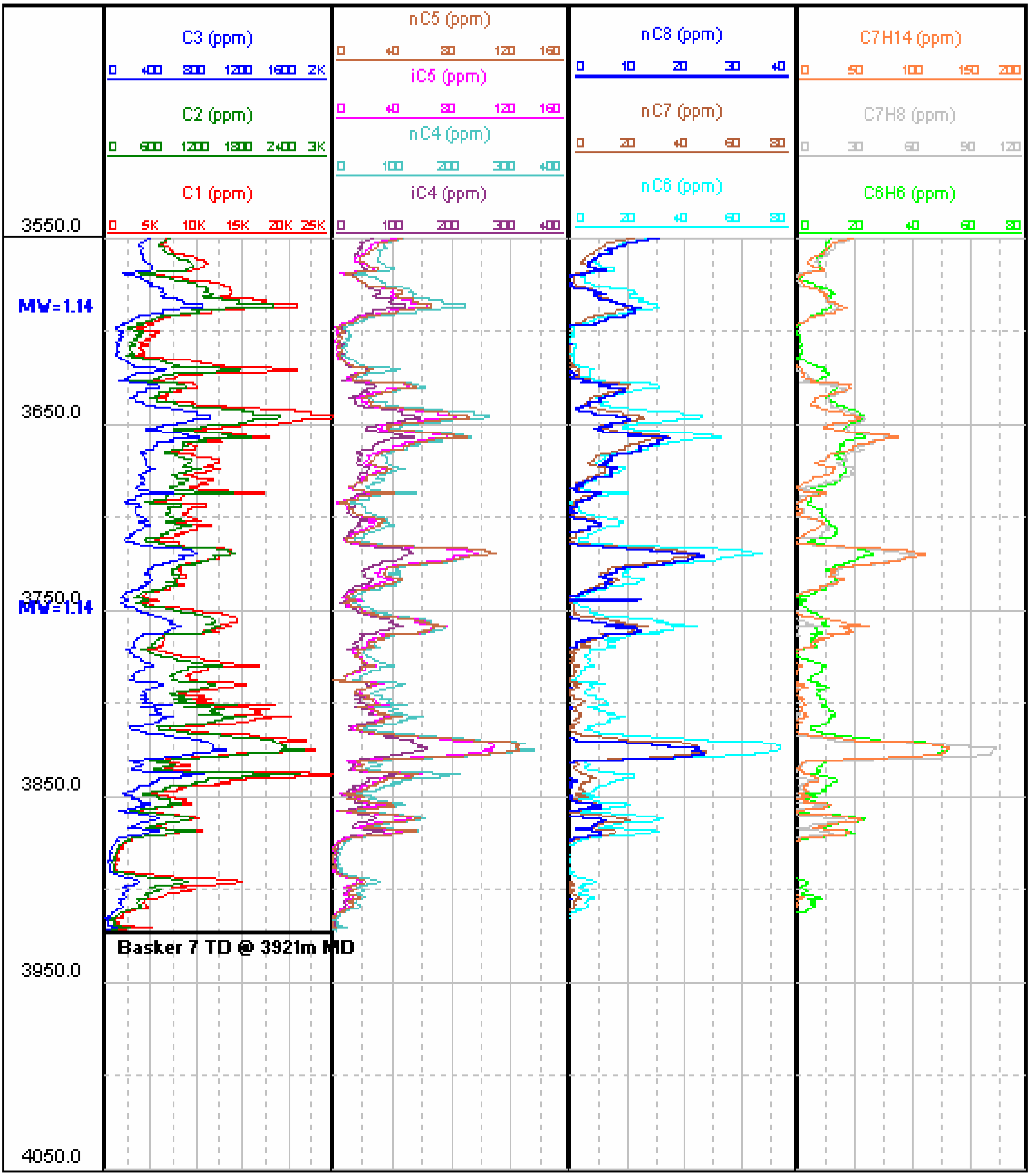


Fig. 15: Chromatolog for actual Gas from formation 3550m to 3921m MD.

From 3550m MD the gas values were quite high, this was seen on all the analysed gas components. The increase on C7H14 and C7H8 was quite significant amongst all the heavies.

Delineation of Potential Zones

The gas data presented has been corrected for recycling effect (GAS OUT-GAS IN) to demonstrate the actual gas contribution from formation.

- Depth monitoring

The depth matching between LWD and gas data is validated.
Gas peaks match with drilling breaks proving the consistency of lag time measurements.

- Definition of the gas level threshold(s)

The standard delineation log is used to identify the potential zones of interest, taking into account the quantity of C1 corrected from recycling, some drilling parameters (mainly ROP, WOB and FLOW Pumps) which mainly affect the gas quantity at surface, and MWD trends.

A plot of C1 values on a linear scale delineates very clearly the potential zones of interest. Results can be compared with those of electrical logs.

A cut off of 1000ppm was applied to C1 to delineate the intervals of potential interest for INFACT analysis.

Gas concentrations below this threshold values were considered as background, whereas all the gas levels above were selected for compositional analysis. A good correlation between the LWD and Gas is seen in this well. However, gas data provides an independent diagnosis on pay zones location.

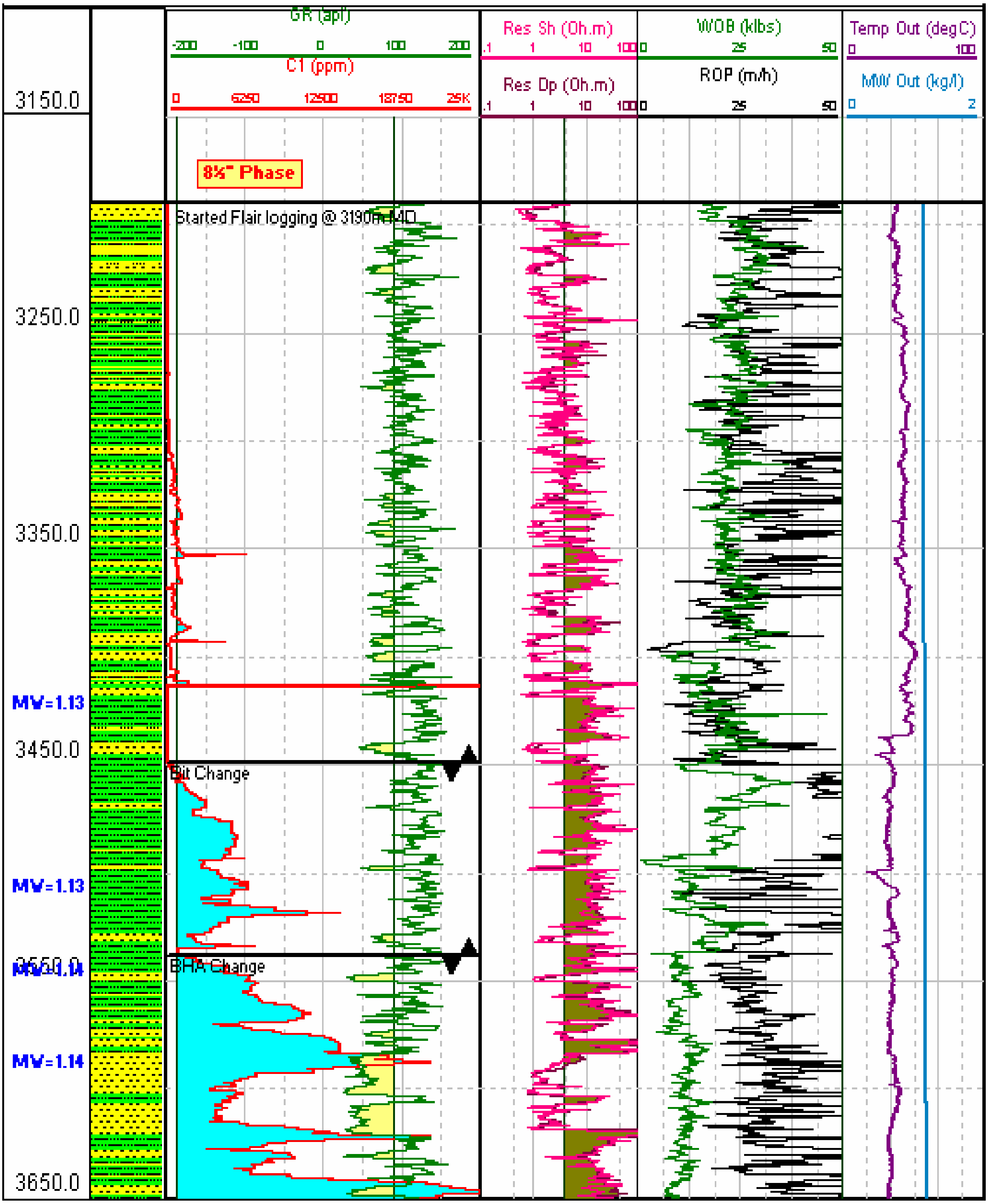


Fig.16: Delineation of potential zones 3190m to 3650m MD.

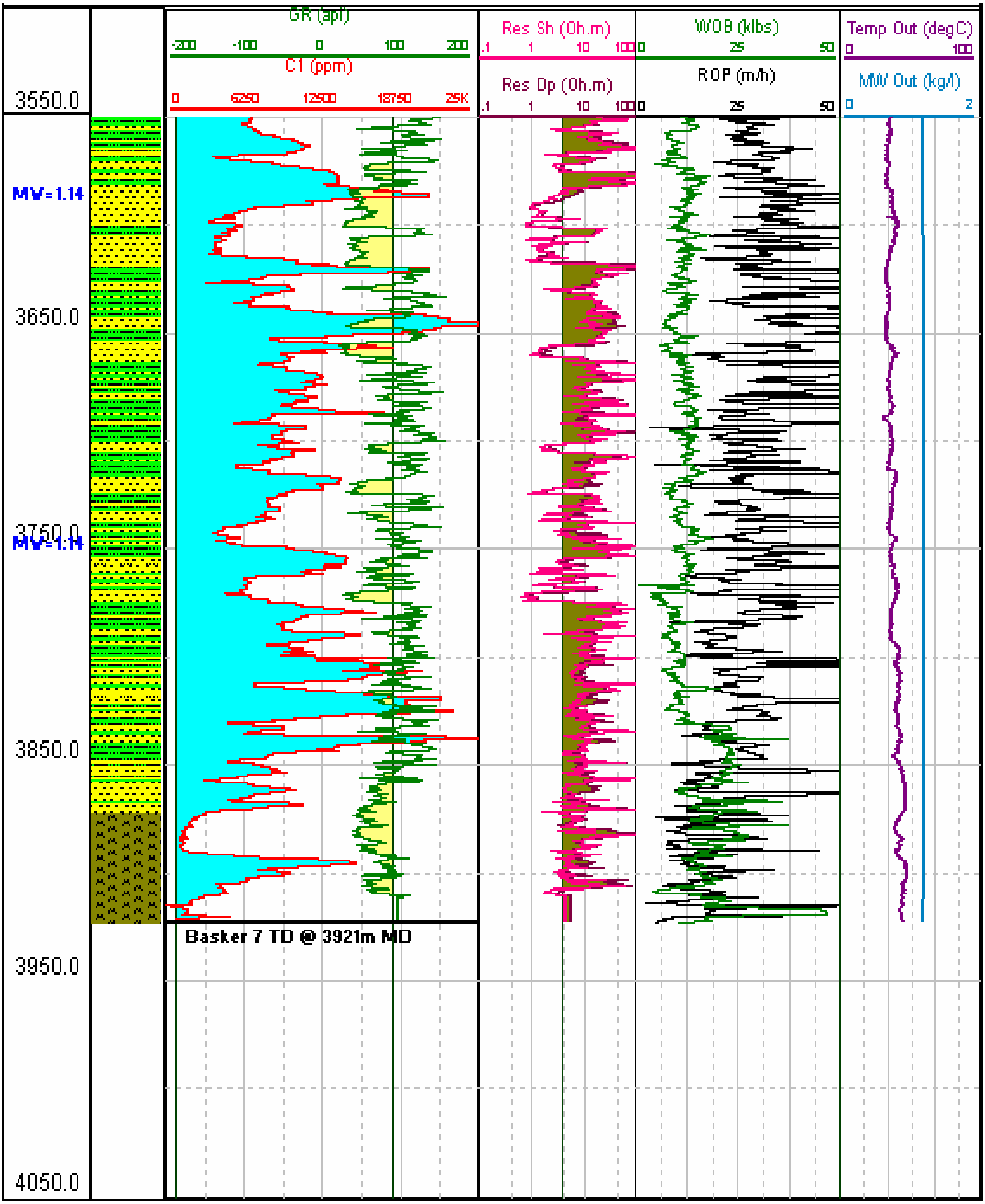


Fig. 17: Delineation of Potential zones 3550m to 3921m MD.

Synthetic Fluid Facies

If two zones are filled with different colours, it indicates compositional differences in the formation fluid. Two zones filled with the same colour are very likely to contain comparable formation fluids.
Comparable formation fluids with similar signature recorded in Basker-7 are labelled same as per fluids encountered in Basker-6ST1 well. The colour was changed for better resolution on Star diagrams.

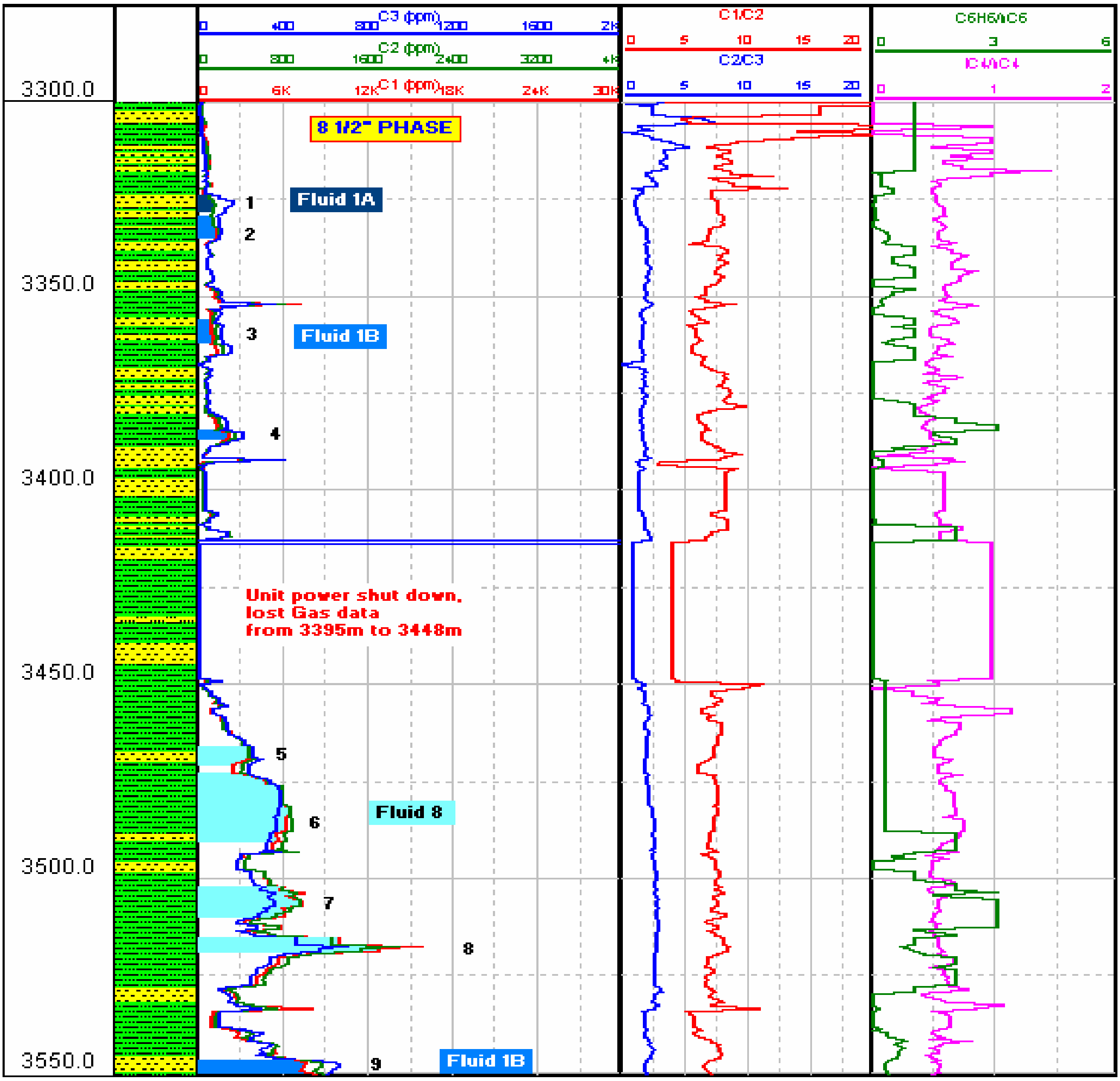
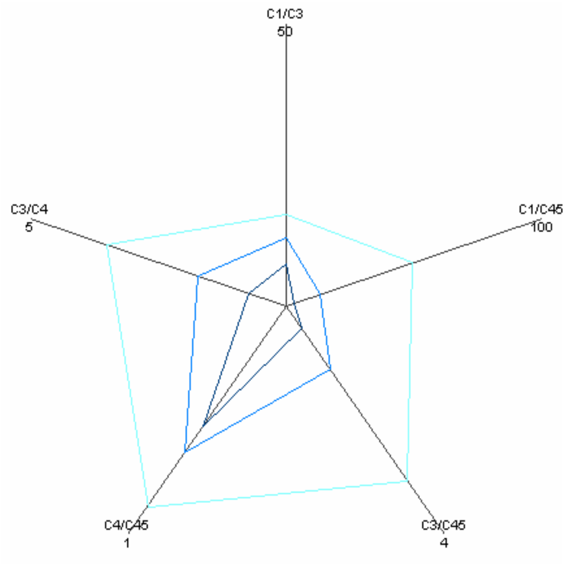


Fig.18: Synthetic Fluid Facies Log from 3200m to 3550m.

Corrected gas data (EEC Applied data) has been utilized for analysis through the well. In the above section Fluid 1 A – B & Fluid 8 were encountered.



FLUID#	PEAK#	Measured Depth From (m)	To (m)
1A'	1	3324	3328.2
1B	2	3328.6	3334.6
	3	3355.5	3361.9
	4	3383.8	3386.5
8	5	3465	3469.7
	6	3471.8	3490
	7	3501	3509
	8	3514	3518
1B	9	3545.5	3549

Fig.19: Star diagram for Fluids 1A, 1B & 8.

The intervals 1-9 are recorded in the silty shaly formation while the sand layers show a general drop in the gas level.

- **FLUID 1A' (Interval 1)** is composed of 61% of C1 in the C1-C5 range. It comprises all the components in the analysed range with relatively very high presence of C6+ especially C7H14, even though the general gas level is very low. The lithology consists of argillaceous sand. *There are no indications of HC bearing zone based on LWD data, however, FLAIR indicates presence of heavy HC composition*

- **FLUID 1B (intervals 2-4, 9)** is composed of 73-75% of C1 in the C1-C5 range. It comprises all the components in the C1-C5 range. The gas level is very low. The lithology consists of argillaceous siltstone in the interval 2-4 and clean sand in the interval 9.

- **FLUID 8** (intervals 5-8) is composed of 80-83% of C1 in the C1-C5 range. It comprises all the components in the C1-C4 range with minor presence of C5s. C6+ components are not present. The gas level is relatively higher compared to the upper intervals. It was recorded in argillaceous siltstone.

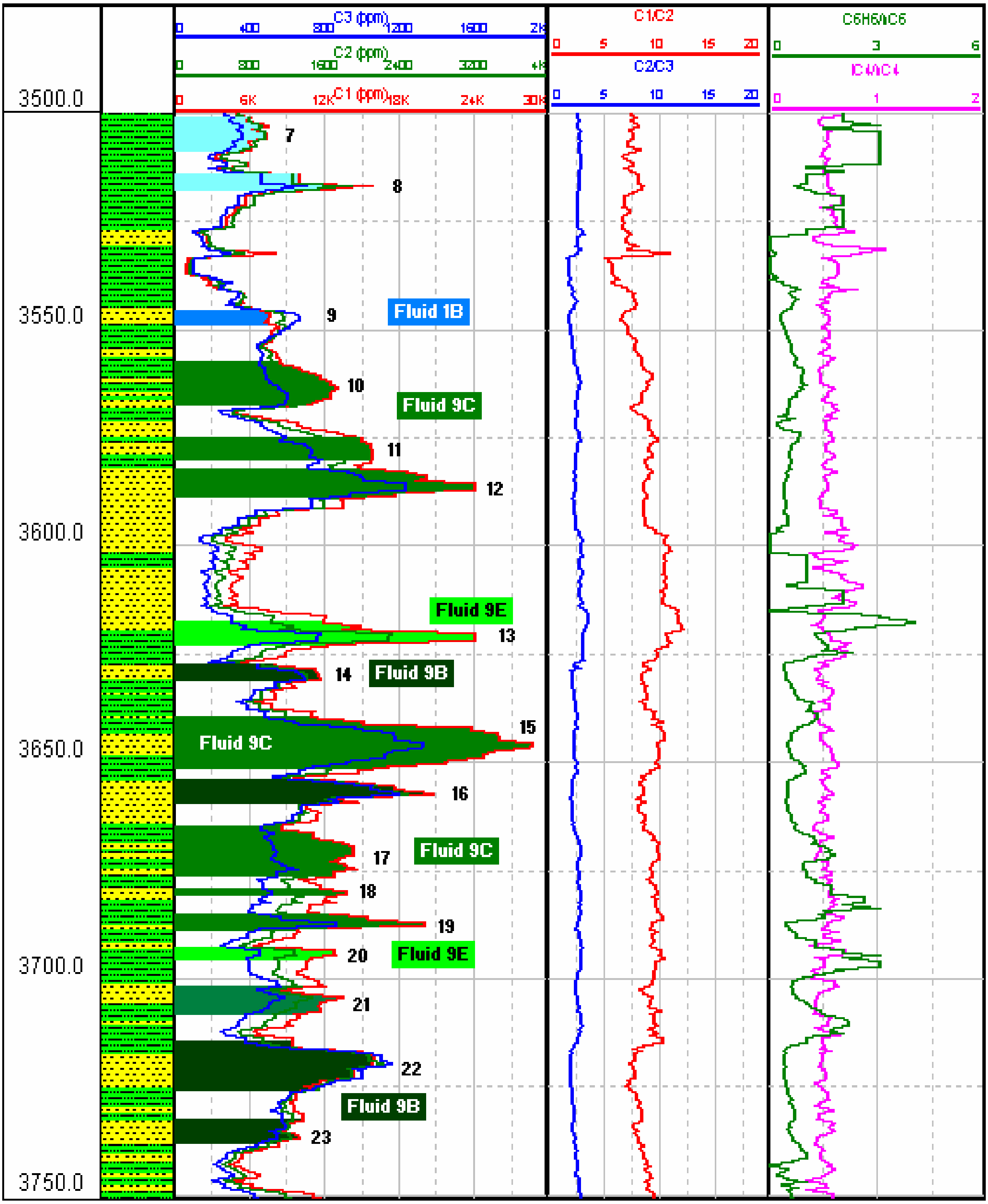
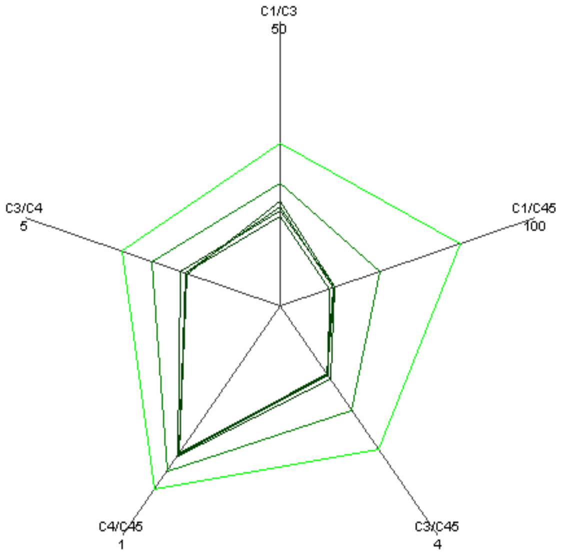


Fig.20: Synthetic Fluid Facies Log from 3500m to 3750 m



FLUID#	PEAK#	Measured Depth From (m)	Measured Depth To (m)
9C	10	3556.9	3567.5
	11	3574.1	3580
	12	3581.3	3588.2
9E	13	3616.2	3622.4
9B	14	3626.2	3630.3
9C	15	3638.1	3650.8
9B	16	3652.7	3658.6
9C	17	3663.6	3675.5
	18	3677.7	3679.9
	19	3684	3687.8
9E	20	3691.3	3694.8
9C	21	3700.2	3707.5
9B	22	3712.6	3724.6
	23	3731	3737
	24	3754.5	3762

Fig.21: Star diagram for Fluids 9B, 9C & Fluid 9E.

- **FLUID 9C (Intervals 10-12, 15, 17-19 and 21)** is composed of 84-85% of C1 in the C1-C5 range. It comprises all the components in the analysed range (C1-C8, Benzene, Toluene and Methylcyclohexane). The gas level is relatively high. It was found in clean sands, intervals 10-12 and 15. Possible HWC can be placed around 3586m MD.

- **FLUID 9B (Intervals 14, 16, 22-24)** is composed of 80-82% of C1 in the C1-C5 range. It comprises all the components in the C1-C5 range with relatively high presence of C6+. The gas level is moderate to high.

- **FLUID 9E (Intervals 13 and 20)** is composed of 88-90% of C1 in the C1-C5 range. It comprises all the components in the C1-C5 range with traces or minor amounts of C6+. The gas level is relatively high. It was recorded in clean sands.

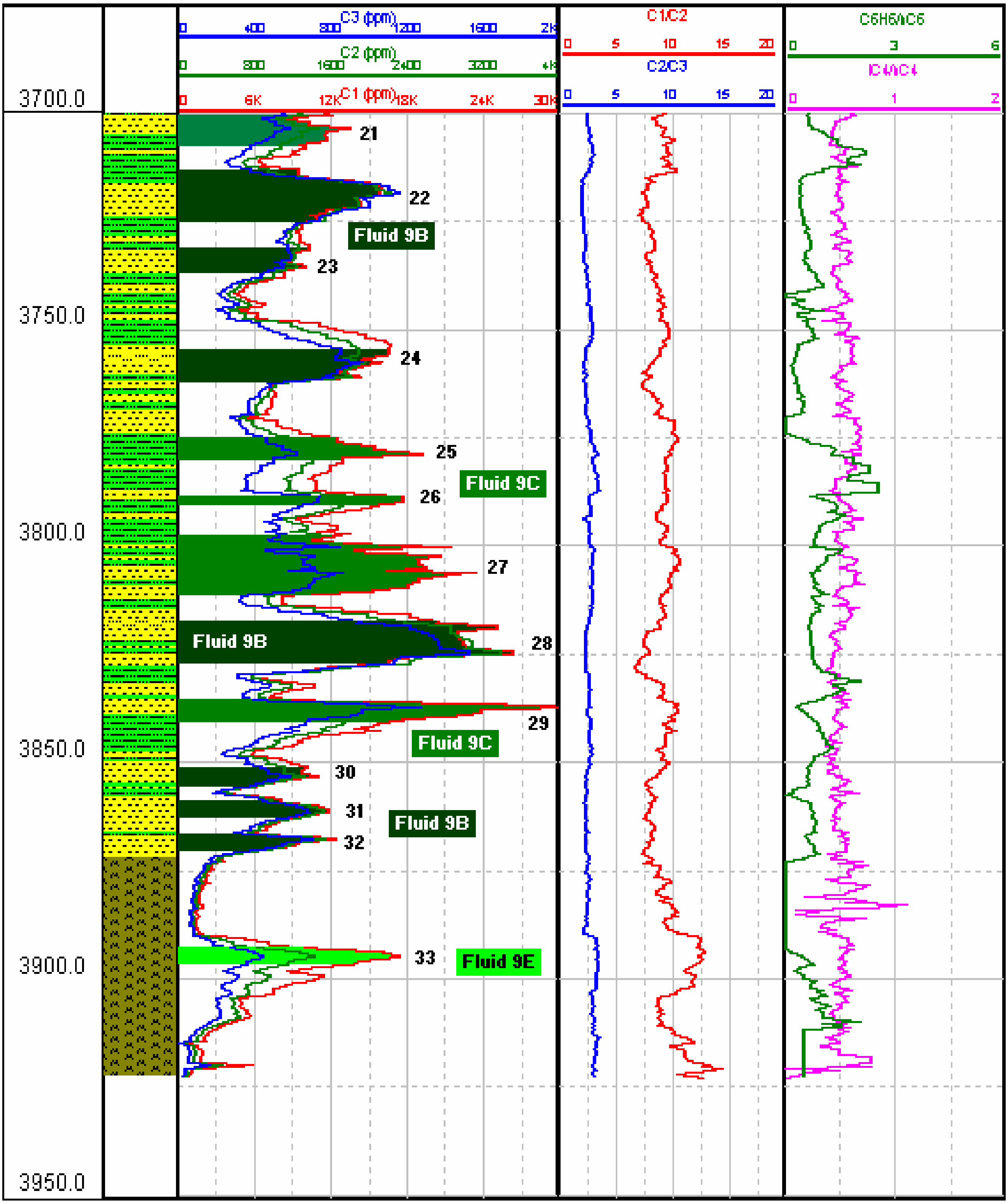
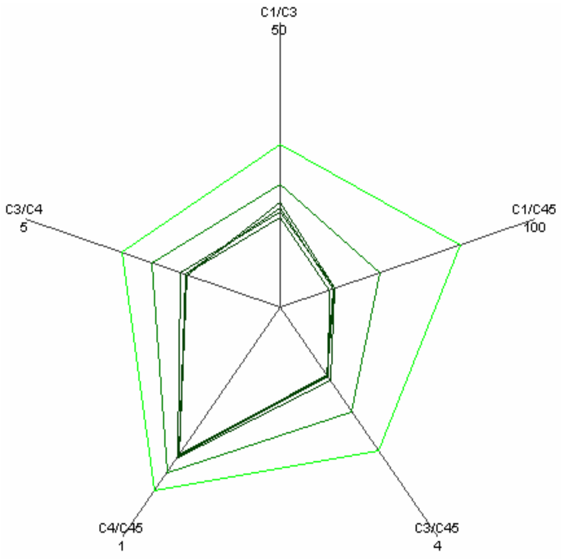


Fig.22: Synthetic Fluid Facies Log from 3700m to 3921m



FLUID#	PEAK#	Measured Depth From (m)	To (m)
9C	25	3774.1	3780
	26	3787.6	3789.7
	27	3796.8	3810.7
9B	28	3816.5	3826.5
9C	29	3834.5	3839.9
9B	30	3850.5	3854.7
	31	3858	3862
	32	3865.5	3869.5
9E	33	3891.5	3895.5

Fig.23: Star diagram for Fluids 9B, 9C & Fluid 9E.

- **FLUID 9C (Intervals 25-27 and 29)** is composed of 84-85% of C1 in the C1-C5 range. It comprises all the components in the analysed range (C1-C8, Benzene, Toluene and Methylcyclohexane). The gas level is relatively high. It was found in a clean sands in intervals 10-12 and 15. Possible HWC can be placed around 3586m MD.

- **FLUID 9B (Intervals 28, 30-32)** is composed of 80-82% of C1 in the C1-C5 range. It comprises all the components in the C1-C5 range with relatively high presence of C6+. The gas level is moderate to high.

- **FLUID 9E (Intervals 33)** is composed of 88-90% of C1 in the C1-C5 range. It comprises all the components in the C1-C5 range with traces or minor amounts of C6+. The gas level is relatively high. It was found in silty sand lithology.

Limits Table

The following limit table is based on the conclusion from Synthetic Fluid Facies. The bar chart shows the normalized average C1-C5 composition of the various gas peaks analysed. The composition has been obtained after correcting the gas data with the recycling effect (Cn gas OUT - Cn gas IN $_{\text{synchronized}}$).

FLUID#	PEAK#	Measured Depth From (m)	Measured Depth To (m)	Vertical Depth From (m)	Vertical Depth To (m)	%C1	%C2	%C3	%iC4	%nC4	%iC5	%nC5
1A'	1	3324	3328.2	2805.38	2808.77	68.331	8.129	7.423	3.25	5.774	3.146	3.947
1B	2	3328.6	3334.6	2809.08	2813.92	79.852	9.673	5.288	1.195	2.125	0.794	1.073
	3	3355.5	3361.9	2830.73	2835.87	77.397	11.655	6.792	1.145	2.005	0.392	0.615
	4	3383.8	3386.5	2853.44	2855.62	79.383	11.131	6.193	0.84	1.721	0.299	0.432
8	5	3465	3469.7	2918.56	2922.37	82.977	10.528	5.155	0.458	0.831	0.038	0.015
	6	3471.8	3490	2924.05	2938.75	84.337	10.337	4.143	0.423	0.627	0.07	0.062
	7	3501	3509	2947.89	2954.4	85.399	10.049	3.348	0.348	0.651	0.097	0.109
	8	3514	3518	2958.47	2961.73	86.228	9.5	3.157	0.32	0.579	0.106	0.109
1B	9	3545.5	3549	2984.3	2987.2	80.042	10.612	5.288	0.961	1.766	0.62	0.712
9C	10	3556.9	3567.5	2993.79	3002.63	86.286	8.988	3.199	0.393	0.742	0.187	0.206
	11	3574.1	3580	3008.13	3013.06	86.861	8.43	3.047	0.435	0.762	0.222	0.242
	12	3581.3	3588.2	3014.15	3019.94	85.832	8.731	3.464	0.5	0.925	0.263	0.284
9E	13	3616.2	3622.4	3043.46	3048.69	89.783	7.241	2.094	0.243	0.432	0.102	0.104
9B	14	3626.2	3630.3	3051.89	3055.34	84.805	8.819	3.712	0.576	1.223	0.418	0.448
9C	15	3638.1	3650.8	3061.94	3072.73	87.289	7.846	3.061	0.455	0.827	0.248	0.274
9B	16	3652.7	3658.6	3074.35	3079.35	84.364	8.999	3.988	0.621	1.186	0.399	0.444
9C	17	3663.6	3675.5	3083.6	3093.8	87.246	8.252	2.877	0.388	0.773	0.216	0.247
	18	3677.7	3679.9	3095.68	3097.57	87.976	8.048	2.642	0.361	0.635	0.163	0.175
	19	3684	3687.8	3101.08	3104.34	87.762	8.094	2.794	0.364	0.631	0.171	0.183
9E	20	3691.3	3694.8	3107.34	3110.35	88.738	7.914	2.473	0.271	0.442	0.071	0.09
9C	21	3700.2	3707.5	3115.02	3121.33	86.807	8.53	3.027	0.375	0.785	0.218	0.258
9B	22	3712.6	3724.6	3125.73	3136.15	82.748	9.633	4.397	0.716	1.443	0.499	0.563
	23	3731	3737	3137.68	3142.71	84.26	9.428	3.917	0.573	1.091	0.33	0.4
	24	3754.5	3762	3157.32	3163.63	84.193	9.29	3.876	0.637	1.15	0.425	0.43
9C	25	3774.1	3780	3179.51	3184.69	88.203	8.053	2.493	0.369	0.574	0.159	0.148
	26	3787.6	3789.7	3185.13	3186.9	87.532	8.25	2.878	0.341	0.673	0.173	0.155
	27	3796.8	3810.7	3199.63	3211.97	88.001	8.035	2.616	0.362	0.635	0.173	0.177
9B	28	3816.5	3826.5	3217.18	3226.14	83.795	9.64	3.827	0.587	1.25	0.419	0.482
9C	29	3834.5	3839.9	3233.32	3238.18	87.942	7.792	2.766	0.371	0.729	0.194	0.206
9B	30	3850.5	3854.7	3247.74	3251.52	85.123	9.136	3.559	0.523	1.041	0.276	0.342
	31	3858	3862	3244.57	3247.99	83.781	9.574	3.872	0.605	1.264	0.426	0.477
	32	3865.5	3869.5	3250.92	3254.33	83.9	9.484	3.891	0.666	1.192	0.403	0.463
9E	33	3891.5	3895.5	3273.04	3276.42	90.676	6.53	1.835	0.255	0.464	0.111	0.13

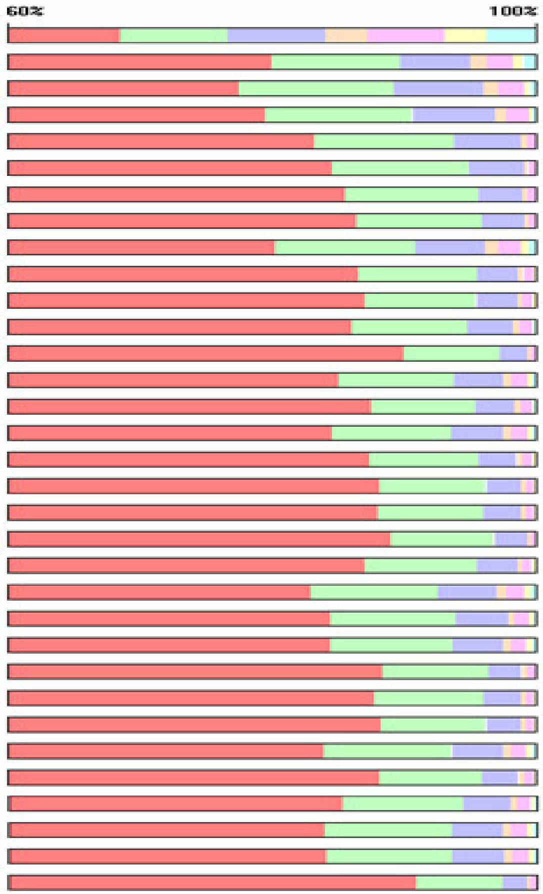
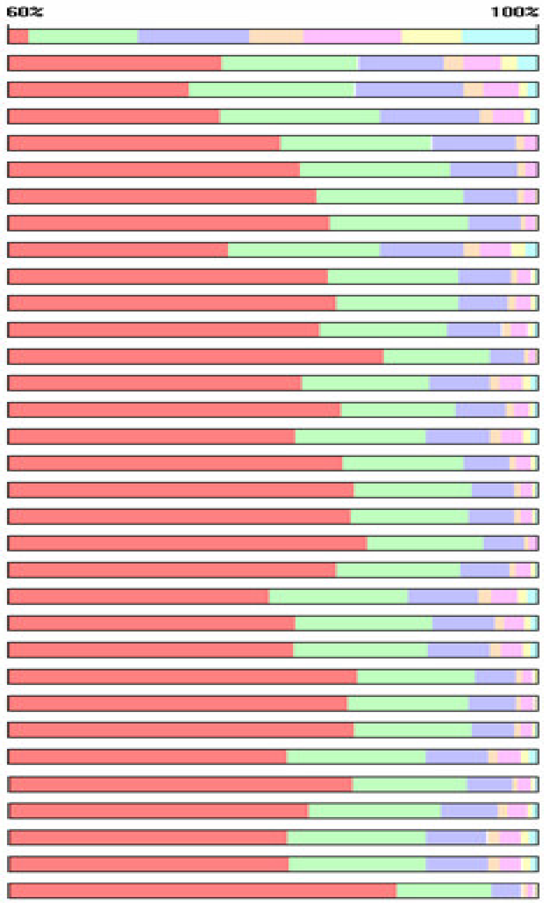


Table.2: Composition of Gas Extracted from Mud

The following bar chart shows composition obtained after applying the EEC coefficients on the gas data corrected for recycling effect (Cn gas OUT - Cn gas IN $_{synchronized}$)*EEC Coefficient of Cn. This composition represents Formation Fluid composition in the C1-C5 range.

Gas Component	C1	C2	C3	iC4	nC4	iC5	nC5
Correcting coefficients	1.1500	1.2962	1.4498	1.5911	1.6536	1.8452	1.9091



FLUID#	PEAK#	Measured Depth From (m)	Measured Depth To (m)	Vertical Depth From (m)	Vertical Depth To (m)	%C1	%C2	%C3	%iC4	%nC4	%iC5	%nC5
1A'	1	3324	3328.2	2805.38	2808.77	61.47	8.243	8.418	4.045	7.388	4.541	5.894
1B	2	3328.6	3334.6	2809.08	2813.92	75.94	10.369	6.34	1.572	2.874	1.212	1.693
	3	3355.5	3361.9	2830.73	2835.87	73.585	12.49	8.14	1.506	2.711	0.598	0.97
	4	3383.8	3386.5	2853.44	2855.62	75.932	12.001	7.469	1.111	2.341	0.459	0.686
8	5	3465	3469.7	2918.56	2922.37	80.372	11.494	6.294	0.613	1.145	0.059	0.023
	6	3471.8	3490	2924.05	2938.75	81.956	11.323	5.076	0.569	0.867	0.109	0.1
	7	3501	3509	2947.89	2954.4	83.162	11.03	4.111	0.468	0.902	0.151	0.177
	8	3514	3518	2958.47	2961.73	84.097	10.443	3.881	0.432	0.803	0.166	0.177
1B	9	3545.5	3549	2984.3	2987.2	76.459	11.426	6.368	1.269	2.399	0.95	1.129
9C	10	3556.9	3567.5	2993.79	3002.63	84.026	9.866	3.927	0.529	1.027	0.292	0.333
	11	3574.1	3580	3008.13	3013.06	84.62	9.257	3.742	0.587	1.055	0.347	0.392
	12	3581.3	3588.2	3014.15	3019.94	83.379	9.559	4.242	0.673	1.278	0.41	0.458
9E	13	3616.2	3622.4	3043.46	3048.69	88.133	8.012	2.592	0.33	0.603	0.161	0.169
9B	14	3626.2	3630.3	3051.89	3055.34	82.037	9.616	4.527	0.772	1.682	0.648	0.719
9C	15	3638.1	3650.8	3061.94	3072.73	85.035	8.615	3.76	0.613	1.146	0.387	0.444
9B	16	3652.7	3658.6	3074.35	3079.35	81.545	9.804	4.86	0.83	1.631	0.618	0.712
9C	17	3663.6	3675.5	3083.6	3093.8	85.062	9.069	3.536	0.523	1.072	0.338	0.4
	18	3677.7	3679.9	3095.68	3097.57	85.971	8.864	3.255	0.488	0.883	0.256	0.283
	19	3684	3687.8	3101.08	3104.34	85.715	8.91	3.441	0.492	0.877	0.268	0.297
9E	20	3691.3	3694.8	3107.34	3110.35	86.961	8.741	3.055	0.368	0.616	0.112	0.147
9C	21	3700.2	3707.5	3115.02	3121.33	84.565	9.366	3.717	0.506	1.087	0.341	0.417
9B	22	3712.6	3724.6	3125.73	3136.15	79.62	10.447	5.333	0.954	1.975	0.771	0.9
	23	3731	3737	3137.68	3142.71	81.518	10.28	4.778	0.768	1.502	0.513	0.642
	24	3754.5	3762	3157.32	3163.63	81.376	10.121	4.723	0.851	1.581	0.658	0.69
9C	25	3774.1	3780	3179.51	3184.69	86.261	8.877	3.073	0.5	0.799	0.249	0.241
	26	3787.6	3789.7	3185.13	3186.9	85.464	9.079	3.542	0.46	0.934	0.271	0.25
	27	3796.8	3810.7	3199.63	3211.97	85.995	8.85	3.223	0.49	0.883	0.272	0.288
9B	28	3816.5	3826.5	3217.18	3226.14	80.923	10.493	4.66	0.784	1.717	0.65	0.773
9C	29	3834.5	3839.9	3233.32	3238.18	85.868	8.575	3.405	0.501	1.013	0.304	0.334
9B	30	3850.5	3854.7	3247.74	3251.52	82.545	9.986	4.351	0.702	1.436	0.429	0.551
	31	3858	3862	3244.57	3247.99	80.898	10.42	4.714	0.809	1.736	0.659	0.765
	32	3865.5	3869.5	3250.92	3254.33	81.041	10.326	4.738	0.89	1.638	0.625	0.742
9E	33	3891.5	3895.5	3273.04	3276.42	89.112	7.233	2.274	0.346	0.648	0.175	0.212

Table.3: Formation Fluid Composition

CONCLUSION

The interpretation of the gas data has led to the identification of THREE (3) main fluids.

The data used is corrected from recycling effect and Extraction Efficiency calibration for C1-C5 components:

Fluids are labeled as per Basker-6ST1 well. Comparable formation fluids with similar signature recorded in Basker-7 are labeled same as per fluids encountered in Basker-6ST1 well.

Fluids 1A, 1B, 8, 9B & 9C of Basker-7 are comparable to the fluids 1A, 1B, 8, 9B & 9C encountered in Basker-6ST1 well. Fluids 9A in Basker 6ST1 and 9E in Basker-7 are compositionally different and thus labeled differently.

FLUID 1A: is composed of 61% of C1 in the C1-C5 range. It comprises all the components in the analysed range with relatively very high presence of C6+ especially C7H14, even though the general gas level is very low. The lithology consists of argillaceous sand. *There are no indications of HC bearing zone based on LWD data, however, FLAIR indicates presence of heavy HC composition.*

FLUID 1B: is composed of 73-75% of C1 in the C1-C5 range. It comprises all the components in the C1-C5 range. The gas level is very low. The lithology consists of argillaceous siltstone in the interval 2-4 and clean sand in the interval 9.

Fluid 1A & 1B were recorded in Basker 6ST1 well. Fluid 1A showed heavy composition in Basker-7

FLUID 8: is composed of 80-83% of C1 in the C1-C5 range. It comprises all the components in the C1-C4 range with minor presence of C5s. C6+ components are not present. The gas level is relatively higher compared to the upper intervals. It was recorded in argillaceous siltstone.

Fluid 8 was recorded in Basker 6ST1 well

FLUID 9B: is composed of 80-82% of C1 in the C1-C5 range. It comprises all the components in the C1-C5 range with relatively high presence of C6+. The gas level is moderate to high.

FLUID 9C: is composed of 84-85% of C1 in the C1-C5 range. It comprises all the components in the analysed range (C1-C8, Benzene, Toluene and Methylcyclohexane). The gas level is relatively high. It was found in clean sands, intervals 10-12 and 15. Possible HWC can be placed around 3586m MD.

FLUID 9E: is composed of 87-90% of C1 in the C1-C5 range. It comprises all the components in the C1-C5 range with traces or minor amounts of C6+. The gas level is relatively high. It was recorded in clean sands.

Fluid 9B & 9C were recorded in Basker 6ST1 well

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TVD COMPARISON BETWEEN BASKER-7 AND BASKER-6ST1 WELLS

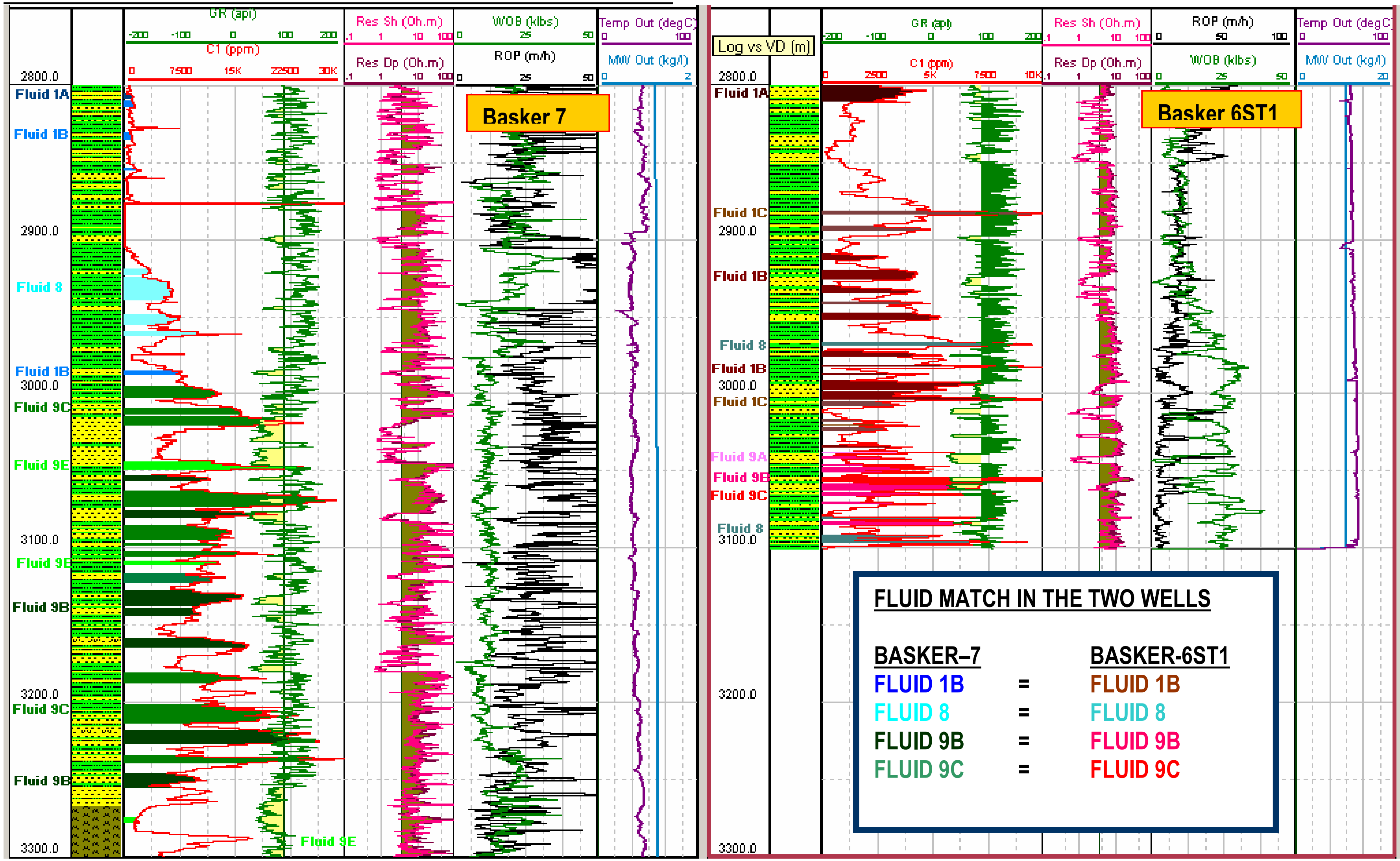
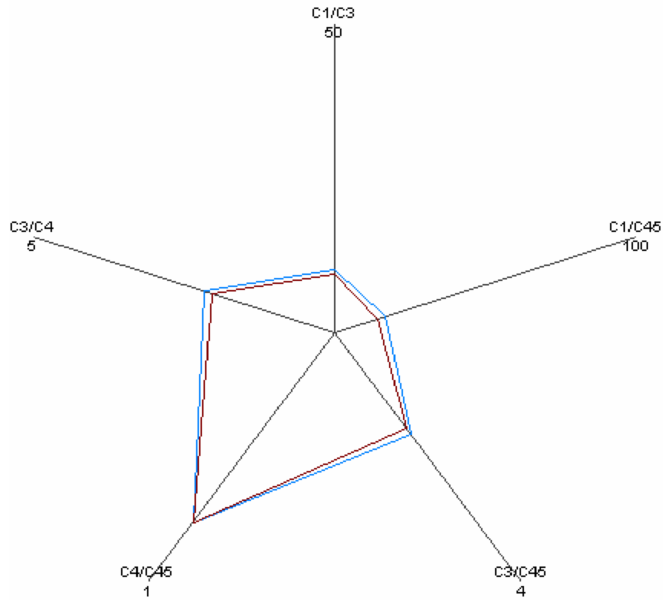


Fig.24: TVD comparison of Basker-7 with basker-6ST1 well.

COMPARISON OF FLUID 1 IN THE TWO WELLS

Basker-7

FLUID#	PEAK#	Measured Depth		Vertical Depth	
		From (m)	To (m)	From (m)	To (m)
1B	2	3328.6	3334.6	2809.1	2813.9
	3	3355.5	3361.9	2830.7	2835.9
	4	3383.8	3386.5	2853.4	2855.6



Basker-6ST1

FLUID#	PEAK#	Measured Depth		Vertical Depth	
		From (m)	To (m)	From (m)	To (m)
1C	3	2953.9	2955.8	2881.4	2883.3
	4	2963.5	2966.8	2890.9	2894.2
1B	5	2981.5	2985.2	2908.9	2912.6
	6	2992	2998.5	2919.4	2925.9
	7	3001.7	3007.1	2929.1	2934.5
1C	8	3012.4	3013.6	2939.8	2941
1B	9	3019.6	3024.5	2947	2951.9
8	10	3038.1	3041	2965.5	2968.4
1B	11	3044.9	3048	2972.3	2975.4
	12	3053.5	3054.5	2980.9	2981.9
	13	3058.4	3060	2985.8	2987.4
	14	3063	3067.2	2990.4	2994.6
	15	3067.6	3070	2994.9	2997.3
	16	3070.1	3073	2997.5	3000.4
	17	3073.5	3075.9	3000.8	3003.2
1C	18	3077	3080.2	3004.3	3007.5
	19	3088.4	3090.5	3015.6	3017.9
1D	20	3091.1	3092.9	3018.5	3020.3
1C	21	3093.5	3095.9	3020.9	3023.3
1B	22	3105.5	3106.8	3032.9	3034.2

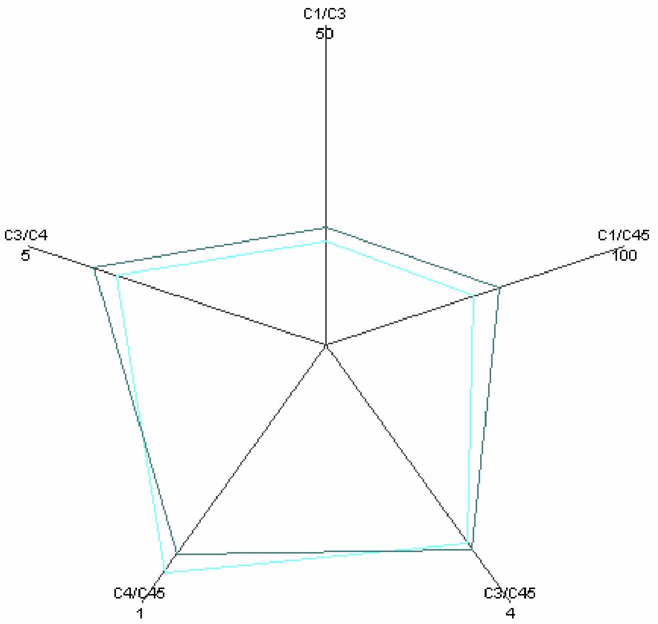
``

Fig.25: Star diagram for Fluids 1B of Basker-7 & Fluid 1B of Basker-6ST1.

Fluid 1B in Basker-7 exhibits good comparison with Fluid 1B in Basker 6ST1

Basker-7

FLUID#	PEAK#	Measured Depth From (m)	Measured Depth To (m)	Vertical Depth From (m)	Vertical Depth To (m)
8	5	3465	3469.7	2918.6	2922.4
	6	3471.8	3490	2924.1	2938.8
	7	3501	3509	2947.9	2954.4
	8	3514	3518	2958.5	2961.7



Basker-6ST1

FLUID#	PEAK#	Measured Depth From (m)	Measured Depth To (m)	Vertical Depth From (m)	Vertical Depth To (m)
8	10	3038.1	3041	2965.5	2968.4

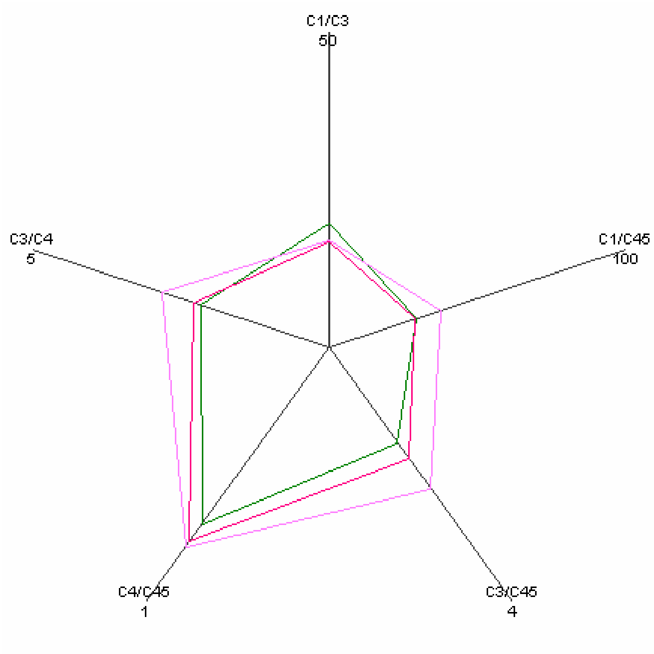
FLUID#	PEAK#	Measured Depth From (m)	Measured Depth To (m)	Vertical Depth From (m)	Vertical Depth To (m)
8	32	3151.5	3152.9	3078.9	3080.3
9B	33	3154.2	3156.9	3081.6	3084.3
8	34	3162.6	3164.9	3090	3092.3
	35	3165	3166.5	3092.4	3093.9
	36	3166.6	3168.5	3094	3095.9

Fig.26: Star diagram for Fluids 8 of Basker-7 & Fluid 8 of Basker-6ST1

Fluid 8 in Basker-7 exhibits good comparison with Fluid 8 in Basker 6ST1

Basker-7

FLUID#	PEAK#	Measured Depth From (m)	Measured Depth To (m)	Vertical Depth From (m)	Vertical Depth To (m)
9C	10	3556.9	3567.5	2993.8	3002.6
	11	3574.1	3580	3008.1	3013.1
	12	3581.3	3588.2	3014.2	3019.9
9E	13	3616.2	3622.4	3043.5	3048.7
9B	14	3626.2	3630.3	3051.9	3055.3
9C	15	3638.1	3650.8	3061.9	3072.7
9B	16	3652.7	3658.6	3074.4	3079.4
9C	17	3663.6	3675.5	3083.6	3093.8
	18	3677.7	3679.9	3095.7	3097.6
	19	3684	3687.8	3101.1	3104.3
9E	20	3691.3	3694.8	3107.3	3110.4
9C	21	3700.2	3707.5	3115	3121.3
9B	22	3712.6	3724.6	3125.7	3136.2
	23	3731	3737	3137.7	3142.7
	24	3754.5	3762	3157.3	3163.6
9C	25	3774.1	3780	3179.5	3184.7
	26	3787.6	3789.7	3185.1	3186.9
	27	3796.8	3810.7	3199.6	3212
9B	28	3816.5	3826.5	3217.2	3226.1
9C	29	3834.5	3839.9	3233.3	3238.2
9B	30	3850.5	3854.7	3247.7	3251.5
	31	3858	3862	3244.6	3248
	32	3865.5	3869.5	3250.9	3254.3
9E	33	3891.5	3895.5	3273	3276.4



Basker-6ST1

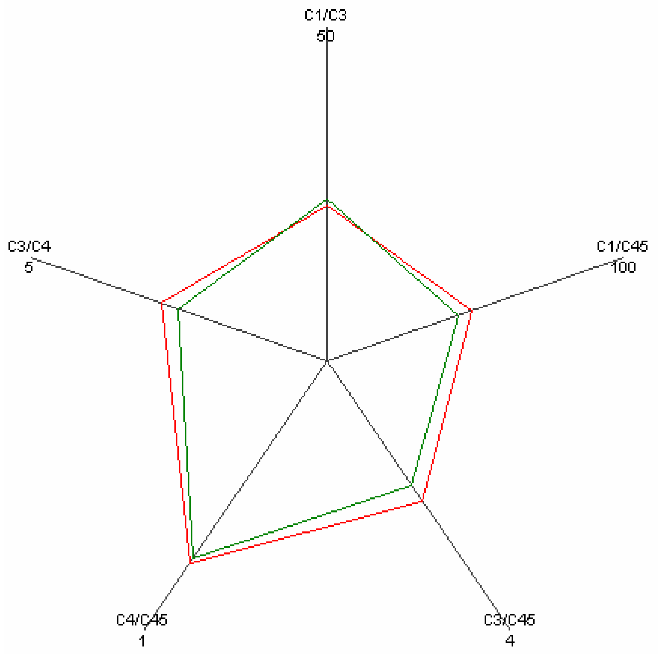
FLUID#	PEAK#	Measured Depth From (m)	Measured Depth To (m)	Vertical Depth From (m)	Vertical Depth To (m)
9A	23	3109.3	3110.3	3036.7	3037.7
9B	24	3111.7	3114.3	3039.1	3041.7
	25	3118	3119	3045.4	3046.4
	26	3119.1	3121	3046.5	3048.4
	27	3121.2	3123	3048.6	3050.4
9C	28	3125.5	3128.8	3053	3056.2
9B	29	3130	3134	3057.4	3061.4
	30	3135.5	3137.9	3062.9	3065.3
	31	3142	3143.1	3069.4	3070.5

Fig.27: Star diagram for Fluids 9B of Basker-7 & Fluid 9A & 9B of Basker-6ST1.

Fluid 9**B** in Basker-7 exhibits good comparison with Fluid 9B in Basker 6ST1
Fluid 9A in Basker 6ST1 is marginally lighter.

Basker-7

FLUID#	PEAK#	Measured Depth From (m)	Measured Depth To (m)	Vertical Depth From (m)	Vertical Depth To (m)
9C	10	3556.9	3567.5	2993.8	3002.6
	11	3574.1	3580	3008.1	3013.1
	12	3581.3	3588.2	3014.2	3019.9
9E	13	3616.2	3622.4	3043.5	3048.7
9B	14	3626.2	3630.3	3051.9	3055.3
9C	15	3638.1	3650.8	3061.9	3072.7
9B	16	3652.7	3658.6	3074.4	3079.4
9C	17	3663.6	3675.5	3083.6	3093.8
	18	3677.7	3679.9	3095.7	3097.6
	19	3684	3687.8	3101.1	3104.3
9E	20	3691.3	3694.8	3107.3	3110.4
9C	21	3700.2	3707.5	3115	3121.3
9B	22	3712.6	3724.6	3125.7	3136.2
	23	3731	3737	3137.7	3142.7
	24	3754.5	3762	3157.3	3163.6
9C	25	3774.1	3780	3179.5	3184.7
	26	3787.6	3789.7	3185.1	3186.9
	27	3796.8	3810.7	3199.6	3212
9B	28	3816.5	3826.5	3217.2	3226.1
9C	29	3834.5	3839.9	3233.3	3238.2
9B	30	3850.5	3854.7	3247.7	3251.5
	31	3858	3862	3244.6	3248
	32	3865.5	3869.5	3250.9	3254.3
9E	33	3891.5	3895.5	3273	3276.4



Basker-6ST1

FLUID#	PEAK#	Measured Depth From (m)	Measured Depth To (m)	Vertical Depth From (m)	Vertical Depth To (m)
9A	23	3109.3	3110.3	3036.7	3037.7
9B	24	3111.7	3114.3	3039.1	3041.7
	25	3118	3119	3045.4	3046.4
	26	3119.1	3121	3046.5	3048.4
	27	3121.2	3123	3048.6	3050.4
9C	28	3125.5	3128.8	3053	3056.2
9B	29	3130	3134	3057.4	3061.4
	30	3135.5	3137.9	3062.9	3065.3
	31	3142	3143.1	3069.4	3070.5

Fig.28: Star diagram for Fluids 9C of Basker-7 & Fluid 9C of Basker-6ST1.

Fluid 9**C** in Basker-7 exhibits good comparison with Fluid 9C in Basker 6ST1

ANNEXES-1

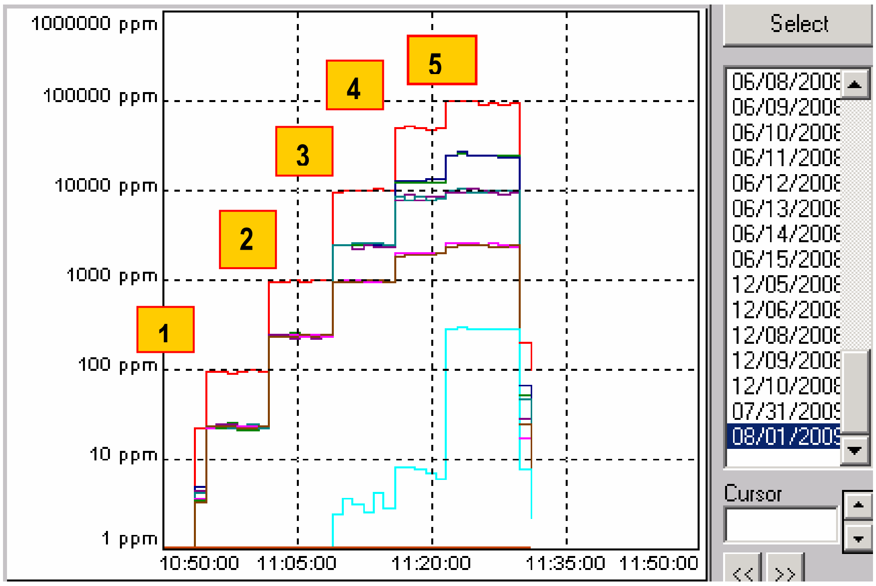
Calibration Report

A. GENERAL INFORMATION			
DATE:	1st Aug 2009	OPERATOR NAME:	Roshan/Aroop
CLIENT:	Anzon	WELL:	Basker-7
RIG NAME:	Ocean Patriot	CALIBRATION FILE:	4A7470C6.CAL
MS NUMBER:	1261763	GC NUMBER:	1261856

B. PROCEDURE INFORMATION

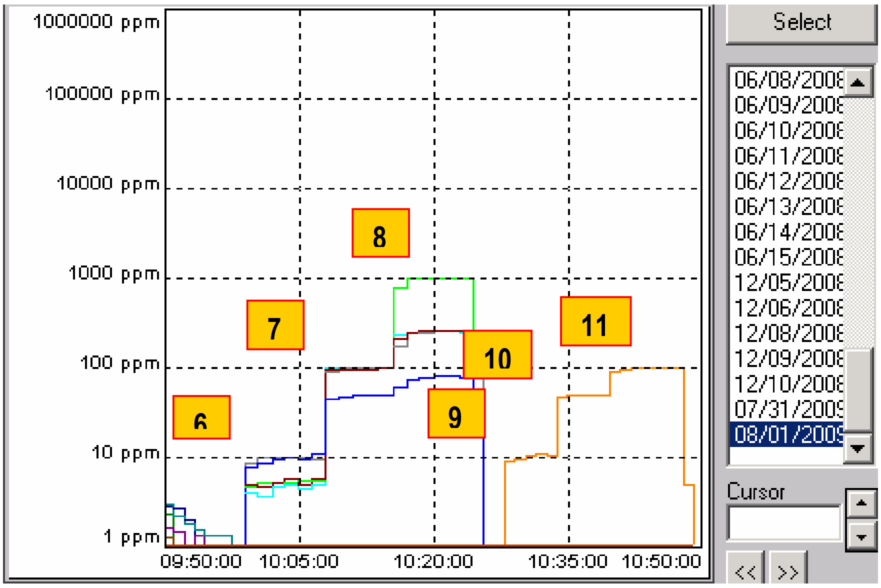
1. Prior to drilling 8½" section of Basker-7, a GC-MS calibration check was performed.
2. An analysis cycle of 90 sec, oven temperature at 82°C and Air Vector at 4.0 bars was used to calibrate from C1 up to C8.
3. The results are recorded and screenshots of the chromatograms were taken.

C. REAL-TIME PLOT



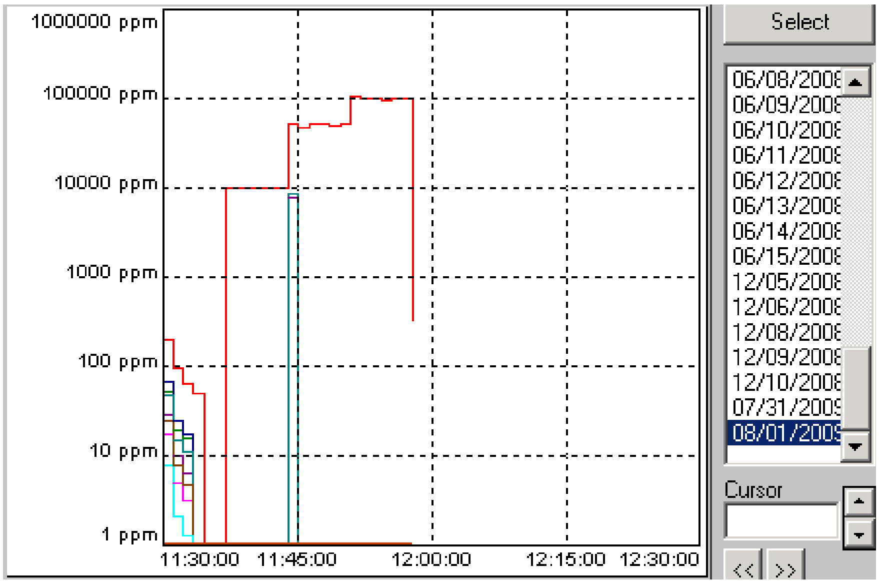
1. 100 ppm C1 to C5 gas calibration mixture.
2. 1000 ppm C1 to C5 gas calibration mixture
3. 10000 ppm C1 to C5 gas calibration mixture.
4. 49900 ppm C1 to C5 gas calibration mixture.
5. 100000 ppm C1 to C6 gas calibration mixture.

Real time screenshot of C1 to C6 gas mixtures



6. 5 ppm C6H6 gas calibration Mixture
7. 100 ppm C6H6 gas calibration Mixture
8. 1000 ppm C6H6 gas calibration Mixture
9. 100 ppm CO2 gas calibration mixture. (C7H14 – 10 ppm)
10. 10000 ppm CO2 gas calibration mixture. (C7H14 – 52 ppm)
11. 100000 ppm CO2 gas calibration mixture. (C7H14 –103)ppm)

Real time screenshot of Benzene and CO2 gas mixtures



12.	10000 ppm C1 Calibration gas
13.	50000 ppm C1-C5 Calibration mixture
14.	100000 ppm C1 Calibration Gas

Real time screenshot of M13 (C1 gas mixtures)

***For 5ppm concentration, % Error margin and STD Deviation % are set at +/-20**
****For 10ppm concentration, % Error margin and STD Deviation% are set at +/-10**
For higher concentrations, % Error margin and STD Deviation% are set at +/-5

100ppm C1-C5	Lot # 98719A				Validity date: Oct 2010			
	Theoretical	Actual 1	Actual 2	Actual 3	Actual 4	Average	Theo/Avge	% Error	Std Deviation %
C1	99.4	94.2	94.7	94.3	100.0	96	1.04	-3.62%	2.93
C2	24.4	24.3	22.1	24.1	23.5	24	1.04	-3.69%	4.23
C3	24.7	22.9	23.5	24.1	24.2	24	1.04	-4.15%	2.54
iC4	24.3	23.1	24.5	24.3	24.0	24	1.01	-1.34%	2.58
nC4	25.1	23.8	23.6	24.1	24.7	24	1.04	-4.18%	1.99
iC5	24.5	22.7	23.5	24.0	23.8	24	1.04	-4.08%	2.43
nC5	24.6	24.1	23.4	23.1	23.3	23	1.05	-4.57%	1.85

1000ppm C1-C5	Lot # 98524A				Validity date: Sept 2010				
	Theoretical	Actual 1	Actual 2	Actual 3	Actual 4	Average	Theo/Avge	% Error	Std Deviation %
C1	1000	974	1001	968	1024	992	1.01	-0.83%	2.61
C2	250	237	258	244	238	244	1.02	-2.30%	3.96
C3	250	250	236	244	242	243	1.03	-2.80%	2.38
iC4	250	242	241	241	240	241	1.04	-3.60%	0.34
nC4	250	235	253	238	252	245	1.02	-2.20%	3.81
iC5	250	237	243	236	242	240	1.04	-4.20%	1.47
nC5	250	239	238	242	238	239	1.04	-4.30%	0.79

1% C1-C5	Lot # 98523				Validity date: Sept 2010				
	Theoretical	Actual 1	Actual 2	Actual 3	Actual 4	Average	Theo/Avge	% Error	Std Deviation %
C1	10000	9995	9793	9975	10388	10038	1.00	0.38%	2.50
C2	2510	2478	2450	2469	2466	2466	1.02	-1.76%	0.47
C3	2500	2504	2534	2437	2439	2479	1.01	-0.86%	1.95
iC4	2500	2470	2369	2397	2367	2401	1.04	-3.97%	2.01
nC4	2500	2414	2600	2520	2527	2515	0.99	0.61%	3.04
iC5	1000	985	1002	964	975	982	1.02	-1.85%	1.64
nC5	1000	970	963	982	991	977	1.02	-2.35%	1.27

5% C1-C5	Lot # 98588				Validity date: Sept 2010				
	Theoretical	Actual 1	Actual 2	Actual 3	Actual 4	Average	Theo/Avge	% Error	Std Deviation %
C1	49900	48180	50819	49883	47994	49219	1.01	-1.36%	2.77
C2	12500	12209	12052	11828	12121	12053	1.04	-3.58%	1.35
C3	12500	12441	13036	12653	13232	12841	0.97	2.72%	2.79
iC4	8510	7890	8468	7883	8471	8178	1.04	-3.90%	4.12
nC4	8500	8467	7900	8685	8107	8290	1.03	-2.47%	4.25
iC5	2000	1980	2060	2016	1966	2006	1.00	0.28%	2.09
nC5	2000	1860	1954	1909	1968	1923	1.04	-3.86%	2.54

10% C1-C6	Lot # 98673					Validity date: Sept 2010			
	Theoretical	Actual				Average	Theo/Avge	% Error	Std Deviation %
		1	2	3	4				
C1	100022	97028	94350	97799	95730	96227	1.04	-3.79%	1.57
C2	25000	24976	24007	24117	24490	24398	1.02	-2.41%	1.79
C3	25000	26752	24730	24516	24274	25068	1.00	0.27%	4.54
iC4	10000	9600	9521	9960	9448	9632	1.04	-3.68%	2.36
nC4	10000	10472	9896	9634	9956	9990	1.00	-0.11%	3.51
iC5	2500	2623	2371	2486	2523	2501	1.00	0.03%	4.16
nC5	2500	2428	2426	2415	2335	2401	1.04	-3.96%	1.85
nC6	297	297	288	293	290	292	1.02	-1.68%	1.34

1% C1	Lot # 98523					Validity date: Sept 2010			
	Theoretical	Actual				Average	Theo/Avge	% Error	Std Deviation %
		1	2	3	4				
C1 M13	10000	10018	10119	9914	9735	9946.5	1.01	-0.54%	1.65

5% C1	Lot # 98588					Validity date: Sept 2010			
	Theoretical	Actual				Average	Theo/Avge	% Error	Std Deviation %
		1	2	3	4				
C1 M13	49900	50741	50292	49497	50173	50175.8	0.99	0.55%	1.03

10% C1	Lot # 98673					Validity date: Sept 2010			
	Theoretical	Actual				Average	Theo/Avge	% Error	Std Deviation %
		1	2	3	4				
C1 M13	100022	101106	98451	97541	100378	99369.0	1.01	-0.65%	1.67

5ppm C6H6	Lot # 99484					Validity date: Nov 2010			
	Theoretical	Actual				Average	Theo/Avge	% Error	Std Deviation %
		1	2	3	4				
C6H6 *	5.2	5.4	5.4	5.5	5.6	5	0.95	5.00%	1.76
nC6 *	4.5	4.7	5.0	4.6	5.1	5	0.93	7.61%	5.32
nC7 *	4.9	5.4	5.9	5.2	5.9	6	0.88	13.72%	6.47
nC8 **	9.9	9.6	10.1	9.7	11.0	10	0.98	1.94%	6.39
C7H8 **	10.5	10.0	10.2	10.2	9.9	10	1.04	-4.12%	1.55

100ppm C6H6	Lot # 96056					Validity date: May 2010			
	Theoretical	Actual				Average	Theo/Avge	% Error	Std Deviation %
		1	2	3	4				
C6H6	100	101	100	100	102	101	0.99	0.68%	0.82
nC6	101	101	99	99	102	100	1.01	-1.09%	1.52
nC7	99.8	98	98	98	101	99	1.01	-1.05%	1.39
nC8	50.6	49	50	50	51	50	1.02	-1.88%	2.07
C7H8	101	100	99	101	102	100	1.01	-0.77%	1.07

1000ppm C6H6	Lot # 97115				Validity date: June 2010			
	Theoretical	Actual				Average	Theo/Avge	% Error	Std Deviation %
		1	2	3	4				
C6H6	1000	1005	1019	1013	1012	1012	0.99	1.21%	0.58
nC6	252	254	257	255	253	255	0.99	1.06%	0.53
nC7	254	259	262	259	259	260	0.98	2.33%	0.56
nC8	75.8	74	81	81	79	79	0.96	3.79%	4.07
C7H8	251	254	261	262	257	258	0.97	2.97%	1.42

100ppm CO2	Lot # 94698A				Validity date: Nov 2010				
	Theoretical	Actual				Average	Theo/Avge	% Error	Std Deviation %
		1	2	3	4				
C7H14 *	10	9.7	10.6	11.0	10.6	10	0.96	4.70%	5.34

1% CO2	Lot # 95126				Validity date: Aug 2010				
	Theoretical	Actual				Average	Theo/Avge	% Error	Std Deviation %
		1	2	3	4				
C7H14	52	50.2	50	51.3	51.1	51	1.03	-2.60%	1.27

10% CO2	Lot # 94697A				Validity date: Apr 2010				
	Theoretical	Actual				Average	Theo/Avge	% Error	Std Deviation %
		1	2	3	4				
C7H14	103	100.2	99.1	101.5	101.1	100	1.03	-2.45%	1.06

Integrity test Report

A. GENERAL INFORMATION			
DATE:	2nd Aug 2009	OPERATOR NAME:	Roshan/Aroop
CLIENT:	Anzon	WELL:	Basker-7
RIG NAME:	Ocean Patriot	CALIBRATION FILE:	4A7470C6.CAL
MS NUMBER:	1261763	GC NUMBER:	1261856

B. PROCEDURE INFORMATION

The gas integrity test was performed During POOH at 3448m in the 8½" Hole.

A check has to be performed using a jerrycan. The aim of this test is to check the integration process and the calibration on a wide range of concentrations.

The jerrycan is connected before the flow restrictor in the filtration assembly of the Flair extractor.

The jerrycan has a dilution port to displace the gas with air and to maintain a constant pressure through the test.

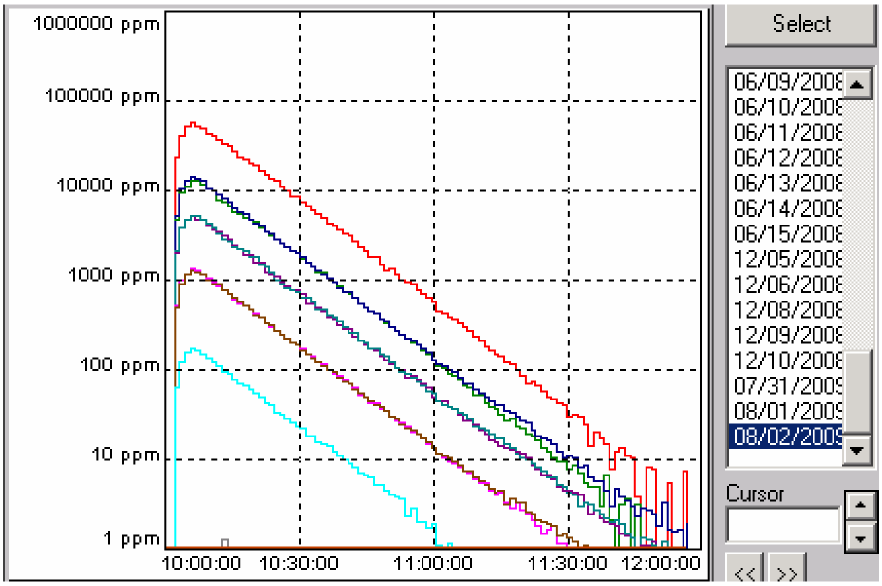
It is ensured that the jerrycan is empty by checking that the MS records almost 0 ppm of gas.

A bottle of 10 % C1 mixture (C1 - C6) is connected to the jerrycan entry and fully opened for five seconds.

The response on the MS must be linear with good integration for each component until very low values are reached.

The computation is checked based on ratios to verify the consistency from high to low range and to ensure the error is within +/- 5% of the theoretical ratios.

C. REAL-TIME PLOT



D. RESULTS

10% C1-C6	Lot # 98673				Validity date: Sept 2010		
	Theoretical	Actual			Average	Theo/Avge	% Error
		1 high	2 medium	3 medium	4 low		
C1/C2	4.001	4.02	4.03	3.90	4.08	4.01	1.00	0.15%
C1/C3	4.001	4.02	4.09	3.86	3.78	3.94	1.02	-1.60%
C2/C3	1.000	1.00	1.02	0.99	0.93	0.98	1.02	-1.72%
C1/iC4	10.002	10.55	11.06	9.36	9.44	10.10	0.99	0.98%
C1/nC4	10.002	9.94	10.81	10.02	8.39	9.79	1.02	-2.14%
C1/iC5	40.009	40.32	42.90	38.27	37.75	39.81	1.00	-0.49%
C1/nC5	40.009	41.47	42.47	38.27	37.75	39.99	1.00	-0.04%

Mud Background Analysis Report

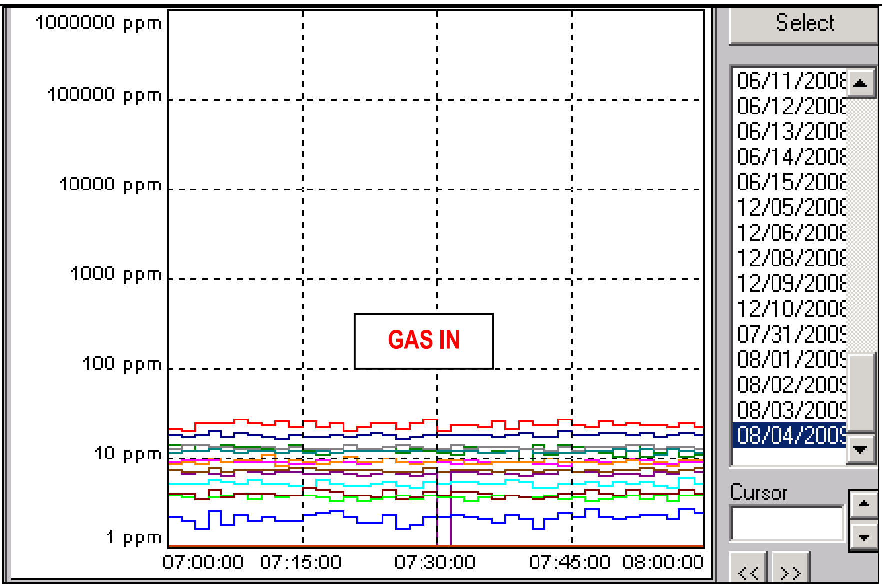
A. GENERAL INFORMATION			
DATE:	4th Aug 2009	**OPERATOR NAME:**	Roshan/Aroop
CLIENT:	Anzon	**WELL:**	Basker-7
RIG NAME:	Ocean Patriot	**CALIBRATION FILE:**	4A7470C6.CAL
MS NUMBER:	1261763	**GC NUMBER:**	1261856
PHASE:	8½”		

B. PROCEDURE INFORMATION

1. The mud background analysis was performed during a trip at 3537m to change Anadrill tools to ascertain the contribution from the WBM and to define an averaged signature.
2. Using FLEX IN, a fresh bucket of mud was taken from active pit, and then the FLEX was switched on and allowed to reach the correct operating temperature and pressure.
3. Once the temperatures and pressures were reached (as per drilling conditions: 90°C and 280 mbar), the FLEX was allowed to work for 1 hours to ascertain the mud background in HC was constant.
4. The results were recorded and screenshots of the chromatograms were taken.

C. MUD PROPERTIES					
MUD TYPE		KCL/KlaStop/Polymer	**Gels 10s/10m**	**Pa**	8/9
MUD Wt.	**sg**	1.14	**R600/R300**	**Rpm**	58/42
FV		51	**R200/R100**	**Rpm**	36/27
PV	**cP**	16	**R6/R3**	**Rpm**	9/7
YP	**Pa**	26	**MUD TEMP IN**	**ºC**	24.7

D. REAL-TIME PLOT

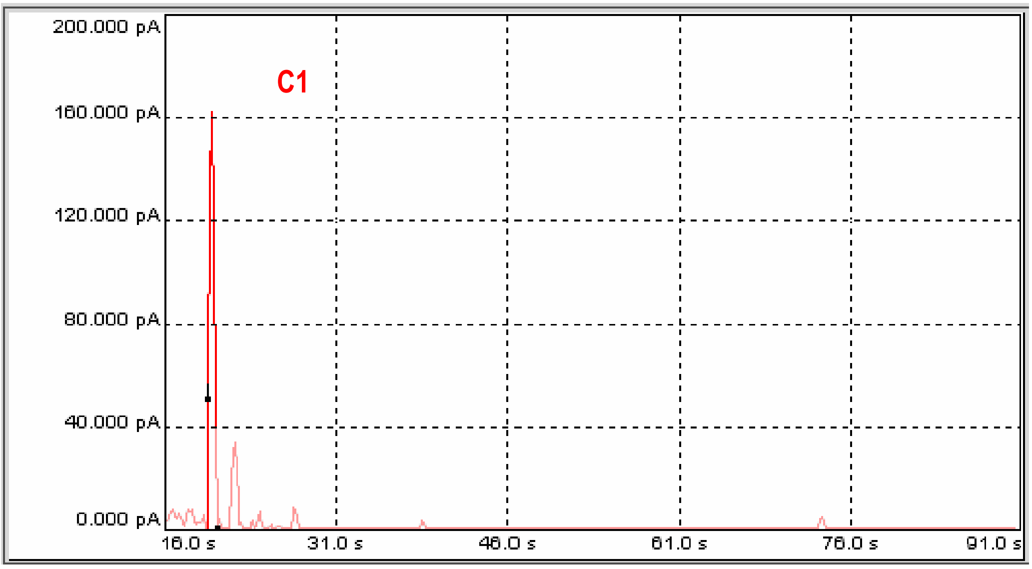


E. RESULTS

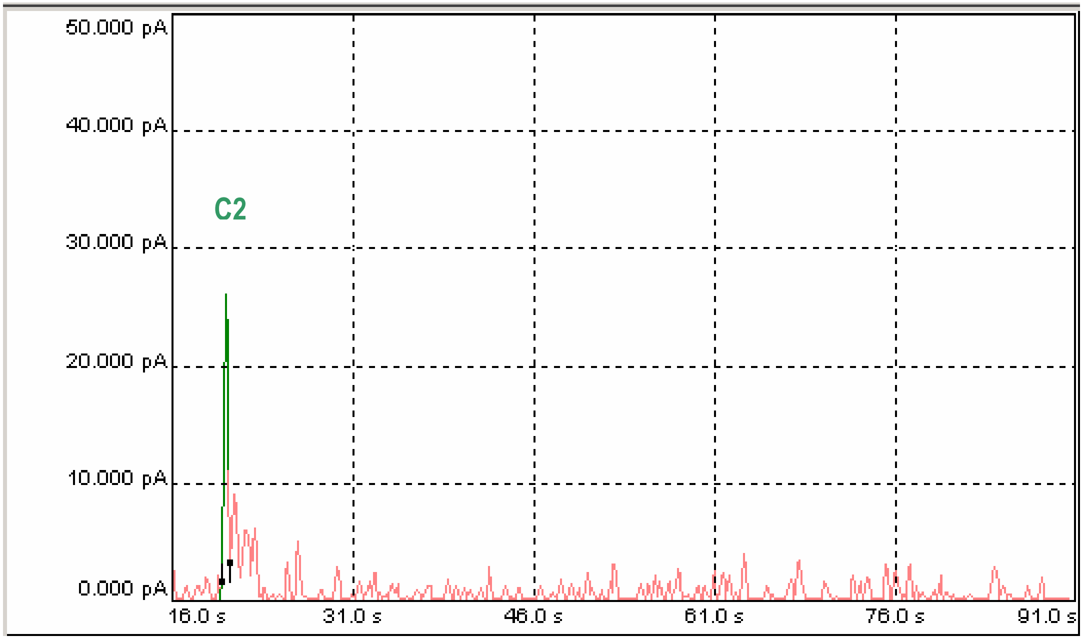
Gas IN	1	2	3	Average Value	Max Value	Min Value
C1	24.15	23.68	24.55	24.13	24.55	23.68
C2	13.25	12.58	12.10	12.64	13.25	12.10
C3	18.25	18.00	18.70	18.32	18.70	18.00
iC4	7.05	6.16	7.00	6.74	7.05	6.16
nC4	12.05	12.05	12.25	12.12	12.25	12.05
iC5	9.30	9.21	9.20	9.24	9.30	9.20
nC5	7.60	7.37	7.70	7.56	7.70	7.37
nC6	5.30	5.37	5.30	5.32	5.37	5.30
nC7	4.20	4.11	4.15	4.15	4.20	4.11
nC8	2.20	2.00	2.20	2.13	2.20	2.00
C6H6	3.90	3.79	3.90	3.86	3.90	3.79
C7H8	13.45	13.47	13.45	13.46	13.47	13.45
C7H14	9.35	9.37	9.25	9.32	9.37	9.25

F. CHROMATOGRAMS

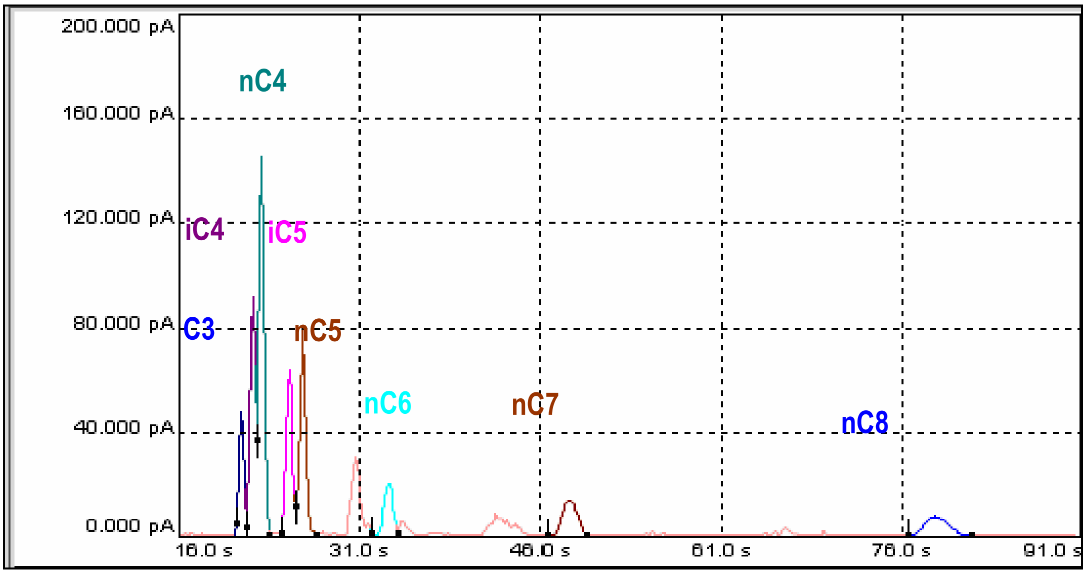
1. Chromatogram for Ion 15

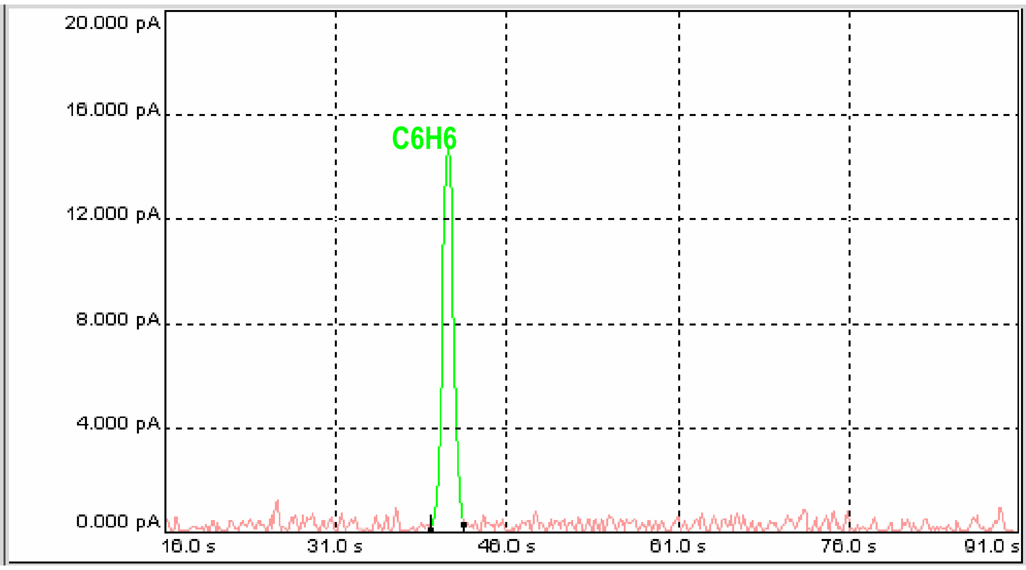


2. Chromatogram for Ion 26

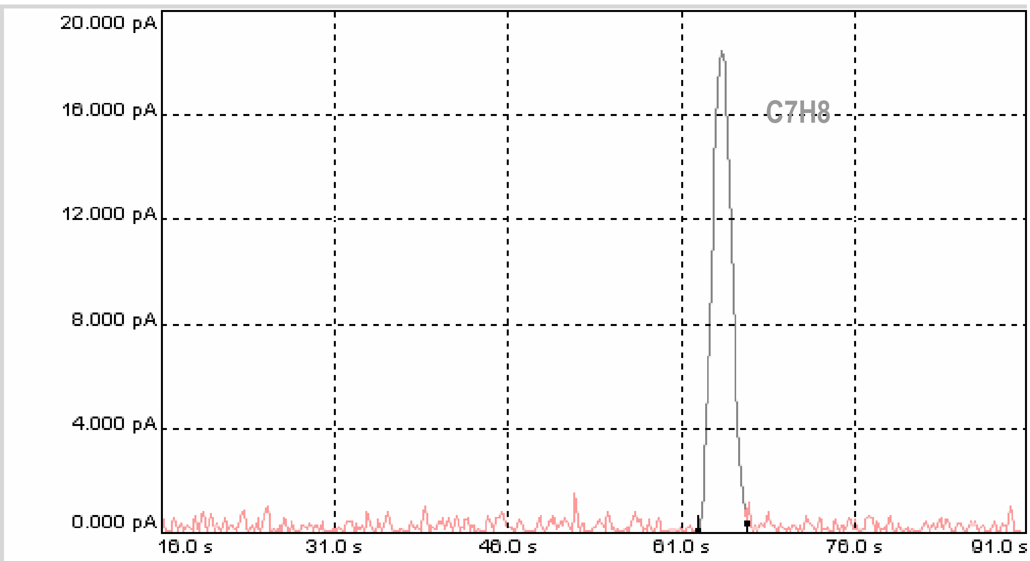


3.Chromatogram for Ion 43

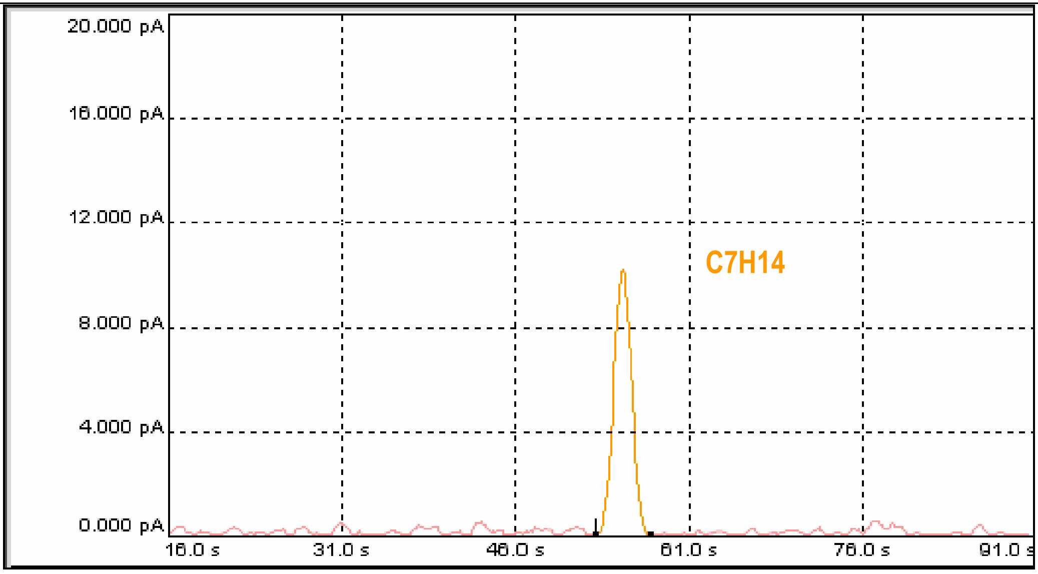




4.Chromatogram for Ion 78



5.Chromatogram for Ion 83



.Chromatogram for Ion 91

G. COMMENTS

The contribution from the KCL polymer water Based mud in use, to the HC readings is:

- High for C1=24.13ppm.
- Medium for C2=12.64ppm, C3=18.32ppm, nC4=12.12ppm & C7H8=13.46ppm.
- Low for iC4=6.74ppm, iC5=9.24ppm, nC5=7.56ppm, nC6=5.32, nC7=4.15ppm, nC8=2.13ppm, C6H6=3.86ppm & C7H14=9.32ppm.

Extraction Efficiency Calibration

The aim of this procedure is to establish the extraction efficiency of the equipment and to correct the gas readings. This allows the operator to finally obtain the real composition of the gas in the mud.

The results presented below were obtained on 05/08/2009 from gas peak at 3824m MD while 8 ½” hole drilling.

Mud Type: WBM. MW: 1.14s g FV:51 PV:16 YP:28 Gel:08/10

Correcting coefficients	C1	C2	C3	iC4	nC4	iC5	nC5
	1.3143	1.3713	1.4745	1.5909	1.6473	1.8350	1.9020